



**LIGO**

**Caltech**



## **Advanced LIGO O3 Calibration**

Ling Sun, LIGO Excellence Award Talk, Feb 2020 @ MIT

DCC-G2000234

# Agenda

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- Why is calibration important
- How does calibration work
- Understanding systematics and uncertainties
- O3 improvements and future perspectives

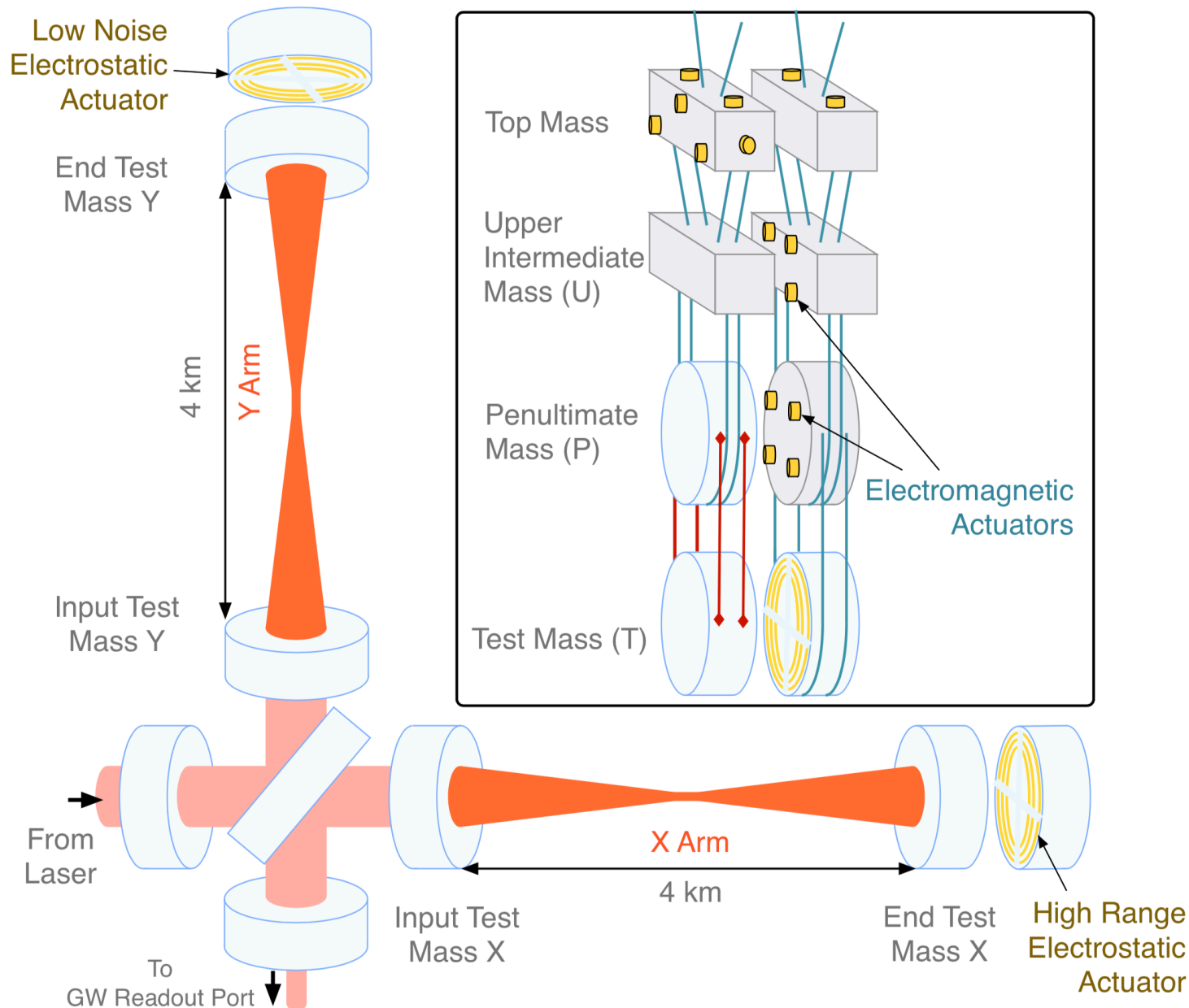
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- **Why is calibration important**
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# Calibration pipeline produces $h(t)$

## Differential arm (DARM) control system



### DARM displacement:

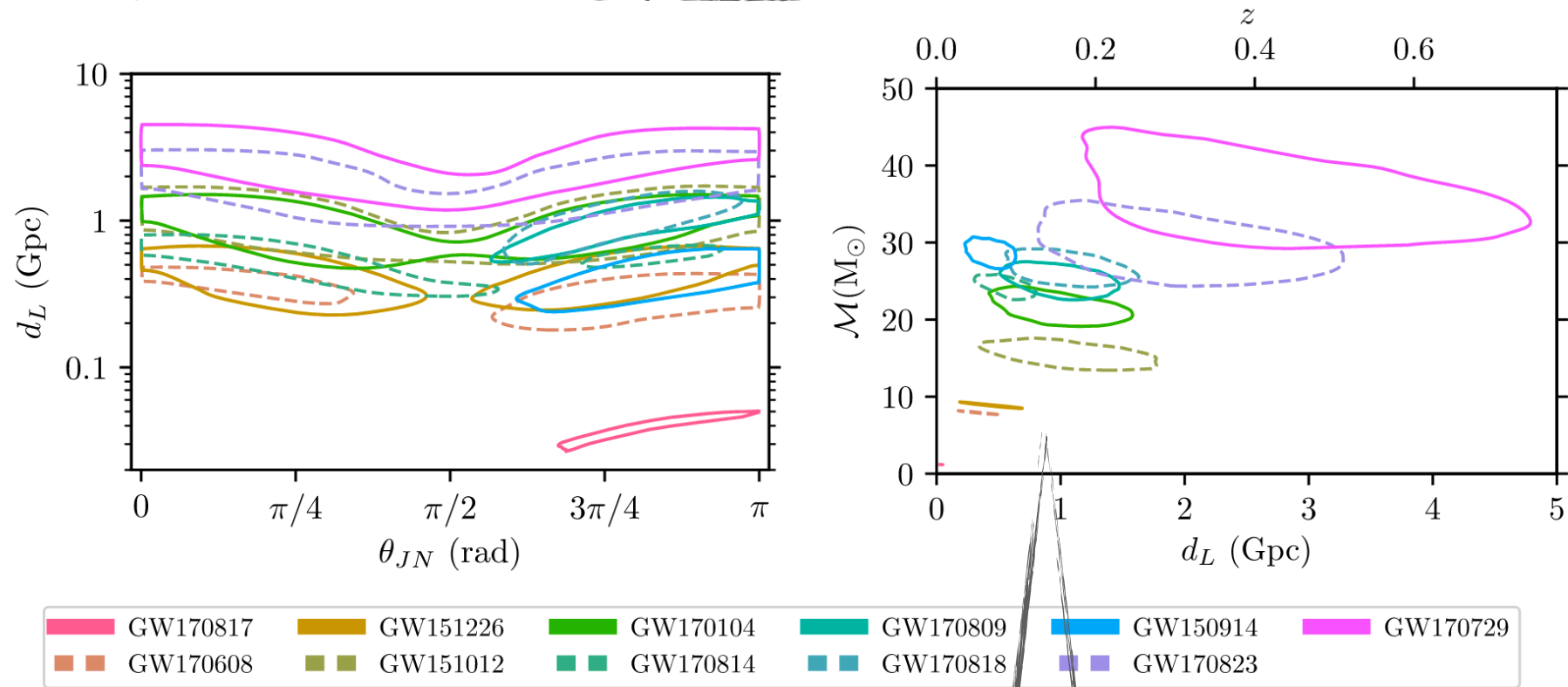
$$\Delta L_{\text{free}} = \Delta L_x(t) - \Delta L_y(t)$$

$$h(t) = \frac{\Delta L_{\text{free}}(t)}{L}$$

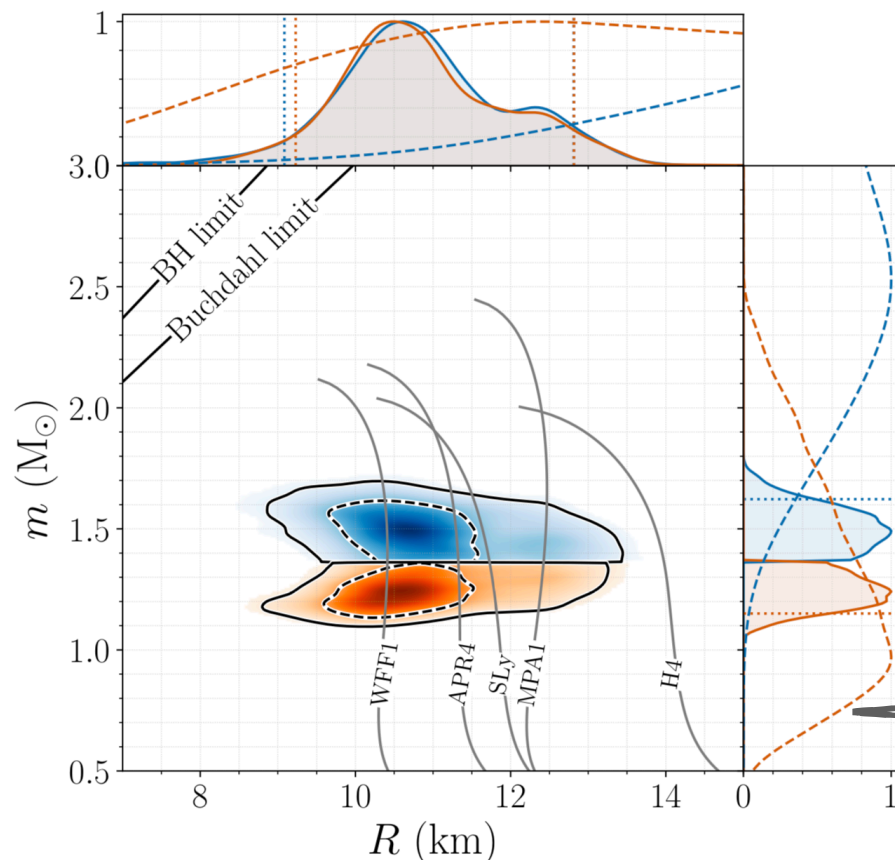
- Need to cancel the signal and keep the detector in null range
- Quadruple pendulum suspension systems
- Active seismic isolation systems
- Not enough – **DARM displacement must be further controlled!**



# Impact on estimating source properties



Abbott et al.  
PRX 9,031040 (2019)



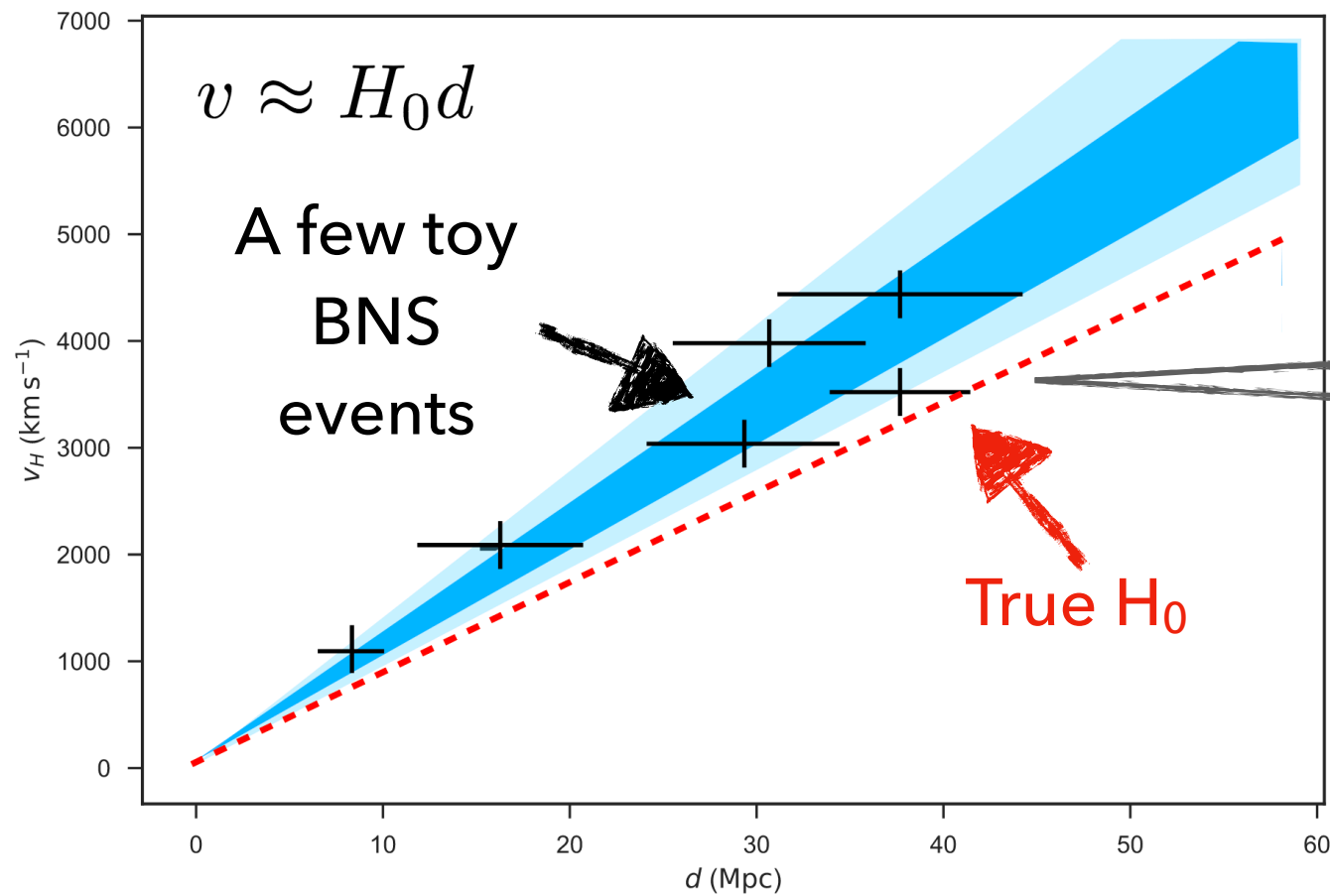
- Calibration magnitude affects the estimation of luminosity distance
- Phase response affects the estimation of intrinsic source properties, e.g., chirp mass

- Further improved instrumental calibration could improve constraints on NS EoS

Abbott et al. PRL 121, 161101 (2018)

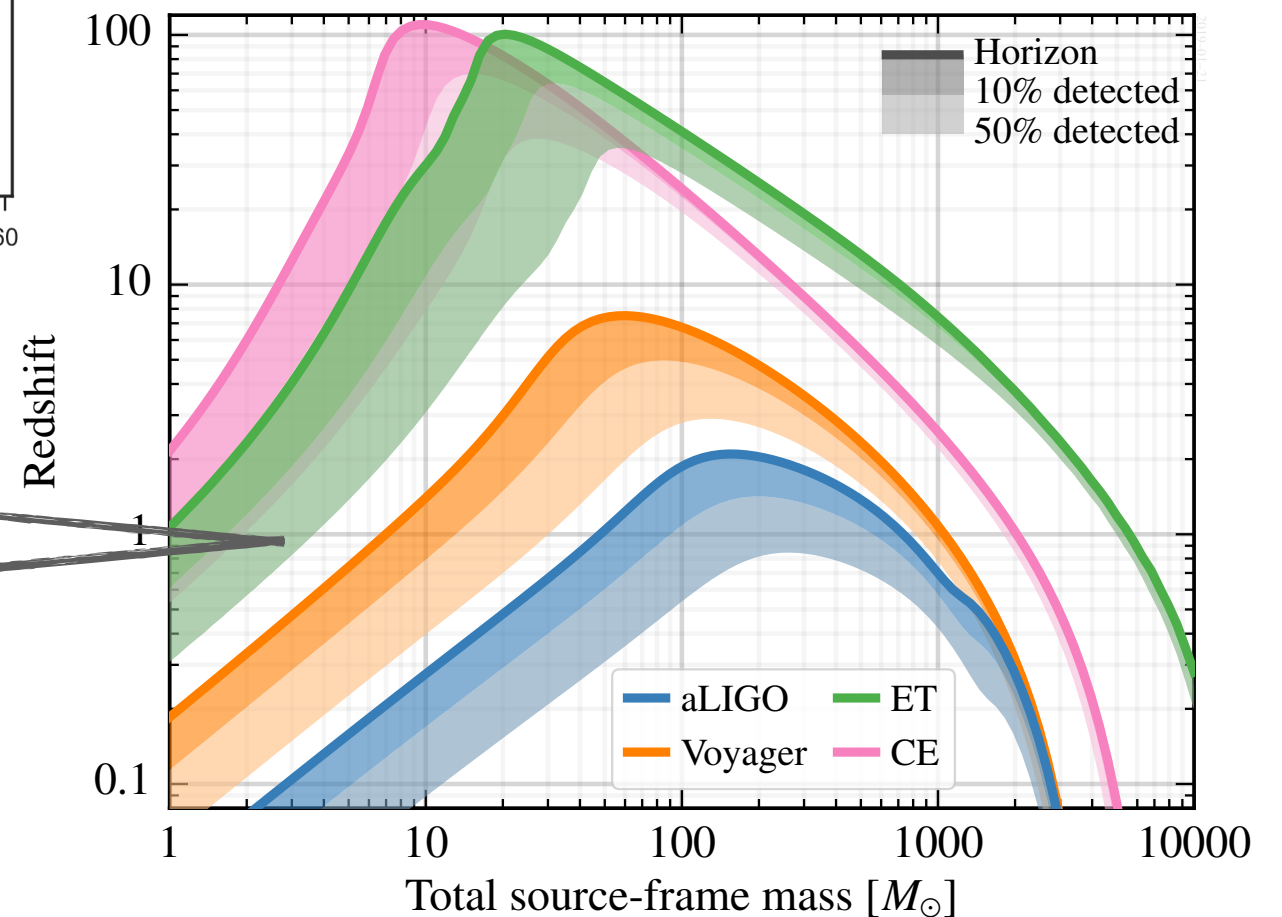
# Impact on cosmology and high-redshift events

Credit: C. Messenger



- Correlated calibration systematic errors impact  $H_0$  measurement

Credit: E. Hall



- Calibration systematic errors and statistical uncertainties impact the horizon distance, source-frame masses, rates, especially at high redshift

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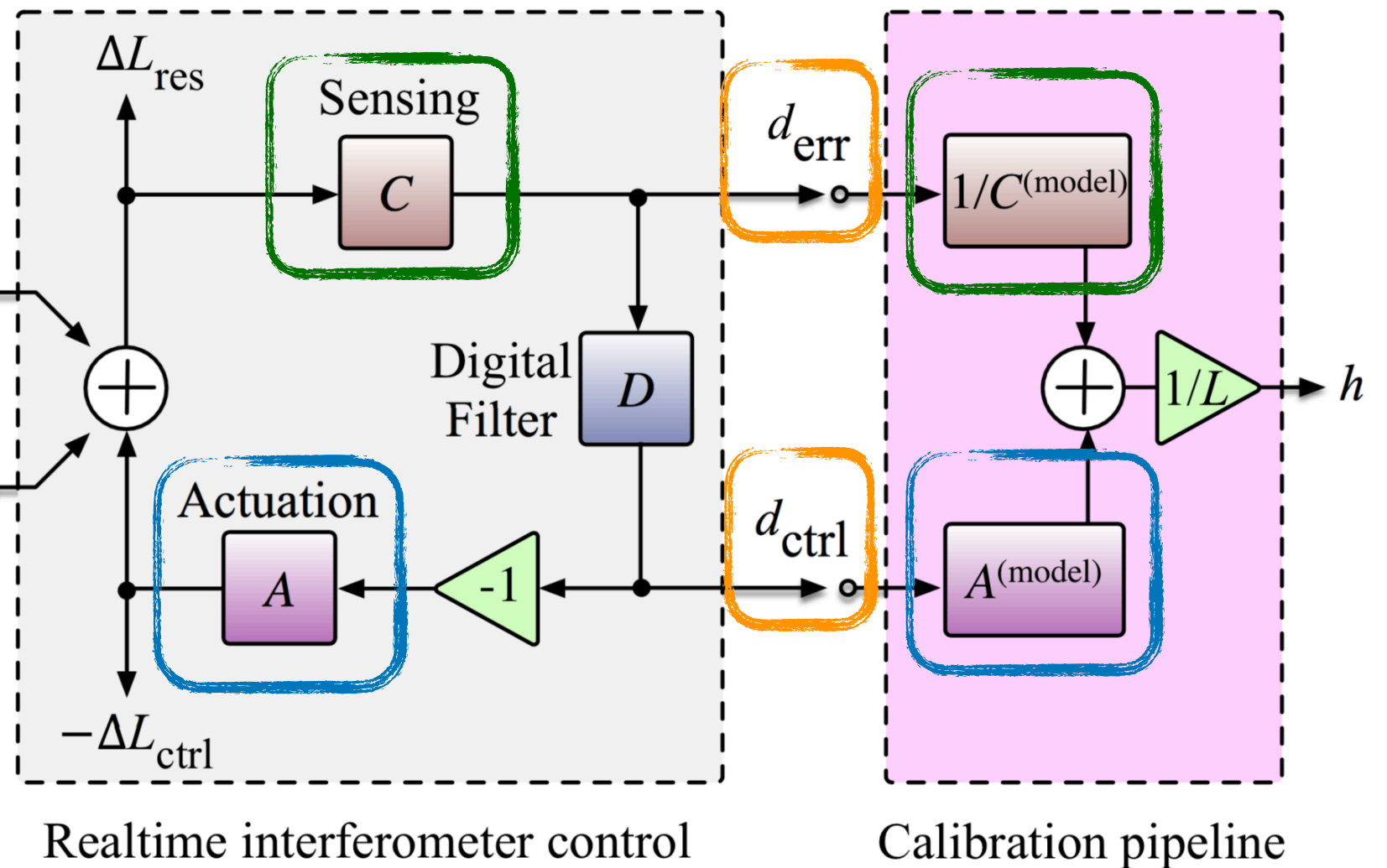
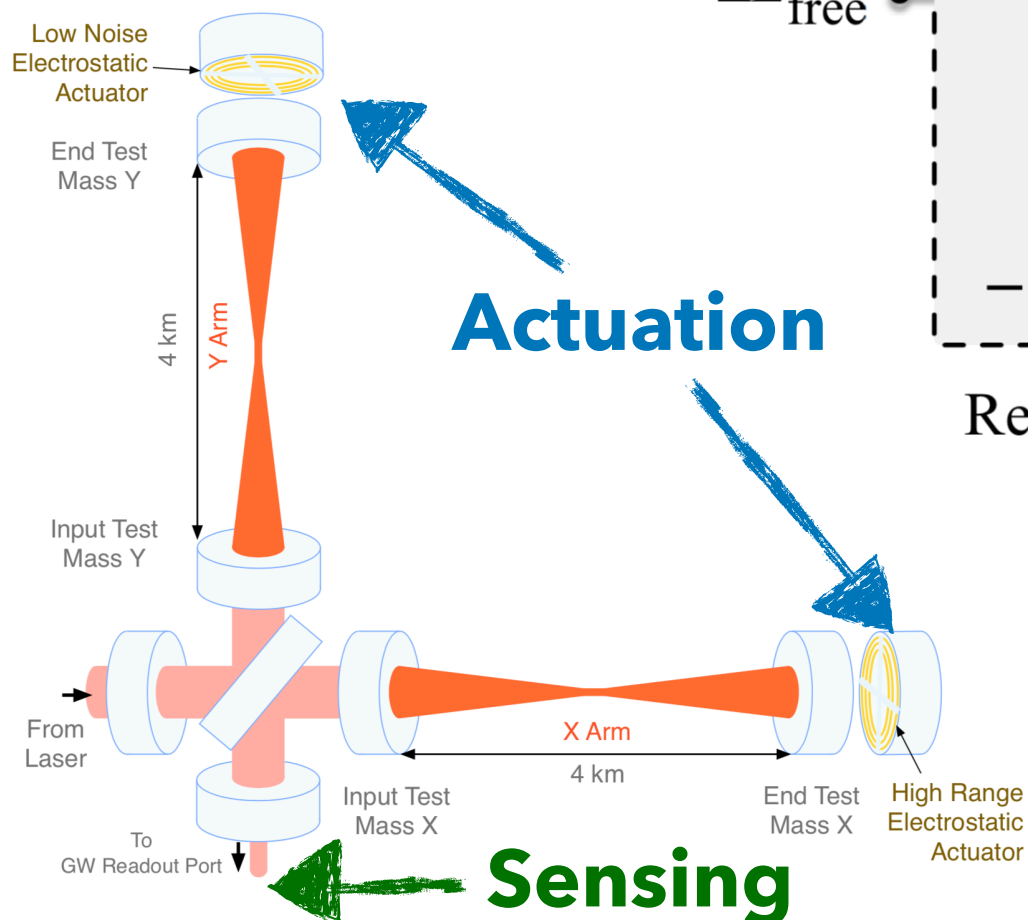
# How does calibration work?

## Differential arm (DARM) control loop

B. P. Abbott, et al. 2017 PRD 95 062003

$$h(t) = \frac{\Delta L_{\text{free}}(t)}{L}$$

Recover me!



