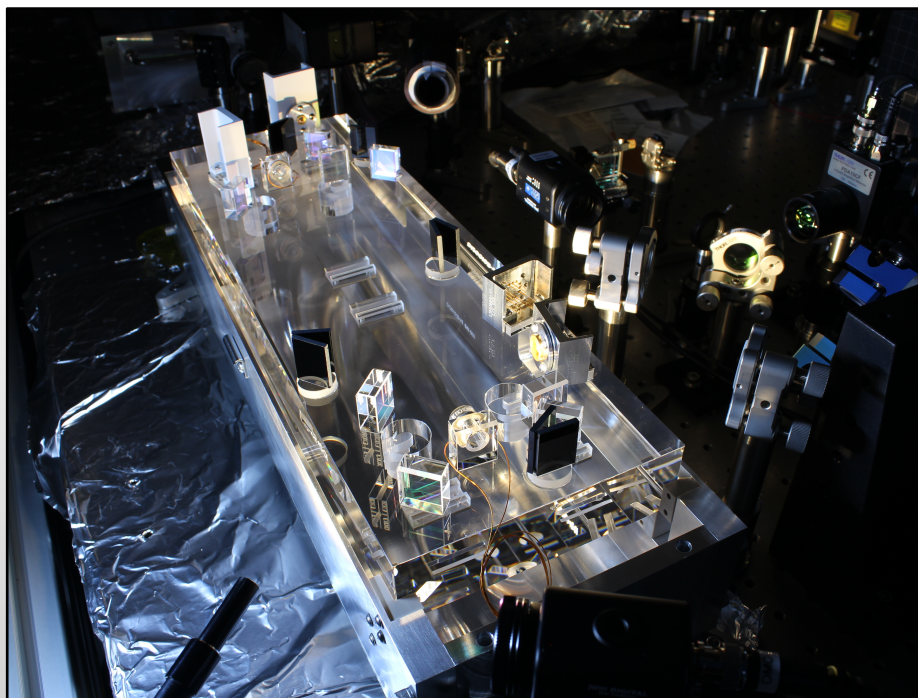


Advanced LIGO Output Mode Cleaner: Design, Fabrication and Installation



Koji Arai

LIGO Project, California Institute of Technology

LVC meeting 2013 September @ Hannover

LIGO-G1301001

Advanced LIGO Output Mode Cleaner (OMC)

- An optical cavity to remove unwanted optical fields from the interferometer output beam.
- The first OMC was built and tested at Caltech, and installed at LLO
- The design, fabrication, and test results

OMC ISC team

Rich Abbott¹, Koji Arai¹, Sam Barnum³, Peter Fritschel³, William Korth¹, Jeffrey Lewis¹, Charles Osthelder¹, Sam Waldman³

OMC SUS team

Stuart Aston², Jeffrey Bartlett⁴, Derek Bridges², Jeffrey Kissel³, Norna Robertson¹

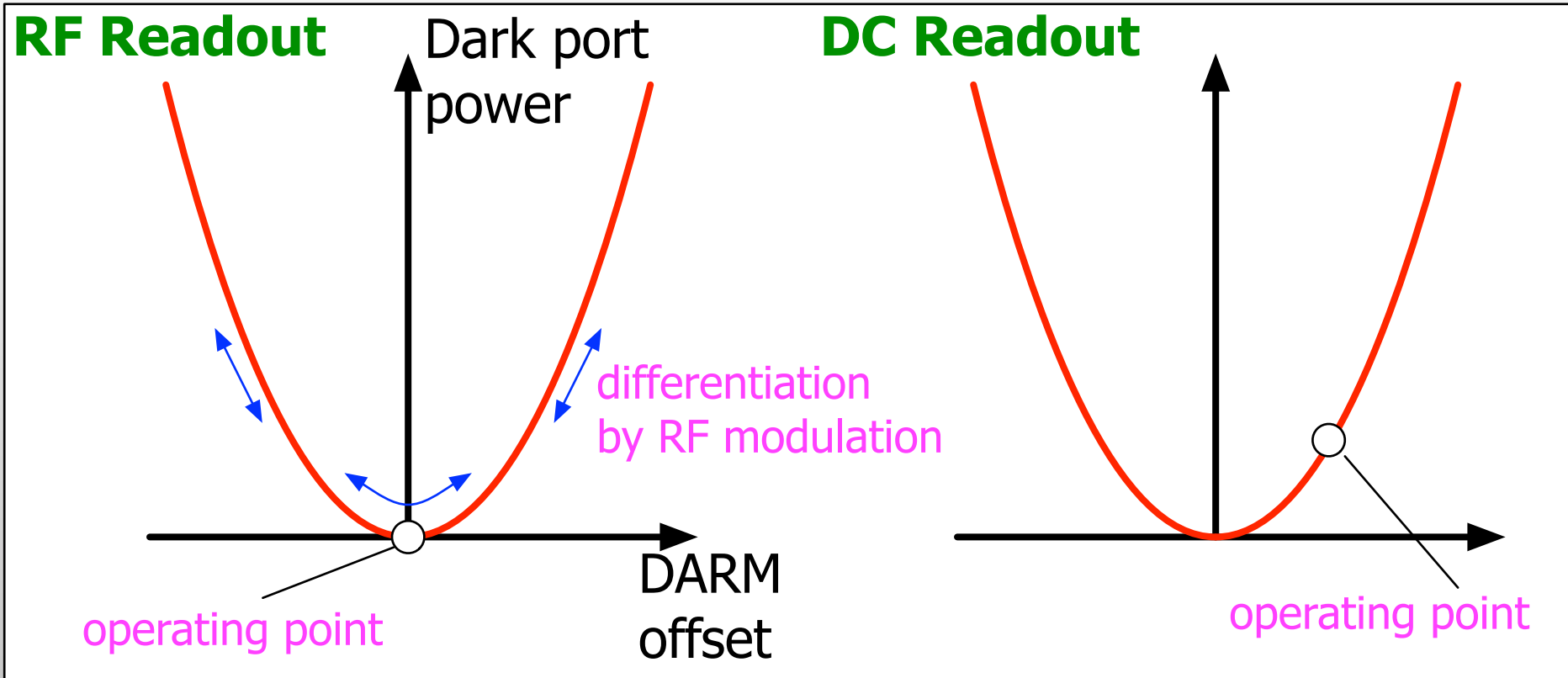
LIGO Laboratory: California Institute of Technology¹, LIGO Livingston Observatory², Massachusetts Institute of Technology³, LIGO Hanford Observatory⁴

Mission of the OMC

Koji Arai
LVC Hannover Sep. 24, 2013
LIGO-G1301001 P3

DC Readout

aLIGO employs a DC readout scheme for sensing of GW signals



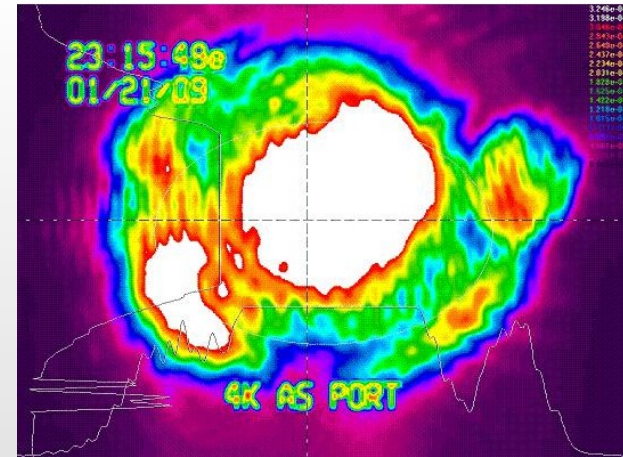
DC Readout is good:

- removes nonstationary shot noise
- mitigates technical noises associated with the RF sidebands

Enemies of the DC Readout

- Carrier HOMs (higher-order modes)
- RF modulation sidebands (any spacial modes)

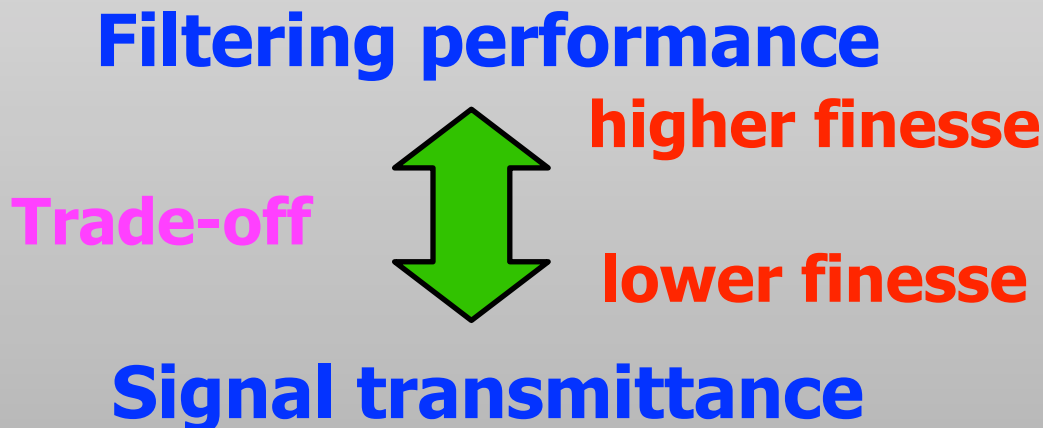
do not contribute to the signal
and increase the shot noise



