

# Thesis Title: Adaptive Modal Damping of Advanced LIGO Suspensions

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Thesis Defense – Mechanical Engineering

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# Abstract

**Motivation:** Observe gravitational waves from astrophysical sources (supernovae, pulsars, black hole mergers, etc) using the LIGO observatories.

**Problem:** Active control to suppresses time varying ground disturbances. This control introduces additional noise. Optimal control requires tuning the trade-off as the disturbances evolve.

1. Many of the LIGO control loops contain non-negligible sensing noise
2. Seismic disturbances evolves in time
3. LIGO optical cavities have a small finite linear operating range

**Solution:** An adaptive algorithm to constantly monitor and tune the performance of this control. Applied to the method of modal damping. Adaptation optimized for astrophysical sources.

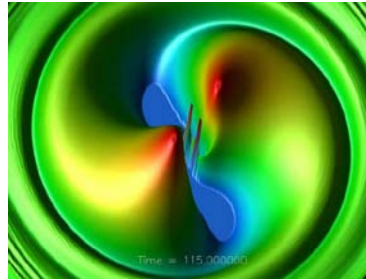
# Outline

1. LIGO and gravitational waves
2. Seismic (vibration) isolation
3. Problems and challenges
4. Method of adaptive modal damping
5. Experimental results
6. Simulated results

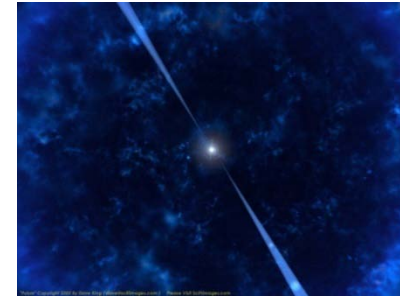
# Gravitational Waves



Supernova

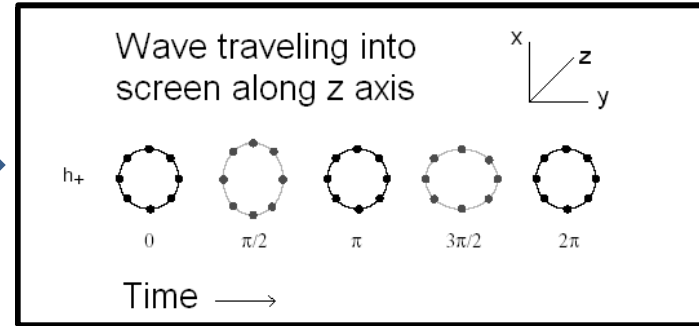
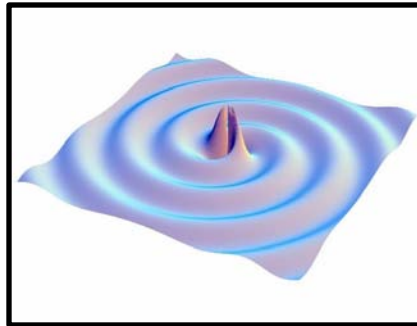


Merging Black Holes



Pulsar

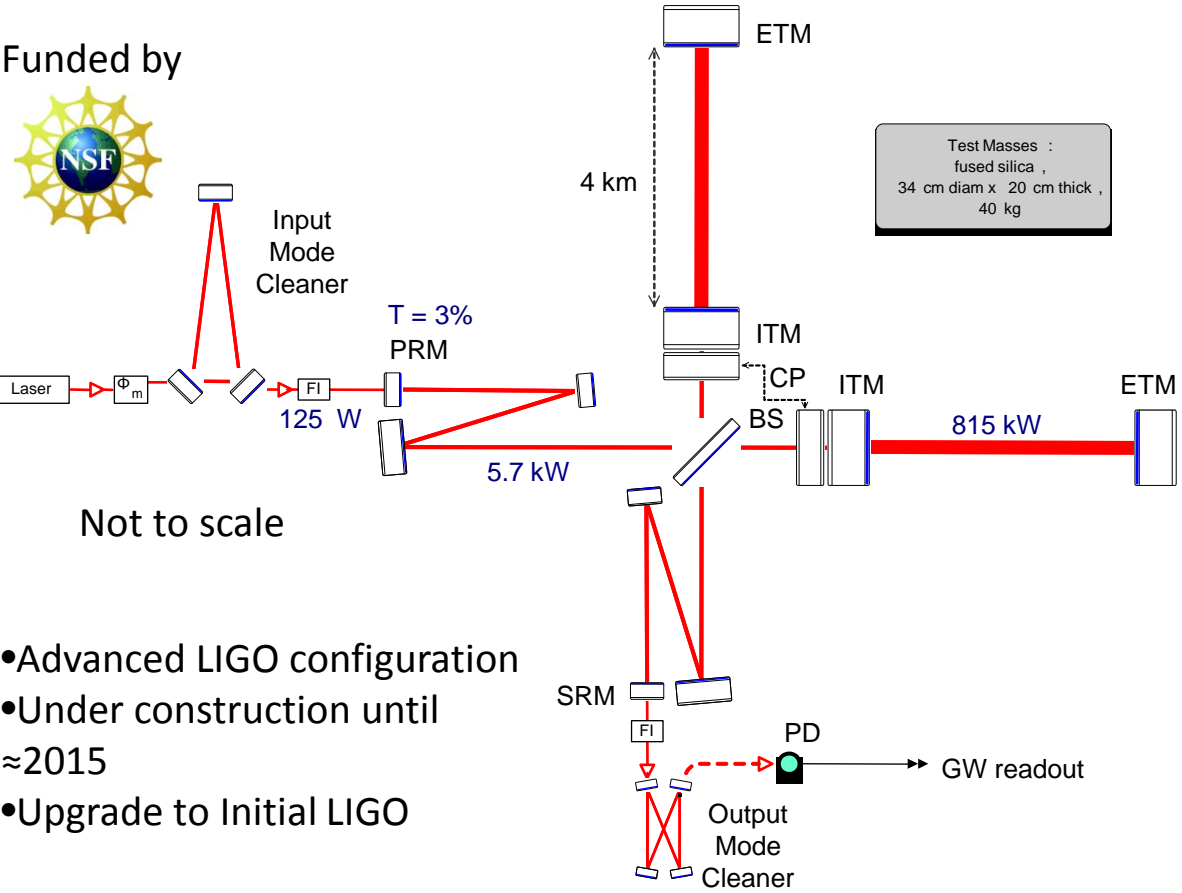
Wave of strain amplitude  $h$



- **Supernovae**
  - Asymmetry required
- **Coalescing Binaries**
  - Black Holes or Neutron Stars Mergers
- **Pulsars**
  - Asymmetry required
- **Stochastic Background (Big bang, etc.)**

# Gravitational-wave Observatory (LIGO)

Funded by



Test Masses :  
fused silica,  
34 cm diam x 20 cm thick,  
40 kg

Not to scale



Hanford, WA



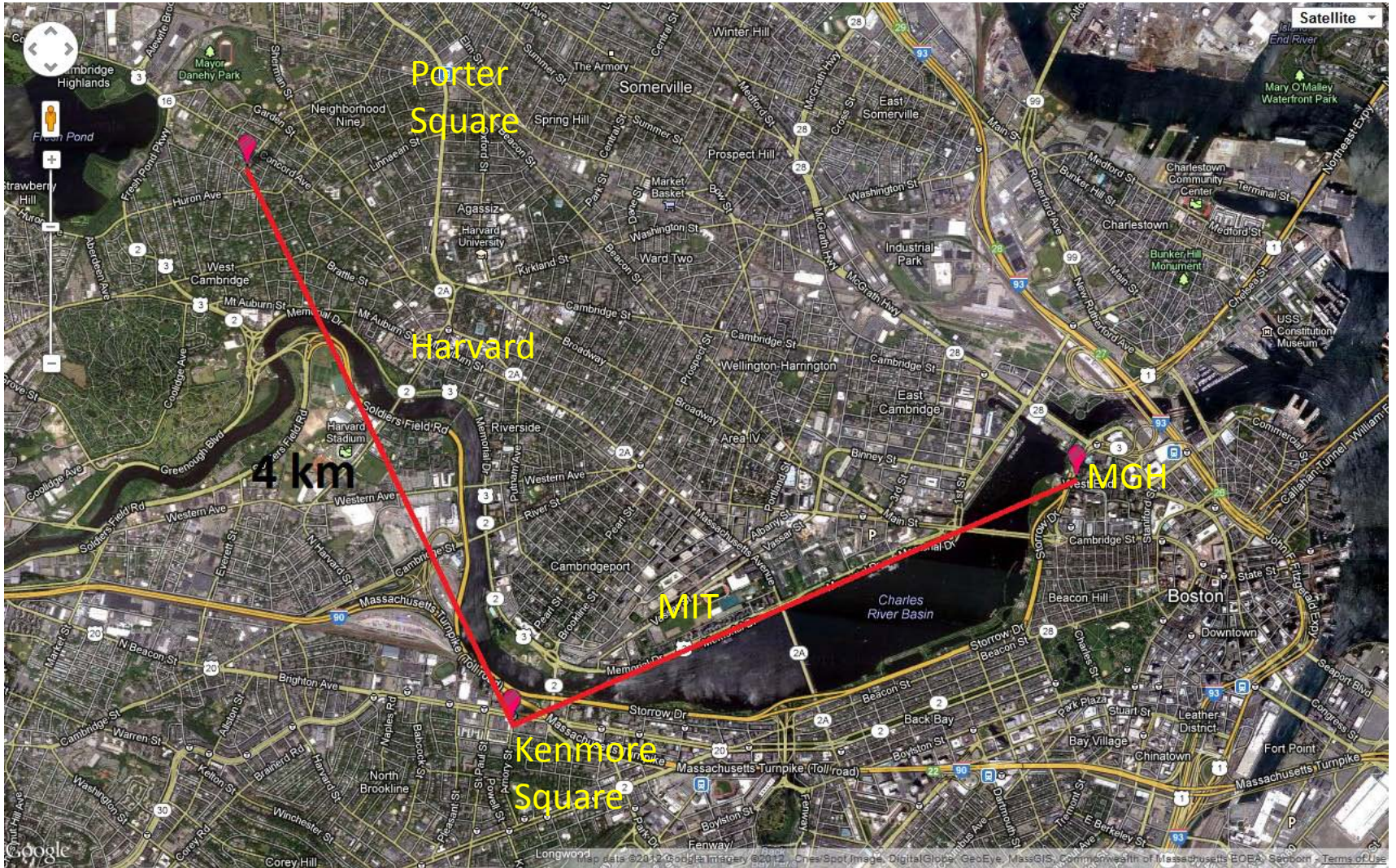
Livingston, LA

- Advanced LIGO configuration
- Under construction until ≈2015
- Upgrade to Initial LIGO

- **3, 4 km interferometers at 2 sites in the US**
- **Michelson interferometers with Fabry-Pérot arms**
- **Optical path enclosed in vacuum**
- **Sensitive to strains around  $10^{-22}$  ->  $10^{-19} m_{rms}$**
- **LIGO Budget ≈ \$60 Million per year from NSF.**
- **Operated by MIT and Caltech.**



# If we put LIGO in Cambridge, MA



LIGO spans 16 km<sup>2</sup>. Cambridge, MA covers 16.65 km<sup>2</sup> (wikipedia [http://en.wikipedia.org/wiki/Cambridge,\\_Massachusetts](http://en.wikipedia.org/wiki/Cambridge,_Massachusetts)).

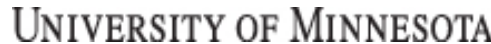
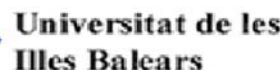
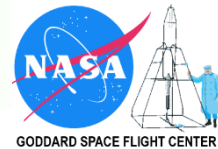


# LIGO

# LIGO Scientific Collaboration



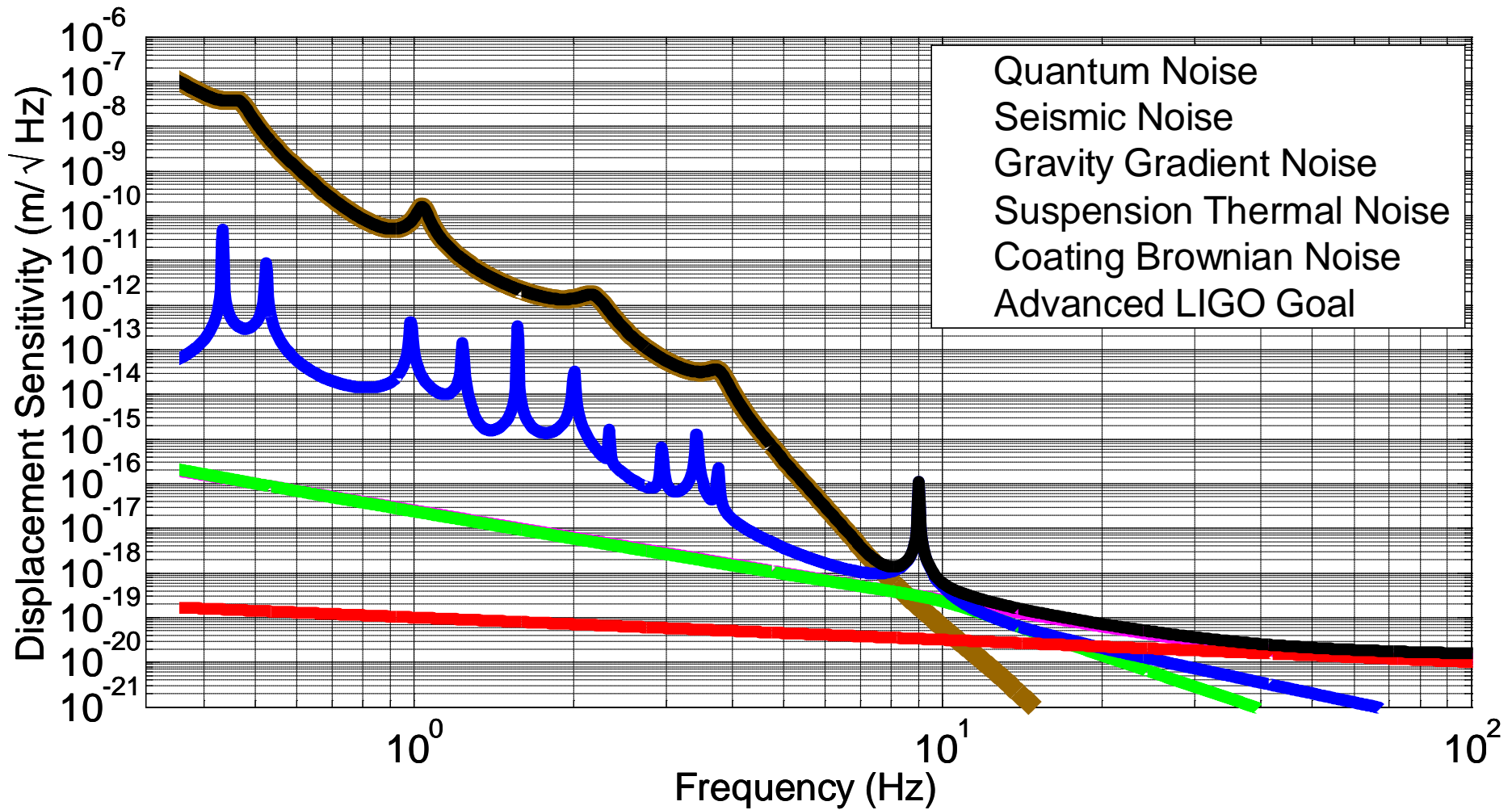
- Australian Consortium for Interferometric Gravitational Astronomy
- The Univ. of Adelaide
- Andrews University
- The Australian National Univ.
- The University of Birmingham
- California Inst. of Technology
- Cardiff University
- Carleton College
- Charles Sturt Univ.
- Columbia University
- CSU Fullerton
- Embry Riddle Aeronautical Univ.
- Eötvös Loránd University
- University of Florida
- German/British Collaboration for the Detection of Gravitational Waves
- University of Glasgow
- Goddard Space Flight Center
- Leibniz Universität Hannover
- Hobart & William Smith Colleges
- Inst. of Applied Physics of the Russian Academy of Sciences
- Polish Academy of Sciences
- India Inter-University Centre for Astronomy and Astrophysics
- Louisiana State University
- Louisiana Tech University
- Loyola University New Orleans
- University of Maryland
- Max Planck Institute for Gravitational Physics



- University of Michigan
- University of Minnesota
- The University of Mississippi
- Massachusetts Inst. of Technology
- Monash University
- Montana State University
- Moscow State University
- National Astronomical Observatory of Japan
- Northwestern University
- University of Oregon
- Pennsylvania State University
- Rochester Inst. of Technology
- Rutherford Appleton Lab
- University of Rochester
- San Jose State University
- Univ. of Sannio at Benevento, and Univ. of Salerno
- University of Sheffield
- University of Southampton
- Southeastern Louisiana Univ.
- Southern Univ. and A&M College
- Stanford University
- University of Strathclyde
- Syracuse University
- Univ. of Texas at Austin
- Univ. of Texas at Brownsville
- Trinity University
- Tsinghua University
- Universitat de les Illes Balears
- Univ. of Massachusetts Amherst
- University of Western Australia
- Univ. of Wisconsin-Milwaukee
- Washington State University
- University of Washington



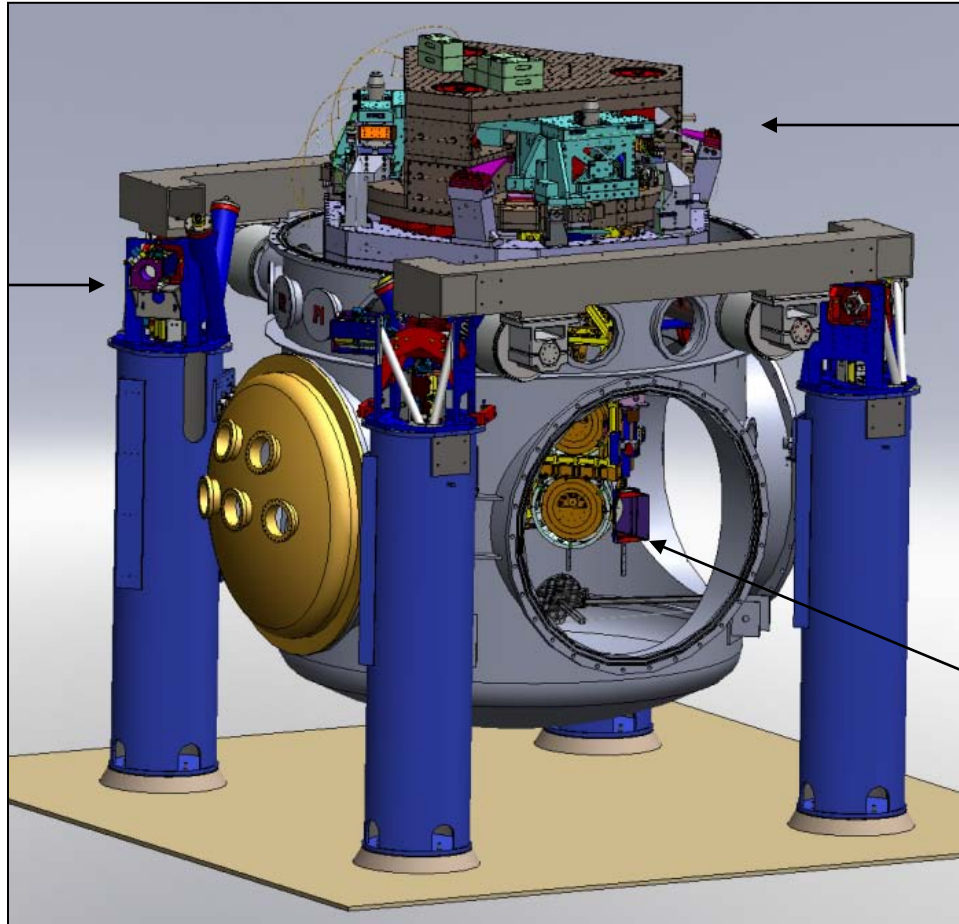
# Projected Sensitivity for Advanced LIGO





# Suspensions and Seismic Isolation

Advanced LIGO test mass isolation



active isolation platform (2 stages of isolation)

hydraulic external pre-isolator (HEPI) (one stage of isolation)

quadruple pendulum (four stages of isolation) with monolithic silica final stage

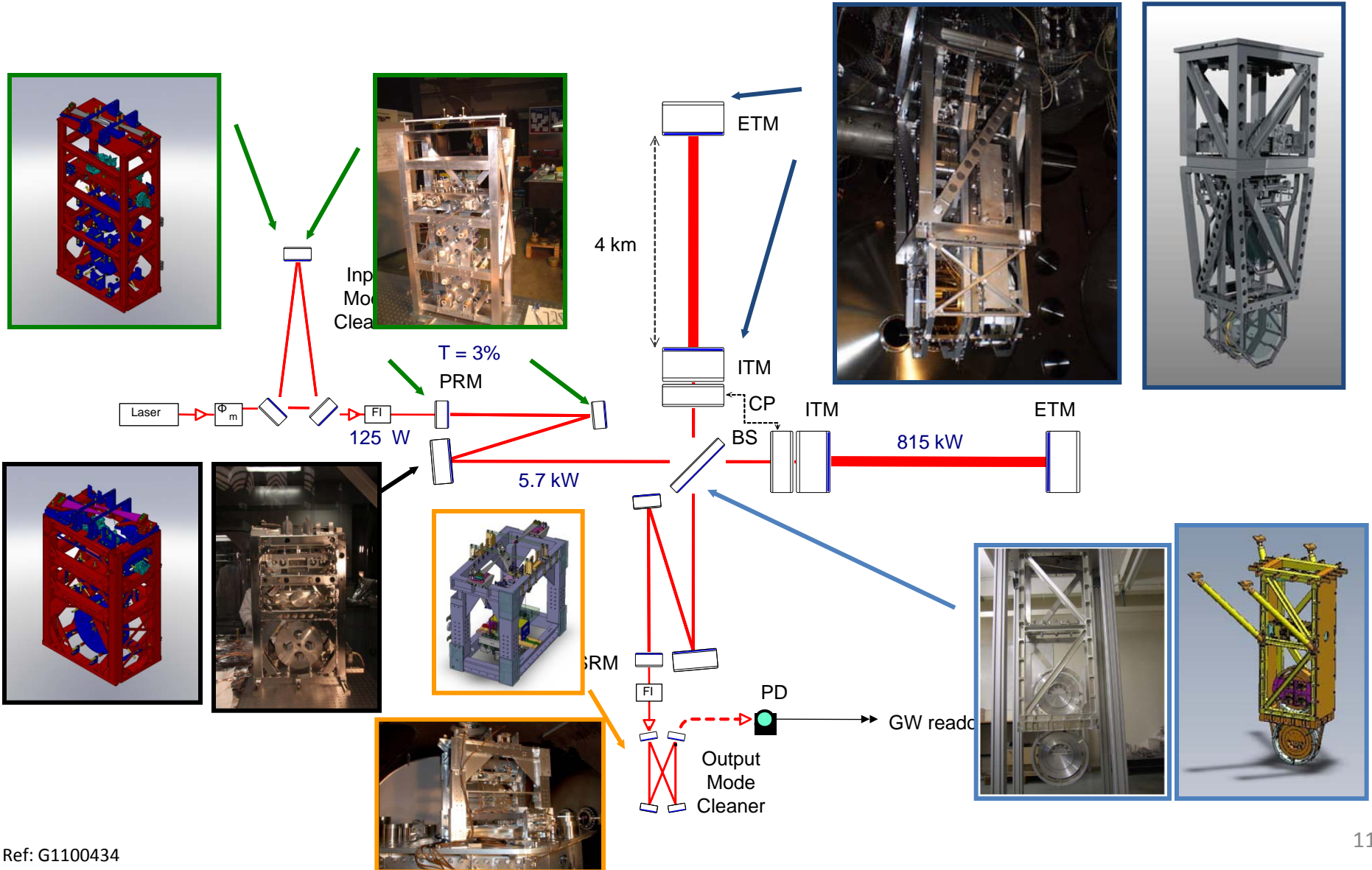


active isolation  
platform (2 stages  
of isolation)

quadruple pendulum (four  
stages of isolation)

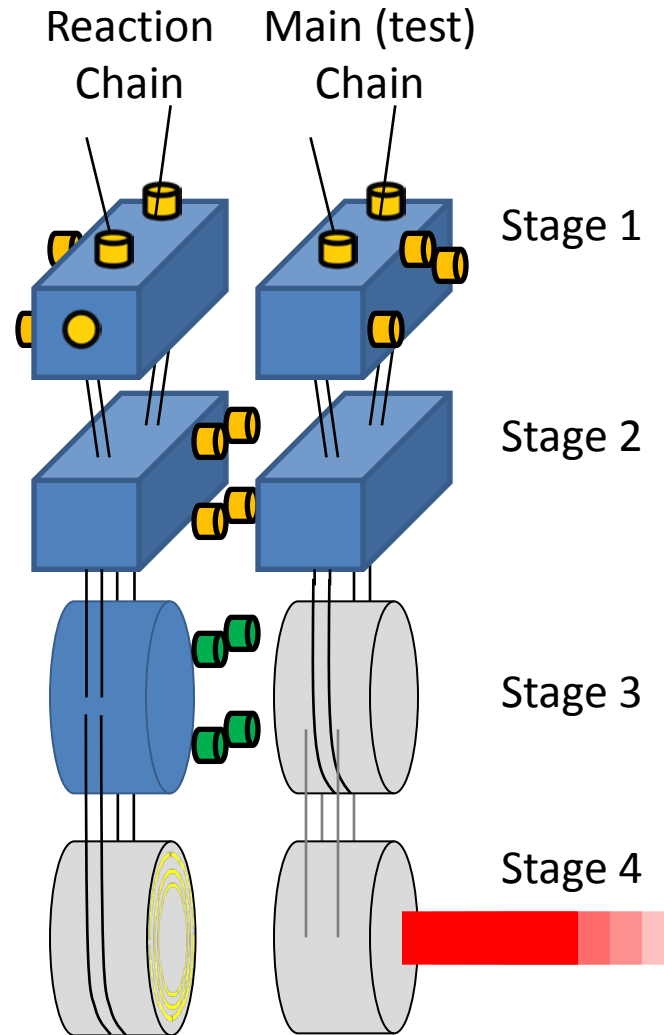
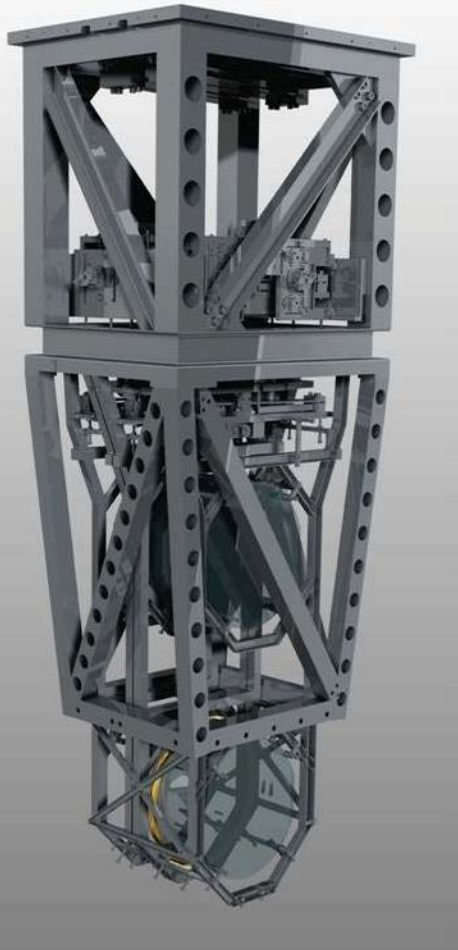
Installing prototype quad  
pendulum with glass optic on  
metal wires, Jan 2009 at MIT.

