

# High Fidelity Probe and Mitigation of Mirror Thermal Fluctuations

Direct observation of Brownian noise in  $\text{SiO}_2/\text{Ta}_2\text{O}_5$  coatings and a plan for optimizing Thermo-Optic noise in AlGaAs coatings.

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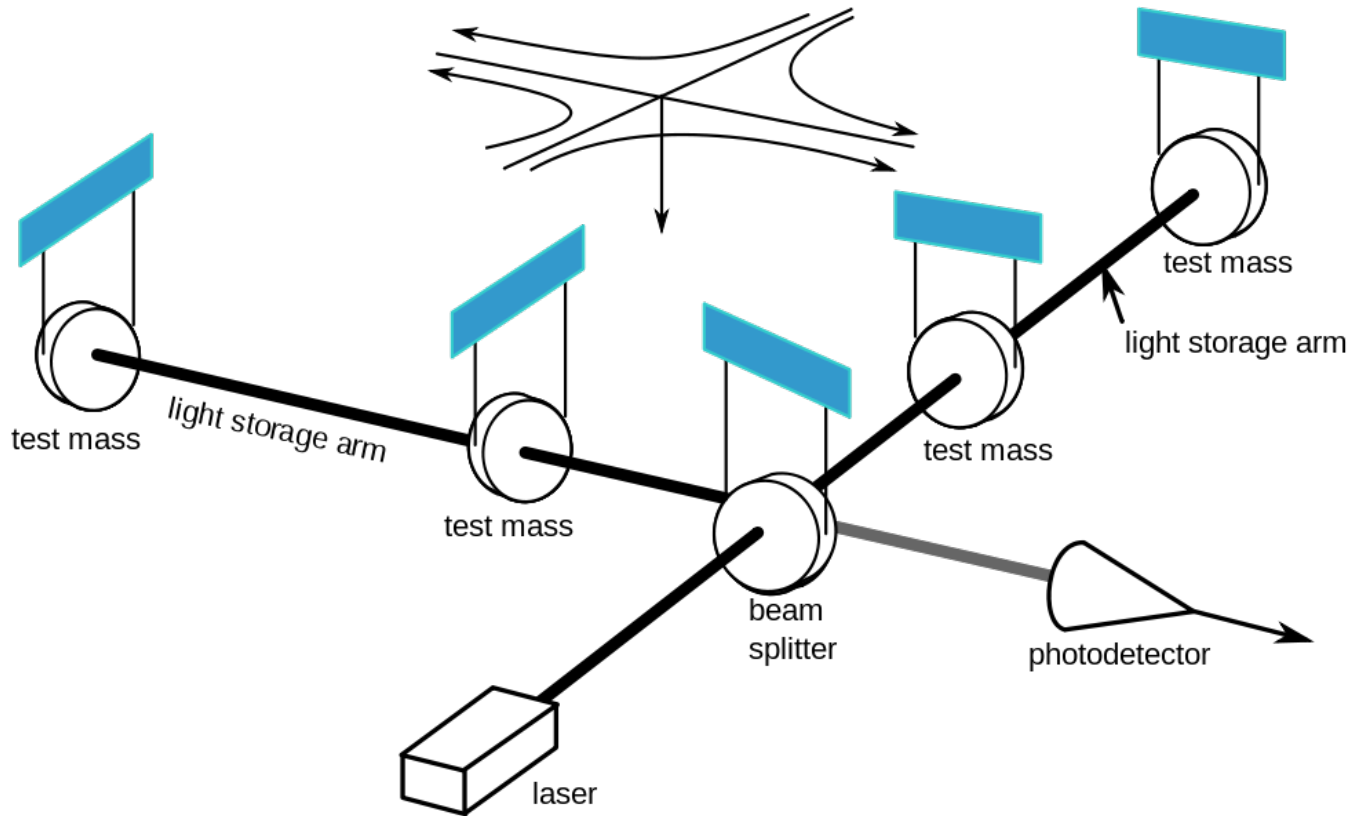
# Introduction to Thermal Noise

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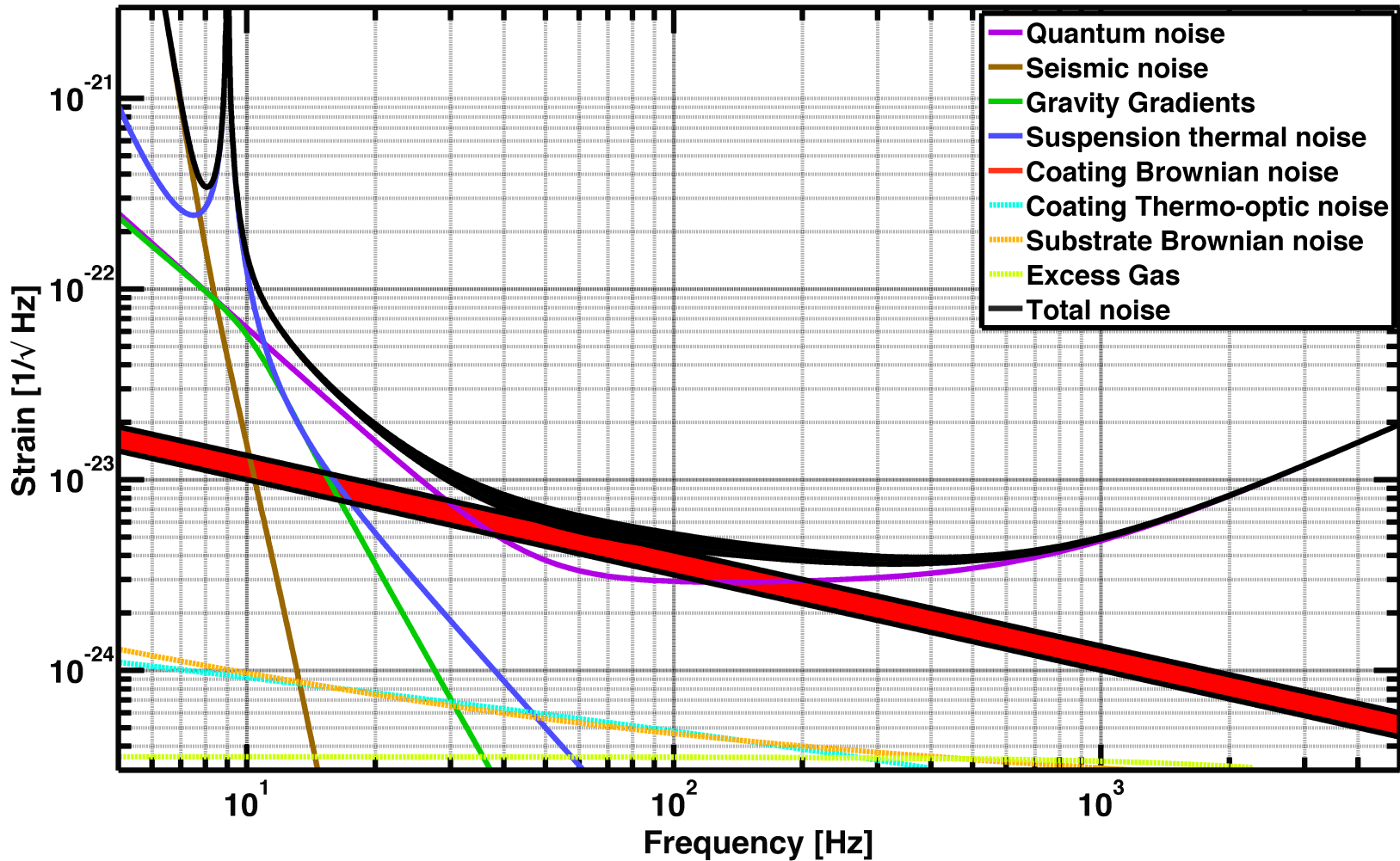
- Motion of molecules, atoms due to thermal energy  $k_B T$
- Johnson-Nyquist Noise in resistors (due to electrons motion),
- Brownian Motion of a particle suspended in liquid (due to collisions from liquid molecules).

# Schematic Diagram of LIGO

## □ Thermal noise in LIGO



# aLIGO Noise Budget



# Thermal Noise calculation

- Fluctuation-Dissipation Theorem: Loss and Noise are related.

$$S_x(f) = \frac{2k_B T}{\pi^2 f^2} \frac{W_{diss}}{F_0^2}$$

- **Mechanical Loss:** dislocations, impurities in materials, can be represented as an imaginary part in the Young's modulus,  $E = E_0(1+i\phi)$ .
  - Causes Brownian noise
- **Heat flow loss:** dissipation due to heat flow down temperature gradients.
  - Causes temperature fluctuations

- Applying force with Gaussian profile
- Calculate dissipated power due to the applied force

- For Brownian noise:

$$W_{Brownian} = 2\pi f U_0 \phi$$

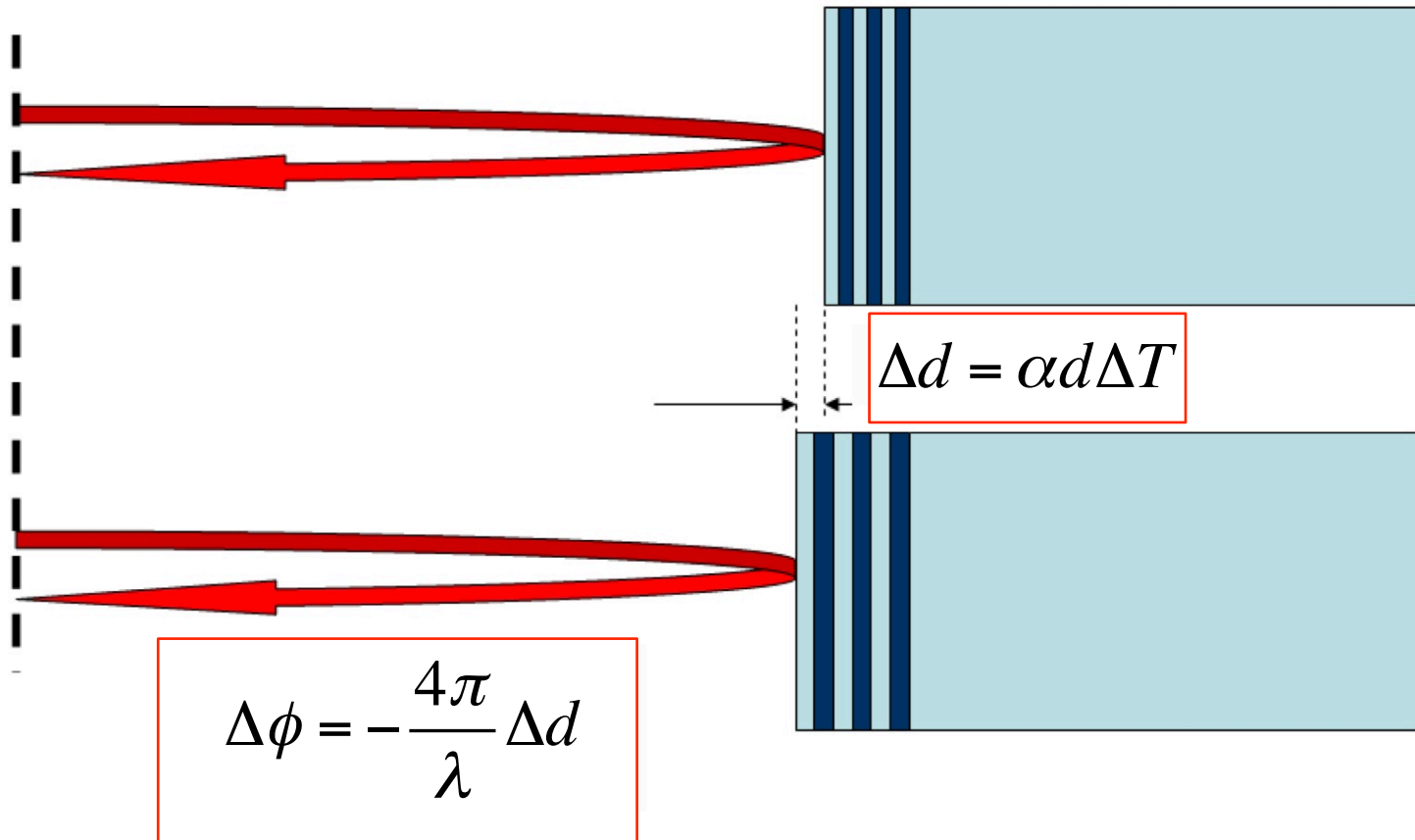
- For temperature fluctuations:

$$W_{thermo} = \left\langle \int d^3r \frac{\kappa}{T} (\nabla \delta T)^2 \right\rangle$$

- For an optical system, temperature noise is converted to displacement noise by thermal expansion coefficient  $\alpha$  and thermorefractive coefficient  $\beta$ .

