

Custom polish figure for O4 ETMs

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Why a custom figure for ETMs?

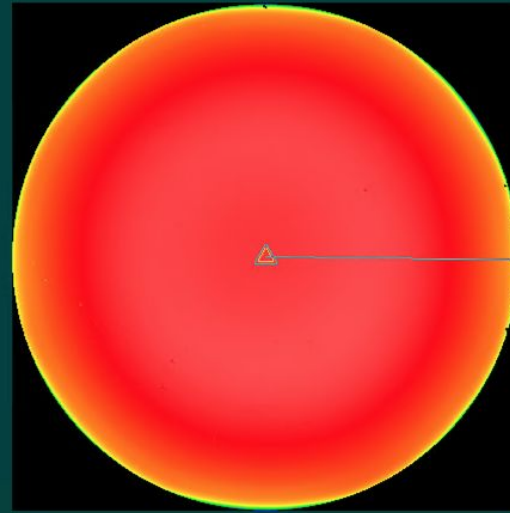
- Maximize loss for 7th order mode with minimum impact on round trip losses just in case we still have coating point absorbers. Systems Meeting 9/30/20
 - G2001747 for the study of the best figure for 7th order mode suppression
 - G2001747 pg 22 for the (small) loss penalty we will have in case there are no point absorbers.

Ion Beam Sputtered (IBS) coatings are deposited by placing the optic within a plume of coating material.

aLIGO coatings were deposited in a planetary system using a coating mask that limited the deposition rate in the center of the optic in order to distribute the material evenly. This proved quite difficult to get exactly right.

We will use a simple turntable movement for coating deposition.

LIGO "After coating" minus "Before Coating" Pen-ITM02



+28.56

nm

Change after Coating:
Subtracting "before coating" from "after coating" measurement of Pen-ITM02. The coating was deposited with no mask. Details and Data at T2000643

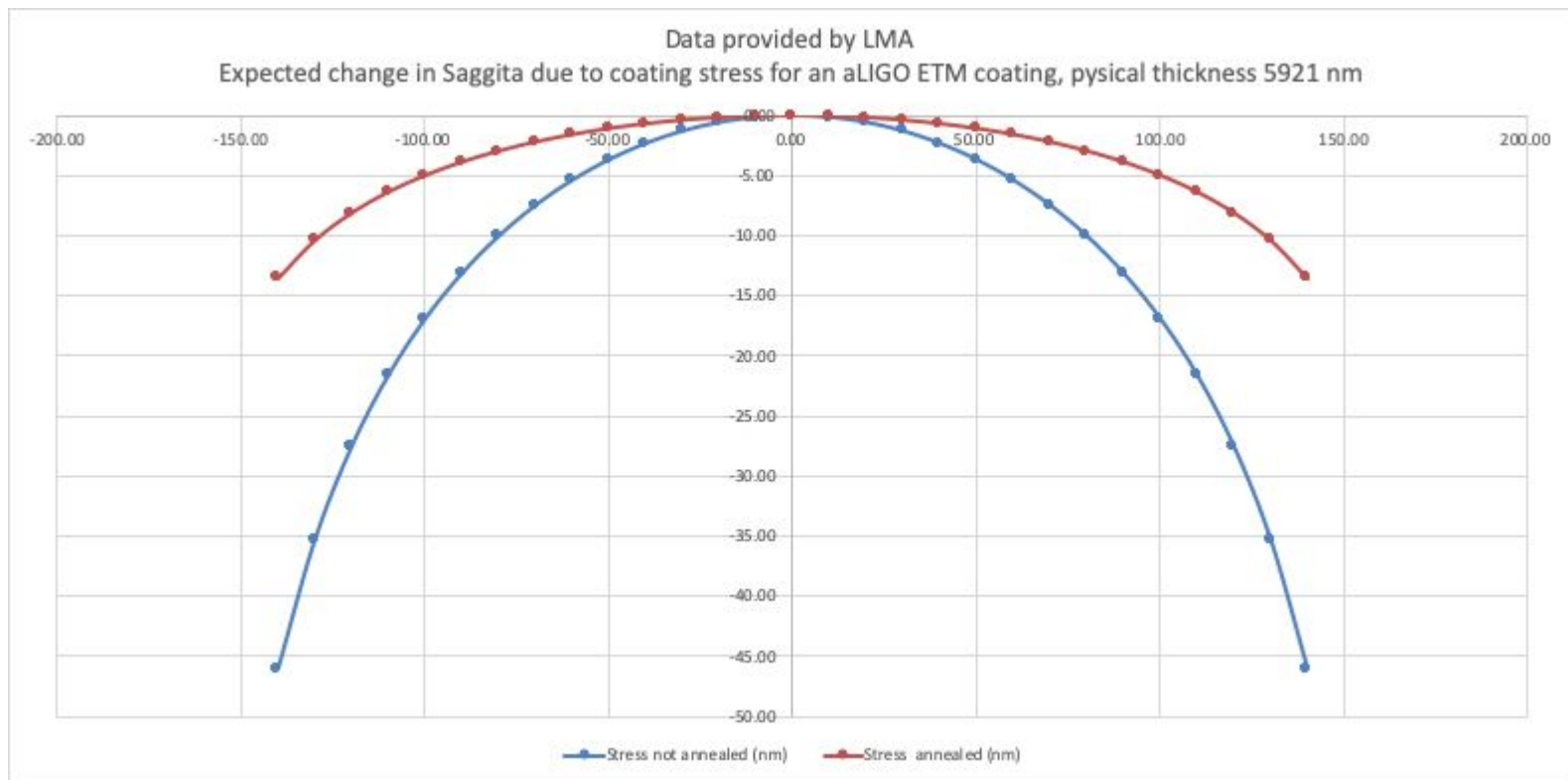
PV	228.882	nm	Removed: PST TLT
rms	24.068	nm	Trimmed: 0
Power	-73.496	nm	Filter: Off
Size X	320.50	mm	Size Y 320.505 mm
TiltX	-1.920	nm	Tref.X -1.415 nm
Tilty	0.440	nm	Tref.Y -1.490 nm
Ast.X	-0.902	nm	2Ast.X 1.648 nm
Ast.Y	-2.585	nm	2Ast.Y -1.665 nm
ComaX	-1.099	nm	2ComaX -0.743 nm
ComaY	0.775	nm	2ComaY -0.716 nm
Sph Ab	-20.949	nm	2Sph Ab -5.219 nm



