



# An Overview of Advanced LIGO Interferometry

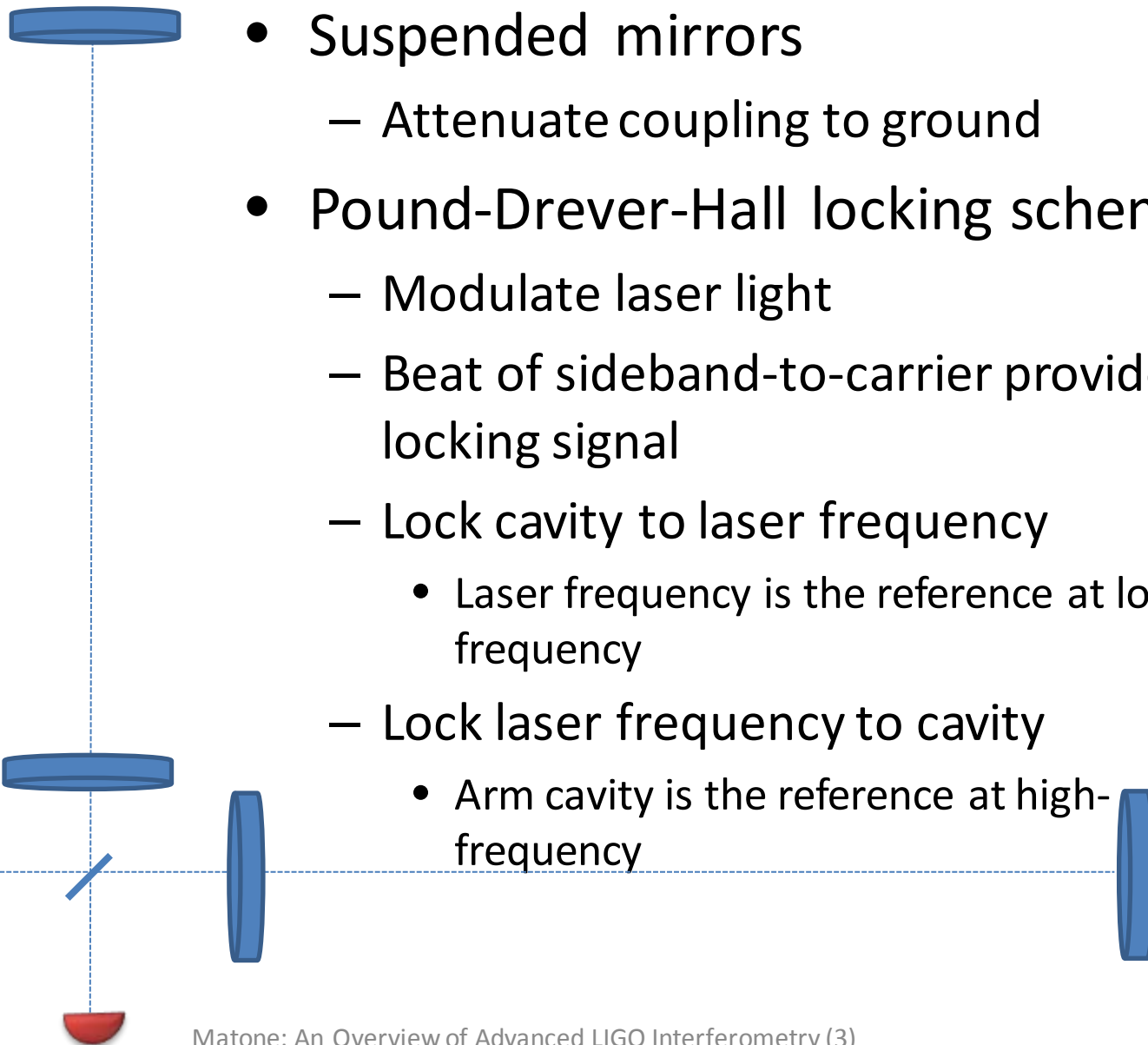
Luca Matone

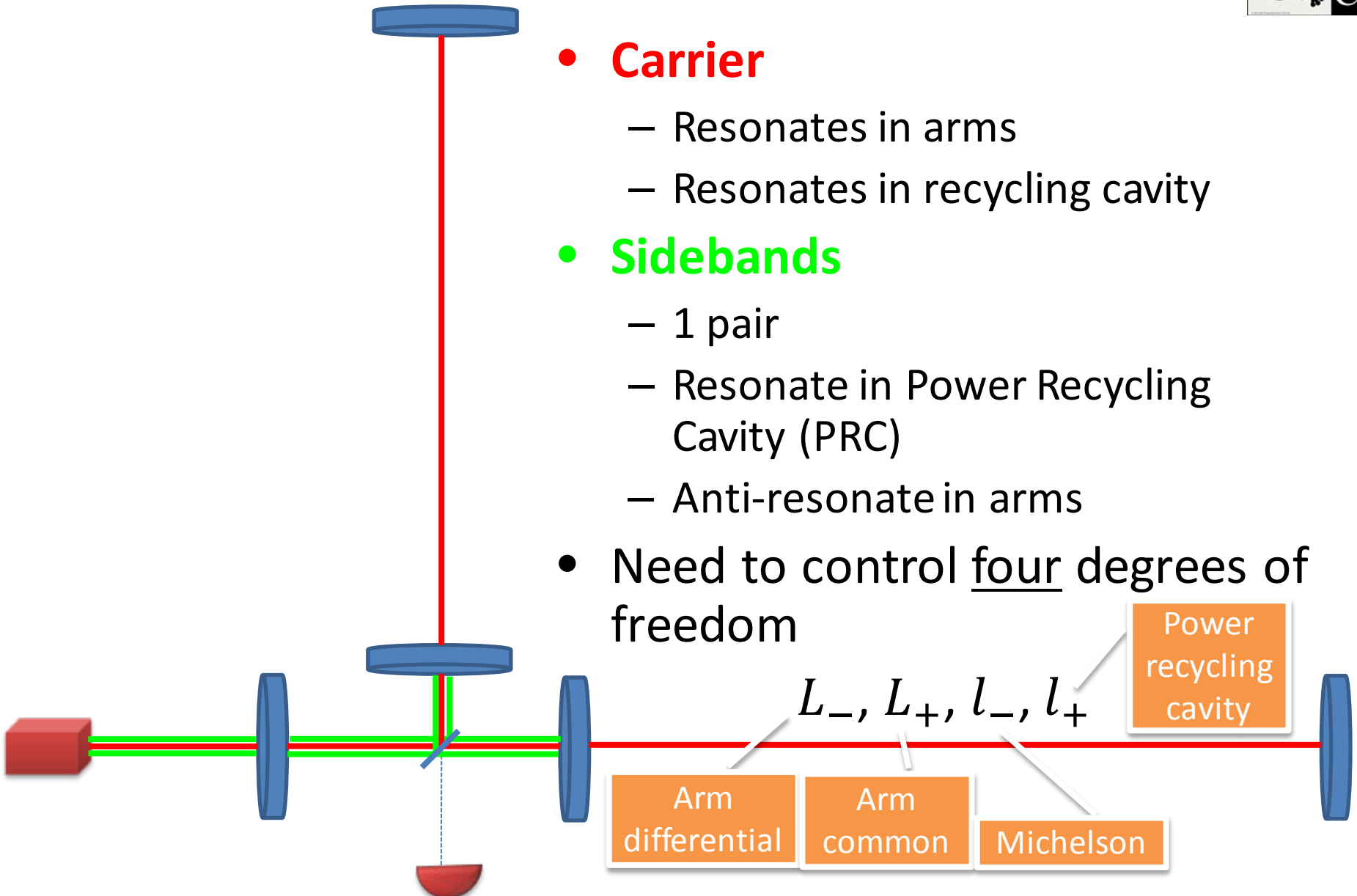
Columbia Experimental Gravity group (GEC Co)

