Note on the radius of curvature of compression fit mirror and a common solution with piezo mirror for SAMS

T2000183

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The calculations are based on document E1900370 (https://dcc.ligo.org/E1900370)

A. Definition of variables:

P_{design} ≡ Mirror's nominal defocus at optical design = $2/R_{design}$ [mD]

P_{manuf} ≡ Manufactured optical power = $2/R_{manuf}$ [mD]

$P_{preload,p}$ ≡ Change of optical power through preloading of the piezo actuator [mD]

$P_{actuation,p}$ ≡ Full range of optical power change through piezo actuation [mD]

$P_{preload,t}$ ≡ Change of optical power by compression fit at ambient temperature (20°C) [mD]

$P_{actuation,t}$ ≡ Full range of optical power change by heating of the thermal mirror [mD]

T_{max} ≡ Maximum operating temperature [°C]

ΔT_{max} ≡ Maximum actuation temperature range [K]

T_{assem} = CFM assembly temperature [°C]

δr = Radial interference [μm]

Sign convention: '+' for concave mirror, '-' for convex mirror

B. Radius of curvature of mirror for CFM mirrors:

Two main limits that will affect the choice of radius of curvature for the CFM:

1. The maximum operating temperature: this affects actuation range, assembly temperature and thus preload defocus ($P_{preload,t}$). Ideally, we want the assembly temperature to be at least 20% higher than that of maximum operating temperature.
2. The maximum allowed preload on piezo mirror: This is important to find a common solution for both piezo and thermal mirrors. The higher $P_{preload,p}$ is, the higher $P_{preload,t}$ can be, thus a higher actuation range for thermal mirror can be achieved. However, we want to make sure that the stress in piezo is within the acceptable range (including some safety factor)

We assume a maximum operating temperature of 70°C

T_{max} [°C]	ΔT_{max} [K]	T_{assem} [°C]	$2\delta r$ [µm]*	$P_{preload,t}$ [mD] **	$P_{actuation,t}$ [mD] **
70	50	84	73	-420	+330

(*) *The diametric interference is computed from the following:*

Let:

$OD_{m,amb}$ ≡ Mirror's nominal diameter at ambient temperature (20°C) = 50.0 mm.

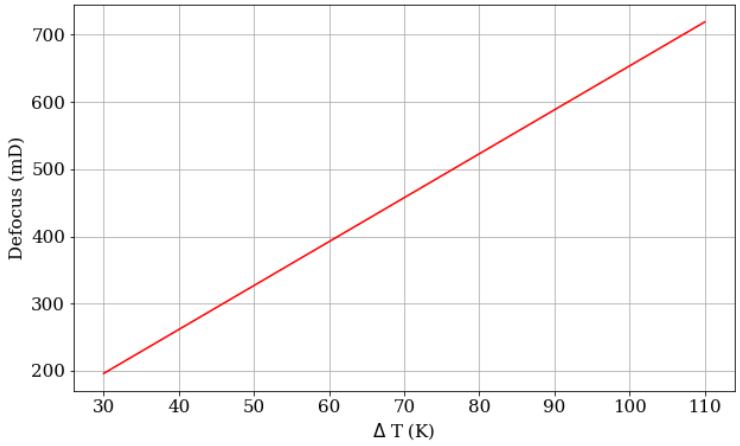
$ID_{r,amb}$ ≡ Mirror's nominal diameter at ambient temperature (20°C) = $OD_{m,amb}$ -2δr

α_m, α_r = Coefficient of thermal expansion of mirror and ring (0.55E-6 and 23.4E-6 respectively)

$$OD_{m,amb}(1 + \alpha_m \Delta T_{assem}) = (OD_{m,amb} - 2\delta r)(1 + \alpha_r \Delta T_{assem})$$

$$\therefore 2\delta r = OD_{m,amb}\left(1 - \frac{1 + \alpha_m \Delta T_{assem}}{1 + \alpha_r \Delta T_{assem}}\right)$$

(**) *Estimation of preload defocus and actuation range from FEA model of the CFM:*



X-axis is change in actuation temperature, y-axis is corresponding change in defocus due to temperature change.

P_{manuf} is expressed as followings in the case of CFM:

$$P_{manuf} = P_{design} + |P_{preload,t}| - \frac{|P_{actuation,t}|}{2}$$

then

$$P_{manuf} = P_{design} + 255\ [mD]$$

According to the current design of the piezo mirror (T2000101), P_{manuf} is determined by:

$$P_{manuf} = P_{design} + |P_{preload,p}| + \frac{|P_{actuation,p}|}{2} = P_{design} + 150[mD]$$

The manufactured mirror need to be more concave for the thermal mirror.

Question: Can we change $P_{actuation,p}$ such that there is a common solution?

$P_{preload,p}$ = -155[mD]

Recent measurement of piezo mirror RoC with ZYGO suggests that $P_{preload,p}$ is -160 [mD] for 80in-lbs preloading → *it looks feasible? What's the stress in flexures at this preload? Is it still in acceptable range?*

Assuming the new preloads, the manufactured RoC of the mirrors are related to the design RoC as followings:

Case 2:

$$R_{manuf} = \frac{R_{design}}{1 + 0.1275 R_{design}}$$

With these new relations, the following manufactured RoC's are proposed:

Maximum operating temperature: 70°C, maximum actuation range: 330 [mD]

Optics	R_{design} [m]	P_{design} [D]	R_{manuf} [m]	P_{manuf} [D]
ZM2	0.85	2.35	0.77	2.59
ZM5	3.4	0.59	2.37	0.84
ZM4	Infty	0	7.84	0.26
OM2-1(nom)	1.7	1.18	1.40	1.43
OM2-2	1.5	1.33	1.26	1.59
OM2-3	1.94	1.03	1.56	1.28