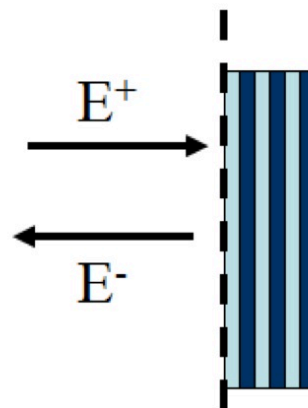
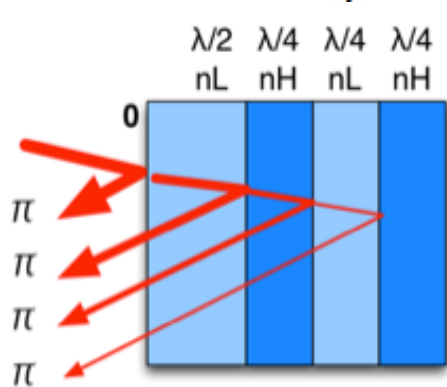
# Review: Thermo-Optic Noise

- **Thermo-Elastic (TE):** Mirror's surface expands into probe beam. By convention, negative  $d\phi/dT$



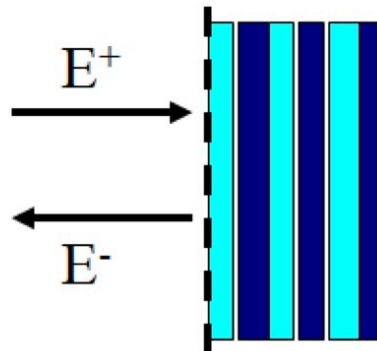
# Review: Thermo-Optic Noise(2)

- **Thermo-Refractive (TR):** Coating layers deviate from  $\lambda/4$  condition – due to both physical expansion and change in index of refraction. To first order, this manifests as a change in the phase of the reflected beam.



Quarter-wave stack:

$$E^- = E^+ r e^{i\varphi} \cong -E^+$$



After expansion, index change:

$$\begin{aligned} E^- &= E^+ r' e^{i\varphi'} \cong E^+ r e^{i(\varphi + \Delta\varphi_{TR})} \\ &= -E^+ e^{i\Delta\varphi_{TR}} \end{aligned}$$

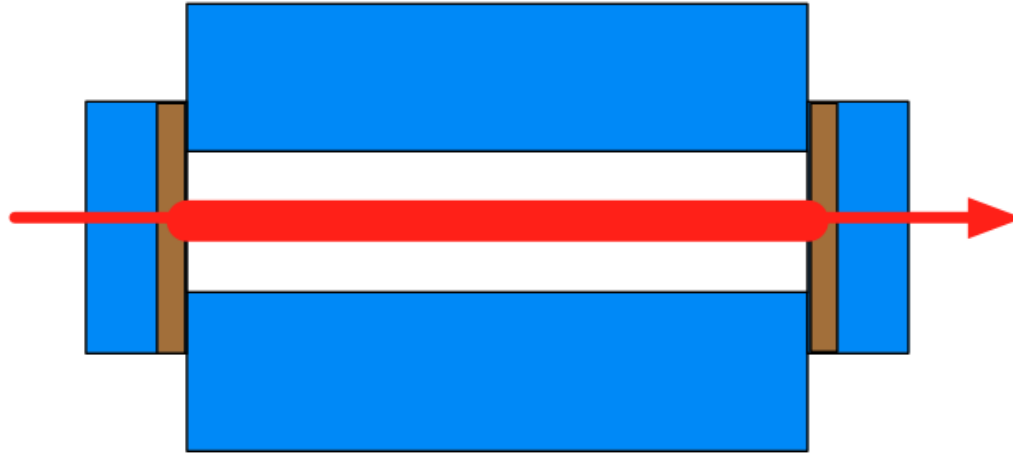


# Direct Measurement

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- Previous experiments (Numata, TNI)
  - Measured coating Brownian noise in 500 – 10 kHz band.
  - Large substrates.
  
- Develop a setup that can measure coating thermal noise around 10 Hz – 1 kHz.
  - Use commercial 1-inch diameter substrate
  - Use fixed-spacer Fabry-Perot cavity

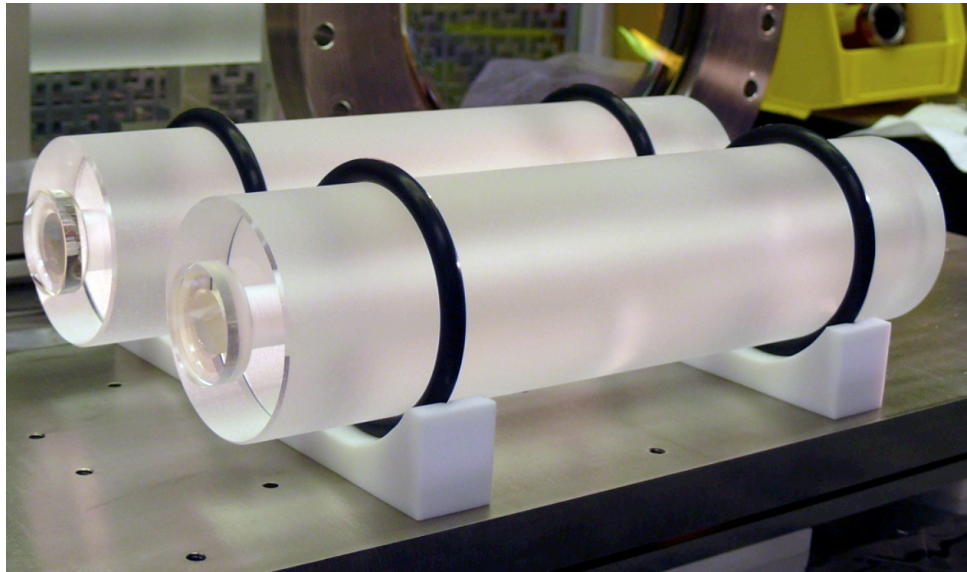
# Thermal Noise in Fixed-Spacer Cavity



	Brownian	Thermo-elastic	Thermo-refractive
Coating	yes	<b>Thermo-Optic Noise</b>	
Substrate	yes	yes	negligible
Spacer	yes	yes	no

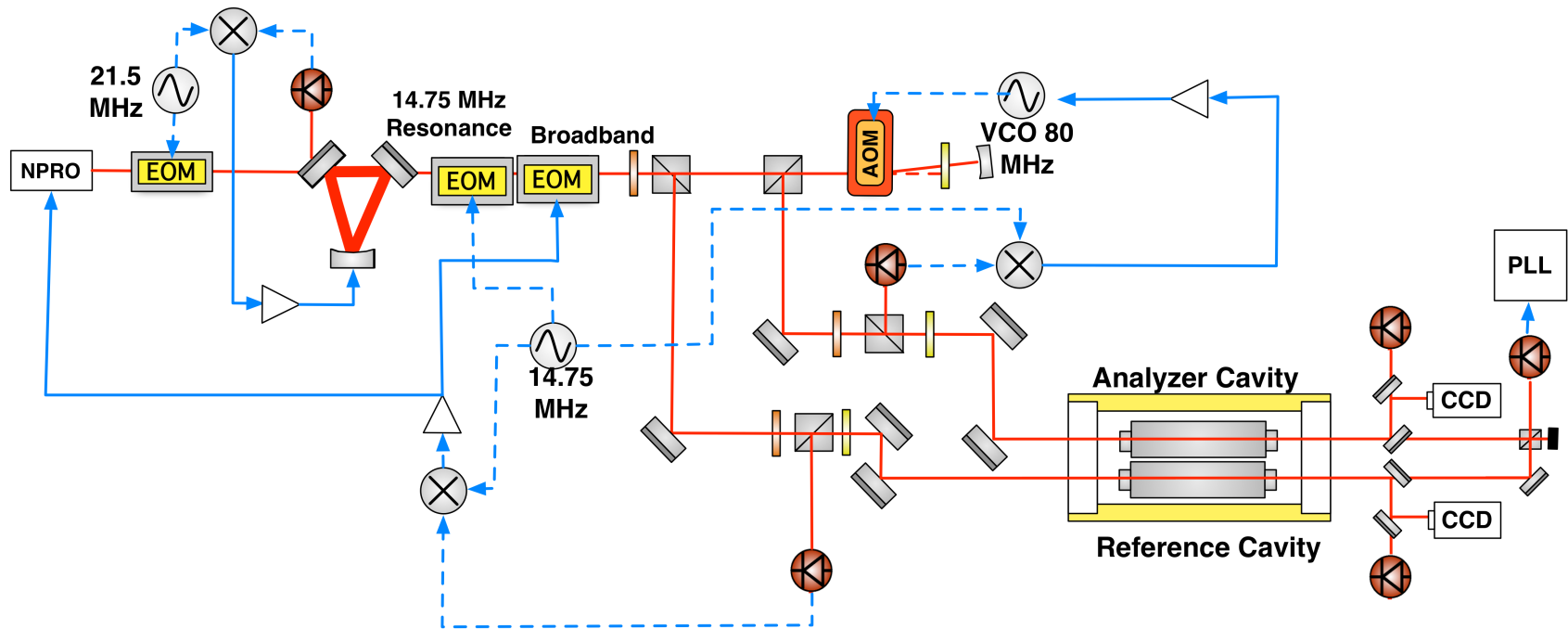
# iLIGO Reference Cavity

- ❑  $\text{SiO}_2$  spacer
- ❑  $\text{SiO}_2$  substrates
- ❑  $\text{SiO}_2/\text{Ta}_2\text{O}_5$  Coatings, 27 Layers +  $\lambda/2$  cap (28 layers total).
- ❑ Coated by REO in 1998, Ion beam sputtering method.
- ❑ Coating Brownian noise limits the cavity sensitivity



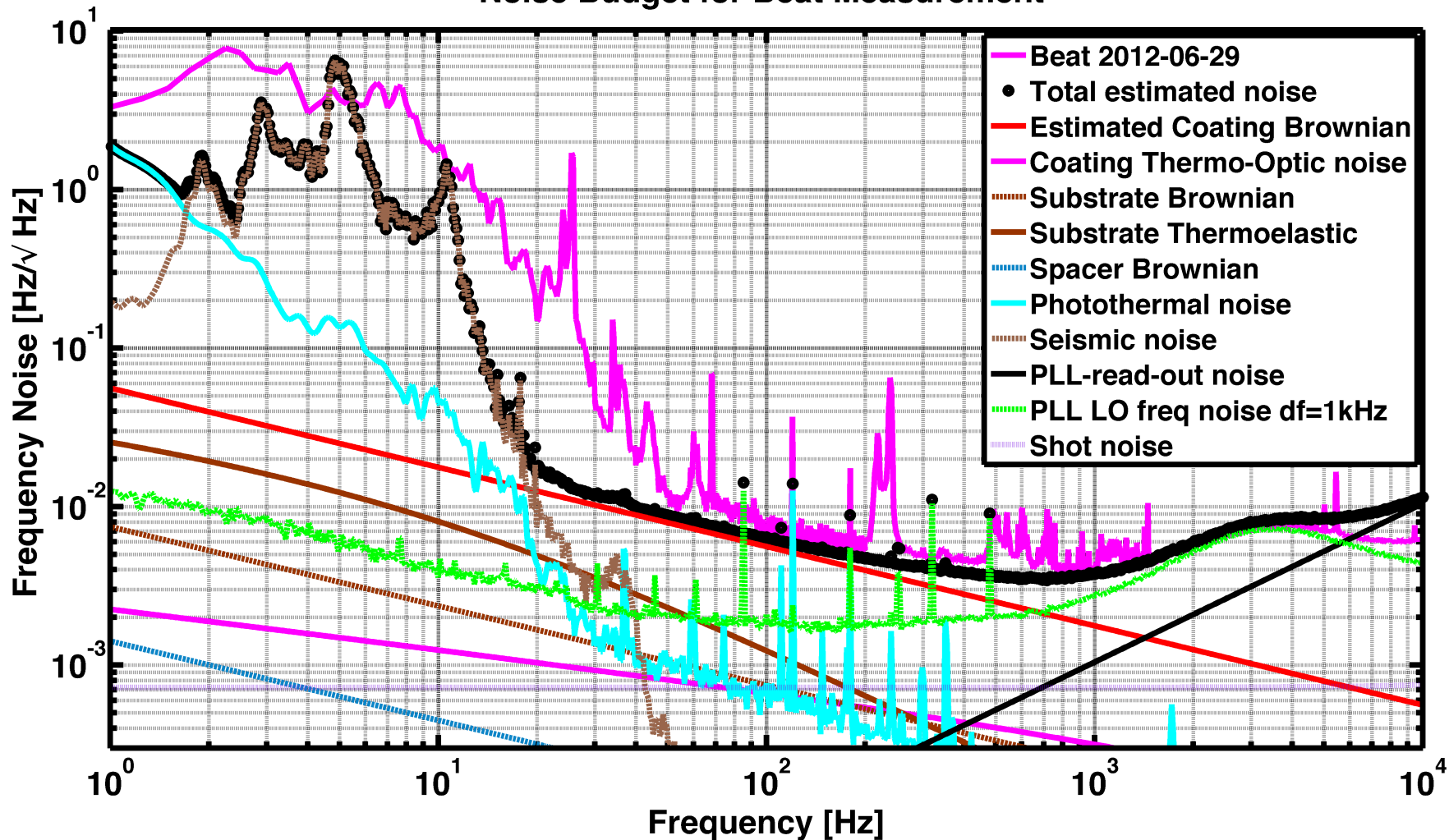
# Setup with 8 Inch Cavities

- Main beam is locked to the first cavity
- Second beam is frequency shifted by a doubled passed AOM, and locked to the second cavity
- Transmitted beams are recombined and readout by Phase Locked Loop (PLL).