# Five Pendulum Designs





# Quadruple Pendulum





## Purpose

- Test mass (stage 4) isolation.  
the test mass consists of a 40 kg high reflective mirror

## Control

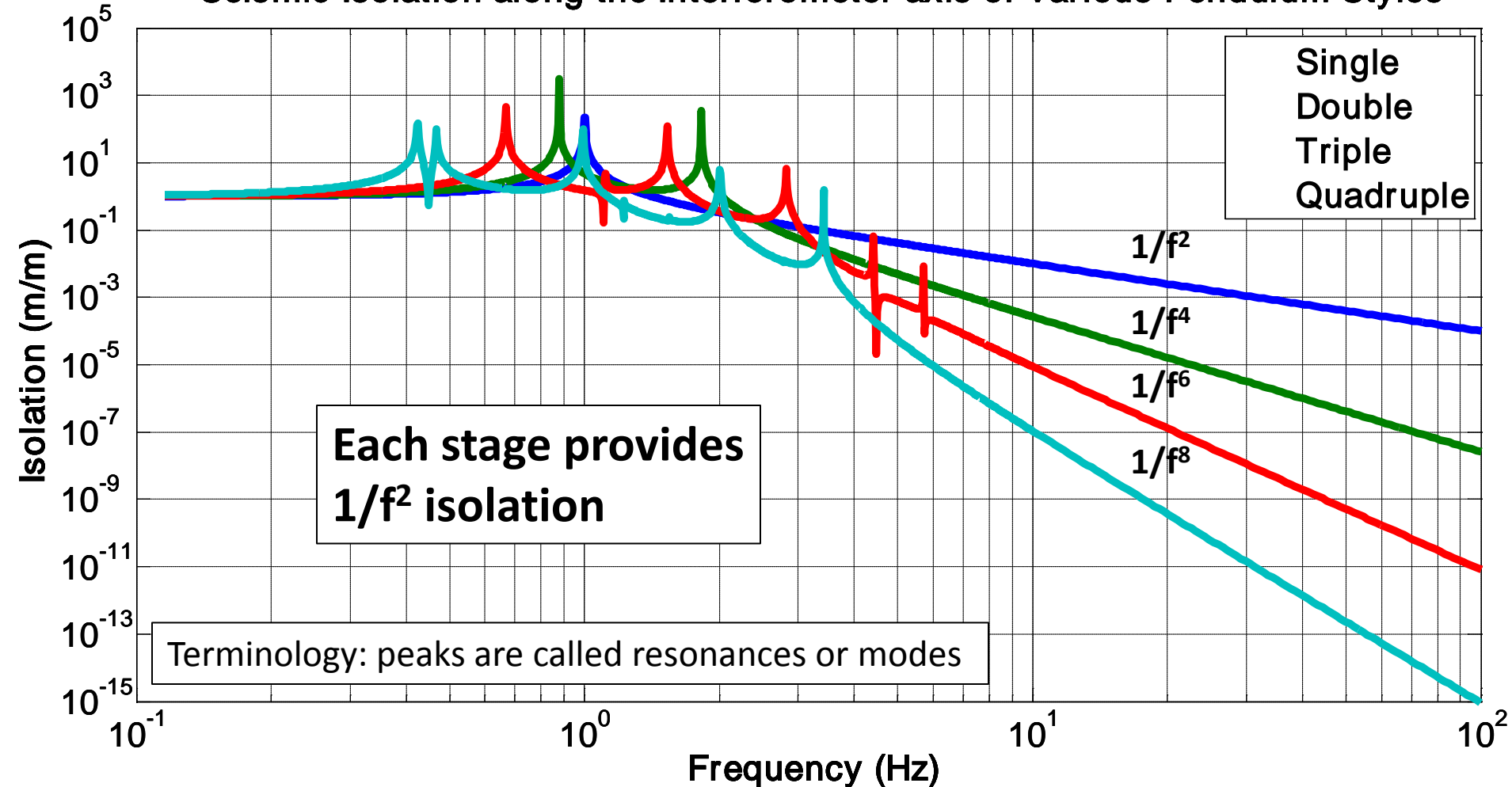
- Damping –stage 1
- Cavity length - all stages

## Sensors/Actuators

-  BOSEMs at stage 1 & 2
-  AOSEMs at stage 3
- Opt. lev. and interf. sigs. at stage 2
- Electrostatic drive (ESD) at stage 4

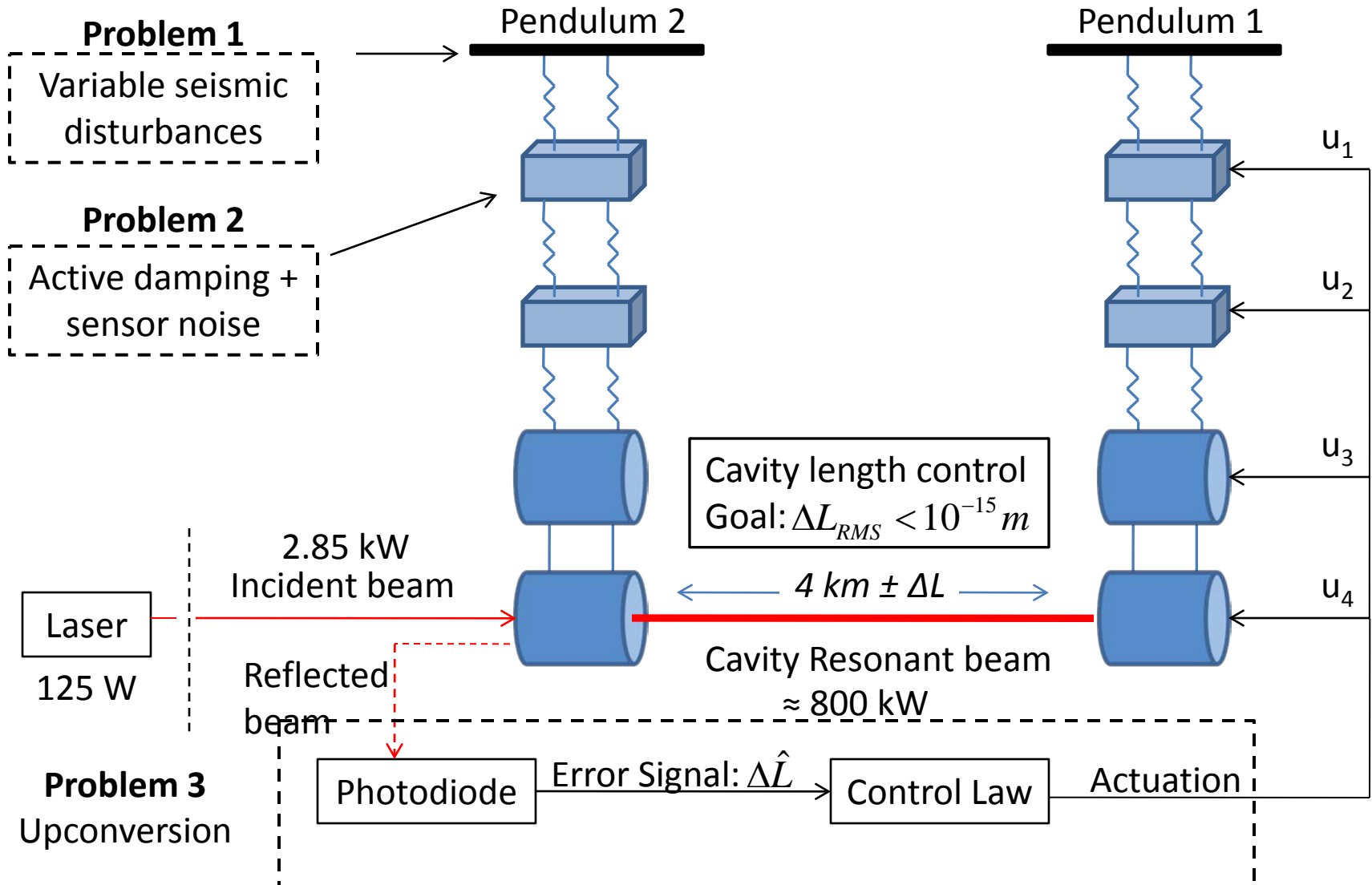
# Multi-stage Isolation Performance

Seismic Isolation along the Interferometer axis of Various Pendulum Styles



# Control: Problems and Challenges

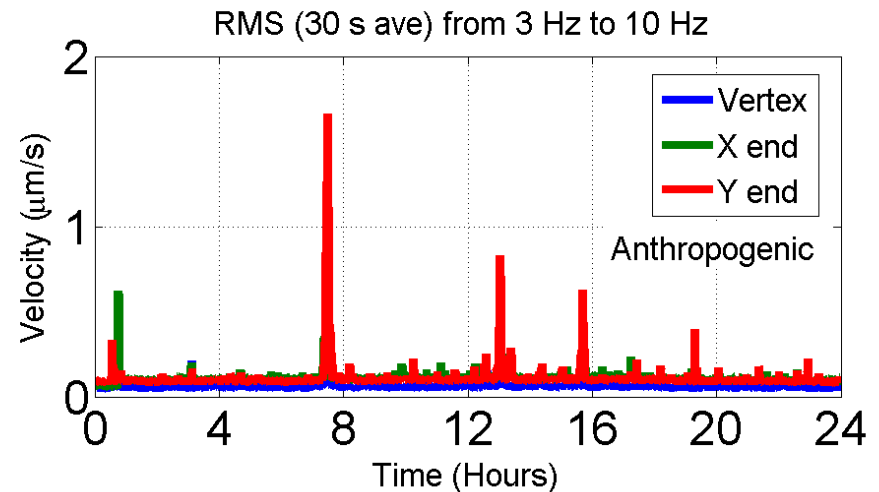
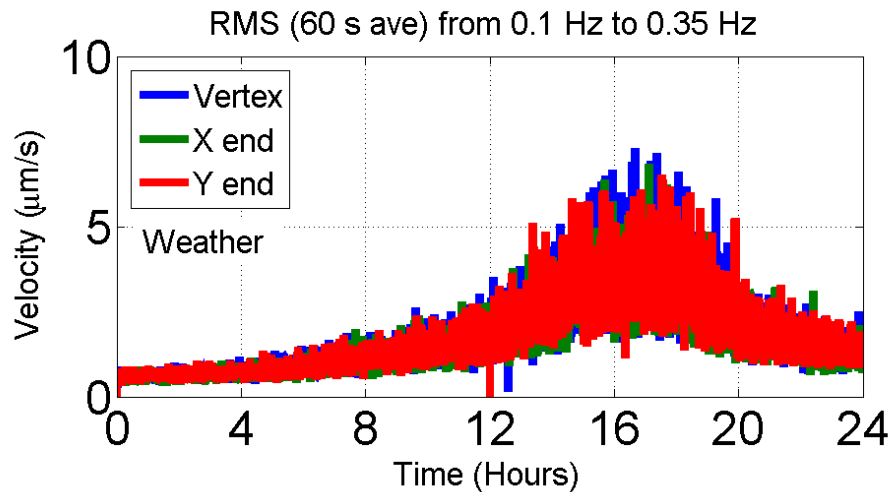
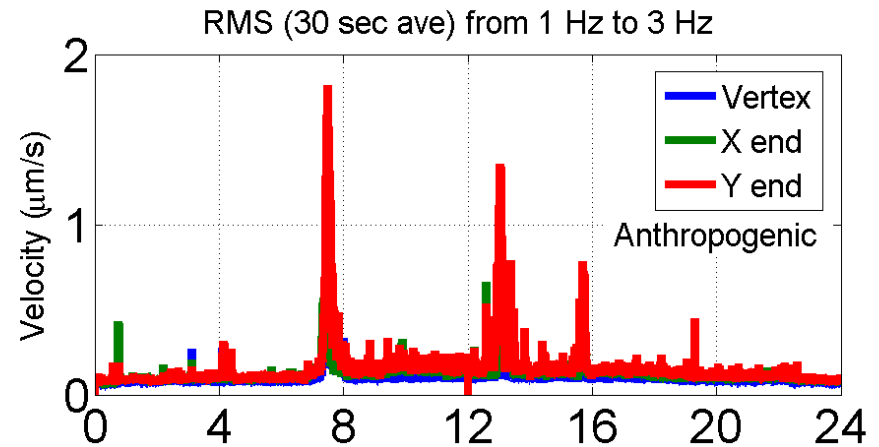
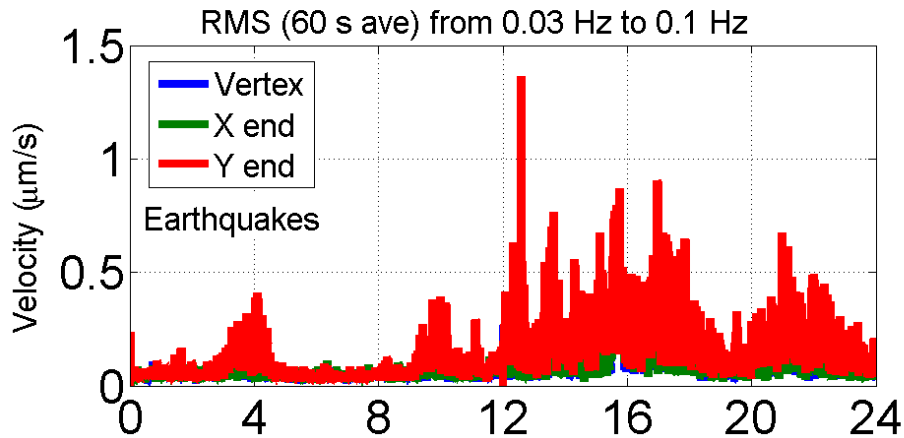
Schematic view of one of LIGO's 4 km Fabry-Perot cavity arms





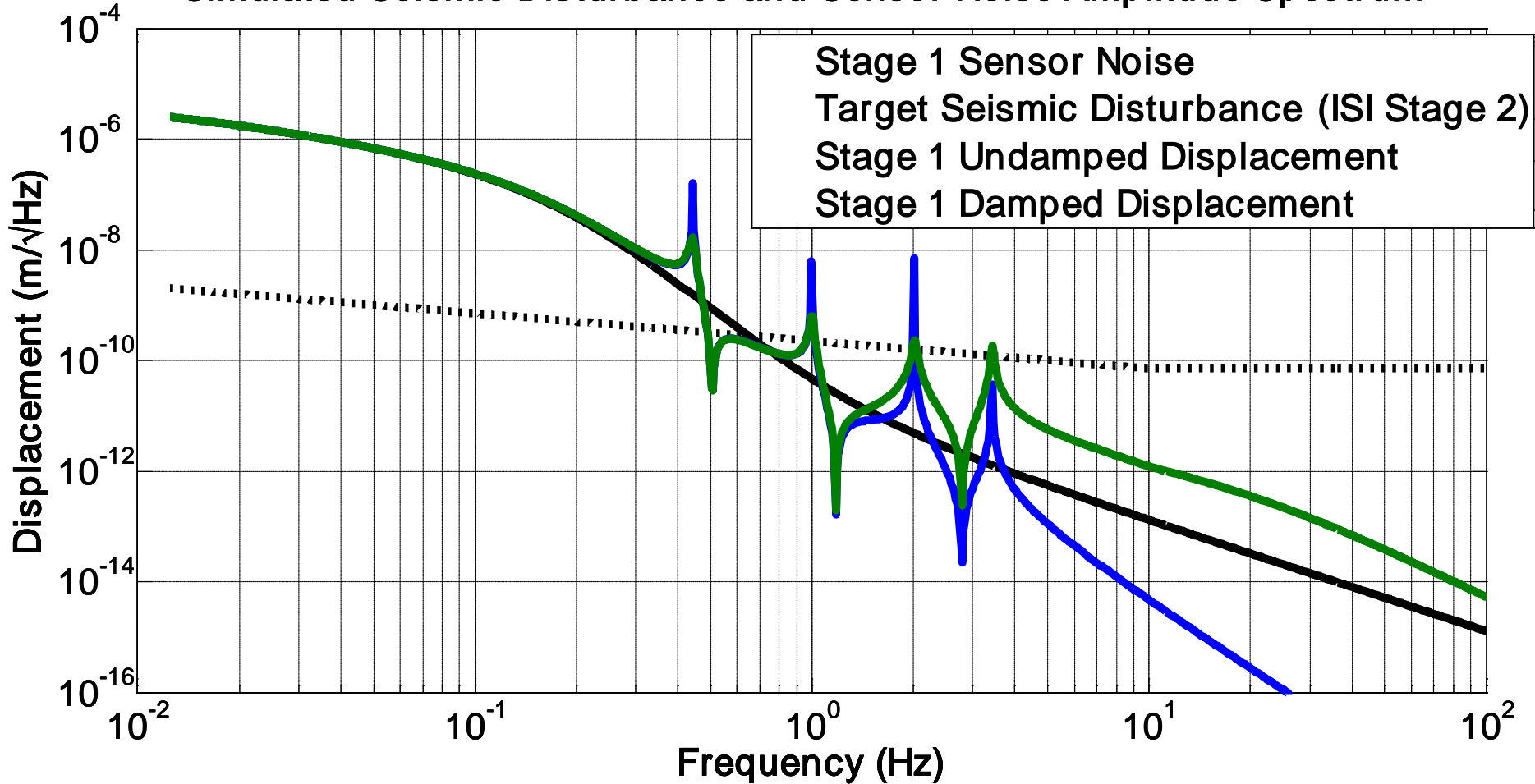
# Problem 1: Nonstationary Disturbance

Seismic disturbance at Livingston Observatory on November 21, 2009



# Problem 2: Damping Sensor Noise

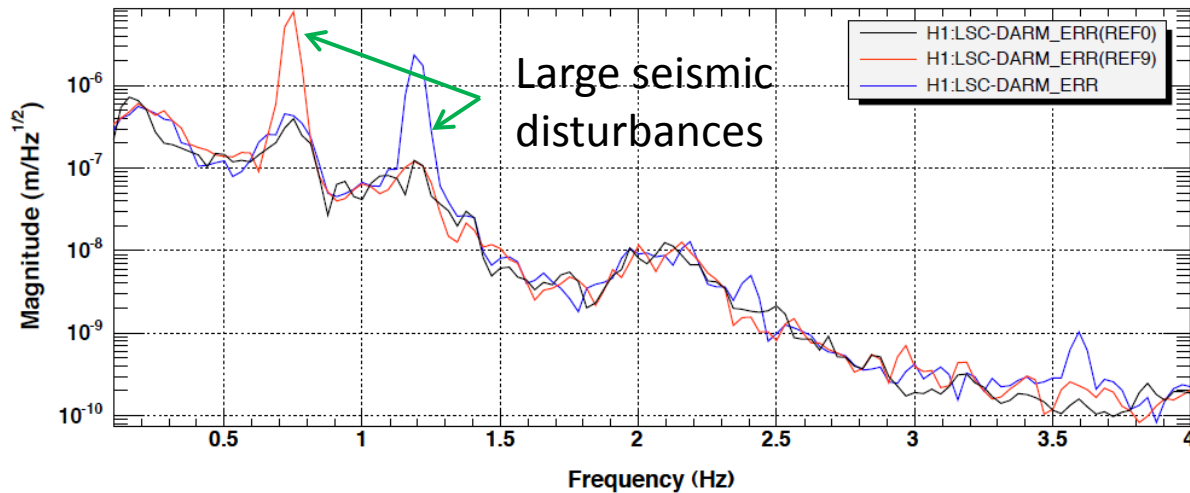
Simulated Seismic Disturbance and Sensor Noise Amplitude Spectrum



# Problem 3: Seismic Upconversion

Mid-Y ground injections: Black: none, Red: 0.75 Hz, Blue: 1.2 Hz

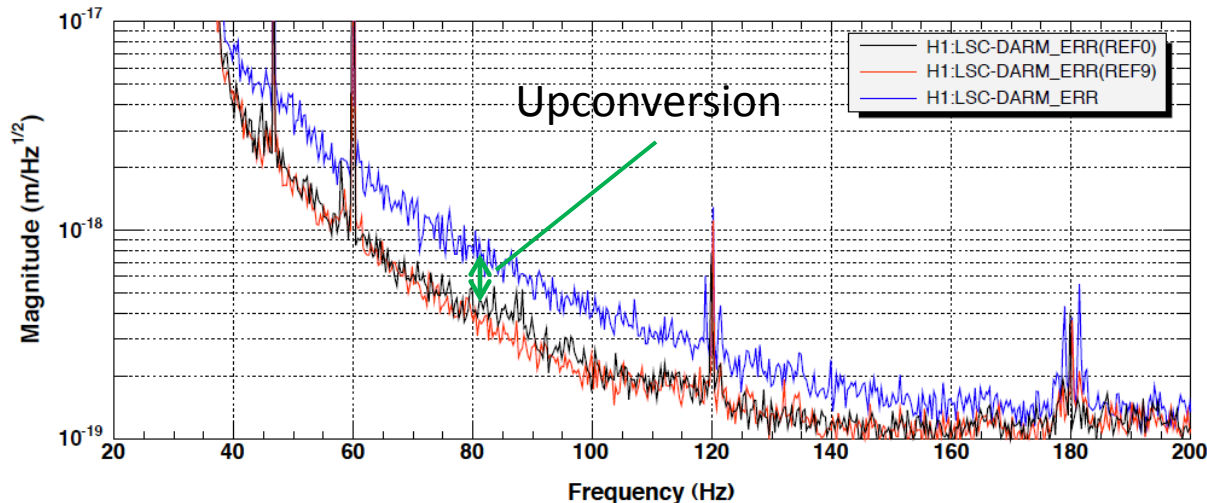
Feb. 2006



Mechanisms for upconversion:

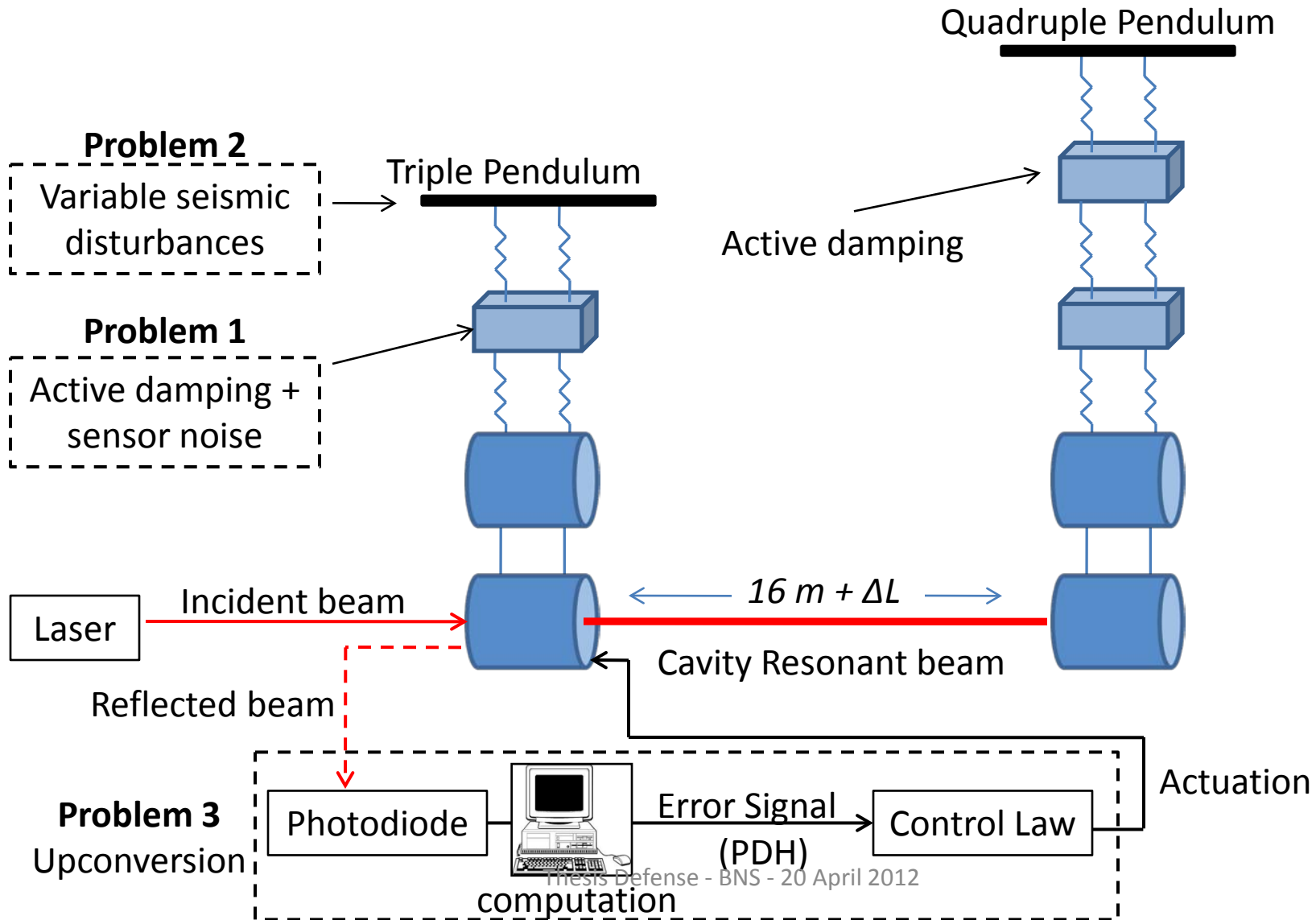
1. Laser beams falling off mirrors
2. Laser scattering off vacuum walls and other objects
3. Interferometer readout method
4. Creak in pendulum springs
5. Actuator nonlinearities
6. ?
7. etc

Same color scheme



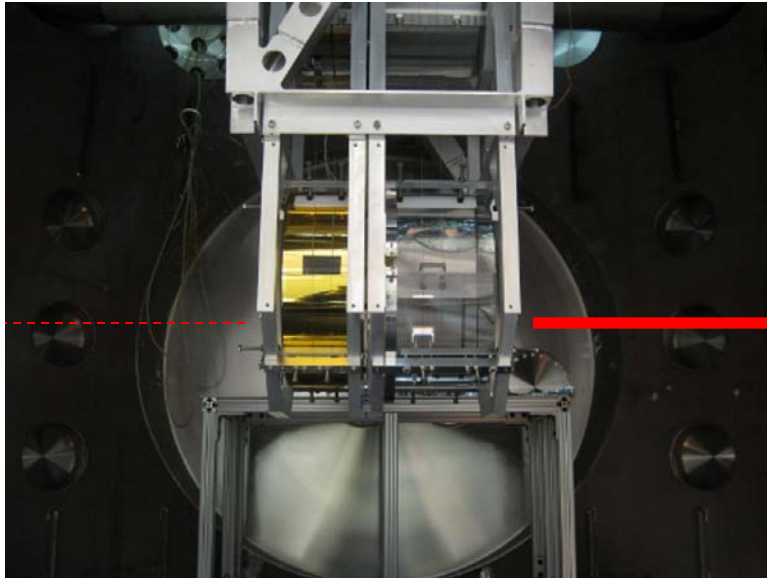


# Experimental Setup at MIT

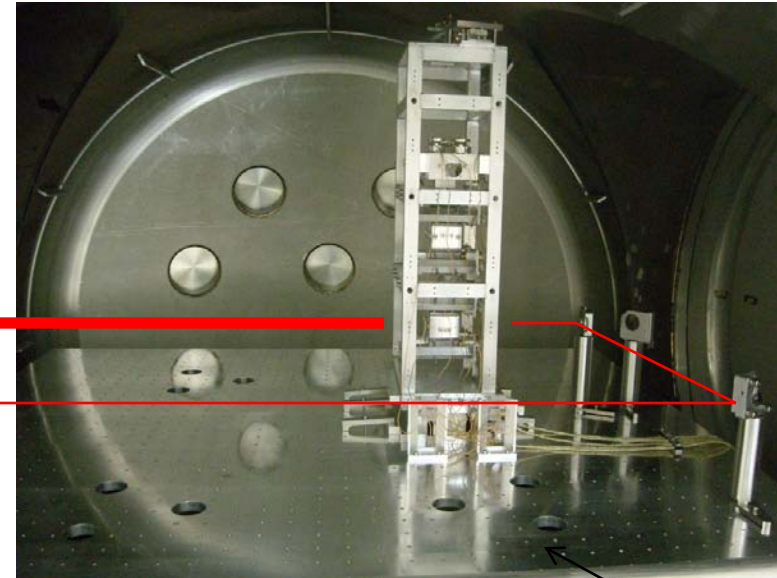


# Experimental Setup at MIT

Quadruple Pendulum Mirror



Triple Pendulum



1064 nm light

Laser

photodiode

16 meters

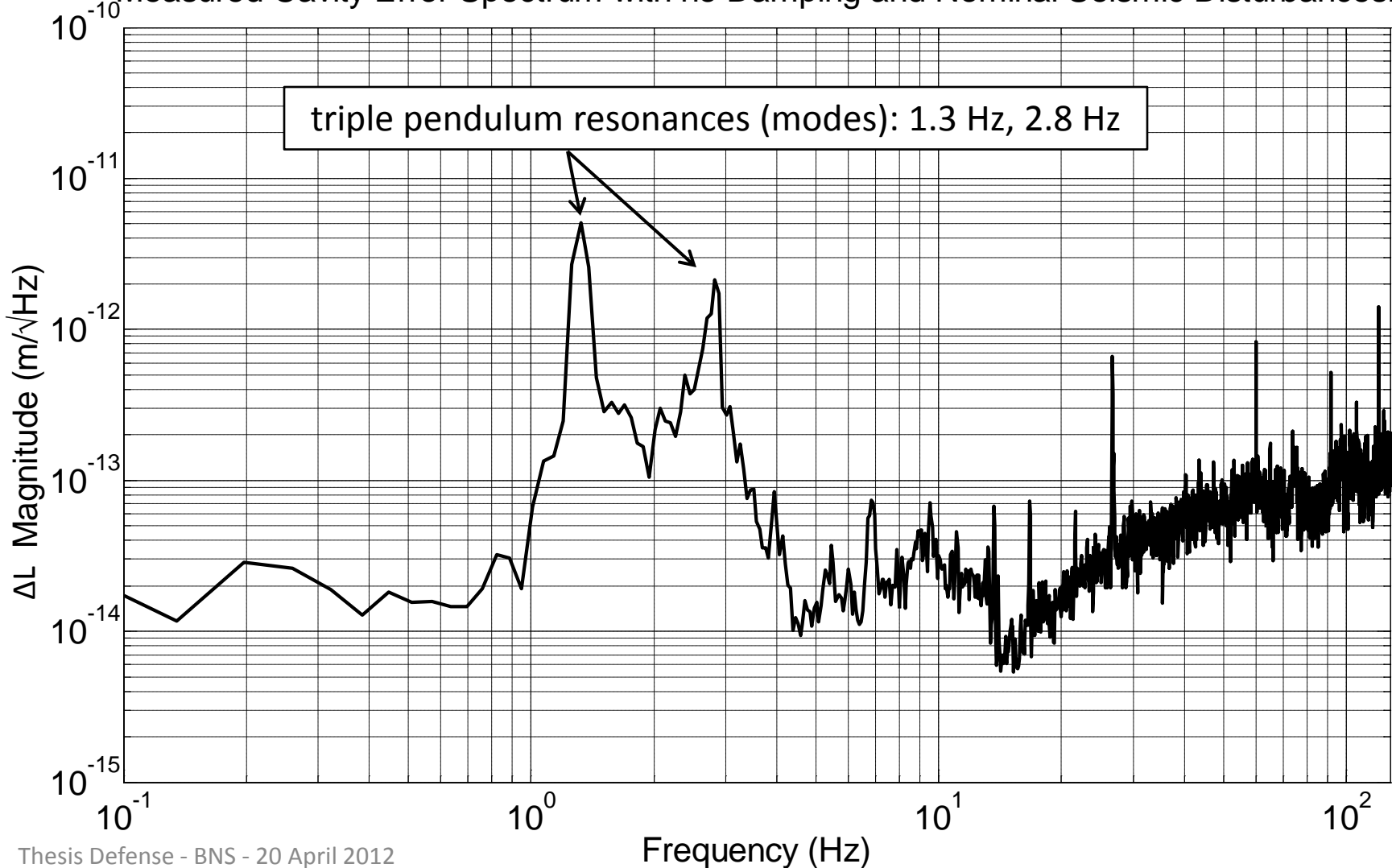
Shaking table

50 ppm light transmission  
through quad mirror

1% light transmission  
through triple mirror

# Measured Displacement Spectrum

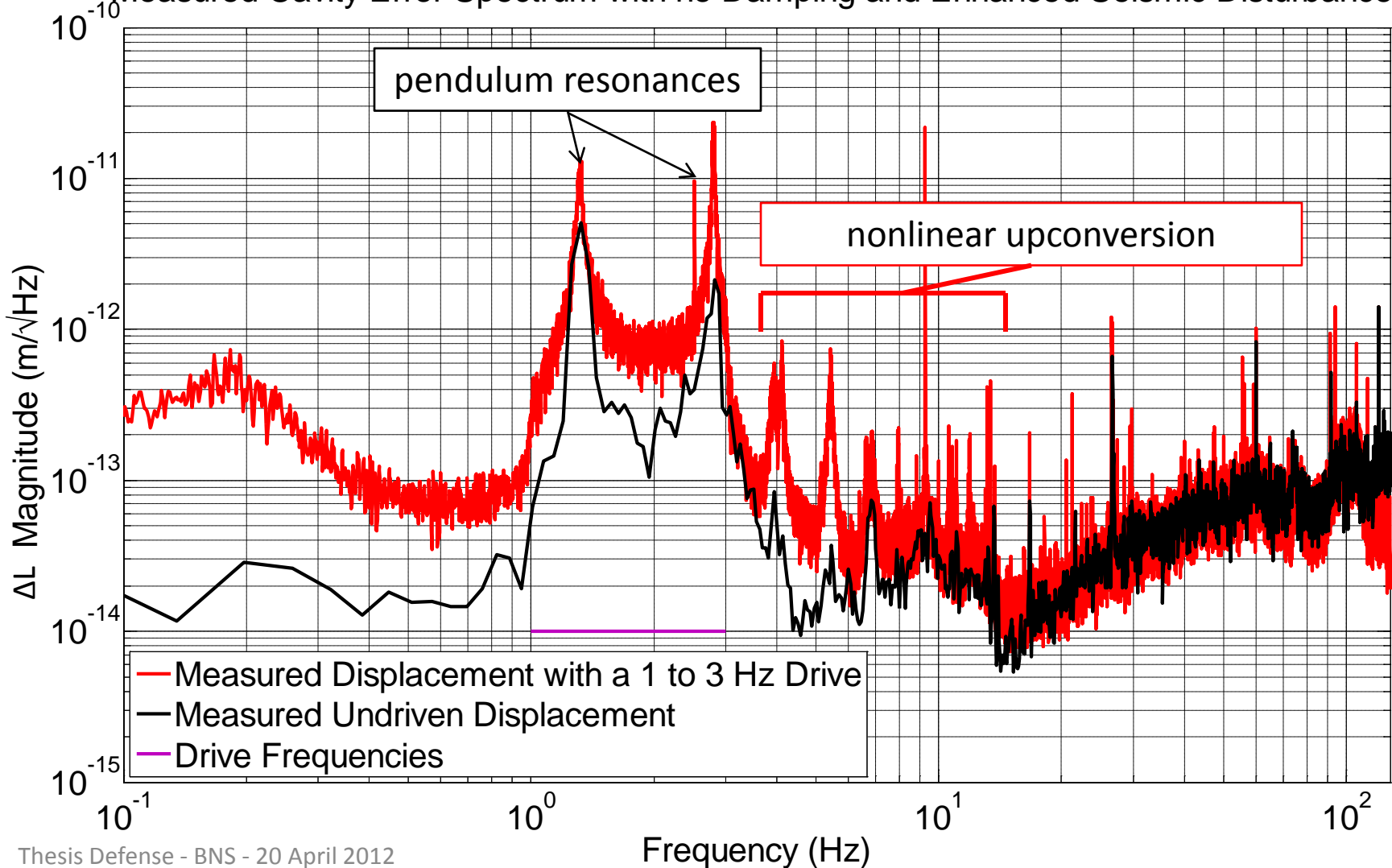
Measured Cavity Error Spectrum with no Damping and Nominal Seismic Disturbances.