eLIGO AS port beam

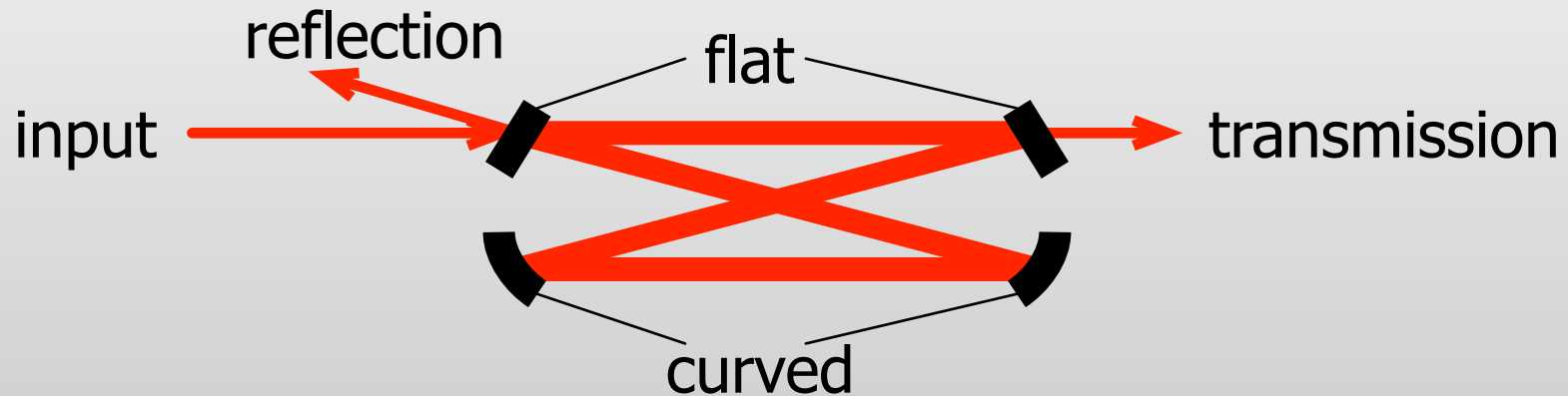
Output mode cleaner

the idea is to use a short ($\sim 1\text{m}$) optical cavity for the filtering



Basically eLIGO OMC design was followed

- Bowtie 4-mirror ring cavity
even mirrors => simpler HOM structure
ring cavity => less back scattering

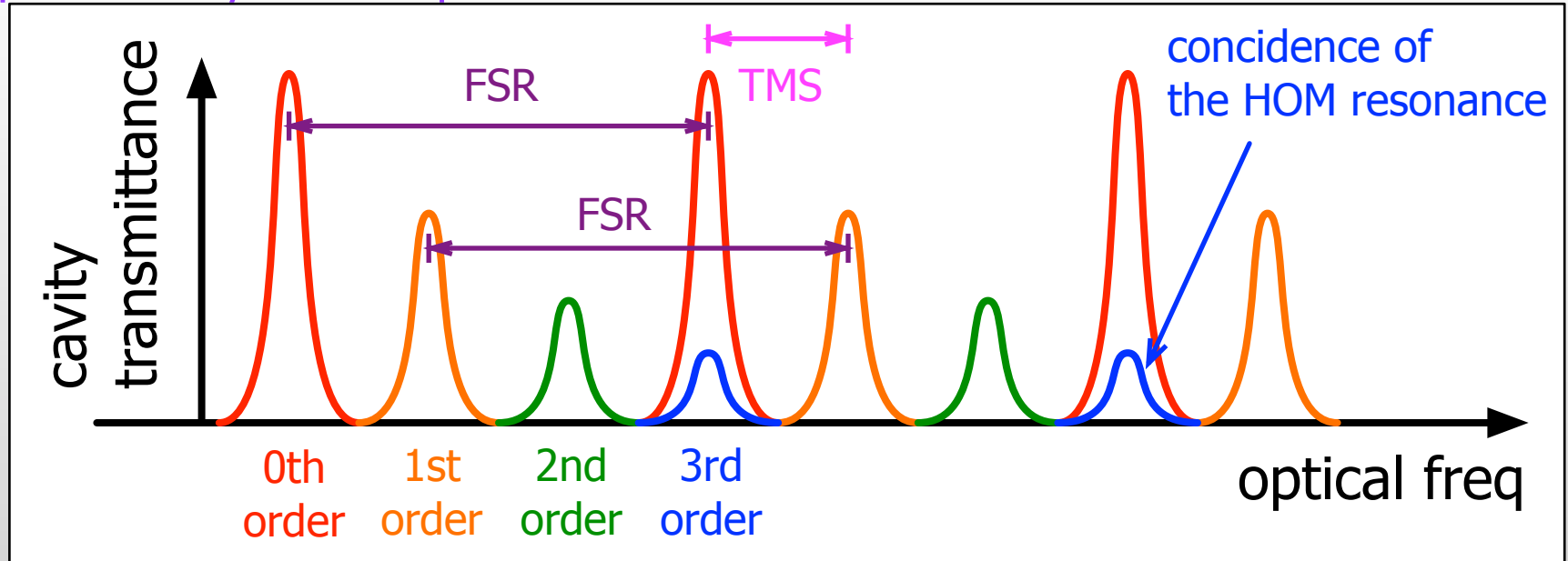


- Finesse: ~ 400 (for $\sim 98\%$ transmission)
Roundtrip length $\sim 1\text{m}$ (the breadboard size)
Curved mirror radius $\sim 2.5\text{m}$

Filtering Performance

Important parameter: Transverse Mode Spacing (TMS)

An optical cavity has a repetitive resonant structure



If TMS/FSR is a rational number (m/n), n -th order HOMs get transmitted

MOREOVER: The vertical and horizontal modes have different TMSs due to astigmatism of the curved mirrors (i.e. non-zero incident angle)
=>The higher the mode number, the wider the resonance is.

TMS/FSR is dependent on the cavity geometry

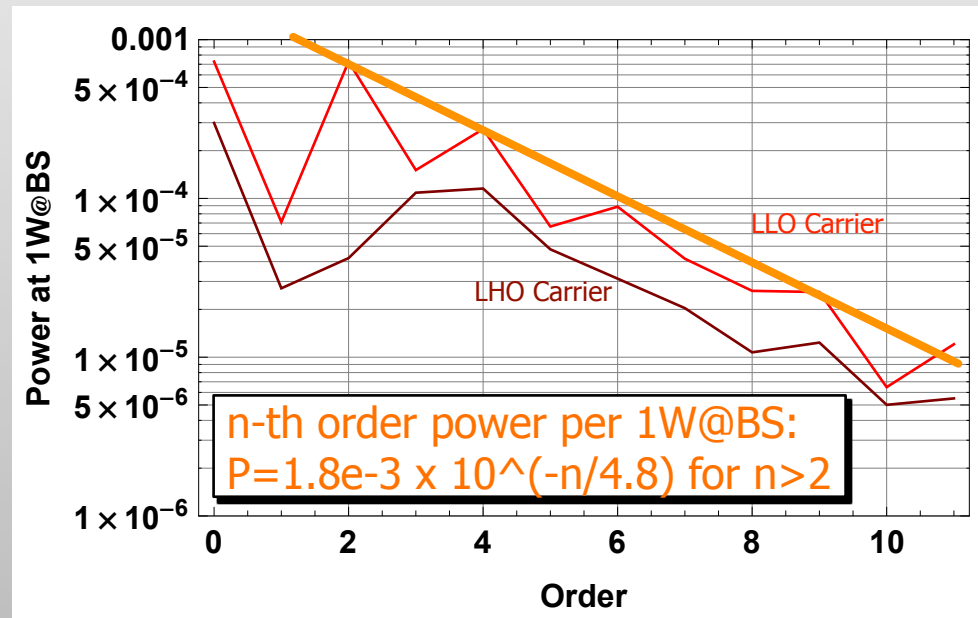
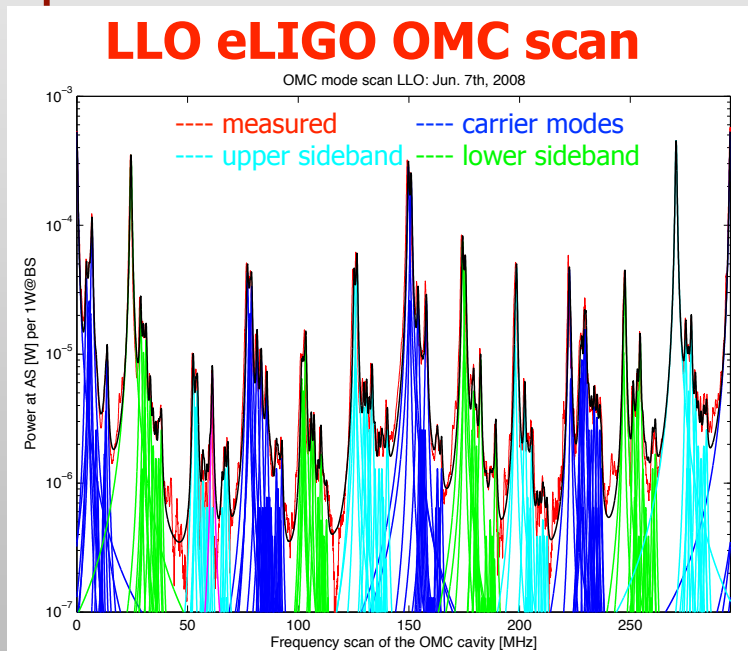
=>Careful adjustment of TMS/FSR is the key to avoid HOMs