Jul 16-20, 2012

LIGO-G1200743

# So far...





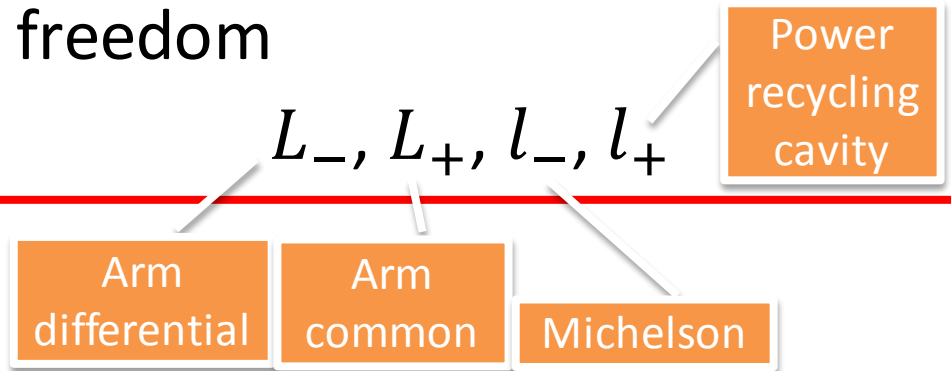
- **Carrier**

- Resonates in arms
- Resonates in recycling cavity

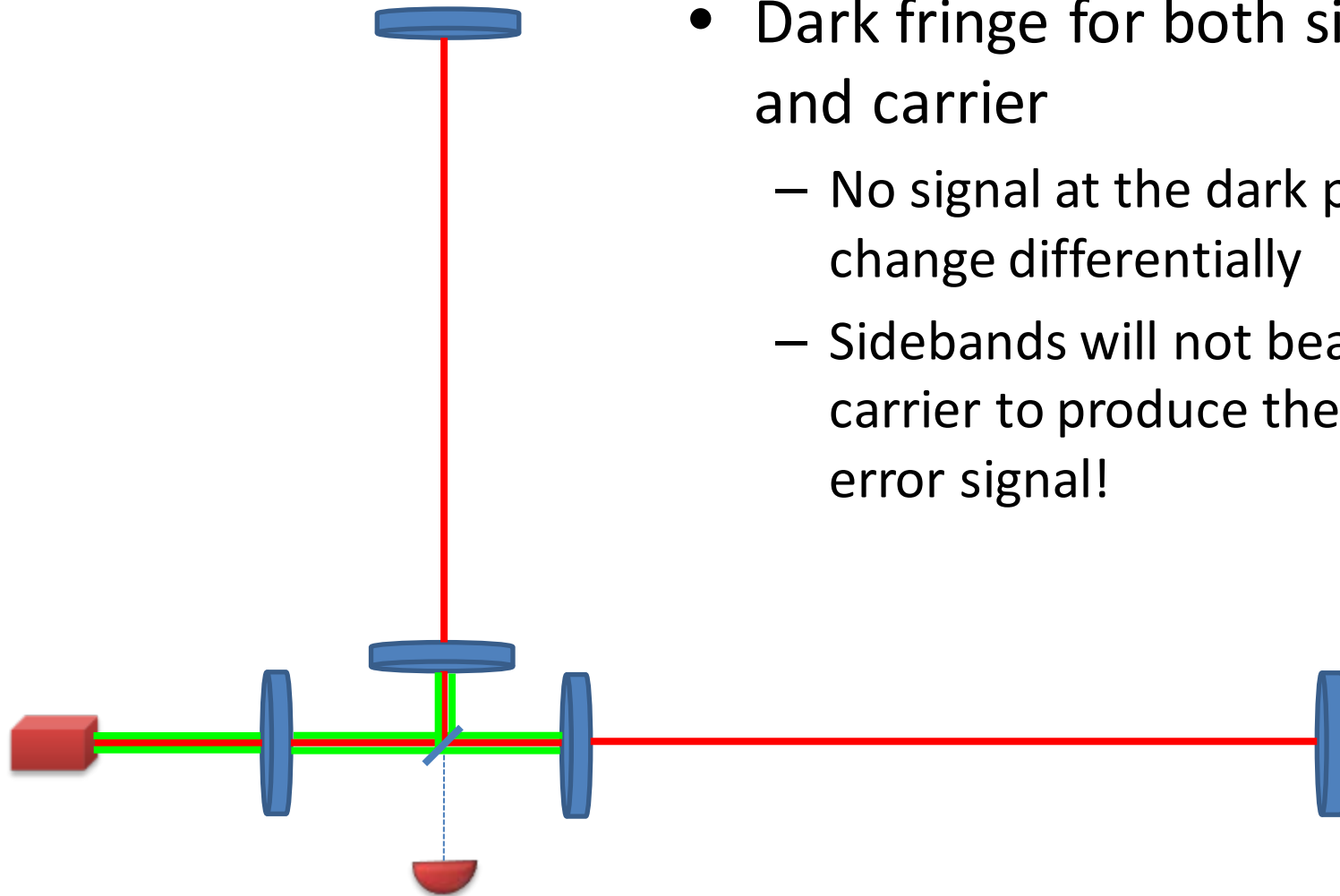
- **Sidebands**

- 1 pair
- Resonate in Power Recycling Cavity (PRC)
- Anti-resonate in arms

- Need to control four degrees of freedom



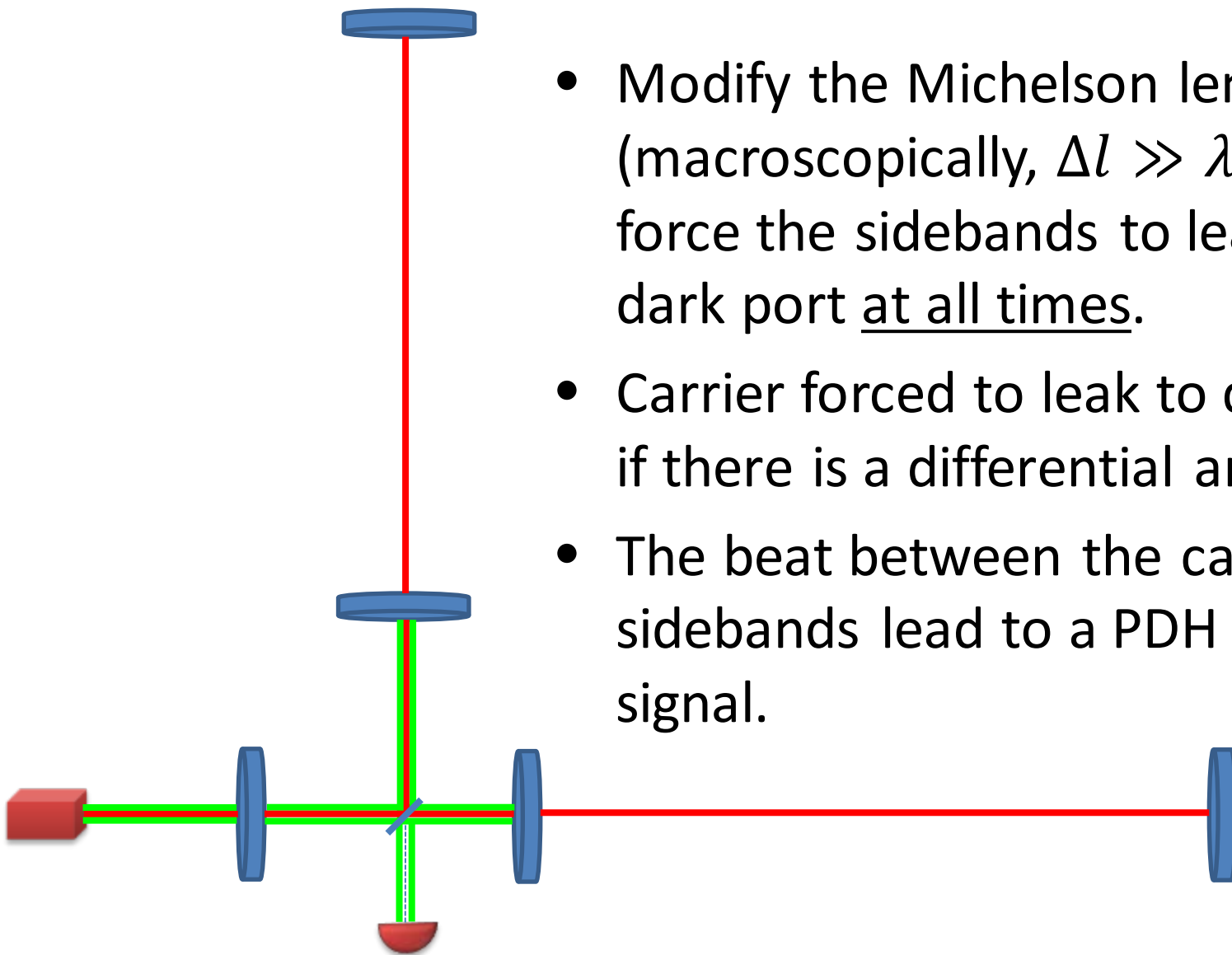
# No signal yet



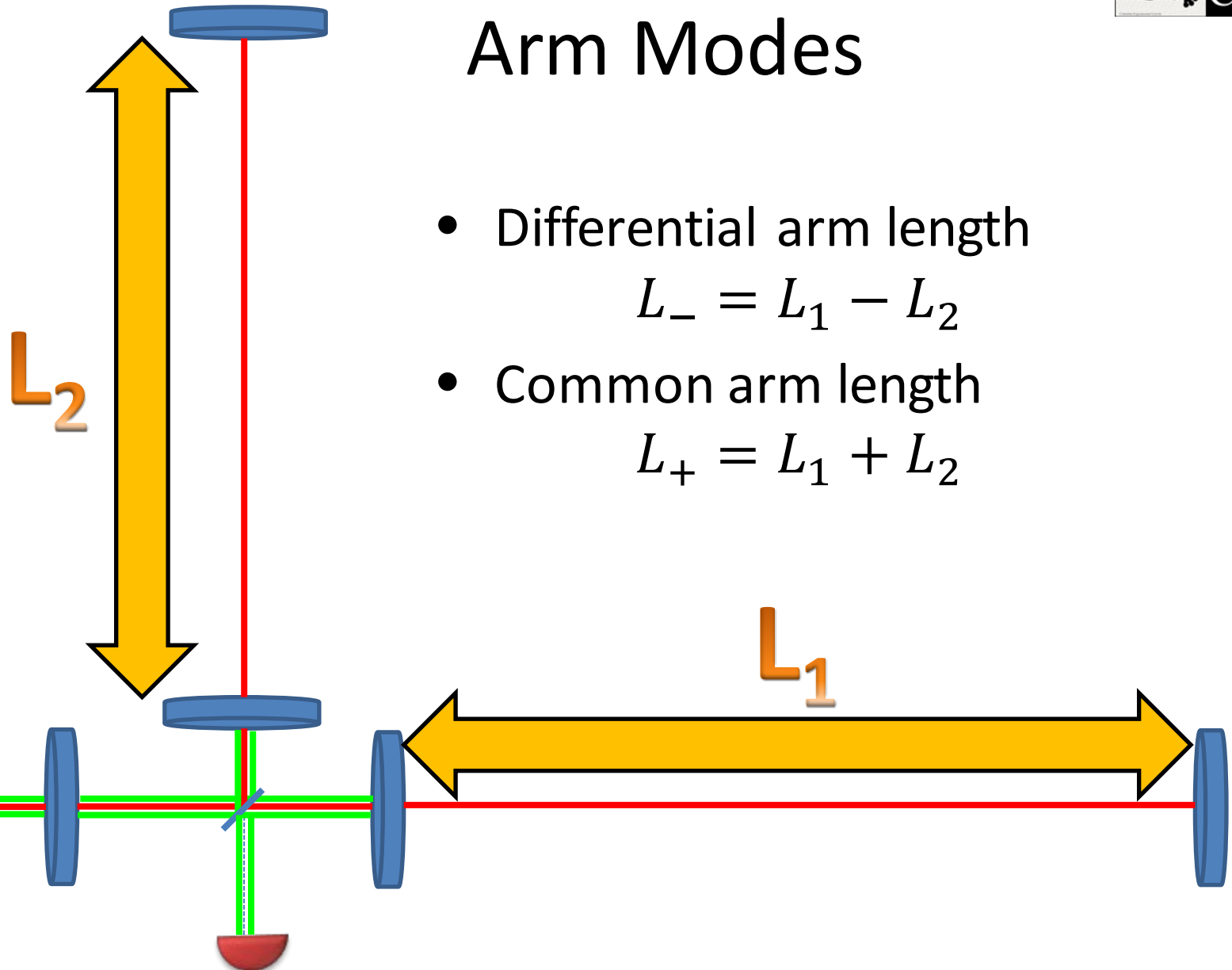
- Dark fringe for both sidebands and carrier
  - No signal at the dark port if arms change differentially
  - Sidebands will not beat against carrier to produce the dark port error signal!

# Schnupp Asymmetry

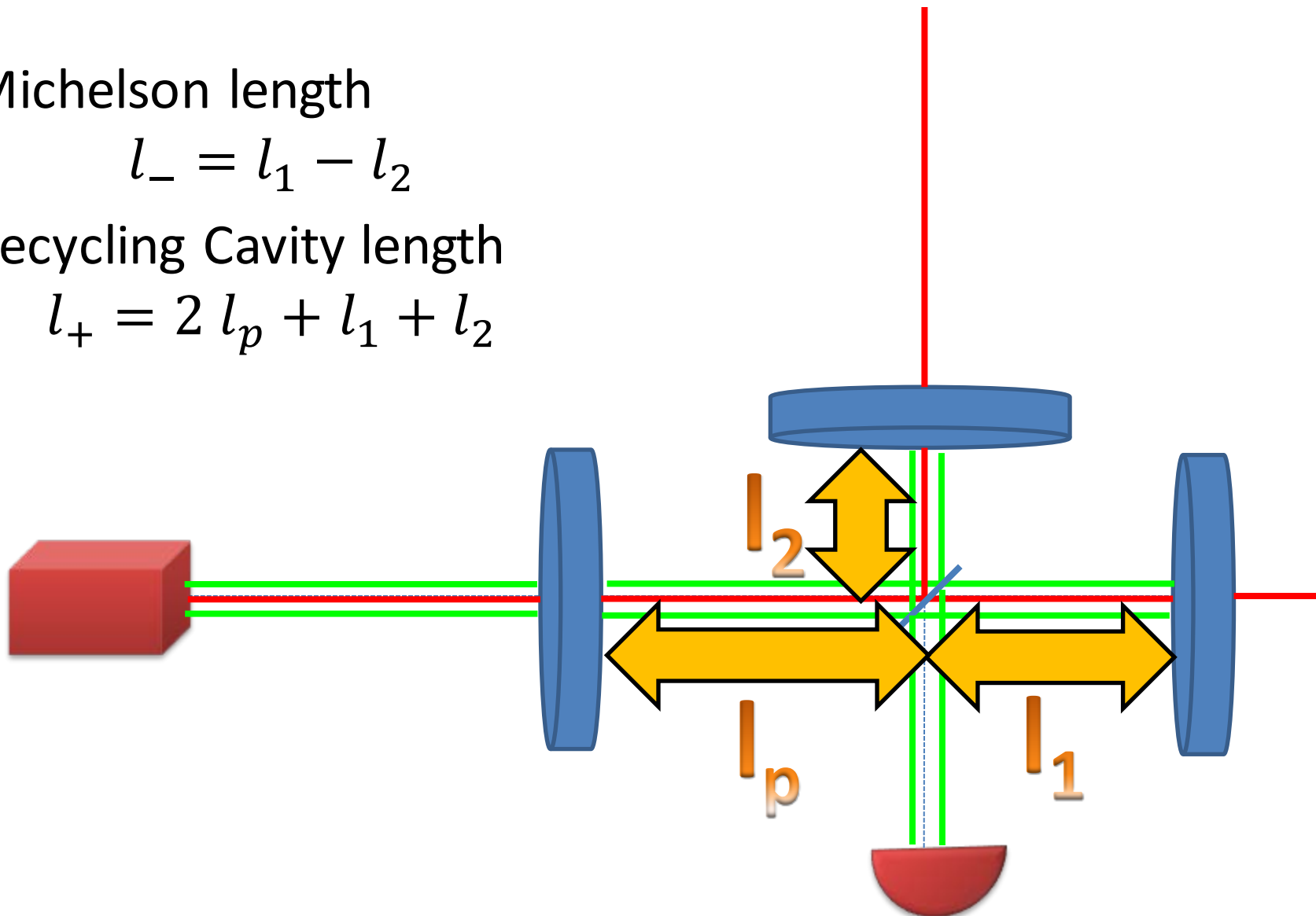
- Modify the Michelson length (macroscopically,  $\Delta l \gg \lambda$ ) so as to force the sidebands to leak to the dark port at all times.
- Carrier forced to leak to dark port if there is a differential arm change
- The beat between the carrier and sidebands lead to a PDH an error signal.



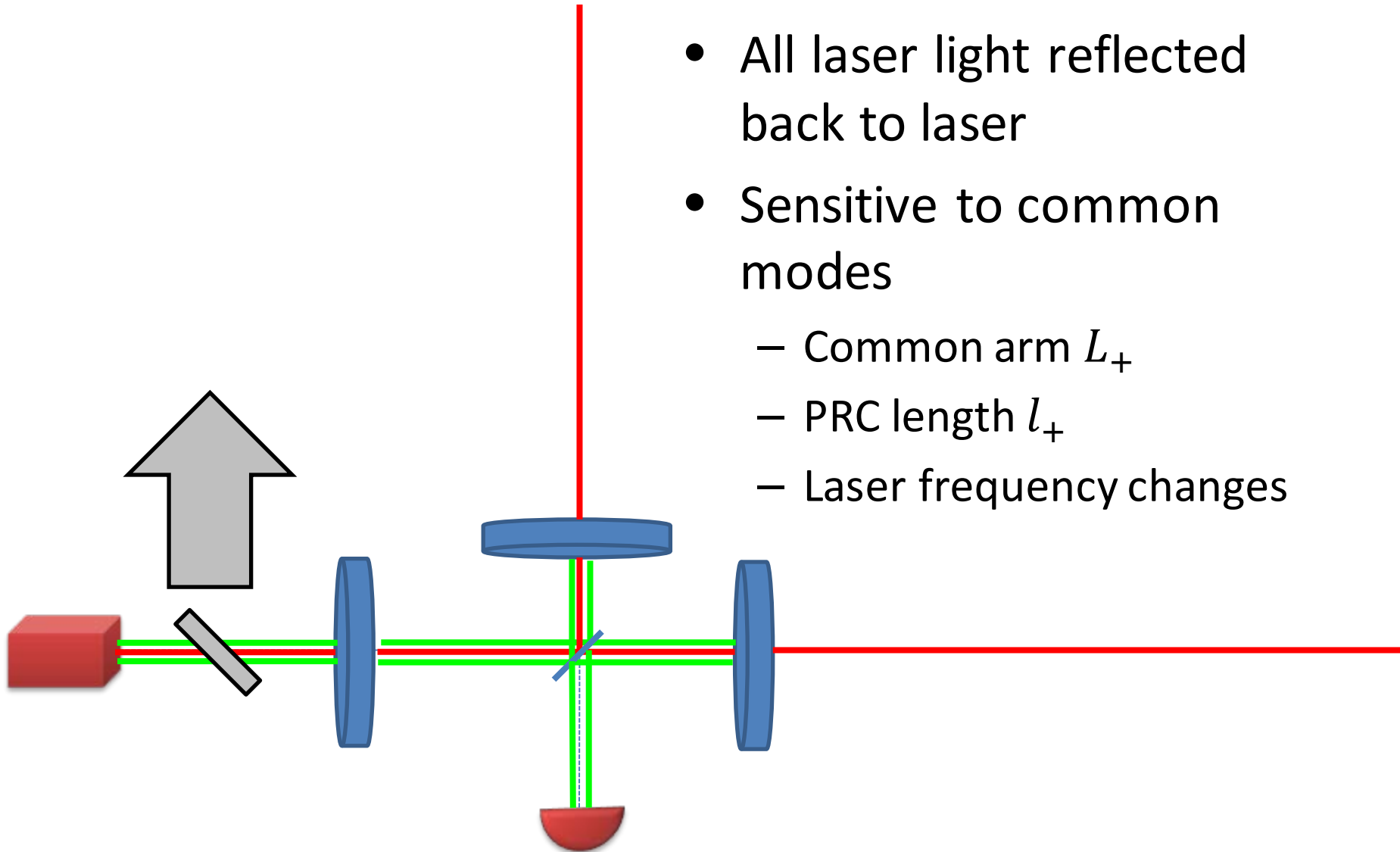
# Common and Differential Arm Modes



- Michelson length
$$l_- = l_1 - l_2$$
- Recycling Cavity length
$$l_+ = 2 l_p + l_1 + l_2$$



# Bright Port (BP)

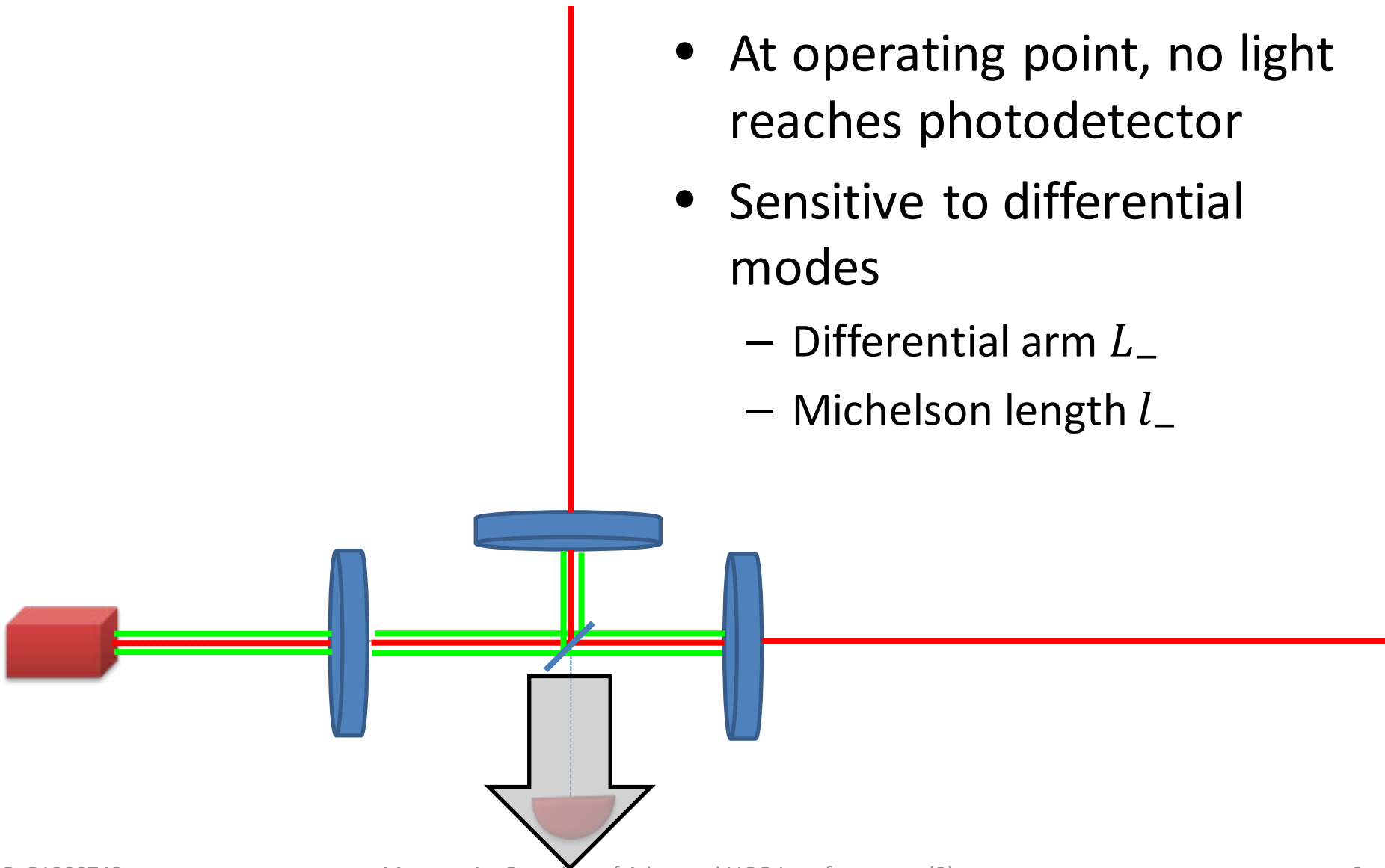


- All laser light reflected back to laser
- Sensitive to common modes
  - Common arm  $L_+$
  - PRC length  $l_+$
  - Laser frequency changes