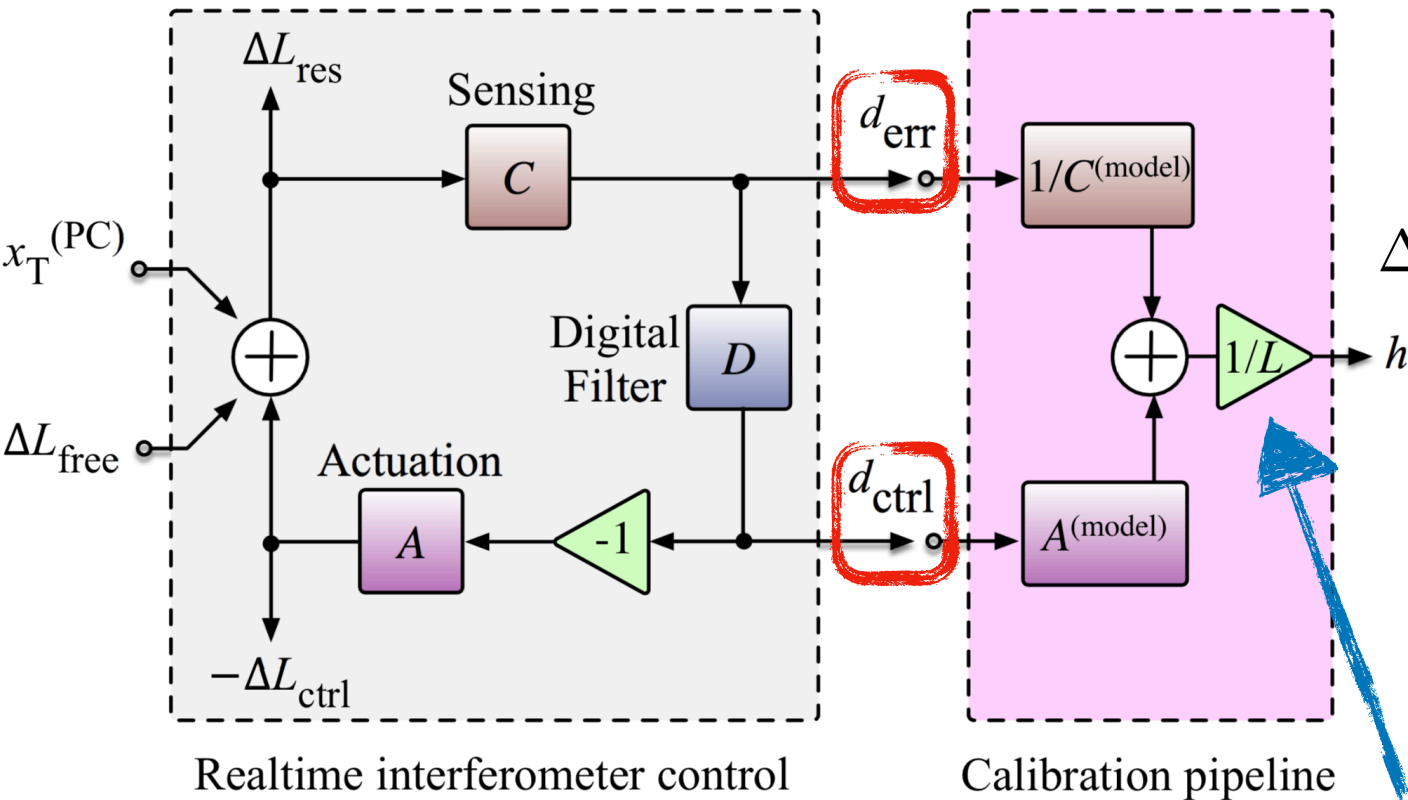
$$\Delta L_{\text{free}}(t) = \frac{1}{C(t)} * d_{\text{err}}(t) + \mathcal{A}(t) * d_{\text{ctrl}}(t)$$

**High freq**
**Low freq**

$$\Delta L_{\text{free}}(f) = \frac{1}{C(f)} d_{\text{err}}(f) + A(f) d_{\text{ctrl}}(f)$$

# Detector's response function

B. P. Abbott, et al. 2017 PRD 95 062003



Calculate  $h(t)$  bypassing digital filter  $D$

$$\Delta L_{\text{free}}(t) = \frac{1}{C^{(\text{model})}} * d_{\text{err}}(t) + A^{(\text{model})} * d_{\text{ctrl}}(t)$$

We can define a response function by writing  $h(t)$  in terms of the error signal  $d_{\text{err}}$

**3994.xxx m +/- (~ mm)**

**Response function**

$$\Delta L_{\text{free}}(t) = \frac{1}{C^{(\text{model})}} * d_{\text{err}}(t) + A^{(\text{model})} * d_{\text{ctrl}}(t) = R^{(\text{model})}(t) * d_{\text{err}}(t)$$

$$d_{\text{ctrl}} = D d_{\text{err}}$$

**Frequency-domain response function**

$$\tilde{R}(f) = \frac{1}{\tilde{C}(f)} + \tilde{A}(f) \tilde{D}(f)$$

$$h = \frac{R^{(\text{model})} * d_{\text{err}}}{L}$$

# Time dependent correction factors (TDCFs)

- If Sensing (C) and Actuation (A) models are perfectly known at any given time, there's no systematic error (there's still statistical uncertainty).

$$\Delta L_{\text{free}} = \frac{1}{C_{\text{model}}} d_{\text{err}} + A_{\text{model}} d_{\text{ctrl}}$$

- But the model parameters are changing slightly – due to charge accumulation around the test/reaction mass, drifts of the optical alignment in the arm cavities, etc.
- Use high SNR calibration lines, track temporal variations in DARM loop model parameters, and correct them

- Including factors for 3 actuation stages

$$\Delta L_{\text{free}} = \frac{1}{\kappa_C(t) C_{\text{model}}} d_{\text{err}} + \kappa_A(t) A_{\text{model}} d_{\text{ctrl}}$$

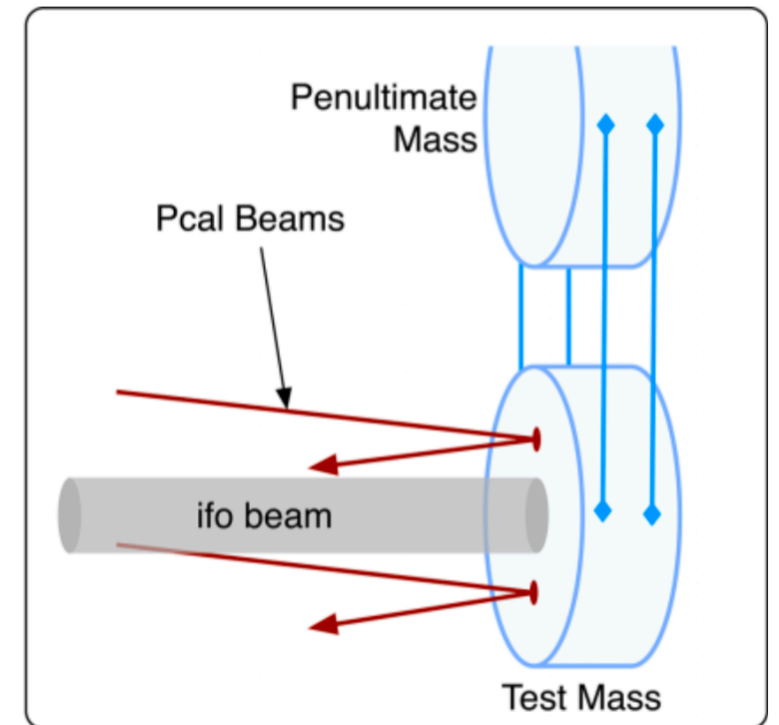
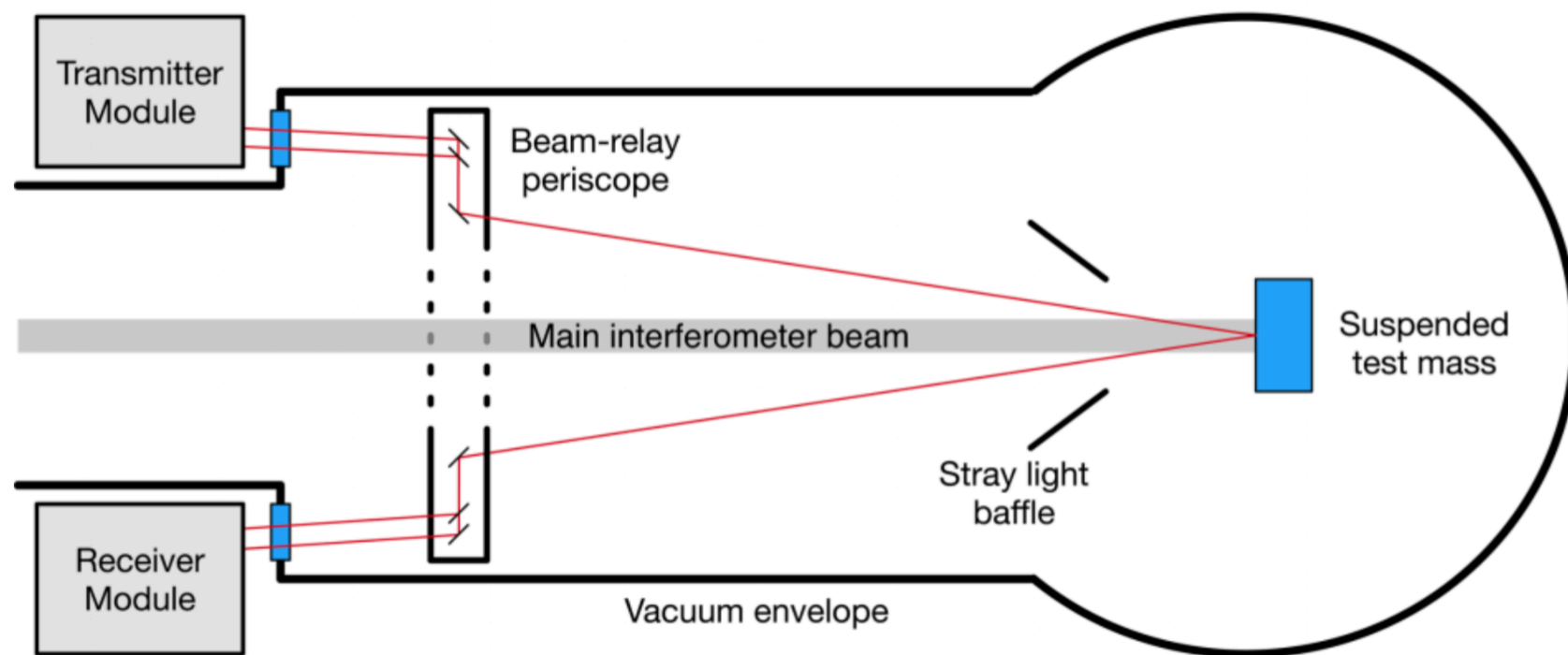
- Frequency-dependent, time-dependent factors

**TDCFs**

See Viets et al. 2018  
(arXiv:1710.09973), T1700106



# Photon calibrator (Pcal)

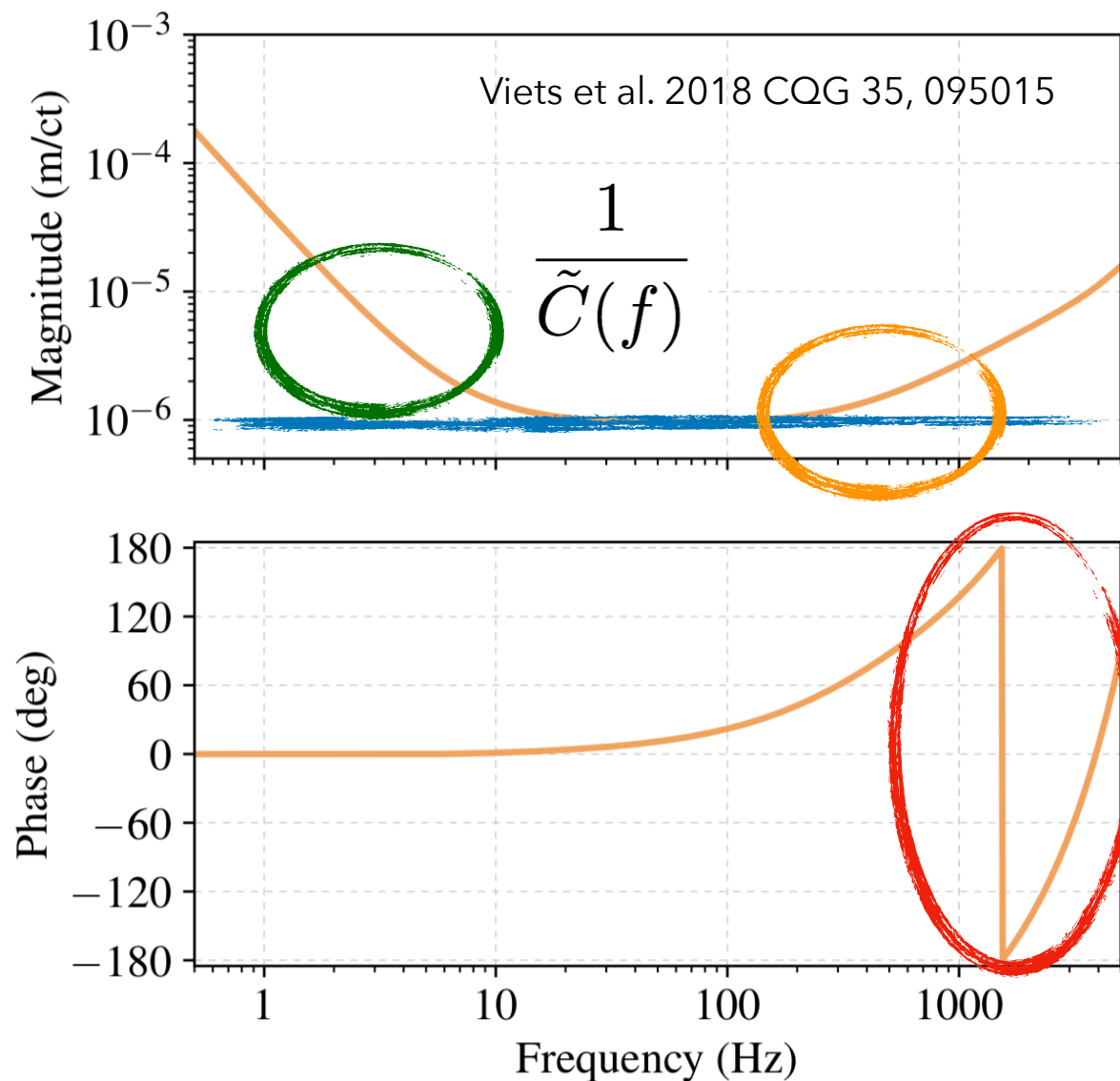


- Photon radiation pressure from auxiliary, power-modulated laser beams
- Sets absolute scale factor for calibration
- Serves as a perfect reference (with statistical uncertainty)
- Laser power, optical efficiency, incidence angle, mass of the test mass, rotation, etc.
- **Laser power** is calibrated by NIST (main contribution to overall uncertainty)

Karki et al. Review of Scientific Instruments 87, 114503 (2016)  
Bhattacharjee et al. (2020) arXiv:2006.00130

- O2 Pcal uncertainty = **0.79%**
- O3 Pcal uncertainty = **0.54%**
- Only in magnitude

# Sensing function (C)

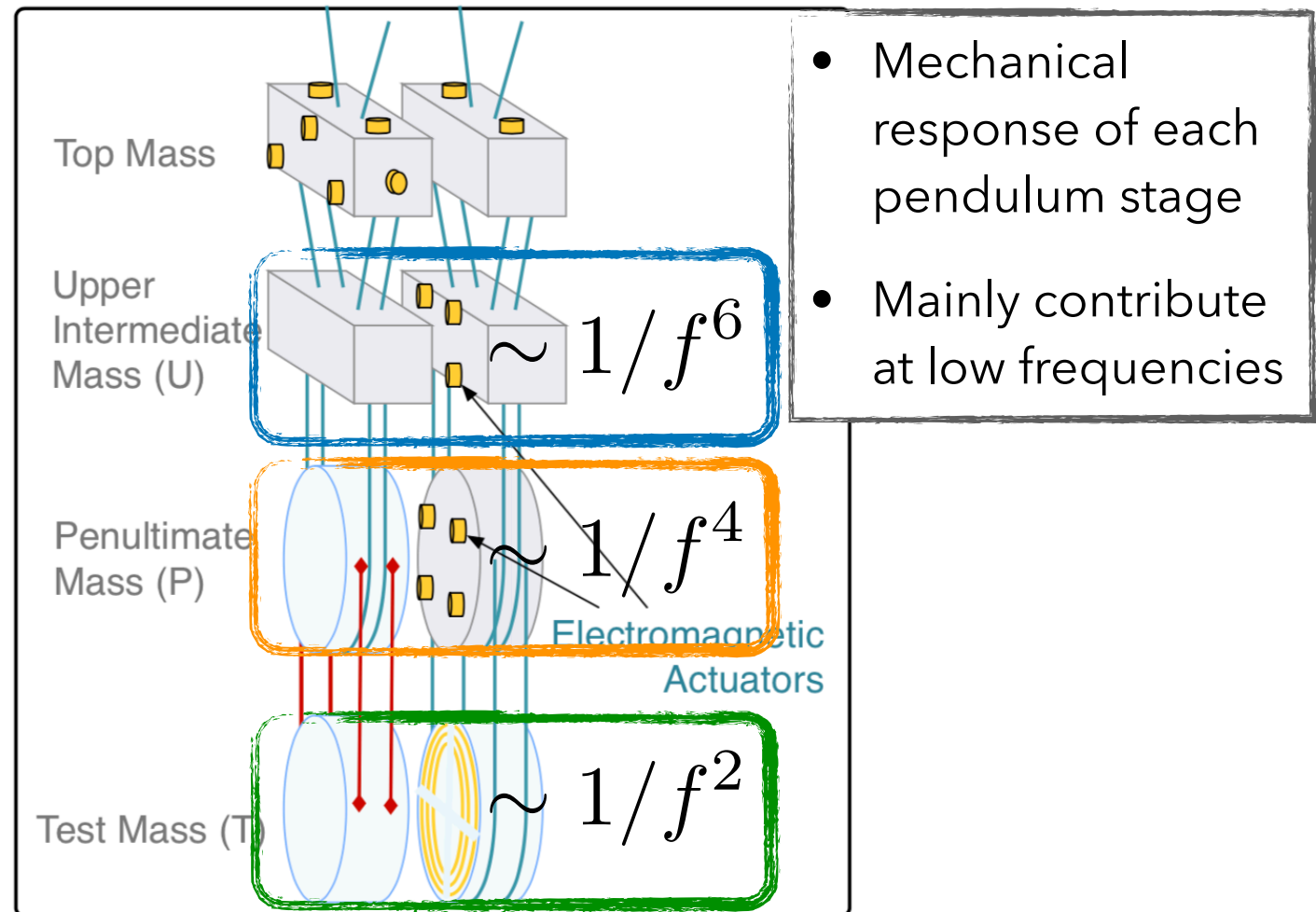
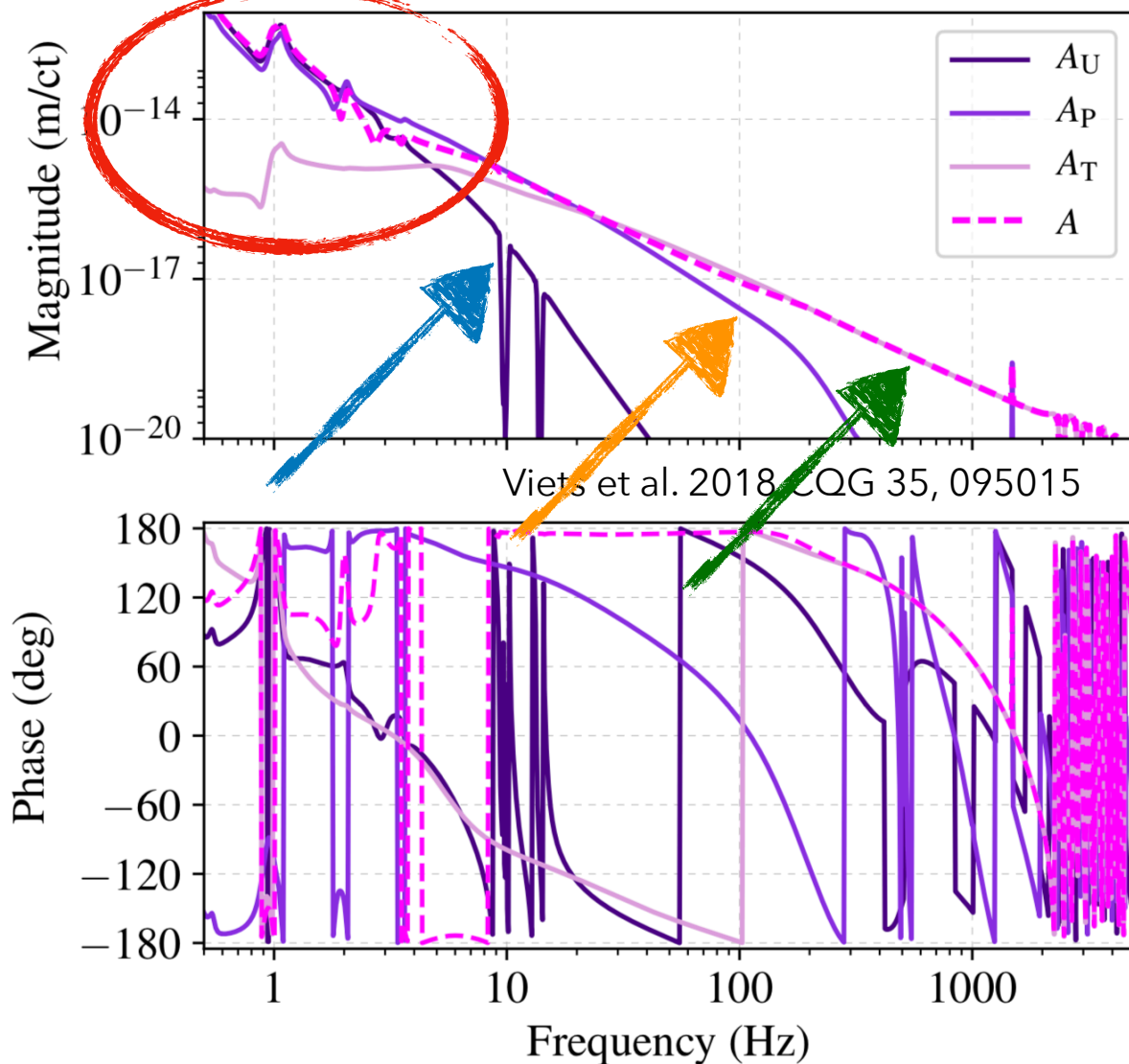


- Transfer function from the differential arm (DARM) residual displacement  $\Delta L_{\text{res}}$  to digitized photodetector output signal,  $d_{\text{err}}$
- **Low frequency (<1kHz):** determined by Fabry-Perot cavity response
- **High frequency (>1kHz):** determined by analog-to-digital conversion process

$$\tilde{C}(f; t) = \underbrace{\kappa_C(t) H_C}_{\text{Overall gain}} \underbrace{\left( \frac{1}{1 + i f f_{cc}^{-1}(t)} \right)}_{\text{Fabry-Perot cavity response (approximated)}} \underbrace{\left( \frac{f^2}{f^2 + f_s^2(t) - i f f_s(t) Q^{-1}(t)} \right)}_{\text{Optical spring from the signal recycling cavity (approximated)}} \underbrace{C_R(f) \exp(-2\pi i f \tau_C)}_{\text{Electronics response and time delay}}$$

# Actuation functions ( $A_U, A_P, A_T$ )

## mechanical resonances



$$\tilde{A}(f; t) = \left[ \kappa_U(t) \tilde{A}_U(f) \right] + \left[ \kappa_P(t) \tilde{A}_P(f) \right] + \left[ \kappa_T(t) \tilde{A}_T(f) \right] \exp(-2\pi i f \tau_A)$$