Estimation of the filtering performance

Total transmitted power

$$= \sum (\text{power in each mode}) \times (\text{transmission of each mode})$$

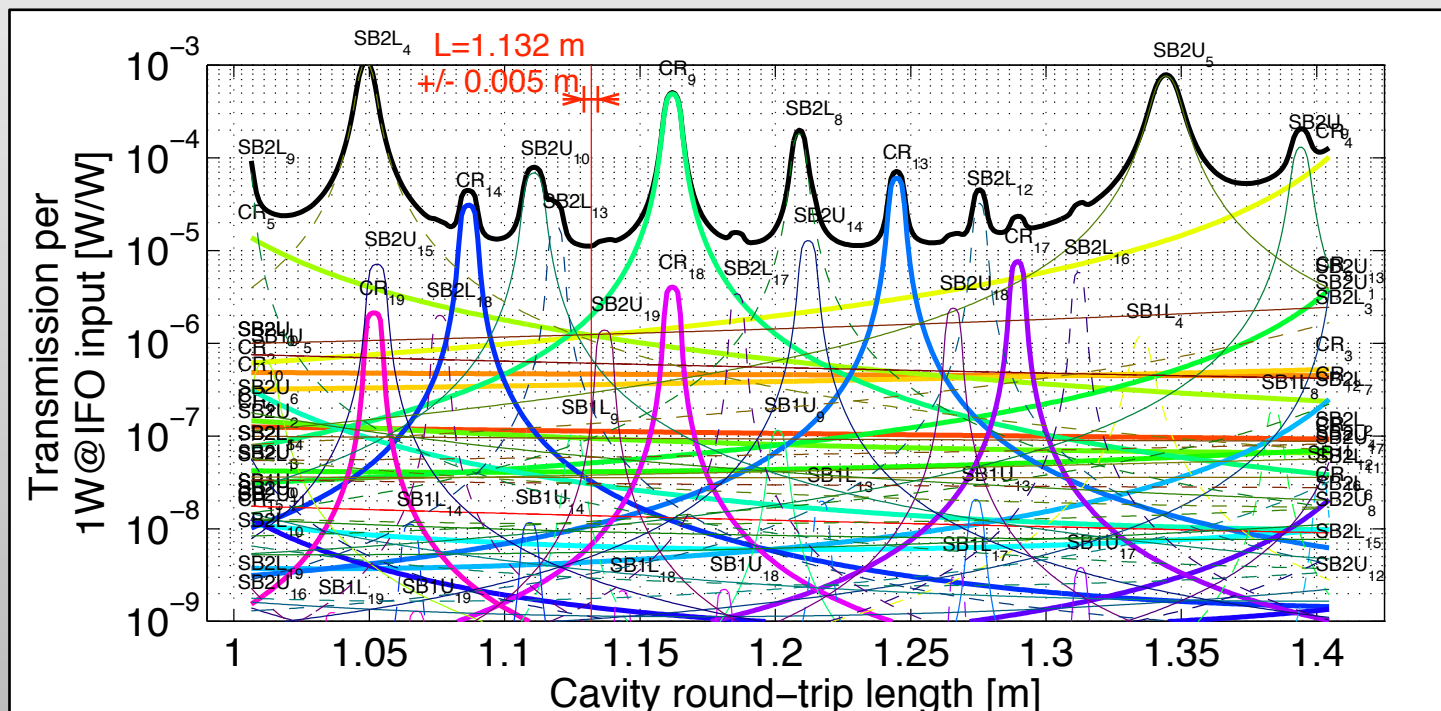
- Modeling of the interferometer output beam (details in G1201111)
power laws based on the eLIGO performance of the IFO optics



This wouldn't be a prediction, but have some usefulness, anyway

Estimated filtering performance

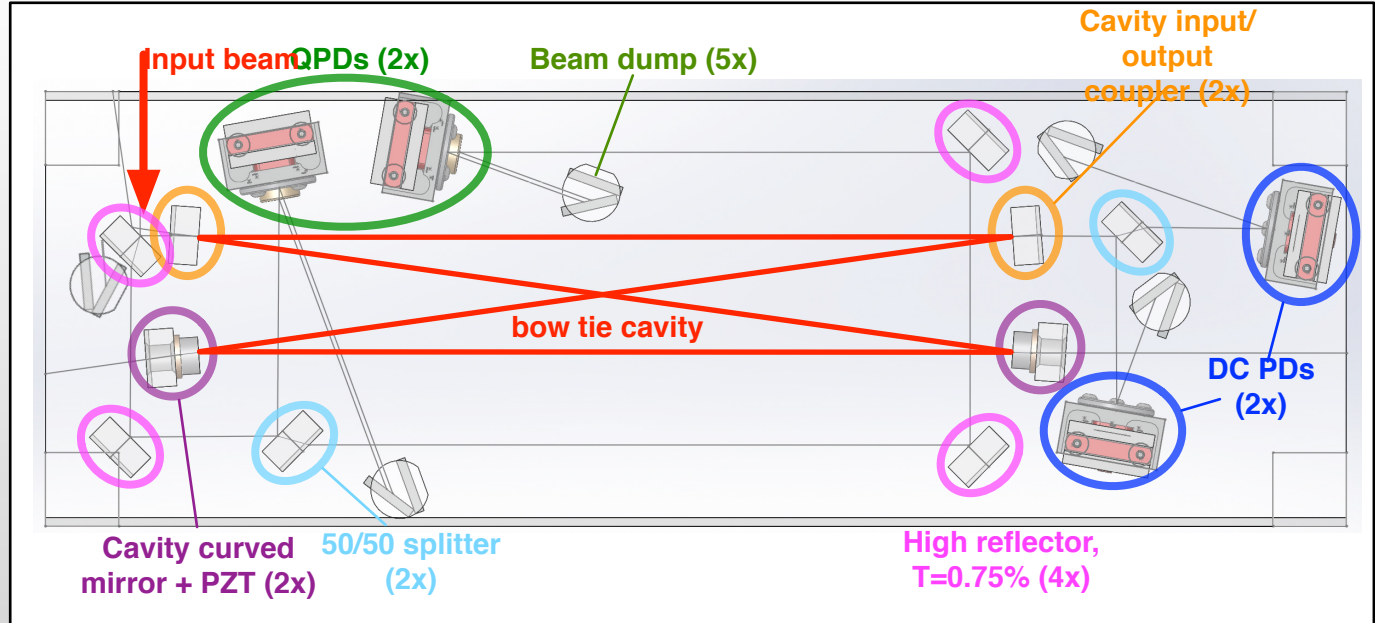
- Expected junk light power at the dark port (100W input = 4kW @BS)
~12W leakage => filtered down to 1mW. Well within the PD capability.
This could become better thanks to mode healing and better optics in aLIGO
- Cavity length tolerance: $L=1.132 \pm 0.005$ [m]
- Mirror RoC tolerance: $R=2.575 \pm 0.015$ [m]



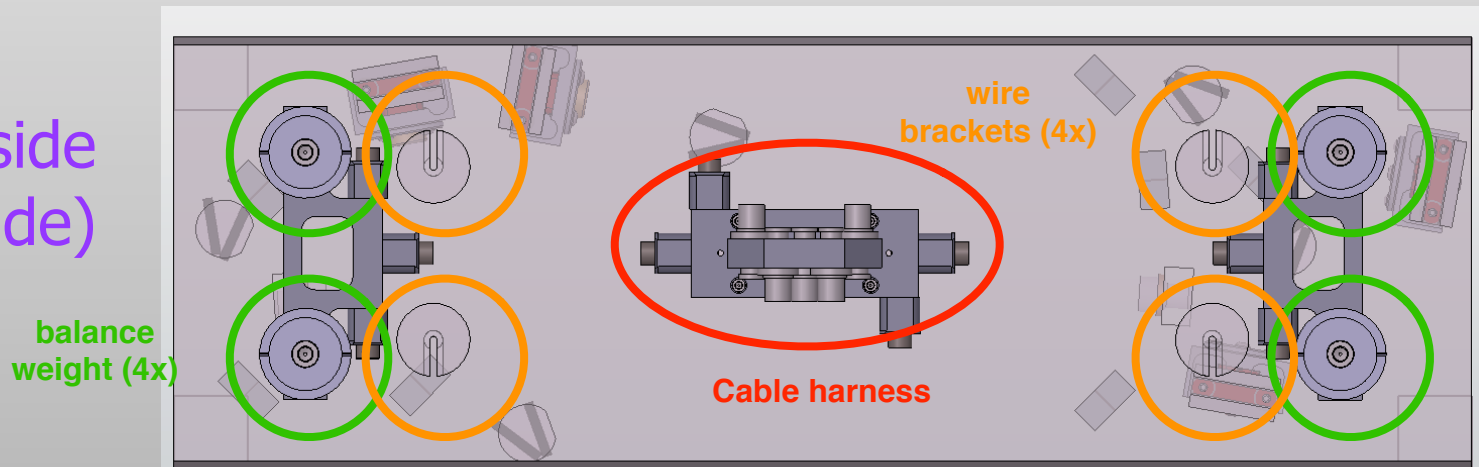
CRn - carrier n-th mode, SB(1,2)(U,L)n - sideband n-th mode,
SB1 - 9MHzSB, SB2 - 45MHz SB, U - upper SB, L - lower SB

How the OMC breadboard looks like

Bottom side
(cavity side)