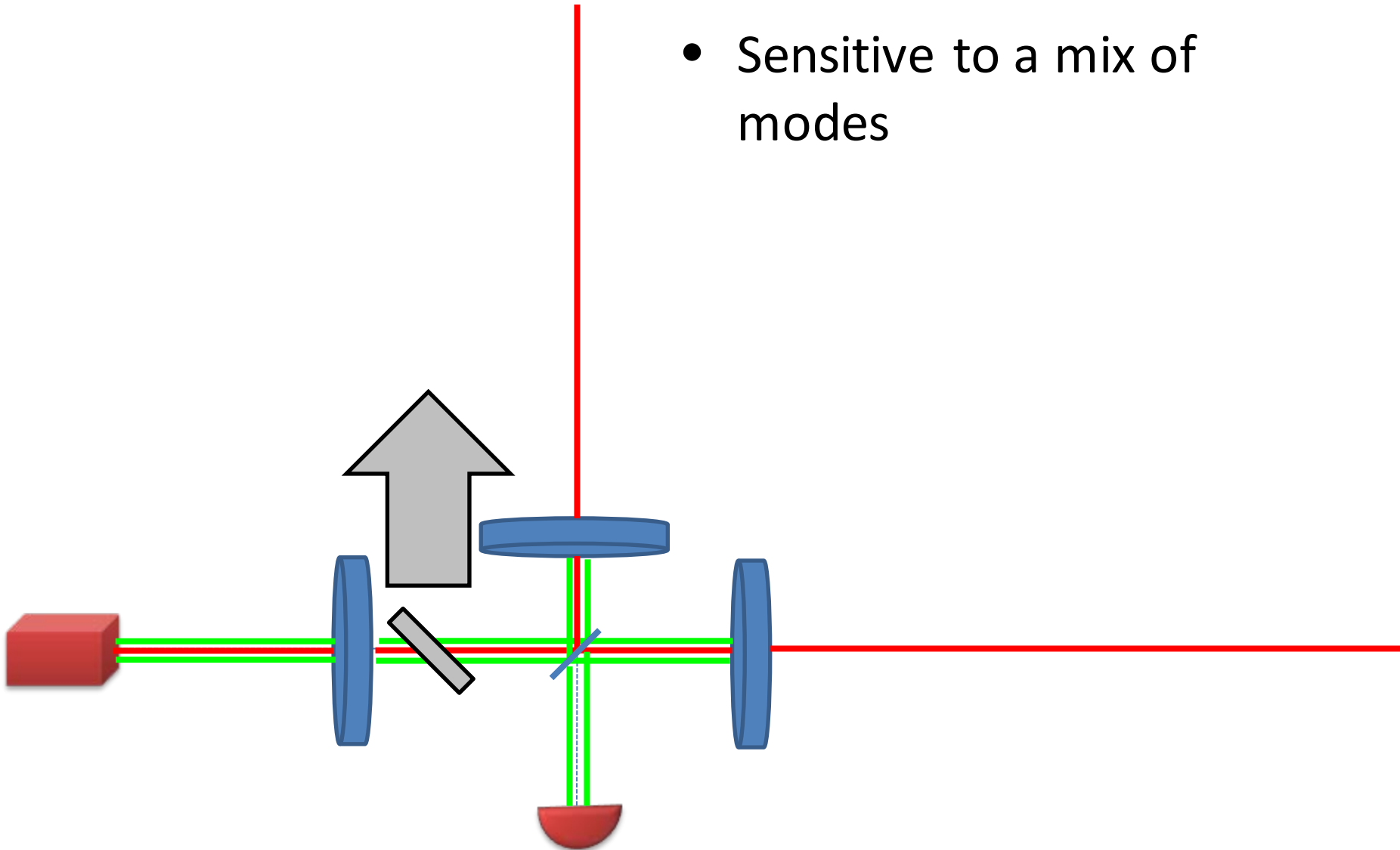
# Dark Port (DP)

- At operating point, no light reaches photodetector
- Sensitive to differential modes
  - Differential arm  $L_-$
  - Michelson length  $l_-$



# Pick-off (PO)

- Sensitive to a mix of modes



# Sensing Matrix

Pick off, Quadrature

Pick off, Inphase

Bright Port, Inphase

Dark Port, Quadrature

	$dS_{AQ}$ (Volts)	$dS_{PQ}$ (Volts)	$dS_{PI}$ (Volts)	$dS_{RI}$ (Volts)
$dL_-$ (m)	$\frac{-9.6 \times 10^{11}}{1 + s/\omega_c}$	$4.72 \times 10^5$	0	0
$dl_-$ (m)	$\frac{-7.3 \times 10^9}{1 + s/\omega_c}$	$6.20 \times 10^7$	0	0
$dL_+$ (m)	0	0	$\frac{-7.82 \times 10^{10}}{1 + s/\omega_{cc}}$	$\frac{2.85 \times 10^{12}}{1 + s/\omega_{cc}}$
$dl_+$ (m)	0	0	$\frac{-3.14 \times 10^8 (1 - s/\omega_p)}{1 + s/\omega_{cc}}$	$\frac{-2.95 \times 10^{10} (1 + s/\omega_r)}{1 + s/\omega_{cc}}$
$dv_l$ (Hz)	$\frac{4.54 \times 10^{-12}}{1 + s/\omega_c}$	0	$\frac{1.11}{1 + s/\omega_{cc}}$	$\frac{82.8}{1 + s/\omega_{cc}}$

Non-diagonal

Laser frequency

**Table 8: Interferometer Optical Plant**

From the "Length Sensing and Control Subsystem Preliminary Design" T970122

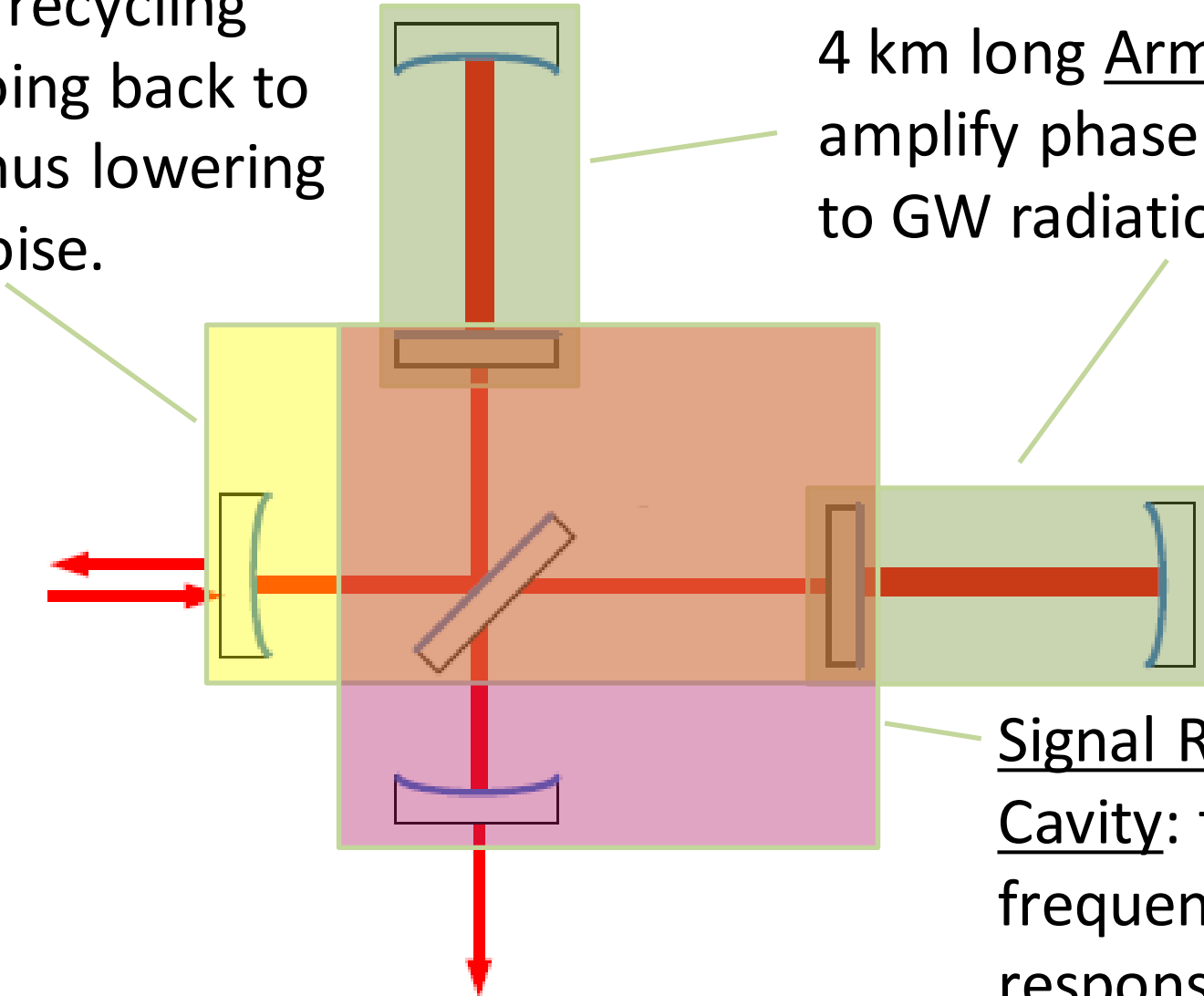
# Advanced LIGO Optical Configuration

Power Recycling

Cavity: recycling light going back to laser thus lowering shot-noise.

## Configuration

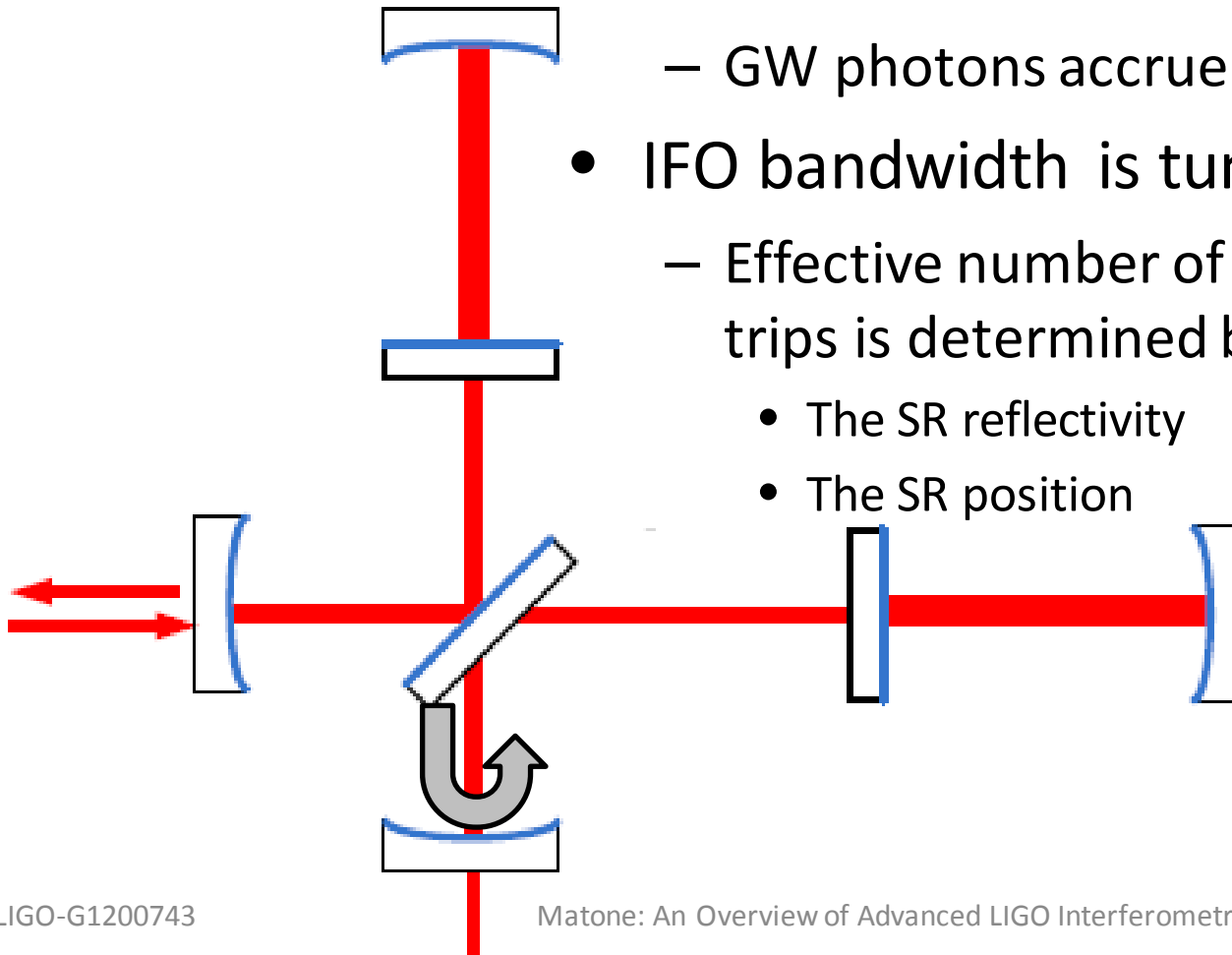
4 km long Arm Cavities: amplify phase shift due to GW radiation



Signal Recycling Cavity: tunes frequency response of IFO

# Resonant Sideband Extraction (RSE)

- Signal Recycling (SR) Mirror
  - Light due to differential change is sent back to IFO
  - GW photons accrue more phase
- IFO bandwidth is tunable
  - Effective number of (GW) photon round trips is determined by
    - The SR reflectivity
    - The SR position





# AdvLIGO Length Sensing and Control (LSC) Requirements



1. Bring the Advanced LIGO IFO to the desired operating point
2. Hold the IFO at the operating point
3. Provide GW signal

From "The AdvLIGO Length Sensing and Control  
Final Design" T1000298

# Degrees of Freedom to Sense and Control

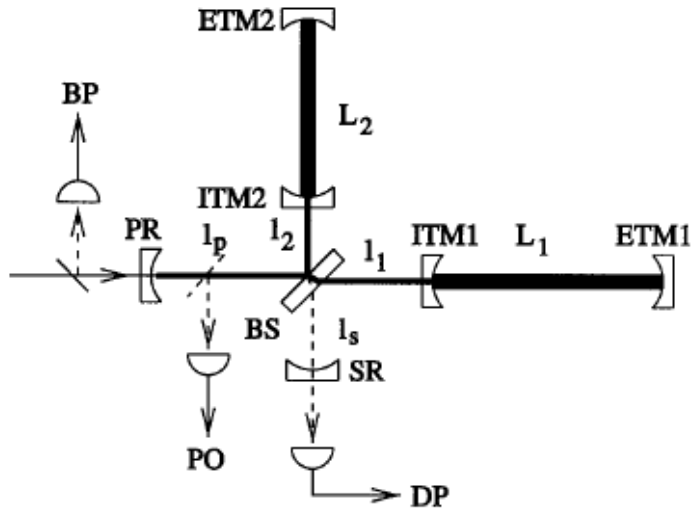


Table 1. Five Relevant Longitudinal Degrees of Freedom in an Advanced LIGO Interferometer<sup>a</sup>

Description	Symbol	Physical Distance
Differential arm cavity	$\Phi_-$	$2k(L_1 - L_2)$
Common arm cavity	$\Phi_+$	$2k(L_1 + L_2)$
Differential Michelson	$\phi_-$	$k(l_1 - l_2)$
Power-recycling cavity	$\phi_+$	$k(2l_p + l_1 + l_2)$
Signal-recycling cavity	$\phi_s$	$k(2l_s + l_1 + l_2)$

<sup>a</sup>It is convenient to describe the two arm cavities by use of their average or common length and their length difference or differential length instead of the individual lengths. The  $k = 2\pi/\lambda$  is the wave number. Note that the phases given under the symbol column correspond to microscopic changes of the macroscopic lengths given in the physical distance column.