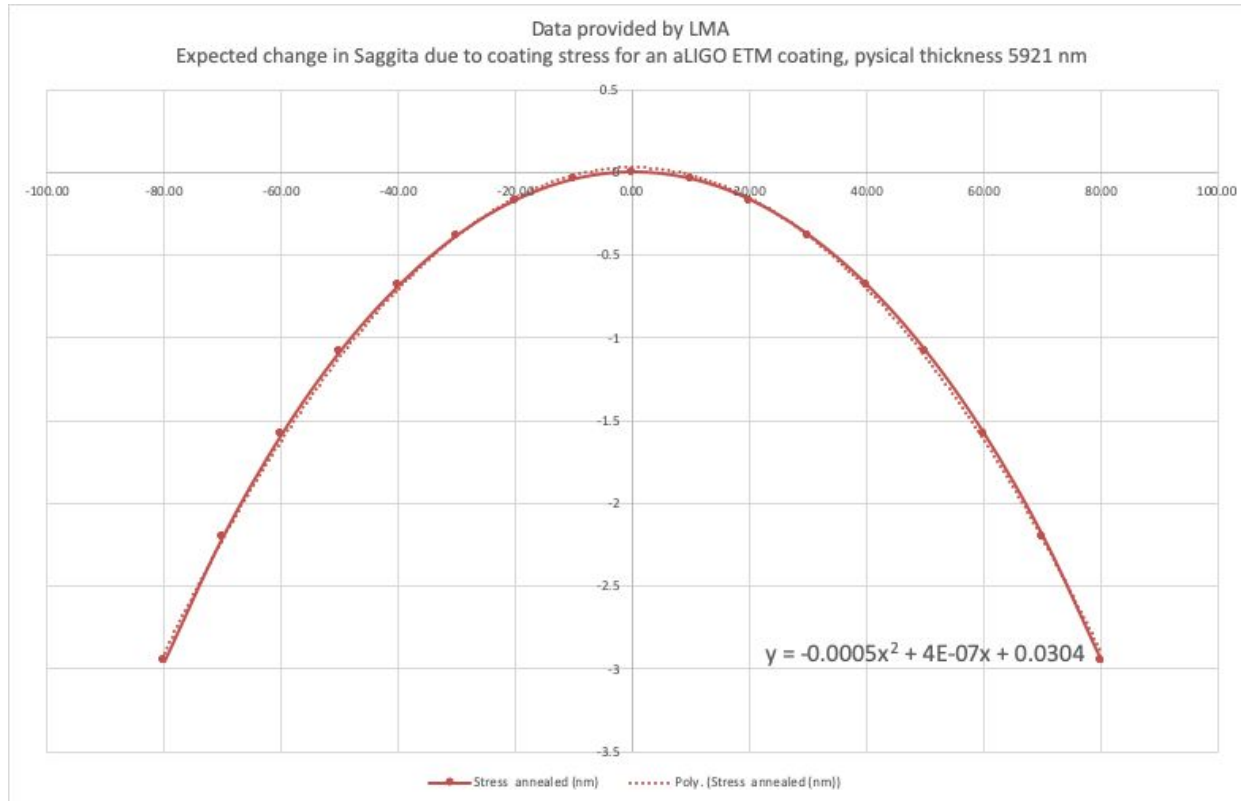
Causes of change in figure after coating