# Result: 8 Inch Cavities

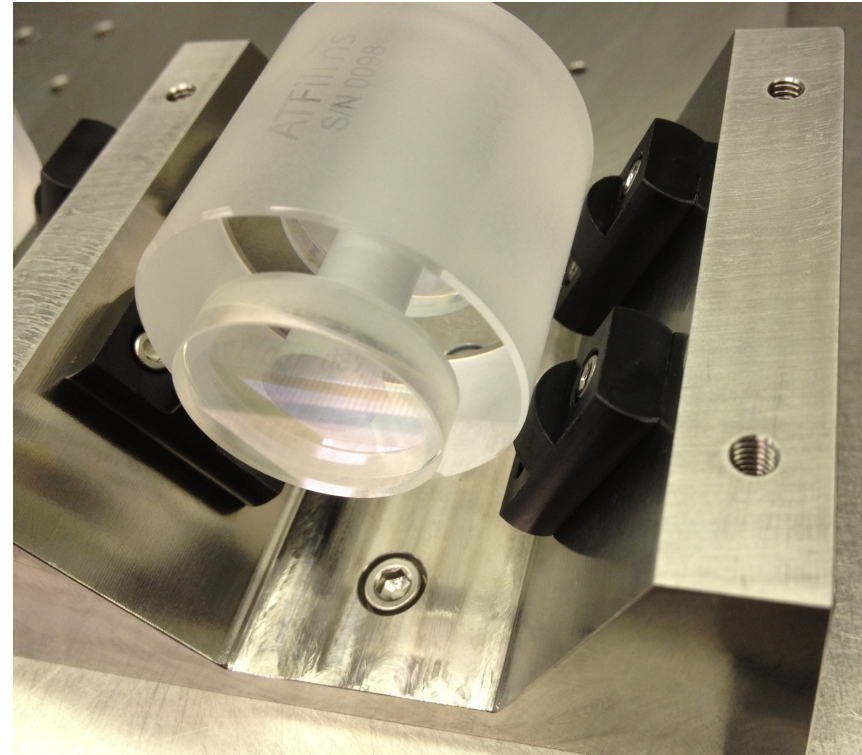
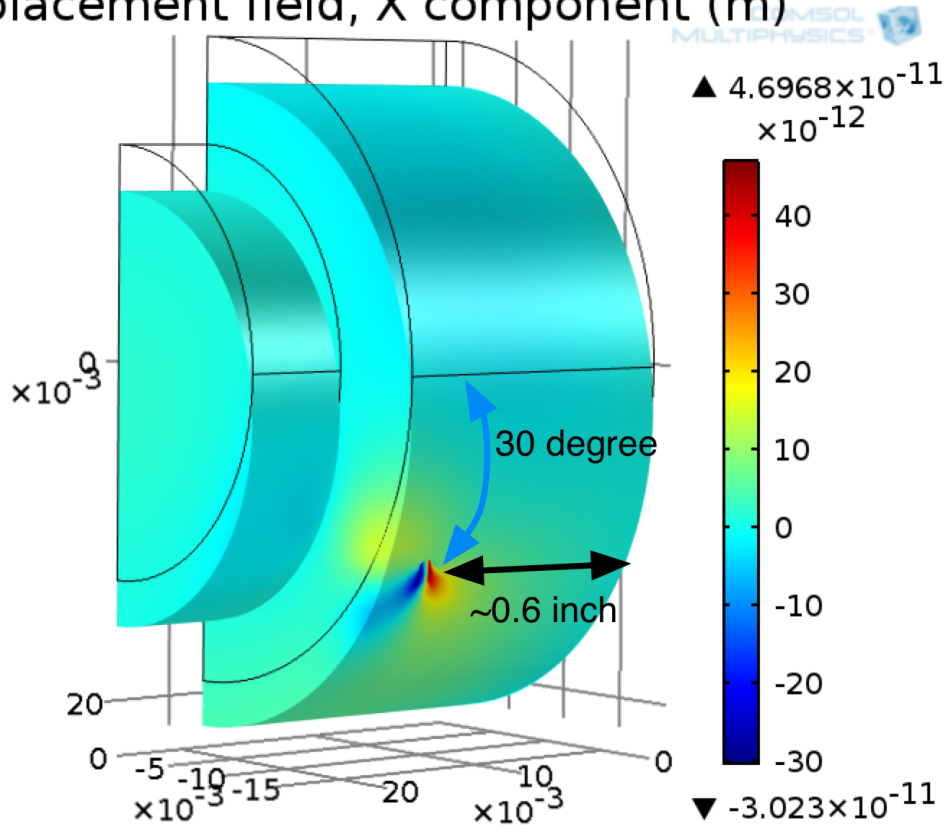
## Noise Budget for Beat Measurement



- ❑ Shorter cavity raises frequency noise  $\frac{\delta\nu}{\nu} = \frac{\delta L}{L}$
- ❑ Shorter cavity gives smaller spot size for similar mirrors (same radii of curvature, same coating run).
- ❑ The lower bound of the cavity length is determined by the ability to tune the cavity via thermal expansion, higher order mode consideration, and cavity stability.
- ❑ Use two lasers instead of one. The beat frequency is not limited by the operational range of the AOM.
- ❑ Similar cavities provide common mode rejection

## Optimum Support for Cavity

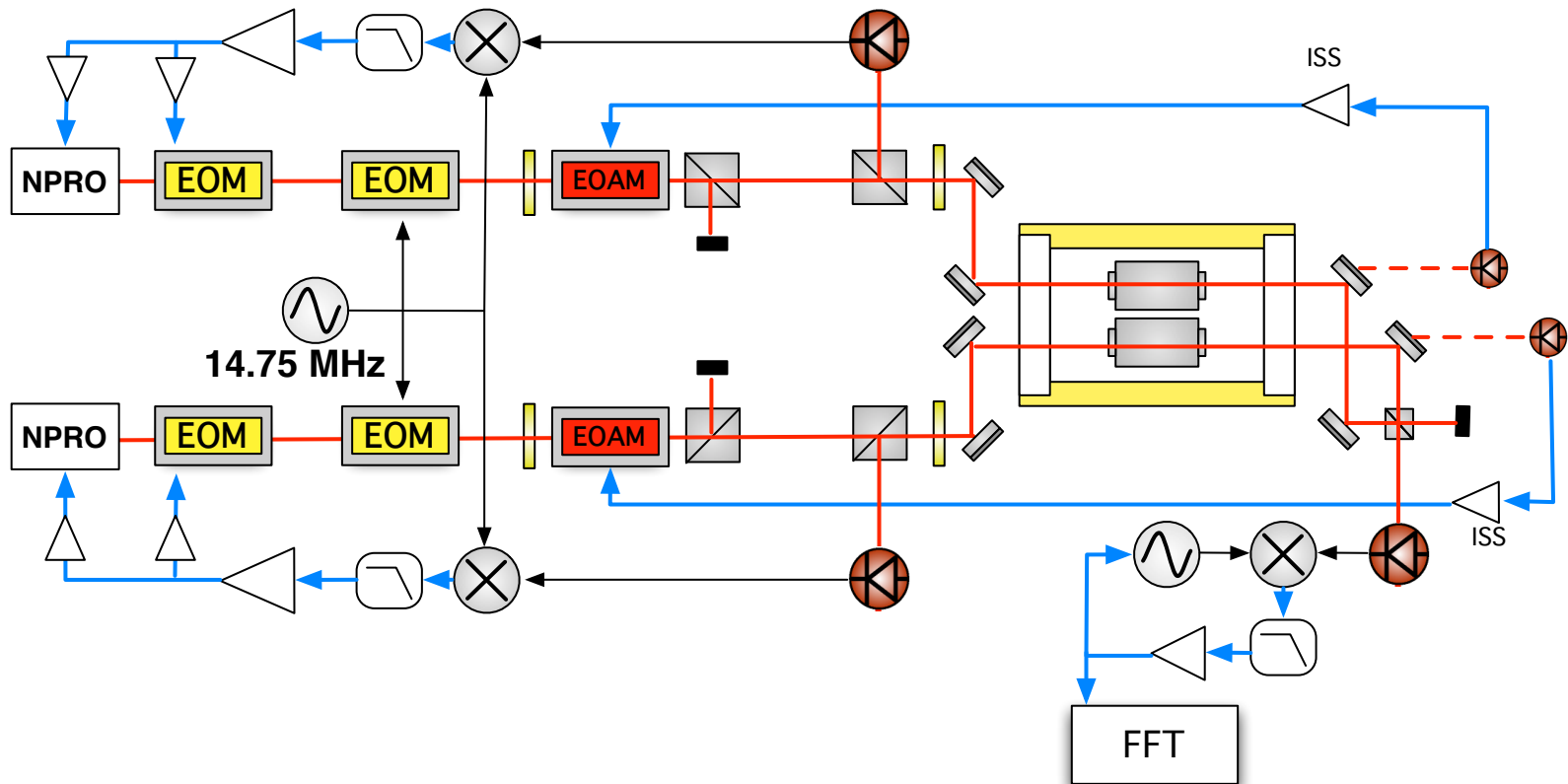
Displacement field, X component (m)



- 1.45" cav Strain  $\sim 10^{-10}$  [s<sup>2</sup>/m], with common mode  $\sim 6 \times 10^{-12}$  [s<sup>2</sup>/m]
- Ludlow 2007/Alnis 2008: football shaped cavity  $\sim 5 \times 10^{-11}$  [s<sup>2</sup>/m]
- Webster 2008:  $\sim 3 \times 10^{-12}$  [s<sup>2</sup>/m]