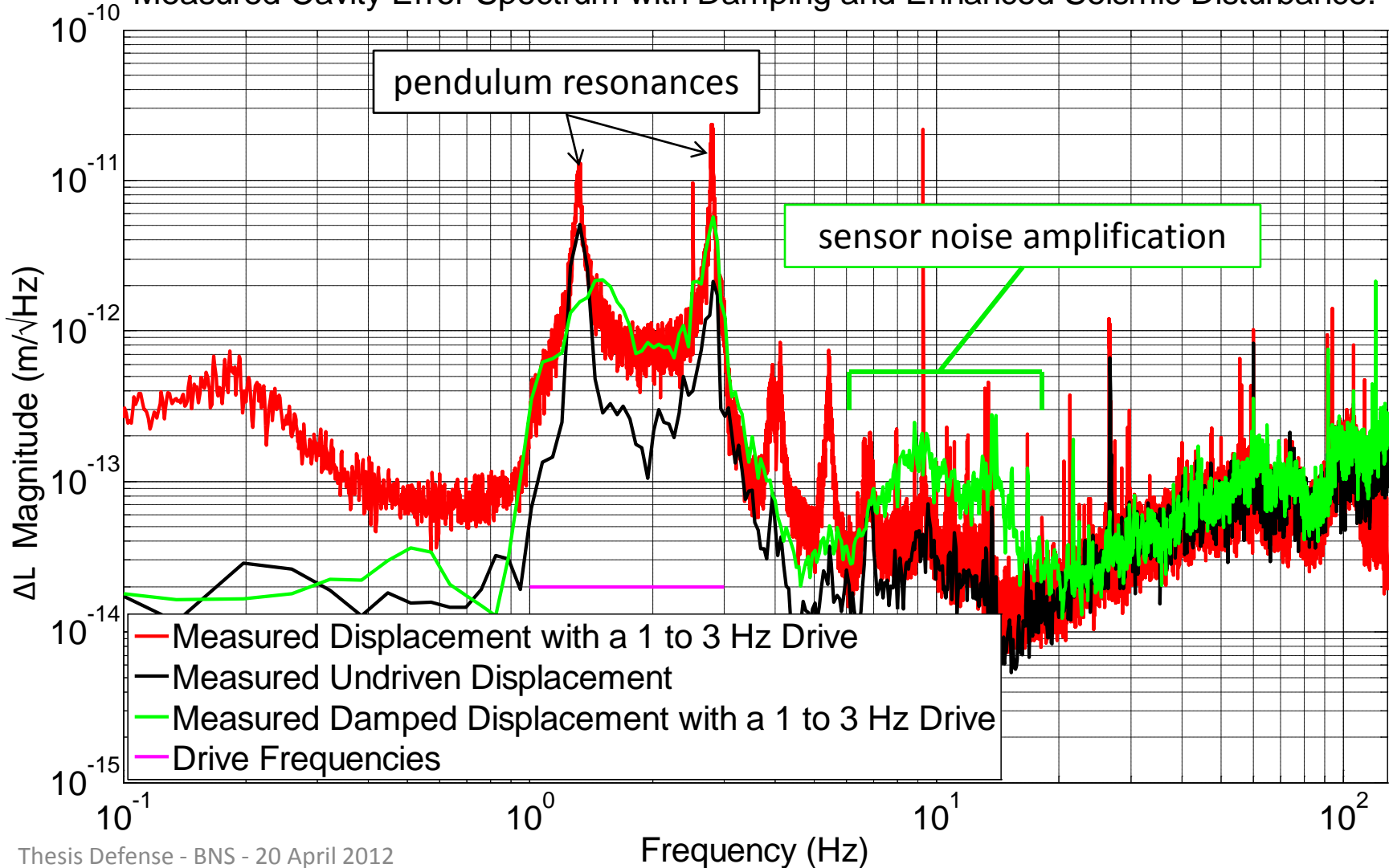
# Measured Displacement Spectrum

Measured Cavity Error Spectrum with no Damping and Enhanced Seismic Disturbance.

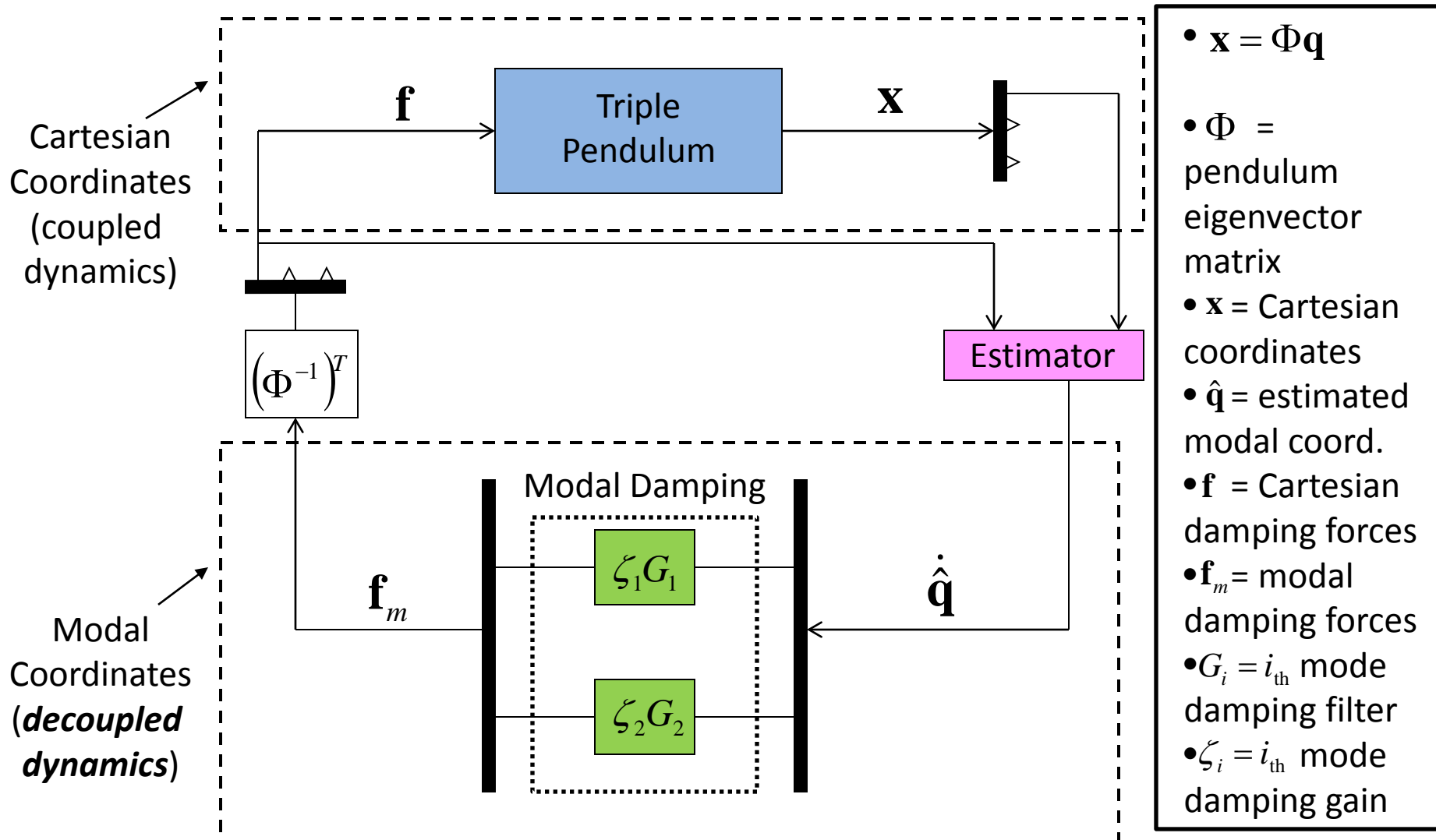


# Measured Displacement Spectrum

Measured Cavity Error Spectrum with Damping and Enhanced Seismic Disturbance.



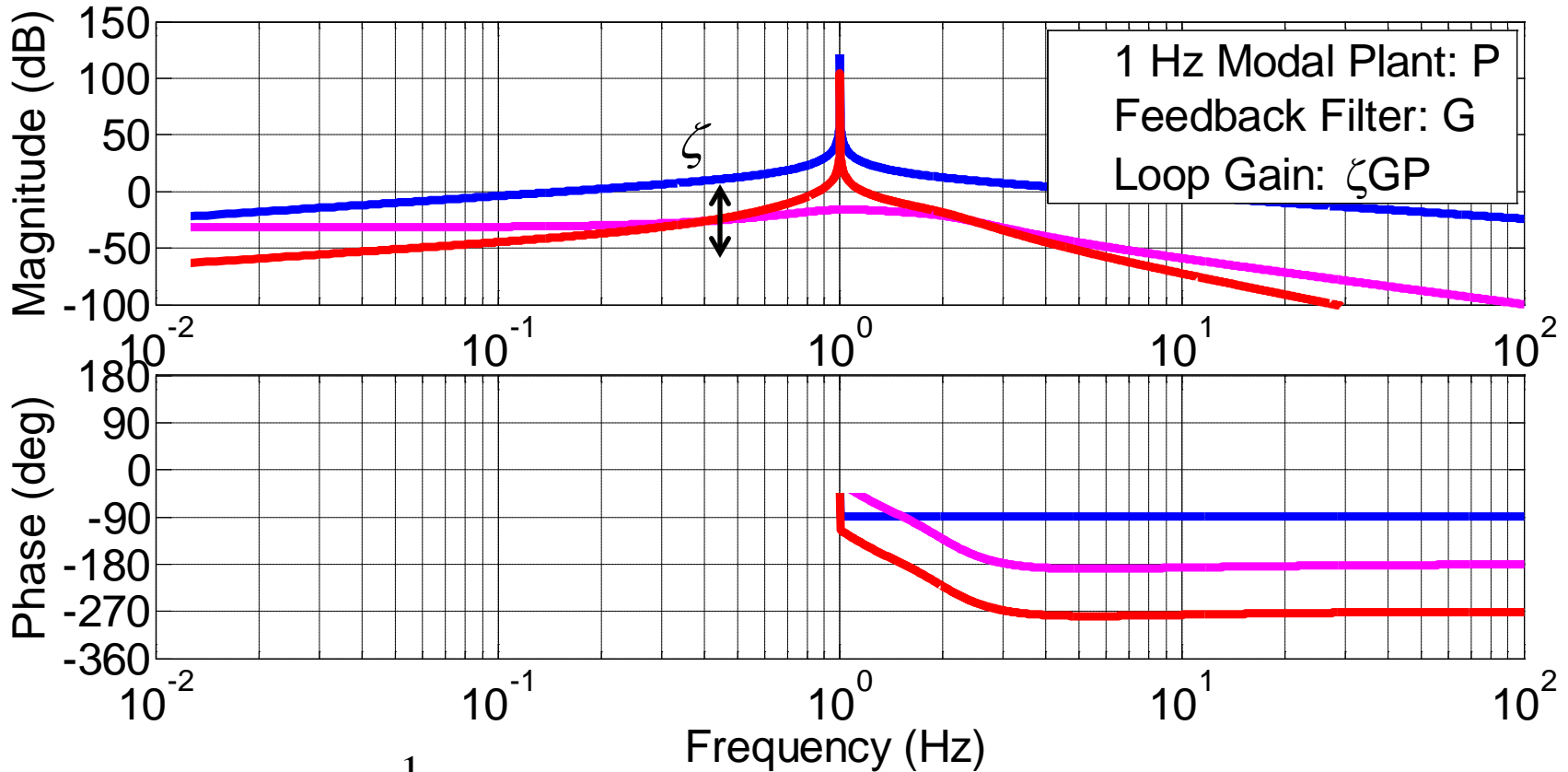
# Modal Damping with State Estimation



# Modal Feedback

Bode Diagram

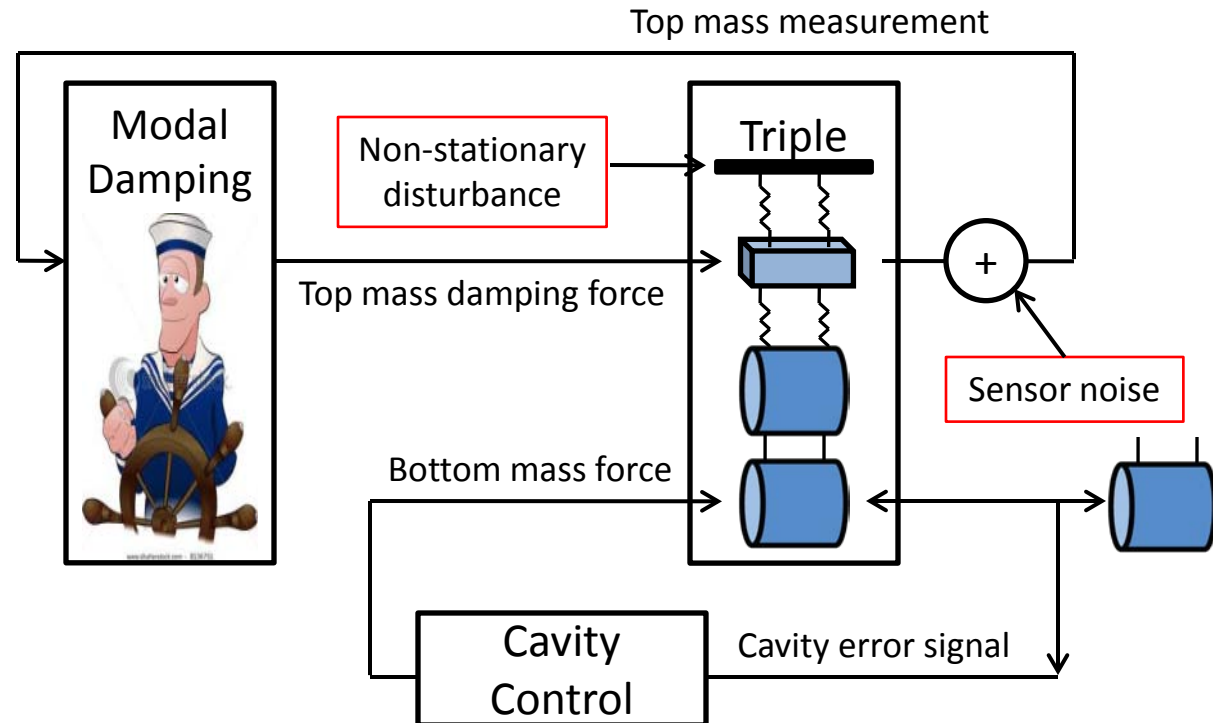
GM = 10.7 (1.53 Hz), PM = 38.2 (1.17 Hz)



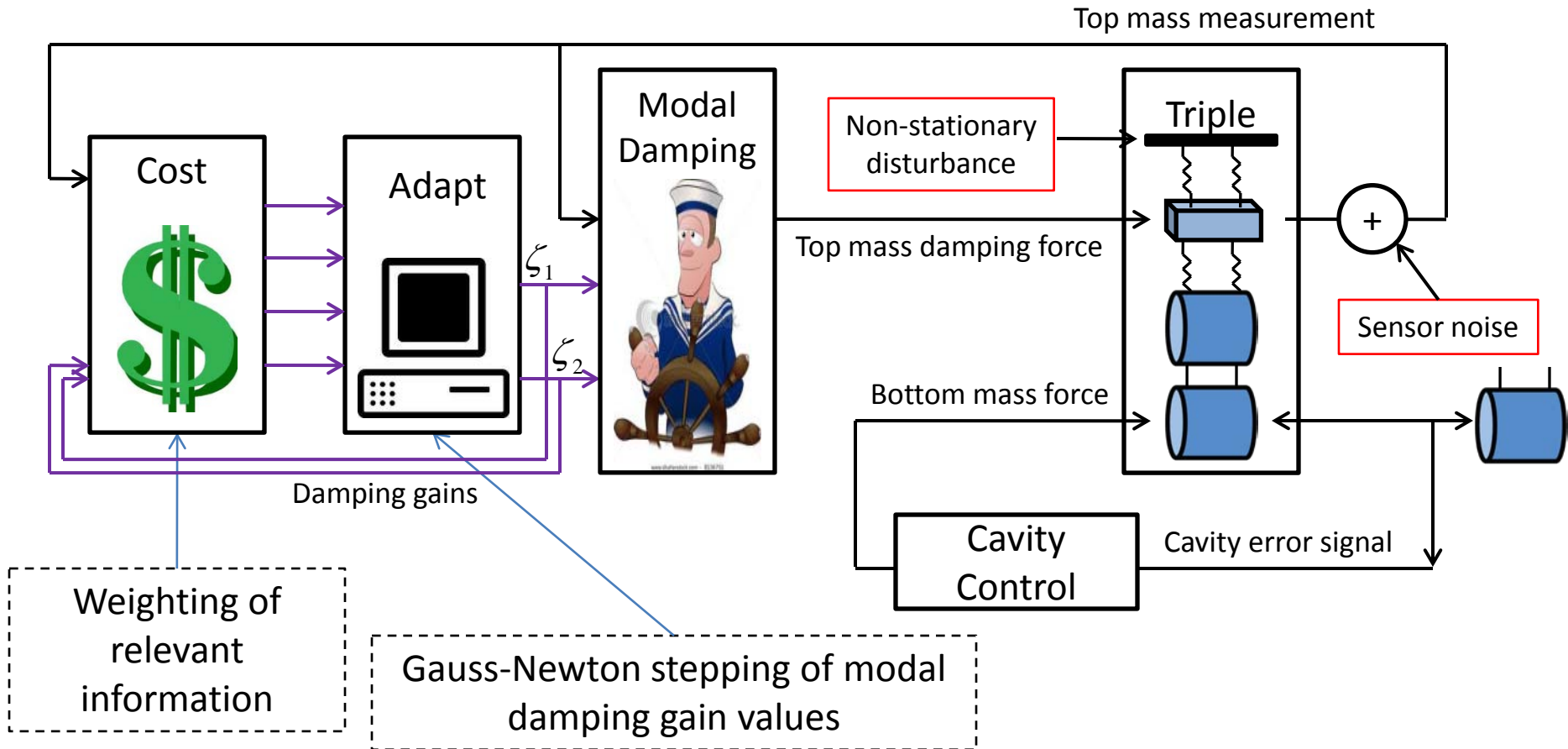
$$G = \frac{(s + \frac{1}{3}\omega_n)(s + 3\omega_n)}{(s^2 + \frac{2}{3}\omega_n s + \omega_n^2)(s^2 + 4\sin(20^\circ)\omega_n s + 4\omega_n^2)}, \quad 0 \leq \zeta < 1, \quad P = \frac{s}{s^2 + \omega_n^2}, \quad \omega_n = 2\pi$$



# Cavity Control with Modal Damping

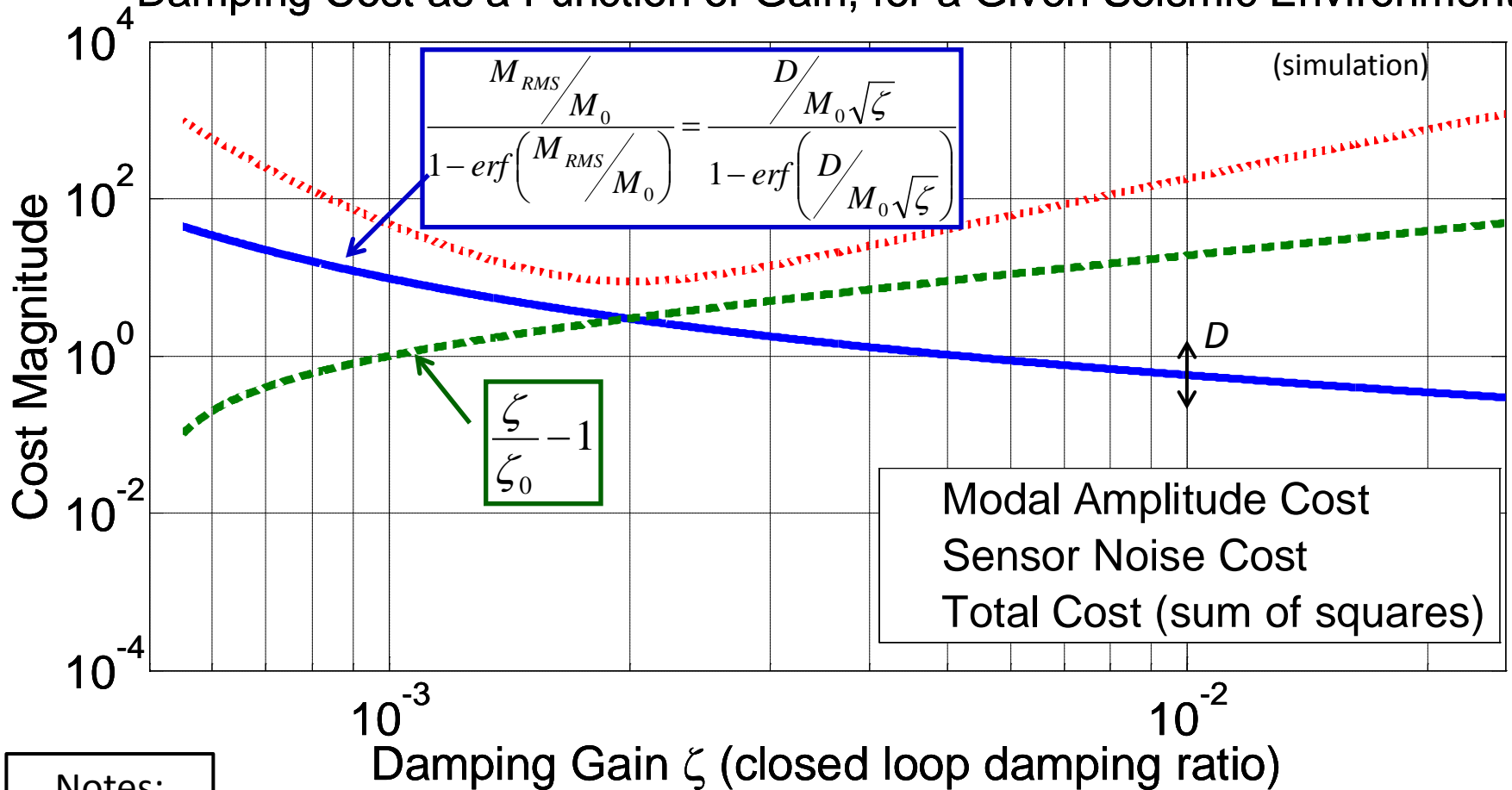


# Cavity Control with Adaptive M.D.



# Ex. Cost Gain Scaling Used in Exper.

Damping Cost as a Function of Gain, for a Given Seismic Environment



Notes:

$$M_{RMS} = \frac{D}{\sqrt{\zeta}}$$

$D$  = seismic amplitude at the modal frequency.

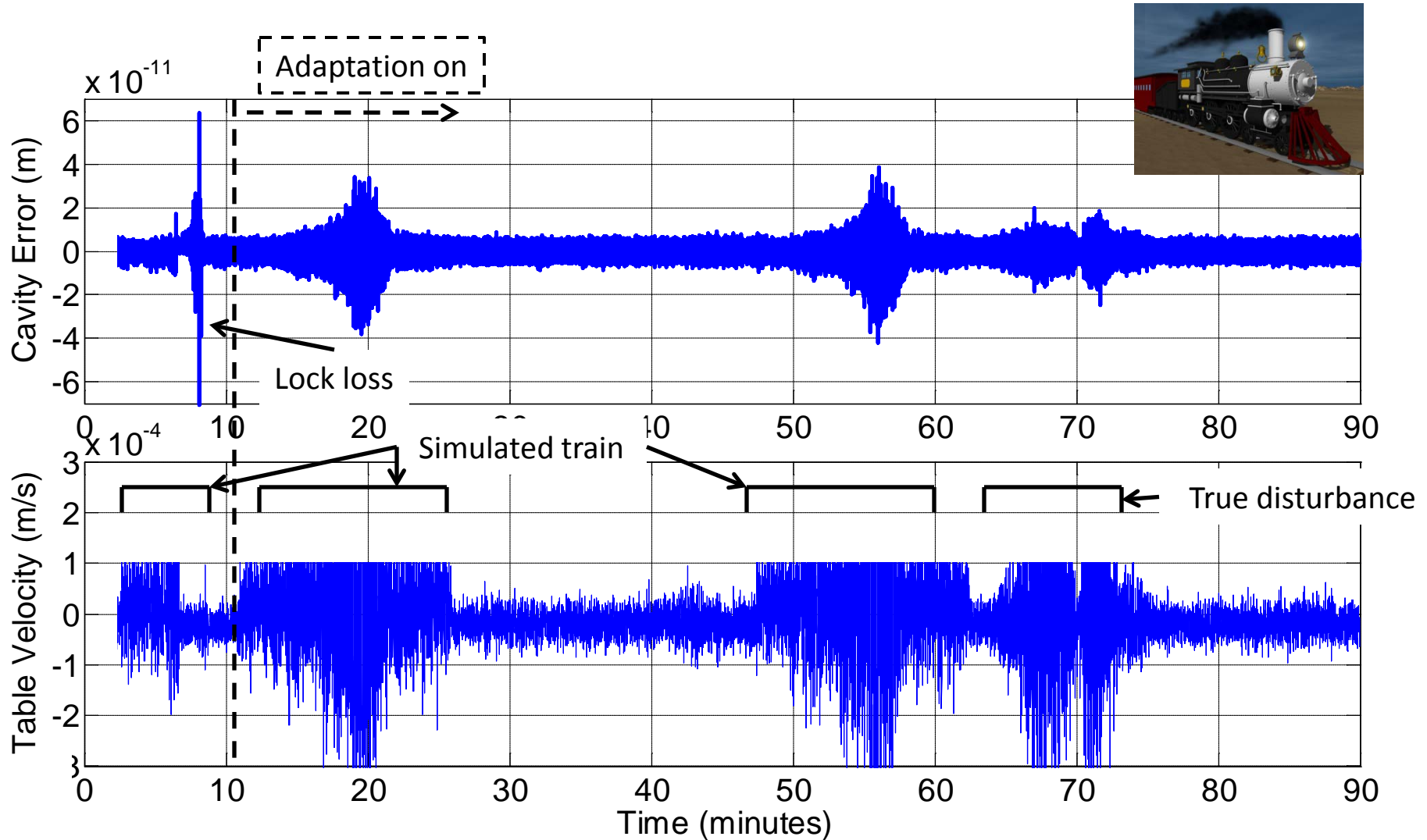
$M_{RMS}$  = measured modal amplitude

$M_0$  = constant scaling term

$\zeta_0$  = highest value where sensor noise is negligible.

