

Quality Testing Optically Contacted Bonds for LIGO Voyager

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Motivation

LIGO's test masses are currently made of many fused silica parts



Image of one of LIGO's test masses from Caltech/MIT/LIGO Lab

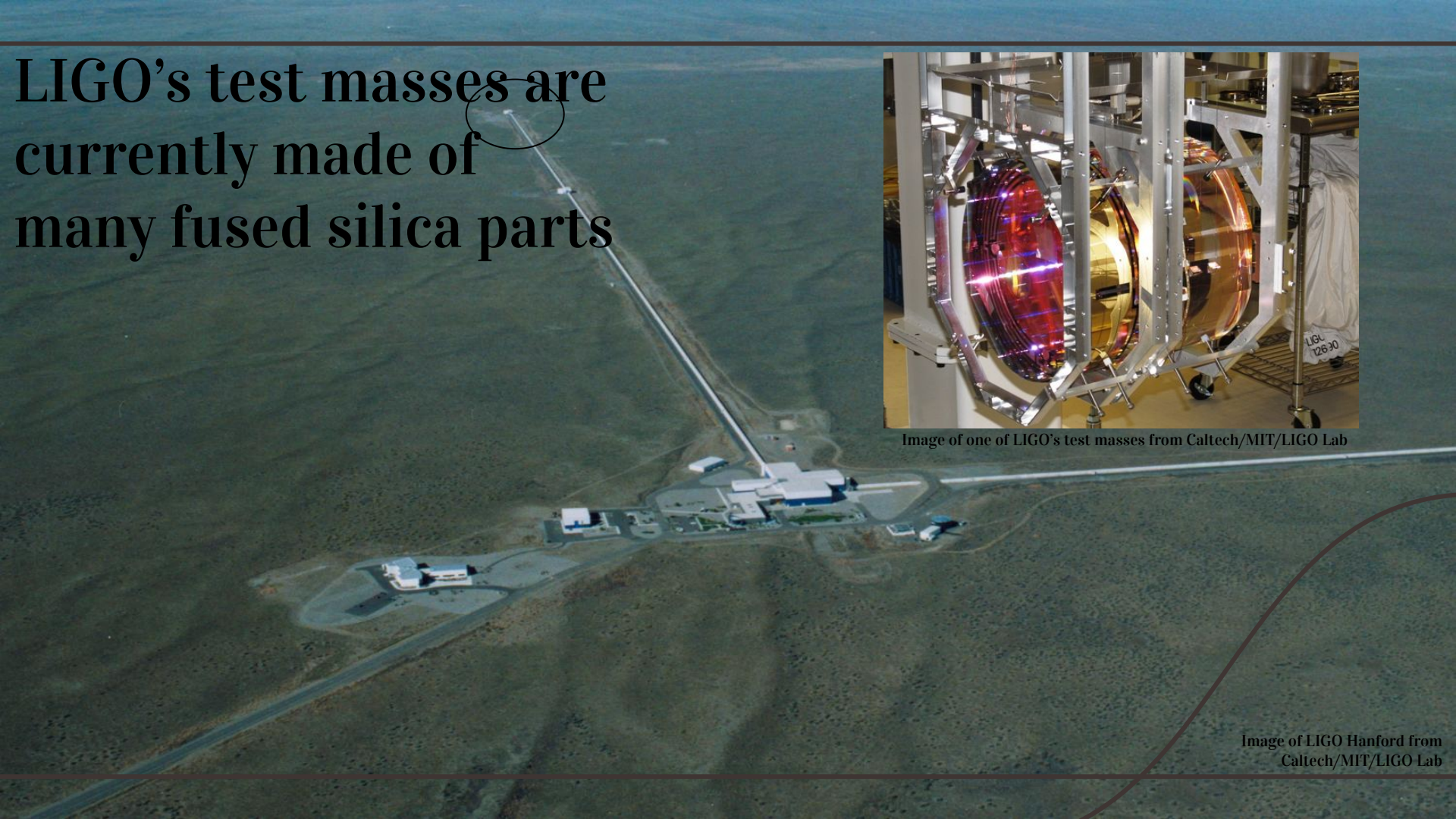


Image of LIGO Hanford from Caltech/MIT/LIGO Lab

The test masses are suspended by ribbons and made out of several smaller pieces which contributes to suspension thermal noise