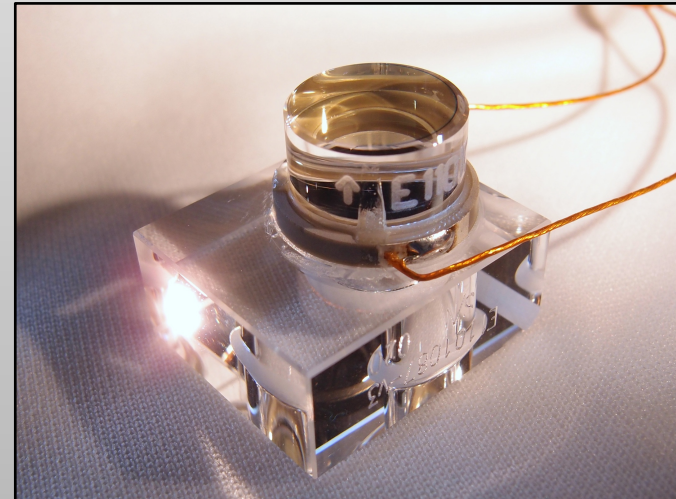
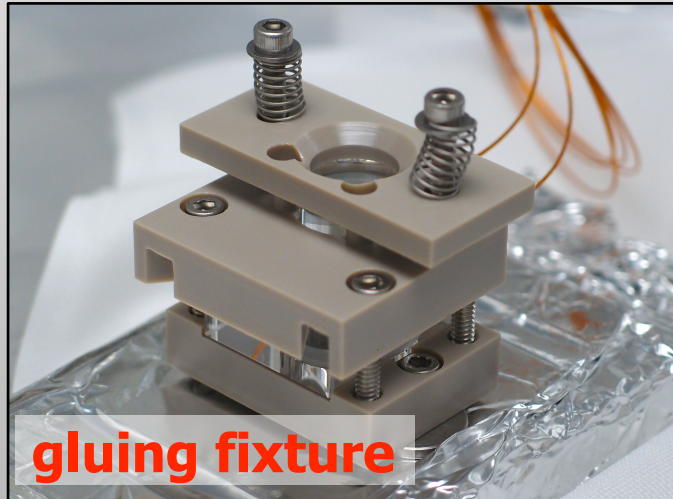
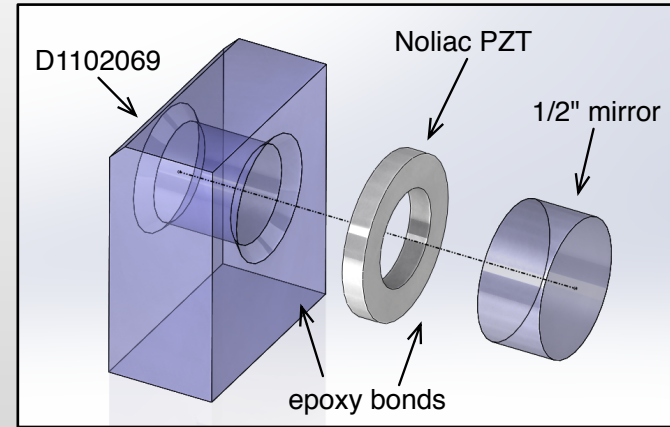


Top side
(cable side)



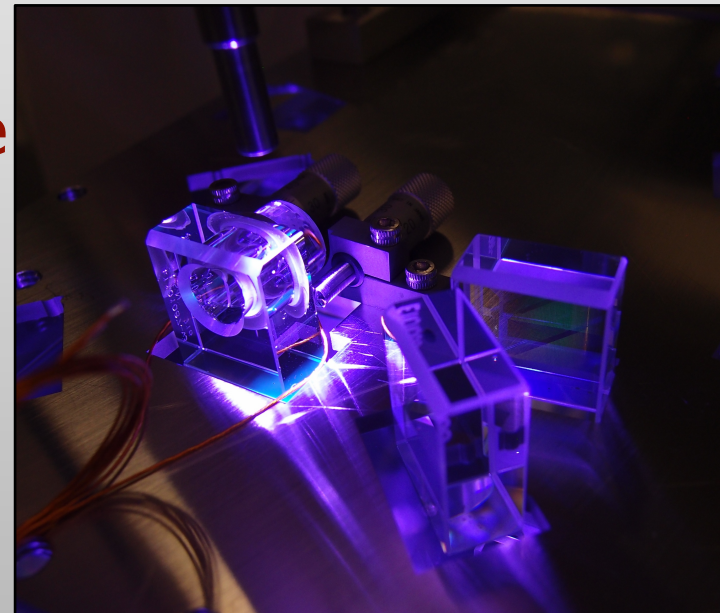
PZT-curved mirror subassembly

- PZT + 1/2" curved mirror: Glued on a mounting prism
- Bonding: Epoxy with borosilicate glass spheres (75-90um dia.)
- Wedging of the components:
Characterized and arranged to minimize pitch misalignment of the cavity



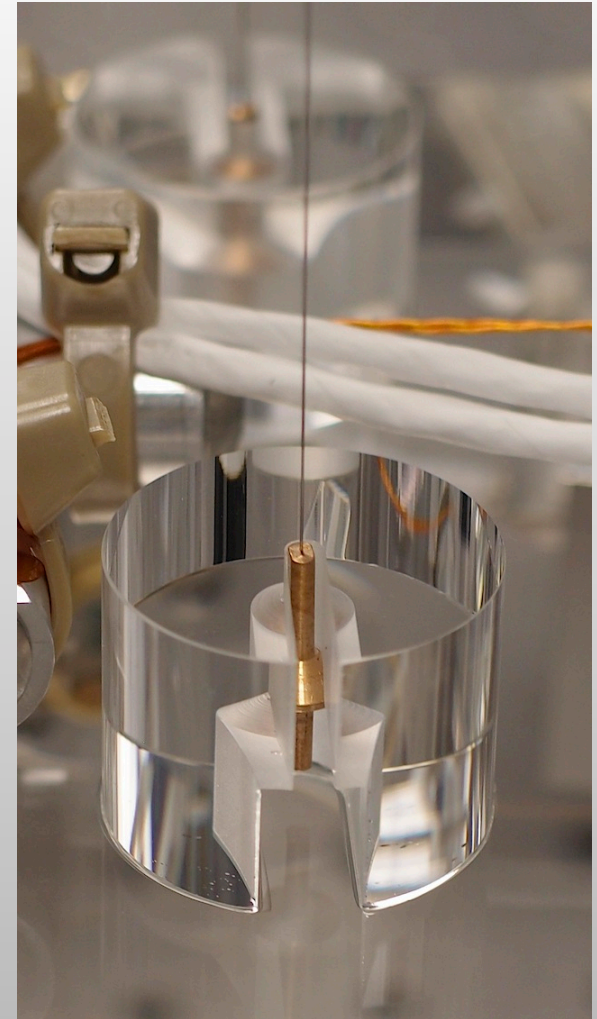
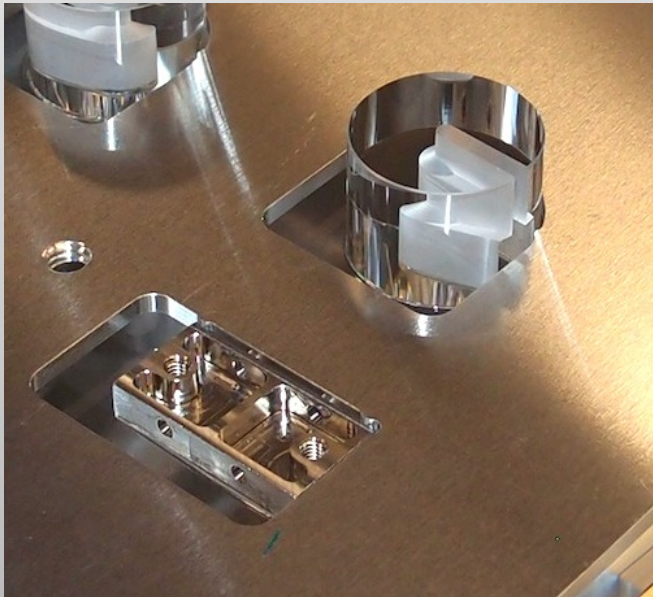
Bottom (cavity) side gluing

- Breadboard: held in a transport fixture
- Flat optics: Fused silica prisms with mirror coatings
- Template: for optics alignment
- Fine alignment:
each curved mirrors were aligned with two micrometers on the template
- Monitoring of the FSR and TMS with an optical testing setup
- Bonding:
UV-cure epoxy & UV illumination



Top (cable) side gluing

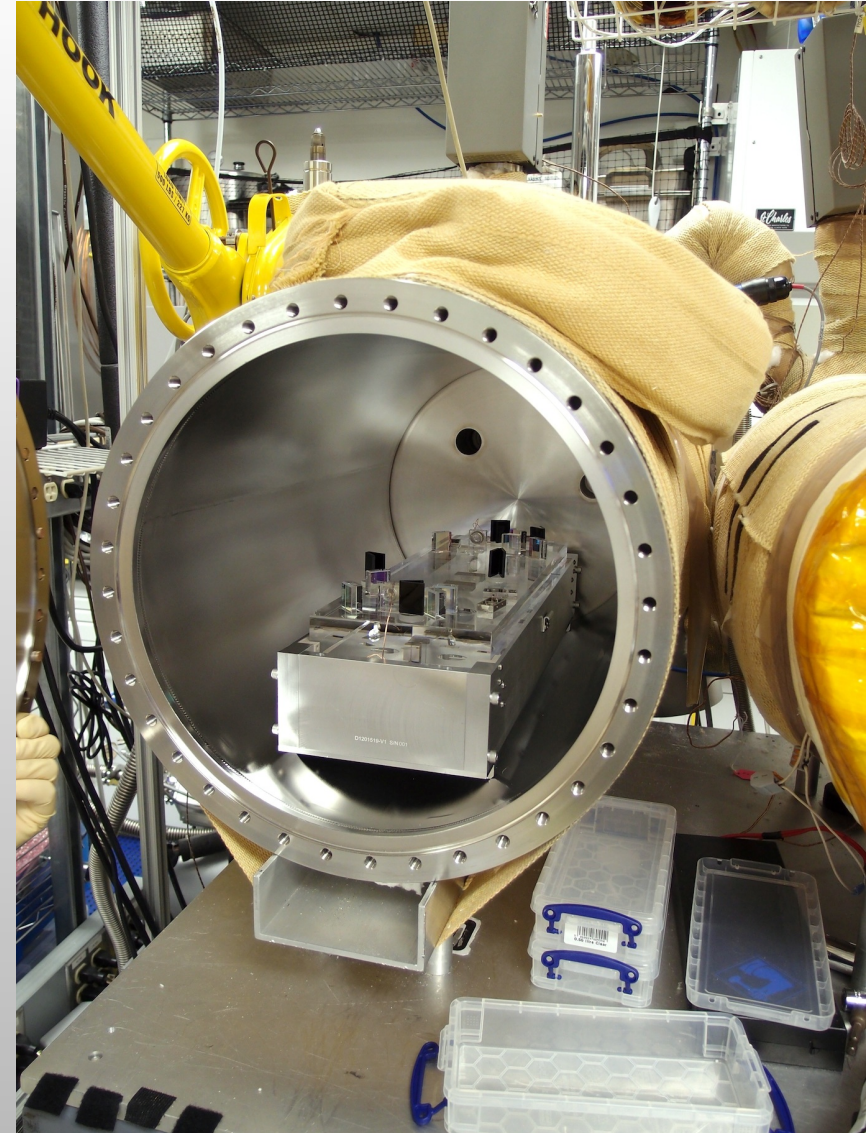
- Suspension interface: Glass wire brackets
To hook the suspension wires with conical clamps crimped
- Mounting blocks:
Made of Invar to minimize CTE difference