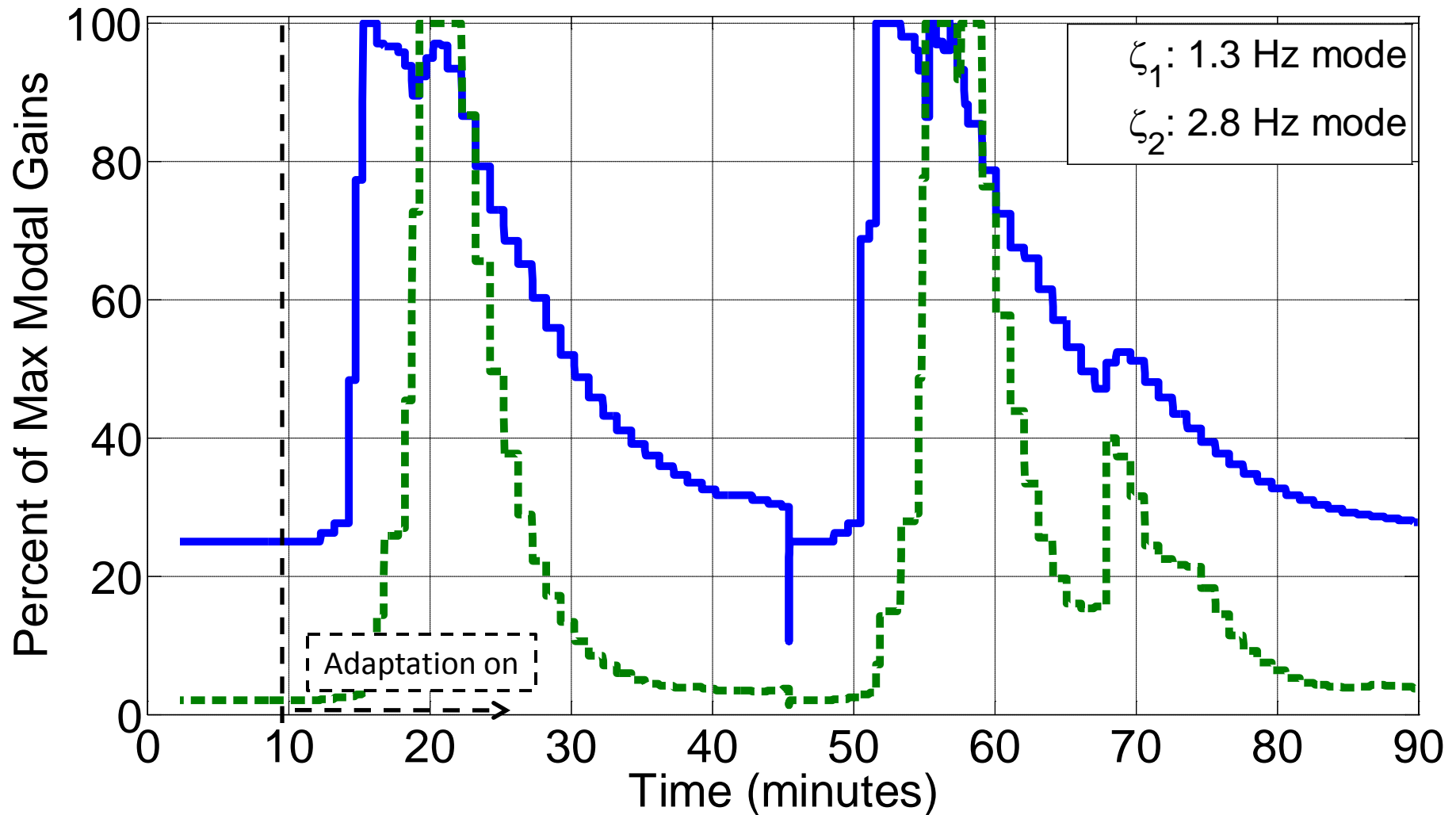
In this case,  $D = 0.53$ ,  $M_0 = 15$ , and  $\zeta_{ideal} = 5e-4$ .

# Measured Response to a 'Test' Train



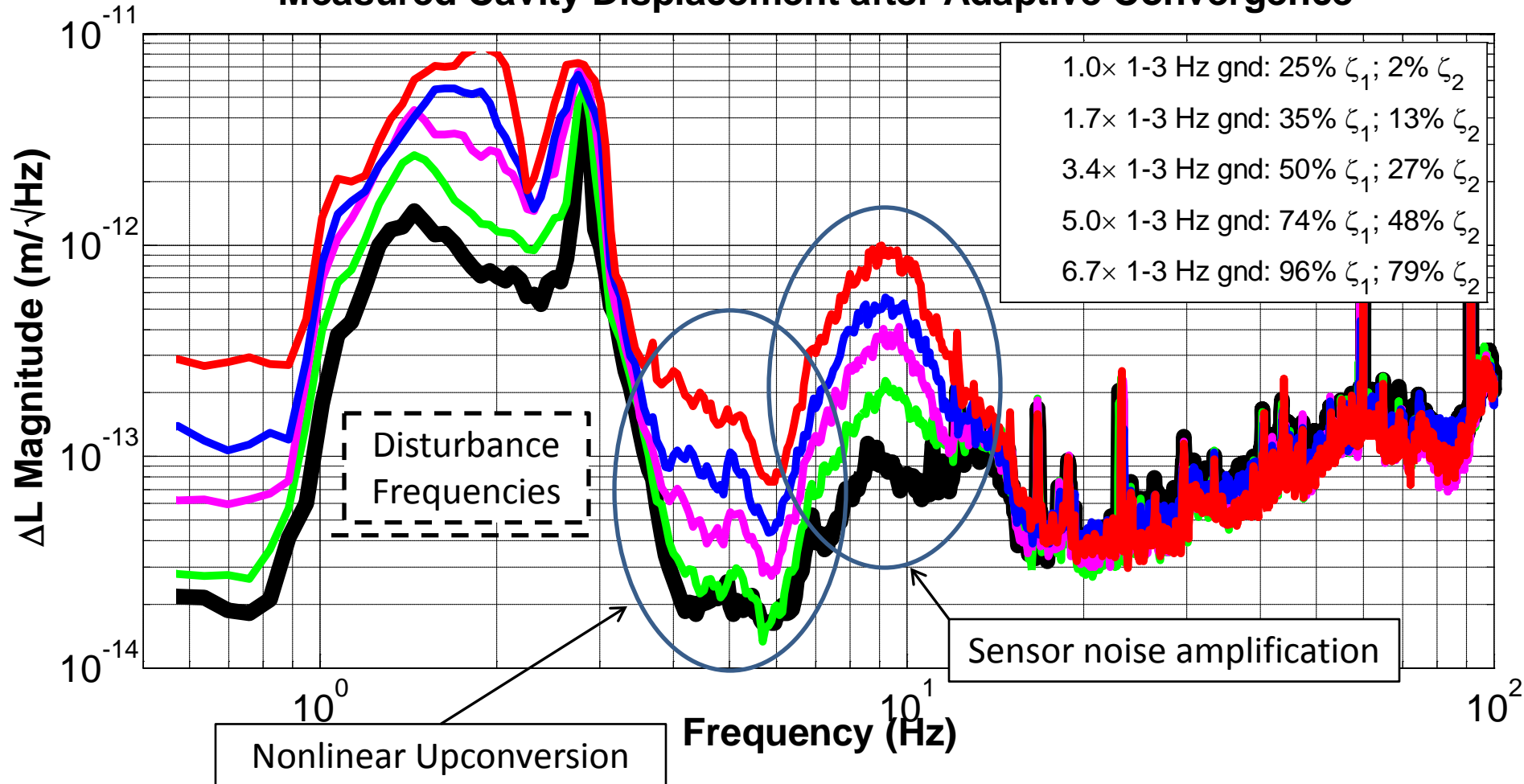


# Measured Response to a 'Test' Train



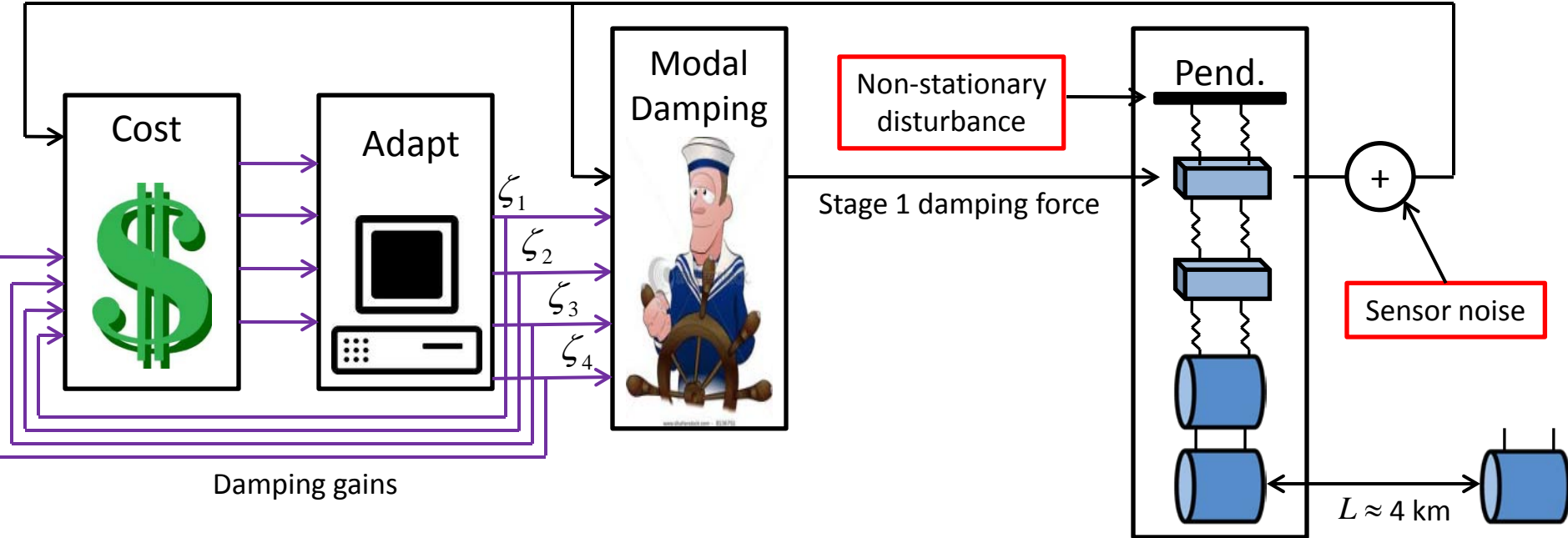
# Cavity Displacement Spectrum

Measured Cavity Displacement after Adaptive Convergence



# Simulation of LIGO cavity with AMD

Stage 1 measurement



$$\Delta \hat{L} = \Delta L - \frac{\Delta L^2}{8 \times 10^{-13} \text{ meters}}$$

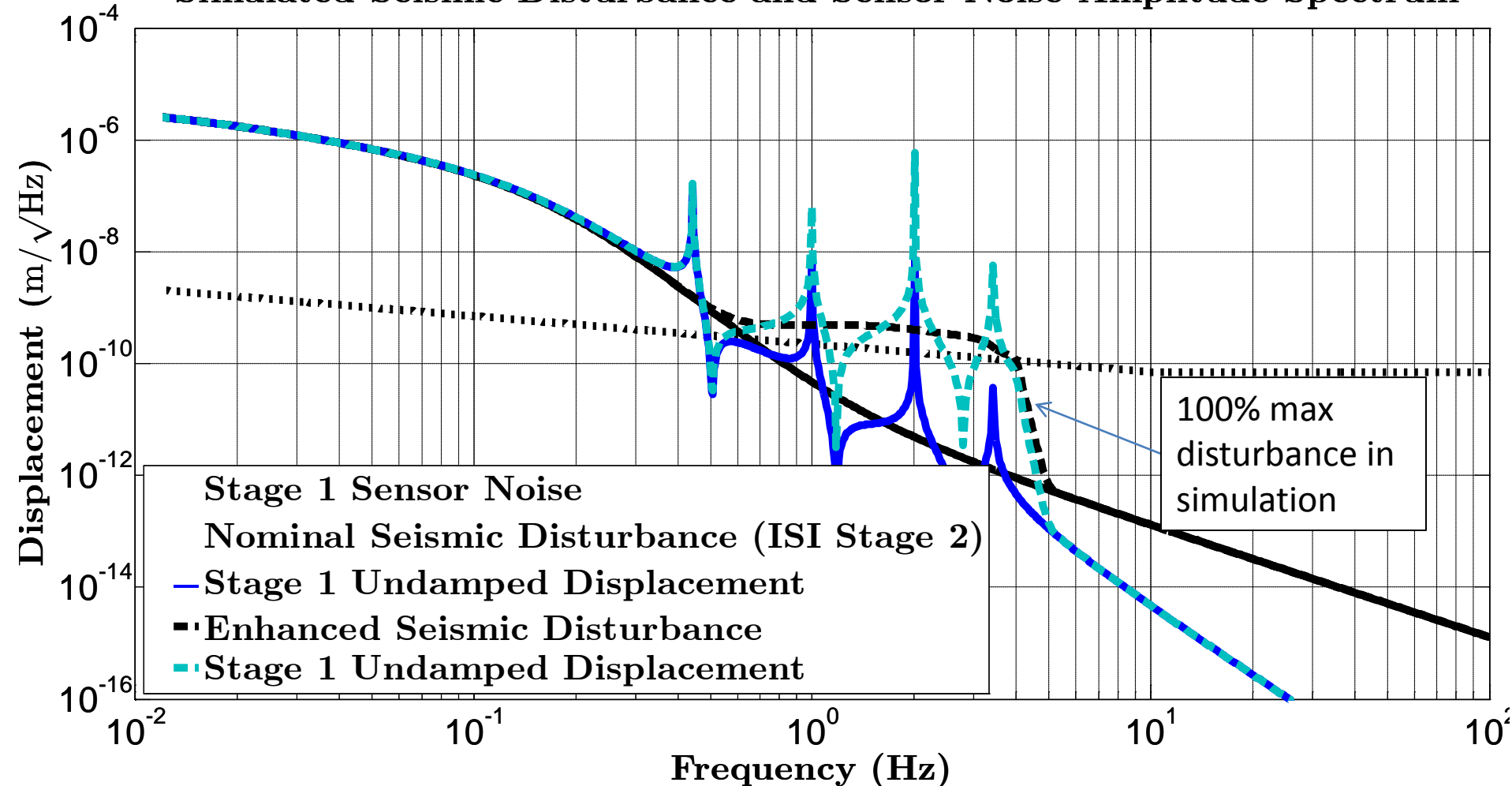
Interferometer signal w/  
nonlinear model

- To model the impact of AMD on LIGO's sensitivity to gravitational wave sources.

Assumption that  
 $\Delta L_{RMS} < 10^{-15}$  meters  
Removes nonlinearity

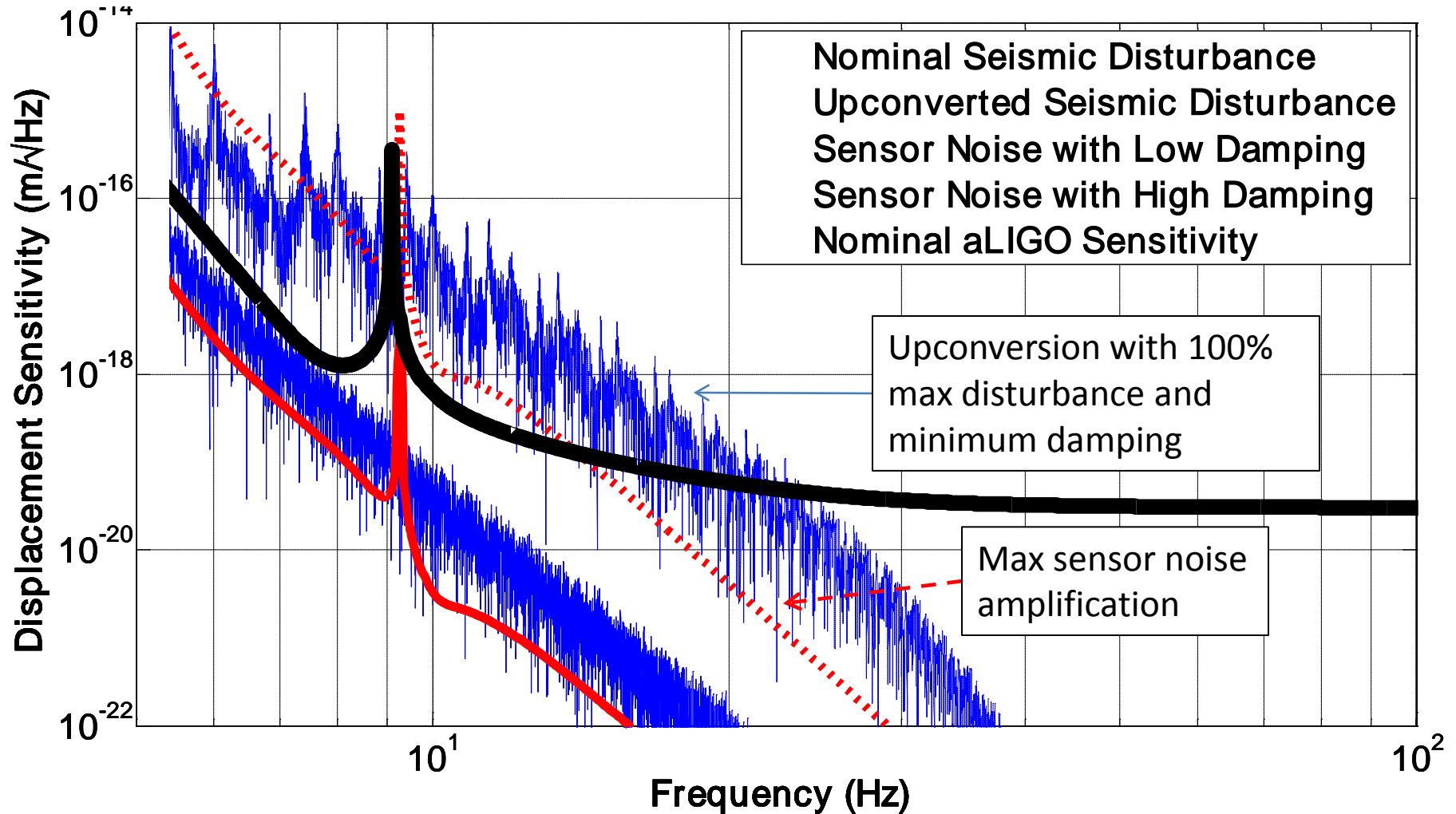
# Simulated Disturbance and Noise

Simulated Seismic Disturbance and Sensor Noise Amplitude Spectrum

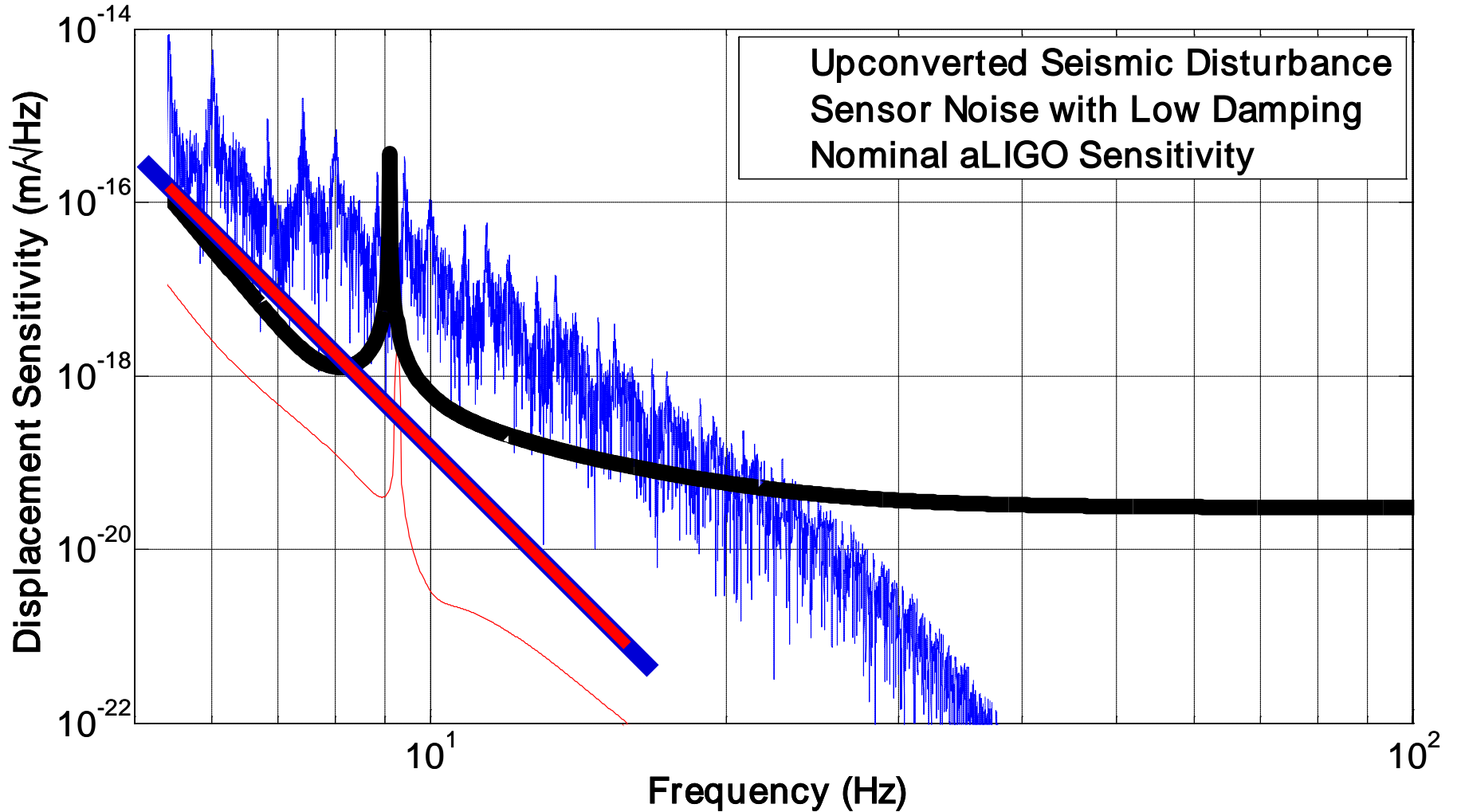




# Relative Noise Scaling

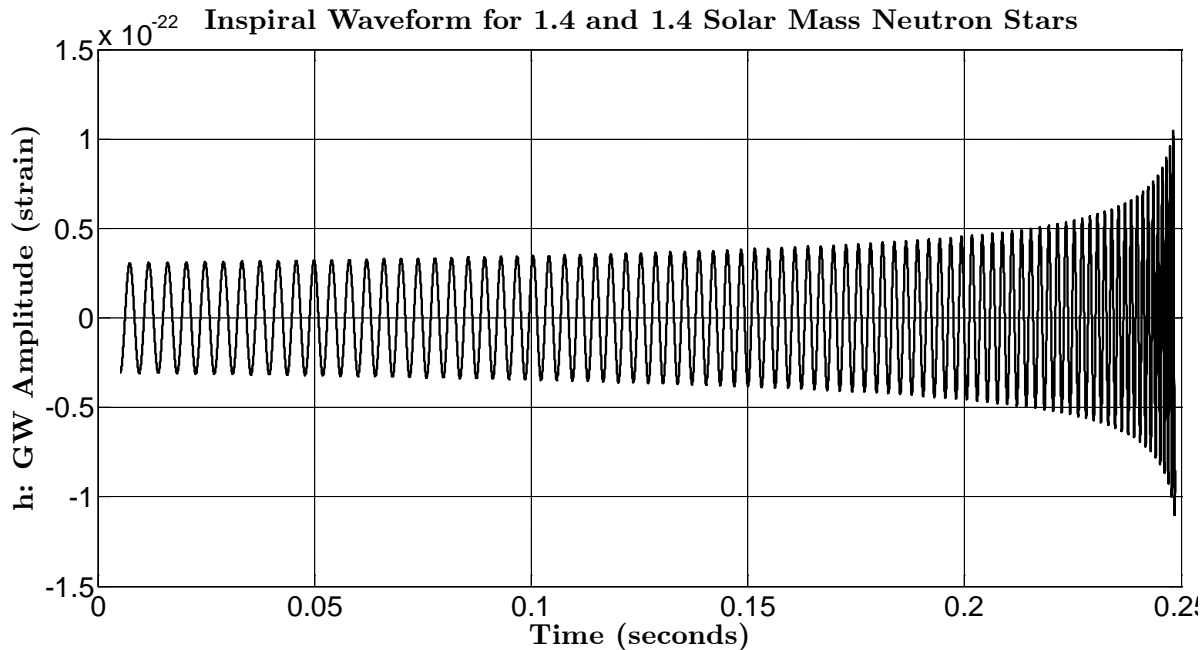


# Optimization Goal



# GW Source: Binary Inspiral

Inspirational Waveform for 1.4 and 1.4 Solar Mass Neutron Stars



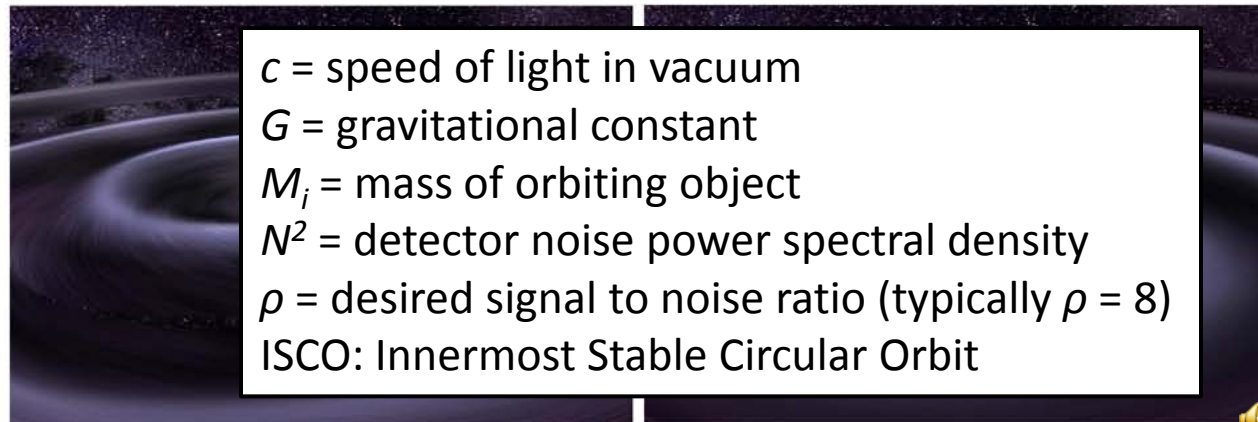
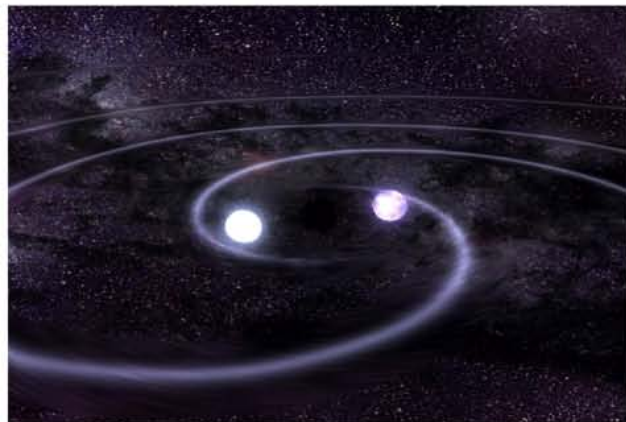
Detectable inspiral range  $r_{1,2}$

$$r^2 = 1.77^2 \frac{5c^{1/3} M^{5/3}}{96\pi^{4/3} \rho^2} \int_0^{f_{ISCO}} \frac{df}{f^{7/3} N^2}$$

$$M = \frac{G}{c^2} \frac{(M_1 M_2)^{3/5}}{(M_1 + M_2)^{1/5}}$$

$$f_{ISCO} = \frac{c^3}{6^{1.5} \pi G (M_1 + M_2)}$$

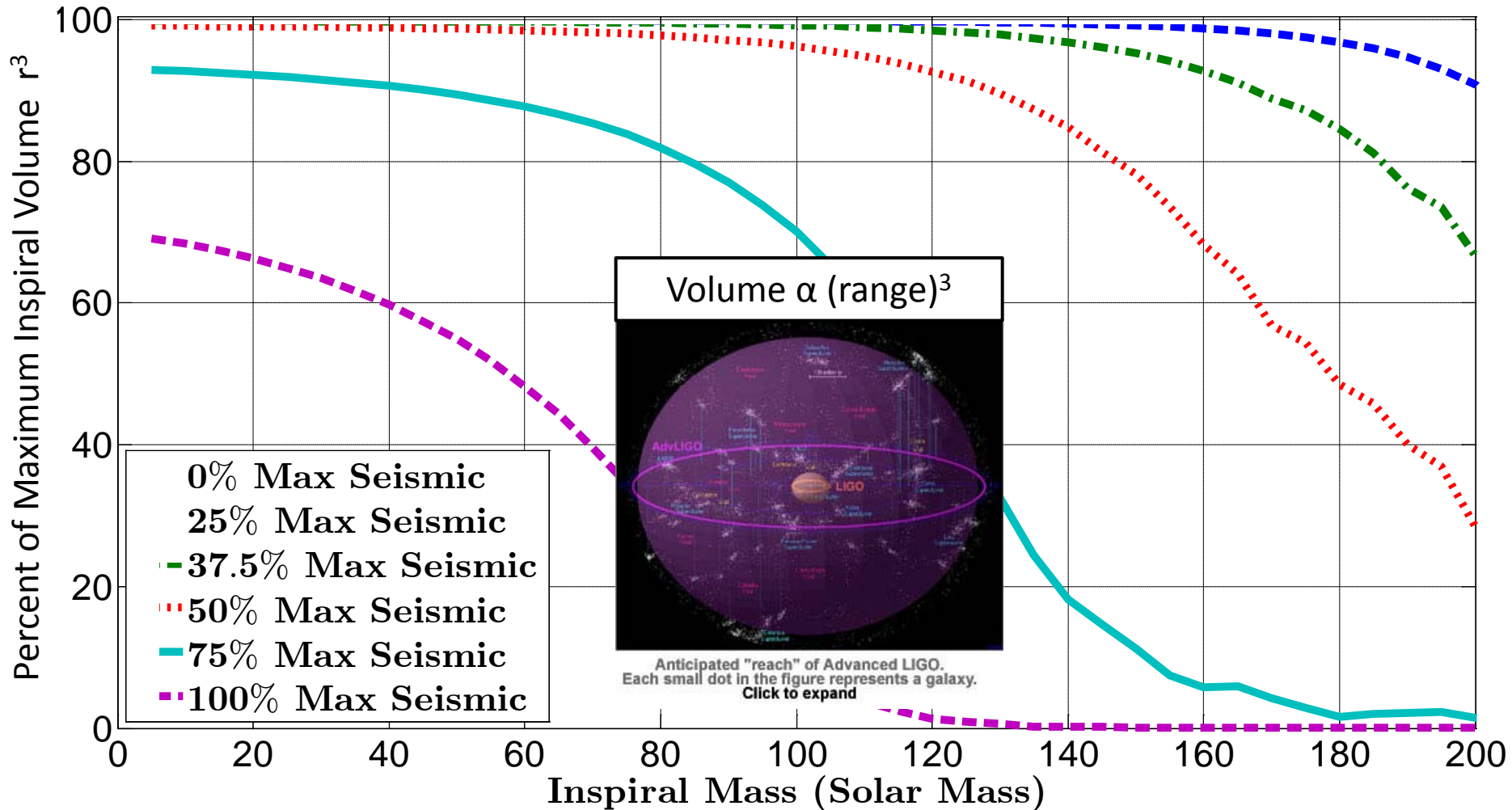
- 1 Patrick Sutton - T030276
- 2 Duncan Brown PhD thesis



$c$  = speed of light in vacuum  
 $G$  = gravitational constant  
 $M_i$  = mass of orbiting object  
 $N^2$  = detector noise power spectral density  
 $\rho$  = desired signal to noise ratio (typically  $\rho = 8$ )  
 ISCO: Innermost Stable Circular Orbit