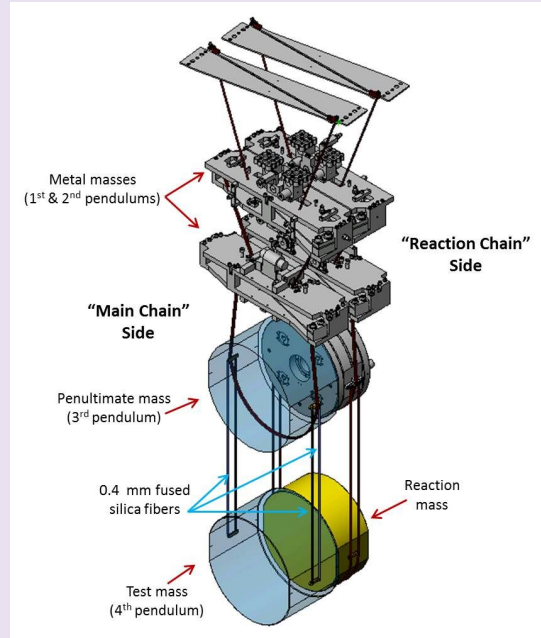


Image of a LIGO quad from IGR, University of Glasgow

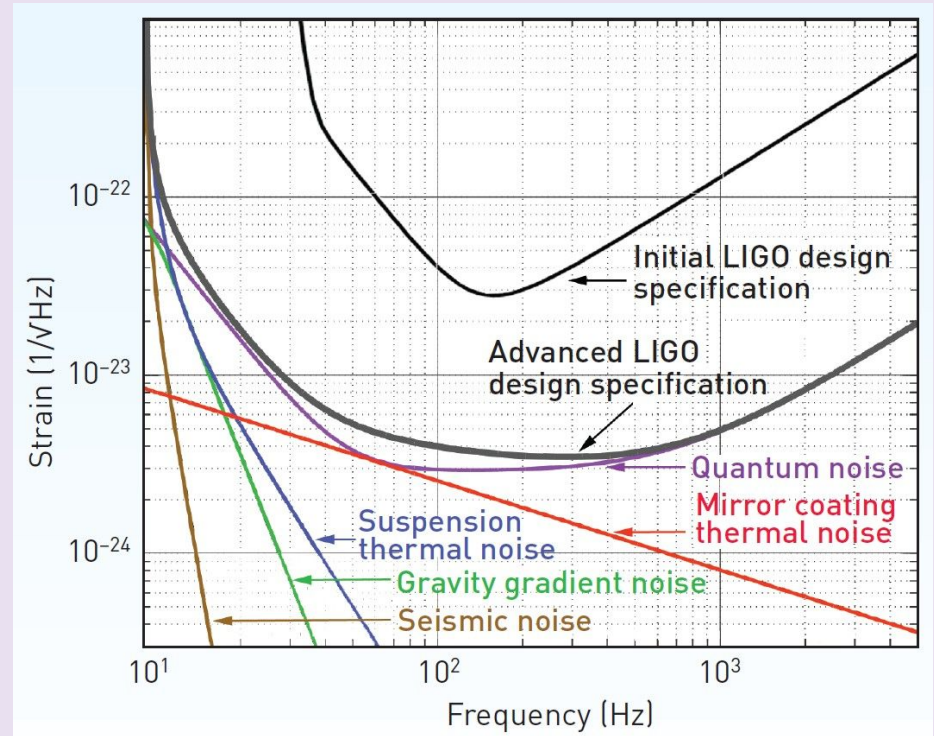
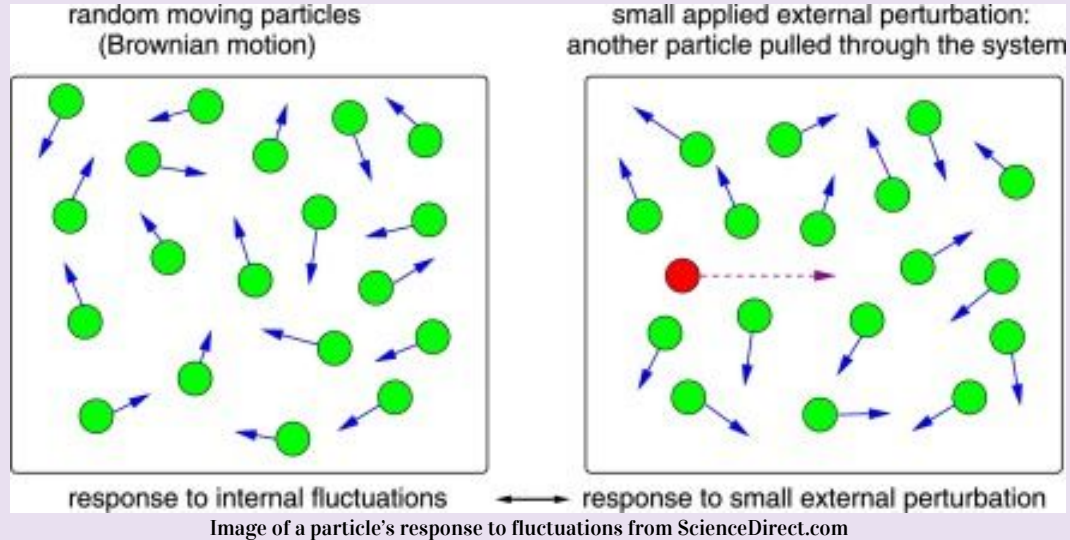


Image of Advanced LIGO principal noise sources as a function of frequency from optica-opn.org

Thermal noise limits the sensitivity of the detector as described by the fluctuation dissipation theorem



Heat dissipation through the interfaces of the mirror parts is a source of fluctuation which causes the mirrors to vibrate

Optically contacted silicon is thought to have low thermal noise but has yet to be tested