Vacuum Baking

at 80degC for 48 hours

- completion of curing epoxy
- reduce surface outgass



Attaching peripheral components:

- DC photodiodes / QPDs

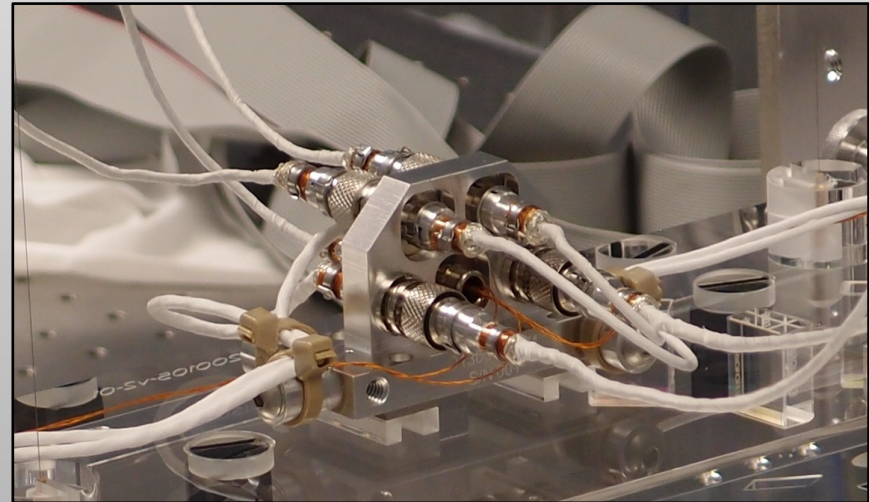
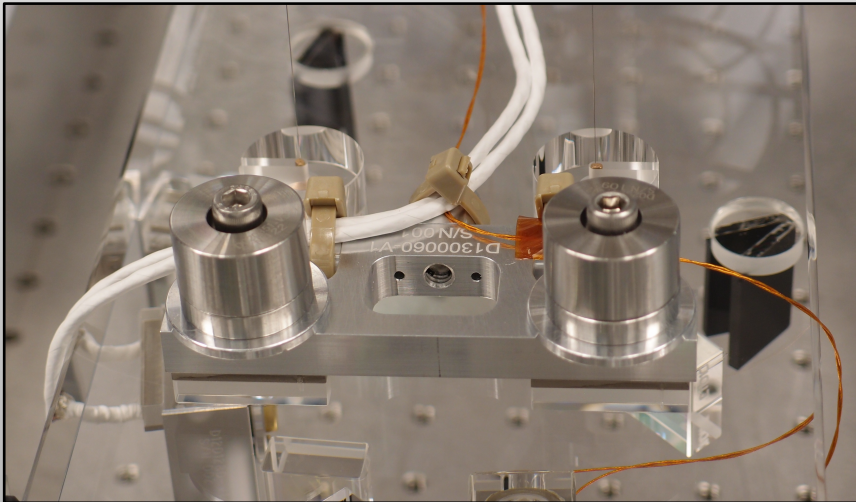
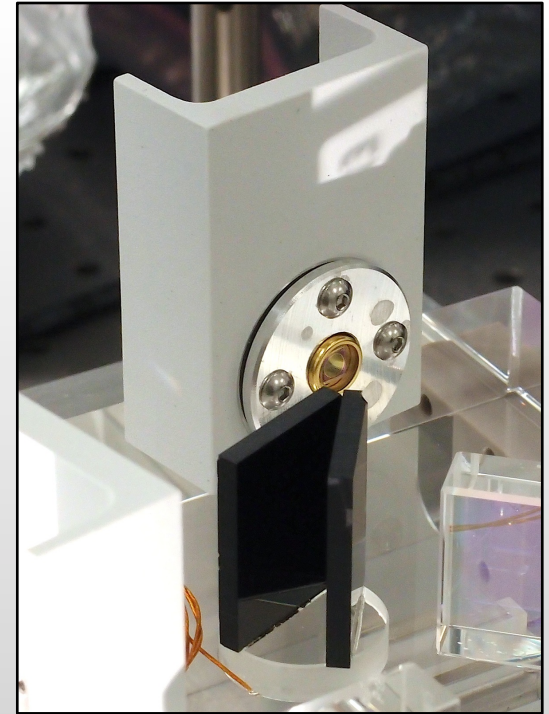
Housings mounted on invar blocks