## Five degrees of freedom

Fig. 4. Advanced LIGO interferometer consists of two arm cavities formed between the mirrors ITM1(2) and ETM1(2) of length  $L_1$  and  $L_2$ . The distances of the arm cavities from the beam splitter (BS) are  $l_1$  and  $l_2$ . The power-recycling (PR) mirror at a distance  $l_p$  in front of the beam splitter and the signal-recycling (SR) mirror at  $l_s$  behind the beam splitter complete the interferometer. The lengths  $L_i$  of the arm cavities are approximately 4000 m whereas the other distances are of the order of a few meters. These distances depend on the final length-sensing scheme and have to match the used modulation frequencies. Note that it is important to distinguish these macroscopic mirror spacings from the microscopic quantities that determine the phase of the light at reflection from the optics. Microscopic displacements are described by their effect on the phase of the light fields. BP, bright port; DP, dark port; PO, pickoff.

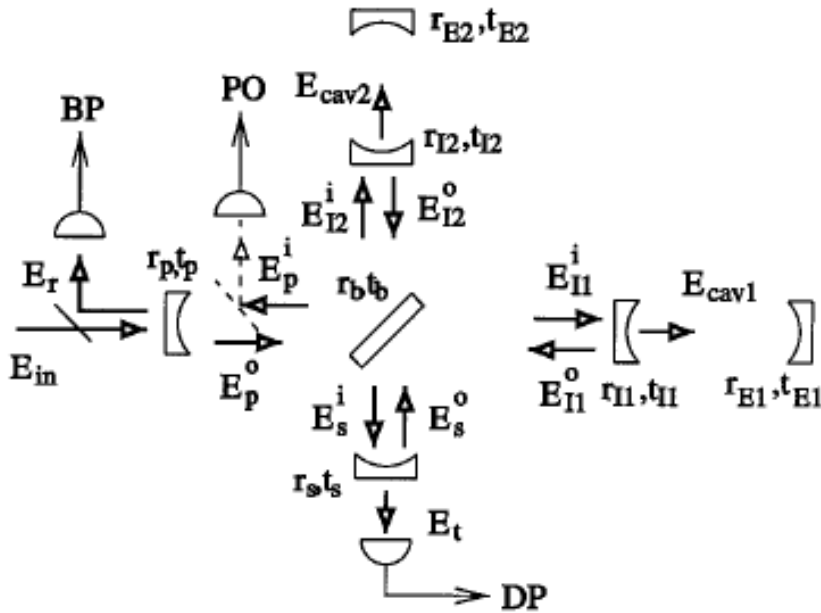


Fig. 5. Fields at the different locations in the interferometer.  $E_r$  is the field that is reflected at the power-recycling mirror outside of the interferometer. It will be detected at the bright port (BP).  $E_t$  is the field that is transmitted through the whole interferometer. It will be detected at the dark port (DP). The subscript  $n$  of all the other fields  $E_n^m$  denotes the mirror at which the field is calculated. The superscript  $m$  denotes the direction of the field. The pickoff (PO) field is proportional to  $E_p^o$ .

$$\begin{aligned}
 E_r &= t_p E_p^i + r_p E_{in}, \\
 E_t &= t_s E_s^i, \\
 E_p^o &= -r_p E_p^i + t_p E_{in}, \\
 E_p^i &= r_b E_{I2}^o \exp[-ik(l_p + l_2)] + t_b E_{I1}^o \\
 &\quad \times \exp[-ik(l_p + l_1)], \\
 E_s^o &= r_s E_s^i, \\
 E_s^i &= -r_b E_{I1}^o \exp[-ik(l_s + l_1)] + t_b E_{I2}^o \\
 &\quad \times \exp[-ik(l_s + l_2)], \\
 E_{I1}^i &= -r_b E_s^o \exp[-ik(l_s + l_1)] + t_b E_p^o \\
 &\quad \times \exp[-ik(l_p + l_1)], \\
 E_{I1}^o &= r_{cav1}(k) E_{I1}^i, \\
 E_{I2}^i &= r_b E_p^o \exp[-ik(l_p + l_2)] + t_b E_s^o \\
 &\quad \times \exp[-ik(l_s + l_2)], \\
 E_{I2}^o &= r_{cav2}(k) E_{I2}^i.
 \end{aligned}$$



# EM fields including sidebands

$$\begin{aligned}
 E_{\text{in}} &= E_0 \exp[i(\omega_0 t + m \sin \Omega t)] \\
 &\approx E_0 \left\{ \exp(i\omega_0 t) + \frac{m}{2} \exp[i(\omega_0 + \Omega)t] \right. \\
 &\quad \left. - \frac{m}{2} \exp[i(\omega_0 - \Omega)t] \right\}, \tag{1}
 \end{aligned}$$

IFO Transfer Function for the carrier

Sideband amplitude (previously  $J_1$ )

$$\begin{aligned}
 E_{\text{out}} &= E_0 \left\{ T_0 \exp(i\omega_0 t) + \frac{m}{2} T_+ \exp[i(\omega_0 + \Omega)t] \right. \\
 &\quad \left. - \frac{m}{2} T_- \exp[i(\omega_0 - \Omega)t] \right\}, \tag{2}
 \end{aligned}$$



# Photocurrents

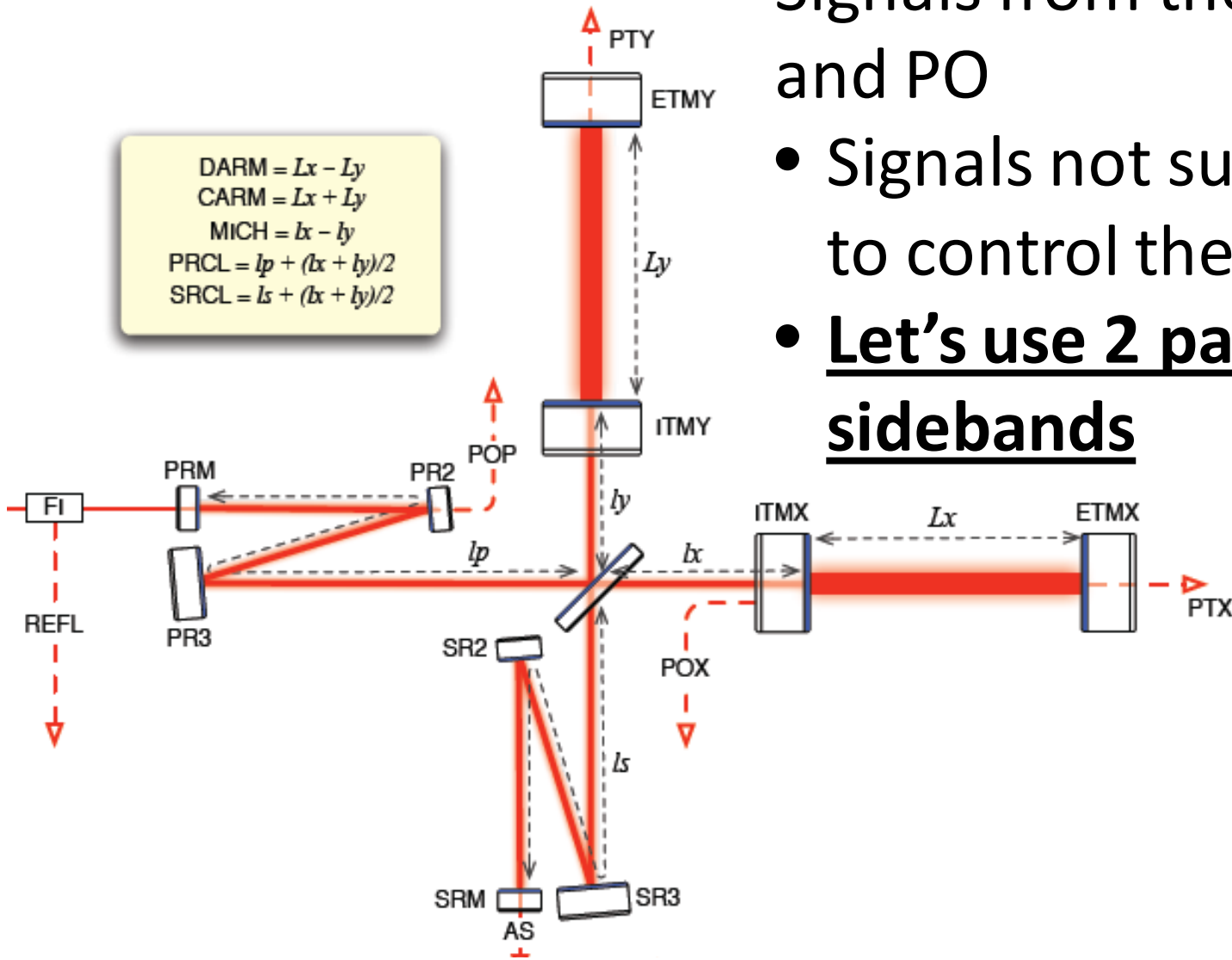
$$I \propto |E_0|^2 + 2m|E_0|^2 \{ \mathcal{R}[T_0(T_+^* - T_-^*)] \cos(\Omega t) + \mathcal{F}[T_0(T_+^* + T_-^*)] \sin(\Omega t) \}, \quad (4)$$

Quadrature

**PDH error signal**

$$S = \begin{cases} 2\mathcal{R}[T_0(T_+^* - T_-^*)] \cos(\alpha) \\ - 2\mathcal{F}[T_0(T_+^* + T_-^*)] \sin(\alpha), \end{cases} \quad (5)$$

In-phase

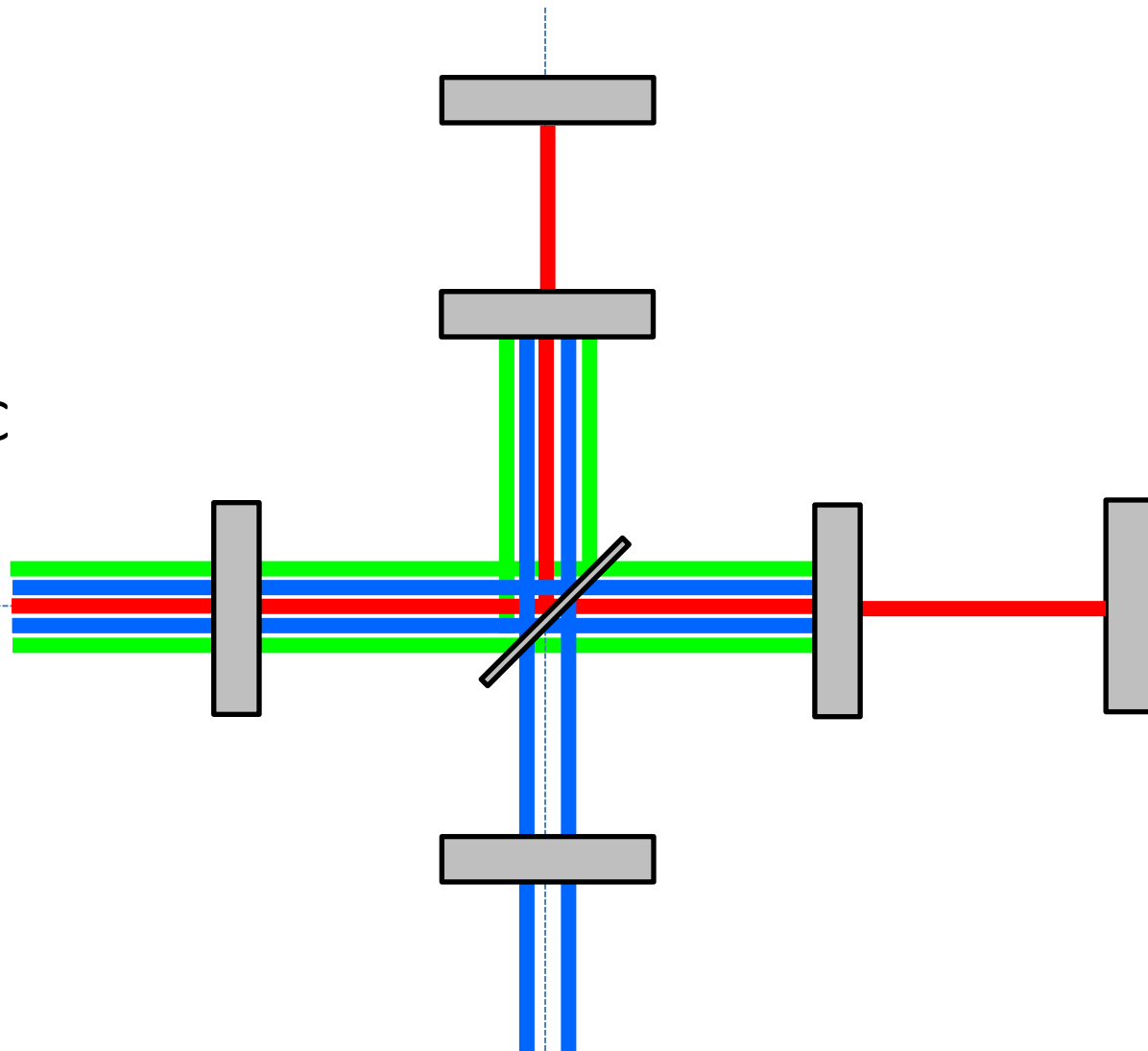


Signals from the BP, DP and PO

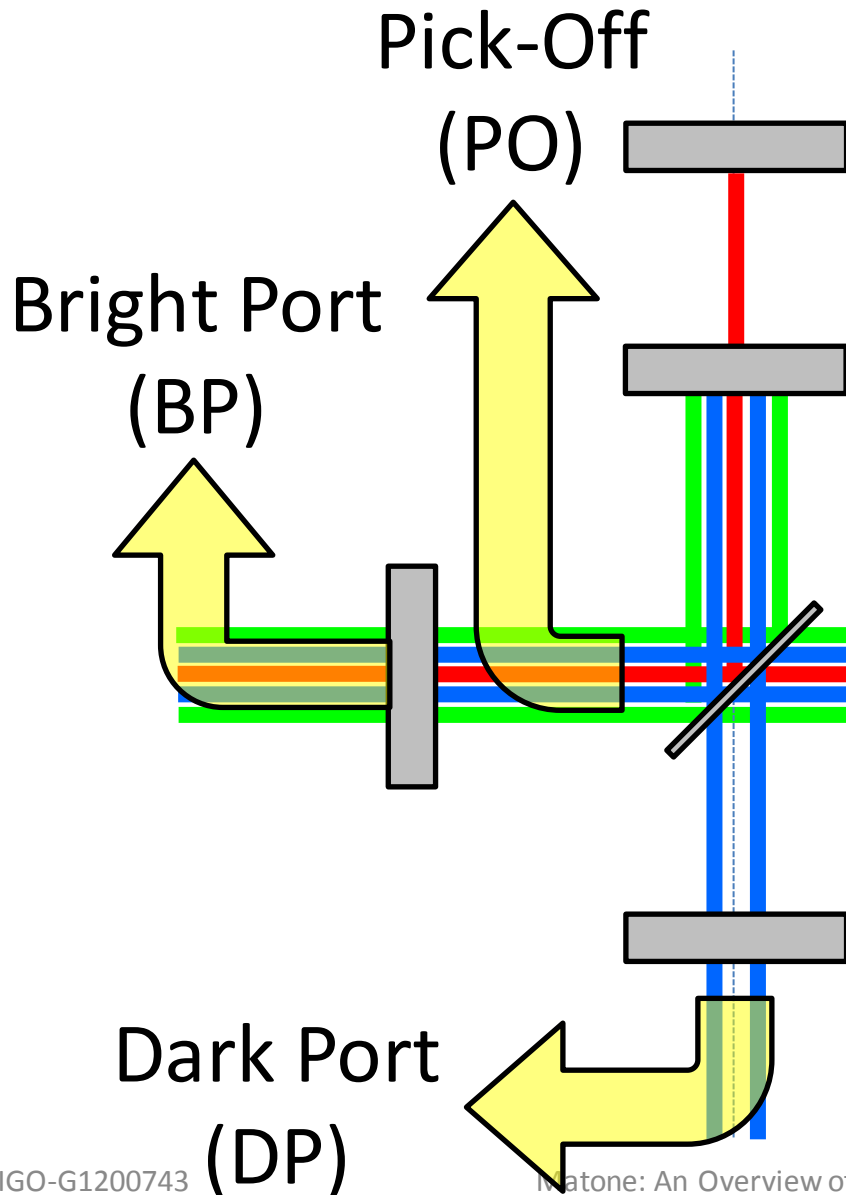
- Signals not sufficient to control the 5 DOF
- **Let's use 2 pairs of sidebands**