Image of optically contacted glass from solarisoptics.eu

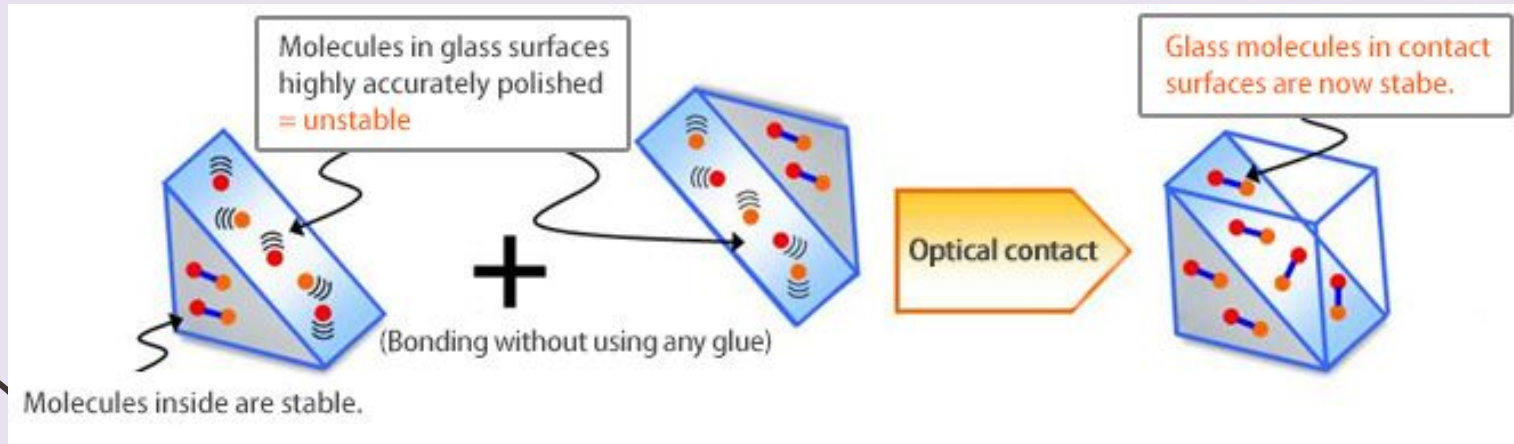
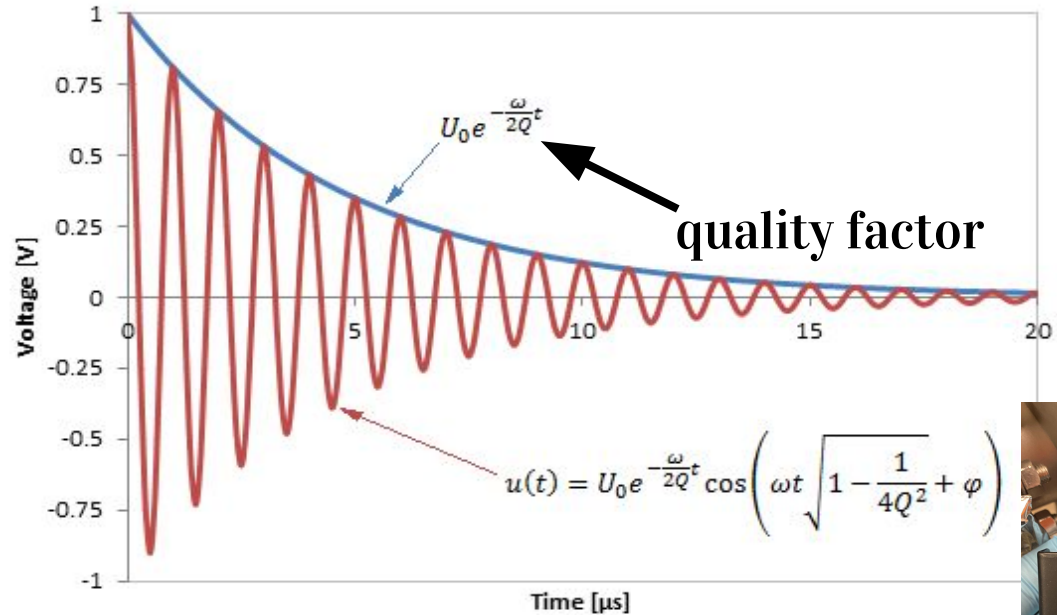
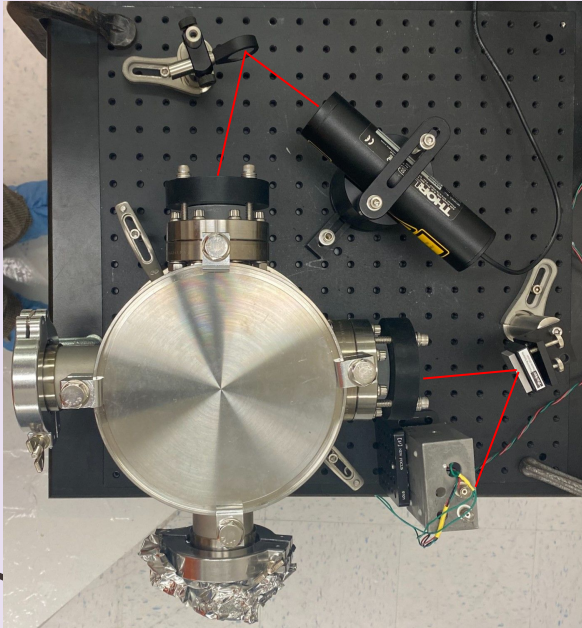


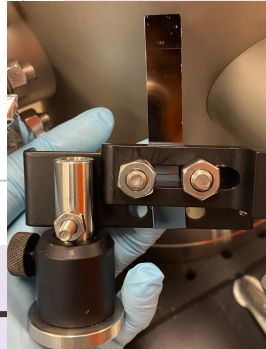
Diagram explaining optically contacting glass from mitsui-om.co.jp