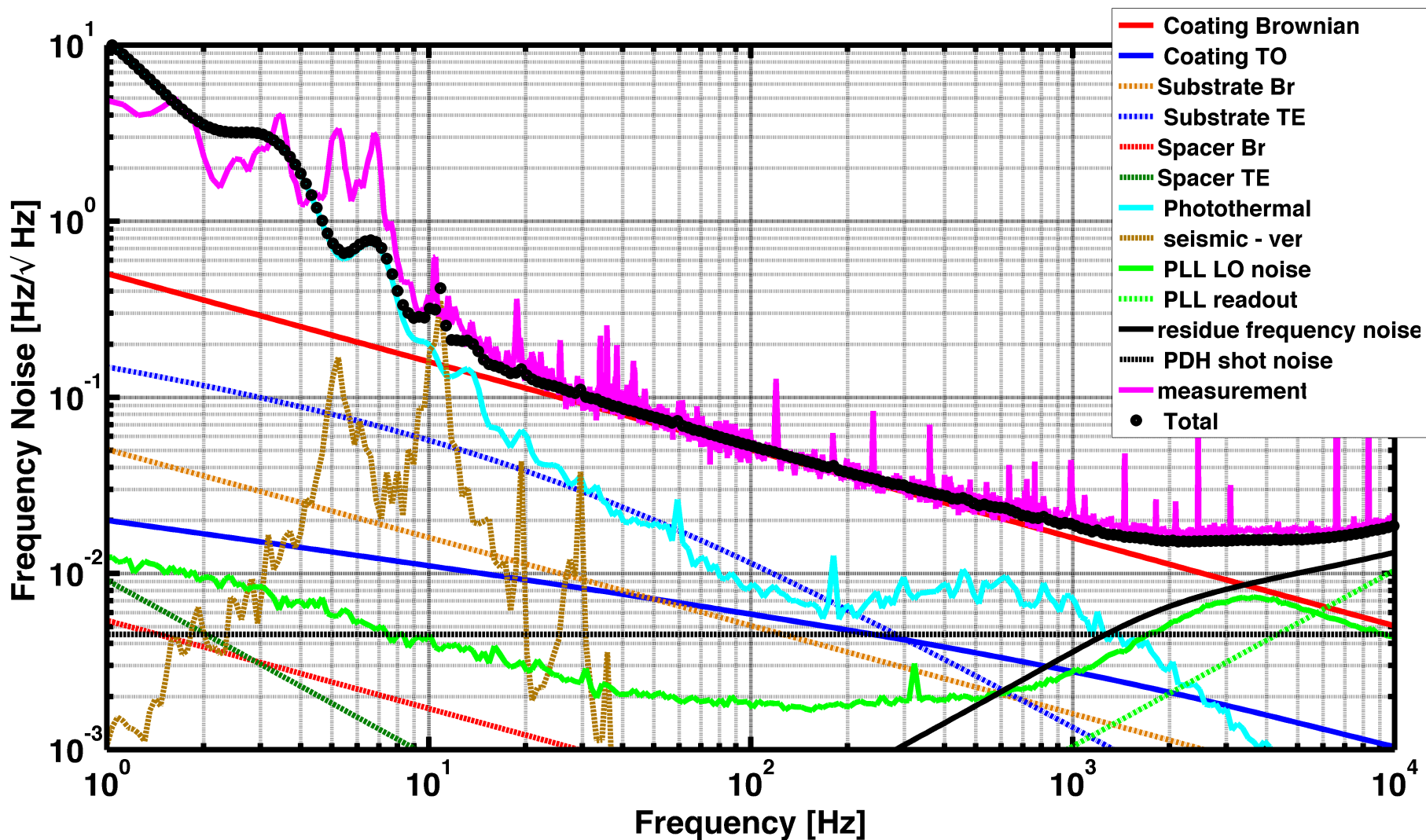
# 2 Laser Setup

- ❑ Increase Coating Brownian Noise: Use Shorter Cavity (see details in LIGO-T1200057-v11)
- ❑ Spotsize  $\sim 200\mu\text{m}$ , similar mirrors from the same coating run

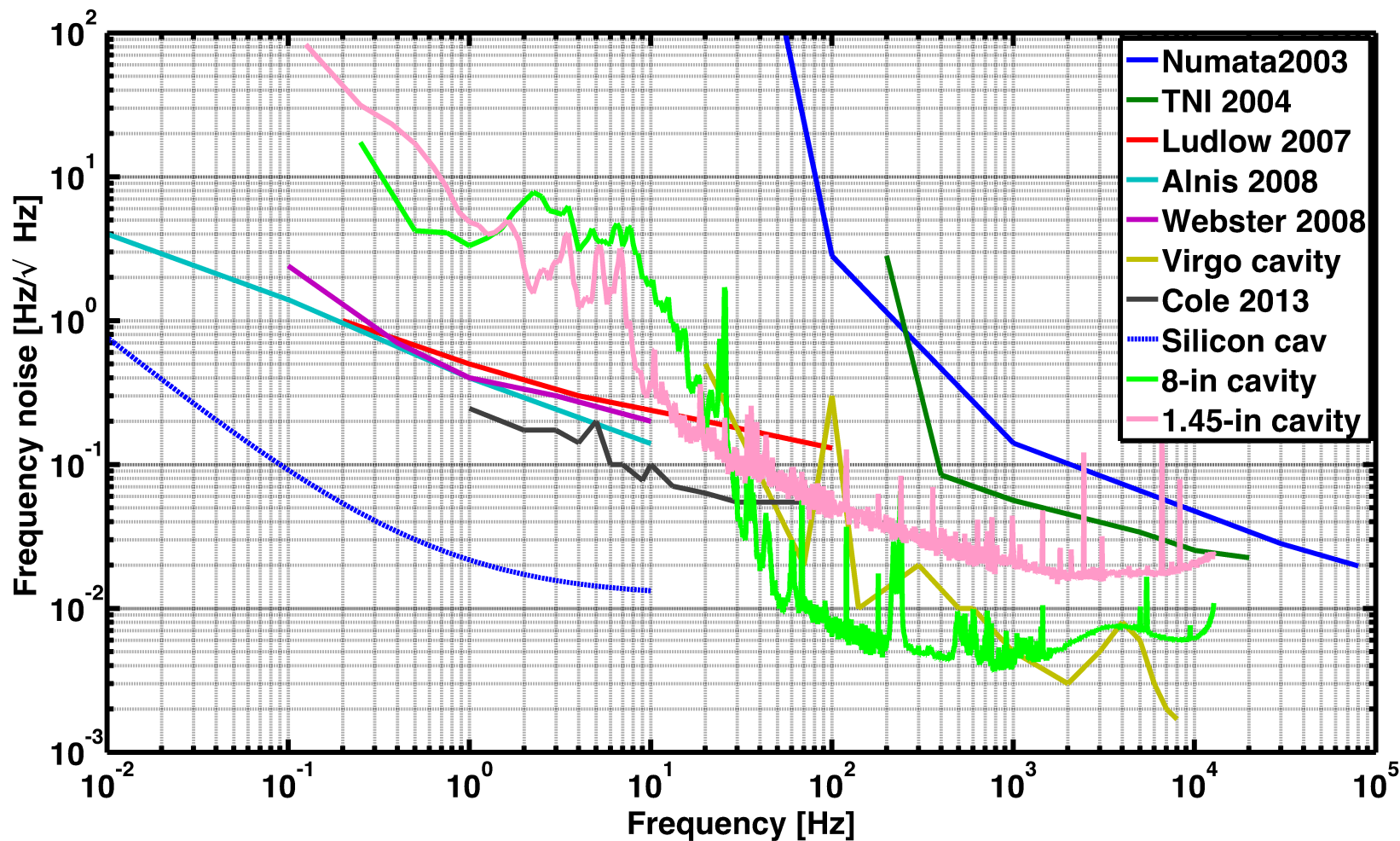




# Result: 1.45 Inch Cavities



# Comparison with Other Exps



# Loss Angle Extraction

- Nakagawa et al. 2002 (assuming coatings and substrate have the same elastic properties)

$$S_x^{(\text{cBr})}(f) = \frac{4k_B T}{\pi^2 f} \frac{(1 - \sigma_s - 2\sigma_s^2)d}{\omega^2 E_s} \phi_c.$$

- Numata et al. 2003:  $\Phi_c = 4 \times 10^{-4}$
- From our measurement:  $\Phi_c = 4.2 \times 10^{-4}$
- Three pieces of evidence suggest that the measured result is coating Brownian noise
  1. The slope of the spectrum goes with  $1/f$ .
  2.  $\Phi_c$  is comparable with previous measurement.
  3. Thermal noise scales correctly with spot size.

# Comparison with Another Calculation

- Hong et al. 2013, calculate coating Brownian noise in bulk and shear deformations.
- If  $\phi_{\text{SHEAR}} = \phi_{\text{BULK}}$ , the estimated thermal noise is

$$S_x(f) = c_1\phi_L + c_2\phi_H$$

- With nominal parameters ( $\phi_L = 1 \times 10^{-4}$ ,  $\phi_H = 4 \times 10^{-4}$ )

$$S_{\text{cal}}/S_{\text{mea}} = 0.6$$

# Comparison with Ring Down Result

- Harry et al. 2002 reported the coating loss due to multilayer of SiO<sub>2</sub>/Ta<sub>2</sub>O<sub>5</sub> (same coating vendor, around the same time).

$$\phi_{||} = \frac{Y_L d_L \phi_L + Y_H d_H \phi_H}{Y_L d_L + Y_H d_H}$$

Y = young's modulus  
d = layer thickness

With our measurement, we can obtain  $\Phi_L$  and  $\Phi_H$ .

$$\phi_L = (1.1 \pm 0.3) \times 10^{-4},$$

$$\phi_H = (8.2 \pm 0.3) \times 10^{-4}.$$

	Penn 2003	Crooks 2004	Crooks 2006	LMA 2014
$\Phi_L$ $\times 10^{-4}$	0.5±0.3	0.4±0.3	1±0.2	0.62±0.4
$\Phi_H$ $\times 10^{-4}$	4.4±0.2	4.2±0.4	3.8±0.2	4.5±0.3

- Higher loss might be due to contaminants during the deposition process.

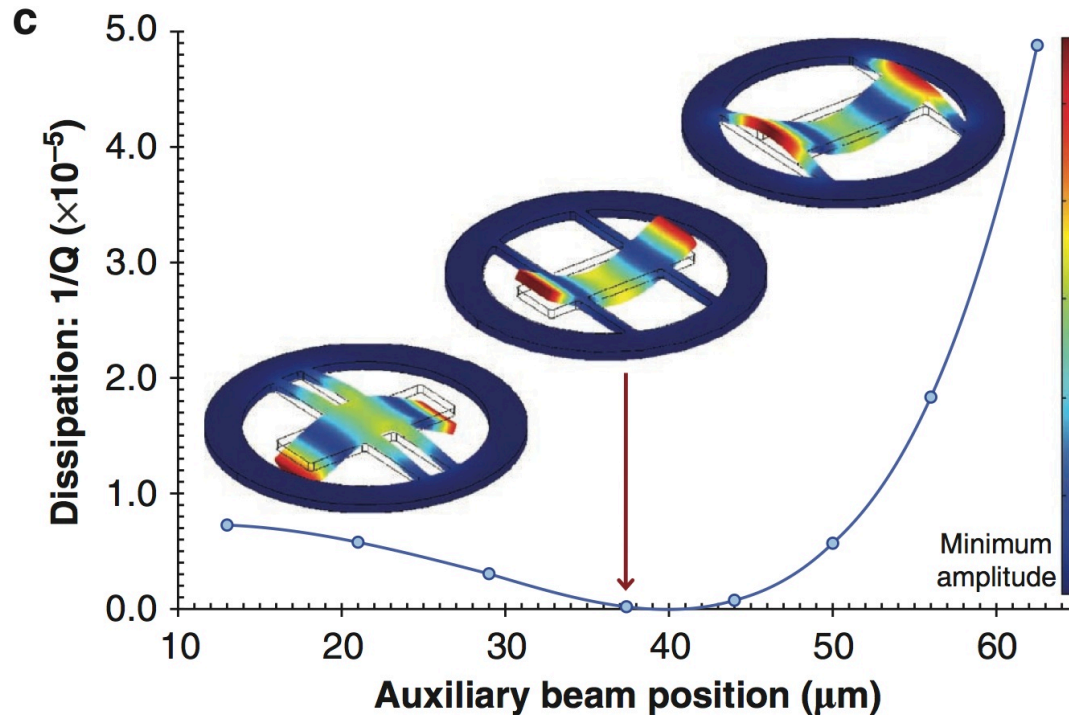
# AlGaAs for High Reflective Coating

# AlGaAs

- ❑ Hetero structure of GaAs and  $\text{Al}_x\text{Ga}_{1-x}\text{As}$ .
- ❑ It has been used as a high reflective device in a laser since 1980s.
- ❑ Optical properties have been well studied.
- ❑ Epitaxial Lift Off technique makes it possible to attach AlGaAs film on a fused silica substrate.