# Visible Universe vs Binary Mass

Increasing seismic amplitude with no damping



Click for more info

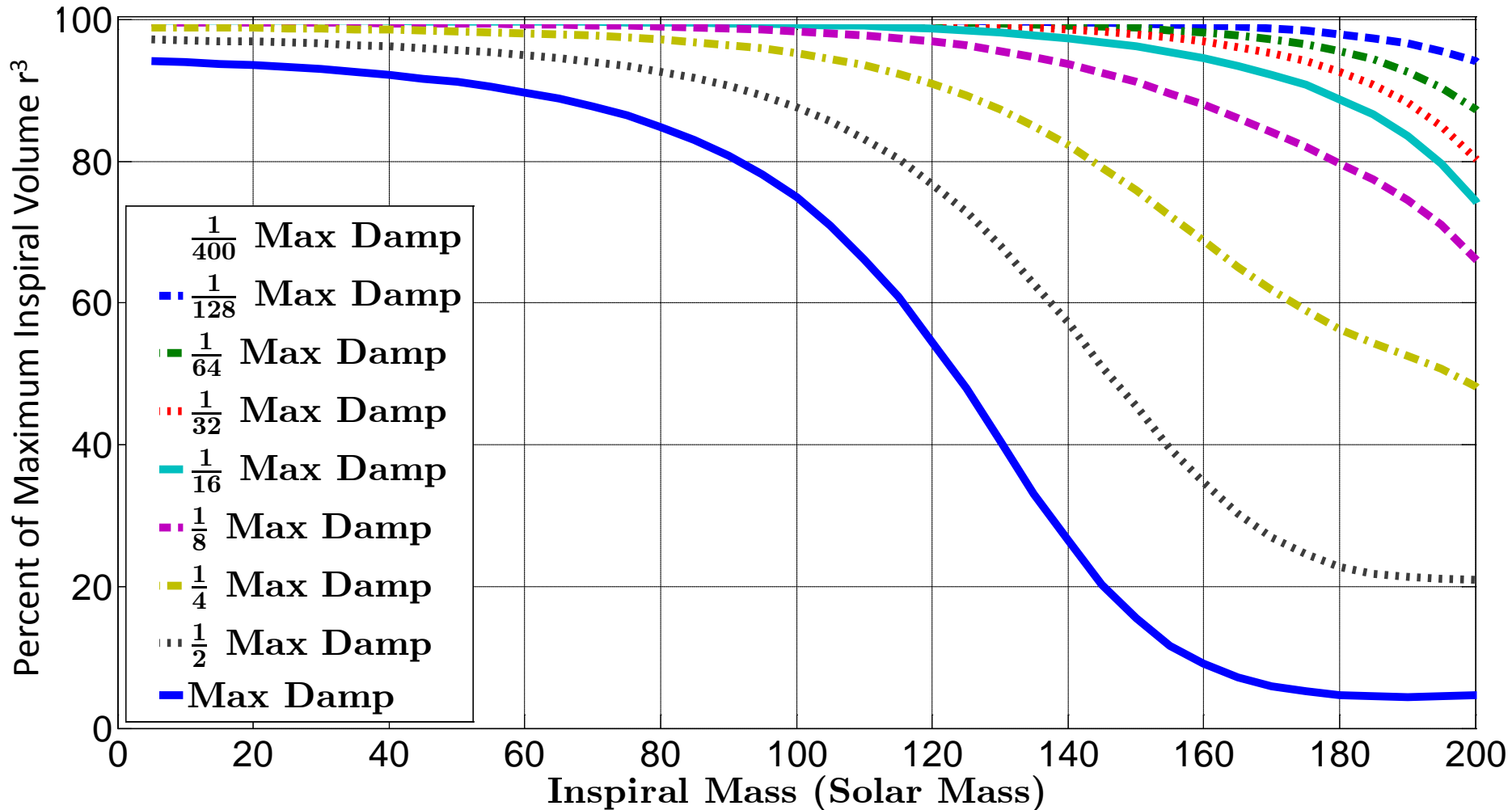
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36



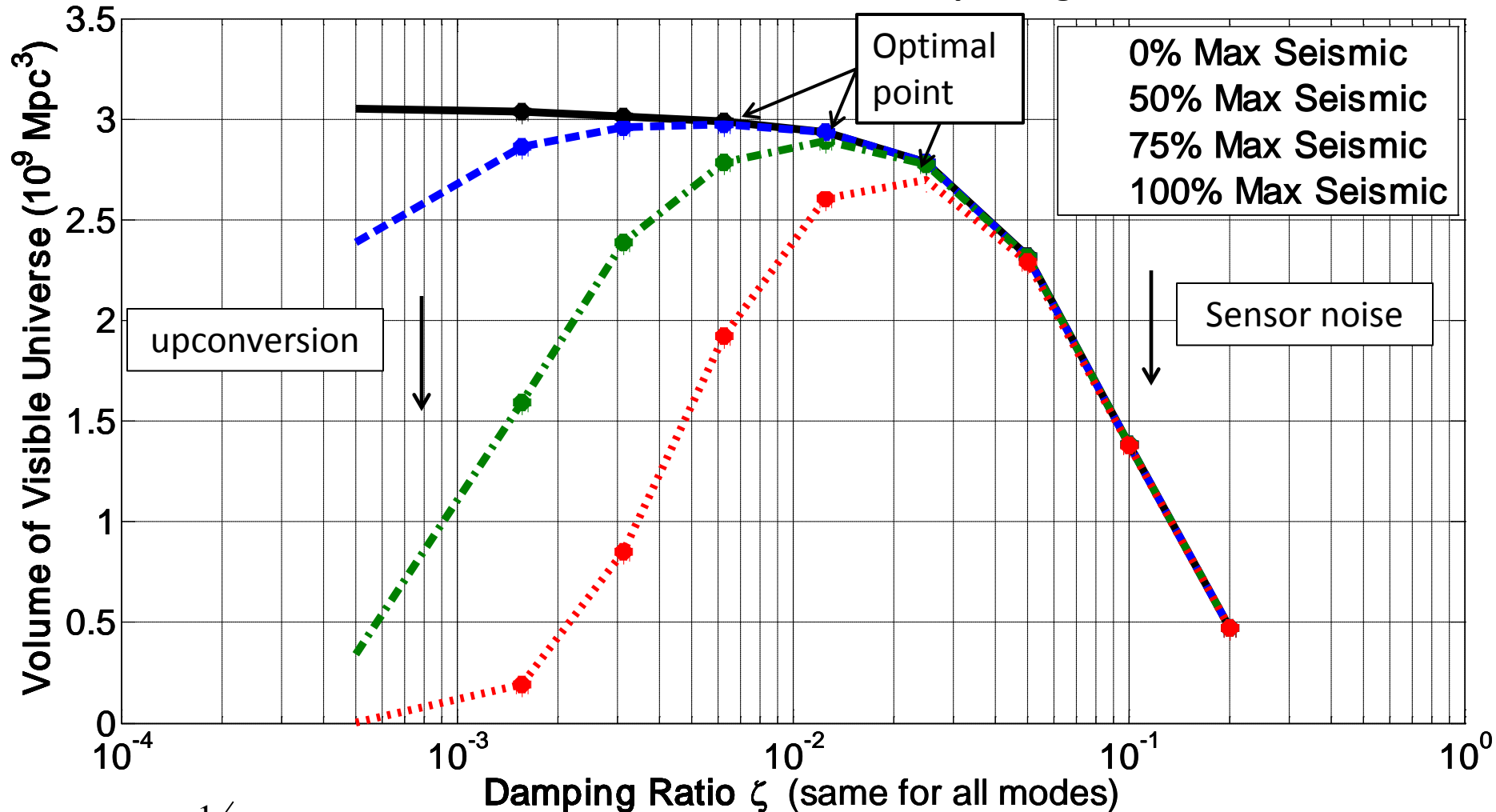
# Visible Universe vs Binary Mass

Increasing damping with nominal low seismic amplitude



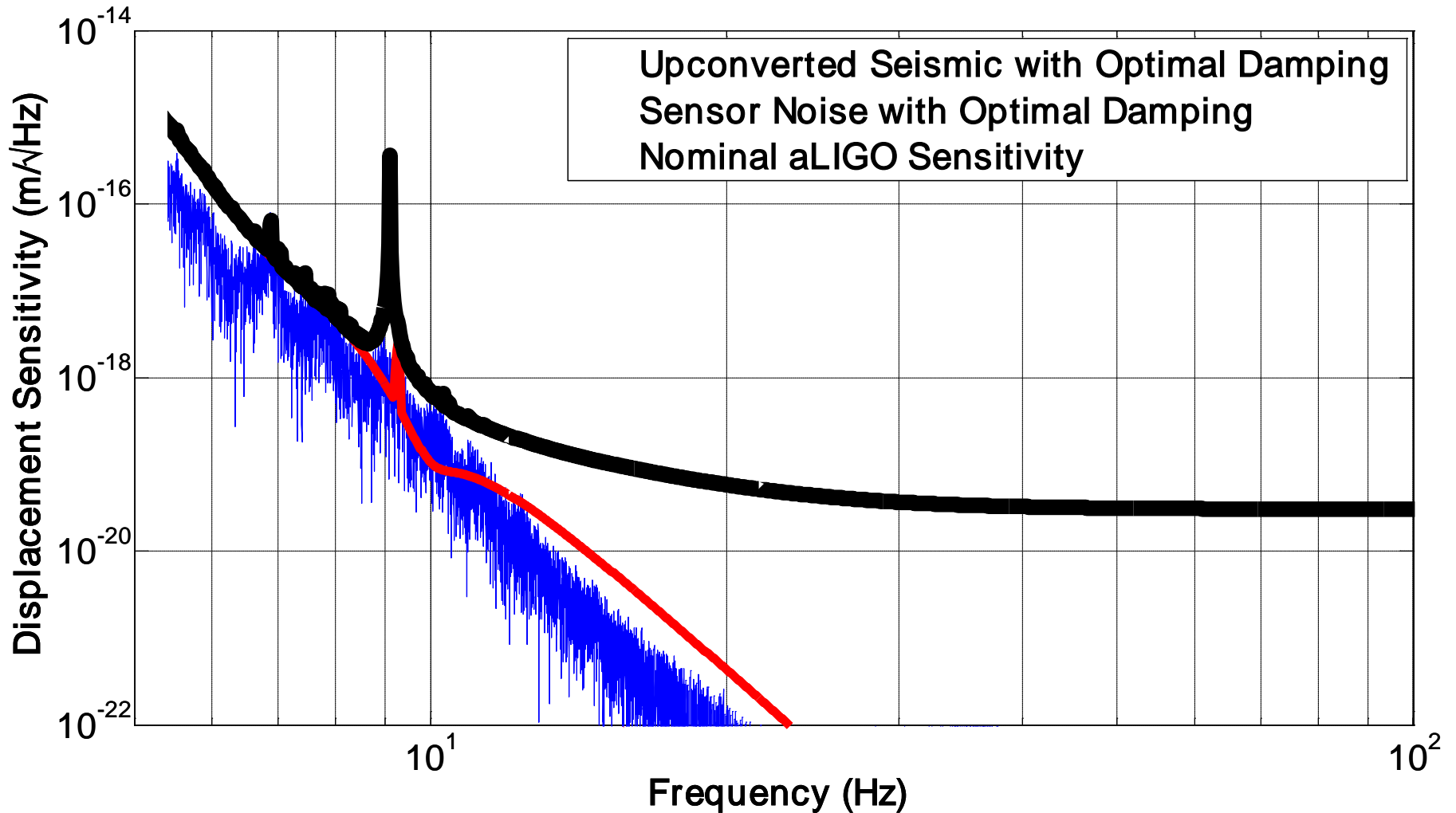
# Combining Seismic and Sensor Noise

Visible Universe for two 150 Solar Mass Inspiring Black Holes

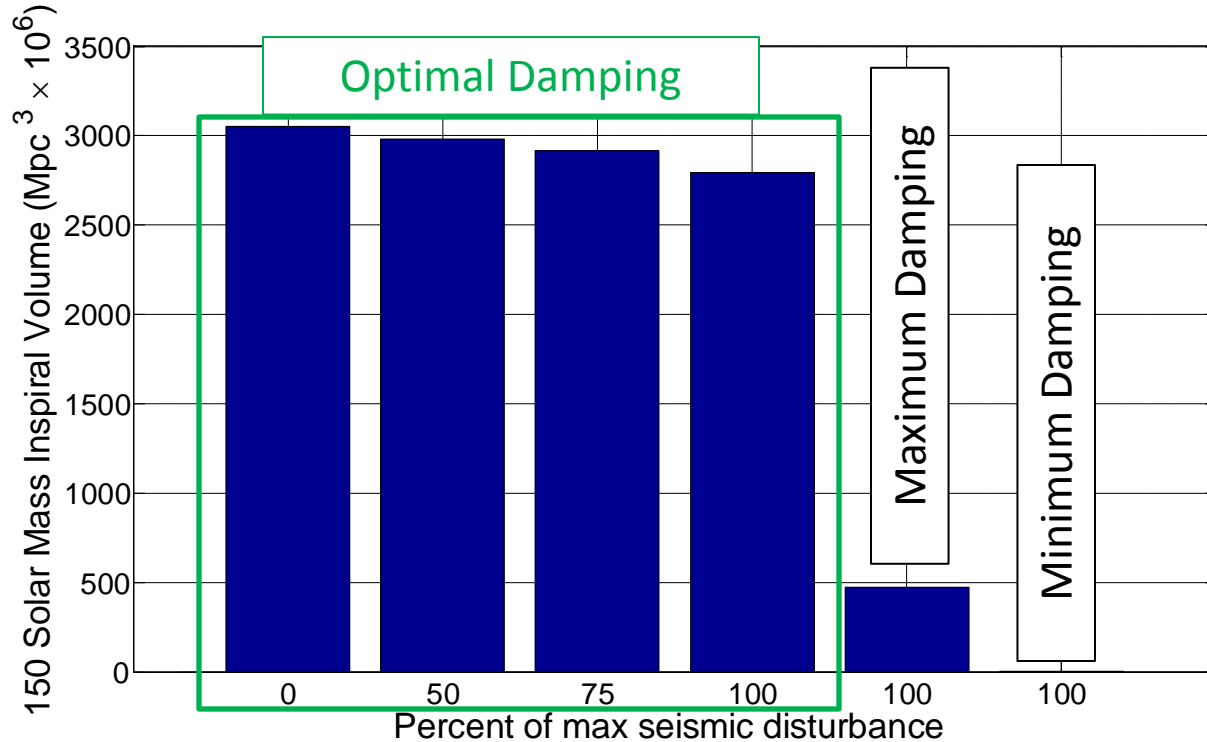


Note:  $\zeta = 1/2Q$ , Q = quality factor

# Optimal Damping for Max Seismic with Adaptation



# AMD Inspiral Simulation Results



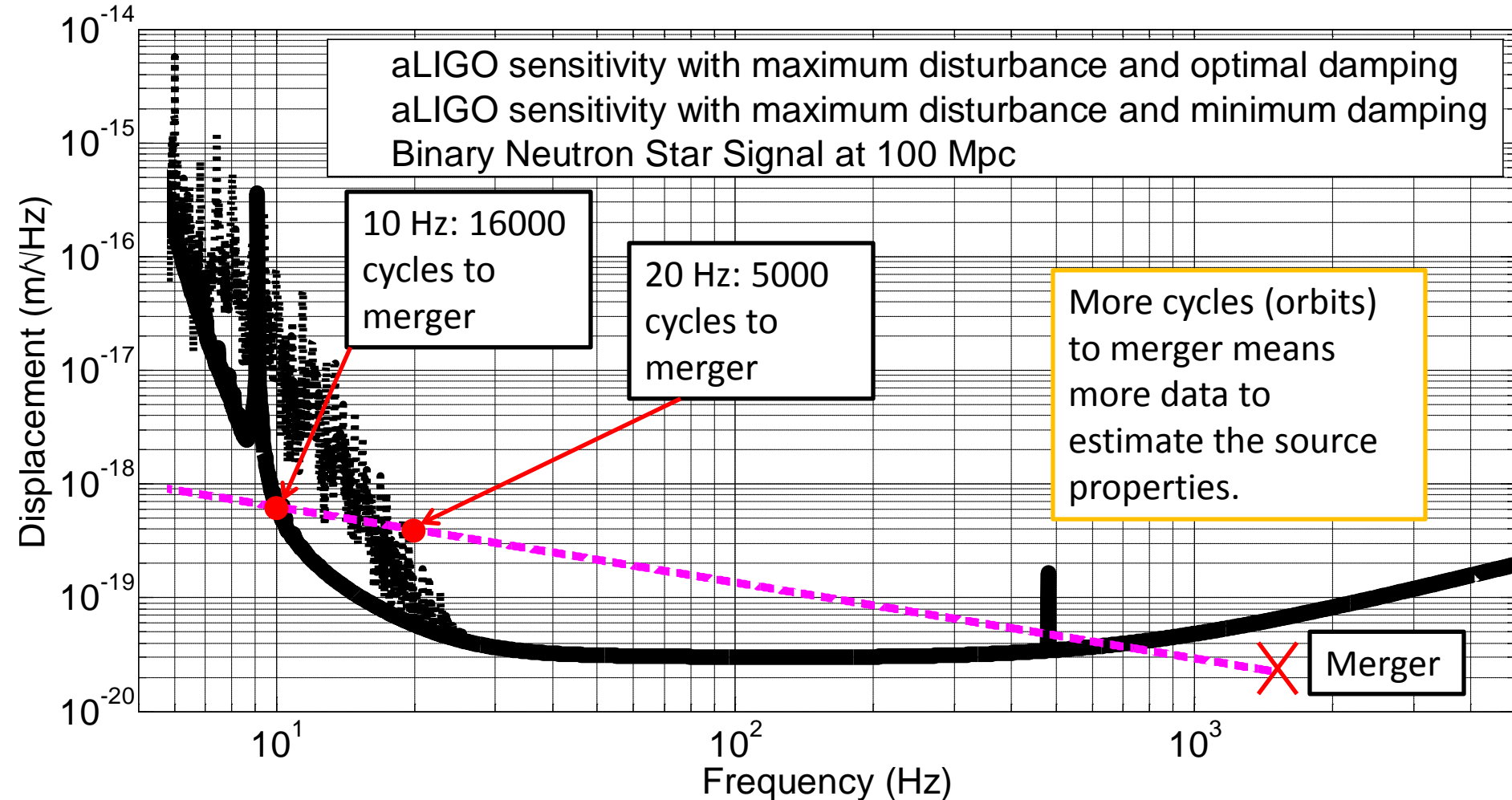
Seismic % of max	$\zeta_1$	$\zeta_2$	$\zeta_3$	$\zeta_4$	150 SM volume Mpc <sup>3</sup> × 10 <sup>6</sup>
0	0.00054	0.00055	0.00051	0.00050	3051 (100%)
50	0.00059	0.0051	0.016	0.0042	2982 (97.7%)
75	0.00073	0.0089	0.029	0.0090	2915 (95.5%)
100	0.00091	0.014	0.046	0.016	2796 (91.6%)
100	0.20	0.20	0.20	0.20	473 (15.6%)
100	0.00050	0.00050	0.00050	0.00050	3.05 (0.1%)

Optimal Damping

Maximum Damping

Minimum Damping

# Binary Neutron Star Inspiral Sensitivity





# AMD Conclusions

- AMD has the power to select modal damping gains that are optimal to the detection of high mass black hole inspirals ( $> 75 M$ ) for a range of disturbances.
- Lower mass inspirals benefit by extending observation time.
- The same gains are also optimal for the stochastic background, pulsars, and supernovae. However, these sources are insensitive to the lowest frequencies, so constant maximum damping is likely to be more reliable.
- This work explored adaptive damping for the quad pendulum, but similar adaption could be useful in other LIGO control loops.
- Practical application of this work depends on the behavior of the true Advanced LIGO interferometers still under construction.

# Thesis Contributions, 1-2

- Adaptive algorithm for modal damping (AMD)
  - Adaptation optimizes the response in real-time to changing environmental conditions.
  - Switching of step rates, estimation time scales, and step sizes based on the measured proximity of these statistics to the optimal solution.
  - Easily adapted to other aspects of interferometer control.

# Thesis Contributions, 2-2

- Optimization of AMD for astrophysical sources
- Optimization and limitations of modal damping
  - Optimal state estimation (ACC 2011)
  - Maximum achievable closed loop damping
- Modeling – procedure for identifying most important measurements and parameter uncertainties of quadruple pendulum.
- Actuator sizing – min. least squares actuation required when driving many DOFs (ACC2012)

# Acknowledgements

## **Committee**

Nergis Mavalvala  
Richard Mittleman  
Jean-Jacques Slotine  
Kamal Youcef-Toumi

## **LIGO-MIT**

Lisa Barsotti  
Matt Evans  
Jeff Kissel  
Myron MacInnis  
David Shoemaker  
Sam Waldman  
Marie Woods

## **LIGO-Suspensions Group**

Mark Barton  
Norna Robertson  
Janeen Romie  
Ken Strain

## **MIT**

Scott Hughes

## **Family**

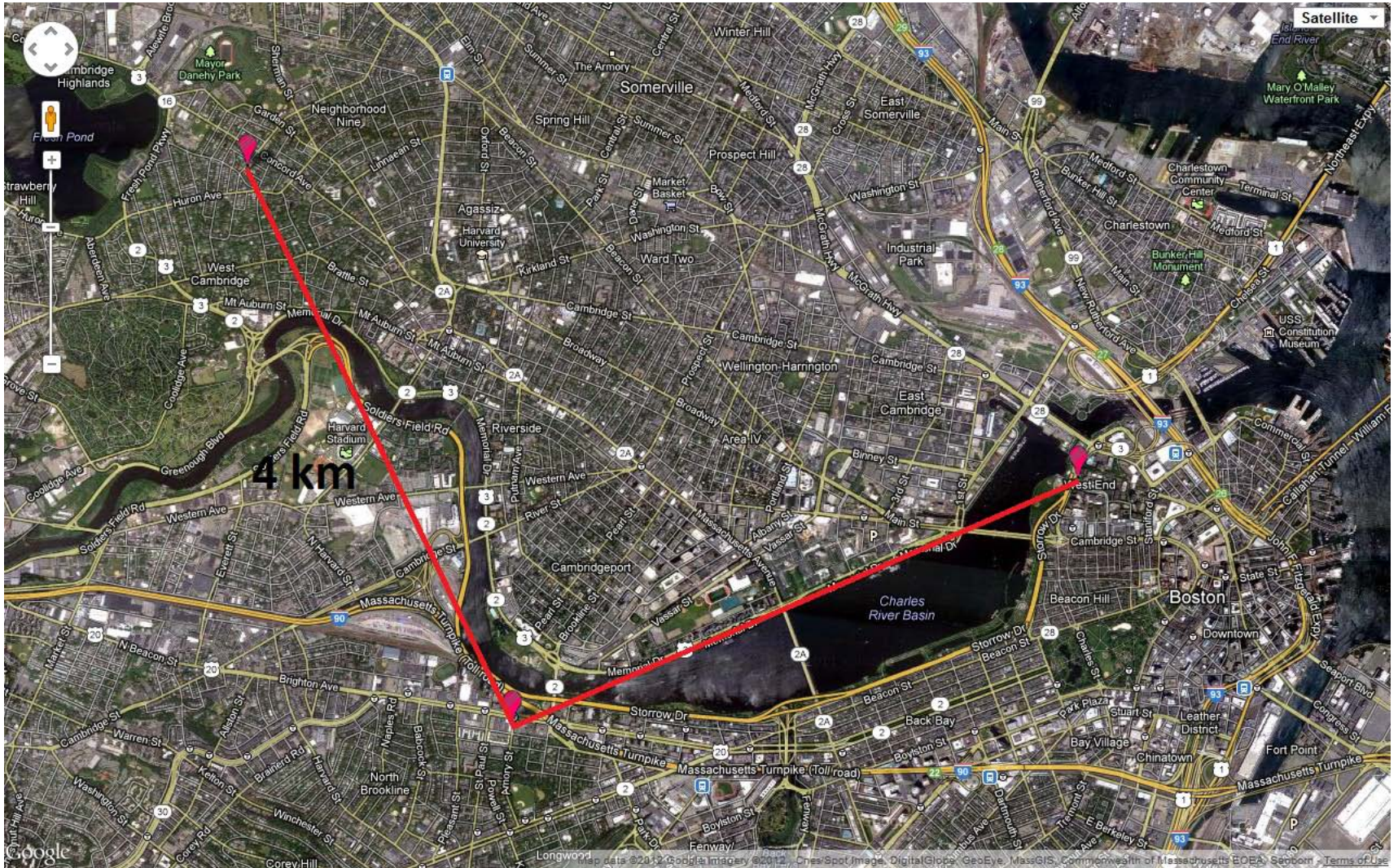
Mom  
Dad  
Nina  
Darren  
Jamie

## **National Science Foundation**





# Backups



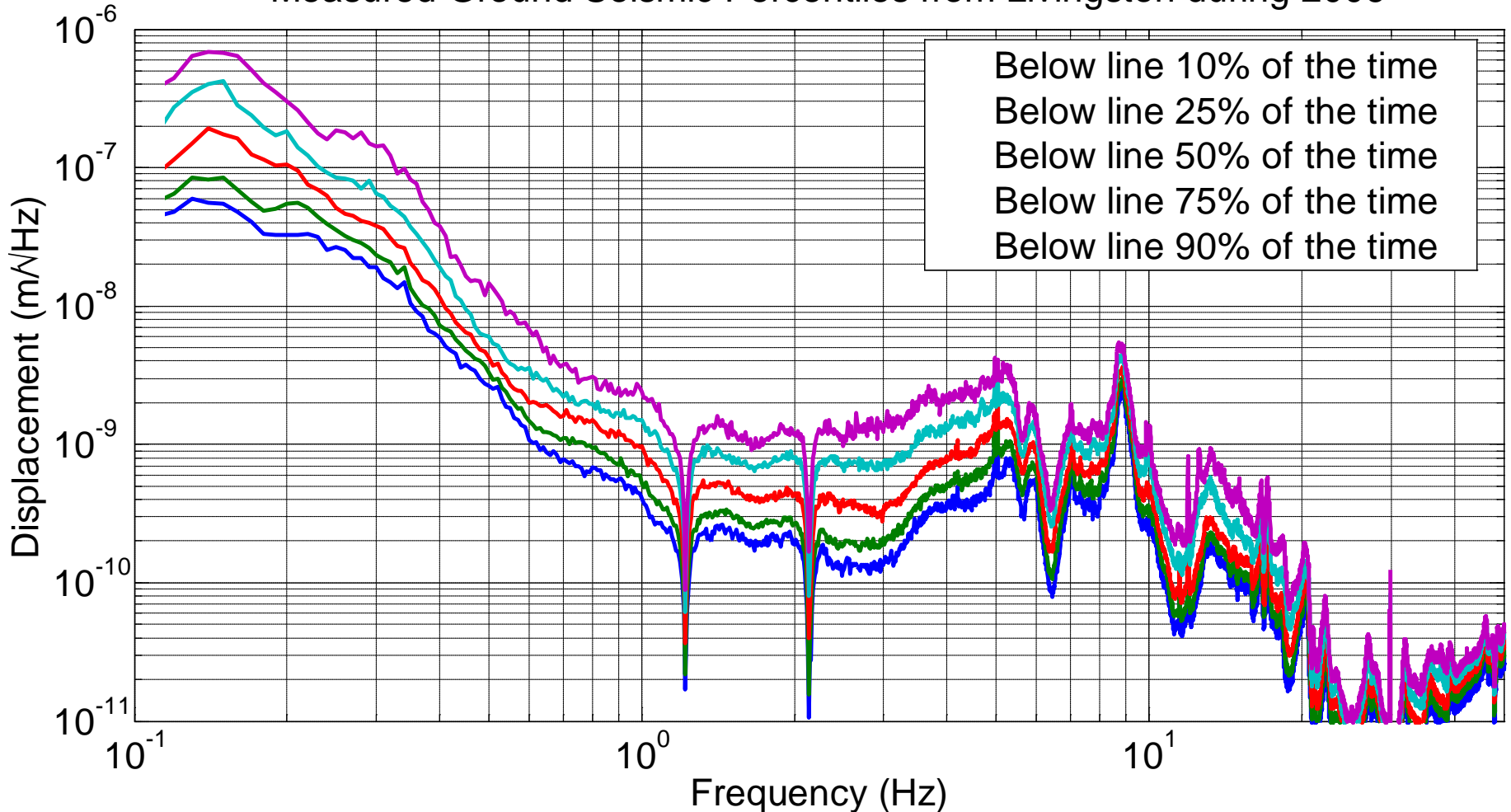
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LIGO spans 16 km<sup>2</sup>. Cambridge, MA covers 16.65 km<sup>2</sup> (wikipedia).