Testing

A high quality factor corresponds to low thermal noise



Graph of a damped oscillation and its fit from giangrandi.ch

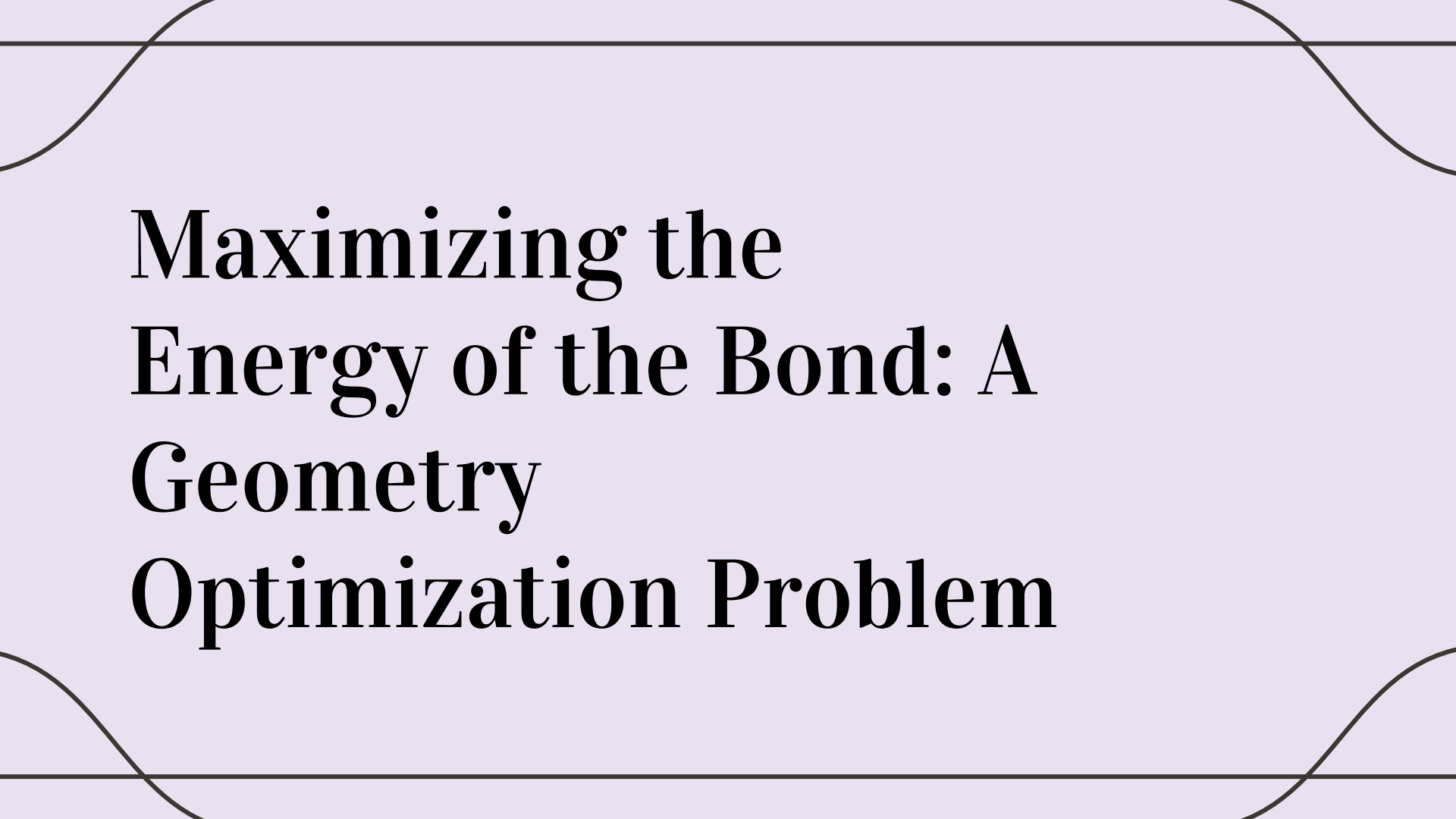


How to find the quality factor of a bond...

$$\frac{1}{Q_{system}} = \sum_{i=1}^n \frac{E_i}{E_{system}} \frac{1}{Q_i}$$

$$\frac{1}{Q_{system}} = \frac{E_{silicon}}{E_{system}} \frac{1}{Q_{silicon}} + \frac{E_{bond}}{E_{system}} \frac{1}{Q_{bond}}$$

...maximize its energy contribution



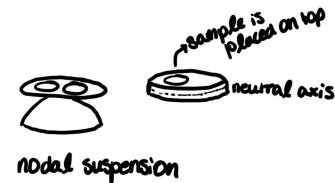
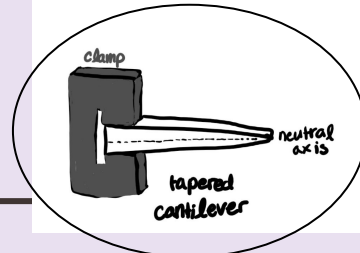
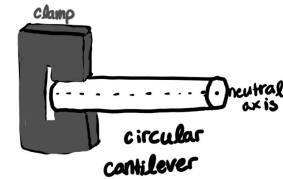
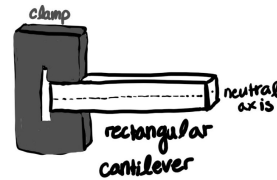
**Maximizing the
Energy of the Bond: A
Geometry
Optimization Problem**

Estimation to Gain an Intuition

Three different cantilever geometries were analyzed in order to find a suitable energy ratio between the bond and the rest of the silicon wafer. The ratio between shear and bending energy was estimated for the geometries shown in figure 1 using the following equations where M is the moment, I is the moment of inertia, l is the length, E is young's modulus, K is a constant that depends on the geometry (1.11 for circular and 0.5 for rectangular sections), V is the traverse shear force, G is the modulus of rigidity, and A is the cross sectional area.

$$\text{constant bending energy} = \frac{M^2 l}{2EI}$$

$$\text{constant traverse shear energy} = \frac{KV^2 l}{2GA}$$



Finite Element Analysis in COMSOL: Pizza Cantilever

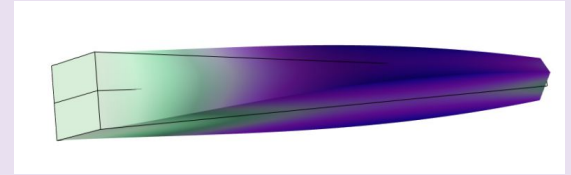


Table 1: Pizza Cantilever Energies.

Eigenfrequency (Hz)	Bulk (N*m)	Shear (N*m)	Total (J)	Shear/Bulk
34557	6.0-13	2.5E-12	1.5E-12	4.2
51994	1.4E-12	5.8E-12	3.6E-12	4.3
1.0385E5	2.8E-12	1.2E-11	7.4E-12	4.3
1.5129E5	5.8E-12	2.8E-11	1.7E-11	4.8
2.1981E5	1.0E-11	4.7E-11	2.8E-11	4.6
* 2.7240E5	2.1E-12	5.6E-10	2.8E-10	270

* is excluded because its shear strain dominates on the edges. We want to maximize the strain at the bond.

Finite Element Analysis in COMSOL: Rectangular Cantilever

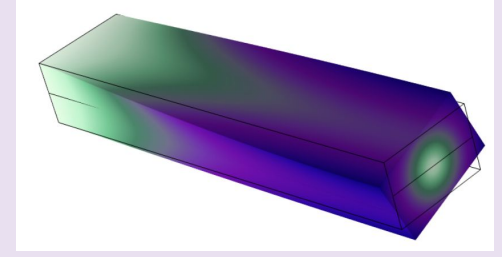
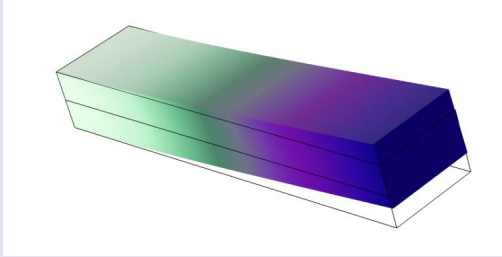


Table 2: Rectangular Cantilever Energies.