# Two Modulation Frequencies (High and Low)

- **Carrier** ———
- **Sideband** ———
  - High frequency ( $f_2 = 45$  MHz)
  - Chosen so as to couple to both PRC and SRC
- **Sideband** ———
  - Low frequency ( $f_1 = 9$  MHz)
  - Chosen so as to couple just to the PRC



# Error Signals



Demodulation and Double-Demodulation at

- $f_1$  (9 MHz)
  - beat of carrier to sideband 1
- $f_2$  (45 MHz)
  - beat of carrier to sideband 2
- $f_1 + f_2$  (54 MHz)
  - beat of sideband 1 to sideband 2
- $f_2 - f_1$  (36 MHz)
  - beat of sideband 1 to sideband 2

## 3.1 Sensing matrix

The following sensing matrices for Science Run 3 are shown in Optickle:

Sensing Matrix in Watts per meter

Port	CARM	DARM	PRCL	MICH	SRCL
REFL I1	<b>9.4e+08</b>	2e+05	7.3e+07	1.1e+06	<b>5.5e+03</b>
AS DC	1.3e+06	<b>4.2e+09</b>	2.8e+05	1.5e+07	7.6e+06
POP I1	3.2e+07	6.7e+03	1.1e+06	1.1e+06	<b>3.1e+02</b>
POP Q2	1.5e+07	2.3e+04	1.1e+06	1.1e+06	<b>3e+04</b>
REFL IM	1.4e+06	<b>2.5e+04</b>	5.5e+03	5.5e+03	<b>2.8e+05</b>

Demodulated at  
 $f_1 = 9 \text{ MHz}$

Demodulated at  
 $f_2 = 45 \text{ MHz}$

Sensing Matrix in Watts per meter

Port	CARM	DARM	PRCL	MICH	SRCL
REFL I1	<b>9.4e+08</b>	1.3e+06	7.3e+07	1.1e+06	<b>1.4e+04</b>
AS DC	3e+06	<b>9.7e+09</b>	2.8e+05	1.5e+07	7e+03
POP I1	3.2e+07	4.4e+03	1.1e+06	1.1e+06	<b>3e+02</b>
POP Q2	8.7e+06	4.2e+04	1.1e+06	1.1e+06	<b>8.8e+04</b>
POP I2	8.7e+06	9e+03	<b>1.8e+06</b>	<b>9.9e+04</b>	<b>3e+05</b>

Demodulated at  
 $f_2 - f_1 = 36 \text{ MHz}$

The contractions used in the port name are: I: I-phase, Q: Q-phase, 1: demodulated at  $f_1$ , 2: demodulated at  $f_2$ , M: demodulated at  $f_2 - f_1$ , P: demodulated at  $f_2 + f_1$ . The main matrix elements are in bold red. The biggest worrisome elements are in blue. The full sensing matrix with all available ports is shown in Figures 20 and 21 of appendix A.

## 3.1 Sensing matrix

Main elements

The following sensing matrices for Science mode 1 and 2 were calculated in Optickle:

Sensing Matrix in Watts per meter at 1 kHz, for Science Mode 2 (NS/NS inspiral)

Port	CARM	DARM	PRCL	MICH	SRCL
REFL I1	<b>9.4e+08</b>	2e+05	7.3e+07	1.1e+06	5.5e+03
AS DC	1.3e+06	<b>4.2e+09</b>	2.8e+05	1.5e+07	7.6e+06
POP I1	3.2e+07	6.7e+03	<b>1.2e+07</b>	6.8e+03	3.1e+02
POP Q2	1.5e+07	2.3e+04	1.4e+06	<b>4.3e+05</b>	3e+04
REFL IM	1.4e+06	2.5e+04	5.1e+06	4.5e+05	<b>2.8e+05</b>

Sensing Matrix in Watts per meter at 1 kHz, for Science Mode 1 (zero detuning)

Port	CARM	DARM	PRCL	MICH	SRCL
REFL I1	<b>9.4e+08</b>	1.3e+05	7.3e+07	1e+06	1.4e+04
AS DC	3e+06	<b>9.7e+09</b>	6.7e+05	3.4e+07	7e+03
POP I1	3.2e+07	4.4e+03	<b>1.2e+07</b>	6.6e+03	3e+02
POP Q2	8.7e+06	4.2e+04	4.6e+05	<b>7.4e+05</b>	8.8e+04
POP I2	8.7e+06	9e+03	1.8e+06	9.9e+04	<b>3e+05</b>

The contractions used in the port name are: I: I-phase, Q: Q-phase, 1: demodulated at  $f_1$ , 2: demodulated at  $f_2$ , M: demodulated at  $f_2 - f_1$ , P: demodulated at  $f_2 + f_1$ . The main matrix elements are in bold red. The biggest worrisome element in the matrix with all available ports is shown in Figures 20 and 21.

Elements off-diagonal

From "AdvLIGO Interferometer Sensing and Control Conceptual Design" T070247 and LSC Final Design T1000298

- Radio Frequency (RF) modulation
  - Heterodyne detection scheme
  - Modulation-demodulation gives rise to the PDH error signal
- Initial LIGO
  - Four DOFs, sensed and controlled by this heterodyne scheme
  - Differential arm motion  $L_+$  measured by the Dark Port quadrature error signal (AS\_Q)
  - Large signal swings found in the Dark Port inphase signal (AS\_I)
    - Due to “junk” light
    - Would saturate the RF electronics



Problem with *heterodyning* at the DP

# Photodetectors

- Large AS\_I signal limits the power on each PD to ~20 mW (leaving some headroom)
- Scaling to the full LIGO-I power of 8W or 50 W in an upgrade would lead to a giant forest of PDs and an associated forest of AS\_I servos, mixers, ADCs, CPUs, etc... **Big headache!**

# of AS port diodes

L1	4	1
H1	8	1
H2	24	1

RF DC

- ✓ DC: No RF electronics!
- ✓ Easy photodetector design. Don't care about diode capacitance: can select based on QE, spatial uniformity (EG&G 5 mm PD?)
- ✓ With the OMC, the  $C_D \sim 5 \times 10^{-6}$
- ✓ 50 W into the MC  
 -> 1800 W on the BS  
 ->  $C_D = 10$  mW!
- ✓ Including the arm offset  $P_{AS} \sim 20$  mW

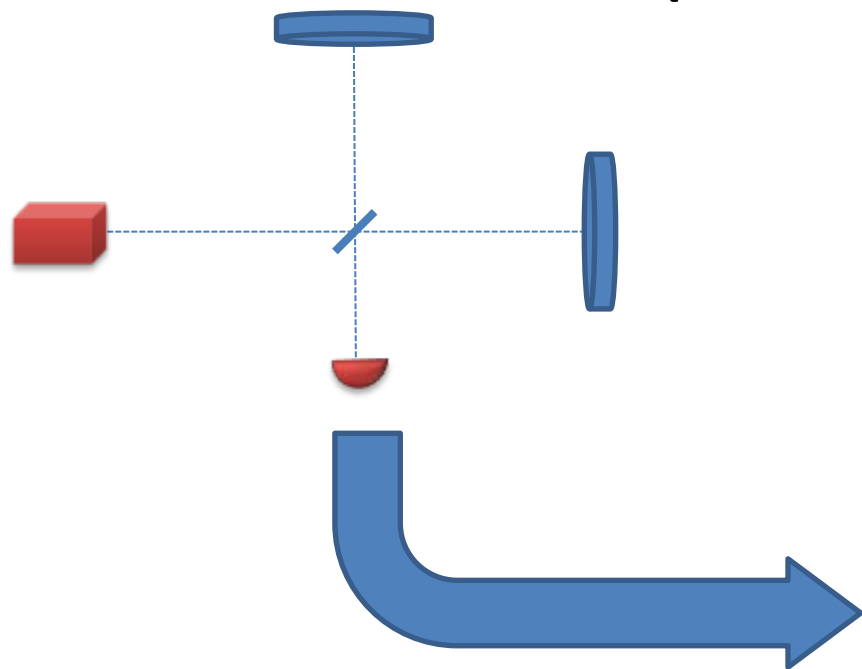
G050091-00-b

DC Readout in 2006

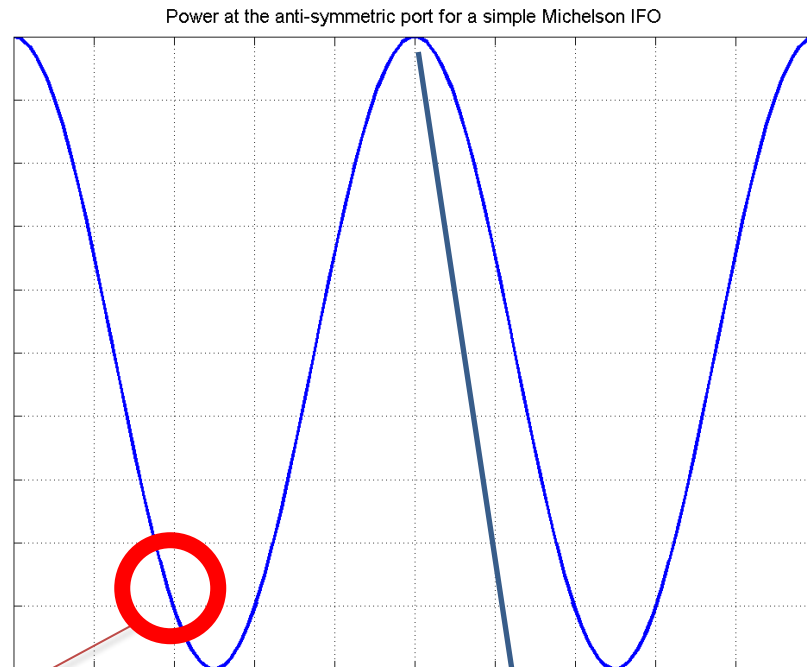
This is Being 40m l

Proposed solution: *homodyne* detection scheme

# Overview of DC Readout (Homodyne)



DC Power [AU]



$L_-$

Bright fringe

Dark fringe

- Introduce (small)  $L_-$  offset
- DC power proportional to  $L_-$
- Advanced LIGO's GW channel

# Expected AdvLIGO sensitivity to GWs

From "AdvLIGO Interferometer Sensing and Control Conceptual Design" T070247

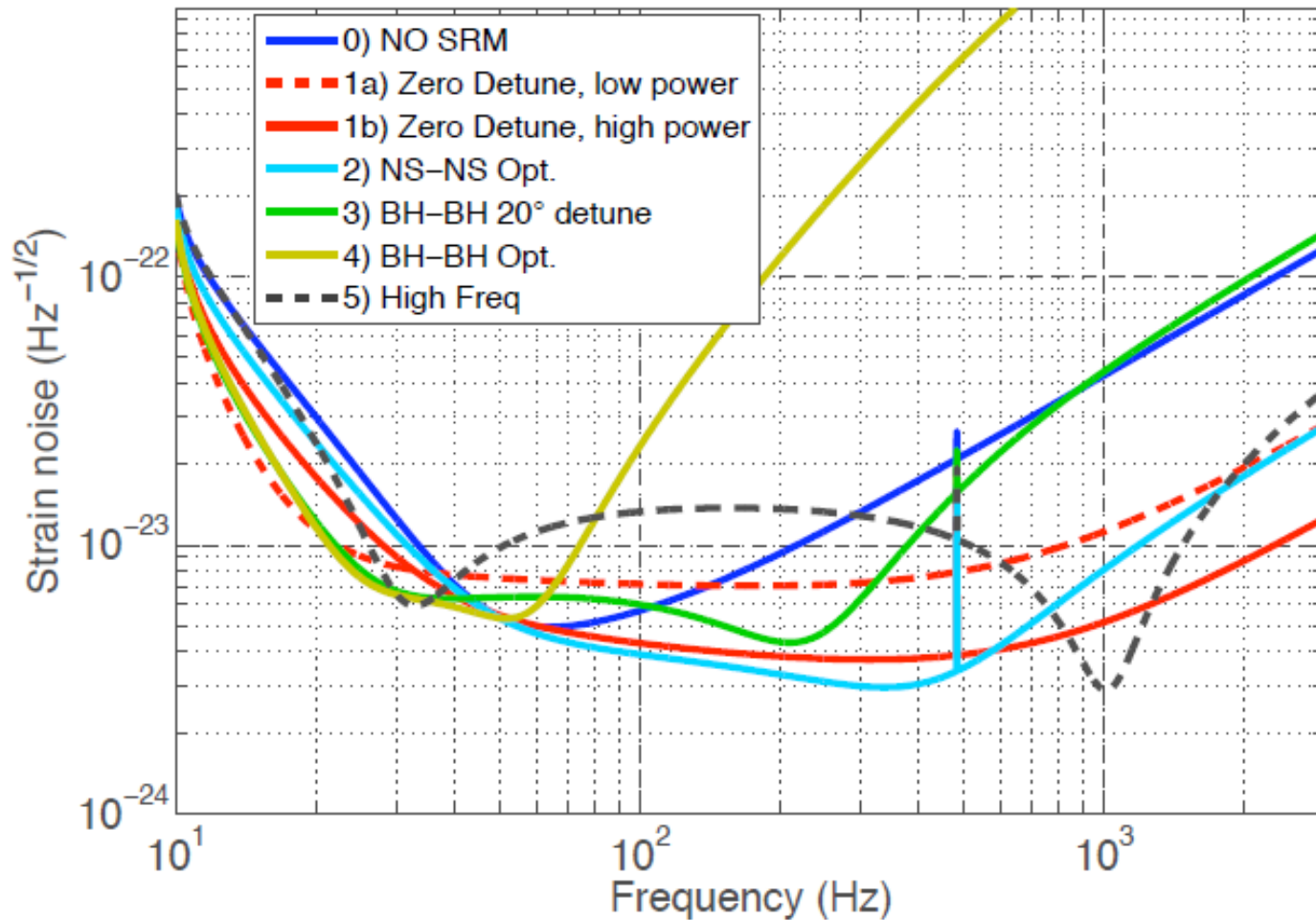

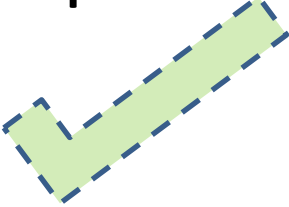


Figure 1: Proposed modes of operation for the Advanced LIGO interferometers. See text for description of the modes.