**UIM** actuation response

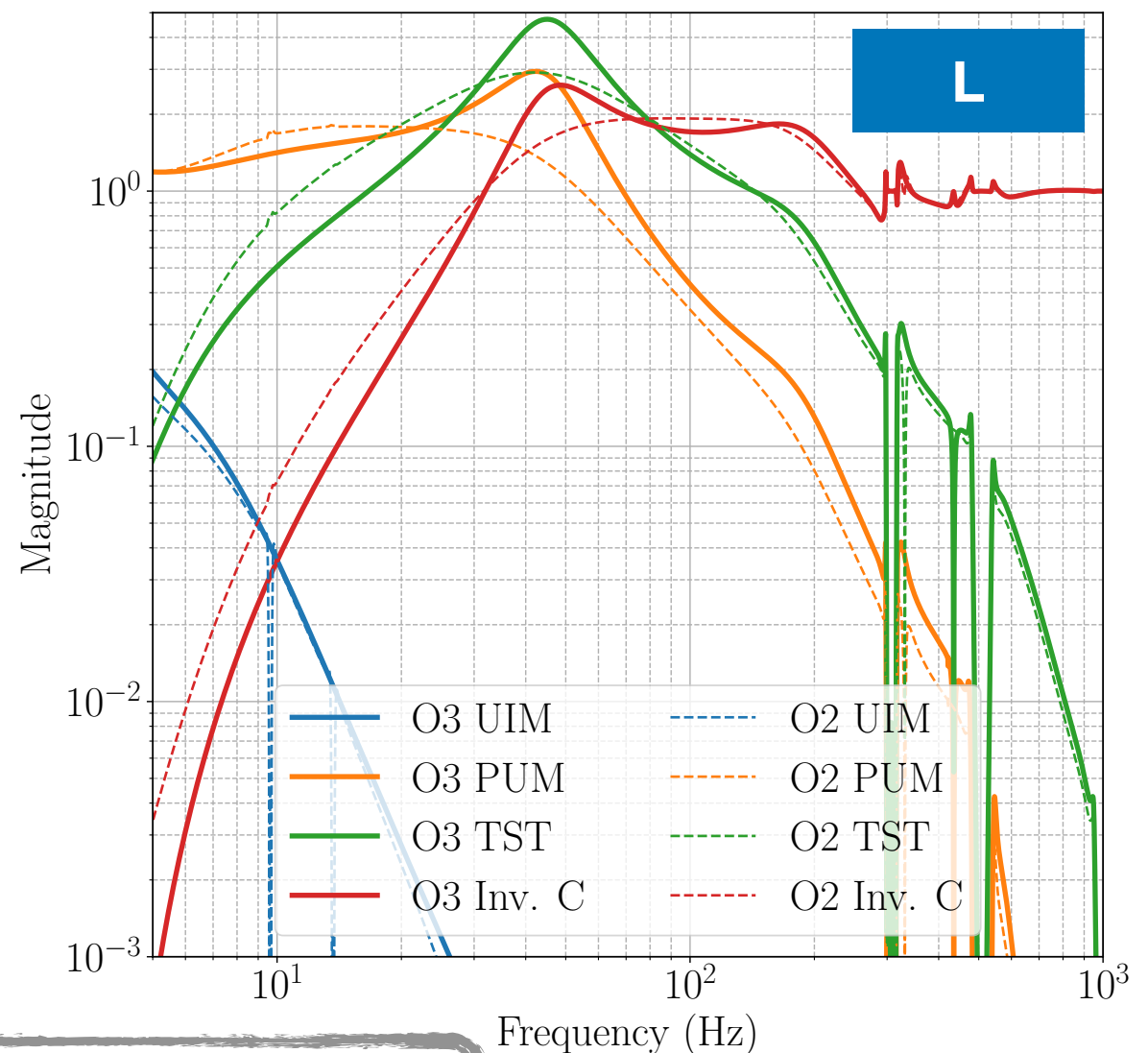
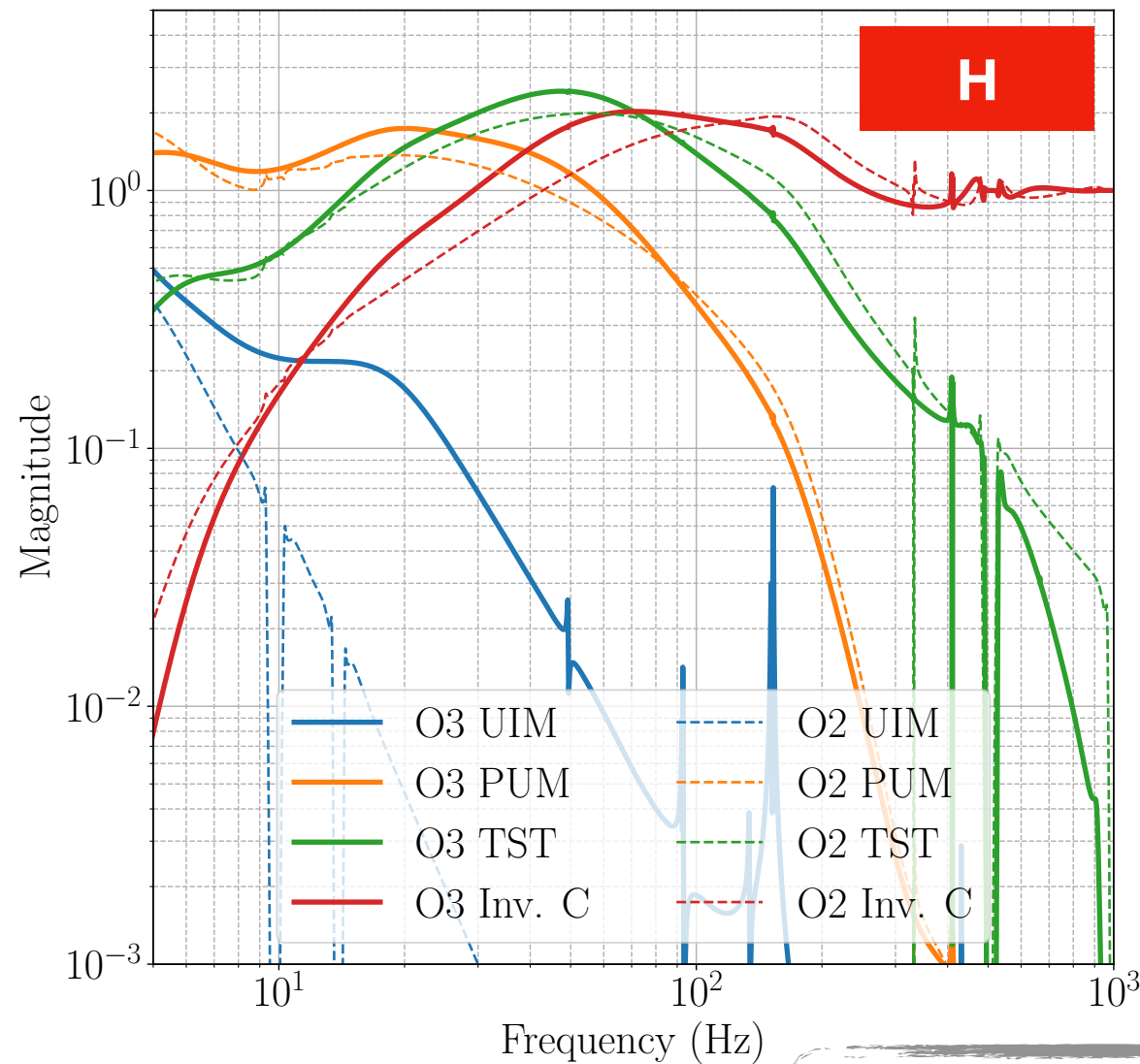
**PUM** actuation response

**TST** actuation response

Time delay

# Contribution from each stage

Sun et al. (2020) arXiv:2005.02531



$$\tilde{R}(f) = \frac{1}{\tilde{C}(f)} + \tilde{A}(f)\tilde{D}(f)$$

$$\frac{1/\tilde{C}^{(\text{model})}(f)}{\tilde{R}^{(\text{model})}(f)}$$

$$\frac{\tilde{A}_U^{(\text{model})}(f)\tilde{D}(f)}{\tilde{R}^{(\text{model})}(f)}$$

$$\frac{\tilde{A}_P^{(\text{model})}(f)\tilde{D}(f)}{\tilde{R}^{(\text{model})}(f)}$$

$$\frac{\tilde{A}_T^{(\text{model})}(f)\tilde{D}(f)}{\tilde{R}^{(\text{model})}(f)}$$

# Agenda

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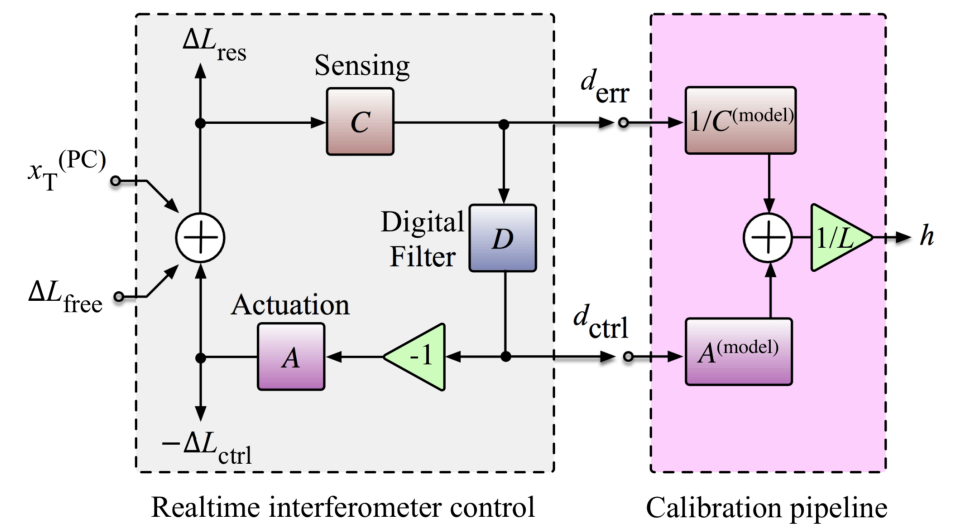
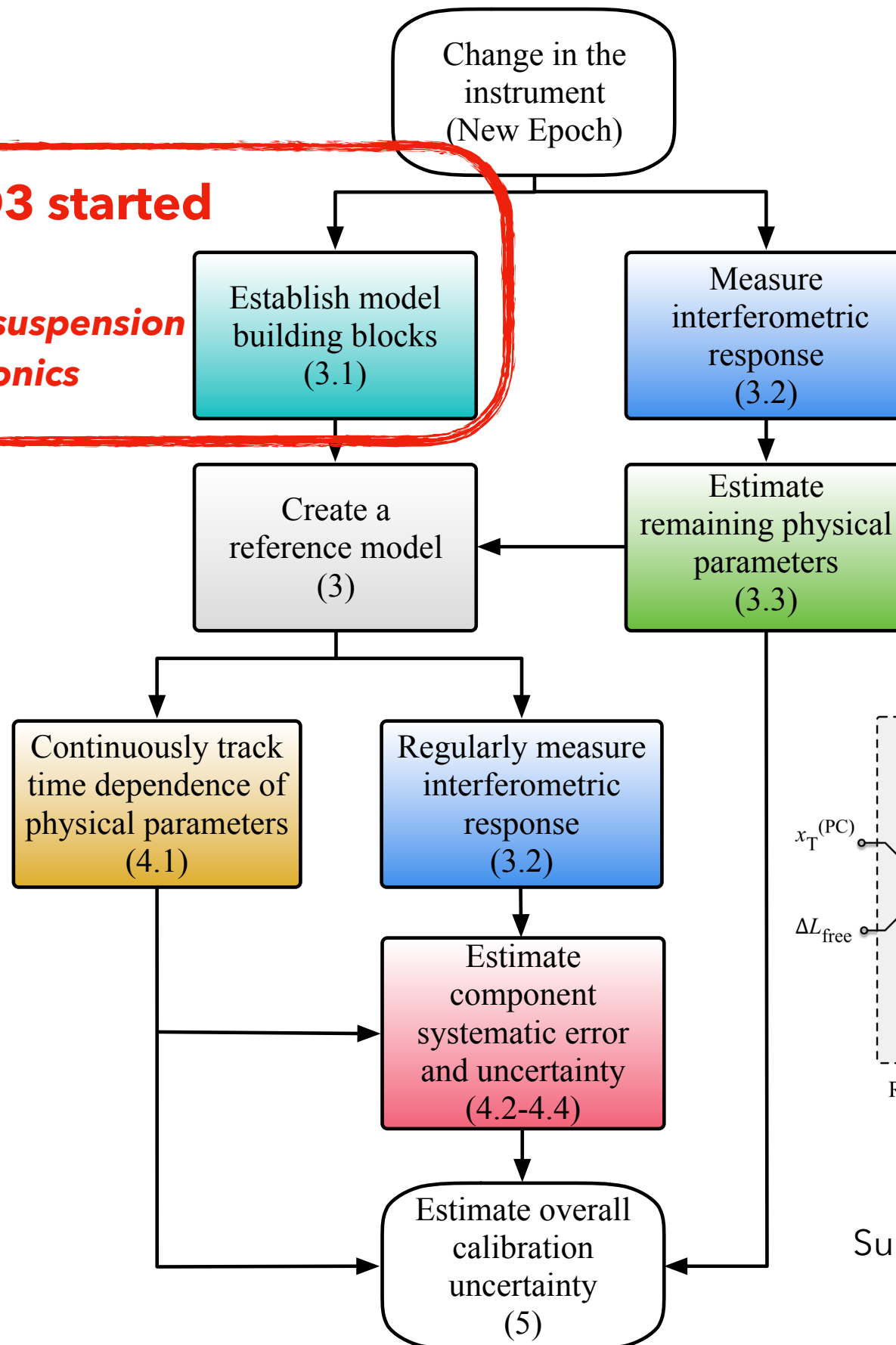
- Why is calibration important
- How does calibration work
- **Understanding systematics and uncertainties**
- O3 improvements and future perspectives



# A brief flowchart of calibration procedure

## 1. Before O3 started

- *Photon calibrator*
- *Dynamics of quadruple suspension*
- *Signal processing electronics*

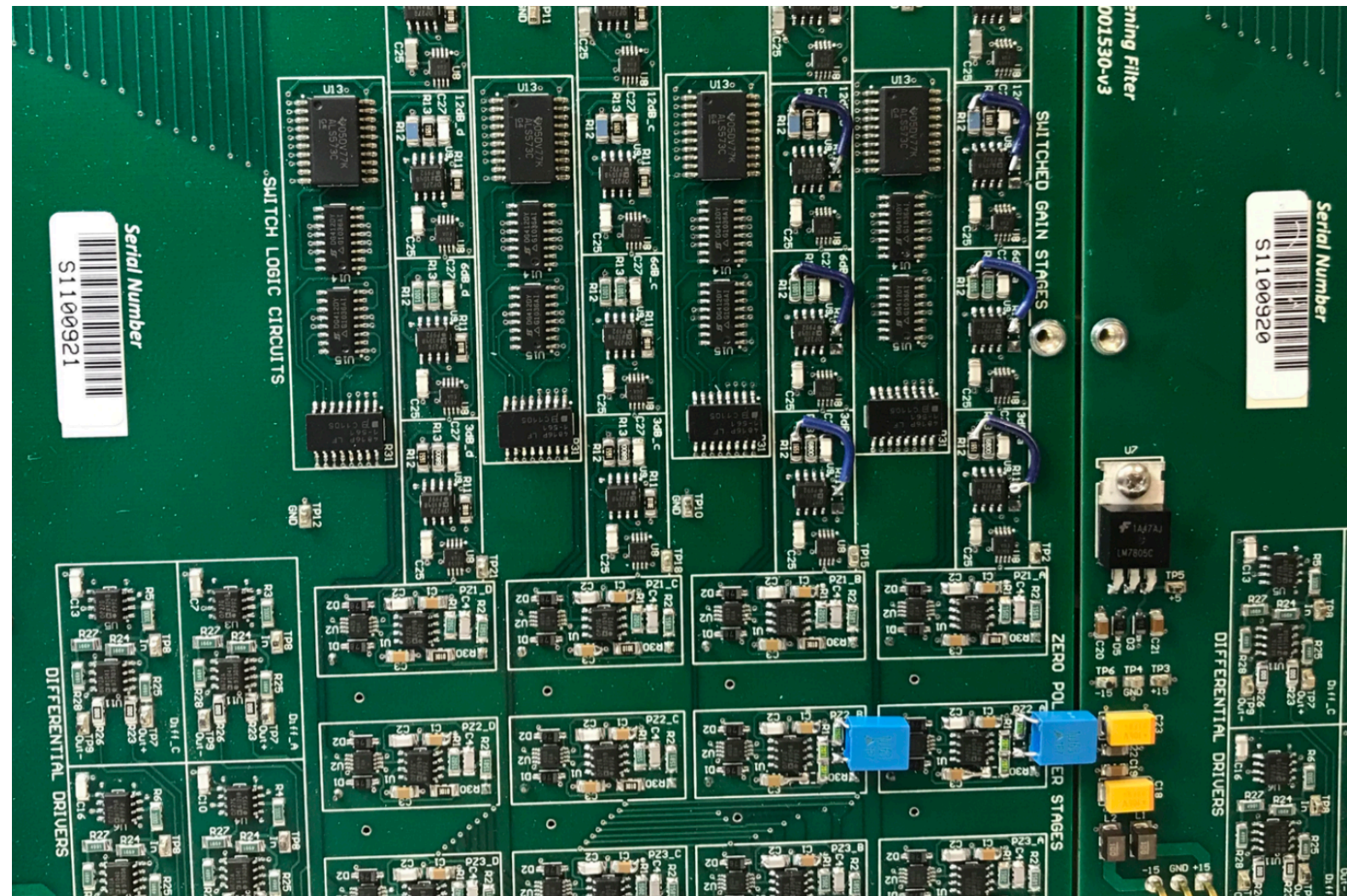


Sun et al. (2020) arXiv:2005.02531



# Signal processing analog electronics

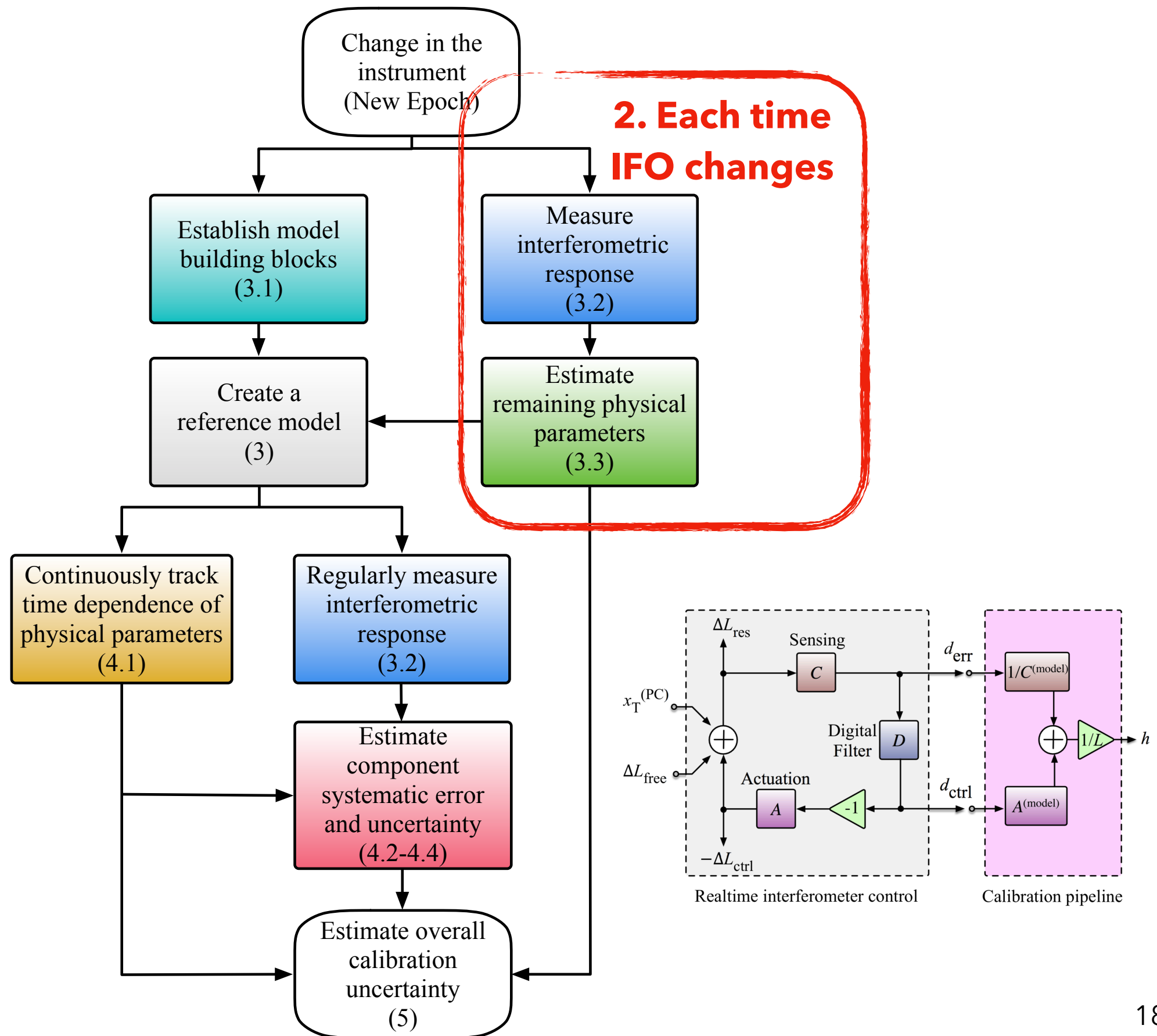
- Anti-aliasing chassis
- Anti-imaging chassis
- Coil driver chassis (UIM and PUM)
- Electro-static driver (ESD) chassis (TST)
- Whitening chassis



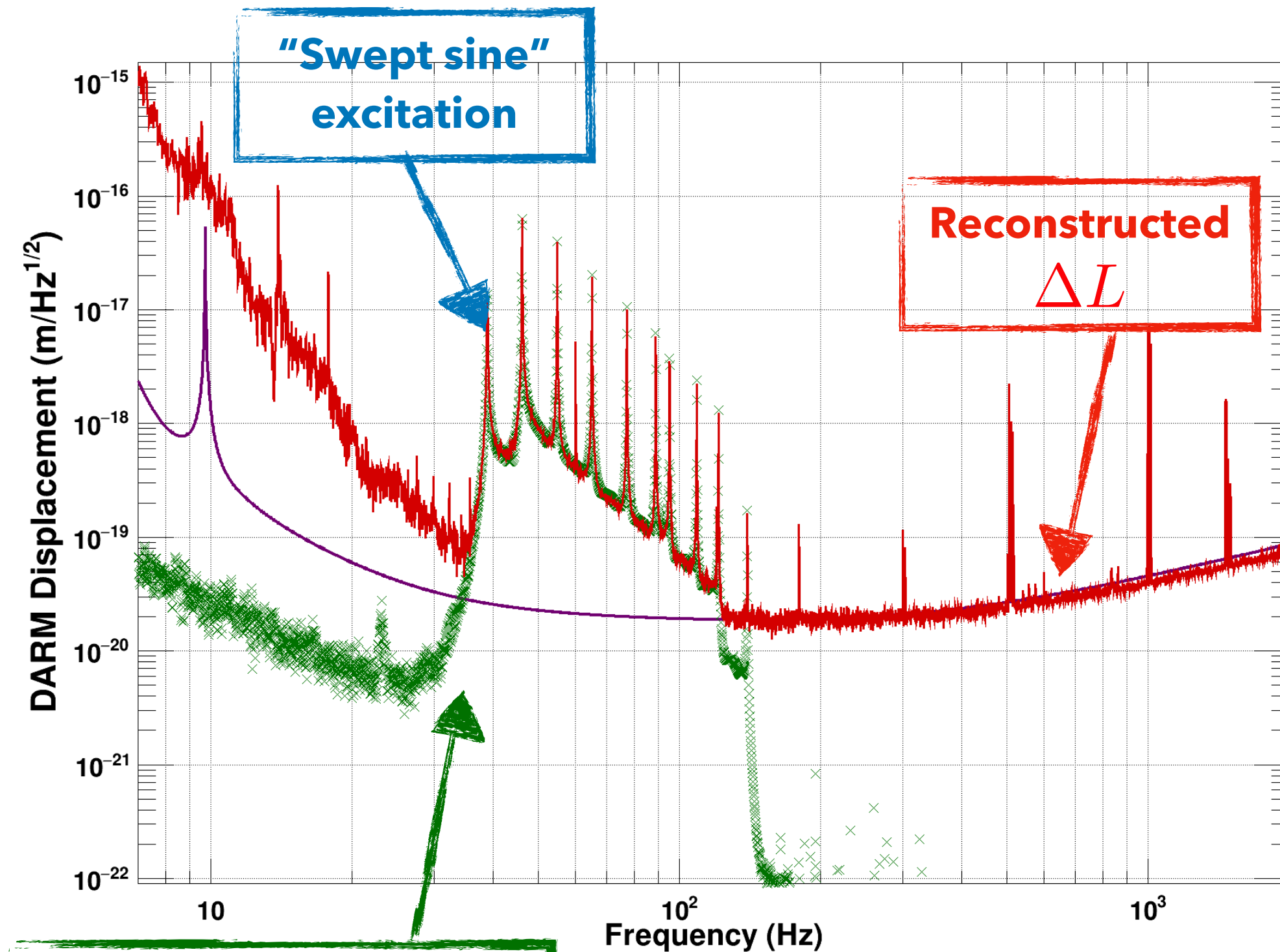
Example: OMC DCPD Whitening chassis D1002559