Eigenfrequency (Hz)	Bulk (N*m)	Shear (N*m)	Total (J)	Shear/Bulk
20385	2.2E-12	8.6E-12	5.4E-12	3.9
30507	4.8E-12	2.0E-11	1.2E-11	4.2
1.1796E5	7.3E-11	3.3E-10	2.0E-10	4.5
* 1.2326E5	1.4E-12	3.6E-10	1.8E-10	260
1.6250E5	1.3E-10	7.3E-10	4.3E-10	5.4
2.2601E5	5.1E-10	2.1E-9	1.3E-9	4.1

* is excluded because its shear strain dominates on the edges. We want to maximize the strain at the bond.

Finite Element Analysis in COMSOL: Lab Dimensions

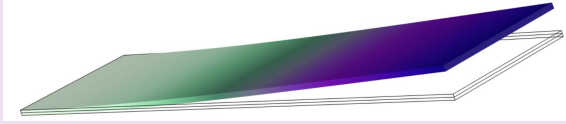


Table 3: Rectangular Cantilever With Lab Dimensions Energies.

Eigenfrequency (Hz)	Bulk (N*m)	Shear (N*m)	Total (J)	Shear/Bulk
1266.0	5.3E-16	1.9E-15	1.2E-15	3.6
7927.1	2.0E-14	7.6E-14	4.8E-14	3.7
* 12012	2.3E-15	1.4E-13	6.9E-14	58
22212	1.6E-13	5.8E-13	3.7E-13	3.6
30433	2.7E-13	1.2E-12	7.4E-13	4.5
36767	3.6E-14	1.2E-12	6.0E-13	3.3

Table 4: Pizza Cantilever With Lab Dimensions Energies.

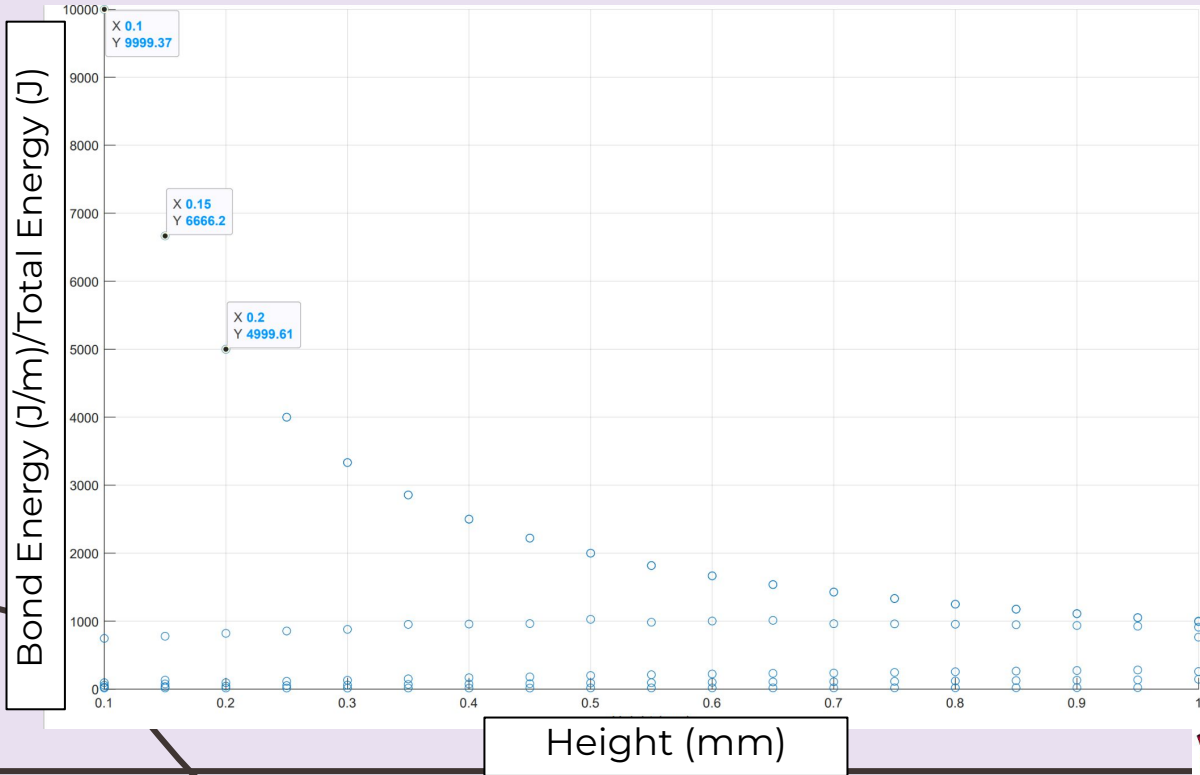
Eigenfrequency (Hz)	Bulk (N*m)	Shear (N*m)	Total (J)	Shear/Bulk
2085.9	1.5E-16	5.9E-16	3.7E-16	4.0
6624.0	8.0E-16	3.2E-15	2.0E-15	4.0
14820	3.4E-15	1.3E-14	8.2E-15	3.9
* 25628	2.6E-15	1.9E-13	9.9E-14	75
26899	1.1E-14	4.0E-14	2.5E-14	3.8
42943	2.6E-14	9.8E-14	6.2E-14	3.7

* is excluded because its shear strain dominates on the edges. We want to maximize the strain at the bond.