- Compressive coating stress flattens the substrate
- Coating uniformity
- Substrate deformation

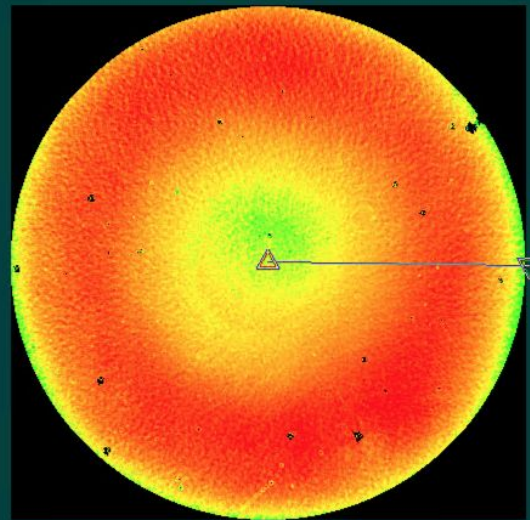
Expected deformation due to coating stress LIGO-C2000282



Second order fit to stress prediction is good over the center 160 mm Ø
Saggita is -2.95 nm on 160 mm Ø - equivalent to ~5 m ROC change

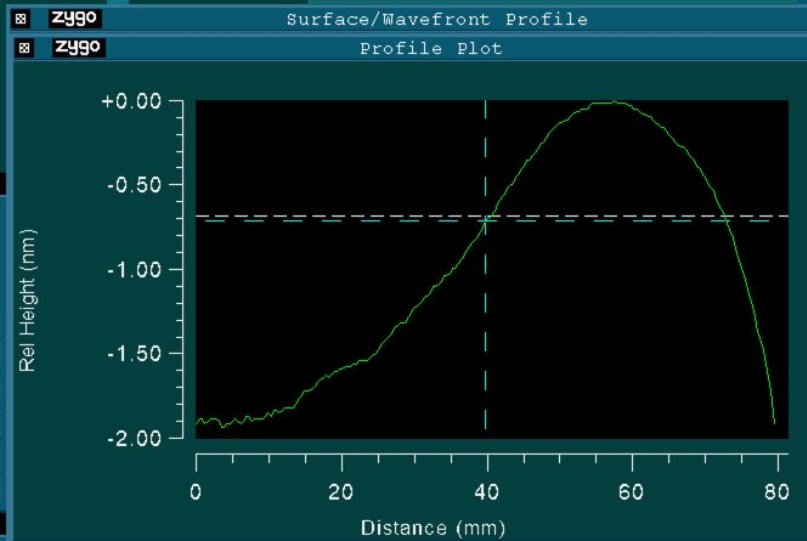


LIGO after subtracting calculated stress (2.95 nm on 160 mm dia)



Coating Uniformity
Significant Spherical Aberration remains within 160 mm Ø after subtracting expected change due to stress.
Calculations shown in G2001747 show this to be beneficial.