Rich Abbott, <https://alog.ligo-wa.caltech.edu/aLOG/index.php?callRep=47254>

# A brief flowchart of calibration procedure



# Take measurements and build the model



**Reconstructed Pcal injection signal  $\Delta L_{\text{Pcal}}$**

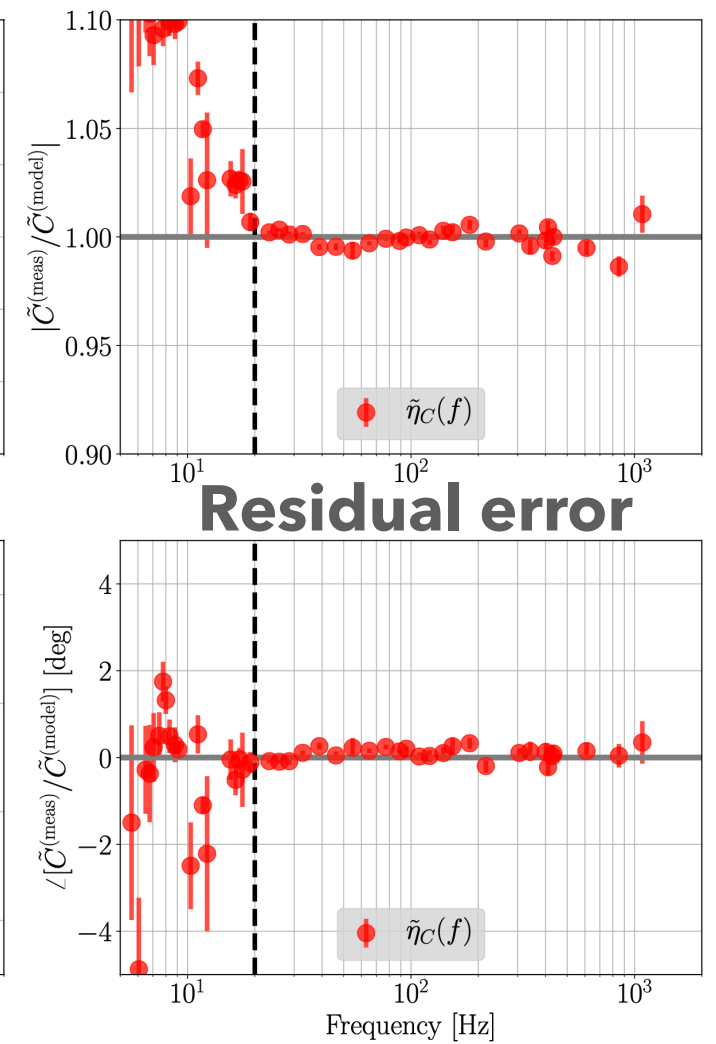
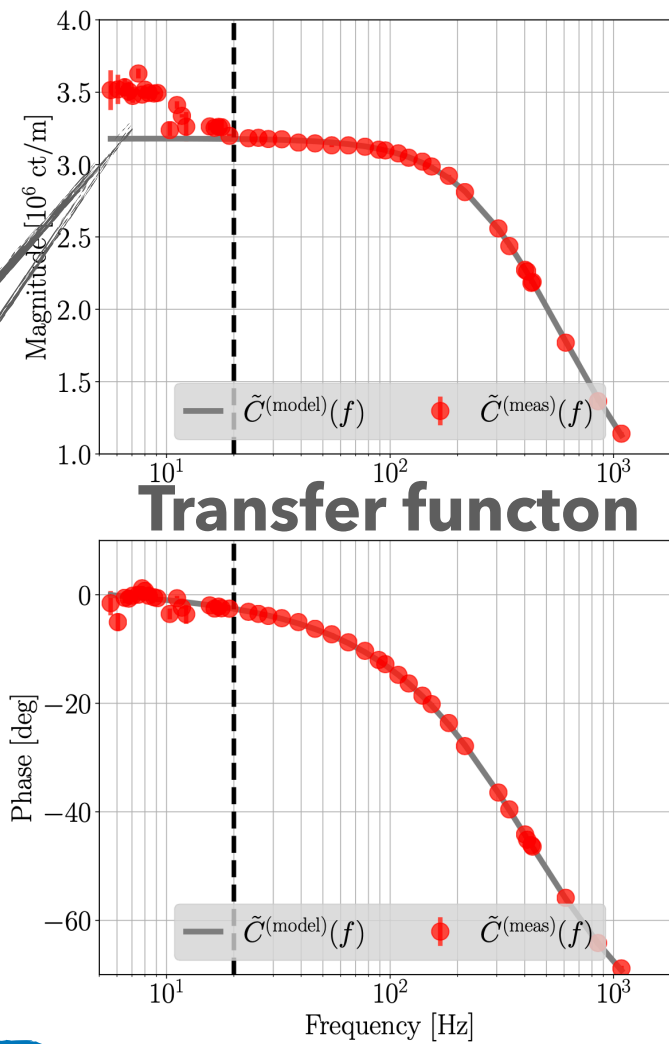
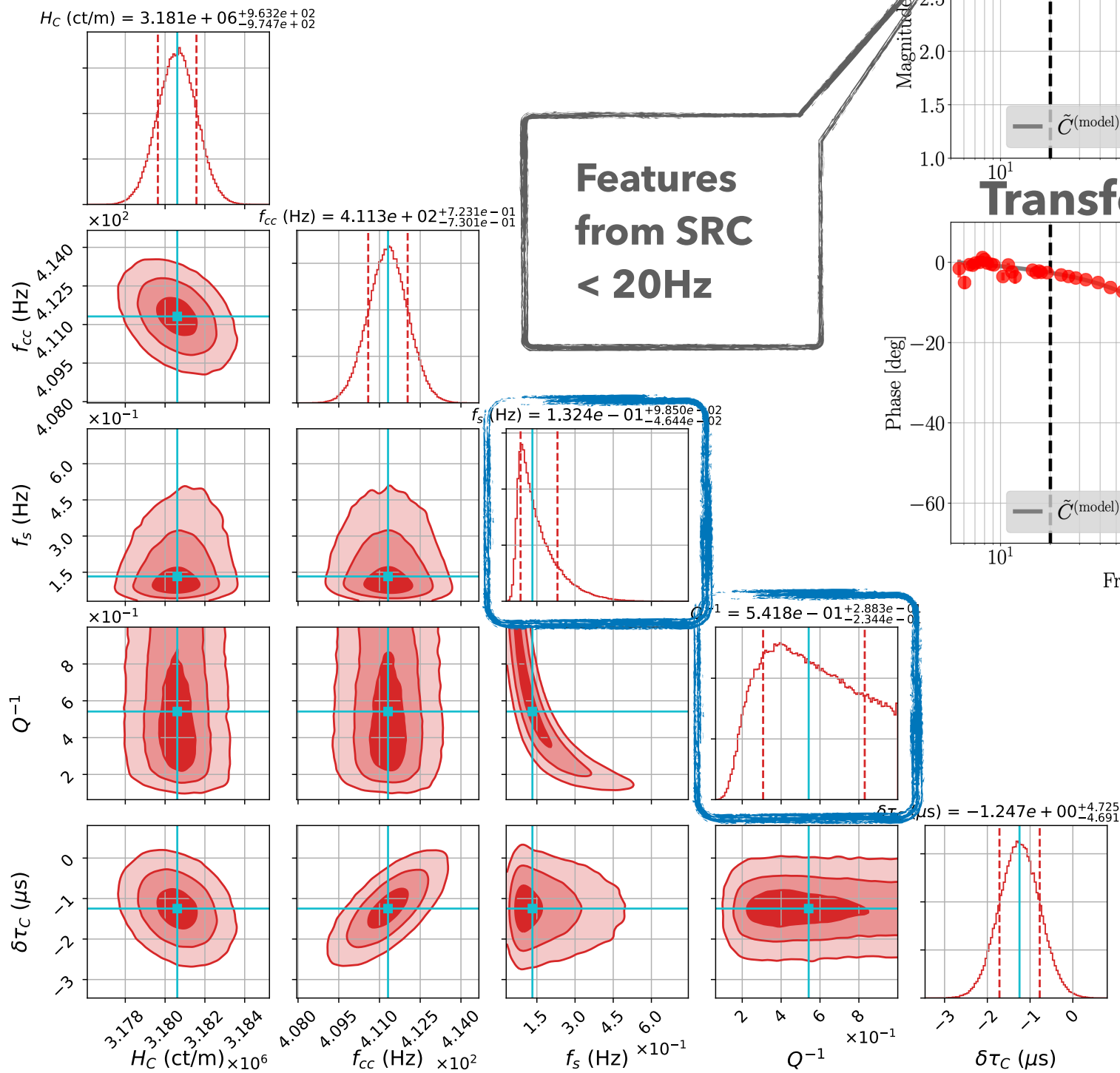
Credit: J Kissel, G1900397



# Parameter estimation and build the model

**H1 Sensing example;  
similar for 3 actuation stages**

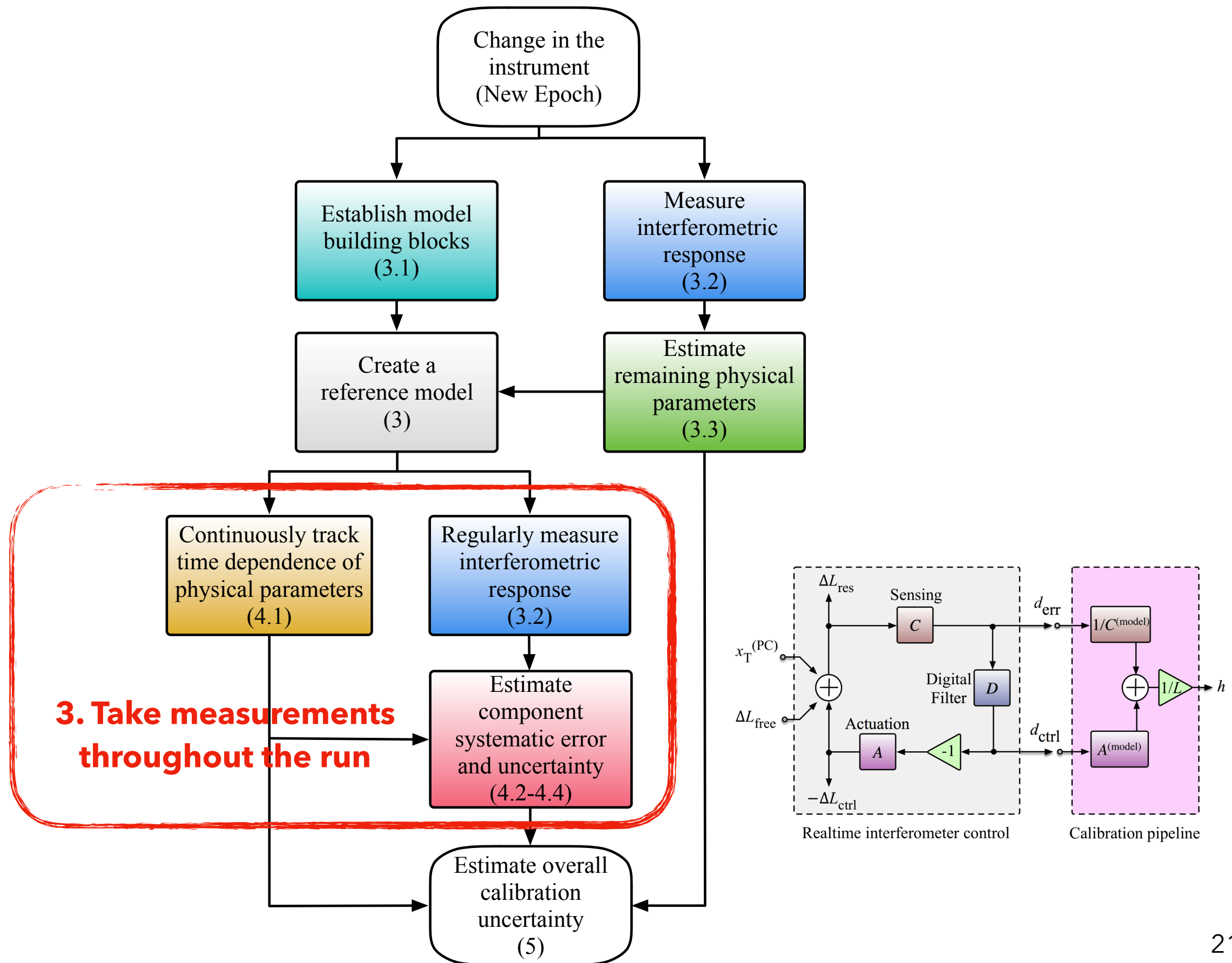
**Features  
from SRC  
< 20Hz**



$$\tilde{C}^{\text{static}}(f) = \left( \frac{H_C}{1 + if/f_{cc}} \right) \times \left( \frac{f^2}{f^2 + f_s^2 - if f_s/Q} \right) \times C_R(f) \exp[-2\pi if \tau_c]$$

Reference model (green box) points to the first term.  
Poorly measured (blue text) points to the second term.  
Poorly measured (red text) points to the denominator of the second term.

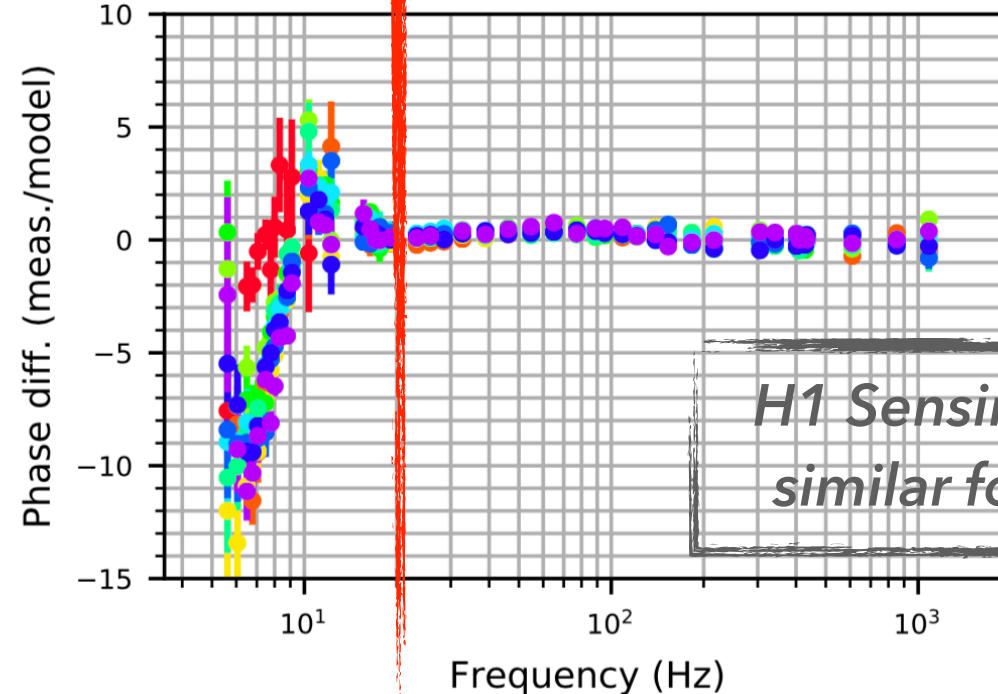
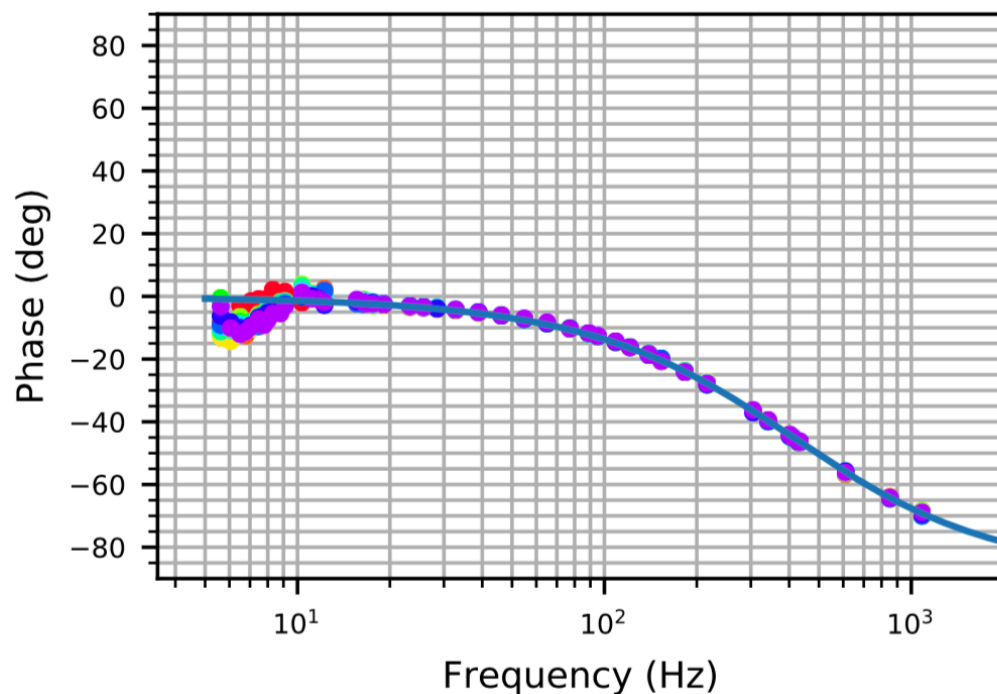
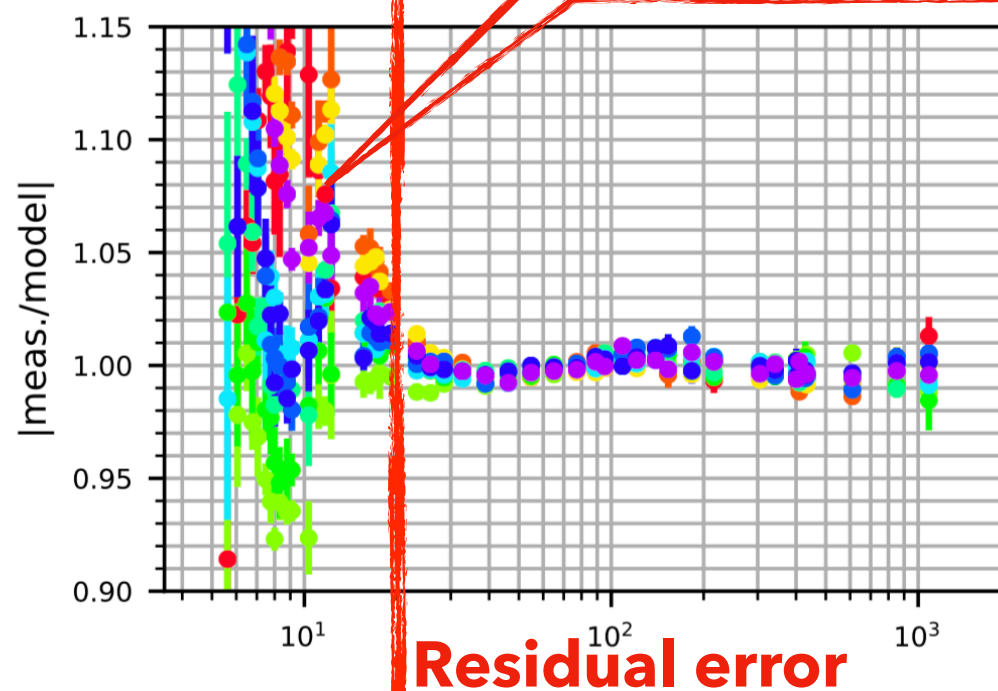
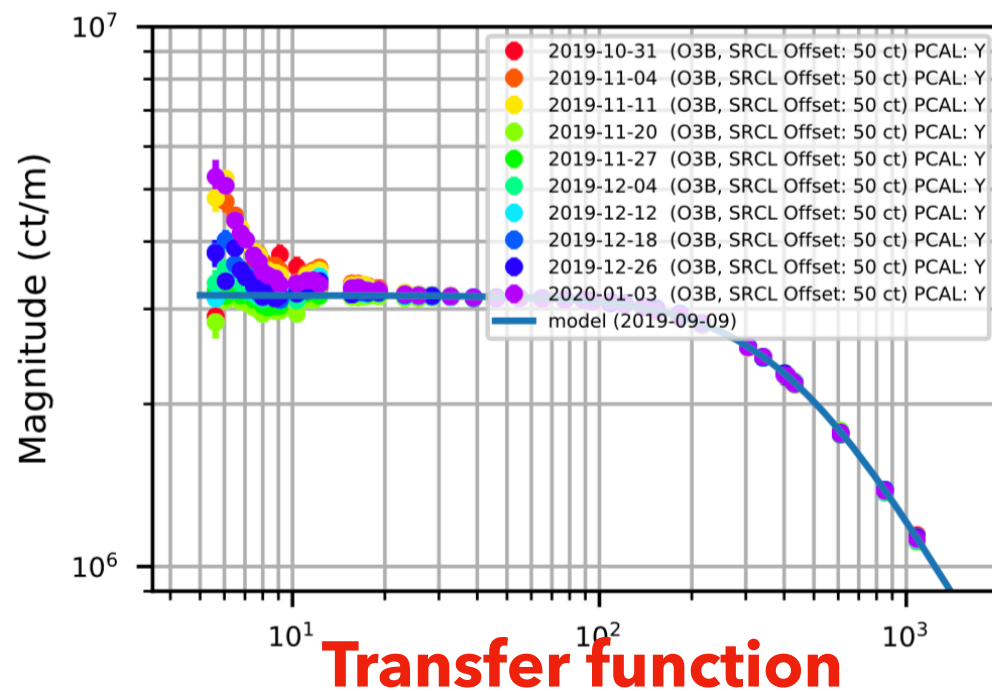
# A brief flowchart of calibration procedure



# Stack multiple measurements

- Collect multiple "swept sine" measurements
- Correct for time dependence
- Stack them together to infer residual error and uncertainty

- *What's happening < 20Hz?*
- *How much does that contribute to the overall uncertainty?*

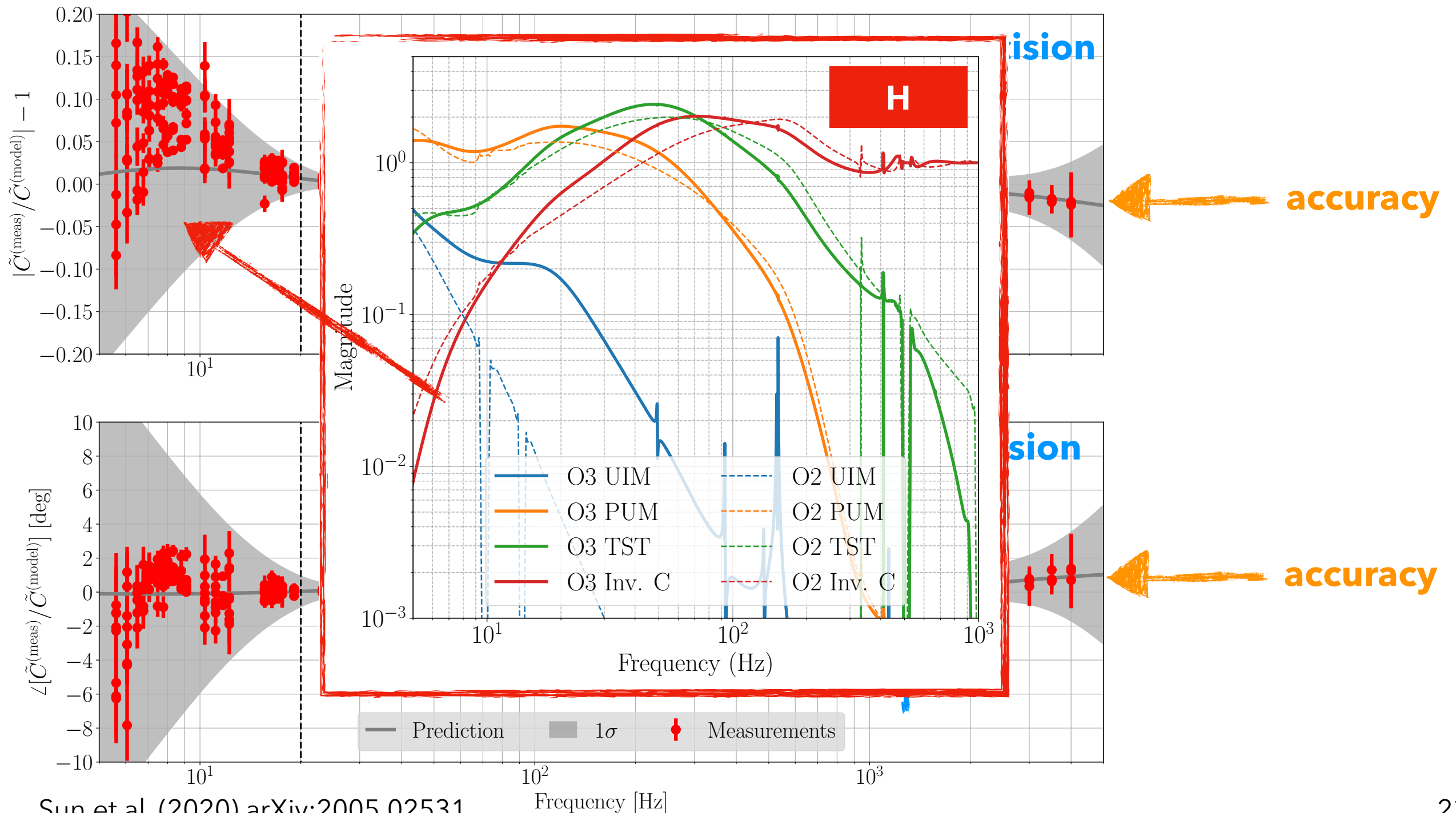


*H1 Sensing example;  
similar for actuation*



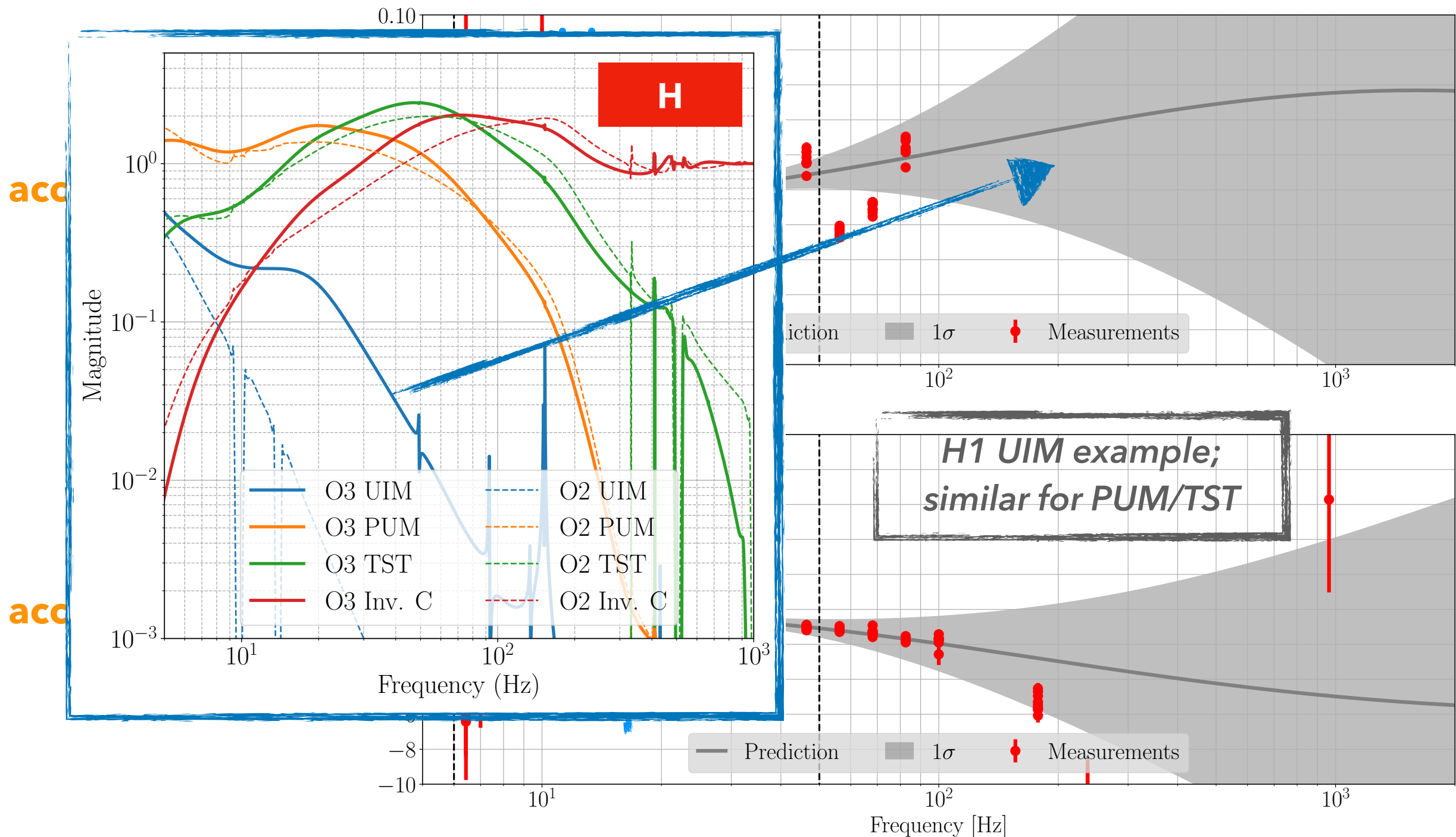
# Estimate residual error and statistical uncertainty (GPR)

- Collect multiple “swept sine” measurements
- Correct for time dependence, and stack all measurements
- Input all the residuals (from all measurements) into **Gaussian Process Regression**