Height adjusted by shims

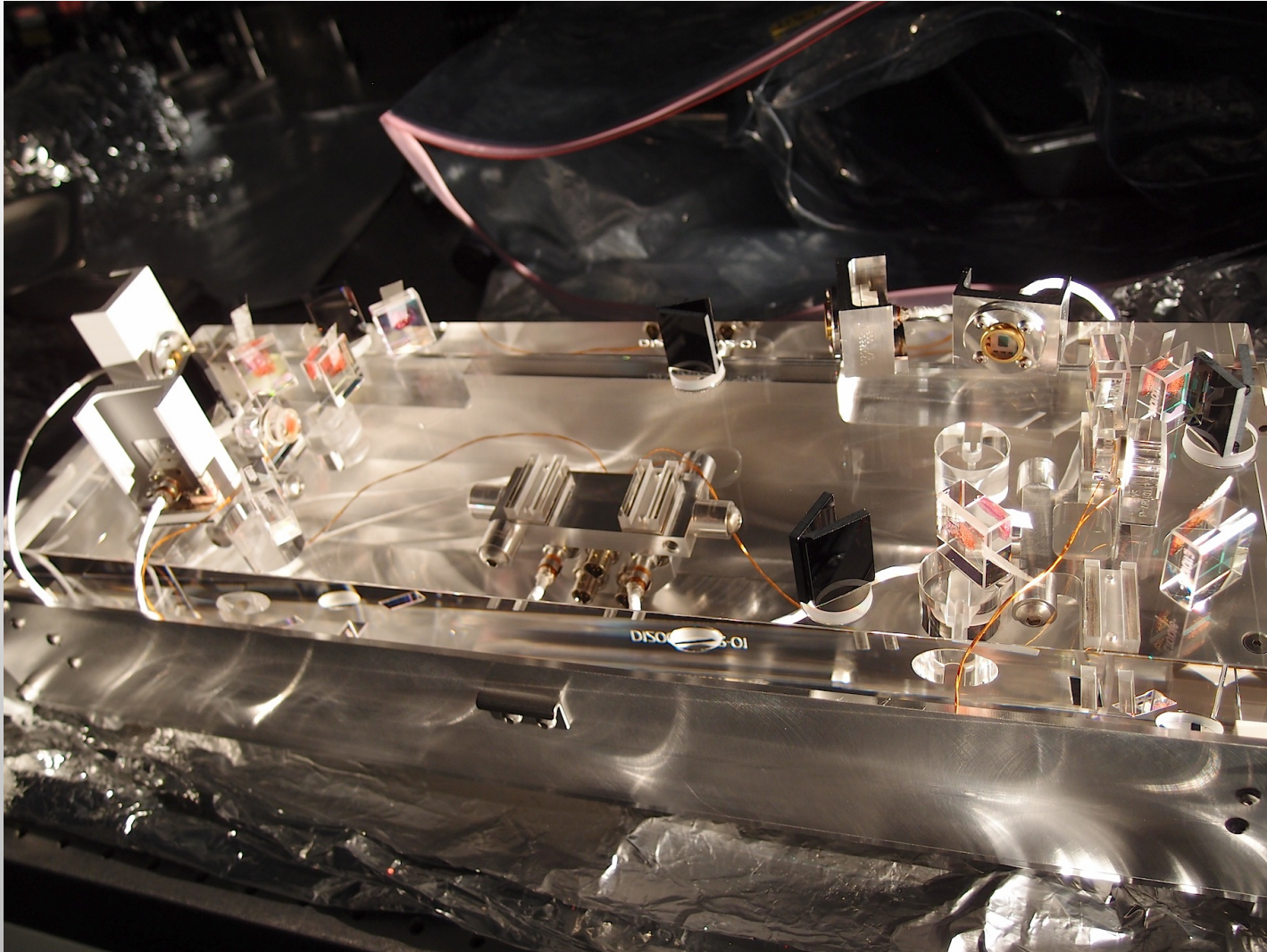
DICPD housing coated with Alumina

- Cables

Routed to the cable harness



OMC ready for the shipment



A tabletop setup@CIT

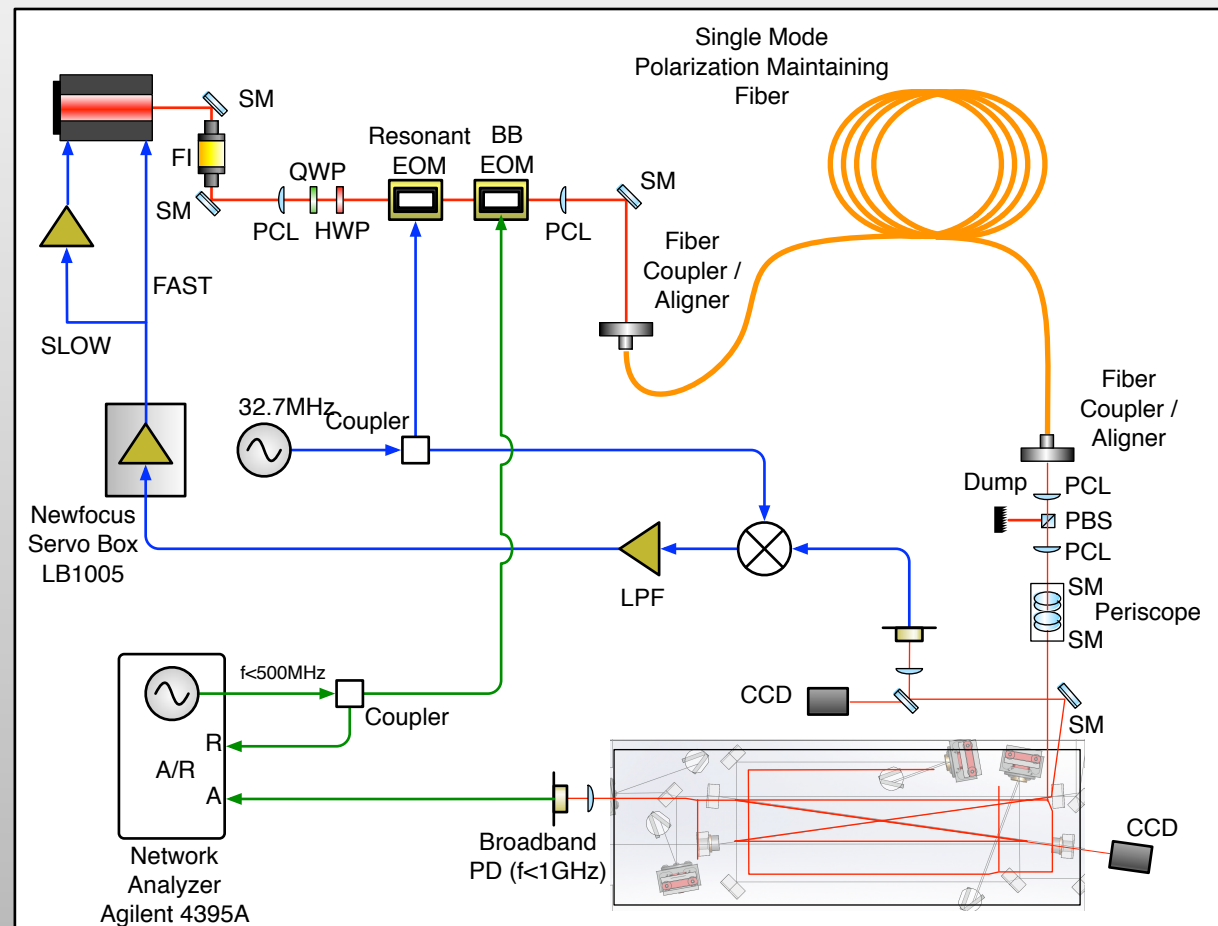
- fine parameter adjustment during the gluing
- characterization after the baking

Power budget

PZT responses

- A broadband EOM

FSR, finesse,
and HOM structure



Power Budget

Estimated from the input power, transmitted power, visibility, and cavity finesse

Specification

Cavity transmission for TEM ₀₀ :	97.8 %	98.4 %
Curved mirror transmission:	42 ppm	50 ppm
Loss per bounce:	22.3 ppm	10 ppm
Loss per roundtrip:	173 ppm	140 ppm
PD Q.E.	92%	
Total thruput of TEM ₀₀	90%	(PD Q.E. = 92%)

About 20% total loss allowed for 6dB squeezing.

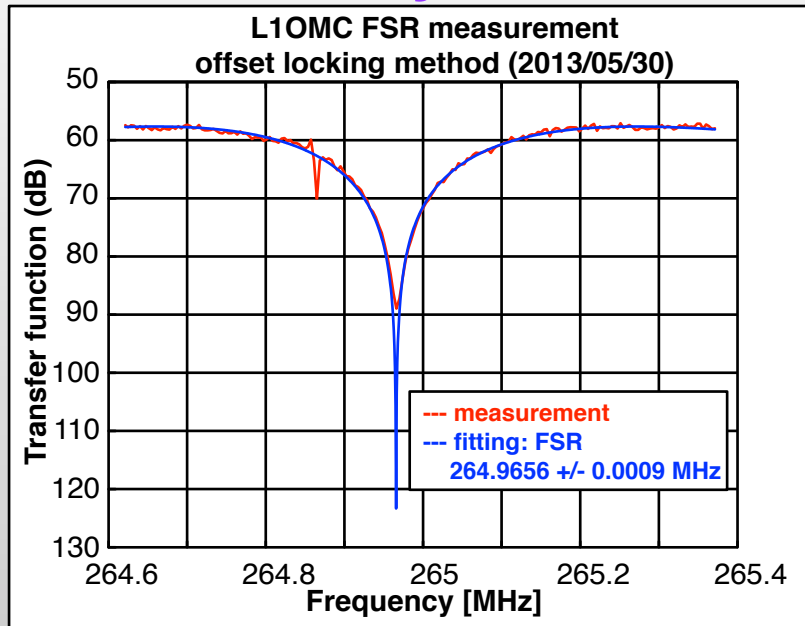
A half of the budget already eaten up by the OMC. **(not nice)**

These PDs were previously (eLIGO) reported to have Q.E. > 95%

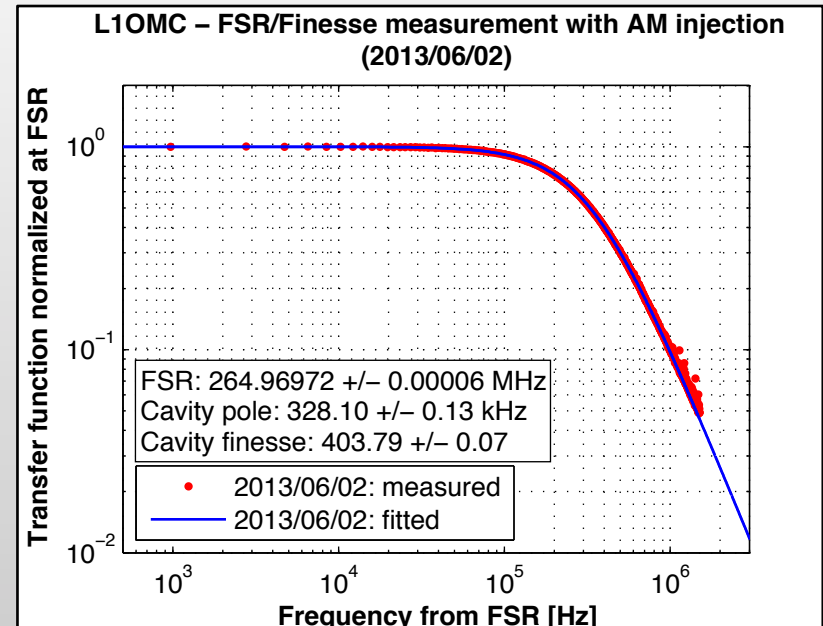
Need further investigation (or replacement)

Cavity round-trip length \sim two methods

- 1) Offset locking: FM-AM conversion at around the FSR
- 2) AM sideband injection



Method1



Method2

Cavity length: (Spec.: 1.132 +/- 0.005 m)

1.131438 +/- 4×10^{-6} m

1.131421 +/- 3×10^{-6} m

Finesse: (Spec. 390)

403.79 +/- 0.07

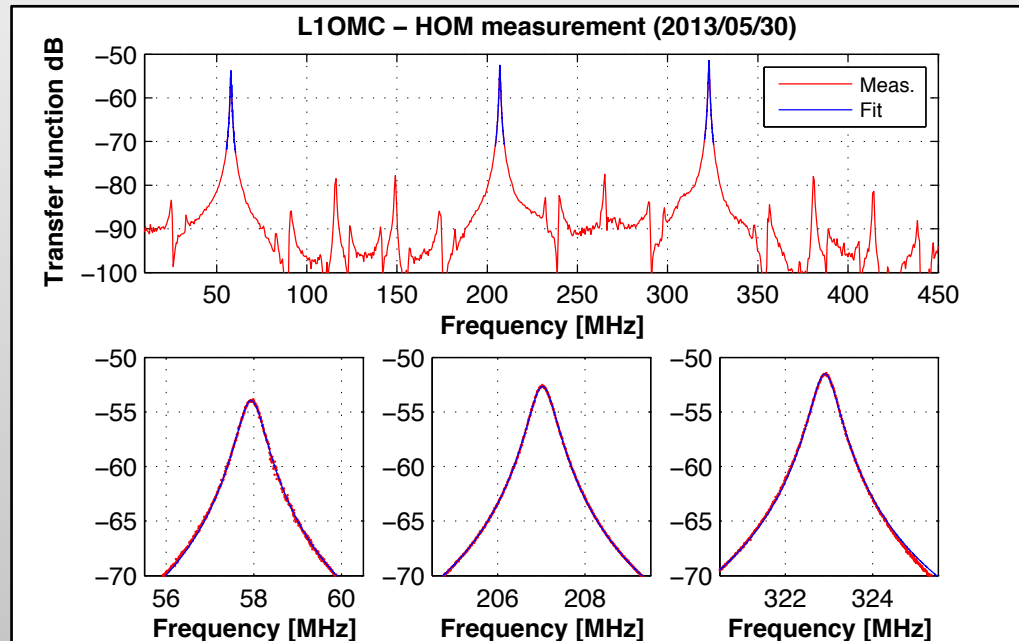
Transverse Mode Spacing (TMS)

PM sideband injection, intentional misalignment of the input beam

-> Carrier TEM₀₀ and RF HOM get resonant

Intentional clipping at the transmission PD

-> RF signal on the PD



Result:

Pitch TMS/FSR: $0.218822 \pm 1 \times 10^{-6}$

Yaw TMS/FSR: $0.219218 \pm 1 \times 10^{-6}$

Spec.