Selecting the Geometry: Results

- The pizza cantilever had a higher shear/bulk ratio than the rectangular cantilever at the frequency I estimated
- The rectangular cantilever had the highest shear/bulk ratio overall
- The ratio was highest when the thickness of the cantilever was minimized

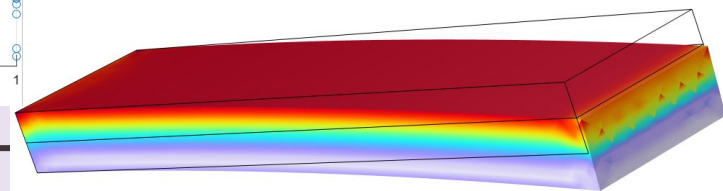
Optimizing the Dimensions



Added a boundary load and ran a stationary study to find the von Mises stress

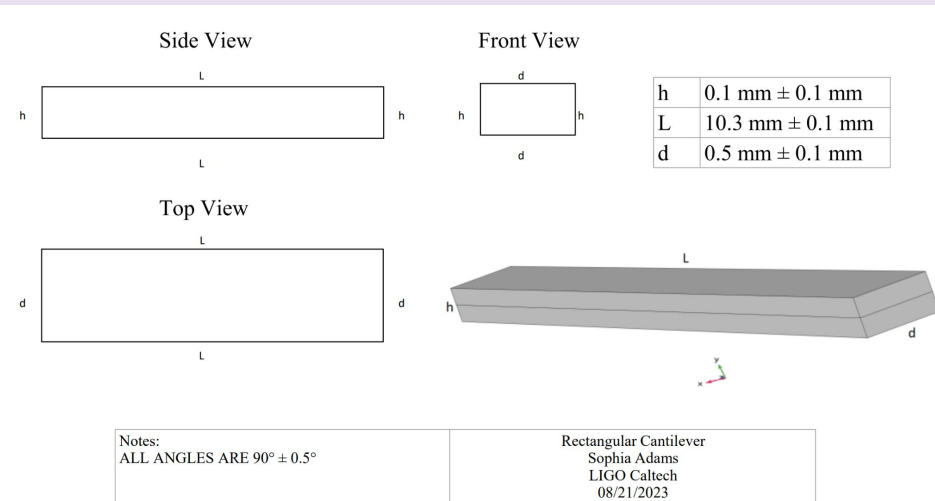
Plotted the shear/bulk ratio and energy per length of the inner surface divided by total energy for different widths/heights/lengths and eigenfrequencies

Simultaneous parameter estimation with fminsearch



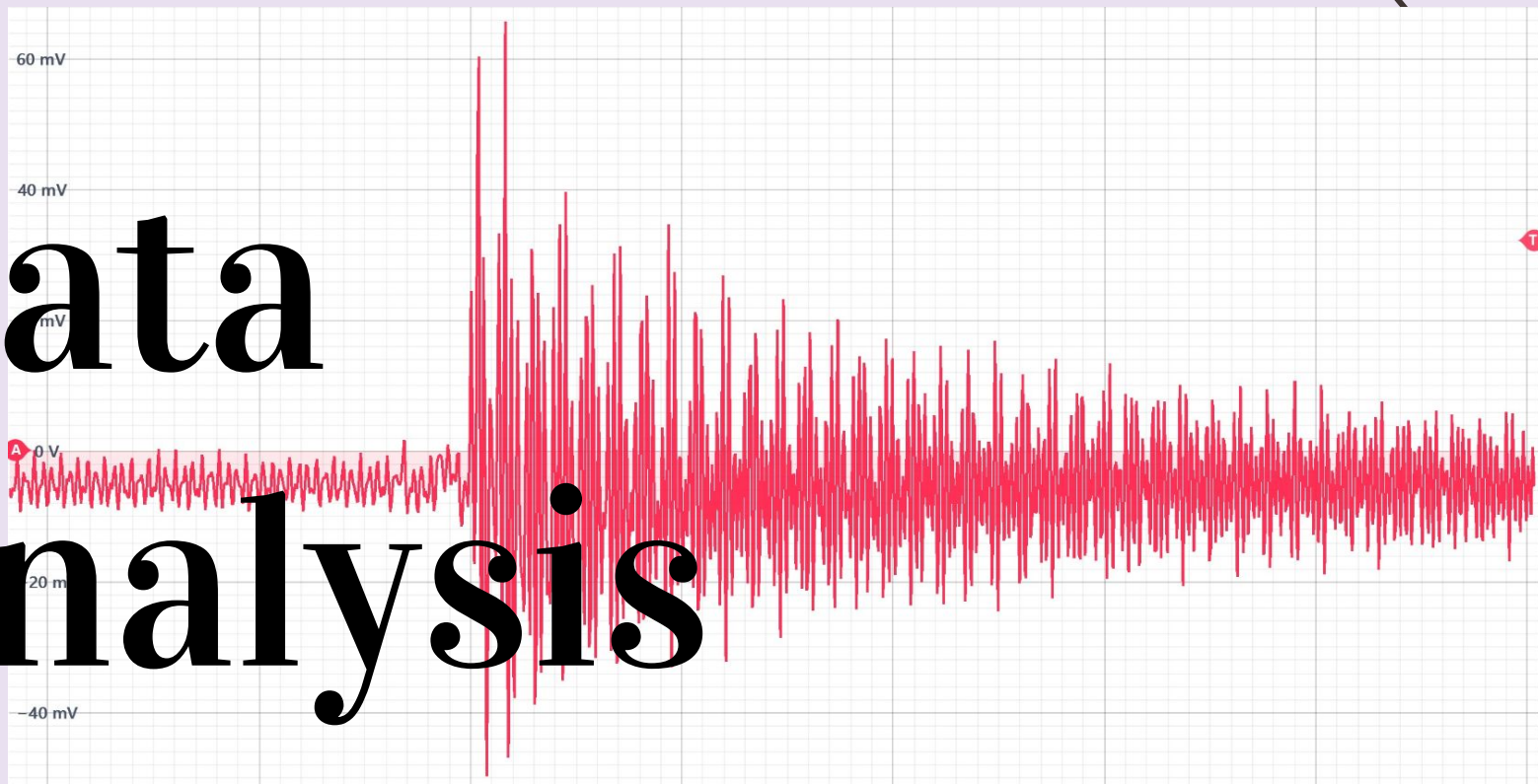
Optimizing the Dimensions: Results

- The stress in the bond was highest when the load was applied normal to the end surface of the cantilever. This was confirmed by an analysis of the eigenfrequencies
- The height of the cantilever should be made as small as possible (in the .1 mm range)
- The width and length should also be minimized but do not have as much of an affect
- The width affected the ratio more and should be 0.5033 mm
- The length should be 1.0313 cm