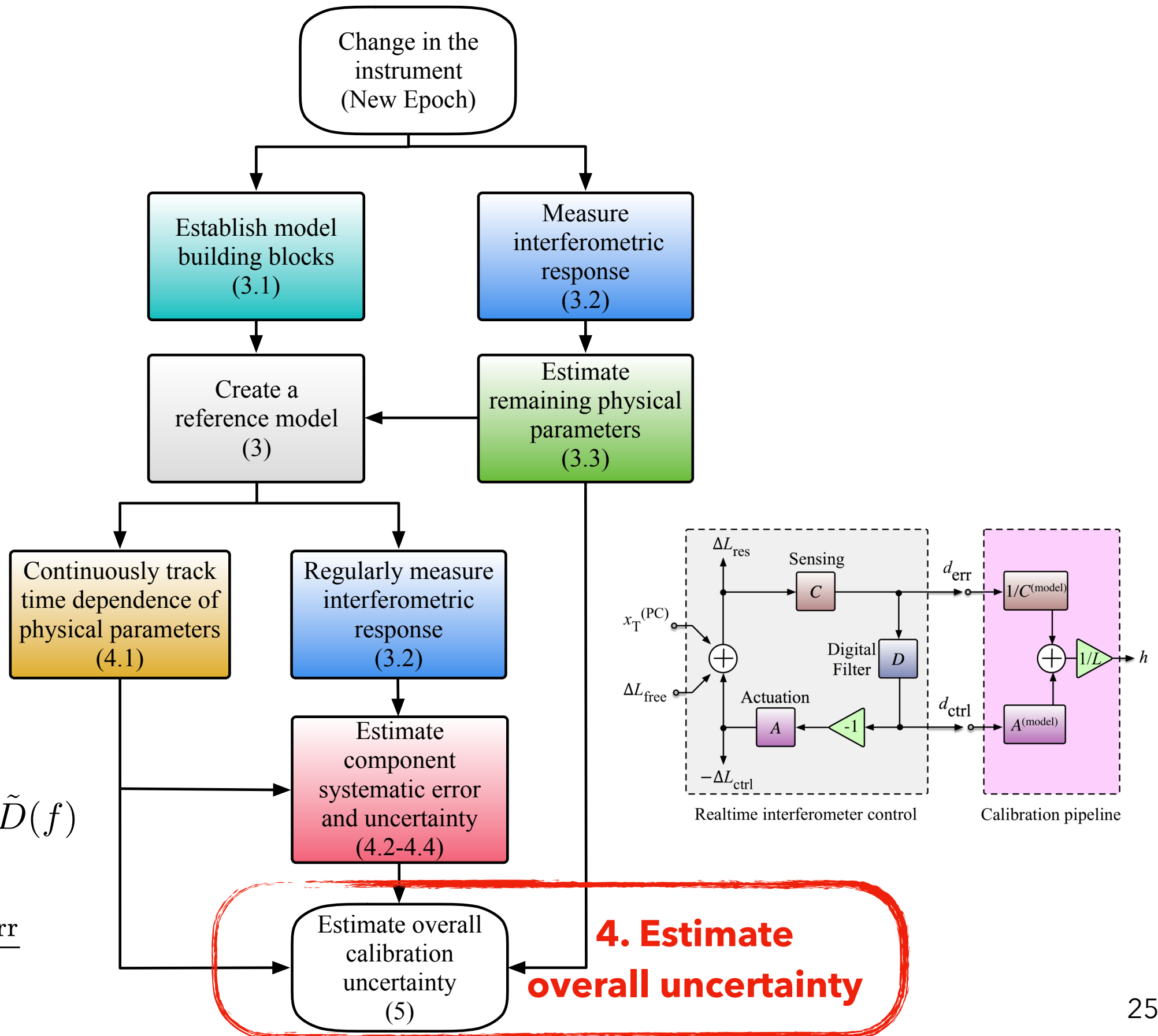


# Estimate residual error and statistical uncertainty (GPR)

- Another example – H1 UIM actuator



# A brief flowchart of calibration procedure



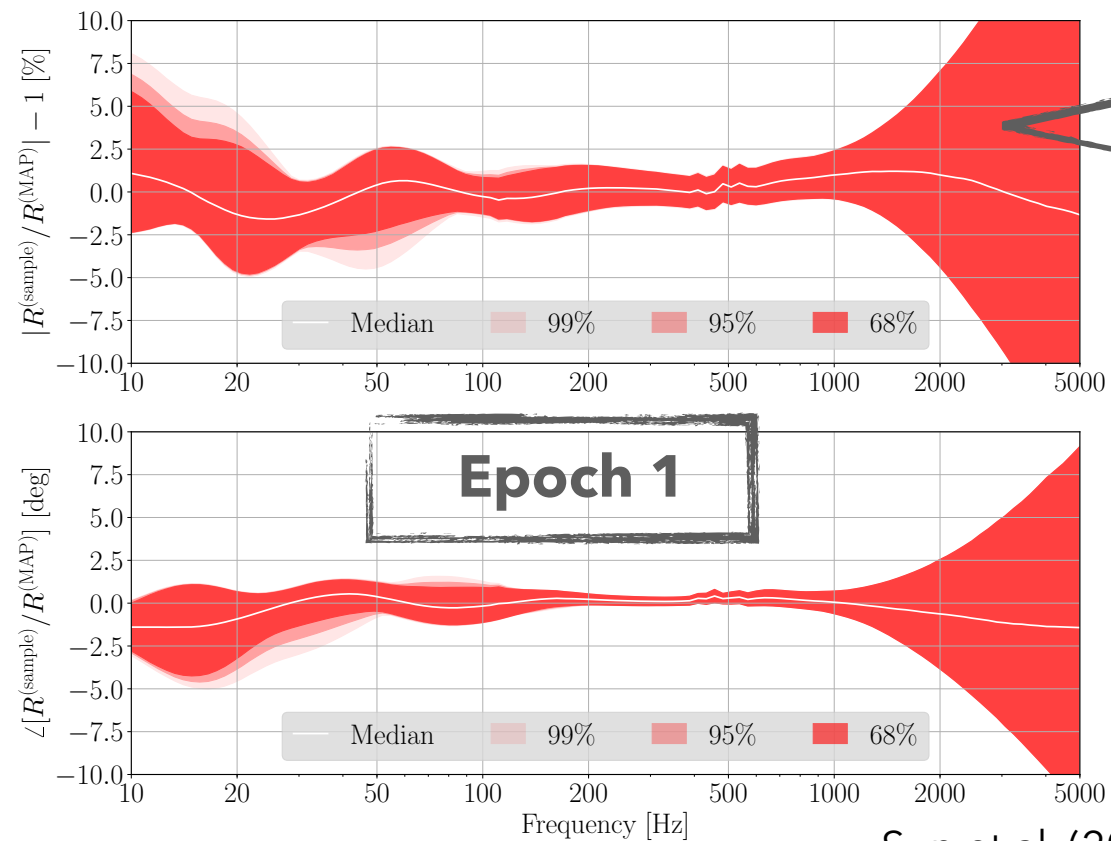
$$\tilde{R}(f) = \frac{1}{\tilde{C}(f)} + \tilde{A}(f)\tilde{D}(f)$$

$$h = \frac{R^{(model)} * d_{err}}{L}$$

# O3A final products (Hanford)

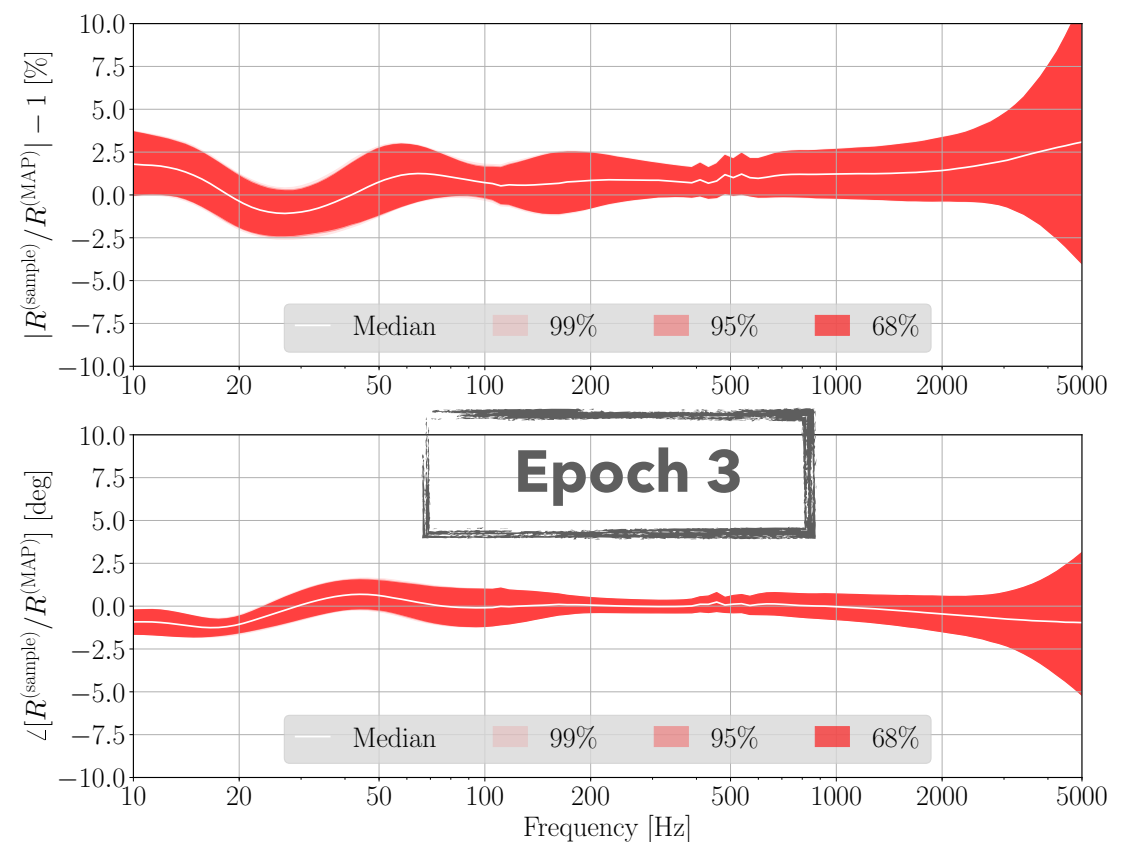
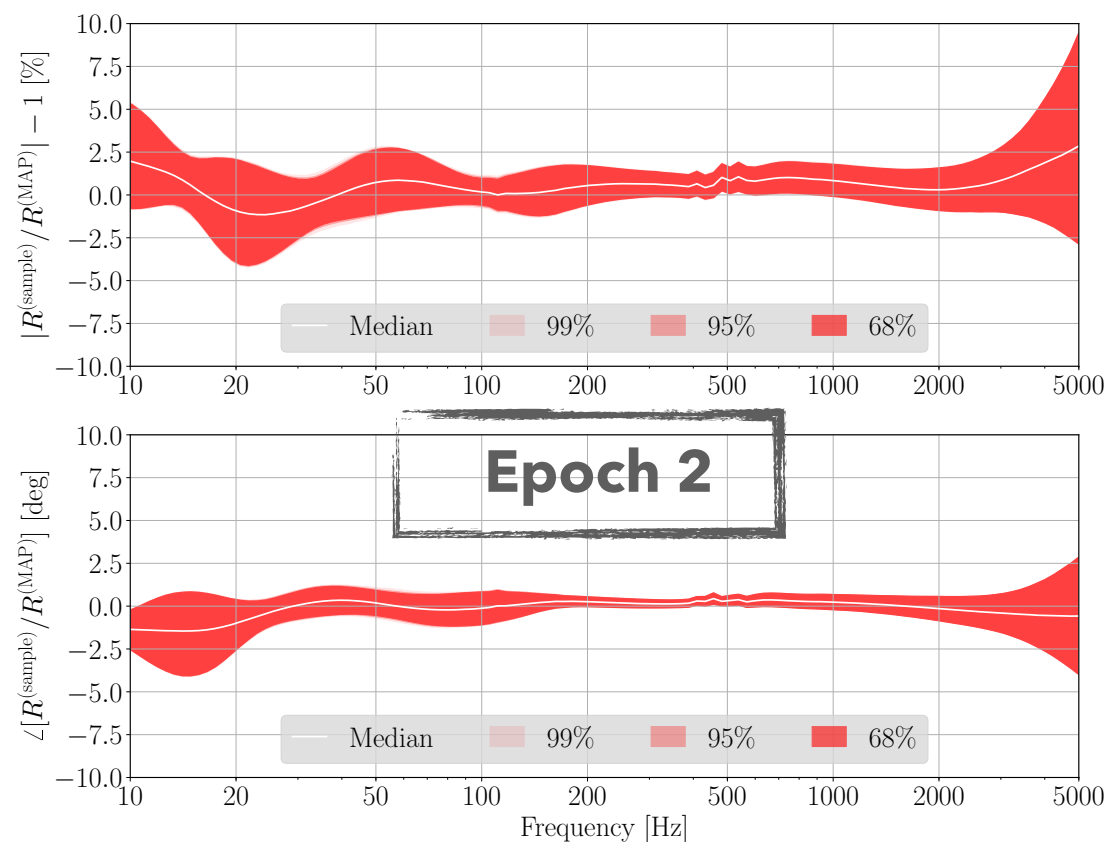
$$\tilde{R}(f) = \frac{1}{\tilde{C}(f)} + \tilde{A}(f)\tilde{D}(f)$$

- 1-sigma limits of systematic error and associated statistical uncertainty
- Excursion from unity magnitude/zero phase



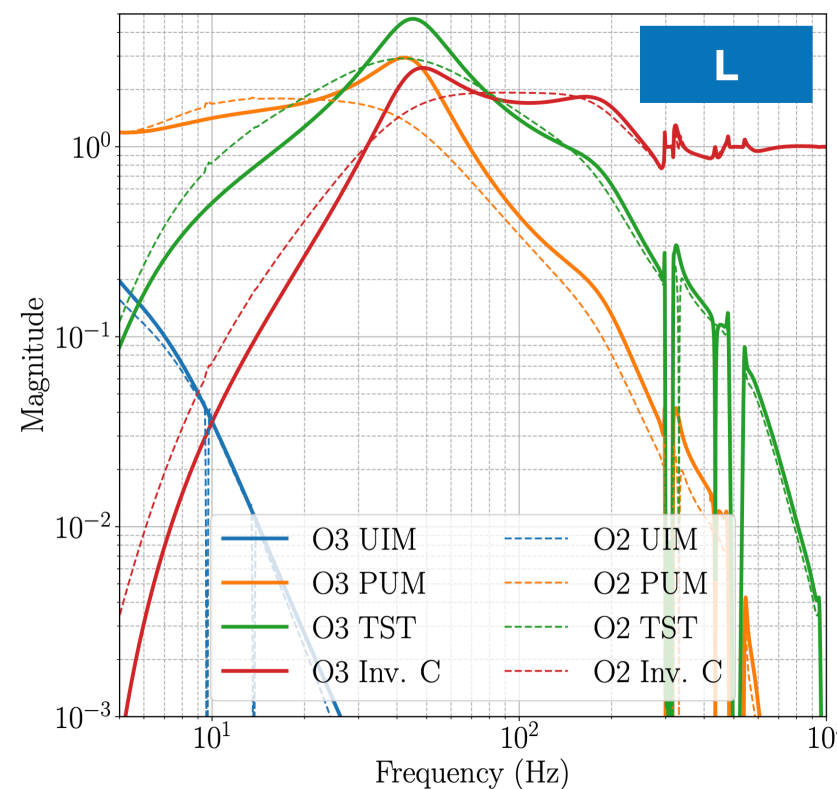
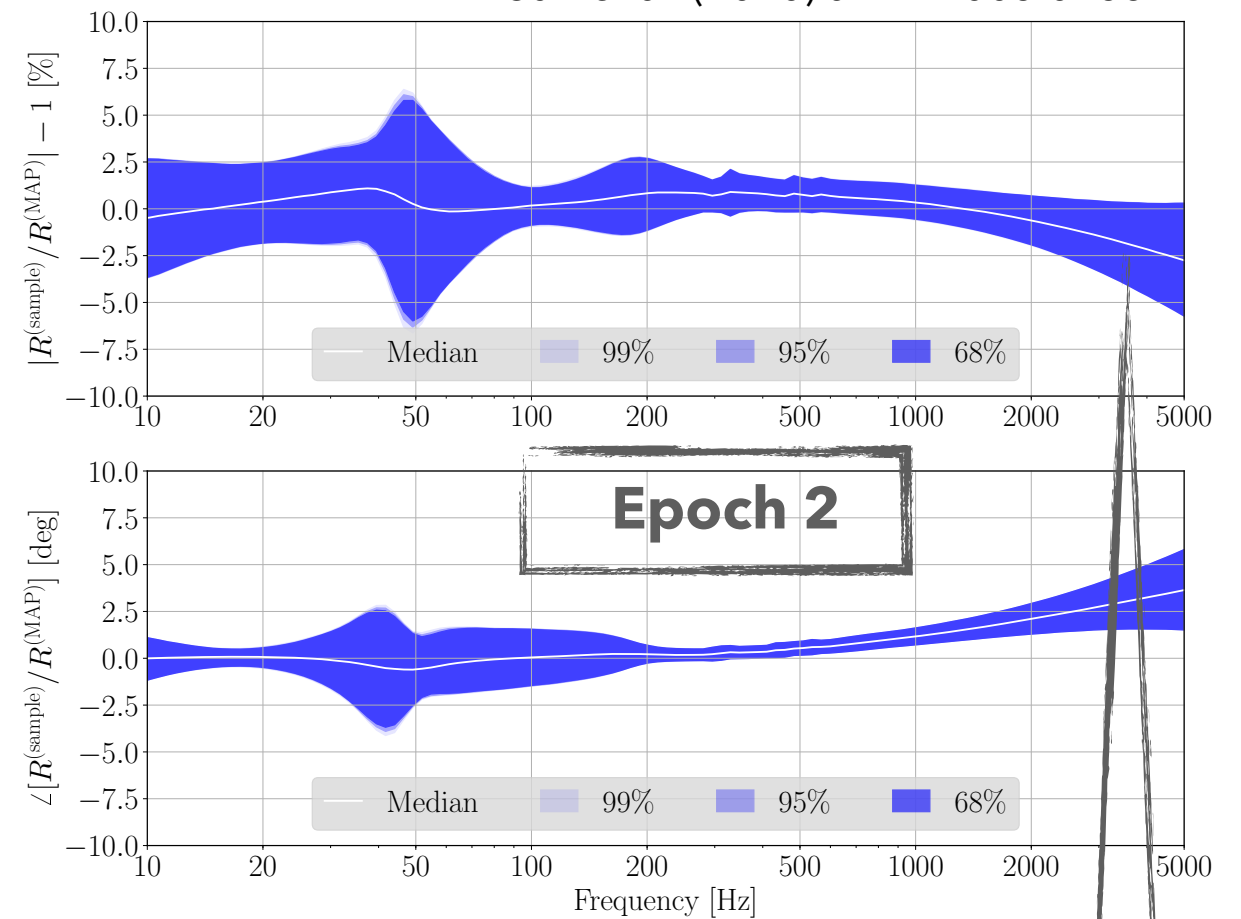
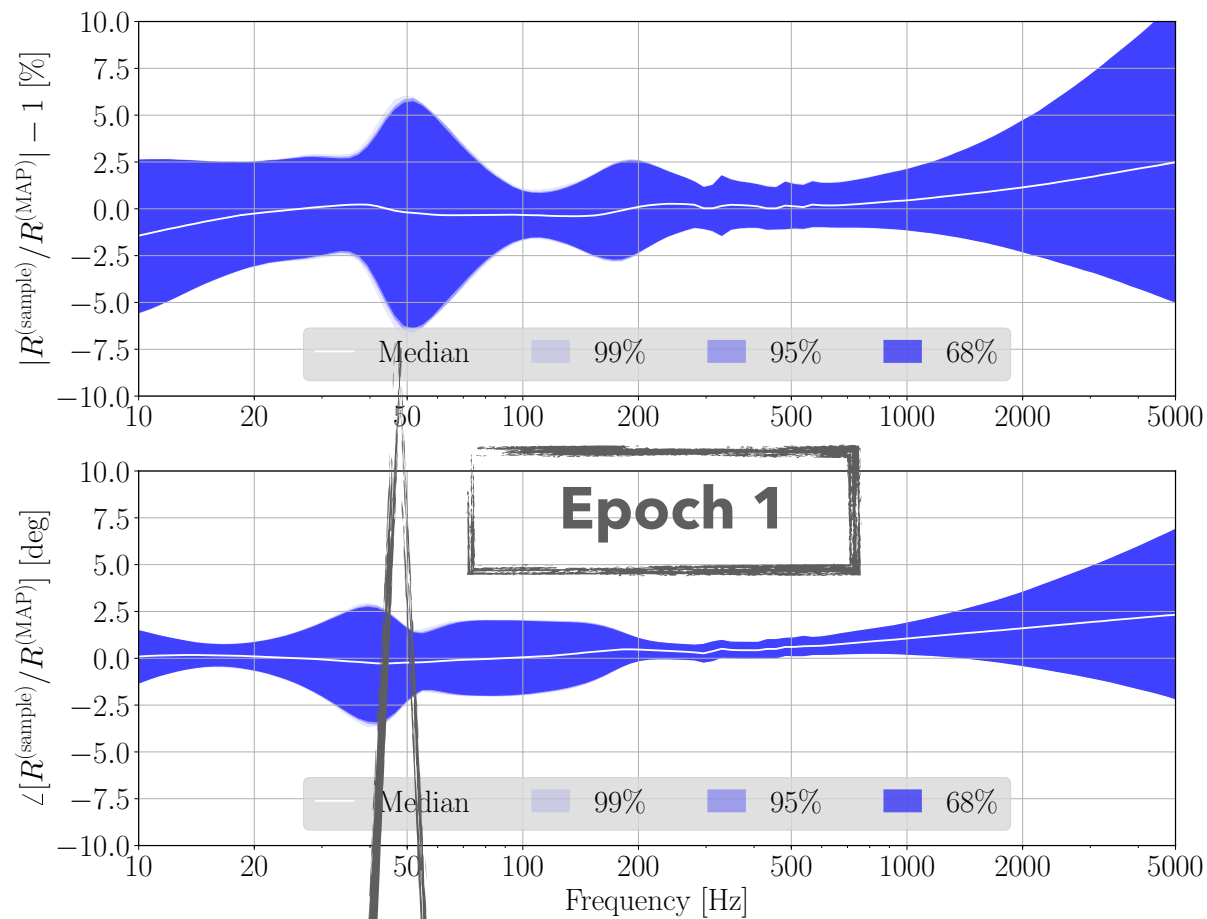
• Not yet taken high-frequency measurements

Sun et al. (2020) arXiv:2005.02531



# O3A final products (Livingston)

Sun et al. (2020) arXiv:2005.02531



- Larger uncertainty due to PUM/TST actuation authority choice in Livingston
- Changed from O2 to O3