# So far...

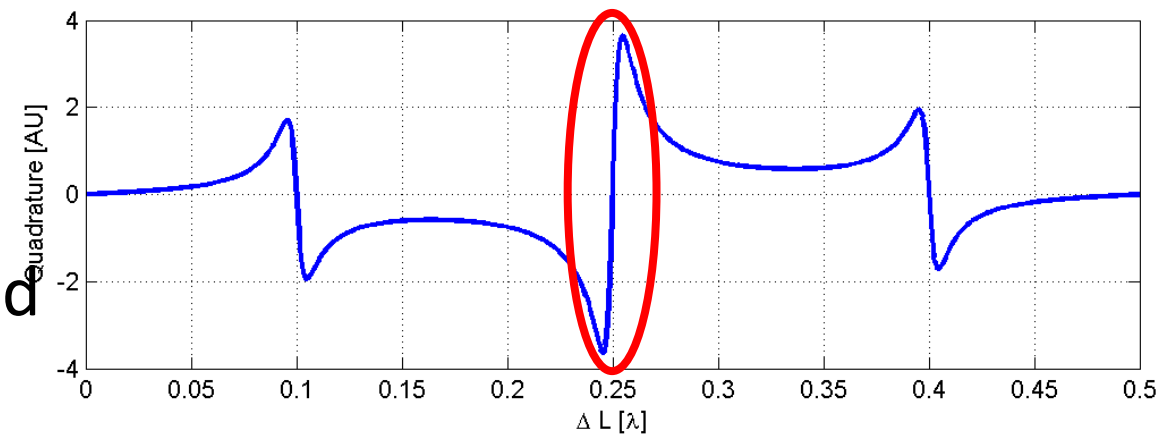
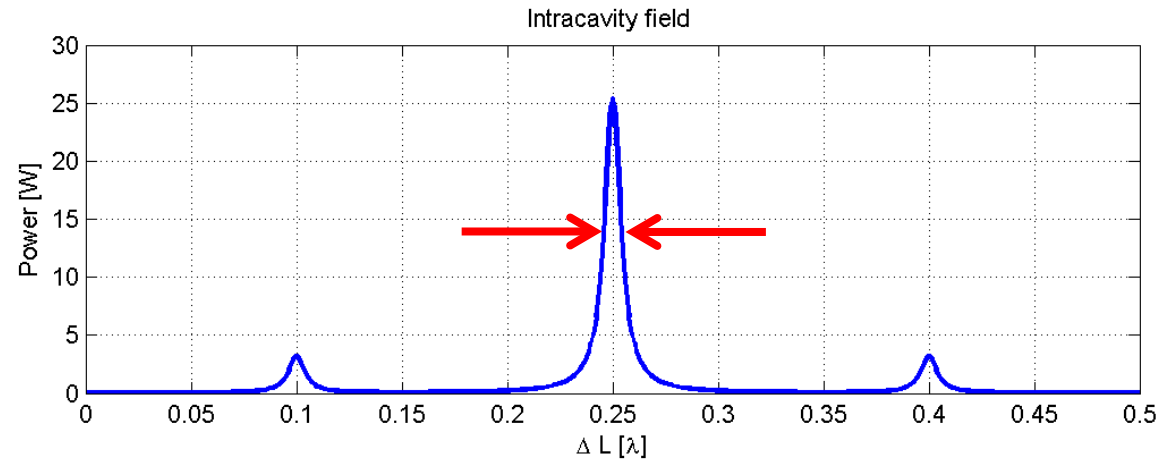
- Advanced LIGO optical configuration
  - Dual-recycling laser interferometer
  - Signal Recycling Cavity
    - Introduces a tunable frequency response
- Longitudinal Degrees of Freedom to Sense and Control
  - From four (initial LIGO) to five
  - Added level of complexity → need two pairs of sidebands
  - Demodulation and Double-Demodulation ( $f_1, f_2, f_1 + f_2, f_2 - f_1$ )
- Non-diagonal sensing matrix
- Homodyne detection scheme
  - Get around heterodyne detection scheme at the DP
  - Requires to lock at small  $L_-$  offset

# AdvLIGO Length Sensing and Control (LSC) Requirements

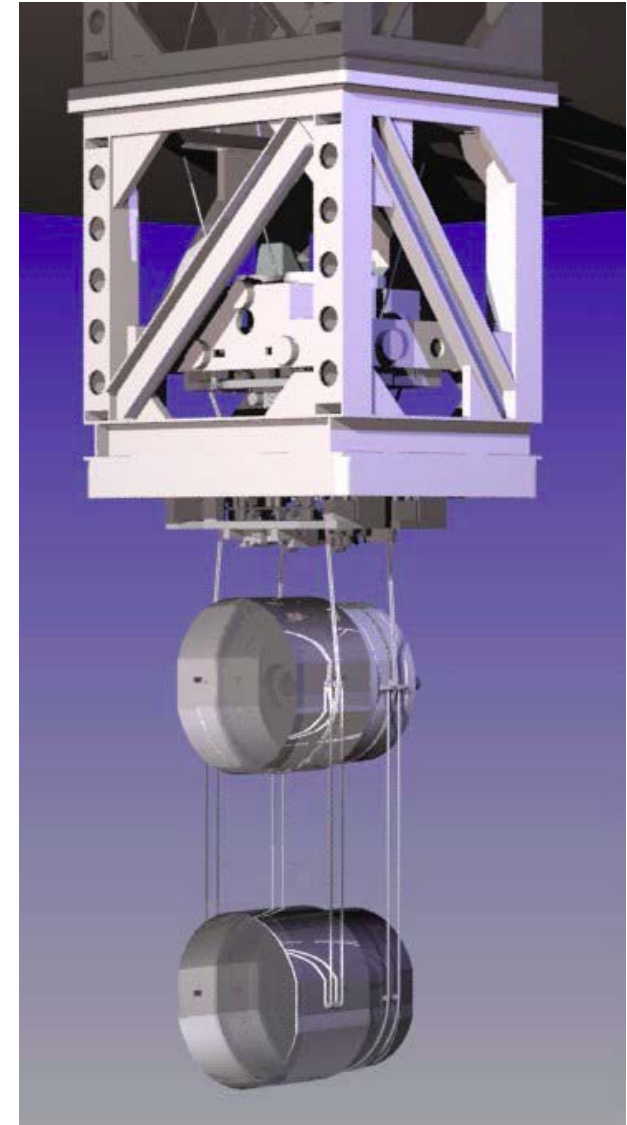
1. Bring the Advanced LIGO IFO to the desired operating point
2. Hold the IFO at the operating point 
3. Provide GW signal 

# Guiding IFO to the operating point: Problem of Lock Acquisition

- Narrow linewidth ( $\sim 1 \text{ nm}$ )
  - Residual arm motion of  $\sim 1 \mu\text{m}$  RMS at  $\sim 1 \text{ Hz}$
- Coupling of multiple optical cavities
- Cannot simply turn control system on and wait



- In addition, Test Mass (TM) actuators will lack sufficient authority when cavities are freely swinging
  - For AdvLIGO (compared with Initial LIGO):
    - weaker TM actuators
    - heavier TMs
- Guiding IFO to operating point is an issue
  - Standard PDH locking scheme not reliable
  - Lock acquisition cannot be a systematic process (cooling and heating of TMs an issue)
  - Impact on detector's duty cycle



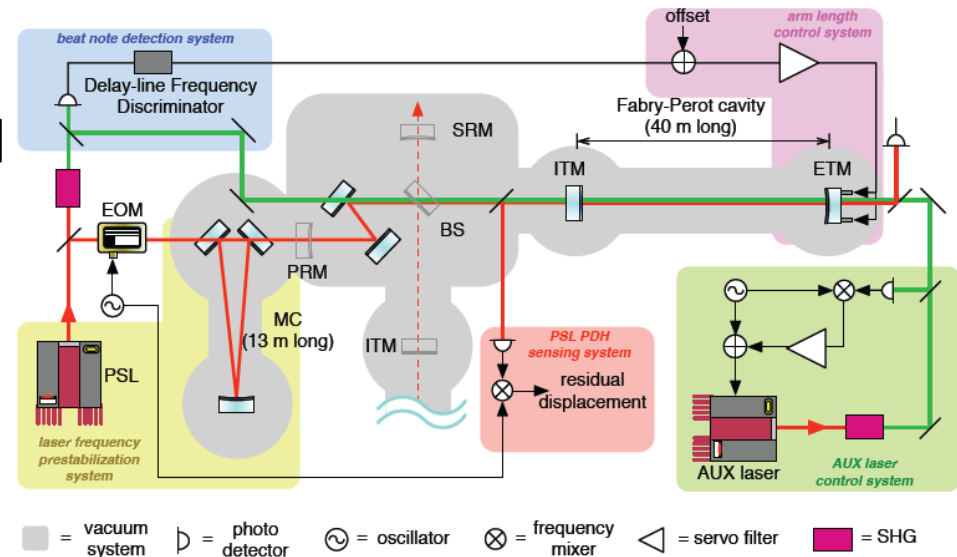
1. Maintain both arm cavities at a fixed (large) offset from resonance
  - Reduce RMS cavity motion to less than cavity linewidth ( $\sim 1 \text{ nm}$ )
2. Lock the central degrees of freedom first
  - ( $l_s, l_+$  and  $l_-$ )
3. Remove cavity offset and bring arms into resonance (IFO @ operating point)
4. Switch control to standard heterodyne/homodyne operation



# How?

How?

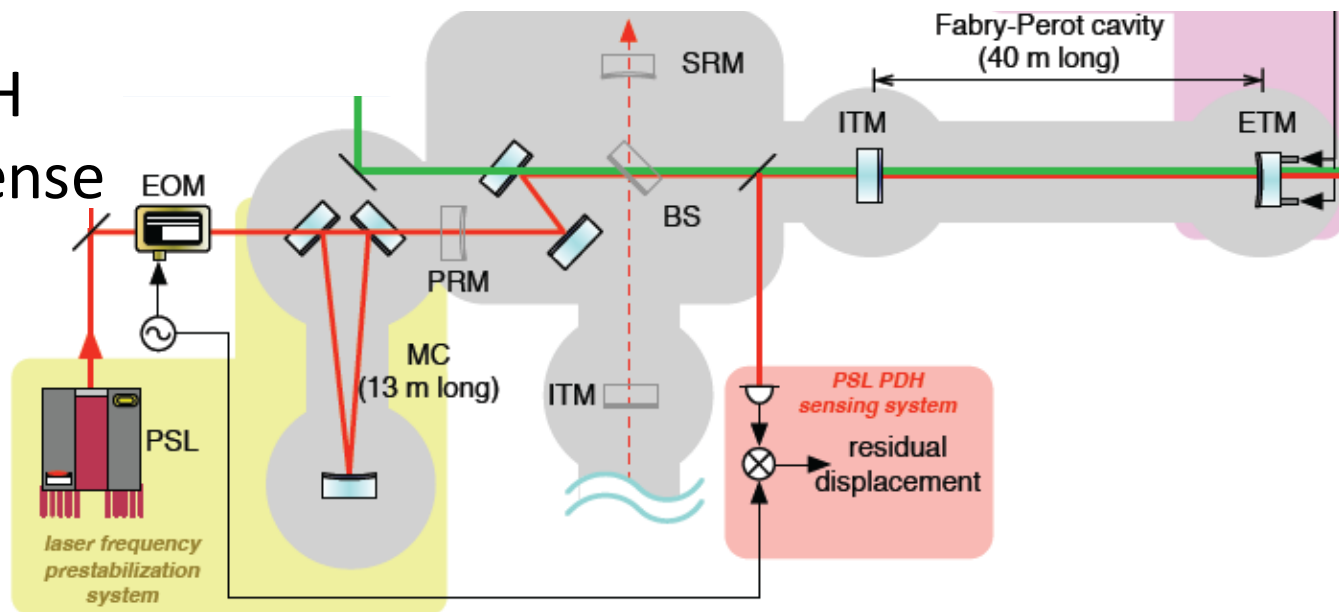
- To significantly increase detector's duty cycle
  - Auxiliary sensing and control system for the arm cavities
- Dual-wavelength locking designed to
  - a. maintain both arm cavities at a fixed offset from resonance
  - b. reduce RMS motion to within cavity linewidth
- Experimentally tested at Caltech's 40 m



(see Rollins J. et al., "Multi-color Cavity Metrology" P1200019-v5 and Mullavey A. J. et al, "Arm-length stabilization for interferometric gravitational-wave detectors using frequency-doubled auxiliary lasers," Optics Express, **20**, 81-89 (2011) )

# Multi-color Cavity Metrology at the 40 m

- Green laser locking
- Apply process to single arm at Caltech's 40m
- First, use standard PDH scheme to sense TM motion (without control) of single arm



= vacuum system   
  = photo detector   
  = oscillator   
 
⊗
 = frequency mixer   
  = servo filter   
 = SHG

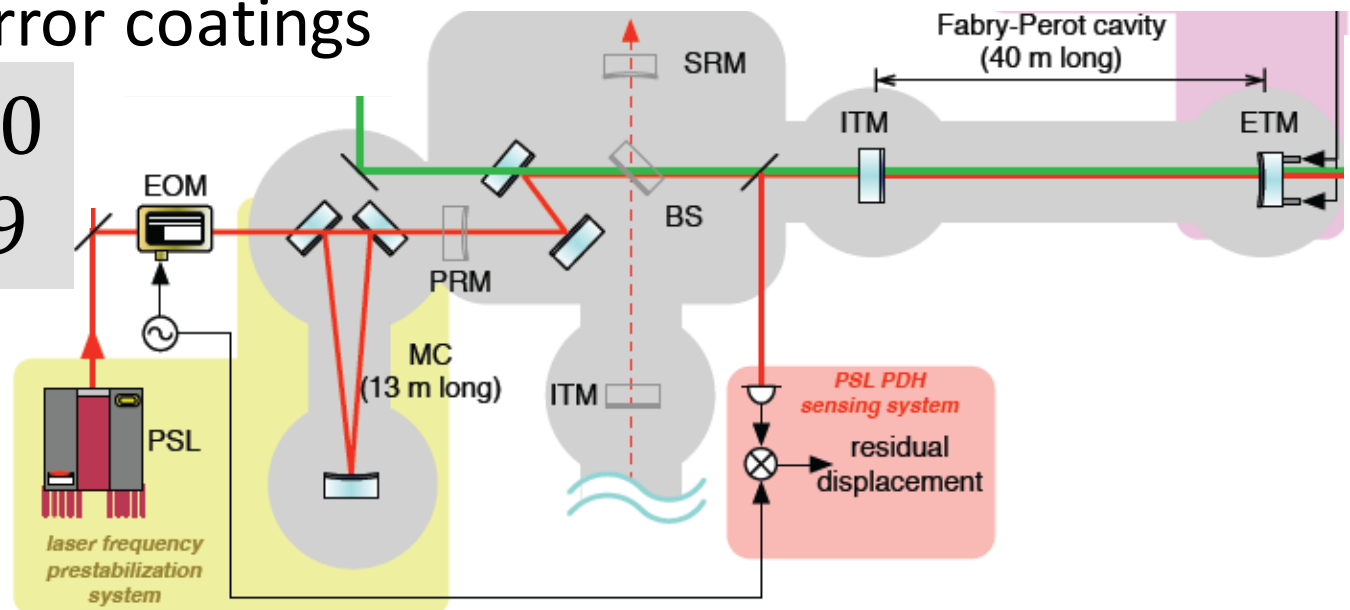
P1200019-V5

- Introduce a frequency-doubled NPRO (532 nm, green)
  - Via second harmonic generation (SHG) in a PPKTP crystal
  - Injected in ETM
- Also modulated producing a 2<sup>nd</sup> PDH error signal
- Dichroic mirror coatings