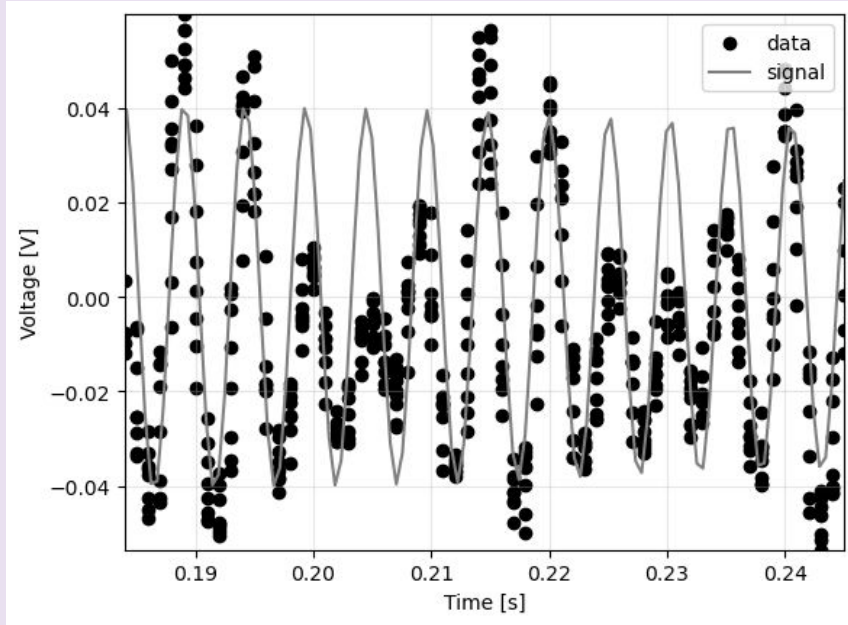


Data

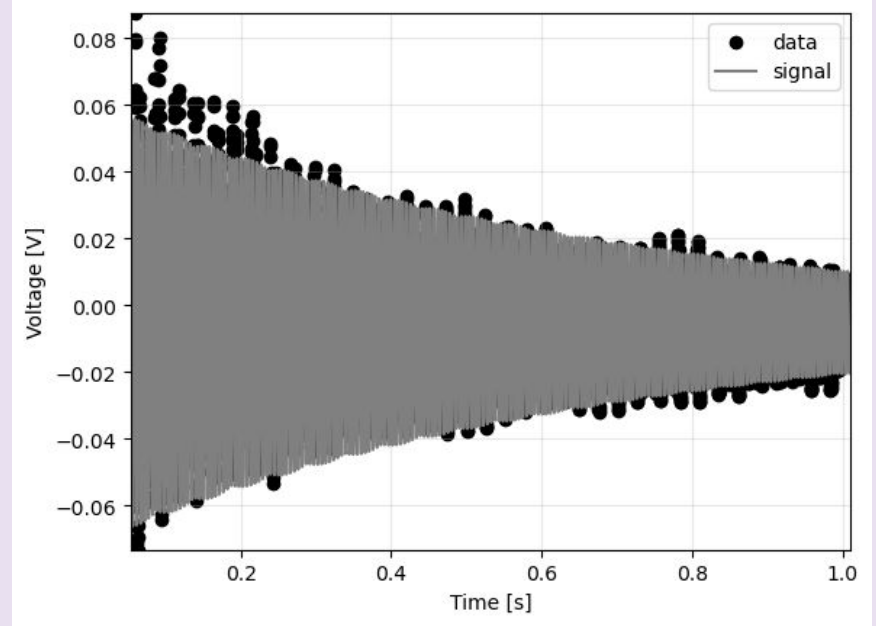
Analysis



1. Educated Guess

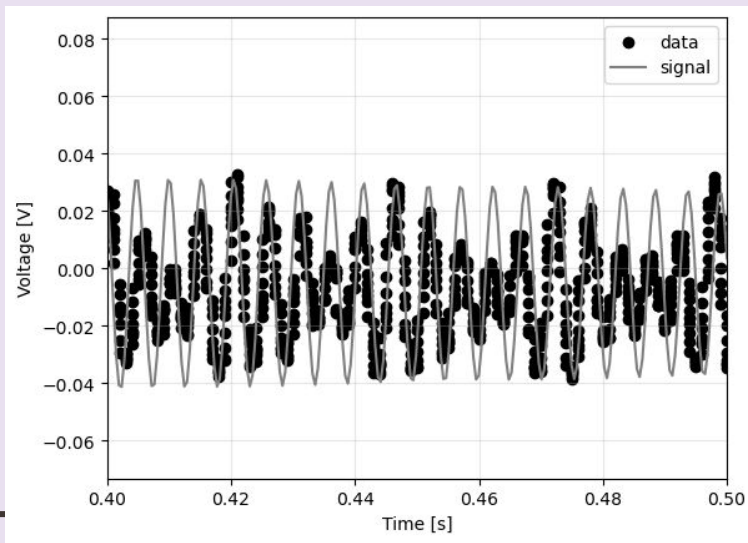
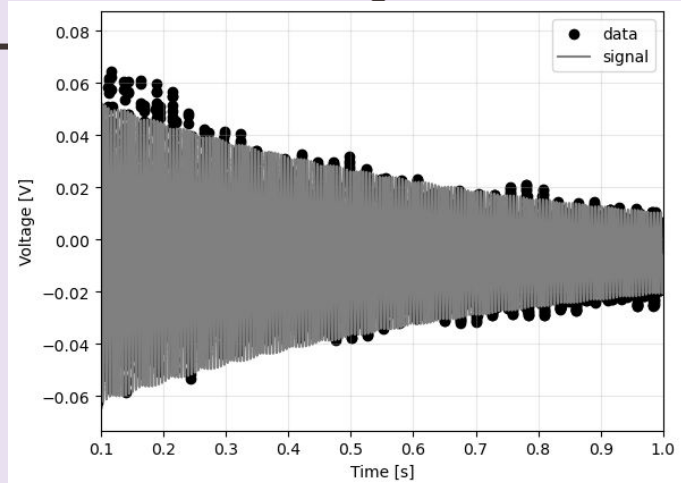
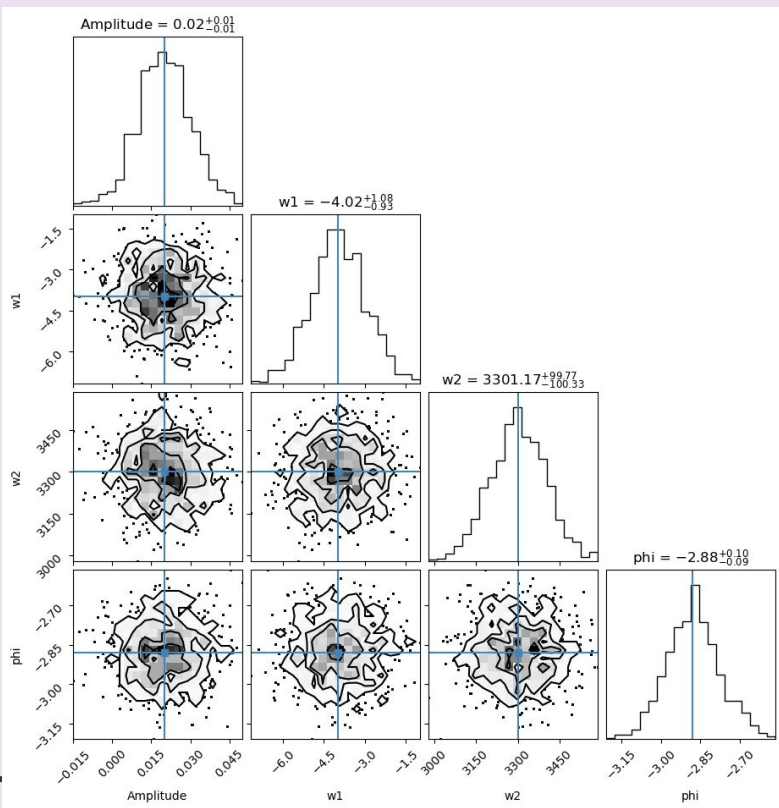


Frequency

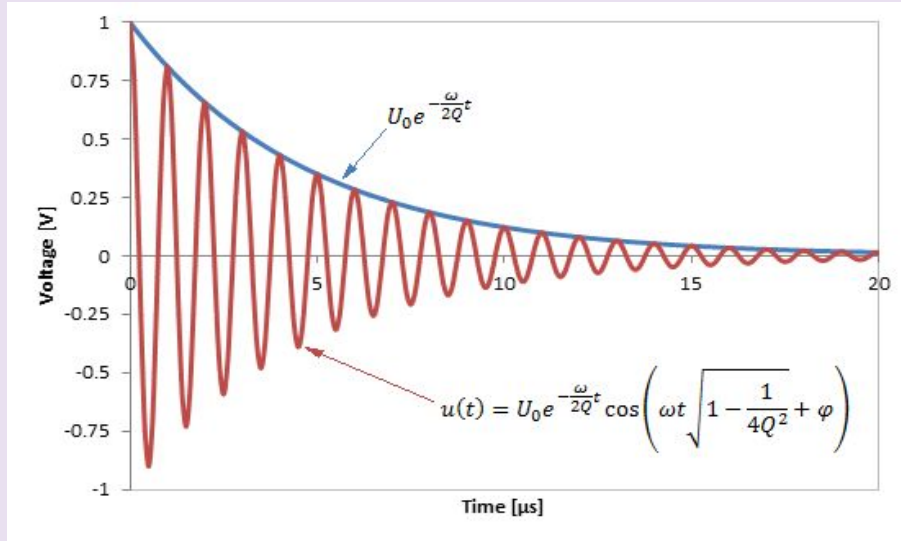


Rate of Decay

2. Bayesian Monte Carlo Method



3. Calculate Q



$$Q = \frac{\sqrt{\left(\frac{w_2}{w_1}\right)^2 + 1}}{2}$$

$$w_1 = -\frac{\omega}{2Q}$$

$$w_2 = \omega \sqrt{1 - \frac{1}{4Q^2}}$$

$$= 470 \pm 70$$

Summary