- Improved by high frequency measurements

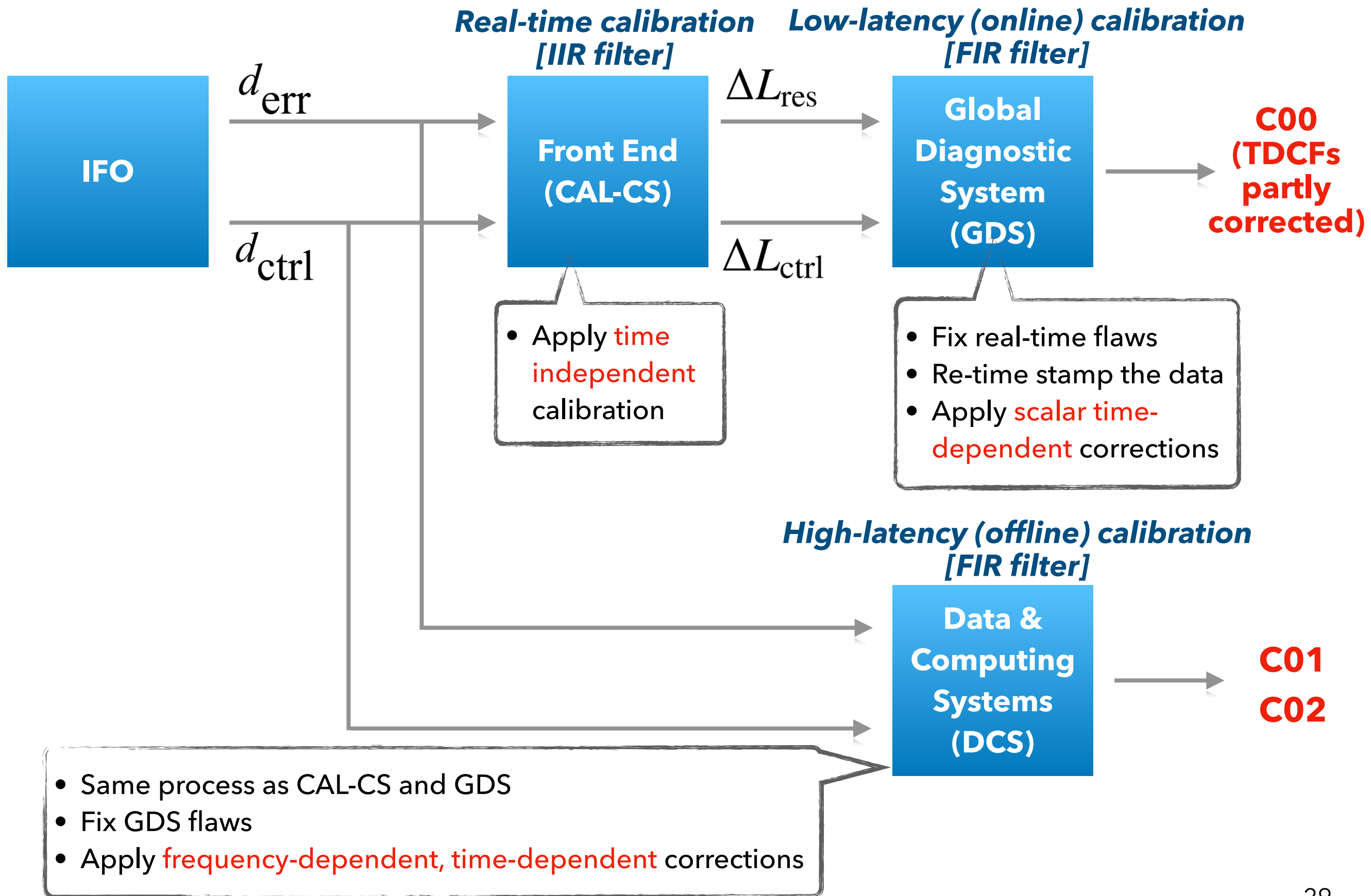
# Agenda

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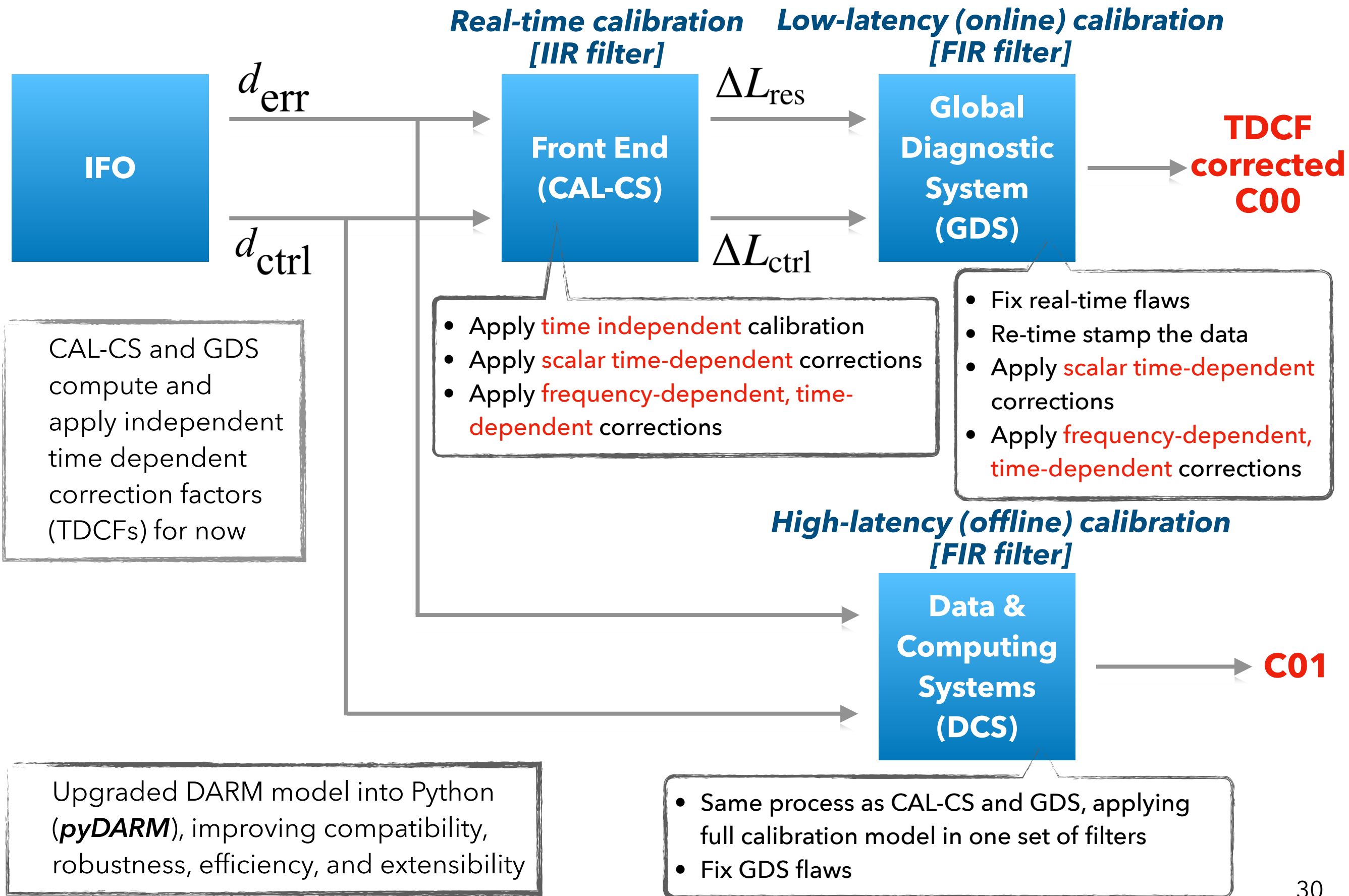
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- Understanding systematics and uncertainties
- **O3 improvements and future perspectives**



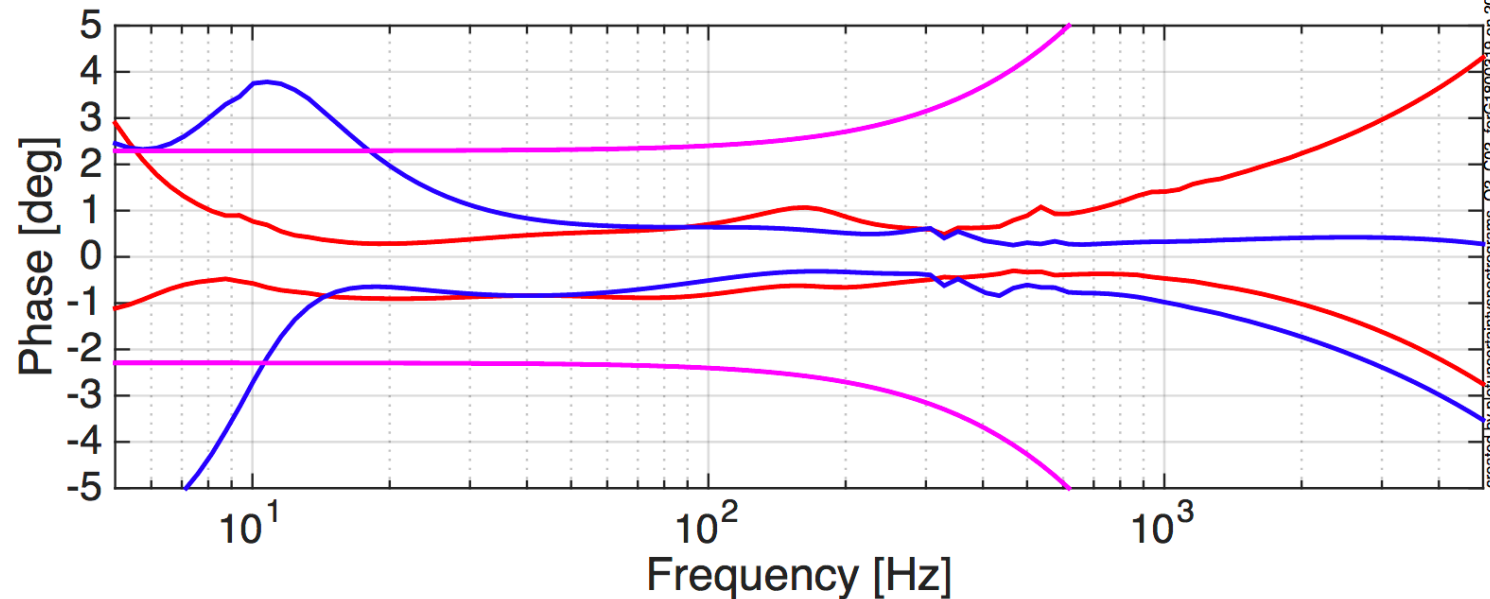
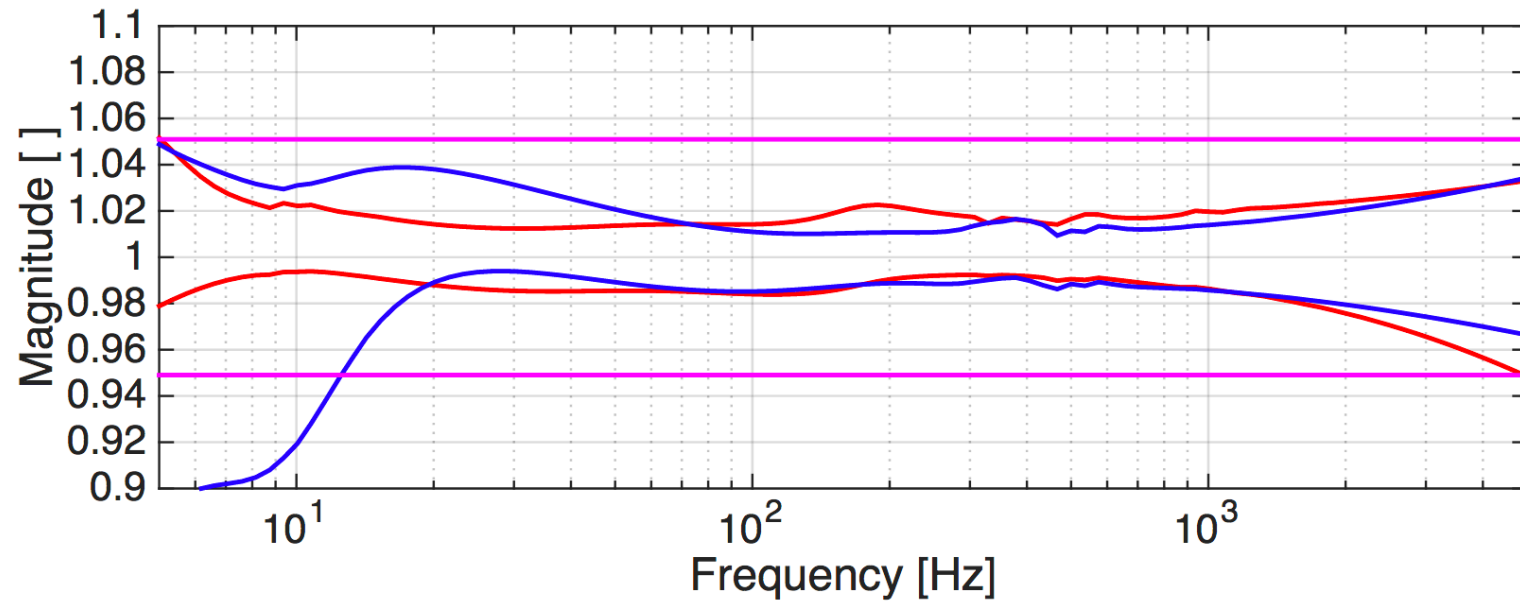
# What we had in O2



# What's new in O3



# Best calibration product in O2

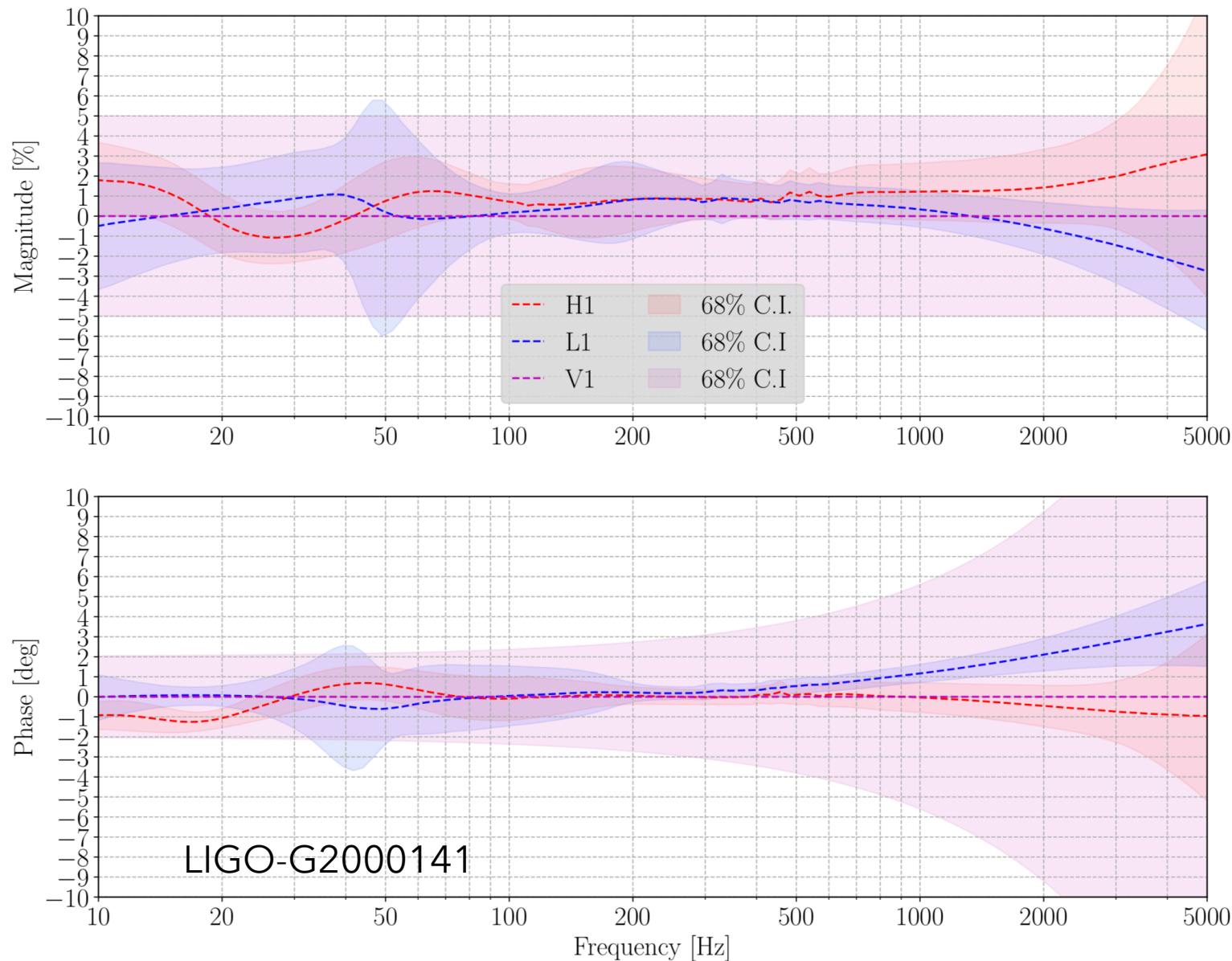


created by plotuncertaintyspectrograms\_O2\_CO2\_forG1800319 on 20-Mar-2018

- Maximum excursion of the 1-sigma limits of **systematic error and statistical uncertainty** from unity magnitude/zero phase (20–1024 Hz):
  - Magnitude error: **~2-3 %**
  - Phase error: **~2-3 deg**
  - **~1%** (mag) and **~1 deg** (phase) in the most sensitive region (~100 Hz)

- Best results achieved in offline calibration (3 months after O2 ended)
  - time-dependent variations (TDCFs) were corrected

# Calibration product in O3A

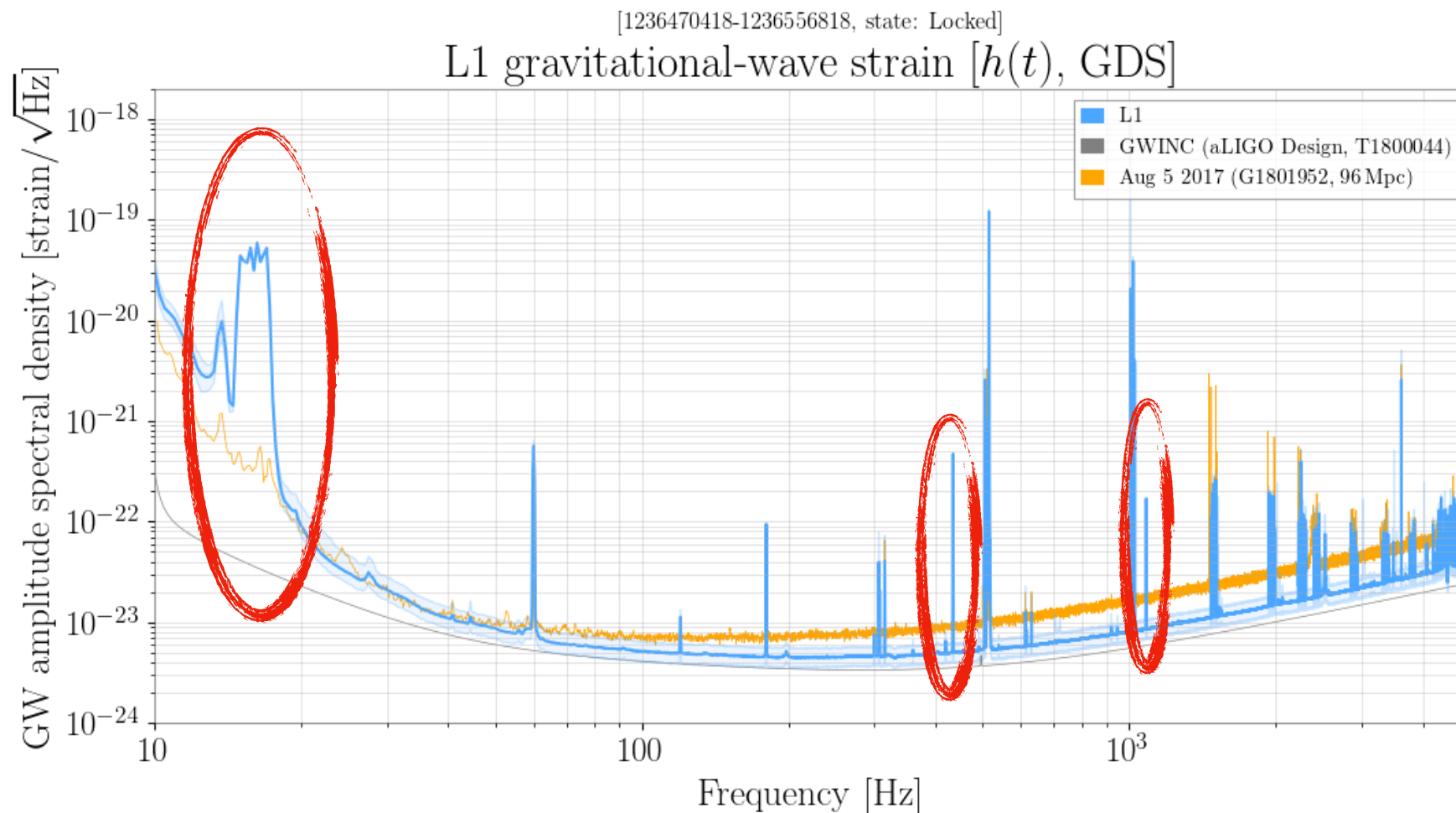


- Maximum excursion of the 1-sigma limits of **systematic error and statistical uncertainty** from unity magnitude/zero phase (20–1024 Hz):

- Magnitude error: **~2-6 %**
- Phase error: **~2-3 deg**
- **~2%** (mag) and **~2 deg** (phase) in the most sensitive region (~100 Hz)

- Low-latency data quality has been improved (all TDCFs applied)
- Same level of precision and accuracy in the most sensitive band
- Remember that interferometers significantly changed from O2 to O3

# Calibration lines moved to new frequencies



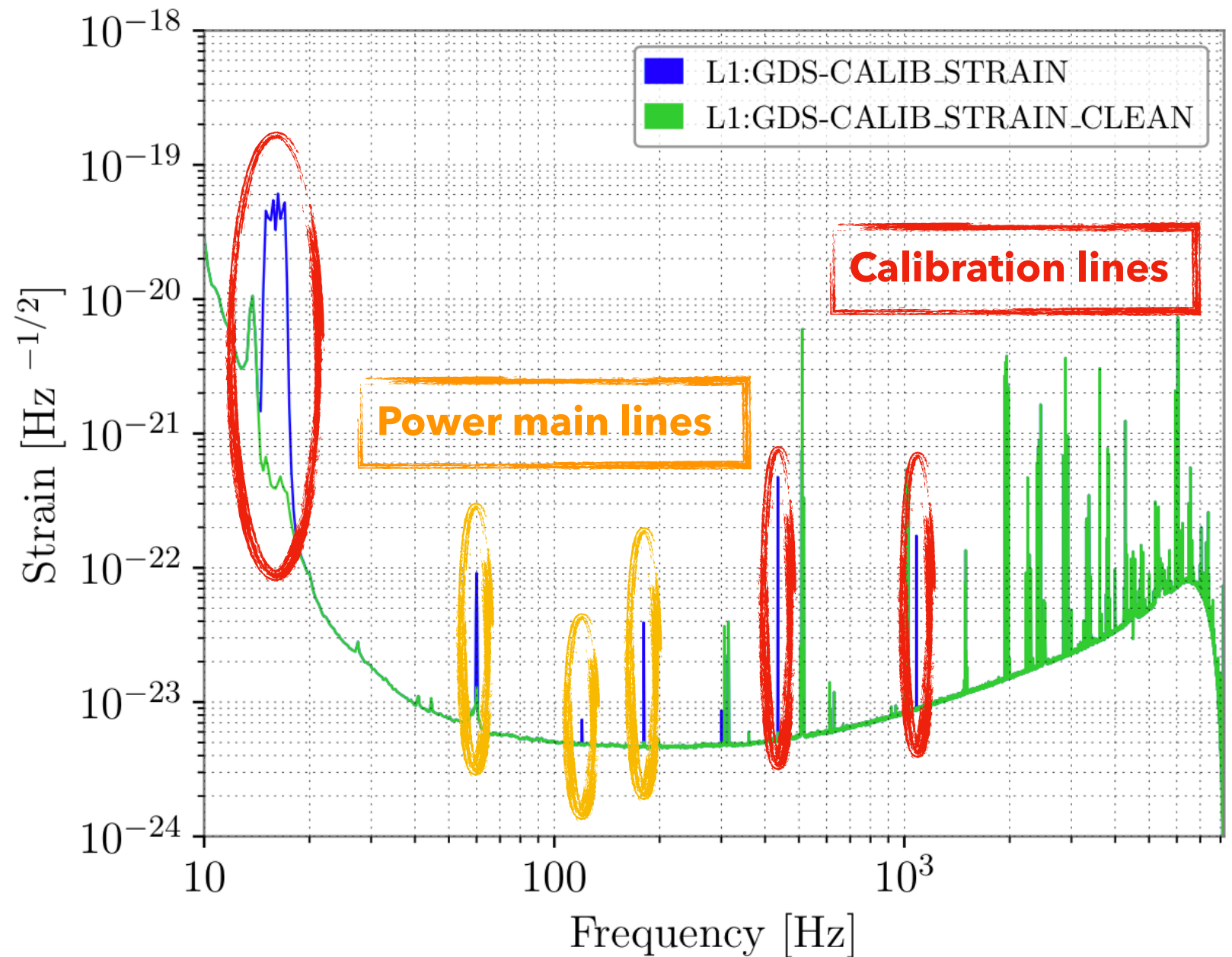
H1 Freq (Hz)	L1 Freq (Hz)
15.6	15.1
16.4	15.7
17.1	16.3
17.6	16.9
410.3	434.9
1083.7	1083.1

- Purpose:
  - Better characterize the new IFOs
  - Facilitate calculation of time-dependent correction factors
  - Move out of the most sensitive, astrophysically interesting band of the detectors
- Actuator lines (O2: H1 ~35, L1 ~15Hz) -> both IFOs to ~15 Hz for O3, out of astro-detection band
- Sensor line (O2: ~330 Hz) -> both IFOs to ~430 Hz
- Injected at different places in the DARM loop for different purposes