PV	6.185	nm	Removed: PST TLT
rms	0.650	nm	Trimmed: 0
Power	0.427	nm	Filter: Off
Size X	160.06	mm	Size Y 160.063 mm
TiltX	-0.328	nm	Tref.X -0.005 nm
Tilty	-0.814	nm	Tref.Y -0.092 nm
Ast.X	-0.332	nm	2Ast.X -0.086 nm
Ast.Y	-0.194	nm	2Ast.Y 0.028 nm
ComaX	-0.190	nm	2ComaX 0.003 nm
ComaY	0.408	nm	2ComaY -0.034 nm
Sph Ab	-1.270	nm	2Sph Ab -0.130 nm



We appear to have a relative uncertainty of ~ 2 meters

Lucky with aLIGO TMs: coating stress/non-uniformity compensate for vendor polish offset

aLIGO Spec 2245 -5, +10 m

T2000644					
All analysis on 160 mm diameter	SN	Uncoated ROC, Polish Vendor (m)	Uncoated ROC, LIGO (m)	∂ ROC LIGO-polish vendor (m)	After Coating ROC, LIGO (m)
mask 1	ETM07	2250.8			2240
mask 1	ETM08	2249.3			2242
mask 1	ETM09	2250.8			2242
mask 1	ETM12	2249.0	2246.6	-2.4	2239
mask 2	ETM11	2250.6	2248.8	-1.8	2250
mask 2	ETM14	2251.0	2248.9	-2.1	2251
mask 3	ETM10	2250.1			2248
mask 3	ETM13	2249.7	2247.6	-2.1	2244
mask 3	ETM15	2249.9	2247.2	-2.7	2245
mask 3	ETM16	2249.6	2247.5	-2.1	2247
no mask	PEN-ITM02	2498			2491

Each coating mask adds a characteristic amount of power?

T2000644					
All analysis on 160 mm diameter	SN	∂ ROC after coating LIGO-Polish vendor (m)	∂ Saggita after coating LIGO-Polish vendor (nm)	∂ Saggita, stress (calculated by B. Sassolas) (nm)	∂ Sag due to coating uniformity?? (nm)
mask 1	ETM07	-11.14	7.1	-2.95	10.0
mask 1	ETM08	-7.74	4.9	-2.95	7.9
mask 1	ETM09	-8.42	5.3	-2.95	8.3
mask 1	ETM12	-10.1	6.4	-2.95	9.4
mask 2	ETM11	-0.6	0.4	-2.95	3.3
mask 2	ETM14	-0.04	0.0	-2.95	3.0
mask 3	ETM10	-2.43	1.5	-2.95	4.5
mask 3	ETM13	-5.54	3.5	-2.95	6.5
mask 3	ETM15	-4.46	2.8	-2.95	5.8
mask 3	ETM16	-2.68	1.7	-2.95	4.6
no mask	PEN-ITM02	-7	3.6	-2.95	6.5

~ 2 nm spread within mask 1

~ 2 nm spread within mask 3

Suggestions for ROC Specification Change

Change ROC spec from 2245 -5+10 m to $\rightarrow 2240 \pm 10$ m

Make the ROC tolerance symmetric ± 10 m (was -5 +15)
this fixes vendor response polish all to ROC = 2250 m

Compensate for stress change (∂ saggita = -2.95 nm, 160 mm \varnothing) which
would flatten the surface by ~ 5 meters (2240 \rightarrow 2245)

Expected Results

Consistency should be good to ~ 2 m

Absolute accuracy is unchanged/unknown to better than ± 7 meters

Same measurement system - proof of concept working in our IFO now.

Final Polishing figure

- New Center ROC
 - Symmetric tolerance
 - Accounting for coating stress
- Customized figure - use the coating
 - Outside fall off is beneficial, actual coating uniformity is similar to, or better than, the “idealized” fall of proposed earlier “A” - see [LIGO-G2001747](#)
 - Polish the optic to a sphere
 - Use the coating fall off to suppress 7th order modes

Comments from Committee - see responses at G2001747

- Recommendation is to go with spherical polish, plus coating shape B (blue curve on slide 5 of G2001747-v3)
- For this case, what is the eigenfrequency for the 6th & 7th order modes (Δf from the TEM00 mode)?
- G2001747-v3, slide 32, upper right plot. Is there any understanding why the RTL for the solid purple curve is lower than for the solid red curve for offsets greater than 2.5 cm ? Also why is the RTL for the dashed cyan curve higher than for the solid cyan at zero offset? As the beam is moved, does the absorbed power stay the same, or decrease as it's moved away from the PA?
- Can you comment on the benefit of retaining or removing the slight spherical aberration, induced by the coating, using a custom polish?
- From G2001747-v3 page 32 - Are labels swapped? Cyan with corr is worse than without at center alignment. Also plots on slide 2 - are the axes labels swapped?