0.2188

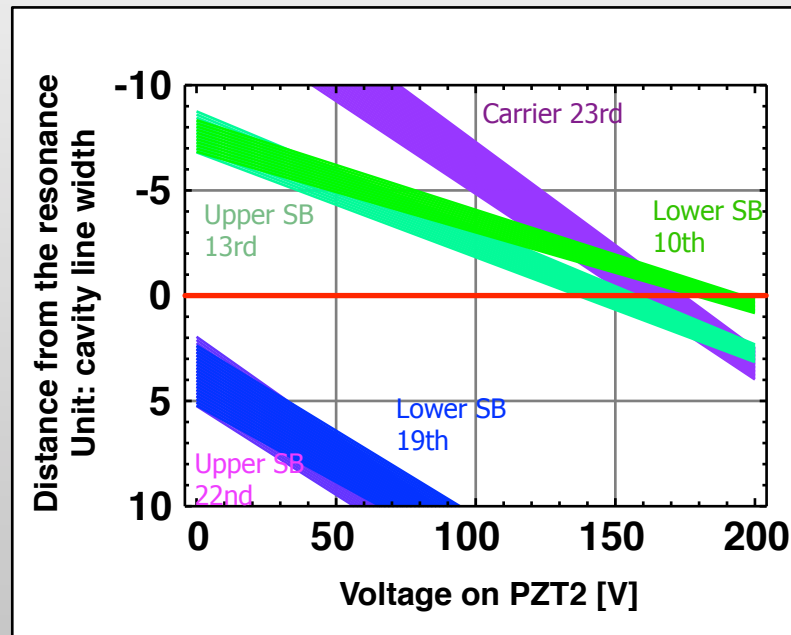
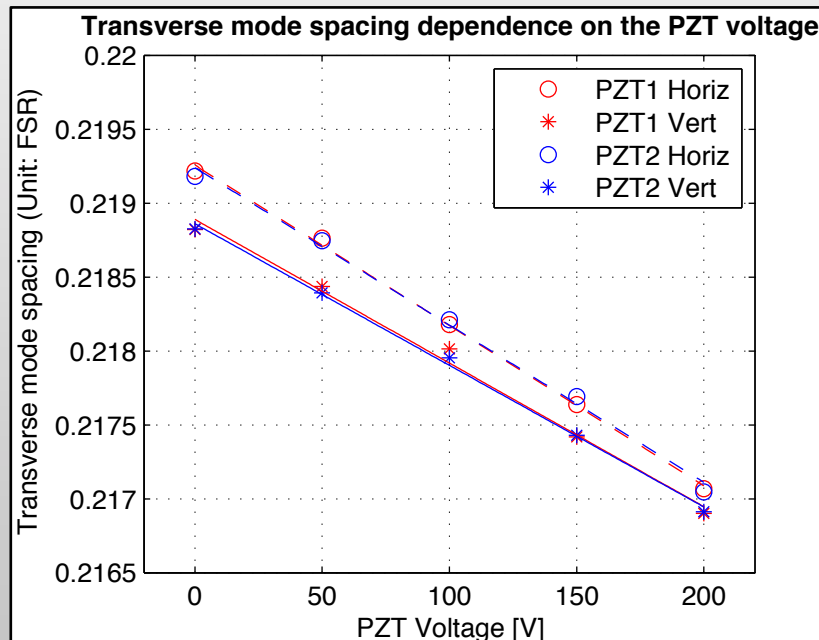
0.2194

TMS depend on the PZT voltage

- 3D deformation of the ring PZT?

Pitch TMS/FSR: $0.2189 - 9.7 \times 10^{-6} V_{PZT1} - 9.6 \times 10^{-6} V_{PZT2}$

Yaw TMS/FSR: $0.2192 - 10.8 \times 10^{-6} V_{PZT1} - 10.6 \times 10^{-6} V_{PZT2}$



The HOMs comes into the resonance at PZT voltage of $\sim 150V$.

This actually does not happen as we limit the PZT voltage to 100V because of some other reason

PZT response

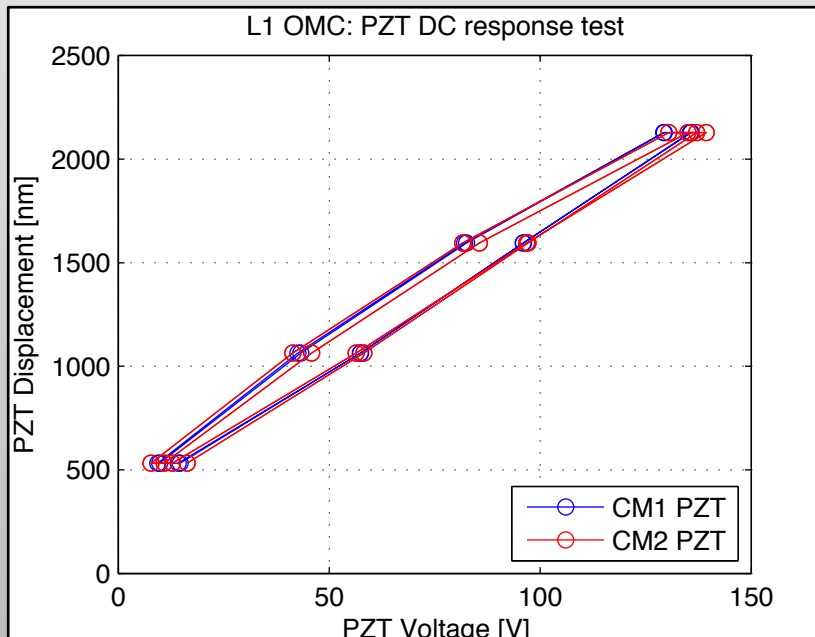
The DC response: checked with free running fringes

The AC response: measured with the cavity locked

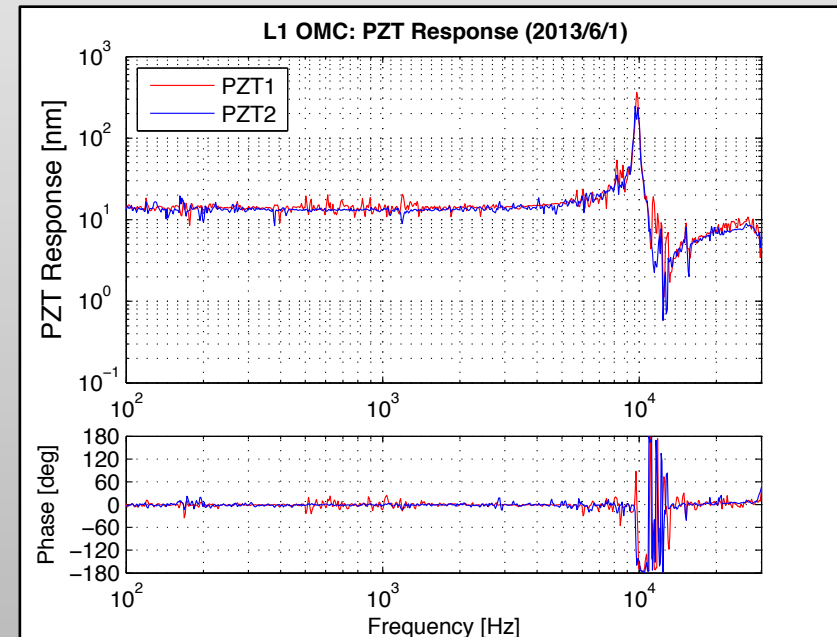
PZT1 response@DC: 13.24 ± 0.02 nm/V (avg)

PZT2 response@DC: 12.9 ± 0.1 nm/V (avg)

First resonance: 10 kHz



▲ PZT DC scan



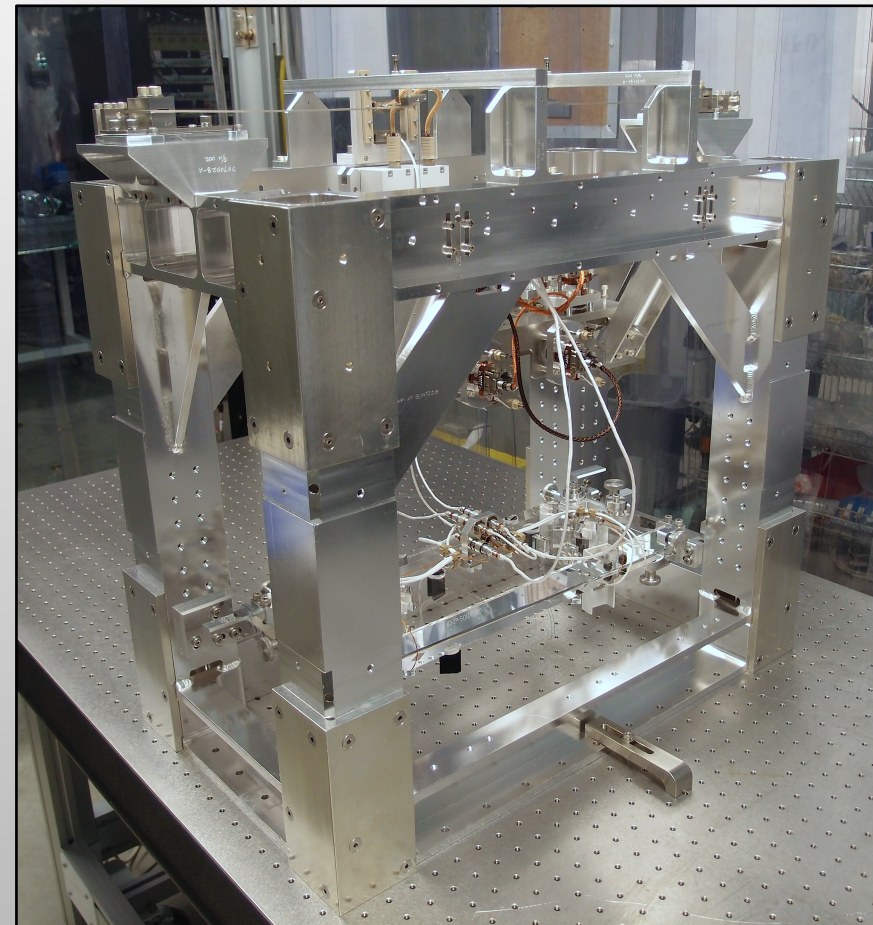
▲ PZT AC response

Integration with the OMC suspension (OMCS)