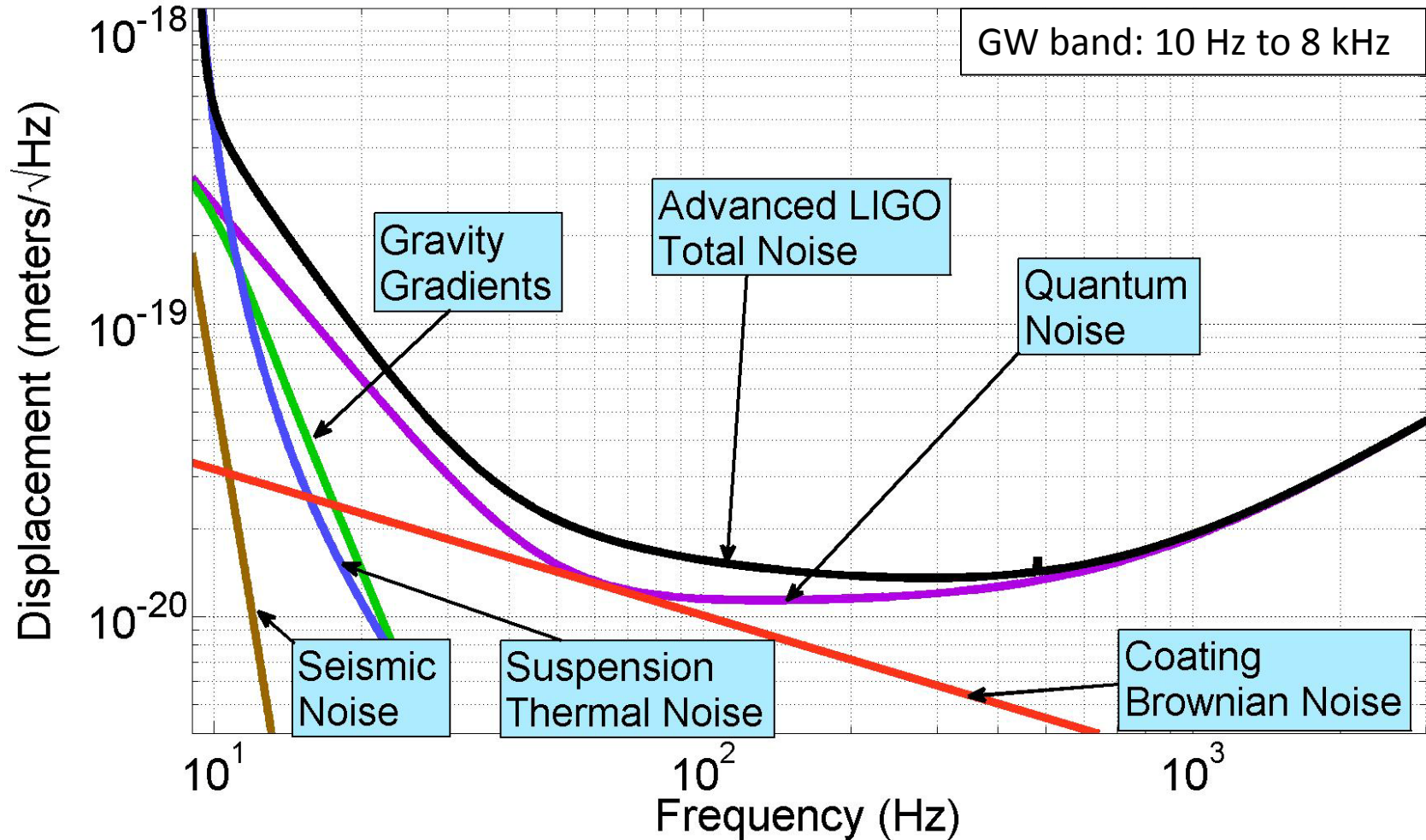


# Problem 1: Nonstationary Disturbance

Measured Ground Seismic Percentiles from Livingston during 2006

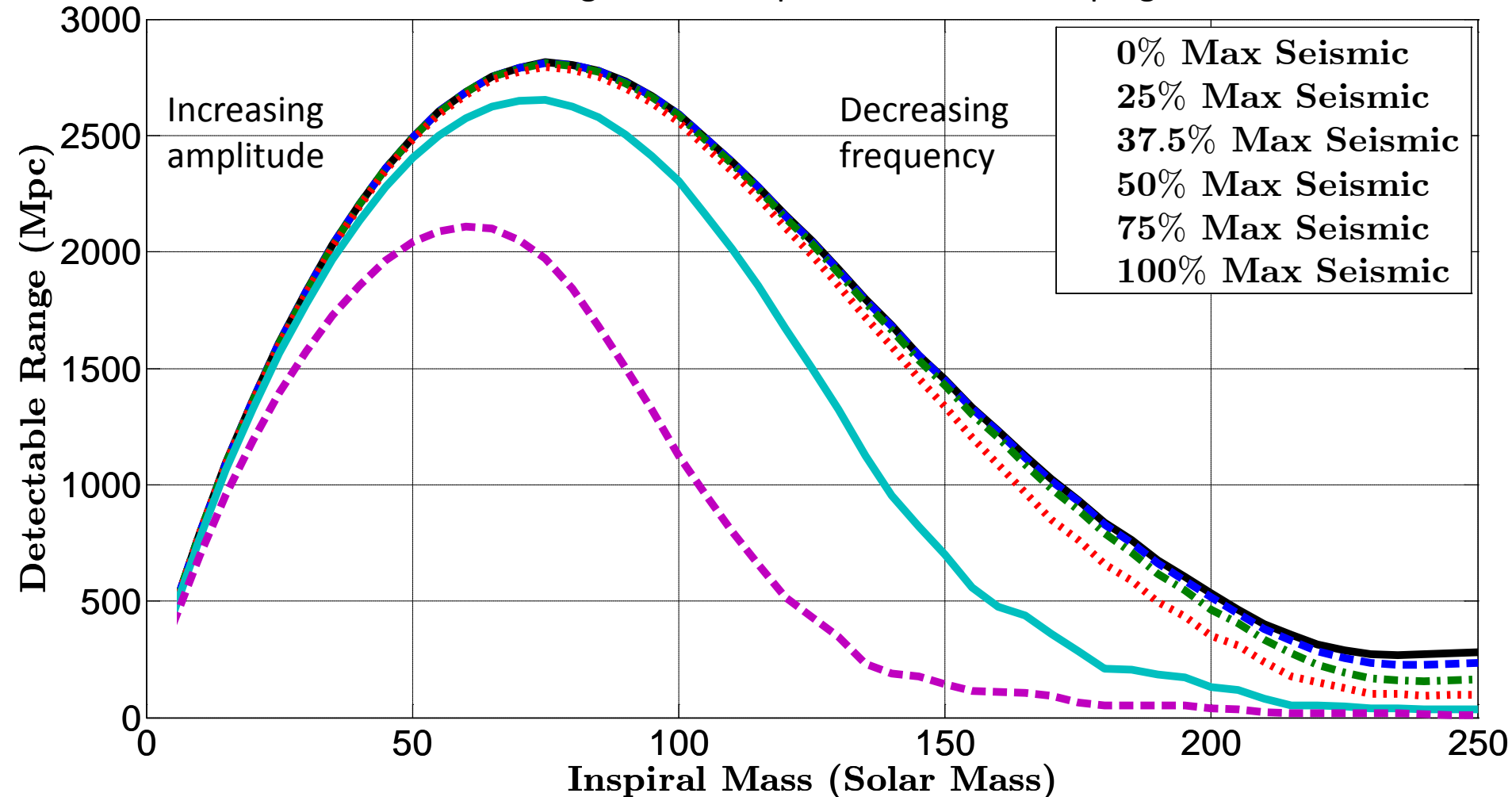


# Projected Sensitivity for aLIGO



# Inspiral Range vs Binary Mass

Increasing seismic amplitude with no damping



# AMD Inspiral Simulation Cost Functions

$$\text{Sensor noise cost} = \frac{\zeta_i}{\zeta_{0,i}} - 1$$

$$\text{Modal amplitude cost} = \frac{M_{RMS,i}/M_{0,i}}{1 - \text{erf}\left(\frac{M_{RMS,i}}{M_{0,i}}\right)}$$

$$\text{Total cost per mode} = \left[ \frac{M_{RMS}/M_0}{1 - \text{erf}\left(\frac{M_{RMS}}{M_0}\right)} \right]^2 + \left[ \frac{\zeta}{\zeta_0} - 1 \right]^2$$

- $M_{RMS}$  measured modal displacement amplitude. Model behavior  $\rightarrow M_{RMS} = \frac{\text{open loop amplitude}}{\sqrt{\zeta}}$   
 $M_0$  modal cost scale factor  
 $\zeta$  modal closed loop damping ratio  
 $\zeta_0$  minimum closed loop damping ratio  
 $i$  mode index

Table I: Adaptive modal damping cost function parameters.

Parameter	Mode 1	Mode 2	Mode 3	Mode 4
$\zeta_0$	0.0005	0.0005	0.0005	0.0005
$M_{RMS}$ with $\zeta_0$ & max seis	$1.45 \cdot 10^{-8}$	$6.54 \cdot 10^{-9}$	$1.17 \cdot 10^{-8}$	$2.00 \cdot 10^{-9}$
$M_0$	$2 \cdot 10^{-8}$	$10^{-9}$	$8 \cdot 10^{-10}$	$5 \cdot 10^{-10}$
$M_{RMS}/M_0$	0.725	6.54	14.625	4

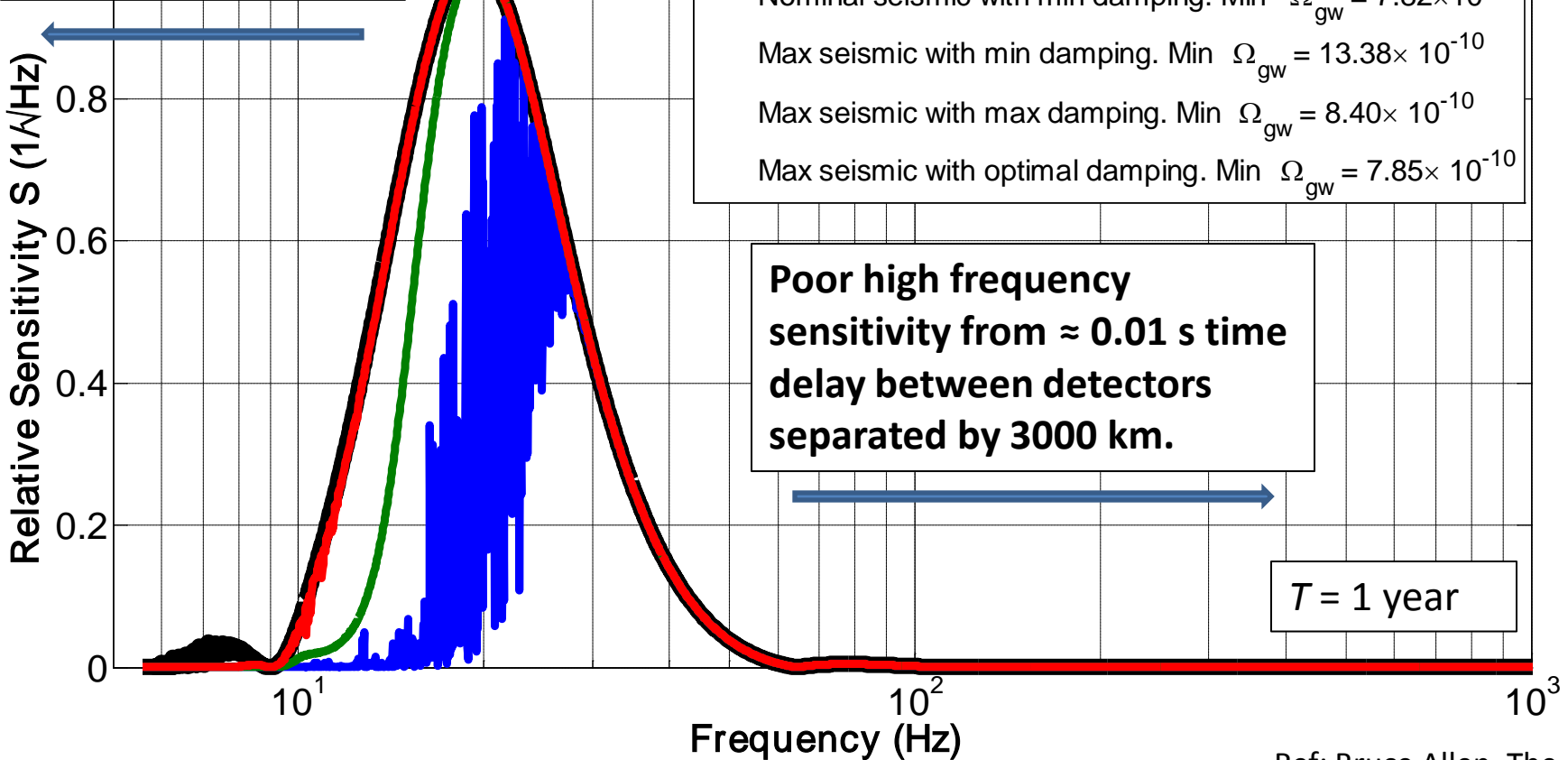
# AMD Inspiral Simulation Results

Table II: **Optimal** damping values determined by the selected cost function parameters.

Seismic % of max	$\zeta_1$	$\zeta_2$	$\zeta_3$	$\zeta_4$	150 SM volume $\text{Mpc}^3 \times 10^6$	
0	0.00054	0.00055	0.00051	0.00050	3051	(100%)
50	0.00059	0.0051	0.016	0.0042	2982	(97.7%)
75	0.00073	0.0089	0.029	0.0090	2915	(95.5%)
100	0.00091	0.014	0.046	0.016	2796	(91.6%)
100	0.20	0.20	0.20	0.20	473	(15.6%)
100	0.00050	0.00050	0.00050	0.00050	3.05	(0.1%)

# Stochastic Sensitivity

Poor low frequency sensitivity from high detector noise.



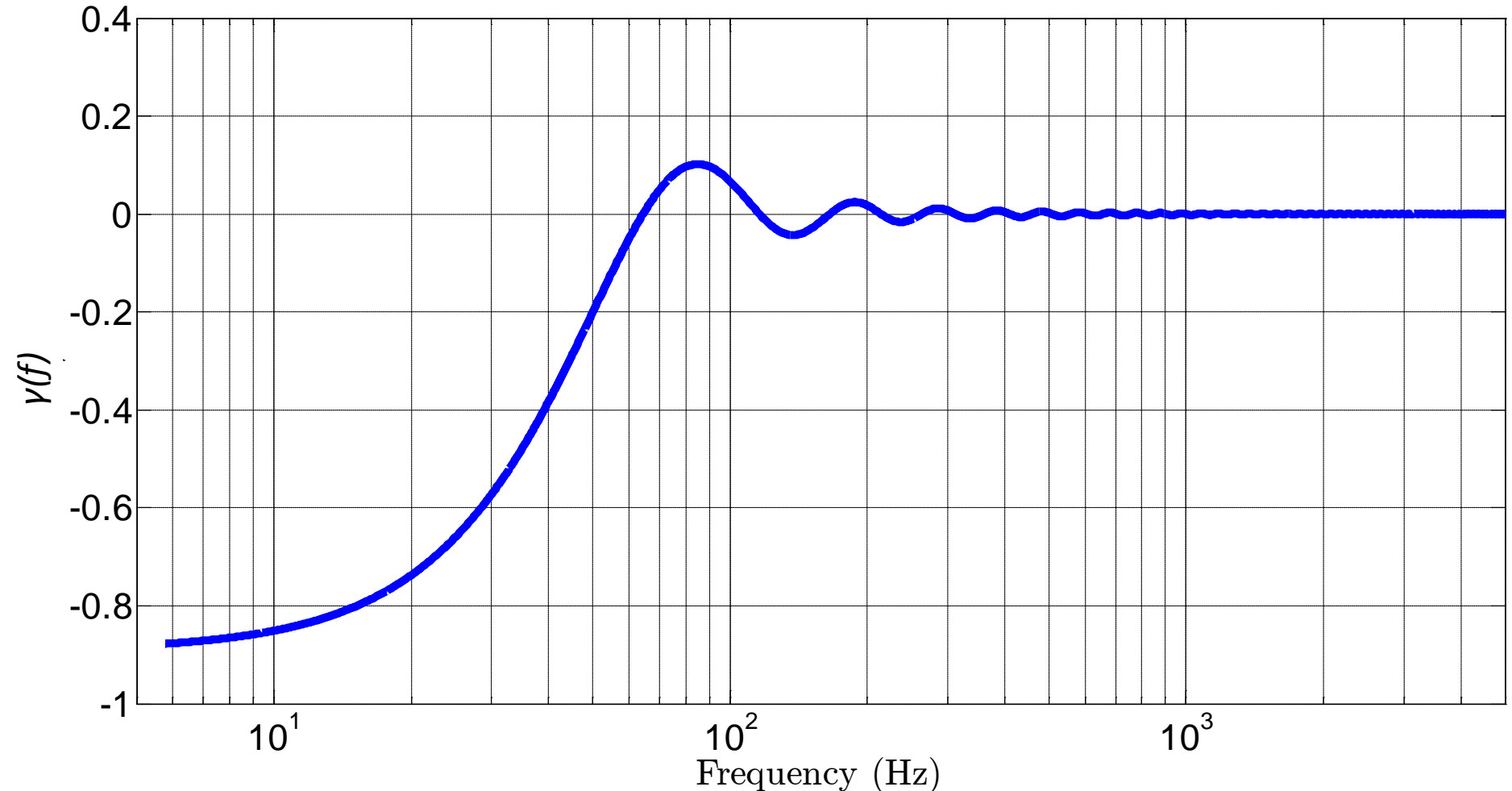
$$\Omega_{gw} = \frac{1.65}{\rho_{critical}} \left[ \frac{32G^2}{25c^4 \pi^2} T \int_0^\infty S^2(f) df \right]^{-0.5}$$

$$\rho_{critical} = \frac{3c^2 H_0^2}{8\pi G} \quad S(f) = \frac{\gamma(f)}{f^3 P(f)}$$

Ref: Bruce Allen. The Stochastic Gravity-wave Background: Sources and Detection. 1996.



# Stochastic Overlap Reduction Function



# Backups: Science from Observations

- Binary black holes
  - Probe nonlinear dynamics of spacetime curvature during merger phase.
  - GW scattering during inspiral phase.
  - Characterize number of neutron star and/or black hole binaries
  - Characterise ringdown phase after merger
  - Test Hawking's law that the event horizon must increase in area
  - Naked singularity test

# Backups: Science from Observations

- Stochastic background
  - Observe early universe from  $10^{-22}$  sec after Big Bang. Currently, CMB observations only get us to about 100,000 years after big bang ( $\approx 35$  orders of magnitude improvement).
  - Quantify background from incoherent sum of many weak/distant sources such as binaries, supernovae, etc.

# Backups: Science from Observations

- Inspirals
  - Quantity in Milky Way
  - Neutron star structure
  - Neutron star ellipticity (how big are the mountains)
  - Neutron star quakes
  - Theory of maximum spin rate of X-ray binaries due to GW emission
- Supernovae
  - Evolution of stellar collapse - no complete models exist.

# Backups: GW Signal Calibration

Cavity Displacement (Eq. 1):

$$x = \frac{1}{1 + P1_{13}C} [GW + v_2 + P1_{11}d_1 + P1_{12}v_1 + P1_{13}d_2 + P2_{11}d_3 + P2_{12}v_3 + P2_{13}d_4] < 10^{-9} m$$

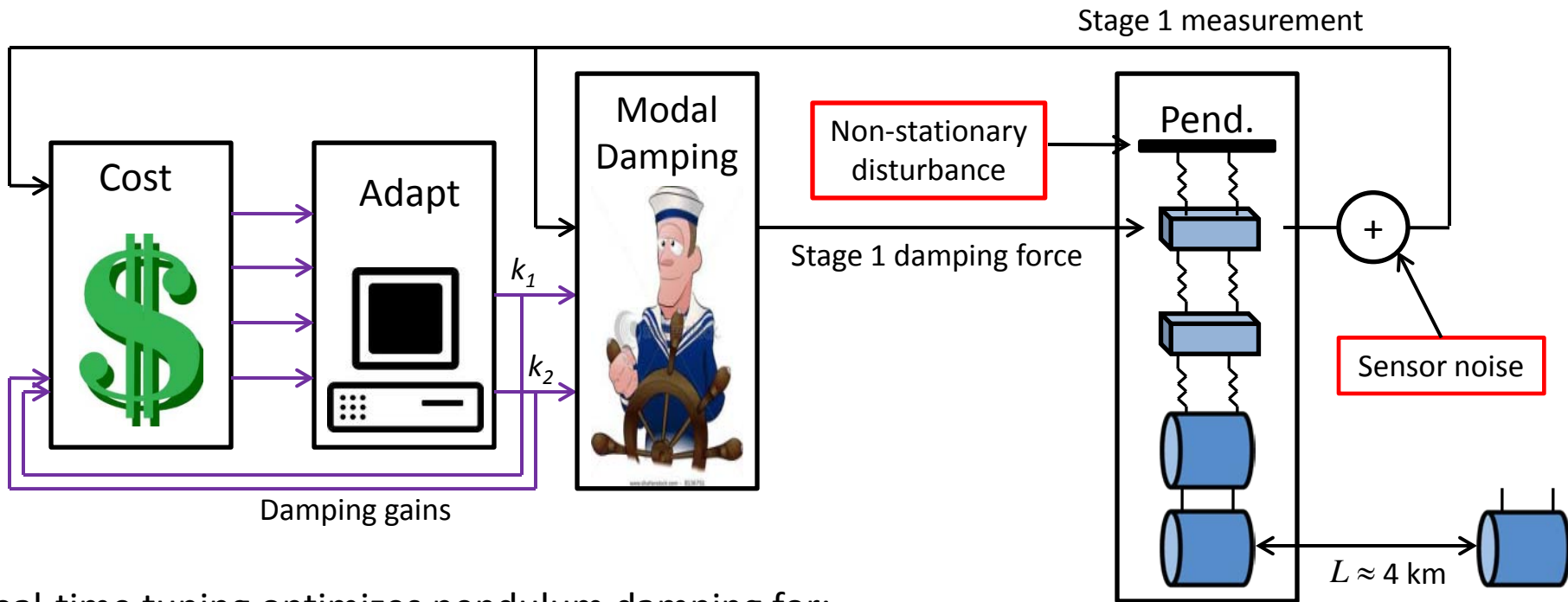
Solving for the GW (Eq. 2):

$$\underbrace{x(1 + P1_{13}C)}_{\approx GW} = GW + v_2 + P1_{11}d_1 + P1_{12}v_1 + P1_{13}d_2 + P2_{11}d_3 + P2_{12}v_3 + P2_{13}d_4$$

Calibrated cavity signal (effectively open loop)

If  $GW$  is much greater than everything else on the right hand side of (2), then the calibrated signal is approximately  $GW$ .

# Simulation of LIGO cavity with AMD



Real-time tuning optimizes pendulum damping for:

1. Nonstationary disturbance
2. Sensor noise
3. Nonlinear interferometer response
  - A. Laser beams falling off mirrors
  - B. Laser scattering off vacuum walls and other objects
  - C. Interferometer readout method
  - D. Creak in suspension springs
  - E. etc

$$e = \Delta L - \frac{\Delta L^2}{8 \times 10^{-13} \text{ meters}}$$

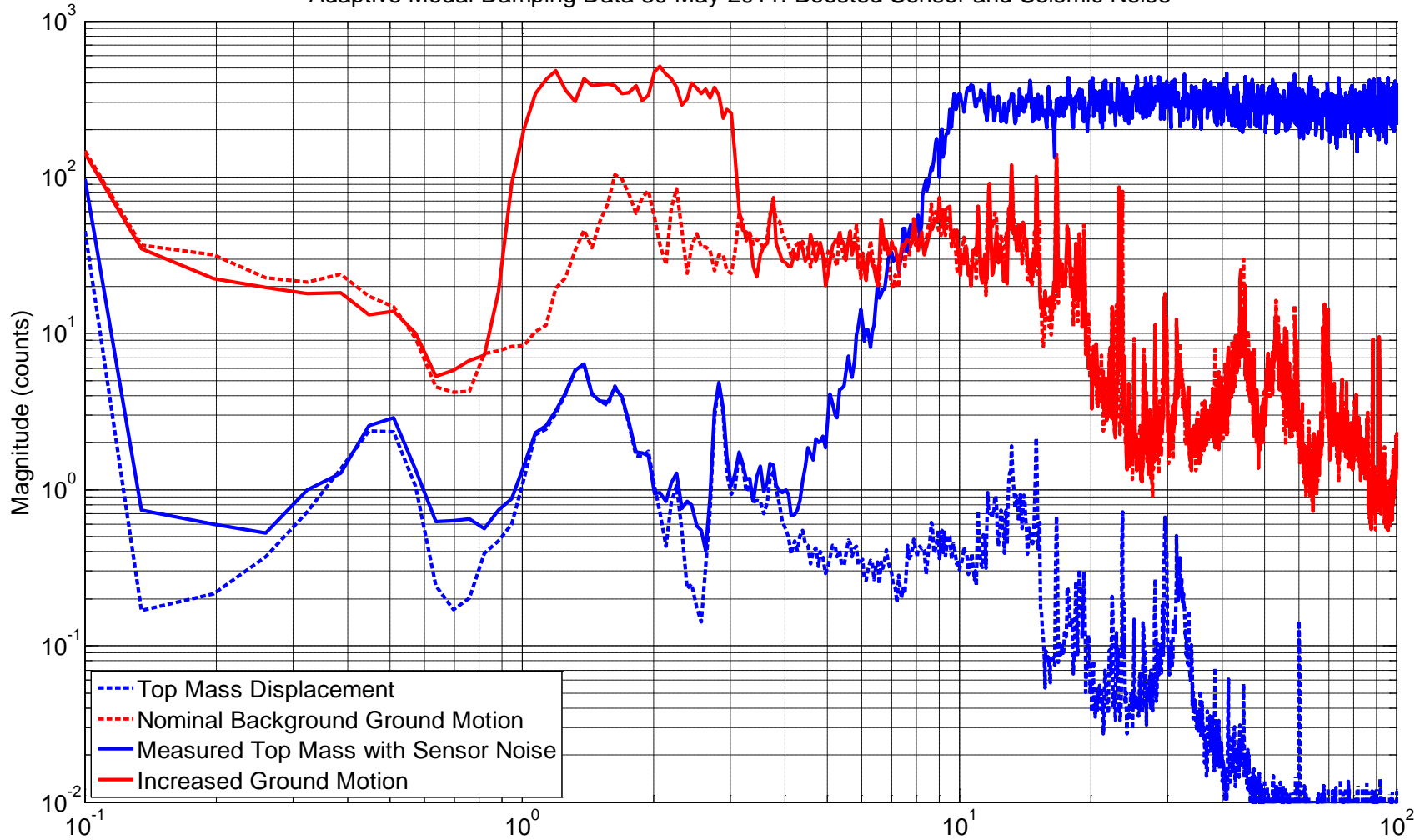
Interferometer signal w/  
nonlinear model

Assumption that  
 $\Delta L_{RMS} < 10^{-15}$  meters  
 Removes nonlinearity<sub>58</sub>

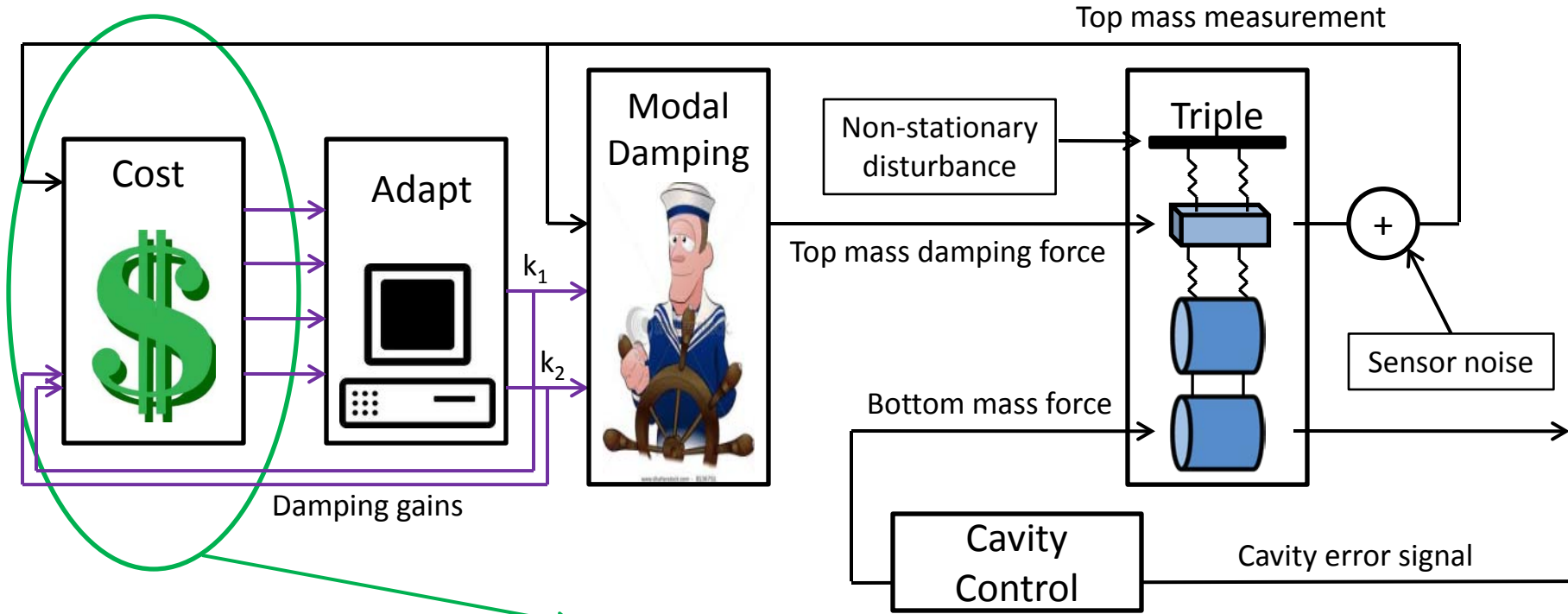


# Backups: Boosted Experimental Noise

Adaptive Modal Damping Data 30 May 2011: Boosted Sensor and Seismic Noise

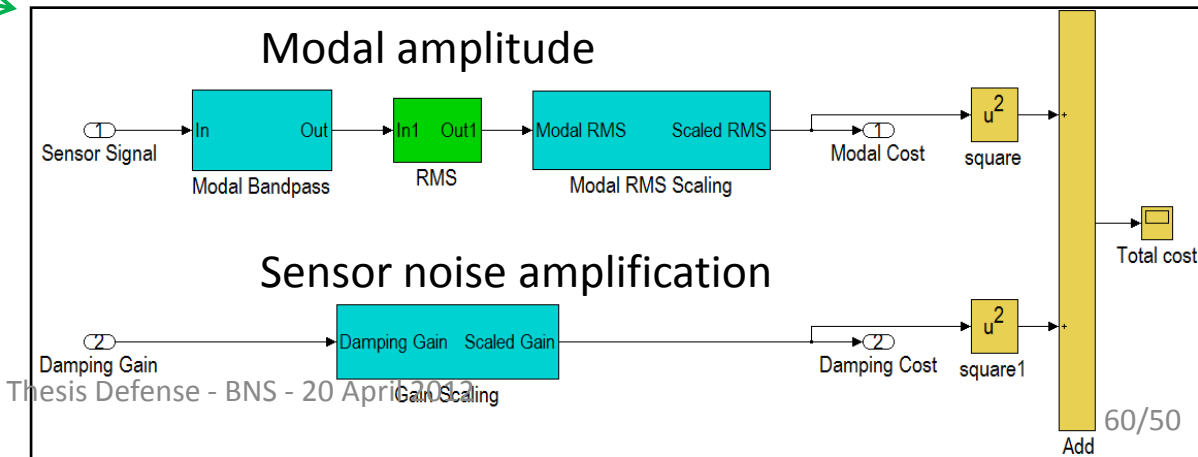


# Cavity Control with Adaptive M.D.



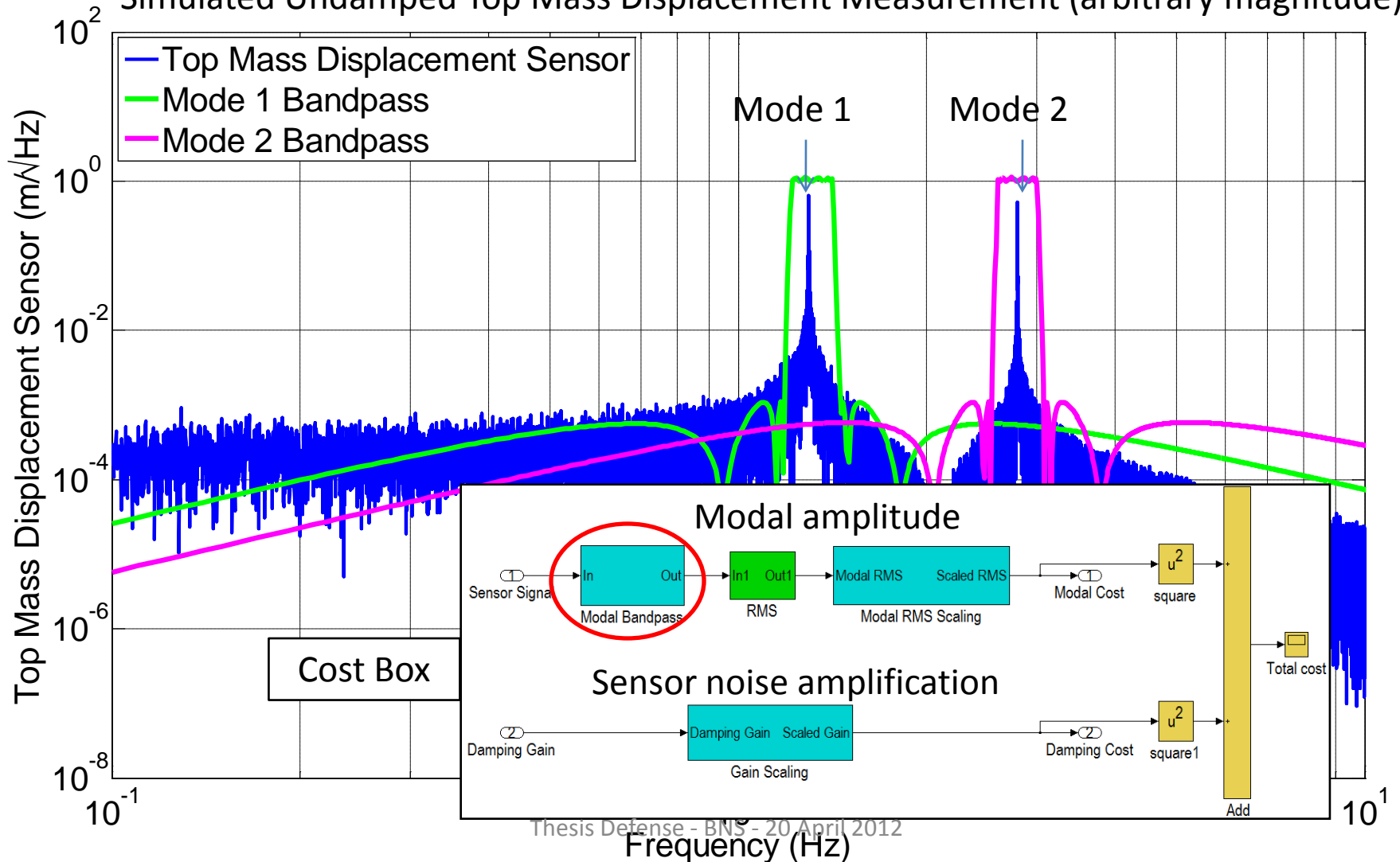
The cost box measures the performance values we care about and scales them to get the costs:

