Cryogenic Silicon Fabry-Perot Cavities: Laser Stabilization with sub-Hertz Linewidth



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- Methodology
- Prior progress
- Analysis
- Results

Introduction

Background

- Laser frequency noise
- External reference cavities
- Noise sources:
 - Seismic noise
 - Shot noise
 - Thermal noise
 - Brownian
 - Thermoelastic
 - Thermorefractive

Work with silicon cavity at cryogenic temperatures

Aim

- Reduce Brownian noise:
 - By fluctuation-dissipation theorem^[1]:
- Reduce seismic noise:
 - Require high quality factor Q at low temperature
 - Silicon has Q ~ 10⁸ at around 100K
- Control thermoelastic noise:
 - CTE of Silicon has zeros at 18K & 123K^[2]



[2] P. B. Karlmann, K. J. Klein, P. G. Halverson, R. D. Peters, M. B. Levine et al.

"Linear Thermal Expansion Measurements of Single Crystal Silicon for Validation of Interferometer Based Cryogenic Dilatometer" AIP Conf. Proc. 824, 35 (2006)

Introduction



 $S_{x}(f) = -\frac{4k_{b}T}{\omega}\Im[H(\omega)]$

Introduction

Applications

- Precision of atomic clocks
 - NIST-F1 uncertainty 3×10⁻¹⁶
 - Optical atomic clocks promise O(10⁻¹⁷)
- Gravitational wave observation
 - Thermal noise limiting after standard quantum limit^[4]





[3] NIST "The Advanced LIGO Gravitational Wave Detector"

[4] S. J. Waldman "The Advanced LIGO Gravitational Wave Detector"

Optical system

- Laser PDH locked to reference cavity
- Initially single cavity
 - Use spectrum analyzer for initial result
- Later work possible with two cavities
 - Measure beat frequency to analyse noise



Methodology

Methodology

Thermal system

- Experimental chamber evacuated to 10⁻⁵ torr
- Cavity cooled to 123K
- Use of radiation shields
- Fine temperature control
 - High precision sensors
 - Resistive heaters
 - Temperature controller



Experimental Chamber

Prior progress

Prior progress

- Optical system
 - Tabletop optics in place
- Cryostat
 - Designed
 - Manufactured
 - Pressure tested
- Experimental chamber
 - Parts manufactured
 - Attachments designed
 - Assembly tested





Prior progress

Project aims

- Test cryostat cooldown
 - Prepare cryostat
- Analyse thermal system
 - Propagation of temperature perturbations
 - Effect of heaters
 - Communication with control system

System schematic





Analysis

Analytic approach

Construct differential equations

$$\frac{d}{dt}(C_{1}\theta_{1}) = \alpha_{1}(\theta_{0} - \theta_{1}) + \beta_{1}(\theta_{0}^{4} - \theta_{1}^{4}) + \alpha_{2}(\theta_{2} - \theta_{1}) + \beta_{2}(\theta_{2}^{4} - \theta_{1}^{4}) + P_{1}$$

$$\frac{d}{dt}(C_{2}\theta_{2}) = \alpha_{2}(\theta_{1} - \theta_{2}) + \beta_{2}(\theta_{1}^{4} - \theta_{2}^{4}) + \alpha_{3}(\theta_{3} - \theta_{2}) + \beta_{3}(\theta_{3}^{4} - \theta_{2}^{4}) + P_{3}$$

$$\frac{d}{dt}(C_{3}\theta_{3}) = \alpha_{3}(\theta_{2} - \theta_{3}) + \beta_{3}(\theta_{2}^{4} - \theta_{3}^{4}) + P_{3}$$



Analysis

• Linearise about equilibrium, with $\theta_i = \hat{\theta}_i + \delta_i$, $P_i = \hat{P}_i + \pi_i$

$$\begin{split} \dot{\delta}_{i} &= \frac{1}{\Gamma_{i}} \Big[J_{i-1} \delta_{i-1} - (I_{i} + J_{i}) \delta_{i} + I_{i+1} \delta_{i+1} + \pi_{i} + O(\delta^{2}) \Big] \\ \text{for} \\ I_{i} &= \hat{\alpha}_{i} + a_{i} \Big(\hat{\theta}_{i} - \hat{\theta}_{i-1} \Big) + 4 \hat{\beta}_{i} \hat{\theta}_{i}^{3} + b_{i} \Big(\hat{\theta}_{i}^{4} - \hat{\theta}_{i-1}^{4} \Big) \\ J_{i} &= \hat{\alpha}_{i+1} + a'_{i+1} \Big(\hat{\theta}_{i} - \hat{\theta}_{i+1} \Big) + 4 \hat{\beta}_{i+1} \hat{\theta}_{i}^{3} + b'_{i+1} \Big(\hat{\theta}_{i}^{4} - \hat{\theta}_{i+1}^{4} \Big) \\ \Gamma_{i} &= \hat{C}_{i} + c_{i} \hat{\theta}_{i} \end{split}$$

- Derive small-perturbation transfer functions
- Determine and substitute in parameter values
 - Two methods used

1. Fit D.E.s to cooldown

- Cool cold plate to 77.4K
- Use known heat capacities
- Assume α_i , β_i constant
- Choose values to best fit D.E. solution to data



Analysis

Analysis **2. Fit T.F.s to step responses**

 Analytically-derived transfer functions have form:

$$\frac{\tilde{\delta}_{2}(s)}{\tilde{\delta}_{0}(s)} = \frac{a(s+b)}{(s-\mu_{1})(s-\mu_{2})} = \frac{A}{s-\mu_{1}} + \frac{B}{s-\mu_{2}}$$
$$\frac{\tilde{\delta}_{3}(s)}{\tilde{\delta}_{0}(s)} = \frac{C}{(s-\mu_{1})(s-\mu_{2})} = \frac{C}{s-\mu_{1}} - \frac{C}{s-\mu_{2}}$$

- Step outer shield temperature
- Choose values A, B, C, μ₁, μ₂ to best fit step responses to data



Predictive ability



Error in predictions by method 1.

Error in predictions by method 2.

Results

Results Estimated transfer functions



Poles and zeros

	Cold plate to Outer radiation shield	Outer shield to Inner shield			Outer shield to Dummy cavity		
		1 st method	2 nd method	% diff	1 st method	2 nd method	% diff
Poles:	-2.5×10 ⁻⁵	-1.4×10 ⁻⁵	-1.2×10⁻⁵	14%	-1.4×10 ⁻⁵	-1.2×10 ⁻⁵	14%
	-7.0×10 ⁻⁶	-1.9×10 ⁻⁶	-1.4×10 ⁻⁶	26%	-1.9×10 ⁻⁶	-1.4×10 ⁻⁶	26%
	-1.4×10 ⁻⁶						
Zeros:	-1.4×10 ⁻⁵	-2.5×10 ⁻⁶	-1.6×10 ⁻⁶	36%			
	-1.9×10 ⁻⁶						

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