# AlGaAs Coatings

- Low loss  $\sim 2.5 \times 10^{-5}$ , at room temp as measured on free standing mechanical resonators.
- Loss at 20K is  $\sim 2 \times 10^{-5}$ , good candidate for Si substrate at cryogenic temperature





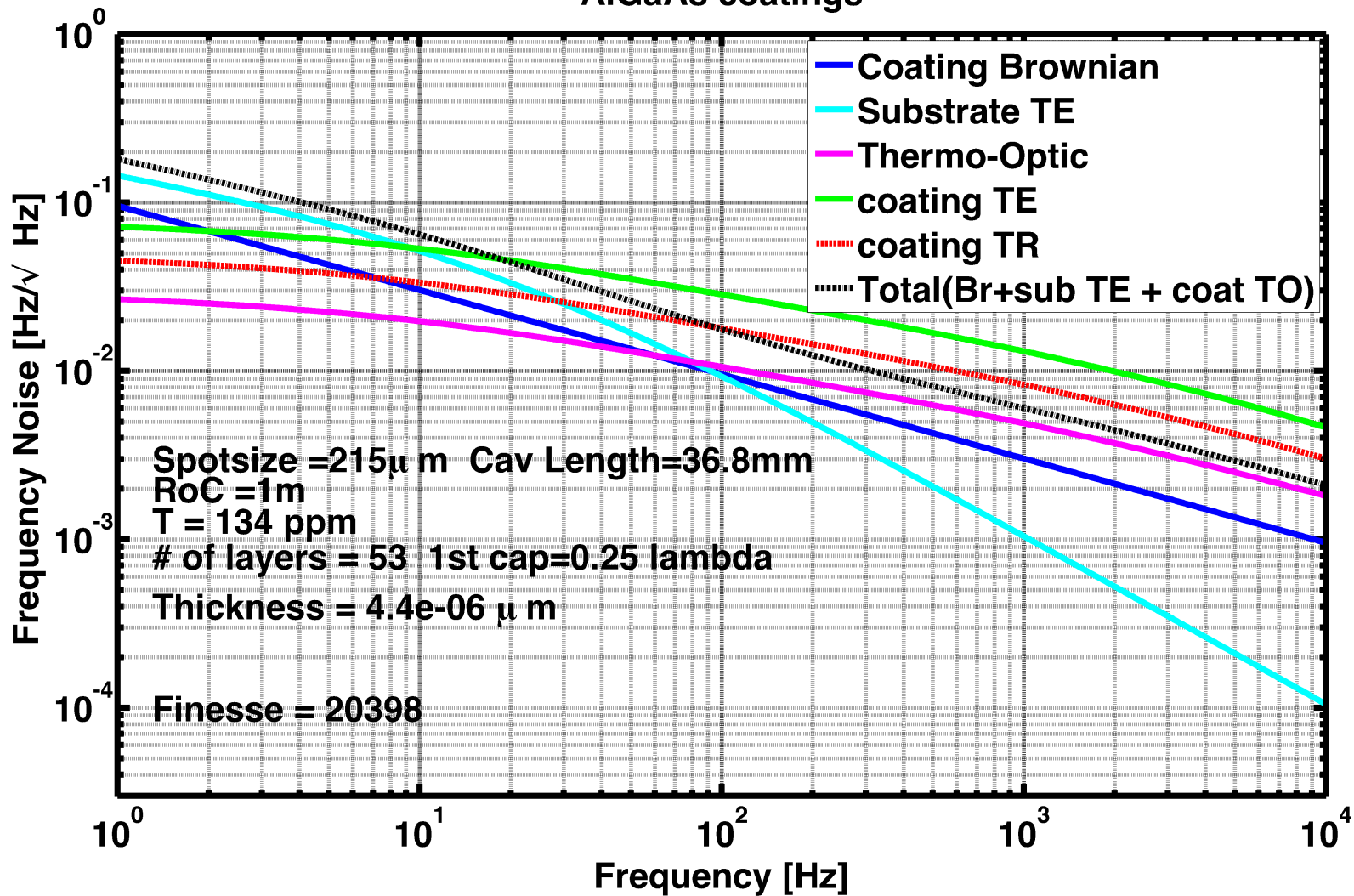
# Thermo-Optic noise in AlGaAs

- Higher Thermal expansion, Thermorefractive coefficient ( $dn/dT$ )
- Thermo-Optic noise is higher than Brownian noise

	$\alpha$ ( $\times 10^{-6}$ ) [1/K]	$\beta$ ( $\times 10^{-6}$ ) [1/K]
SiO <sub>2</sub>	0.5	8
Ta <sub>2</sub> O <sub>5</sub>	3.6	14
GaAs	5.7	366
Al <sub>0.92</sub> Ga <sub>0.08</sub> As	5.2	179

# Noise Budget: QWL T~150ppm

AlGaAs coatings



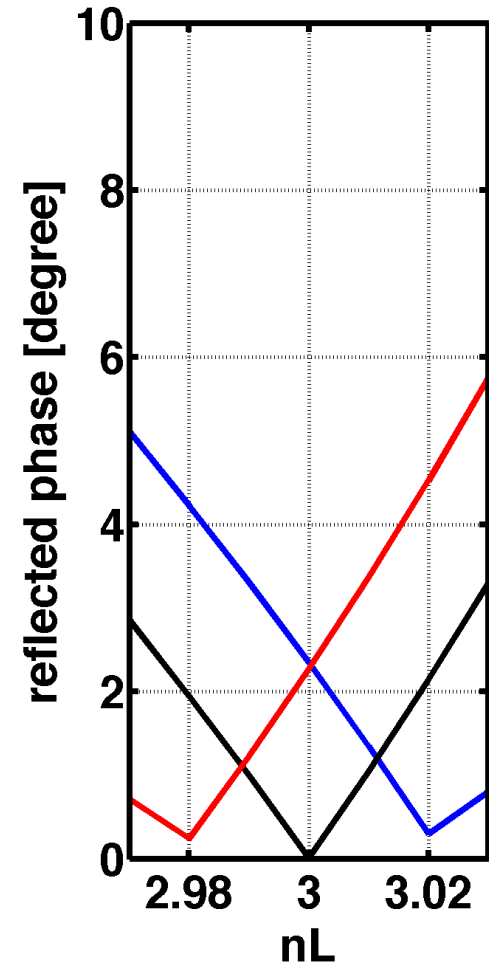
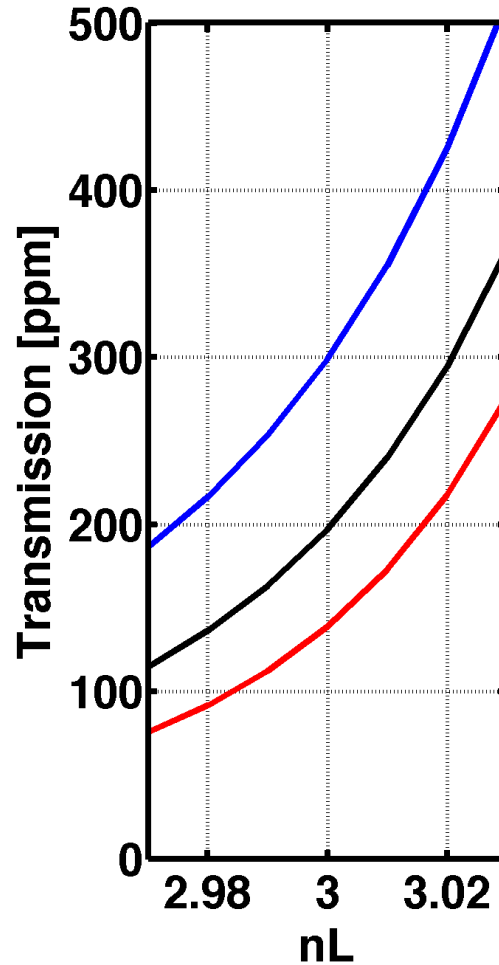
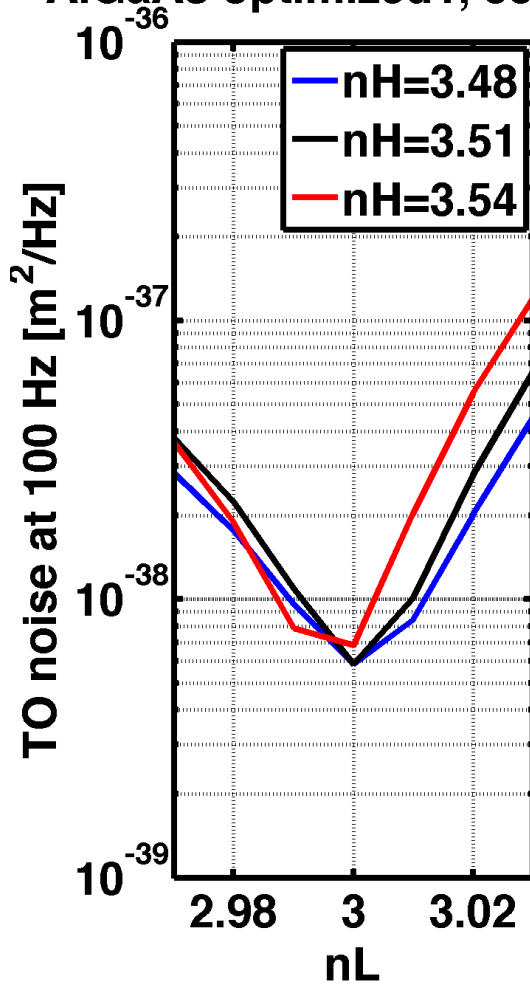
# How to Reduce TO Noise

- ❑ Alter layer thickness, to change  $\beta_{\text{eff}}$
- ❑ Achieve required transmission (100 ppm – 300 ppm)
- ❑ Get correct reflected phase (to prevent surface burning)
  
- ❑ Use fminsearch for minimizing a cost function.
- ❑ Cost function can be given by these three parameters:

$$y = (\text{TO noise}) * w_1 \\ + (\Delta \text{Transmission}) * w_2 \\ + (\Delta \text{Reflected phase}) * w_3$$