1. Modal Amplitudes
  2. Noise Amplification
- directly proportional to damping gain

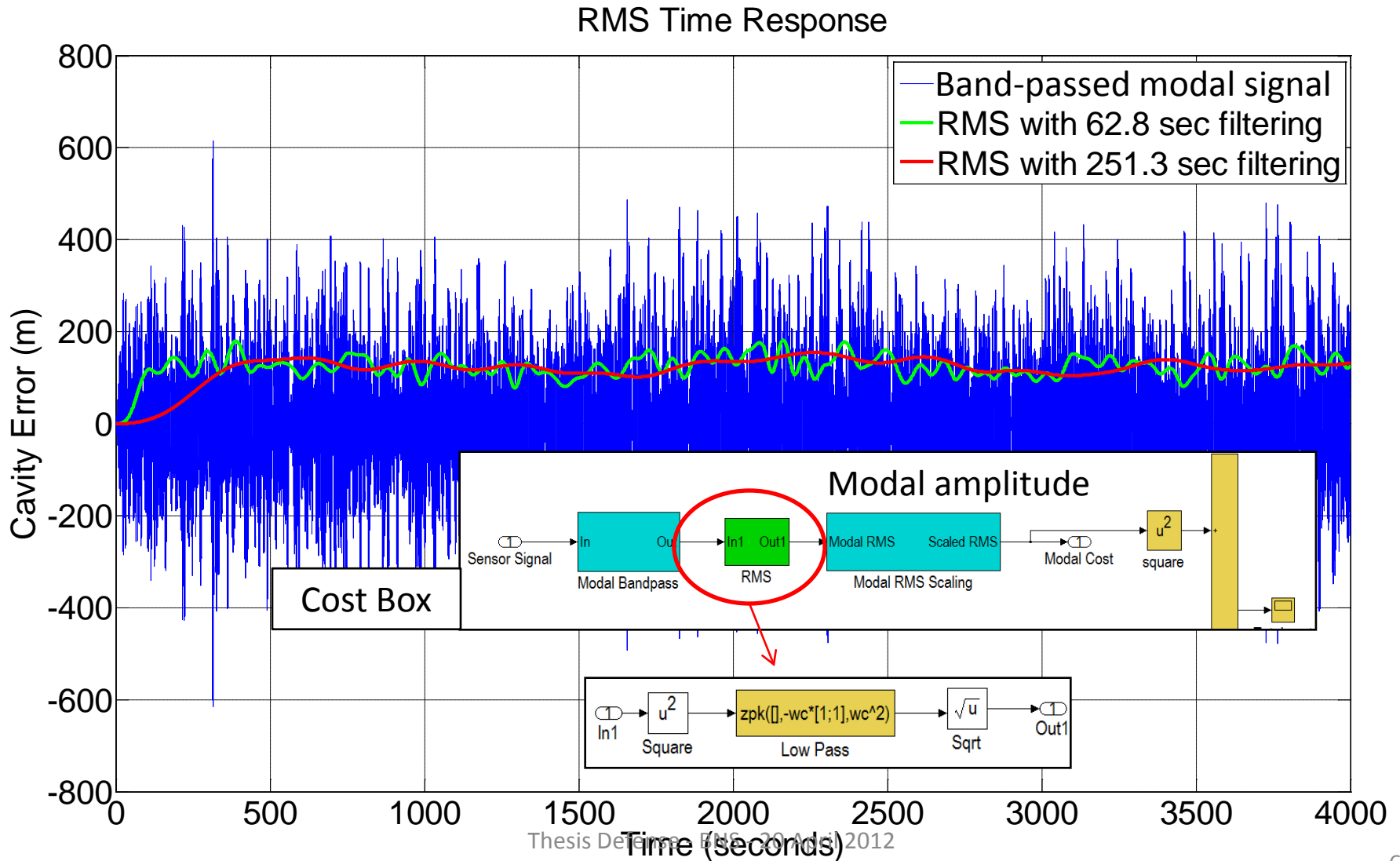


# Cost Input 1: Modal Amplitudes

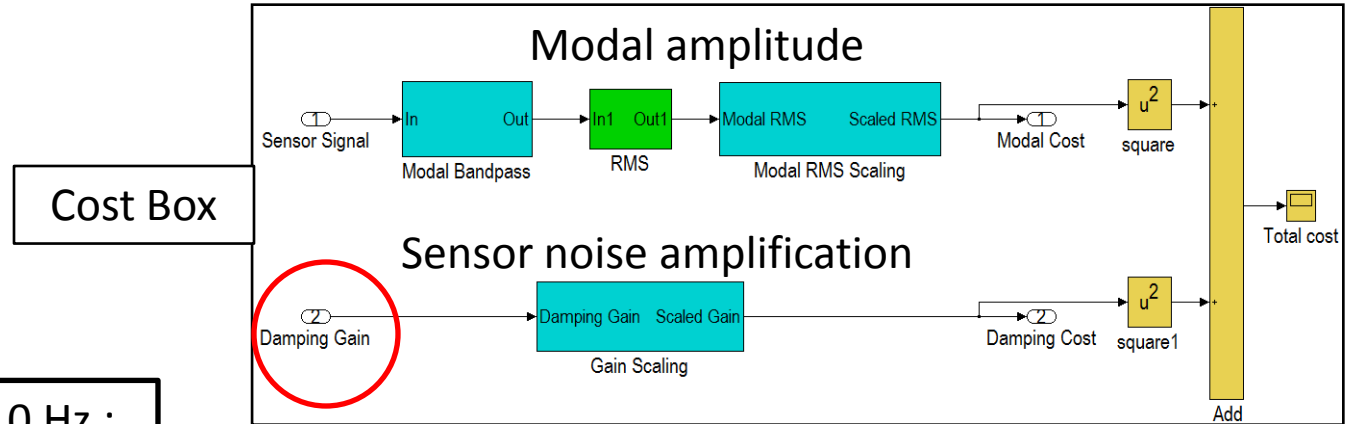
Simulated Undamped Top Mass Displacement Measurement (arbitrary magnitude)



# Modal Amplitude Variance Estimation



# Cost Input 2: Noise Amplification



For frequencies  $\geq 10$  Hz :

$$P_1 = \frac{k_1 G_1}{1 + (Plant)_1 k_1 G_1} v \approx k_1 G_1 v \longrightarrow P_i \propto k_i v$$

mode 1 damping force                      stationary sensor noise                      linear in  $k_i$

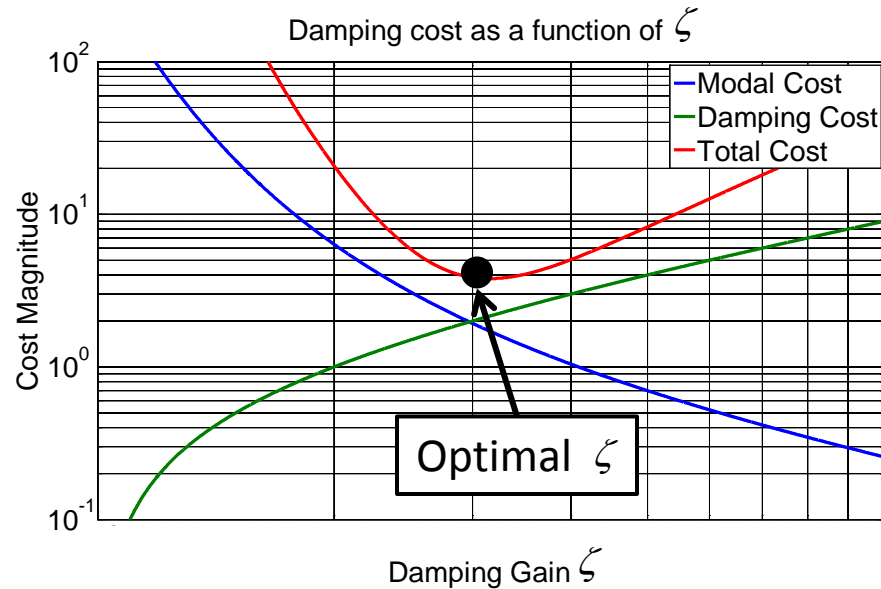
Since the sensor noise amplification for a given mode is directly proportional to its damping gain, the damping gain, rather than a measured noise term is used for this calculation. This is a quicker and more accurate estimate than measuring the noise directly like the modal amplitude.

# Gauss-Newton Adaptation

Recursive damping gain equation

$$\zeta_{i,n+1} = \zeta_{i,n} - \alpha_{i,n} J_{i,n}^+ \bar{c}_{i,n}$$

<sup>+</sup> = pseudoinverse



## Notes

$k_{i,n}$  =  $i_{th}$  mode damping gain at time step  $n$ . Each time step is 30 to 60 sec.

$J_{i,n}^+$  = pseudoinverse of the  $i_{th}$  mode Jacobian descent matrix at time step  $n$  (model based).

$$J_{i,n} = \begin{bmatrix} \text{(Modal amplitude gradient wrt } k_i) \\ \text{(modal noise amp. gradient wrt } k_i) \end{bmatrix}$$

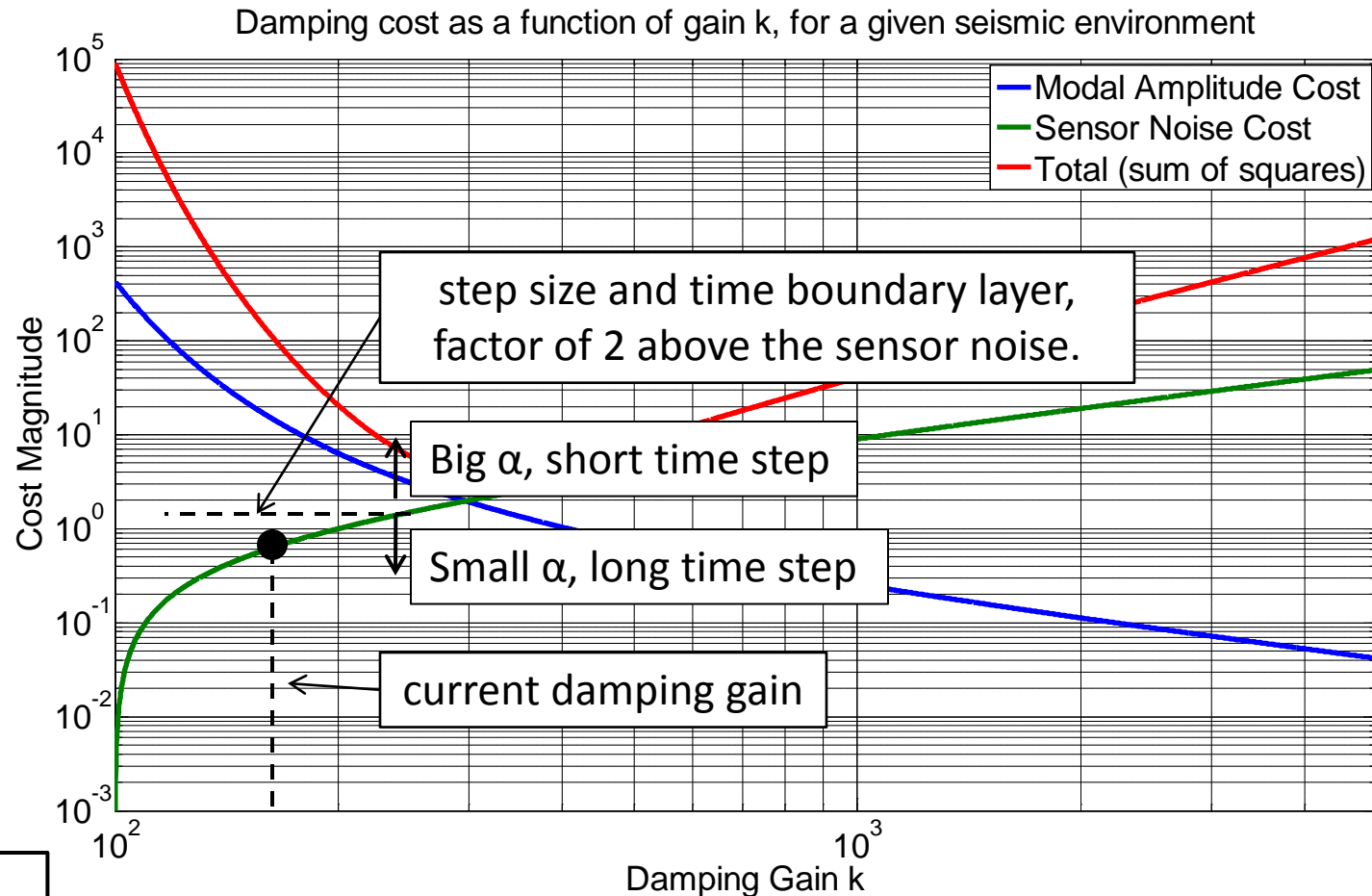
$\bar{c}_{i,n}$  = cost vector of the  $i_{th}$  mode at time step  $n$ .

$$\bar{c}_{i,n} = \begin{bmatrix} \text{(scaled modal amplitude)} \\ \text{(scaled modal noise amplification)} \end{bmatrix}$$

$\alpha_{i,n}$  = step size of the  $i_{th}$  mode damping gain at time step  $n$ .



# Adaptive Step Sizes and Step Rates

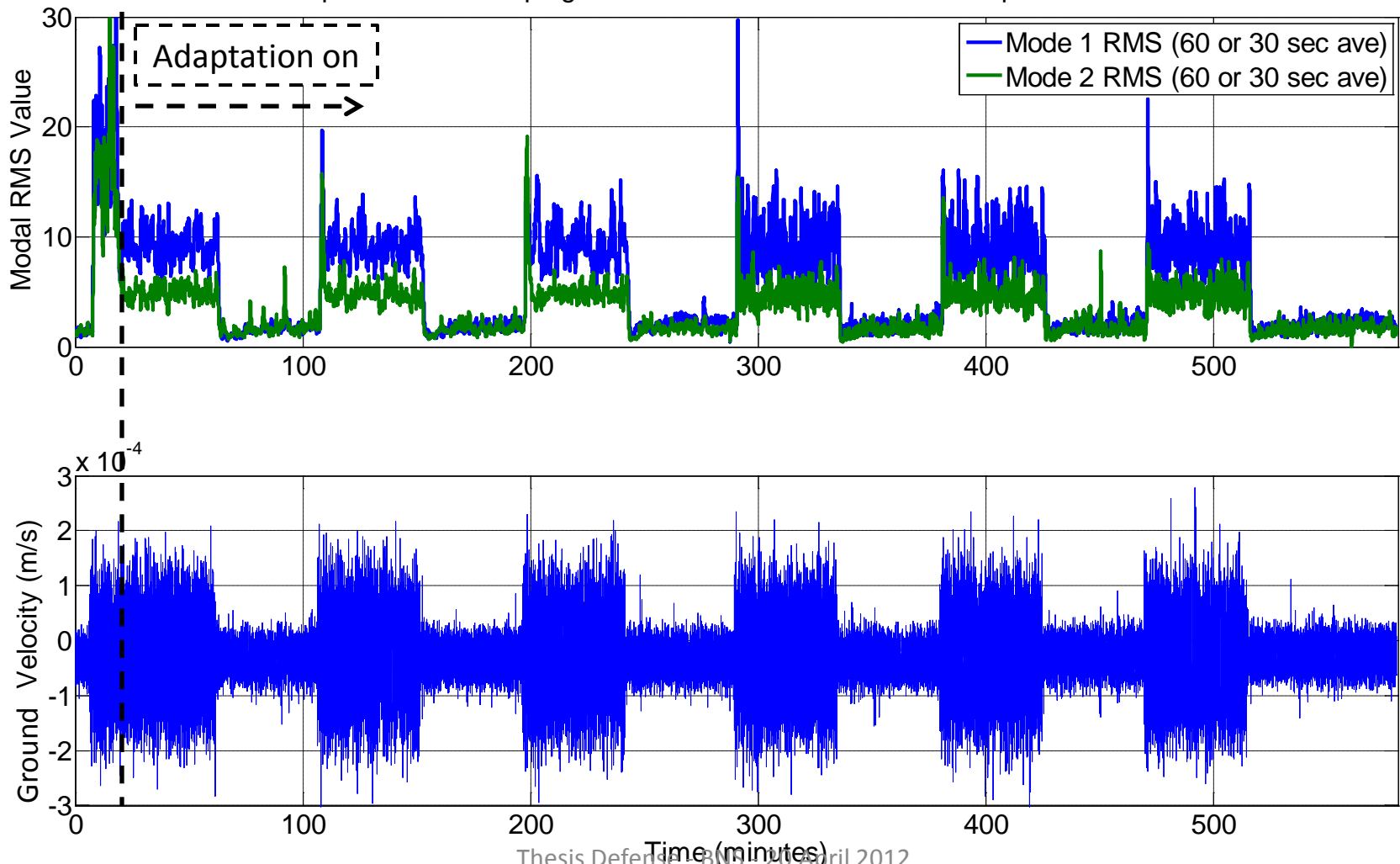


## Notes:

- If the measured modal amplitude is above the moving boundary layer, the adaptation takes large, quick steps with short RMS time constants to respond to sudden seismic events quickly.
- When the modal amplitude goes below the line, the adaptation takes small slow steps with long RMS time constants to converge accurately to the optimal damping solution.

# Measured Response to a Seismic Square Wave: Modal RMS

Adaptive Modal Damping Data 17-18 June 2011: Seismic Square Wave Test

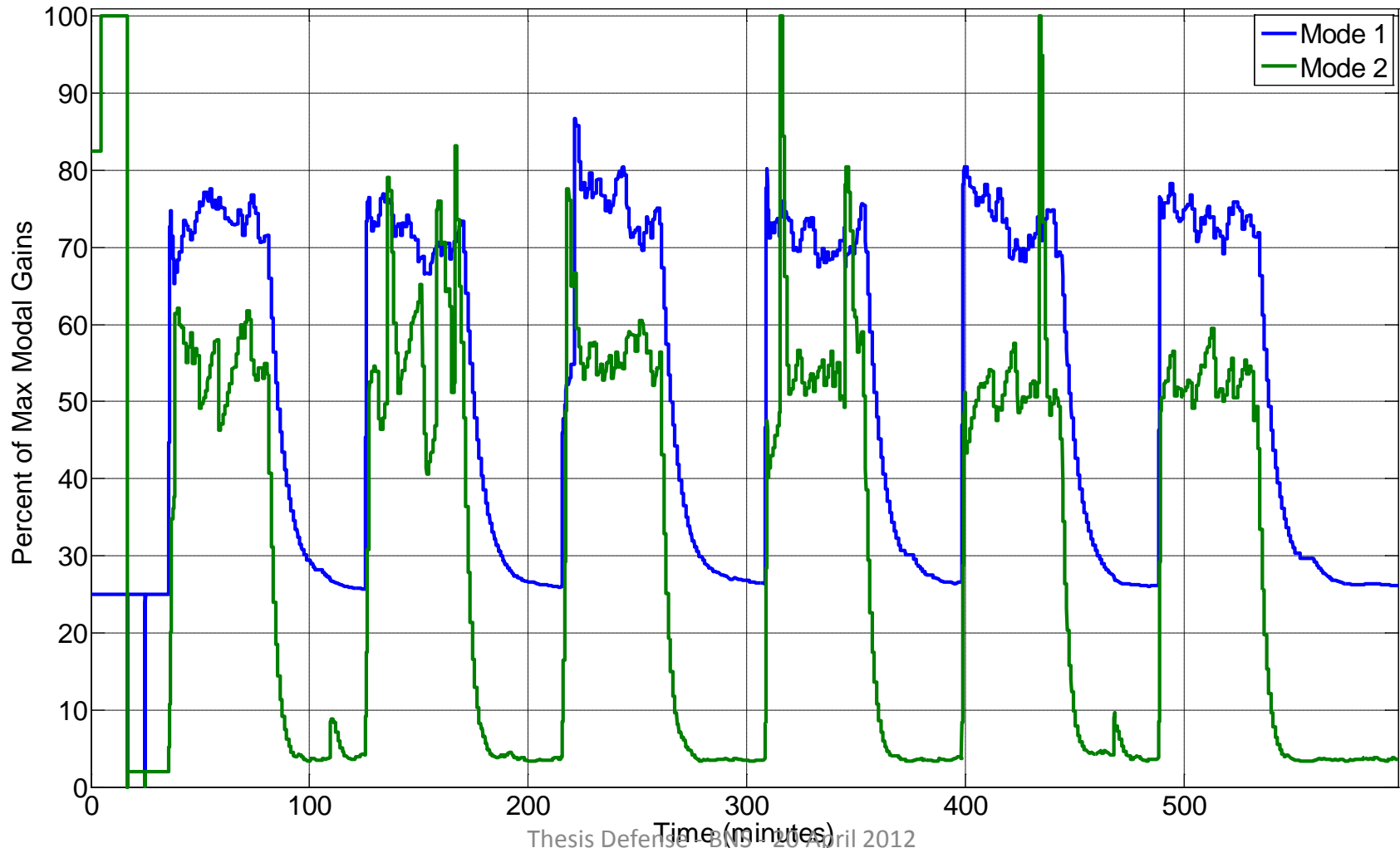


Thesis Defense BMS 20 April 2012

Notes: 3, 30 sec quicksteps steps; 3, 15 sec quicksteps steps; all 60 sec slow steps.

# Measured Response to a Seismic Square Wave: Damping Gains

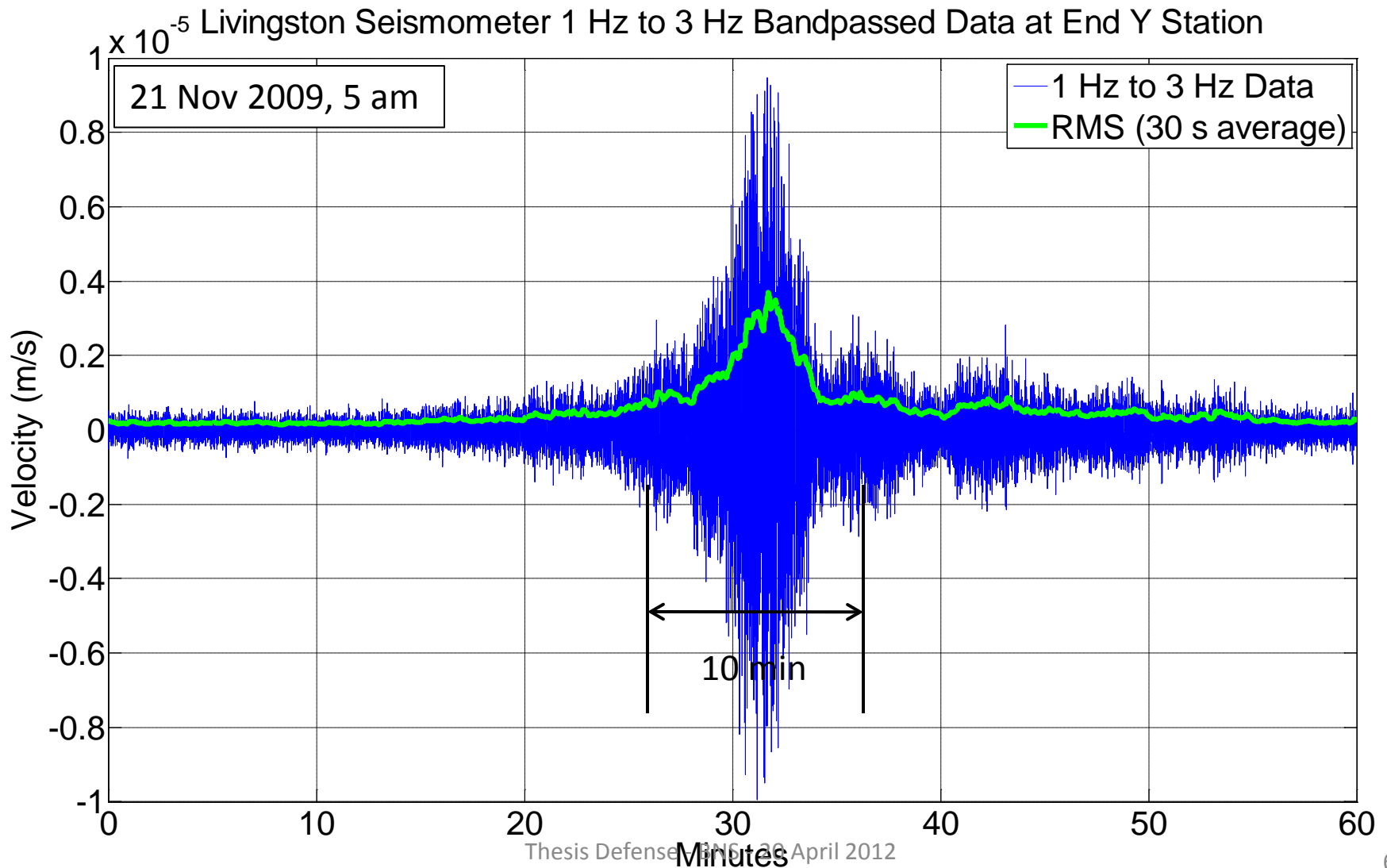
Adaptive Modal Damping Data 17-18 June 2011: Seismic Square Wave Test



Thesis Defense BNS 20 April 2012

Notes: 3, 30 sec quicksteps steps; 3, 15 sec quicksteps steps; all 60 sec slow steps.

# Ex. Train Passing Through Livingston



# Backups: Adaptive Damping Interface Screen

ADAPTIVE\_v4.adl

### Scaling Values

Mode 1 Goal	Mode 1 Scale
15.000	1.000
Mode 2 Goal	Mode 2 Scale
4.000	1.000
G1 Scale	G2 Scale
500.000	100.000

### Measured Responses

Mode 1 RMS
0.0000000000e+00
Mode 2 RMS
0.0000000000e+00

### Plant

Triple

Quad

### Control Filters

Modal Damp

Estimator

Cavity Control

### Cost Components

Mode 1 Signal	Mode 1 Signal
0.000000	2.021996
Mode 2 Signal	Mode 2 Signal
0.000000	2.021996
G1 Noise	
0.000000	
G2 Noise	
-0.000000	

$\sum U^2$

Total Cost

0.000000 0.000

### Adaptation: stepping controller parameters in descent direction

0.000000	0.680000	0.000000	
0.000000	0.680000	0.000000	
pinv(J)			
-97.460335	0.000000	19.779491	0.000000
0.000000	-19.492065	0.000000	3.955898

ALPHA1: 0.125, 2.000, 0.250, 4.000

### Control Parameters

	G1	G2
OUT	500.000	100.000
LIMITS	2000.00, 500.000	5000.00, 100.000
IN	500.000	100.000

### Estimation of descent direction

J	
-0.00985	0.000000
0.000000	-0.04927
0.002000	0.000000
0.000000	0.010000

9889.745117 395.589783

### System State

Step Number	Time to Step
0.0	30.0
Step Length	60.0
30.0	
Error Gain	Reset Switch
3.23624	OFF ON
CPU 54	Pause/Resume
FE Diagnostics	OFF ON
Modal Switch	OFF ON

### Version Notes:

-v4 for tuning triple modal damping to Qs and noise.  
No RLS.