# Low-latency Line Subtraction

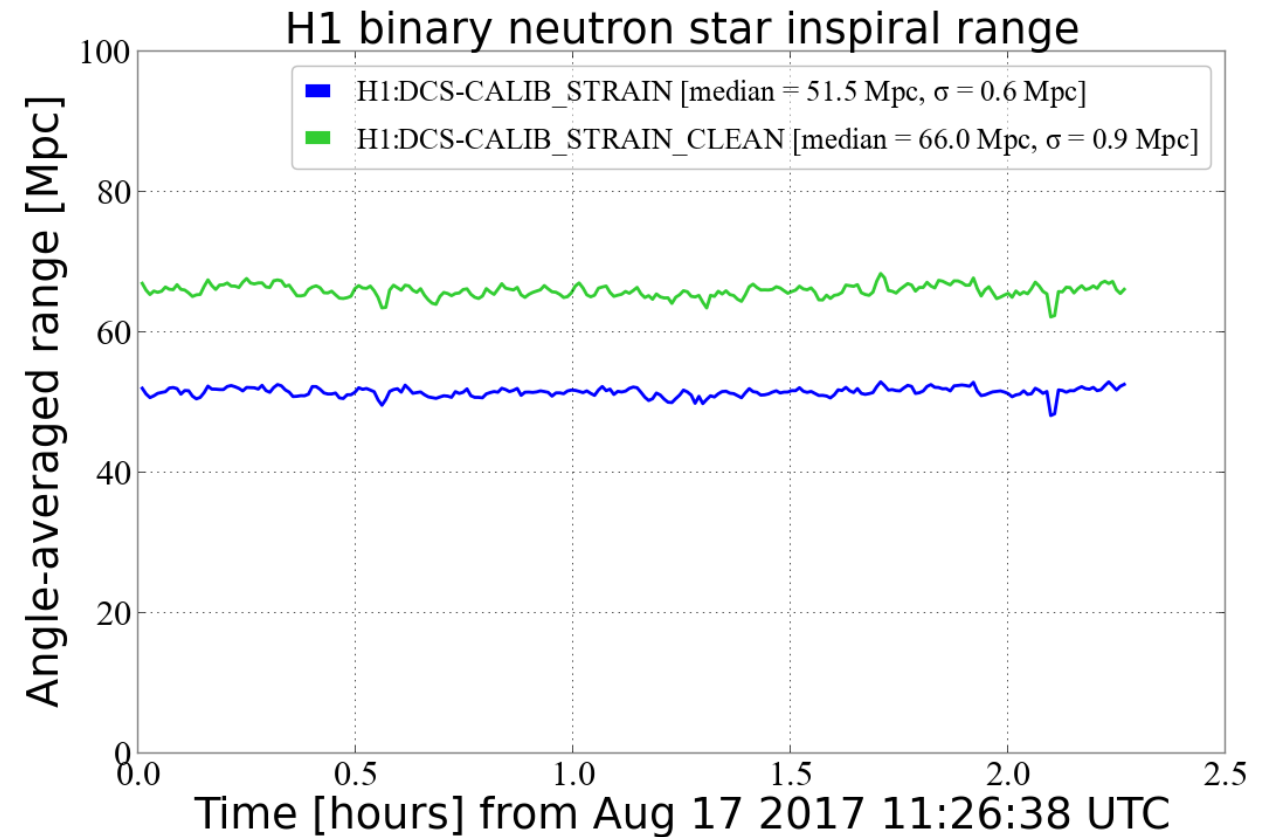
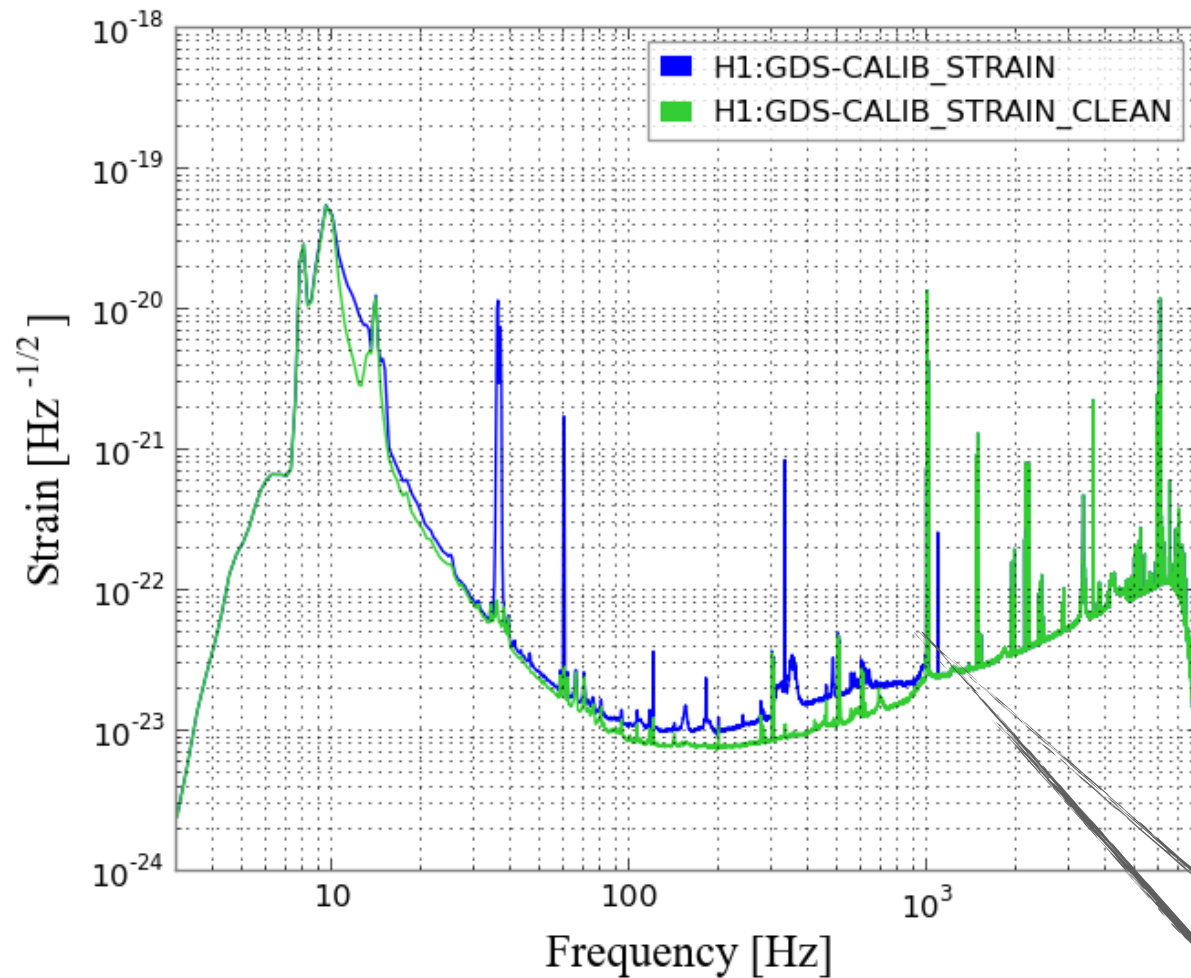
- Additional channel in C00 frames: **GDS-CALIB\_STRAIN\_CLEAN**
- Calibration lines and power main lines are subtracted (power main line subtraction is not perfect)
- Line subtraction is done in **low latency**
- Negligible impact on calibration latency



A. Viets, G1801495



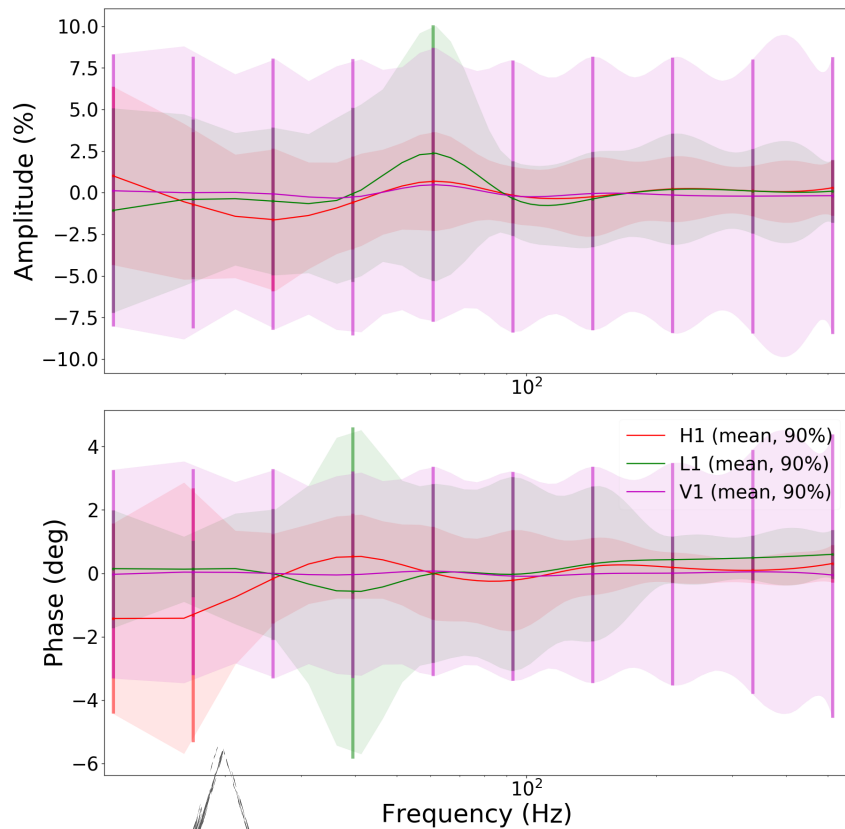
# Future: Low-latency Noise Subtraction



- Low-latency broadband noise subtraction – code frame available
- Similar methods to DetChar's subtraction done in O2
- Require witness channel

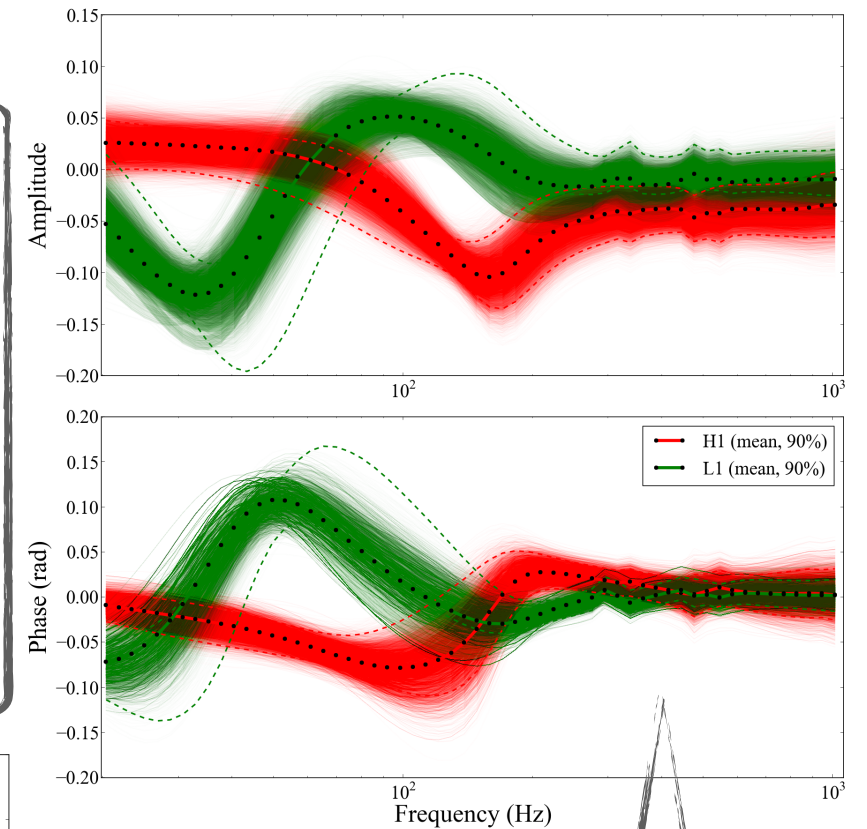
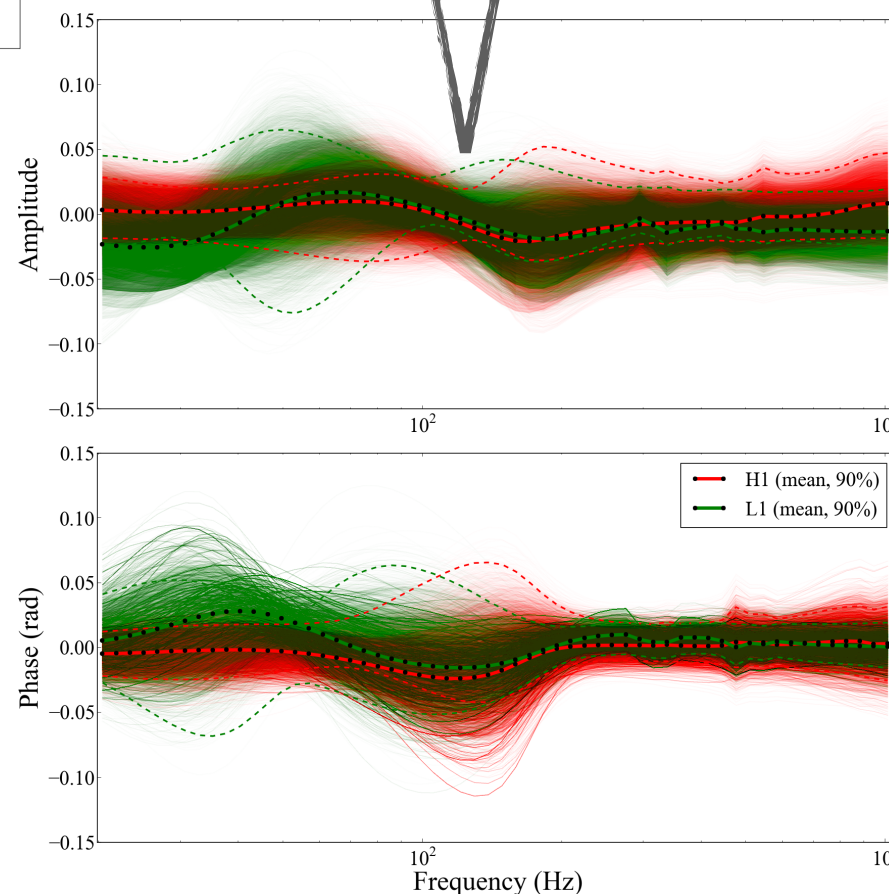
- Example: at time ~GW170817 (excess jitter noise)
- BNS range increases by **28%**
- Total detectable volume increases by **110%**
- In O3, impact has been small

# Future: Astrophysical calibration



- Directly use the samples of detector response function (drawn from calibration parameters) as CBC PE input, estimating **astrophysical** and **calibration** parameters at the same time.

- Have been using calibration error budget produced by calibration team as a **spline** in CBC parameter estimation



- Could larger number of loud events tell us what's wrong in our detector calibration? (assuming waveforms are correct)

*Vitale, Haster, Farr, Payne, Goetz, Hulko, Kissel, Sun*

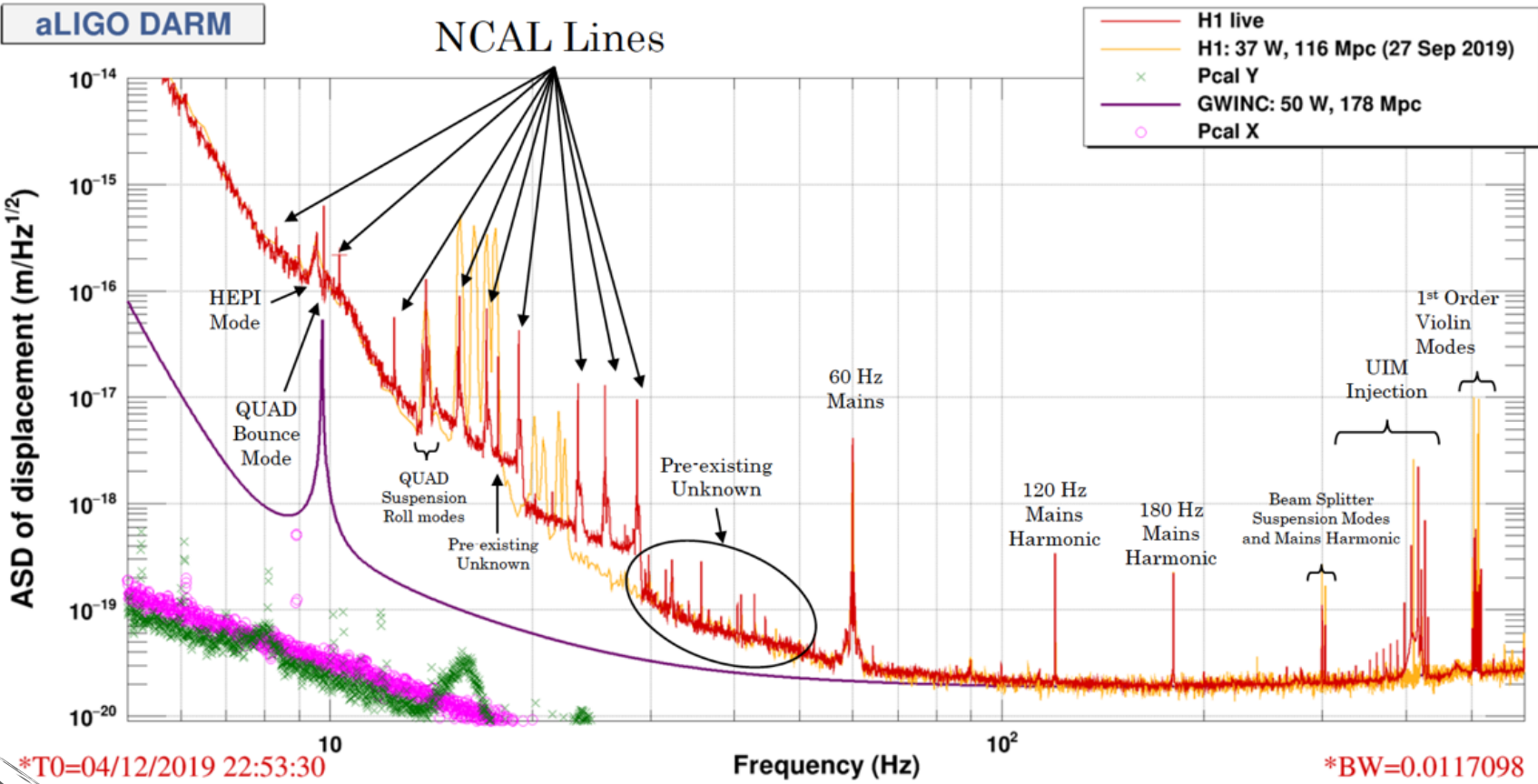
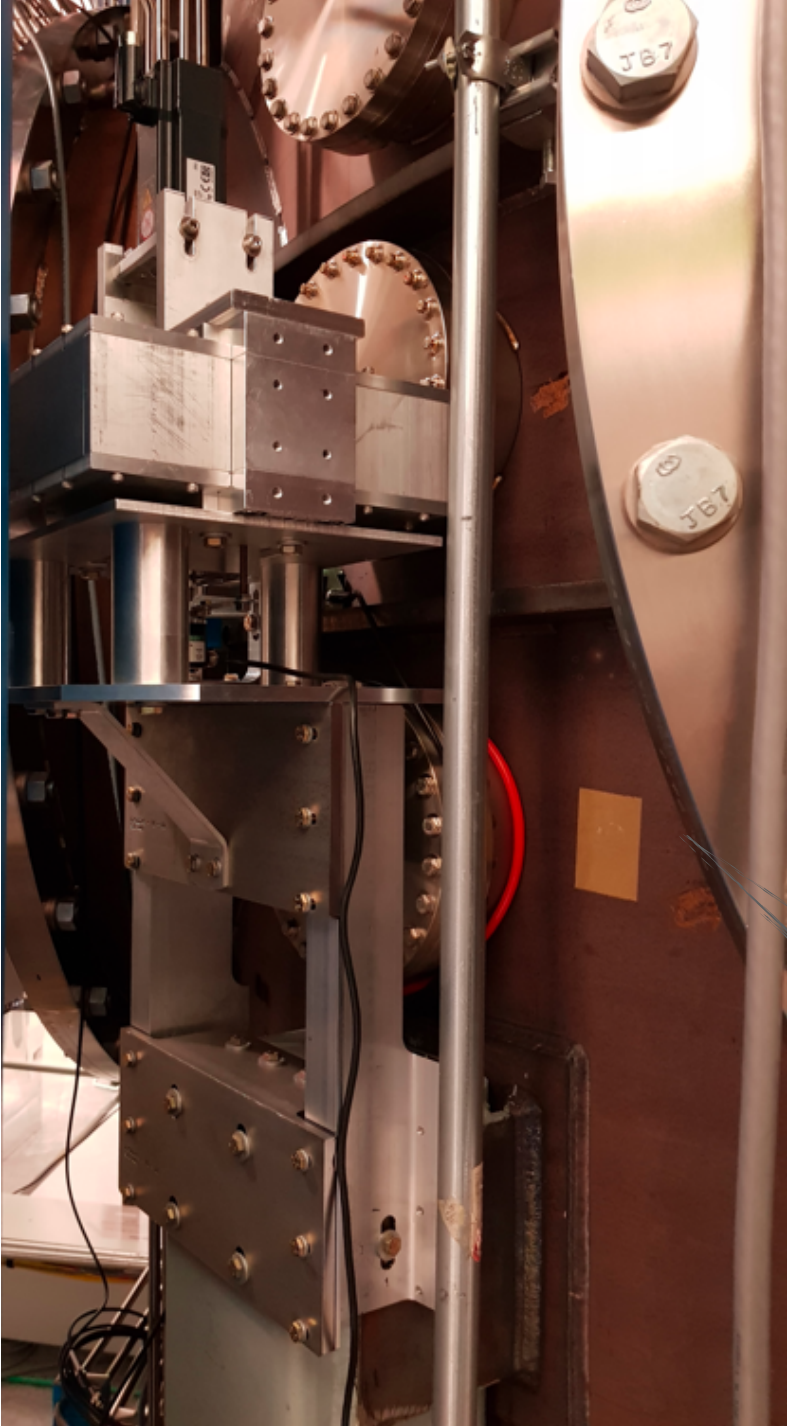
## Future: better accuracy and precision is required

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- Determine the calibration accuracy and precision requirements for future generations of detector network (SNR  $\sim 100$ )
- Quantify the impact of calibration accuracy and precision on astrophysical interpretations, e.g., non-GR physics
- Further improve the absolute reference uncertainty of photon calibrator (already 0.54%)
- Investigate and remove sub-percent systematic errors
- Correct for the high-frequency effects ( $> 2\text{kHz}$ ) caused by the approximation of the detector's response

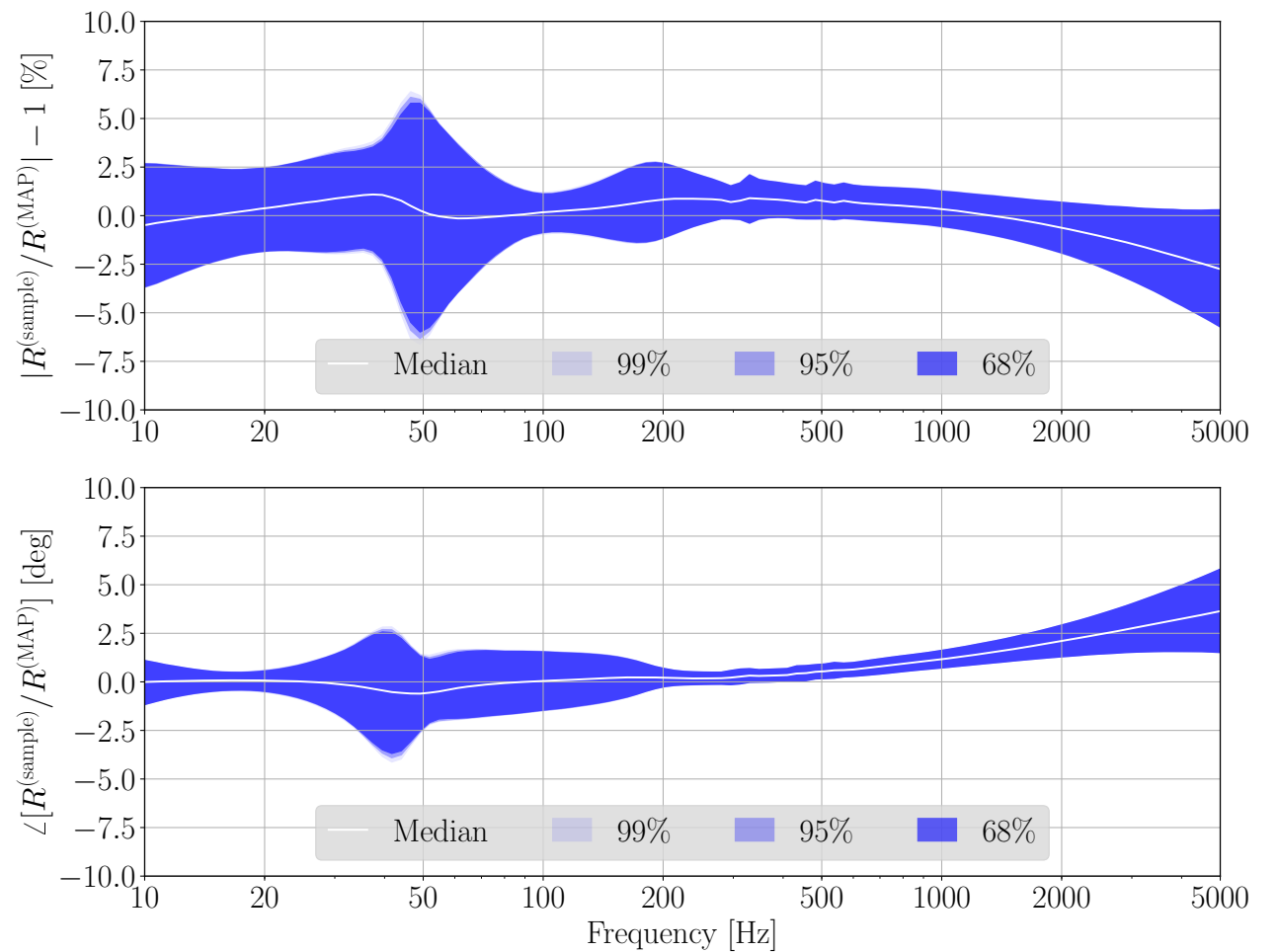
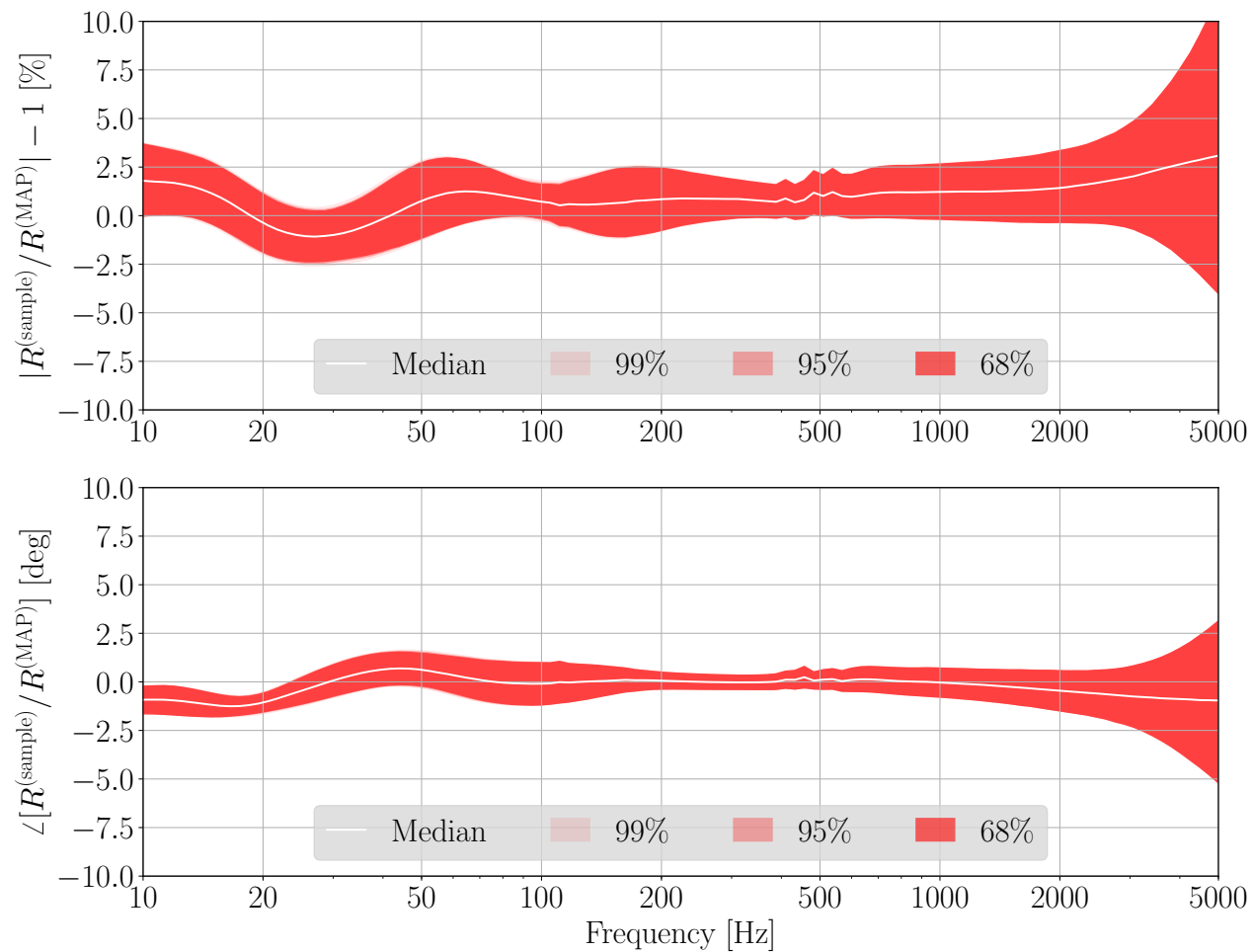