- OMCS prepared with a metal bench
- Swapped the metal bench with the glass bench at LVEA
- Cabling / Weight balance
- Suspension tests in LVEA
 - transfer functions
 - damping control

Placement on HAM6

- Loading on the ISI
 - a compact lift truck
 - to raise the OMCS
- Suspension tests in HAM6



aLIGO OMC

Designed based on the eLIGO experience and lessons

The first OMC was built

The building procedure was established

Optical testing

Observed the as-designed cavity transmission of $\sim 98\%$

Total thruput (for the carrier TEM00): $\sim 90\%$

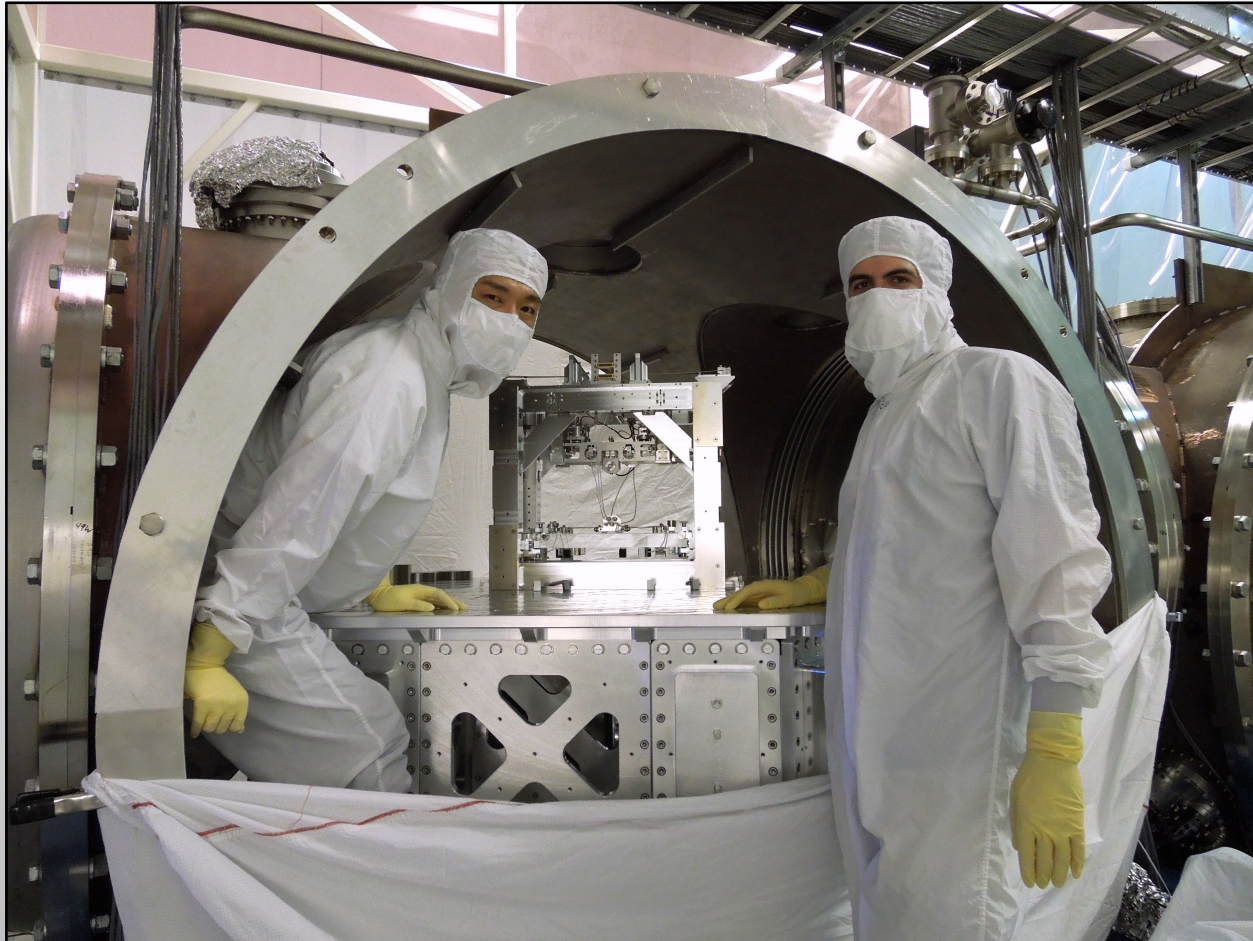
Confirmed that avoidance of the low-order HOMs

Found that the TMS is dependent on the PZT voltages.

Installed on LLO HAM6 in Jun 2013

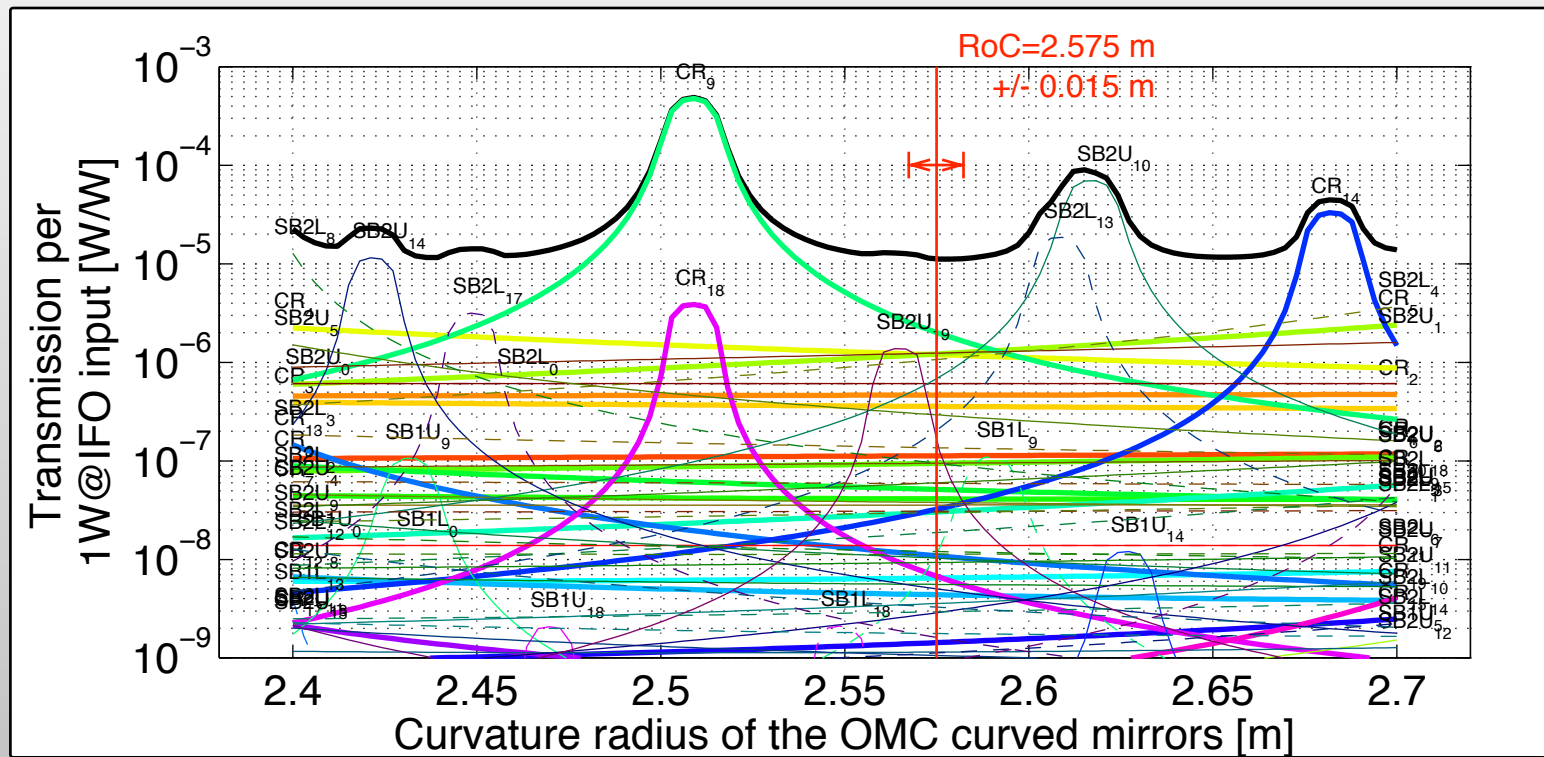
Now in commission at the LLO site!

Thank you for your attention!



Estimated filtering performance

- Mirror RoC tolerance: $R=2.575 \pm 0.015$ [m]



CRn - carrier n-th mode, SB(1,2)(U,L)n - sideband n-th mode,
SB1 - 9MHzSB, SB2 - 45MHz SB, U - upper SB, L - lower SB

Comparison between eLIGO/aLIGO OMCs

cavity design:

semi monolithic same for flexibility of the cavity parameters

breadboard material/cavity design:

ULE fused silica (dT of the order of 0.1K -> just 0.06um)

mirrors

Glued on the back side of
the fused silica prisms Glued on the front side of
the fused silica prisms better access

Actuators

1 PZT + 1 heater Two PZTs (for redundancy)

Suspension

double pendulum
(actively damped) same

Wire clamps

screwed on the breadboard glass wire bracket on the top side