# Optical Properties vs nH and nL: Optimization with Single Cost Function

AlGaAs optimized1, 55Layer

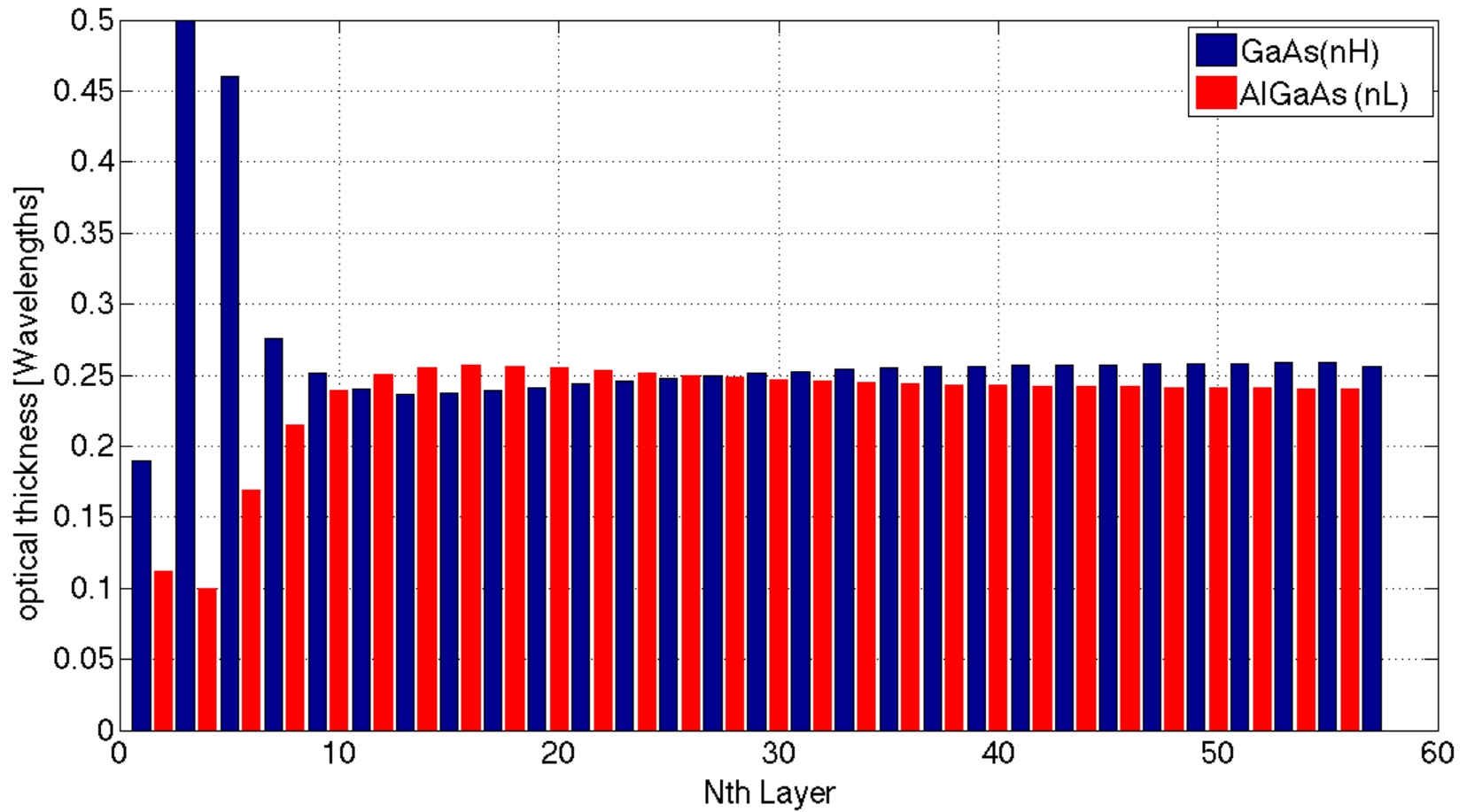


# Modified Cost Function

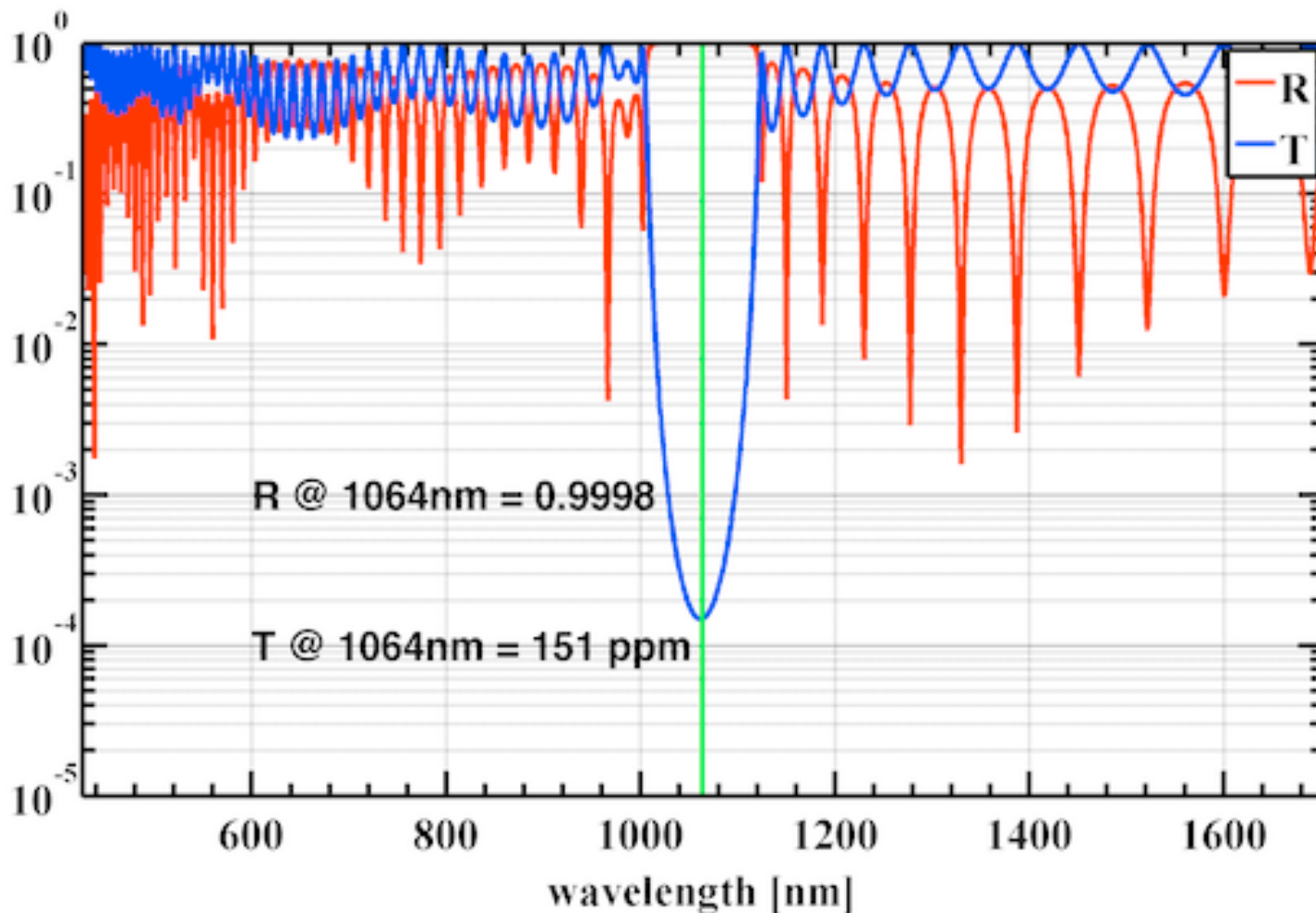
- Coatings' properties (Transmission, reflected phase, TO noise) may change from the desired values due to uncertainties in parameters. Mostly refractive indices.
- Modified Cost function: sum of cost functions from different values of refractive indices

$$y' = \sum_{n_H} \sum_{n_L} y(n_H, n_L)$$

# Optimized Structure

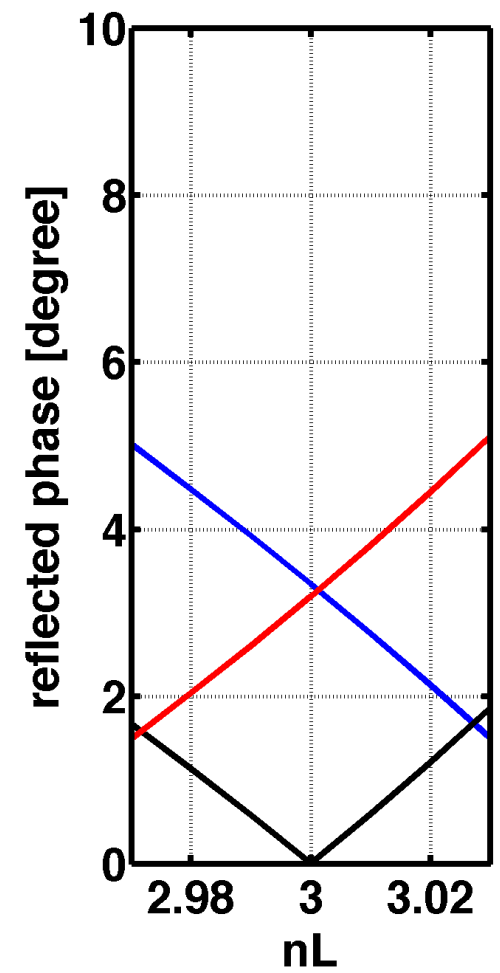
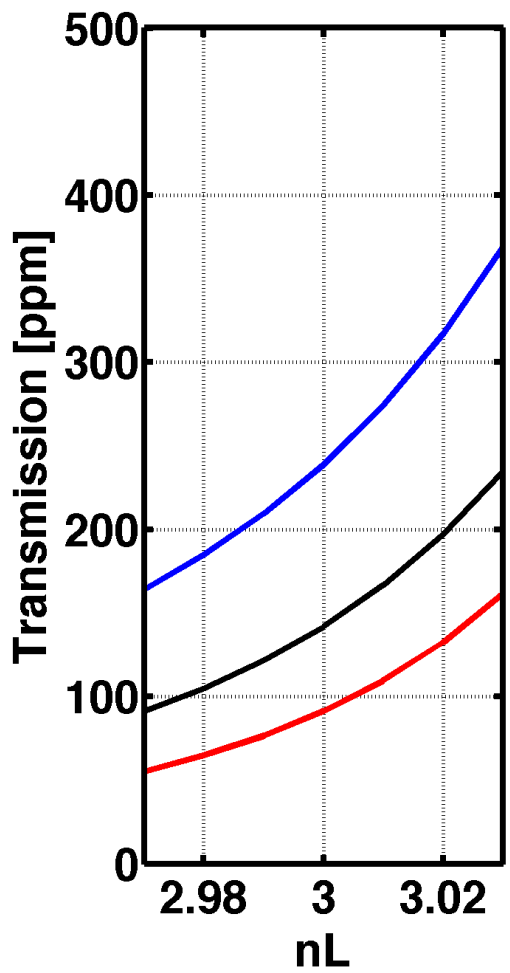
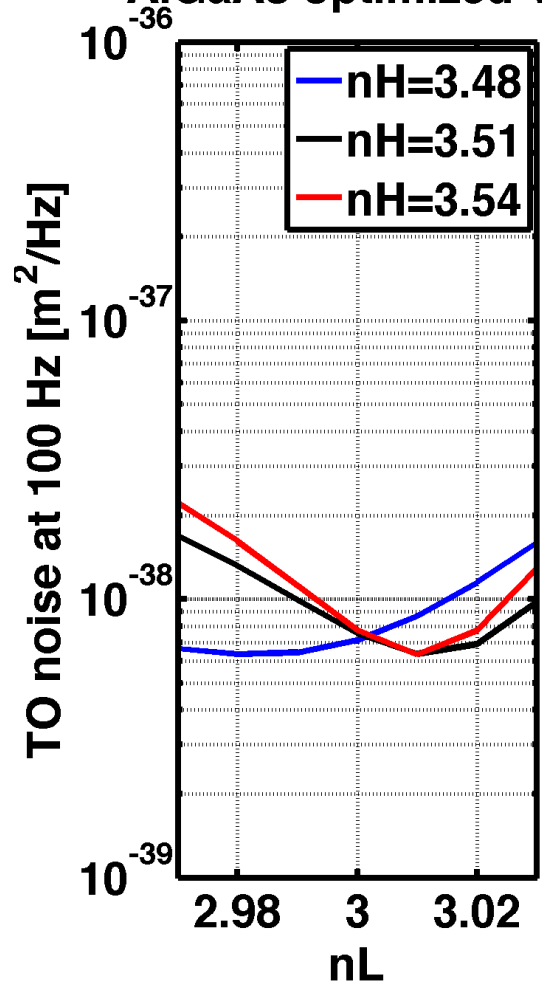