# New techniques: Newtonian calibrator



- Prototype is installed and characterized at Hanford
- NCAL line sweep is seen as expected in DARM

# Summary



- O3a overall calibration uncertainty (20-2000 Hz):
  - ▶ < 7% in magnitude
  - ▶ < 4 deg in phase
- Systematic error alone (20-2000 Hz):
  - ▶ < 2% in magnitude
  - ▶ < 2 deg in phase

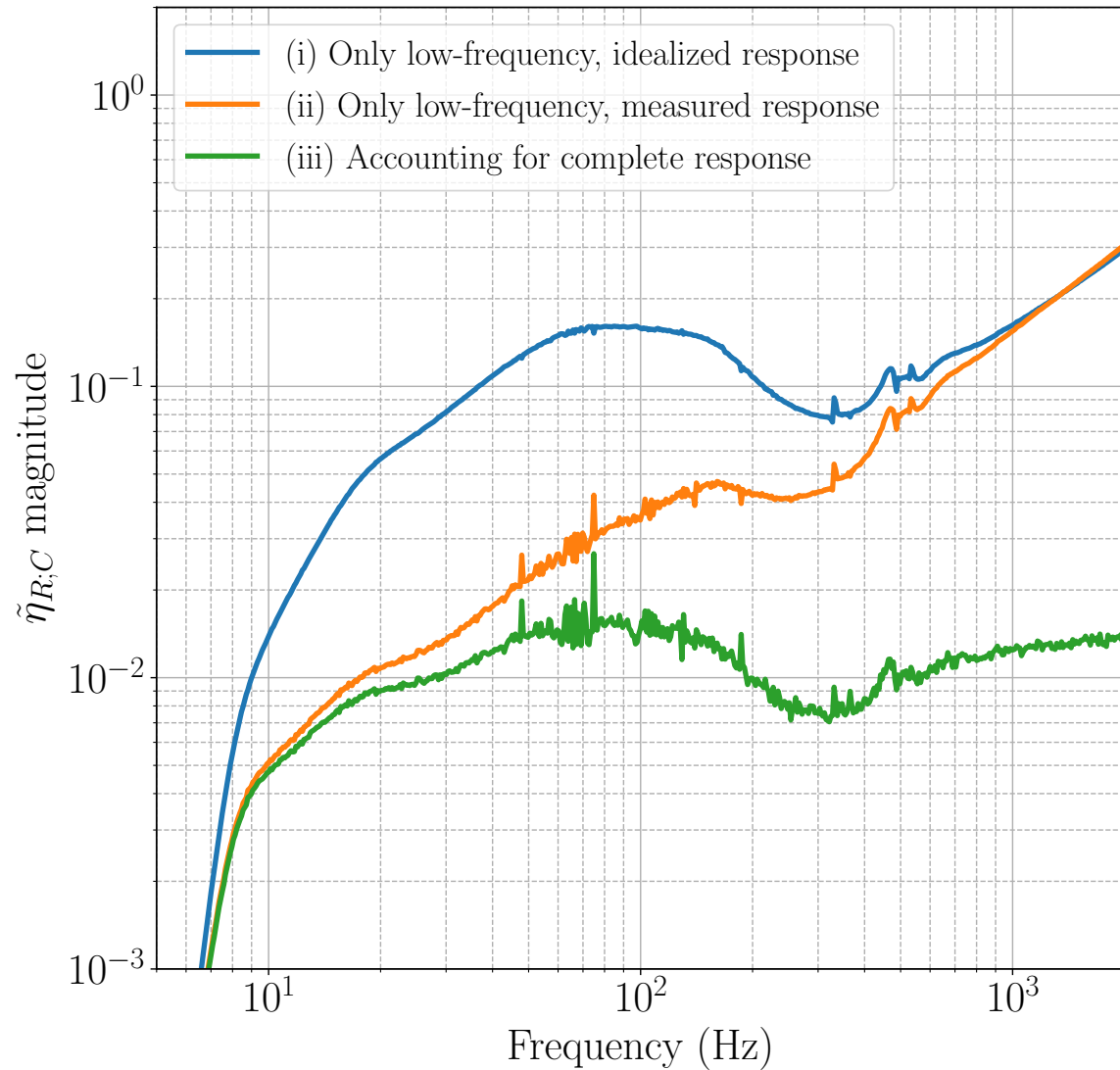
**Thanks!**  
**Questions?**

# Backup Slides

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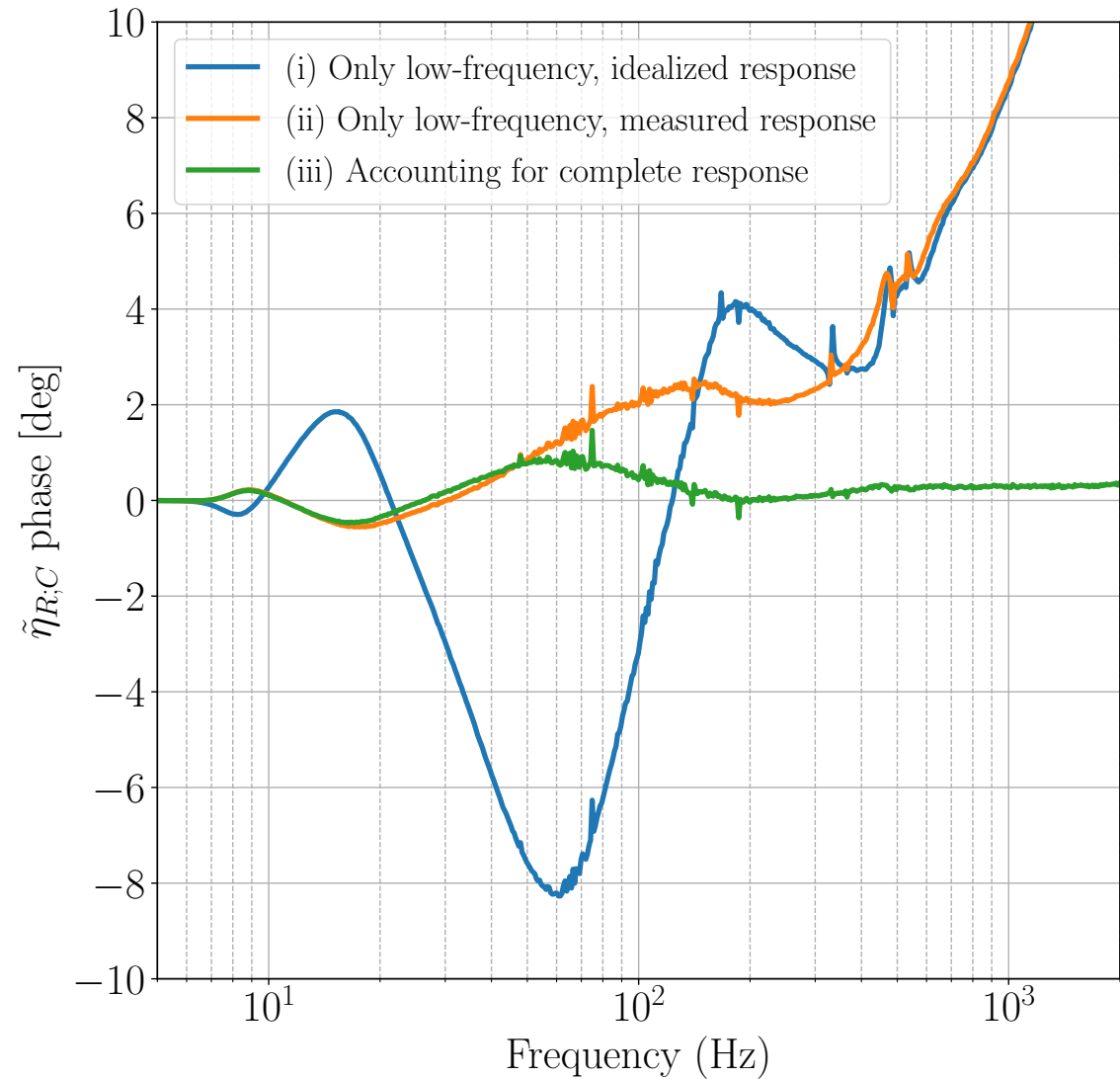


# Understanding the behavior of electronics



How good is good enough?

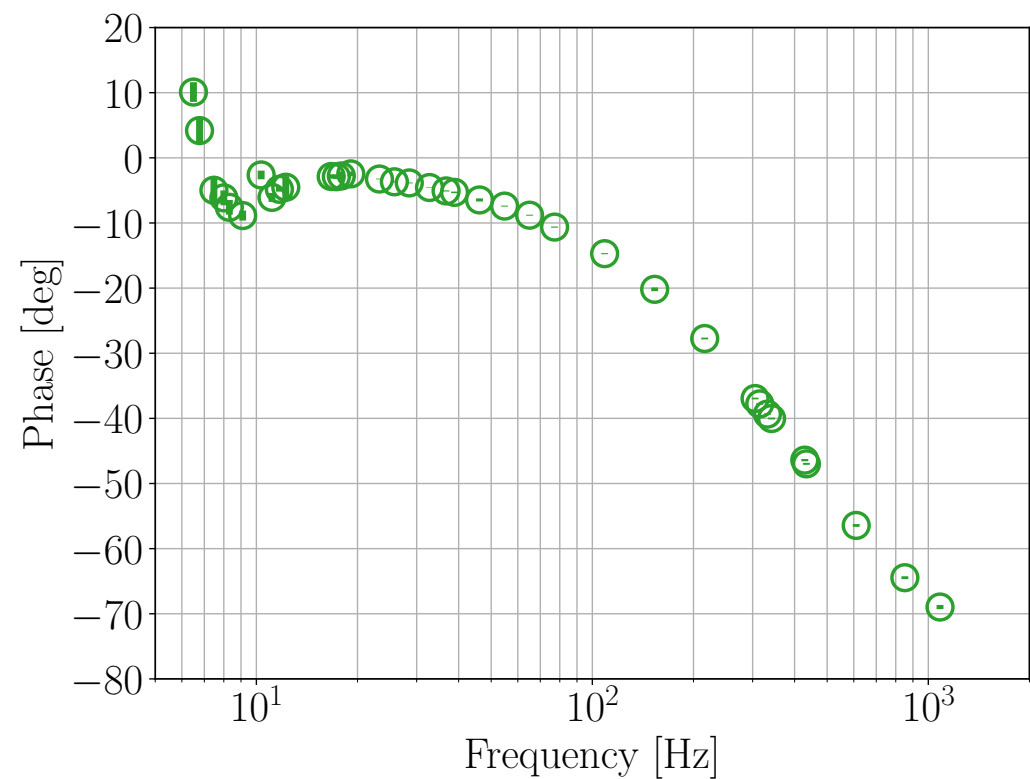
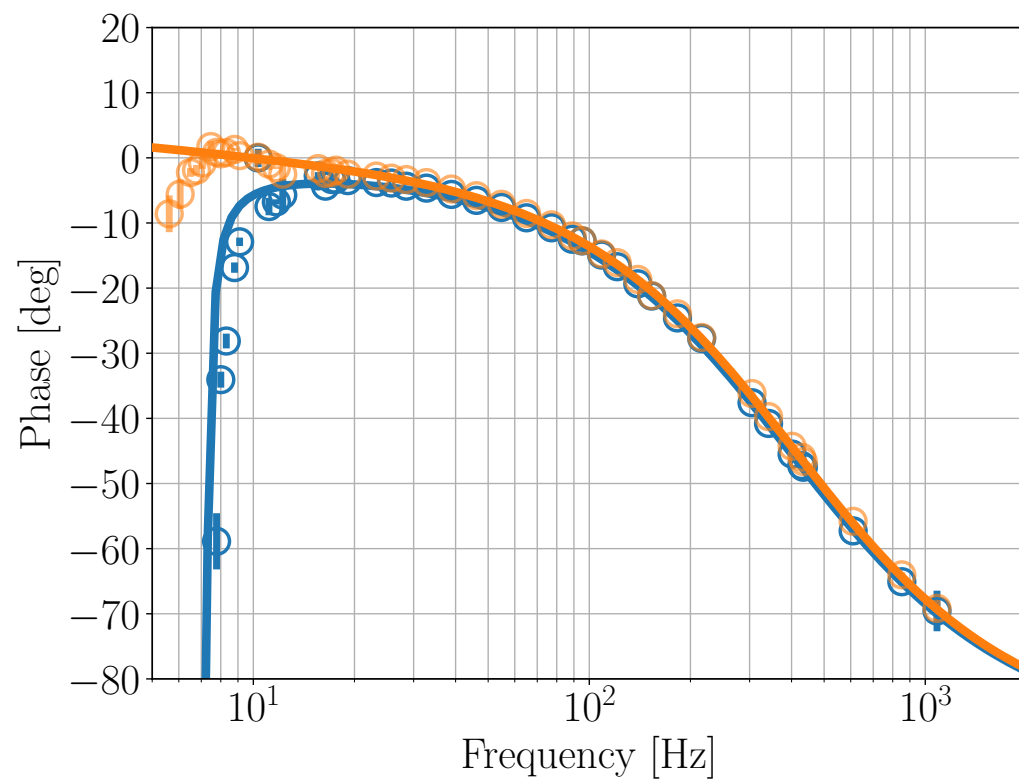
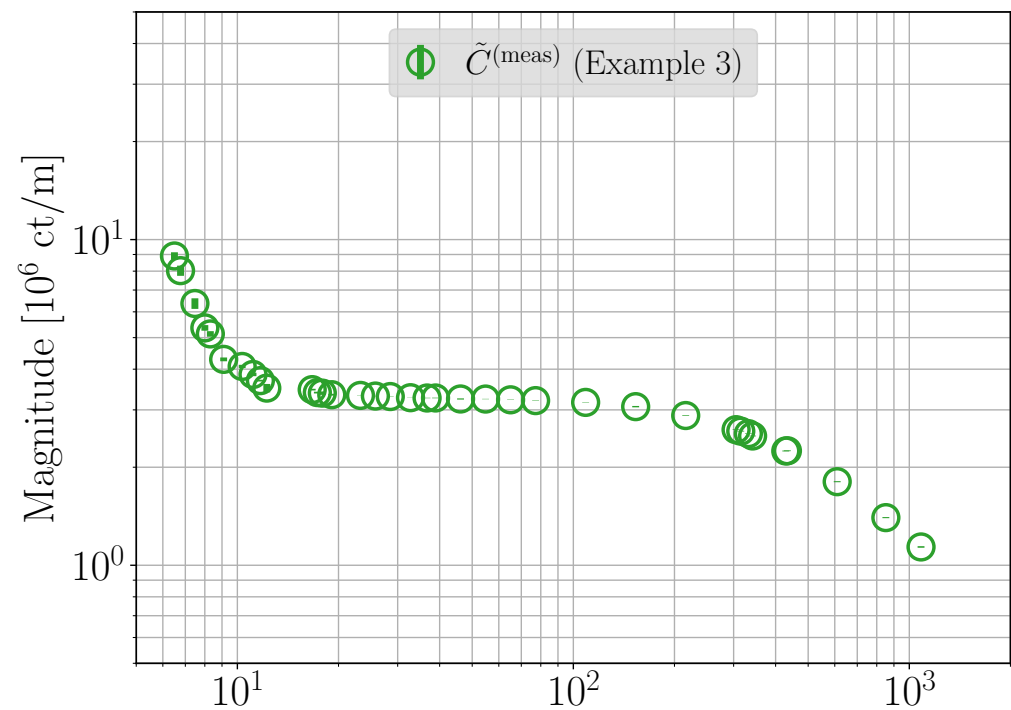
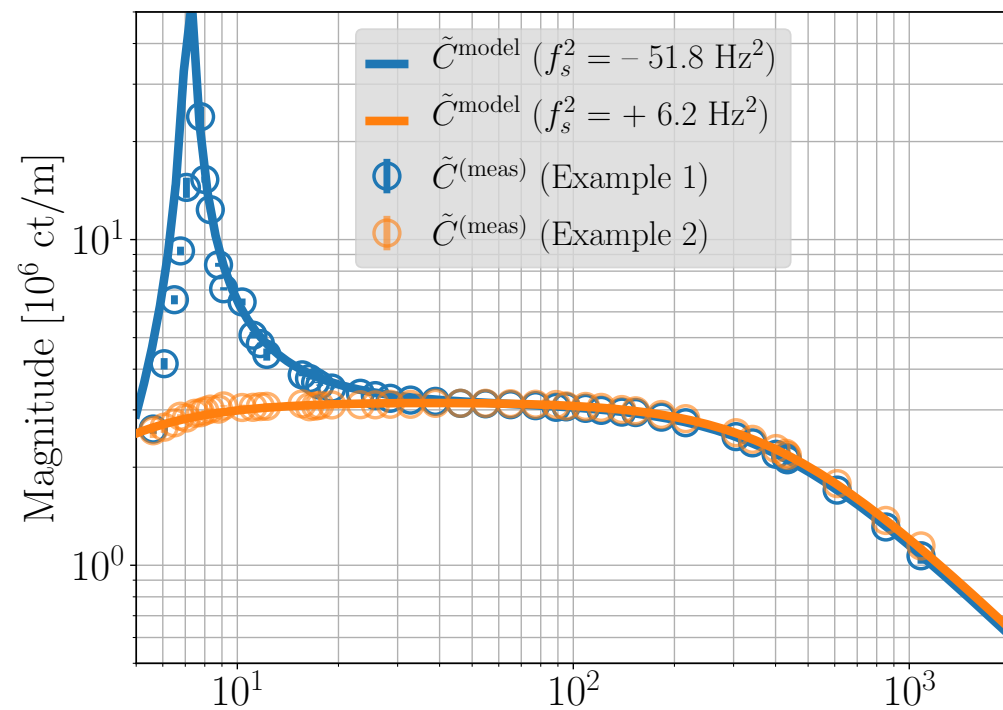
$$\tilde{R}(f) = \frac{1}{\tilde{C}(f)} + \tilde{A}(f)\tilde{D}(f)$$



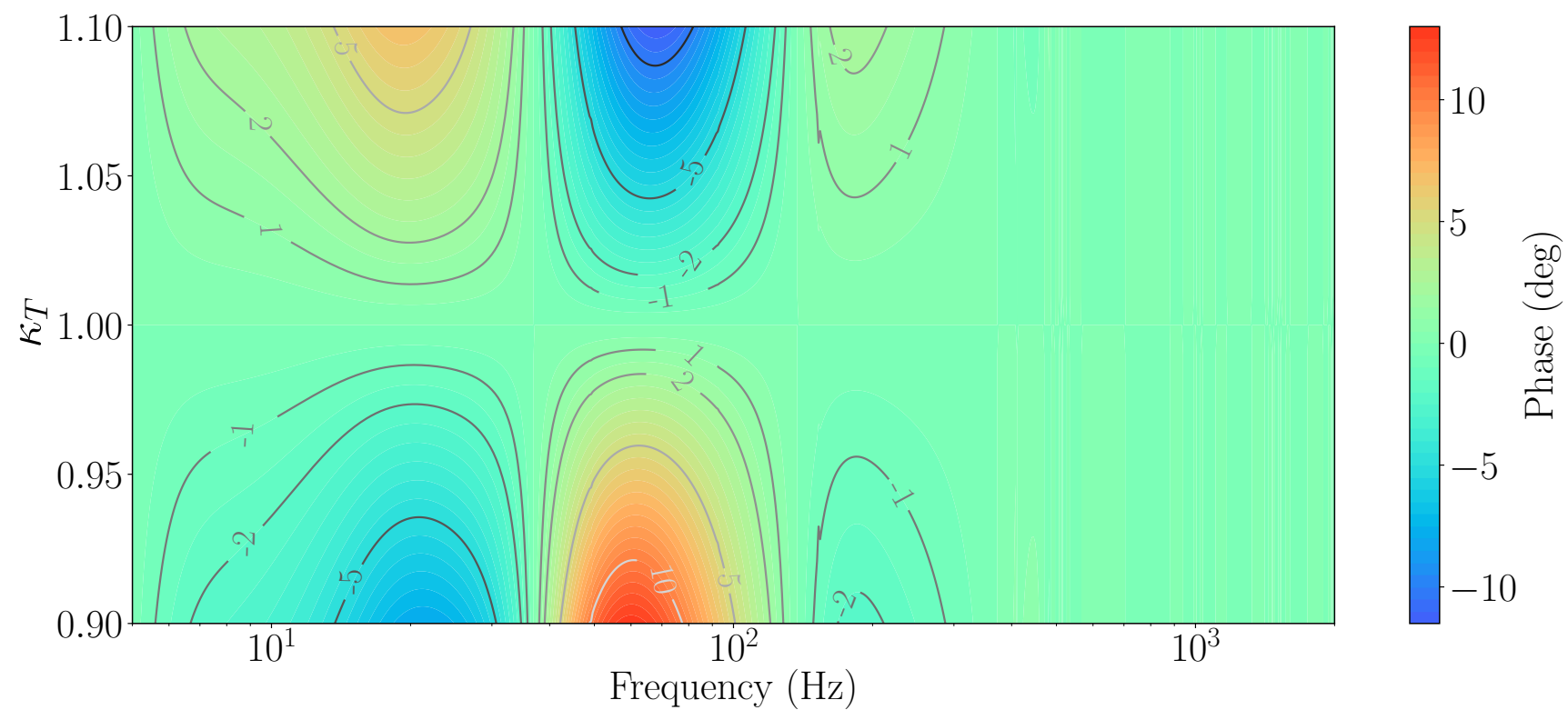
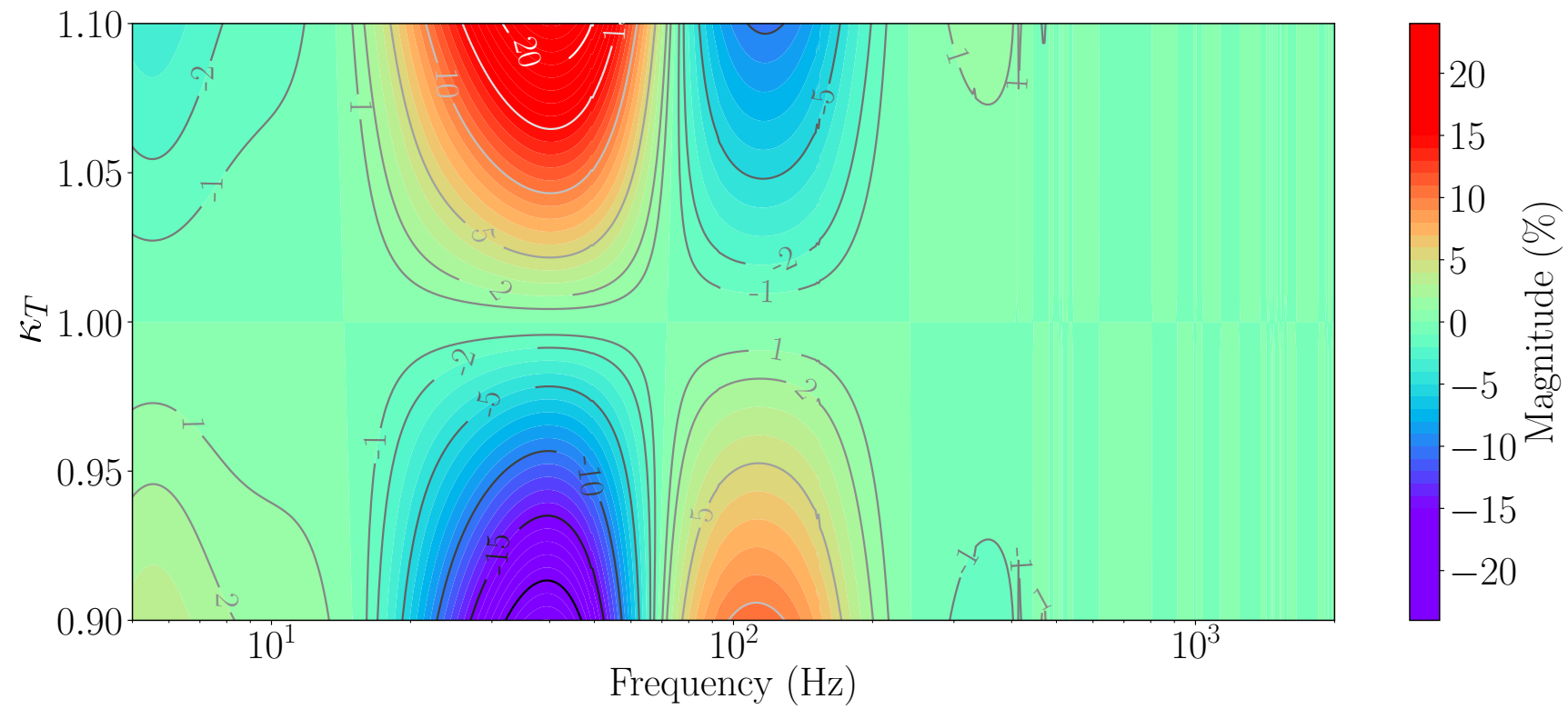
Evaluate residual contribution

$$\tilde{\eta}_{R;C} = \frac{1}{\tilde{R}(\text{model})} \left[ \frac{1}{\tilde{\eta}_C \tilde{C}(\text{model})} + \tilde{A}^{(\text{model})} \tilde{D} \right]$$

# O3A sensing function measurements at H1



# Impact from H1 TST



# Verify the uncertainty budget envelope