01

Problem

How to find the Q of
a bond



02

Development

Brainstorm possible
geometries based
on mathematical
inference
Geometry
optimization using
COMSOL
Mechanical drawing



03

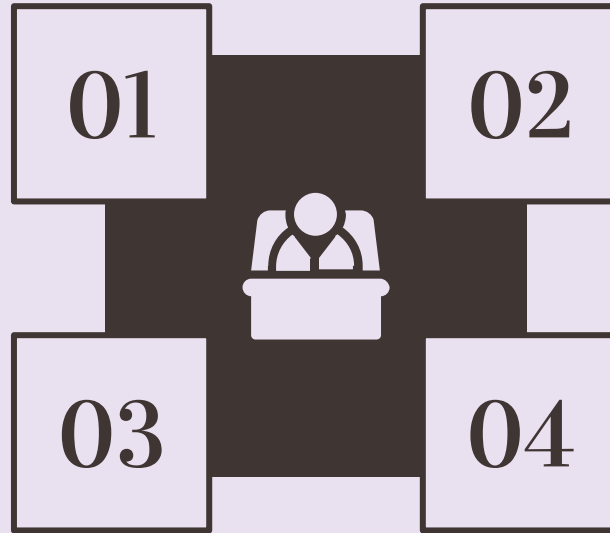
**Data
Collection
and Analysis**

Optical engineering
to make an optical
lever
Parameter
estimation using
Bayesian inference

Future Work

Test bonded
silicon

Cryogenic
temperature
/vacuum



Test under
stress

Model
clamp loss

References

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