# Transmission and Reflection at 1064 nm



# Optical Properties vs nH and nL: Optimization with Robust Cost Function

AlGaAs optimized V4





# Will it Work?

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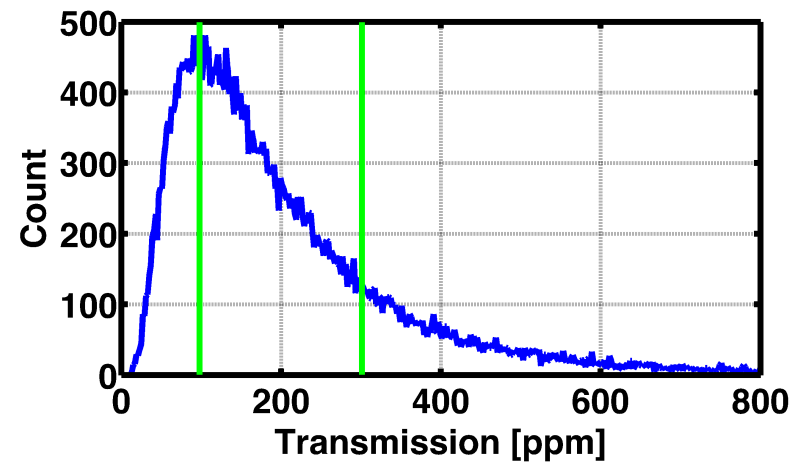
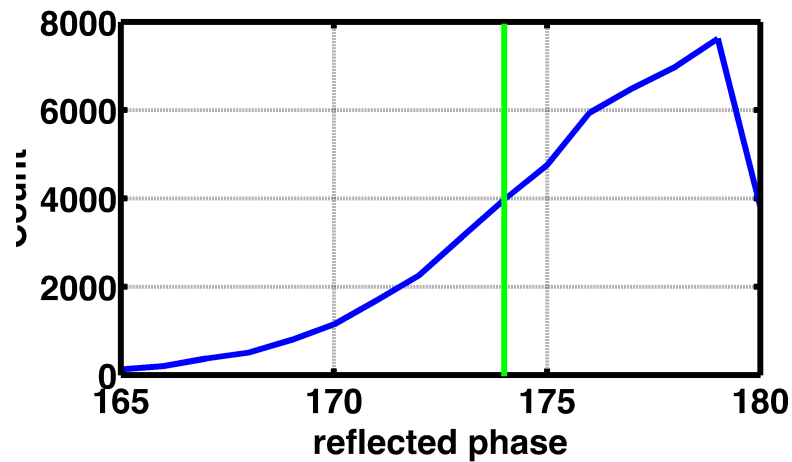
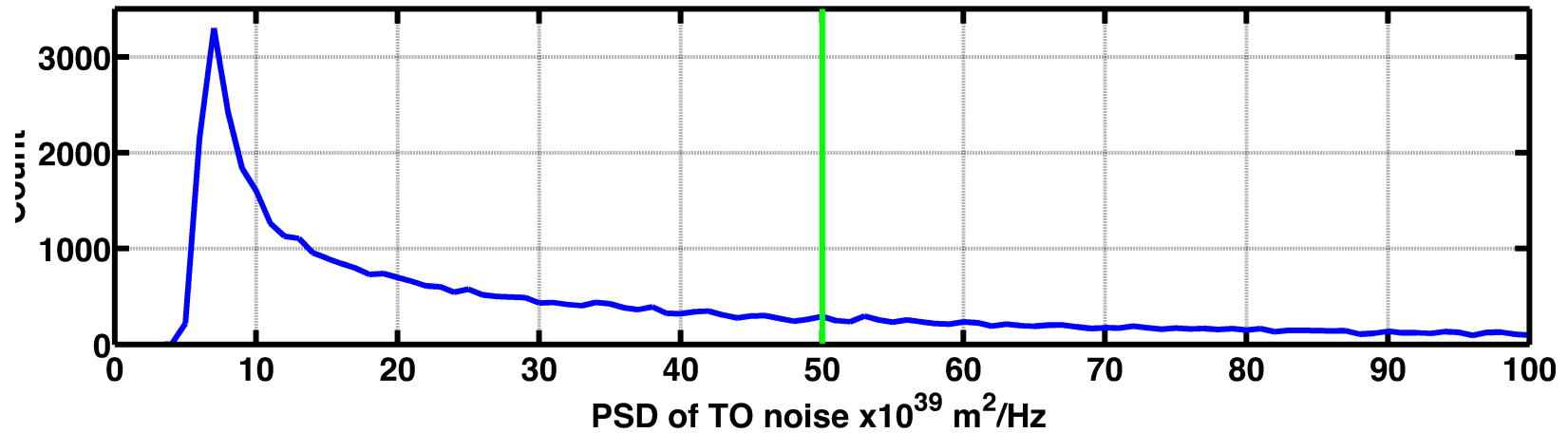
- Run MONTE CARLO test taking uncertainties in material parameters and errors from fabrication process

- Thickness Control: GaAs,  $\sigma \sim 0.5\%$

- AlGaAs,  $\sigma \sim 1\%$

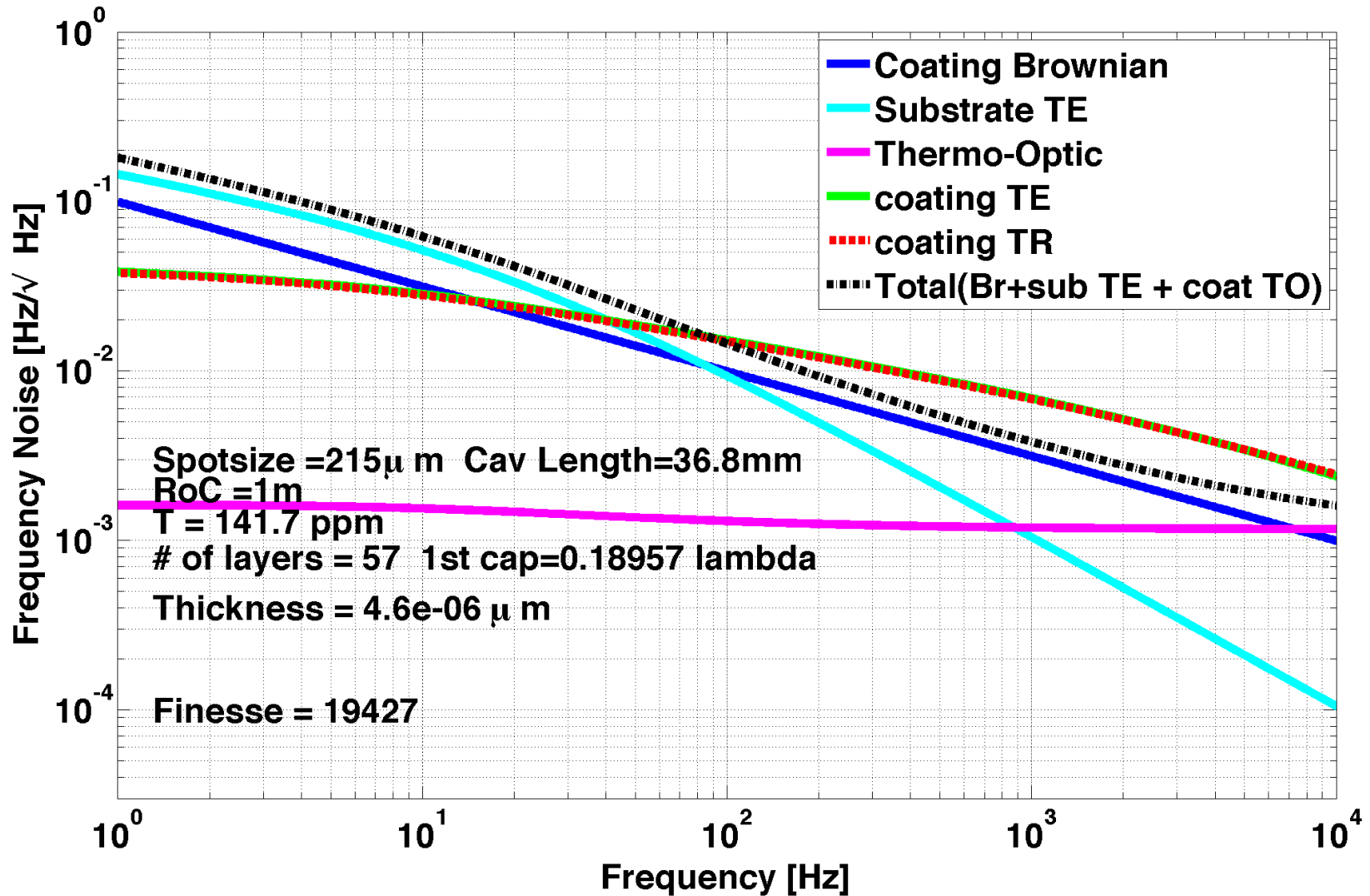
- Al Content 92%  $\pm 0.6\%$

# Histogram of Coating Properties



# Noise Budget: Optimized

## T~150ppm



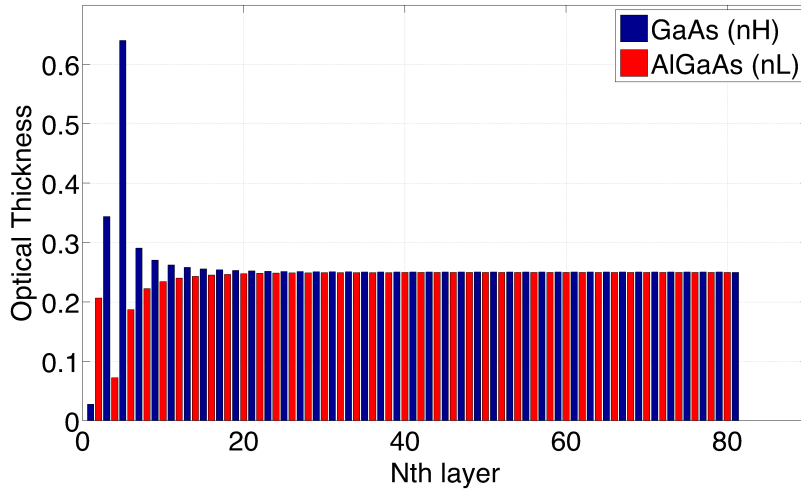
# Implications for aLIGO

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- ❑ If the optimized structure works for our test cavity, we can do the same optimization for ITM, ETM.
- ❑ For fused silica substrate.
- ❑ At room temperature.

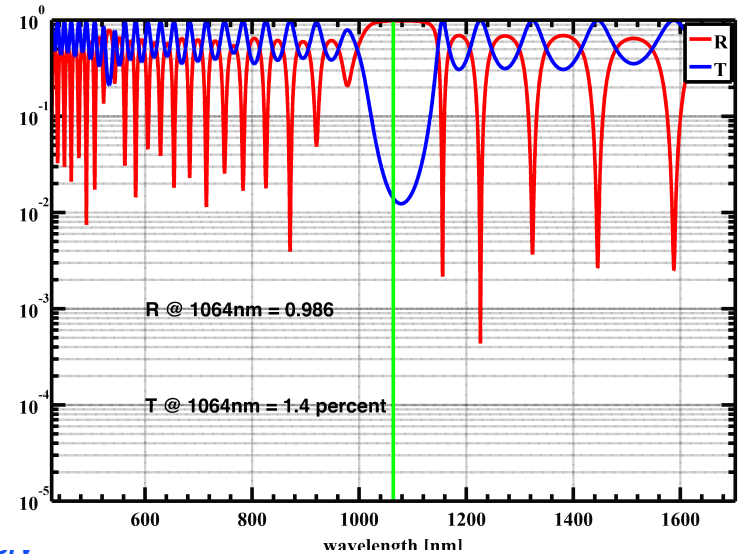
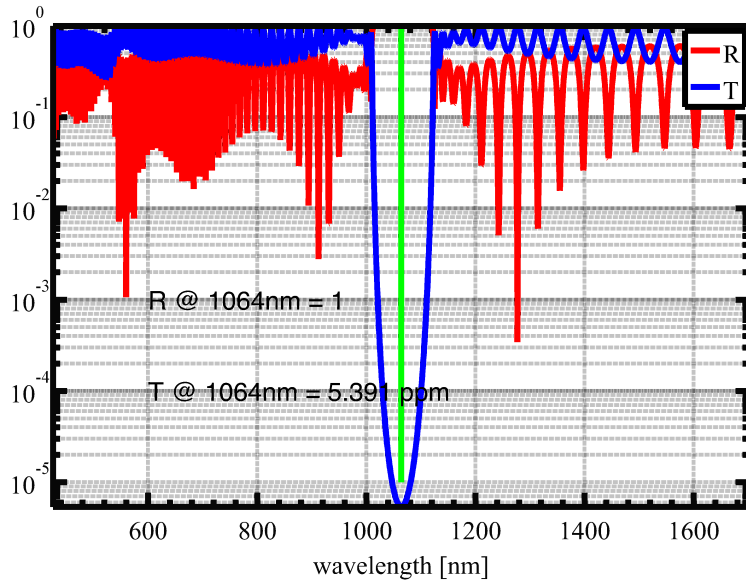
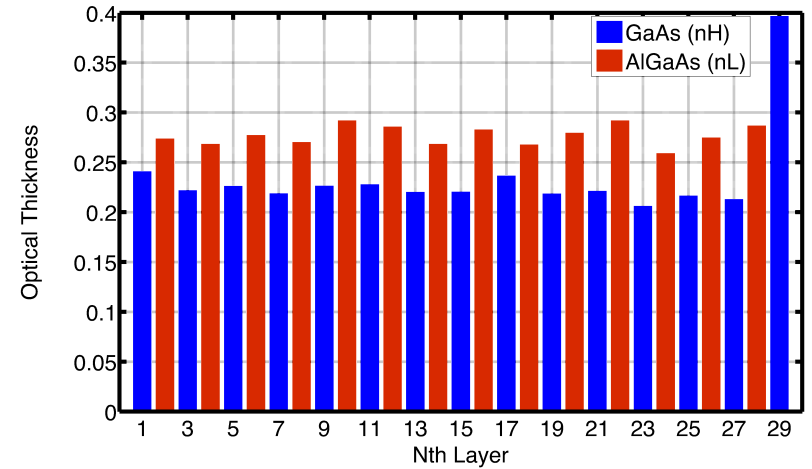
# ETM