P1200019-V5

$$\mathcal{F}_{1064} = 450$$

$$\mathcal{F}_{532} = 109$$



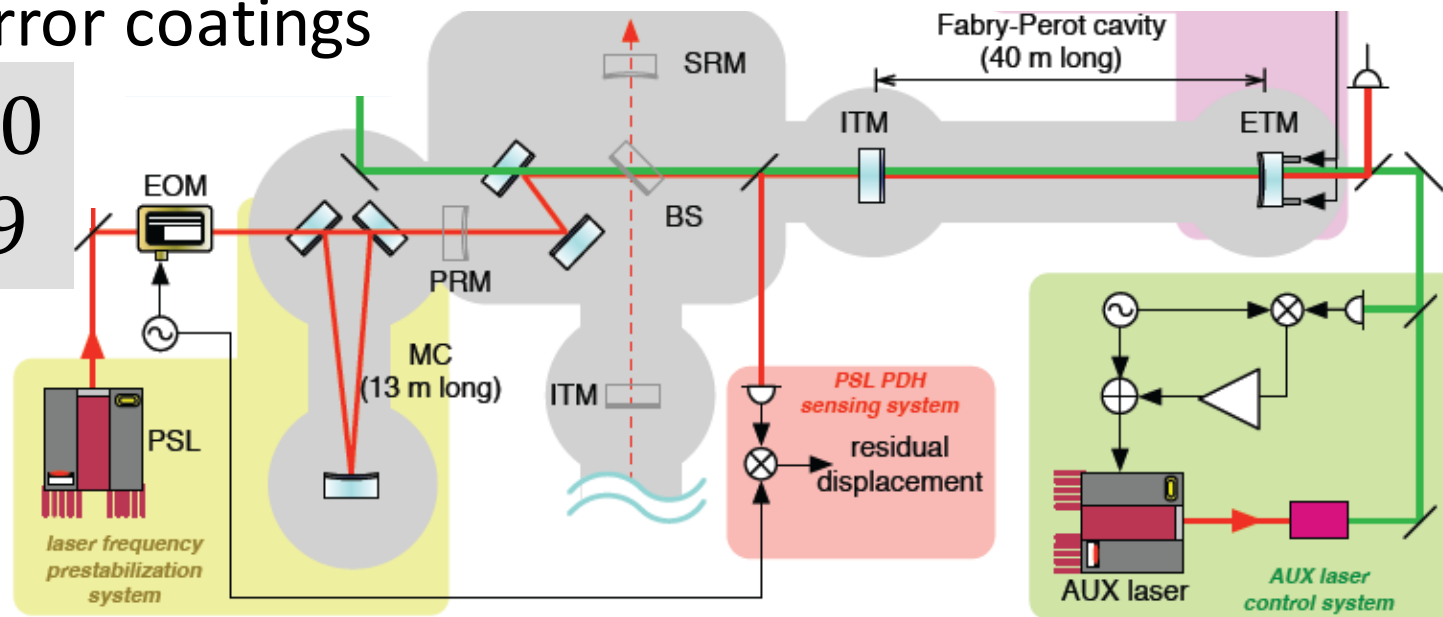
= vacuum system   
  = photo detector   
  = oscillator   
 ⊗ = frequency mixer   
  = servo filter   
  = SHG

- Introduce a frequency-doubled NPRO (532 nm, green)
  - Via second harmonic generation (SHG) in a PPKTP crystal
  - Injected in ETM
- Also modulated producing a 2<sup>nd</sup> PDH error signal
- Dichroic mirror coatings

P1200019-V5

$$\mathcal{F}_{1064} = 450$$

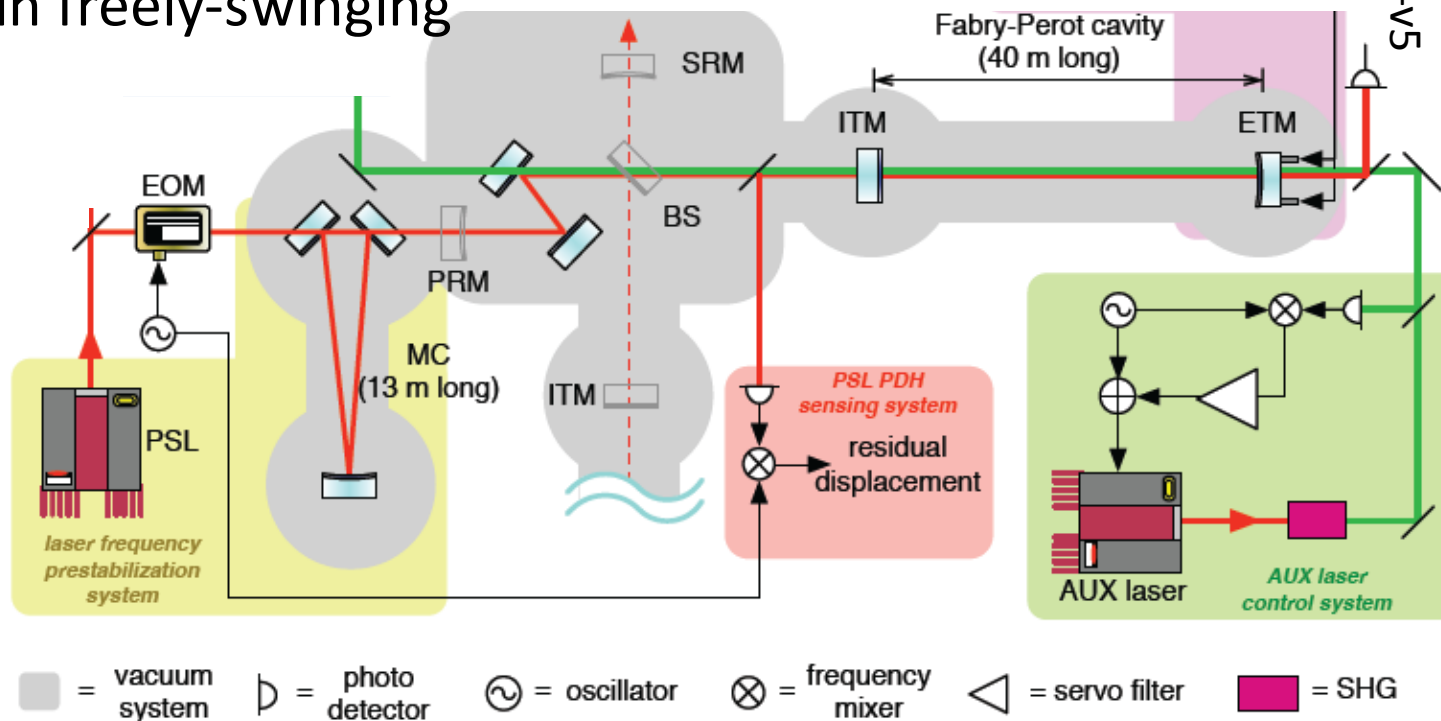
$$\mathcal{F}_{532} = 109$$



= vacuum system   
  = photo detector   
  = oscillator   
  = frequency mixer   
  = servo filter   
  = SHG

# Locking of the AUX laser

- At this point, AUX laser frequency locked to free-swinging arm cavity
- High-gain and high-bandwidth control
- AUX laser frequency tracks cavity length at all times
  - TMs remain freely-swinging

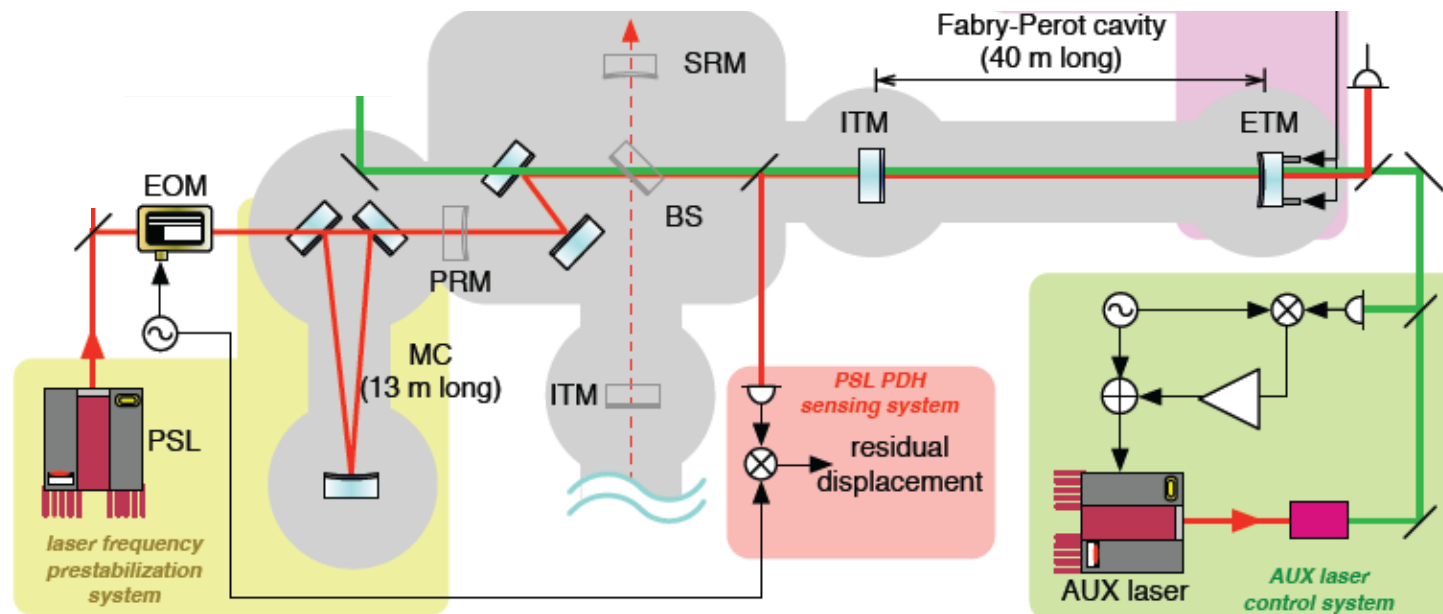


P1200019-v5

# Comparing Frequencies

- 532 beam sample compared to 1064 sample
  - 532 laser frequency tracks the cavity length, 1064 is free-running
- Frequency comparison → how far PSL is from resonance
  - Comparison results in a beat note frequency, measured with DFD

P1200019-V5

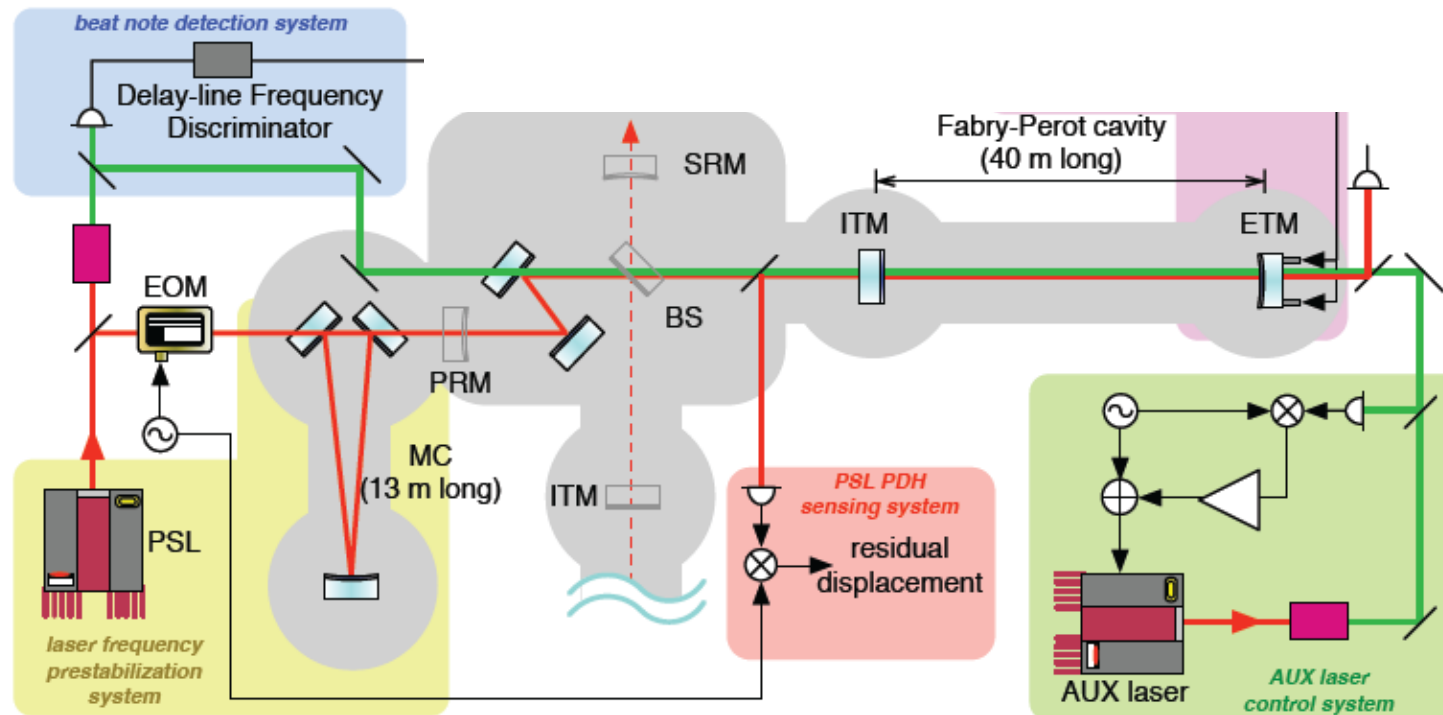


= vacuum system  
  = photo detector  
  = oscillator  
  = frequency mixer  
  = servo filter  
  = SHG

# Comparing Frequencies

- 532 beam sample compared to 1064 sample
  - 532 laser frequency tracks the cavity length, 1064 is free-running
- Frequency comparison → how far PSL is from resonance
  - Comparison results in a beat note frequency, measured with DFD