T = 5 PPM

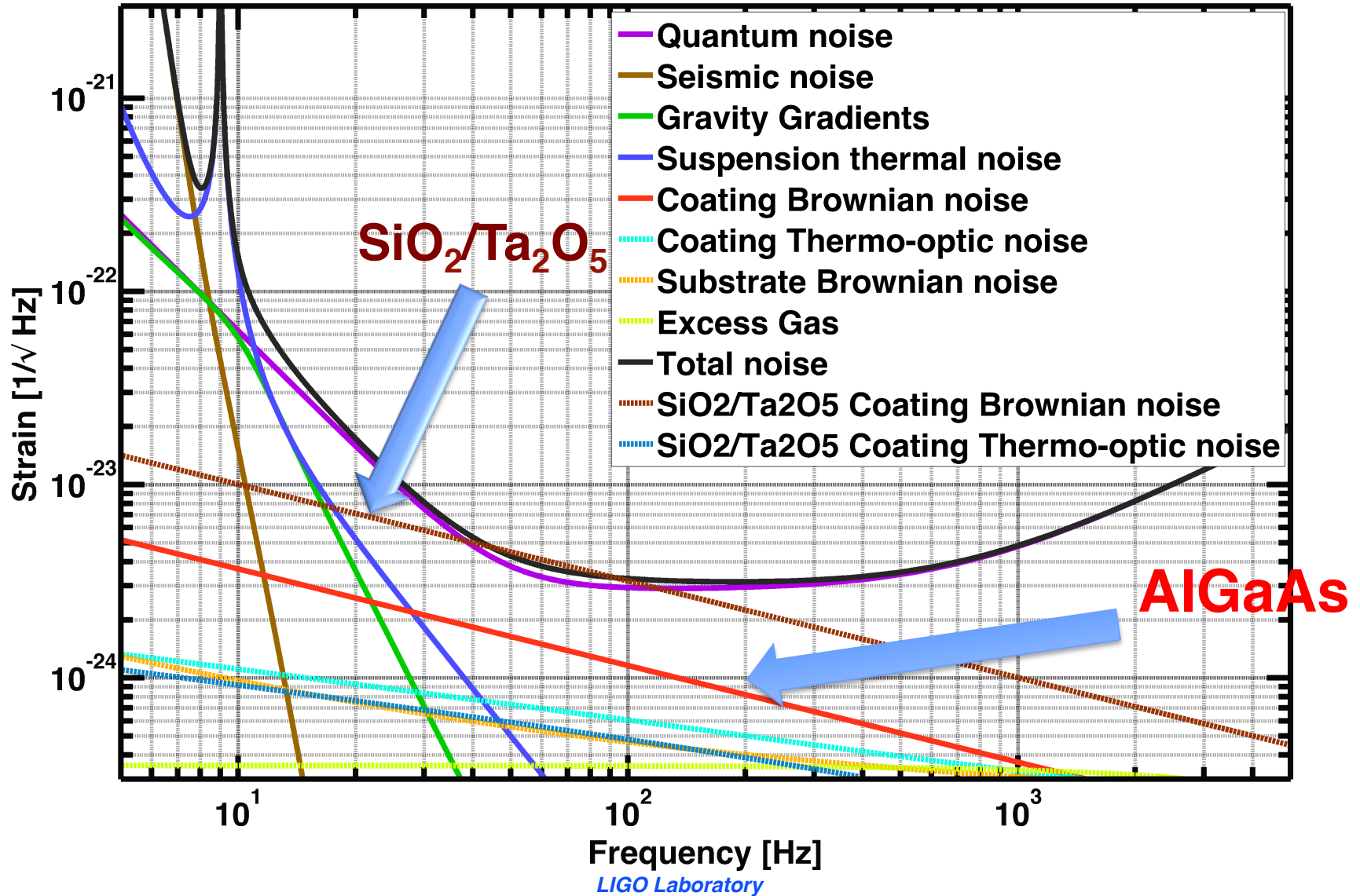


# ITM

T = 1.4 %



# aLIGO with Optimized AlGaAs Coatings



# Conclusion

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- ❑ We demonstrate a setup that can measure thermal noise in a reference cavity from 10 Hz to 1 kHz
- ❑ With data from a ring down measurement, loss angles of  $\text{SiO}_2$  and  $\text{Ta}_2\text{O}_5$  can be extracted.
  
- ❑ AlGaAs optimized coating is proposed.
- ❑ Fabrication is in progress.
  
- ❑ Optimization for AdvLIGO can improve its sensitivity.

**Thank You**



# Acknowledgement

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**The experiment is made possible because of all of them**

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- ❑ LIGO and NSF PHY-0757058.

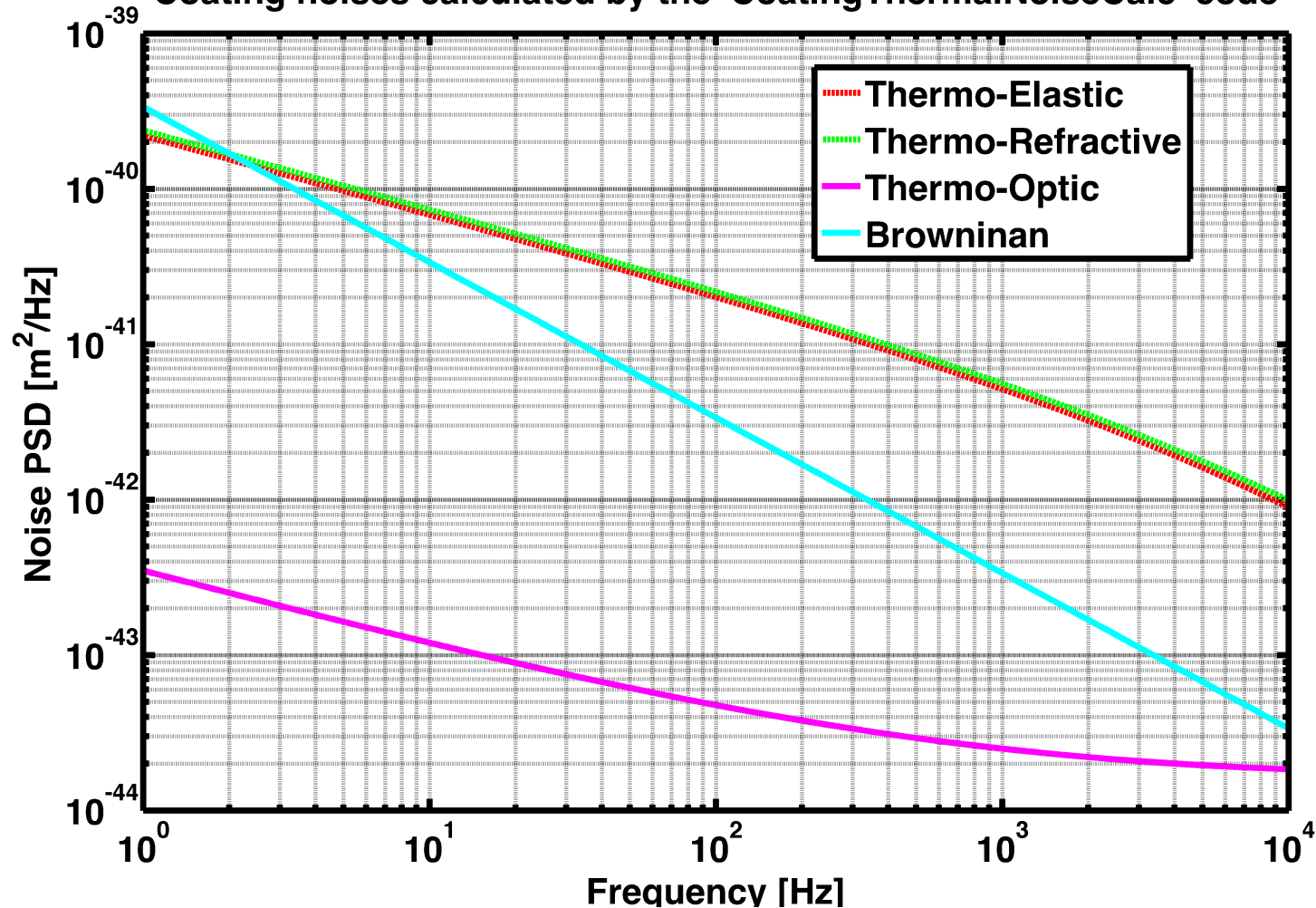


# Supplementary Information

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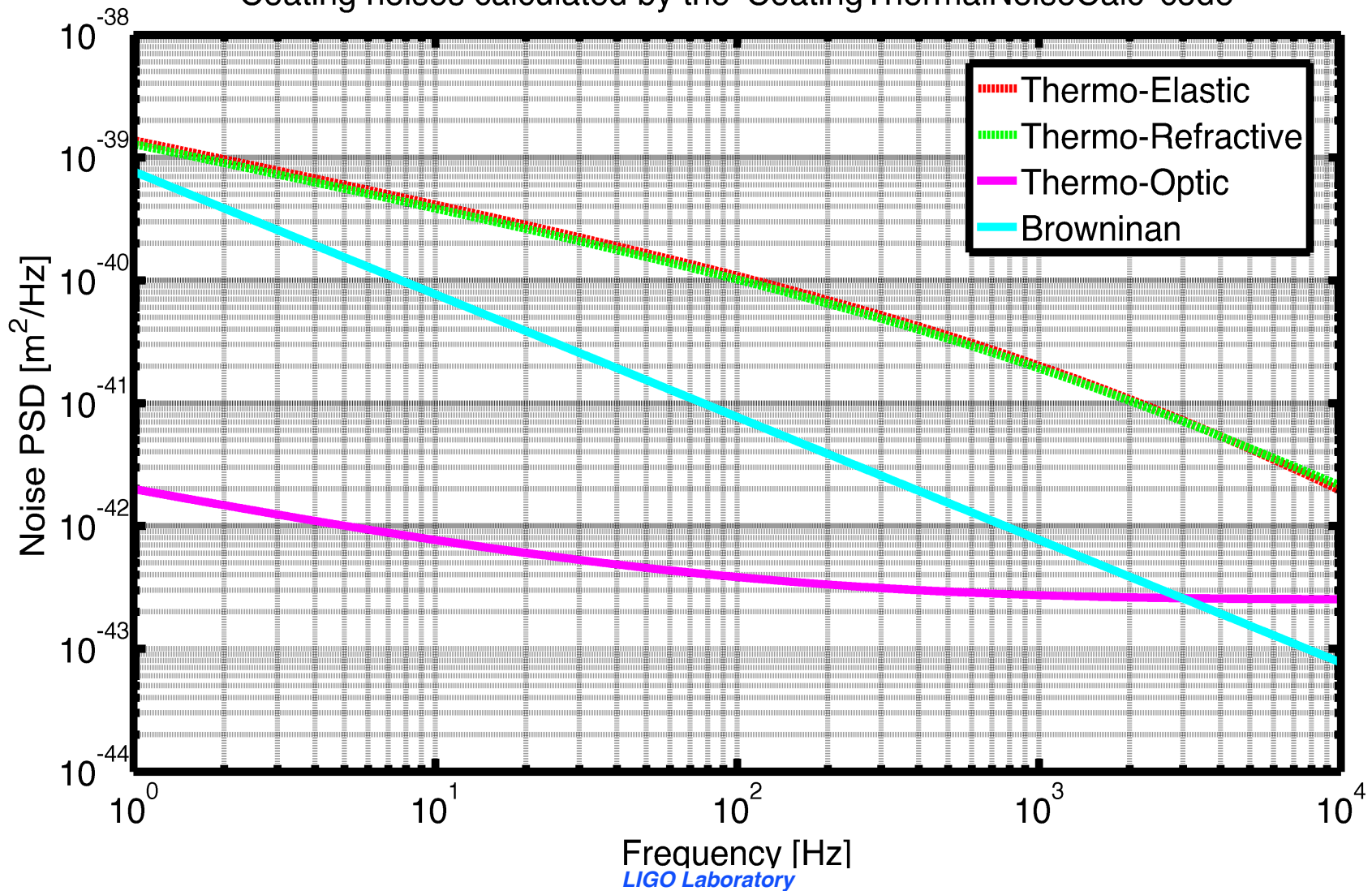
# ITM: Noise Budget

Coating noises calculated by the 'CoatingThermalNoiseCalc' code



# ETM: Noise Budget

Coating noises calculated by the 'CoatingThermalNoiseCalc' code



# Photothermal response