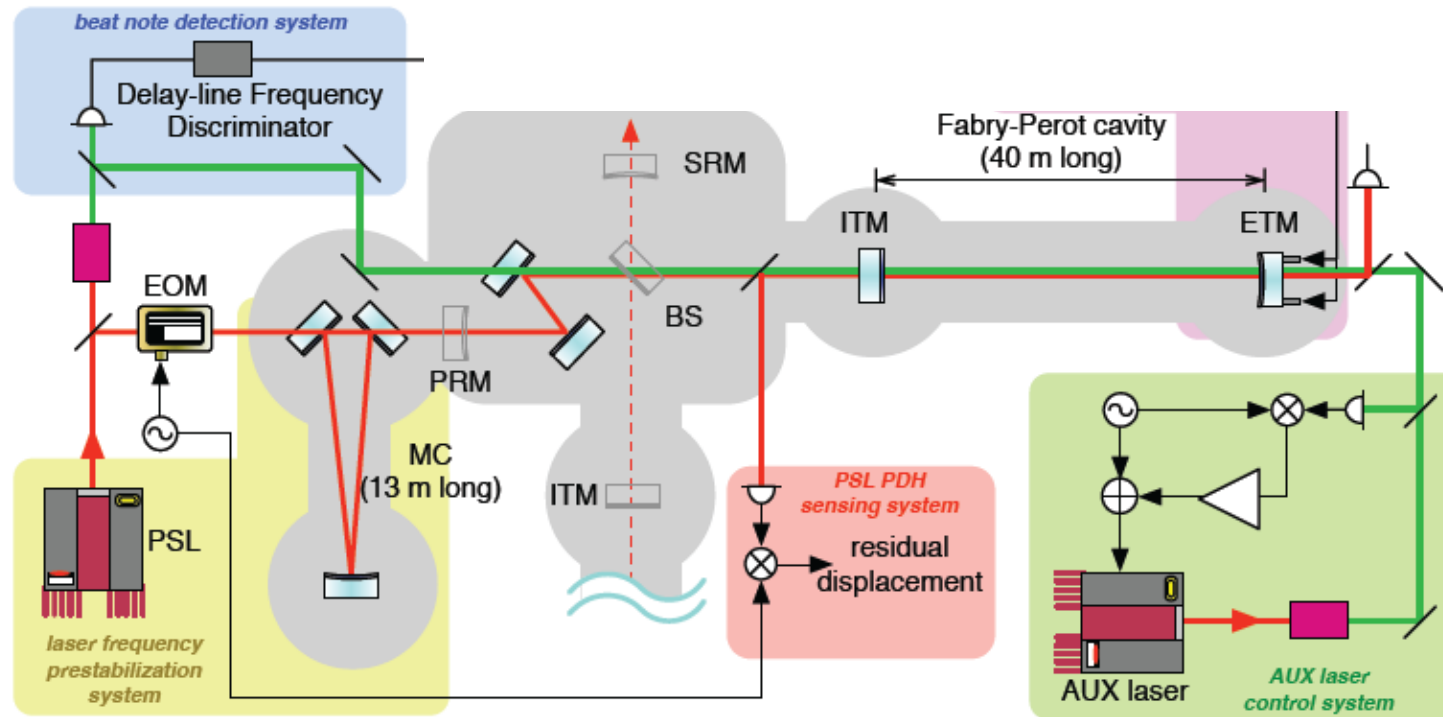
P1200019-V5



= vacuum system   
  = photo detector   
 ~ = oscillator   
 ⊗ = frequency mixer   
 ◁ = servo filter   
  = SHG



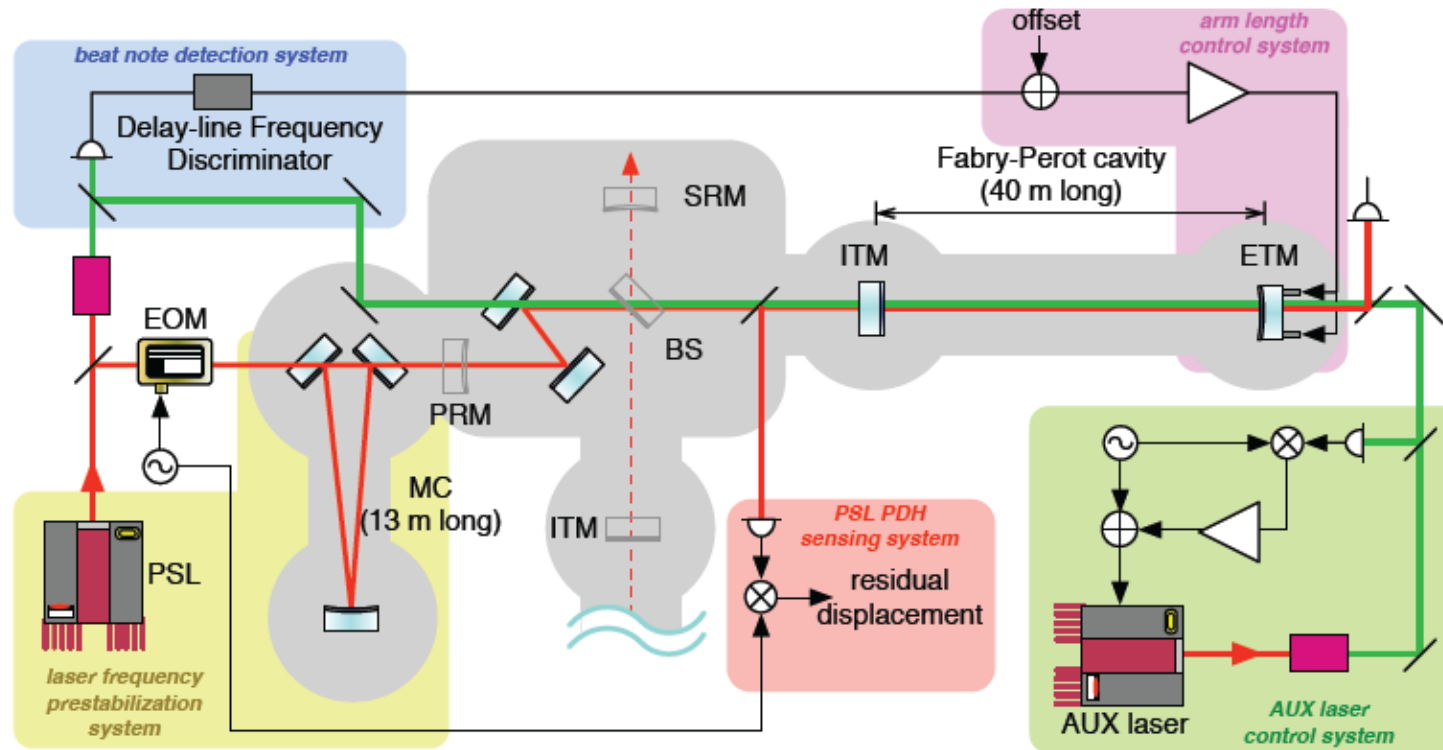
- New error signal
  - Beat frequency used to lock the cavity to the PSL (with the PSL resonating or not)
  - Control signal sent to the ETM, suppressing cavity motion (relative to the PSL)
- Offset allows to change locking point



P1200019-v5

= vacuum system  
  = photo detector  
  = oscillator  
 
⊗
 = frequency mixer  
  = servo filter  
  = SHG

- New error signal
  - Beat frequency used to lock the cavity to the PSL (with the PSL resonating or not)
  - Control signal sent to the ETM, suppressing cavity motion (relative to the PSL)
- Offset allows to change locking point

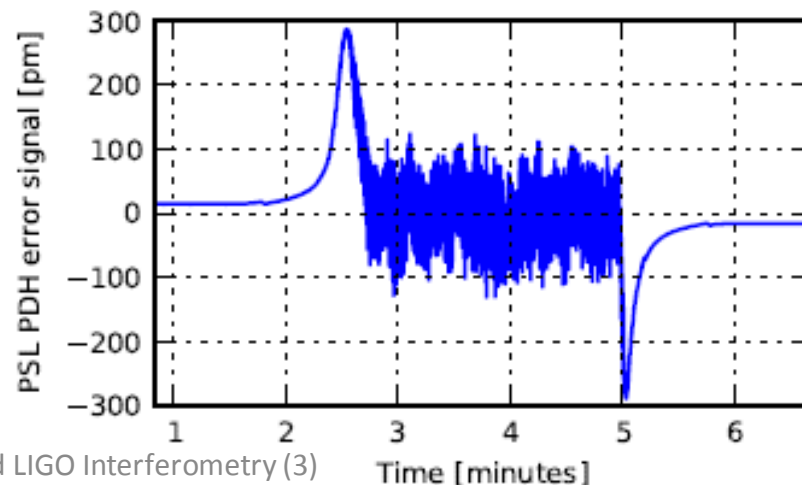
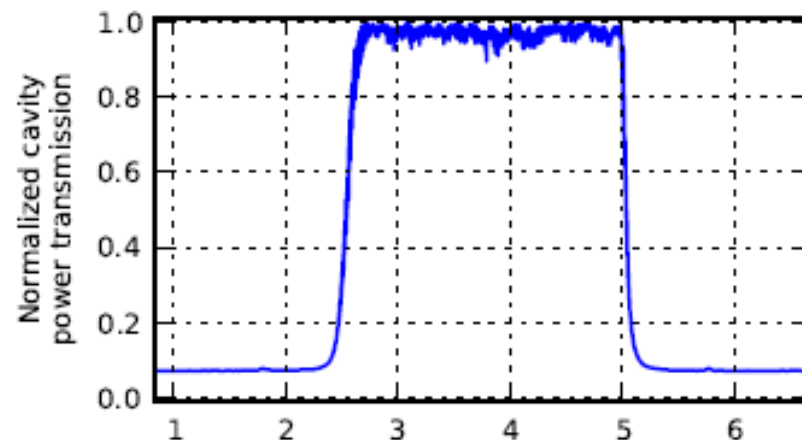
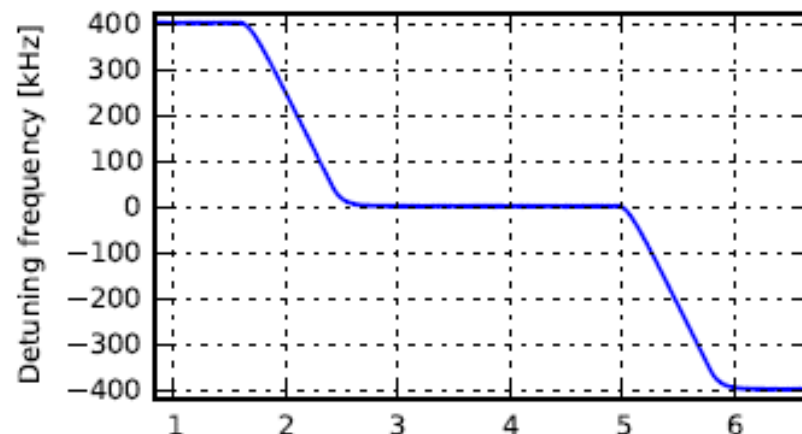


P1200019-v5

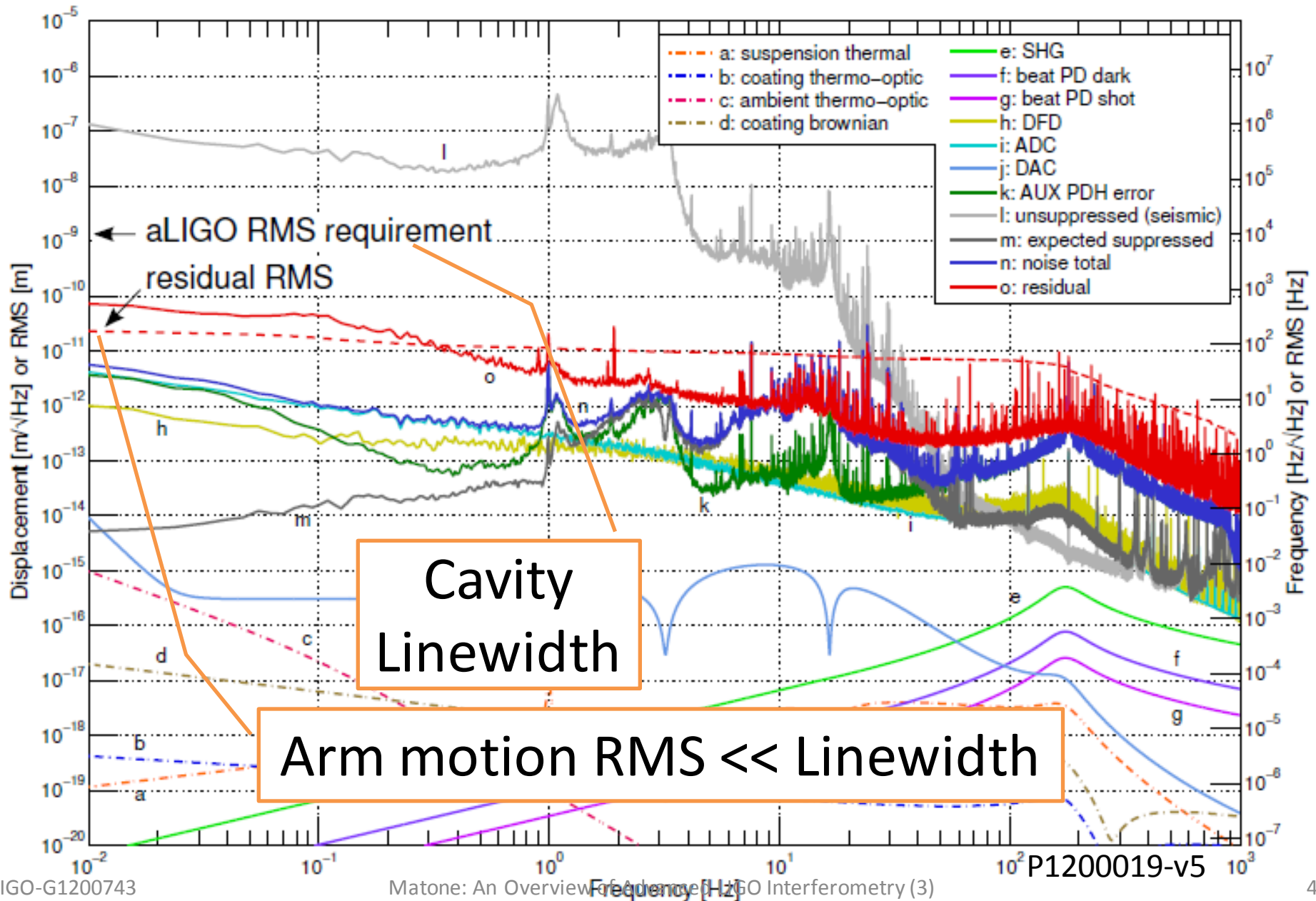
= vacuum system  
  = photo detector  
  = oscillator  
  = frequency mixer  
  = servo filter  
  = SHG

# Results

- AUX laser frequency locked to arm
- Arm cavity length locked to PSL (using beat frequency)
- Cavity length offset allows to scan the cavity length, looking for the 1064 resonance
- PSL PDH error signal is used to measure the residual displacement noise



P1200019-V5



# Adv LIGO Strategy

1. Use AUX laser system to
  - a. Lock arms away from resonance
  - b. Reduce RMS motion
2. Lock the central degrees of freedom
  - ( $l_s, l_+$  and  $l_-$ )
3. Reduce arm offset and bring IFO to operating point

# Control of $l_s$ , $l_+$ and $l_-$ during acquisition

- Error signals for the central IFO degrees of freedom
  - Need to be independent of arm cavities
- Signals on reflection and demodulated at  $3f$  have been studied and shown to be independent of arms
  - Modulation frequencies at 27 Hz and 135 Hz

- Advanced LIGO optical configuration
  - Dual-recycling laser interferometer
  - Signal Recycling Cavity
    - Introduces a tunable frequency response
- Longitudinal Degrees of Freedom to Sense and Control
  - Five DOF, added level of complexity, two pairs of sidebands
  - Demodulation and Double-Demodulation ( $f_1, f_2, f_1 + f_2, f_2 - f_1$ )
- Homodyne detection scheme
  - Get around heterodyne detection scheme at the DP
  - Requires to lock at small  $L_-$  offset
- Lock Acquisition
  - Green laser locking: AUX laser system to stabilize LIGO arms, locking them away from resonance
  - Lock central degrees of freedom (demodulating at  $3f$ )
  - Bring arms into resonance
  - Switch control to standard heterodyne/homodyne operation

# Group Activity

- Post questions on the board
- Group discussion
- In preparation for tomorrow
  - Read “The Advanced LIGO Reference Design”  
M060056-v2
  - Prepare questions