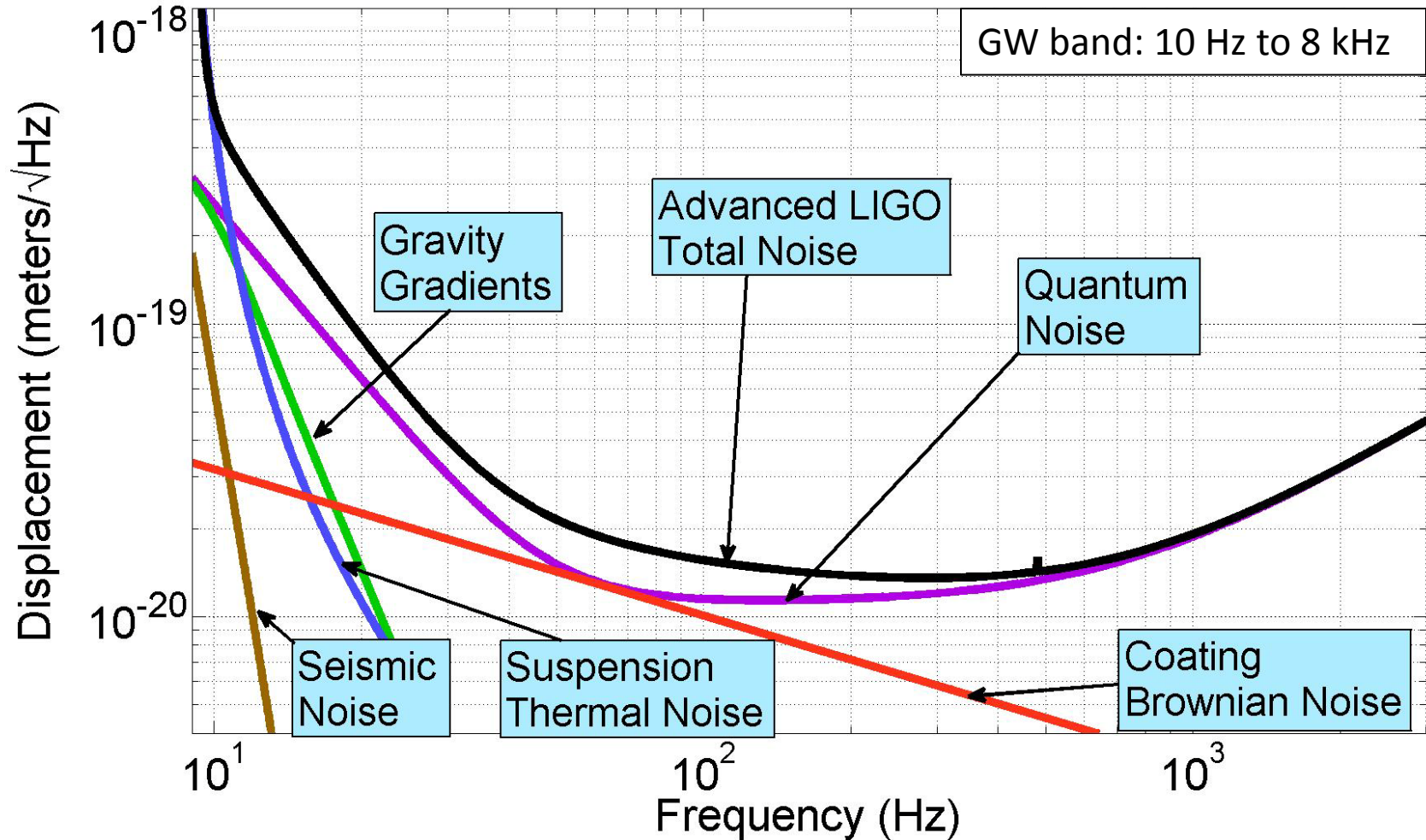
### Graphs

Monitor 1 Monitor 2

Total Cost

Thesis Defense - BNS - 10 April 2012

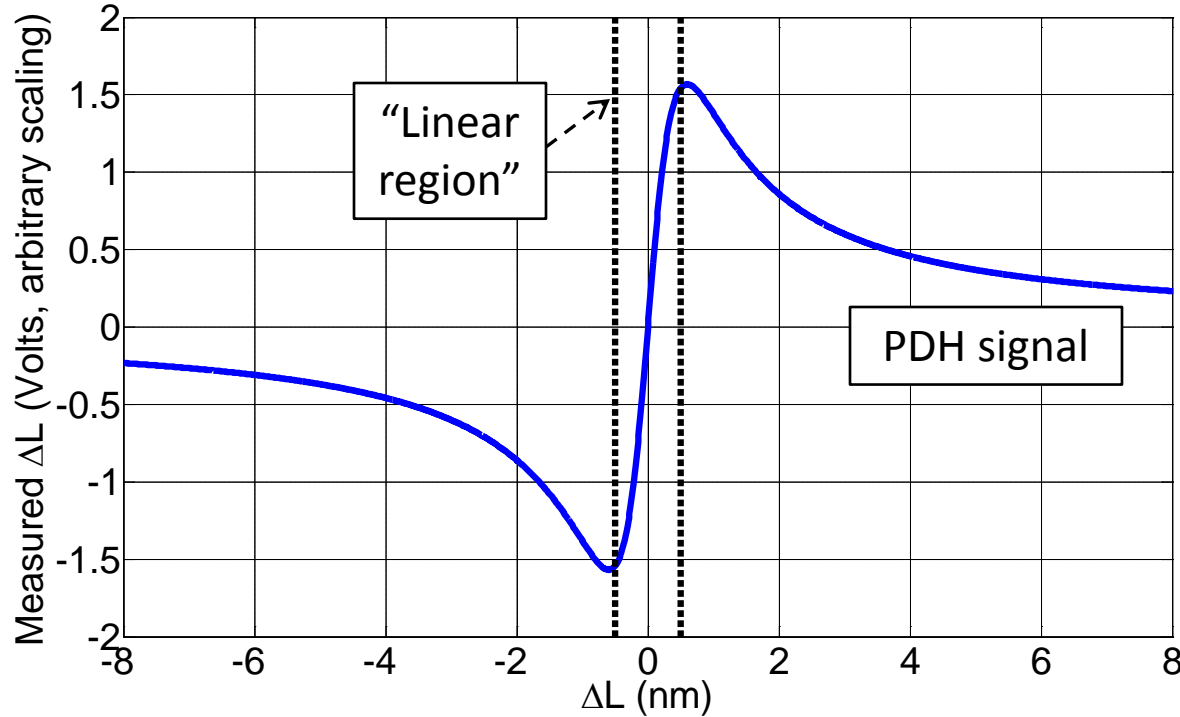
# Projected Sensitivity for aLIGO





# Problem 3: Cavity Signal

Plot of the Pound–Drever–Hall (PDH) Signal for aLIGO



The PDH signal for a 4 km aLIGO Fabry-Perot cavity with mirror power transmissions of 1.4% and 7.5 ppm. The cavity finesse is 445. The linear region between the dashed lines is 1 nm wide.

$$PDH = C \frac{\sin\left(4\pi \frac{\Delta L}{\lambda}\right)}{1 + \left[\frac{2F}{\pi} \sin\left(2\pi \frac{\Delta L}{\lambda}\right)\right]^2}$$

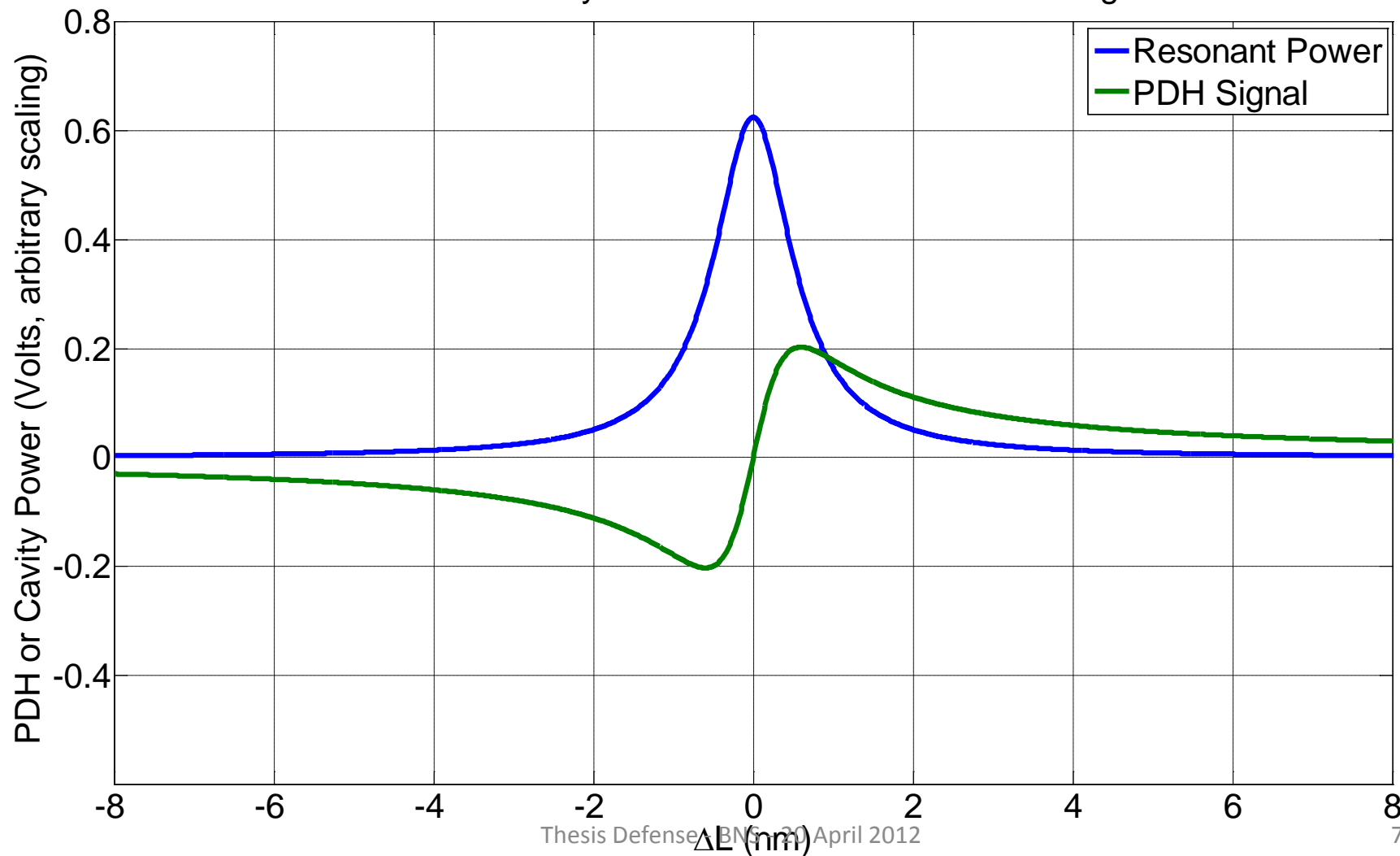
$F$  = cavity finesse = 445

$\lambda$  = laser wavelength = 1064 nm

$C$  = arbitrary electronic scaling

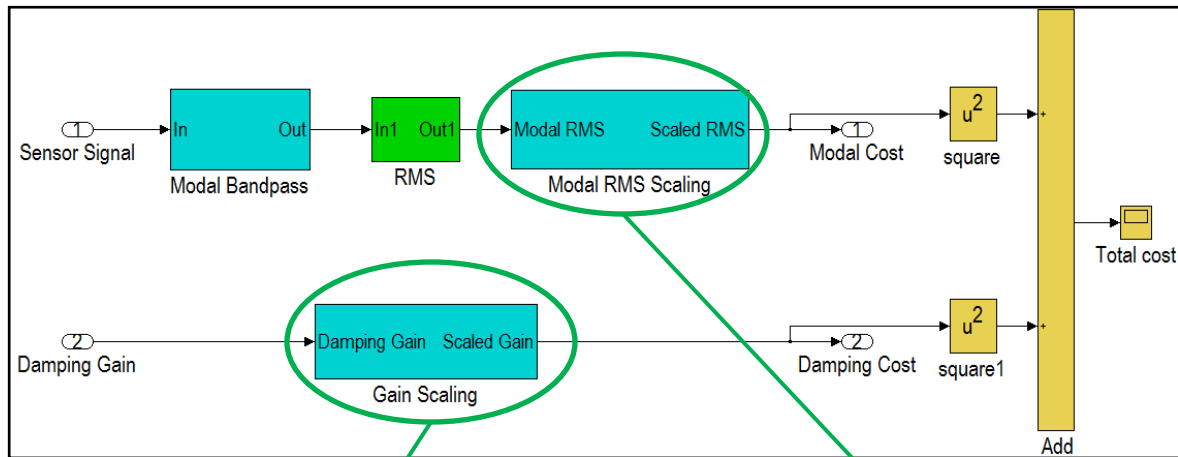
# Backups: PDH and Resonant Cavity Power

Plot of the Cavity Resonant Power and the PDH Signal



# Backups: Cost Scaling Details

# Backups: Cost Scaling Details



$$\frac{G}{G_0}$$

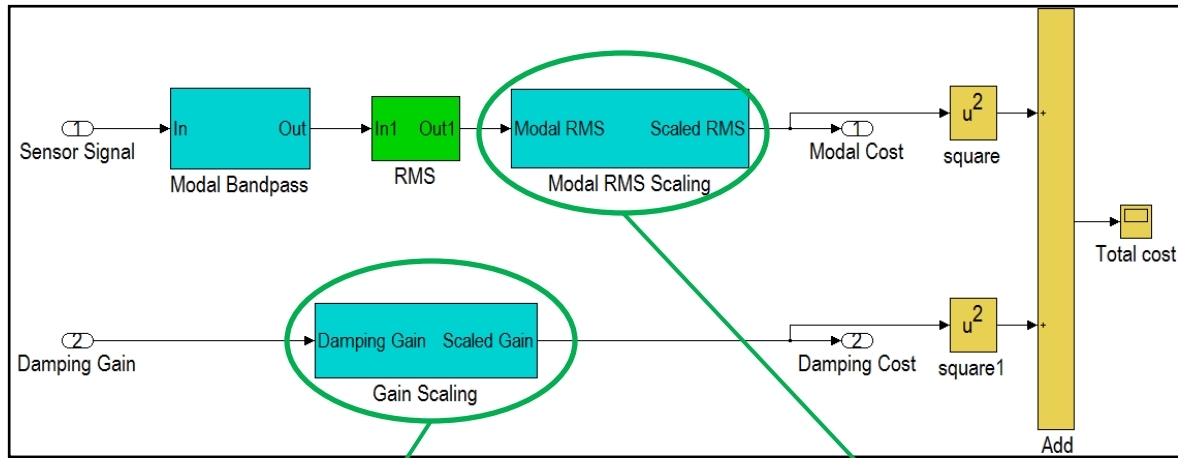
Damping Gain Scaling

<- equal trade off ->

$$\frac{M_{RMS}}{M_0}$$

Modal RMS Scaling

# Backups: Cost Scaling Details



$$\frac{G}{G_0}$$

Damping Gain Scaling

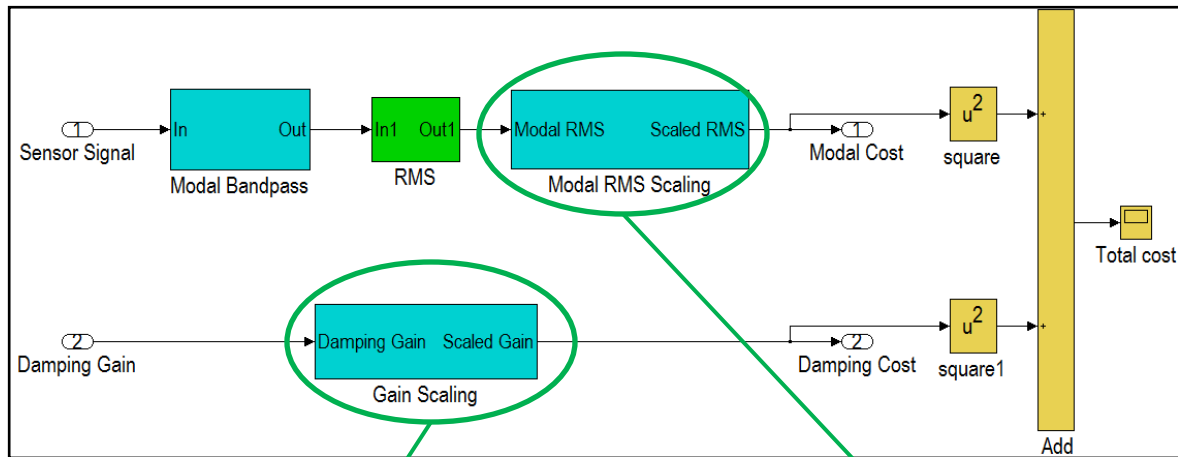
<- progressive trade off ->

$$\frac{M_{RMS}/M_0}{1 - M_{RMS}/M_0}$$

Modal RMS Scaling

- Progressive trade off anticipates cavity lock loss for large amplitude disturbances.

# Backups: Cost Scaling Details



$$\frac{G}{G_0}$$

Damping Gain Scaling

<- progressive trade off ->

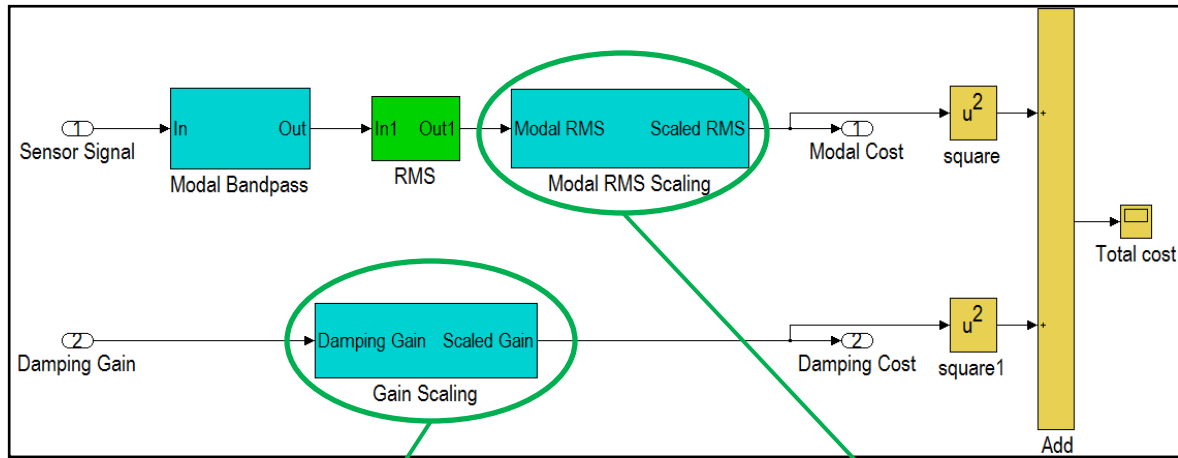
$$\frac{M_{RMS}/M_0}{1 - \text{erf}\left(\frac{M_{RMS}}{M_0}\right)}$$

Modal RMS Scaling

- Progressive trade off anticipates cavity lock loss for large amplitude disturbances.
- erf() removes the pole and reduces the aggressiveness.



# Backups: Cost Scaling Details



$$\frac{G}{G_0} - 1$$

Damping Gain Scaling

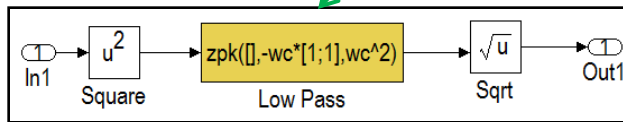
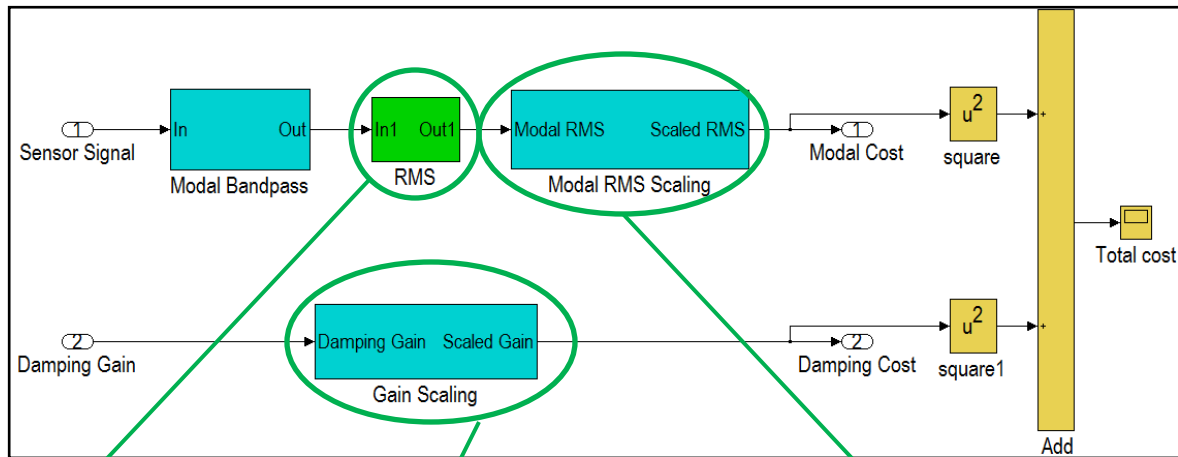
<- progressive trade off ->

$$\frac{M_{RMS} / M_0}{1 - \text{erf}\left(\frac{M_{RMS}}{M_0}\right)}$$

Modal RMS Scaling

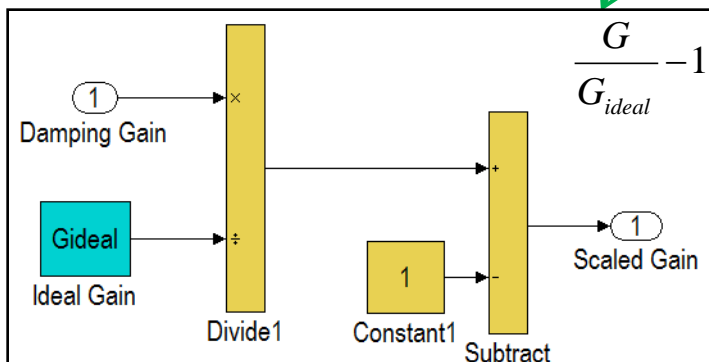
- Progressive trade off anticipates cavity lock loss for large amplitude disturbances.
- erf() removes the pole and reduces the aggressiveness.
- Subtracting 1 from the gain scaling simply provides a '0' cost target gain.

# Backups: Cost Box Details

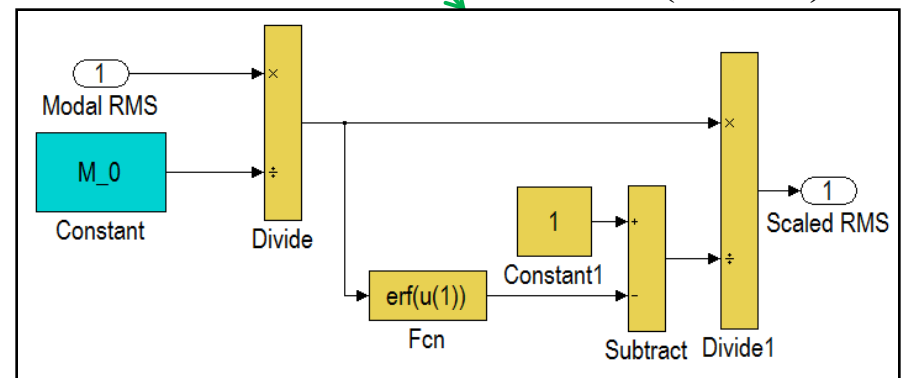


RMS Filter

$$\frac{M_{RMS}/M_0}{1 - \text{erf}\left(\frac{M_{RMS}/M_0}{1}\right)}$$



Damping Gain Scaling

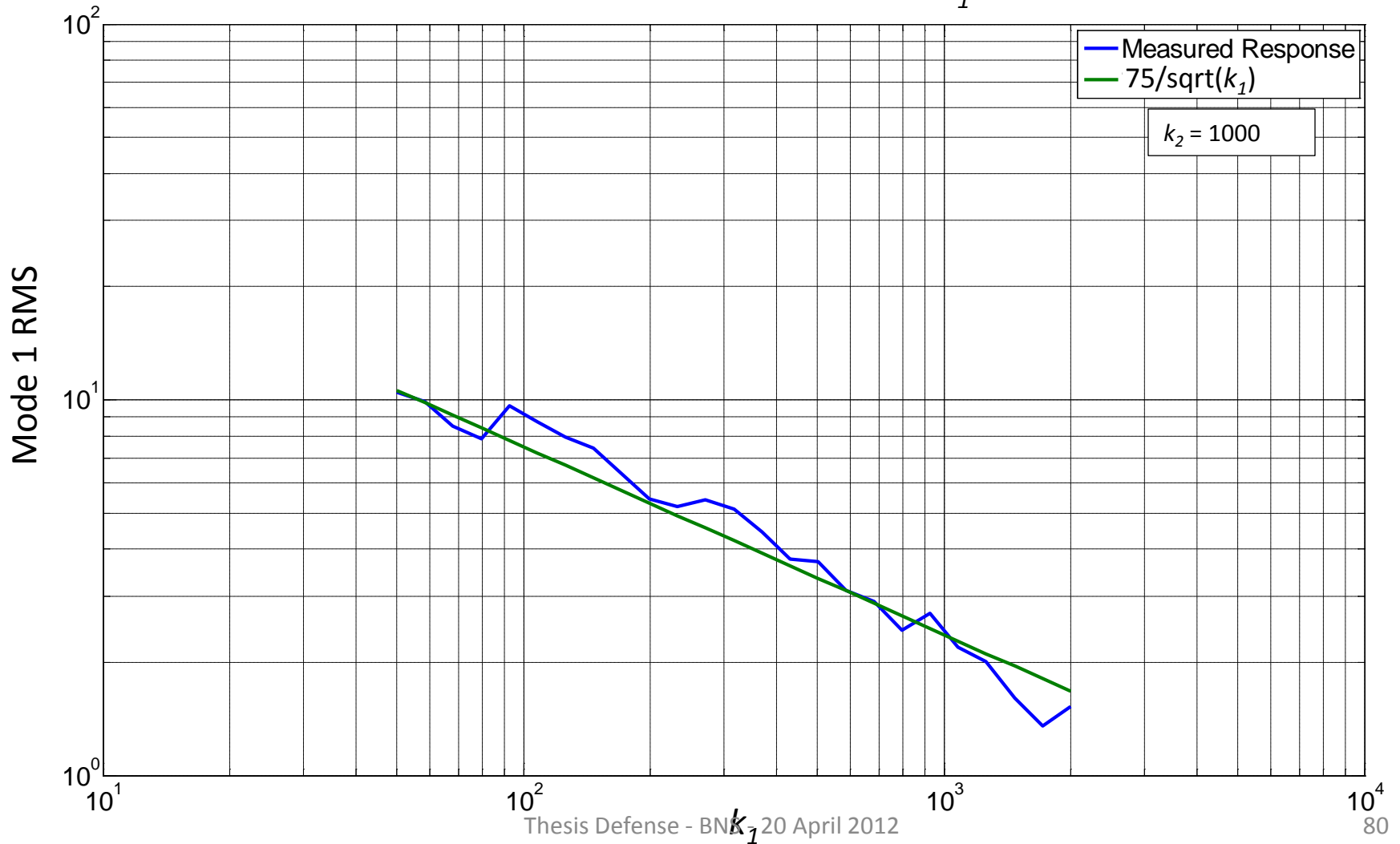


Modal RMS Scaling

# Backups: Measurement of modal RMS dependence of damping gain (Jacobian Measurement)

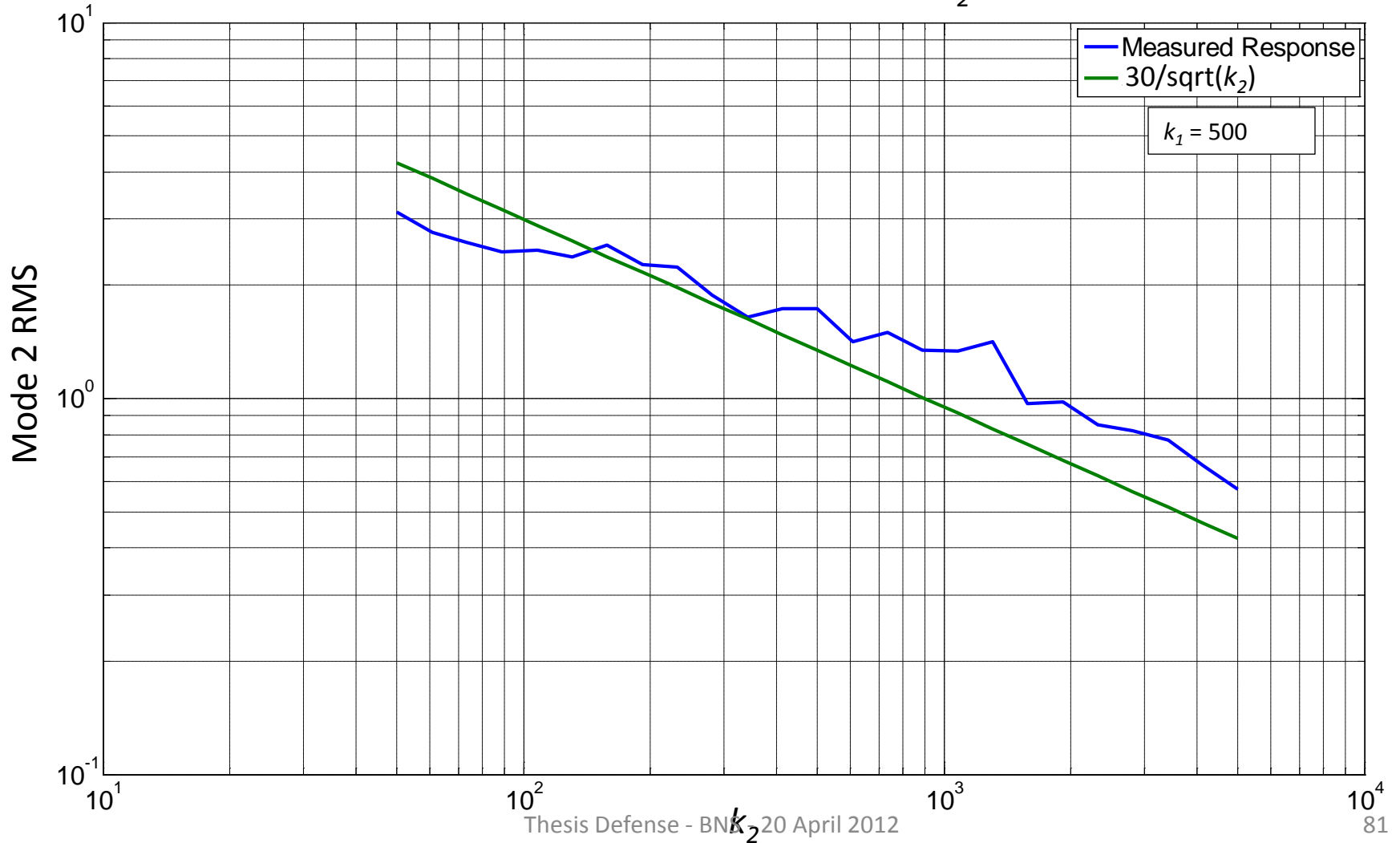
# Backups: Jacobian Measurement

Mode 1 RMS as a function of  $k_1$



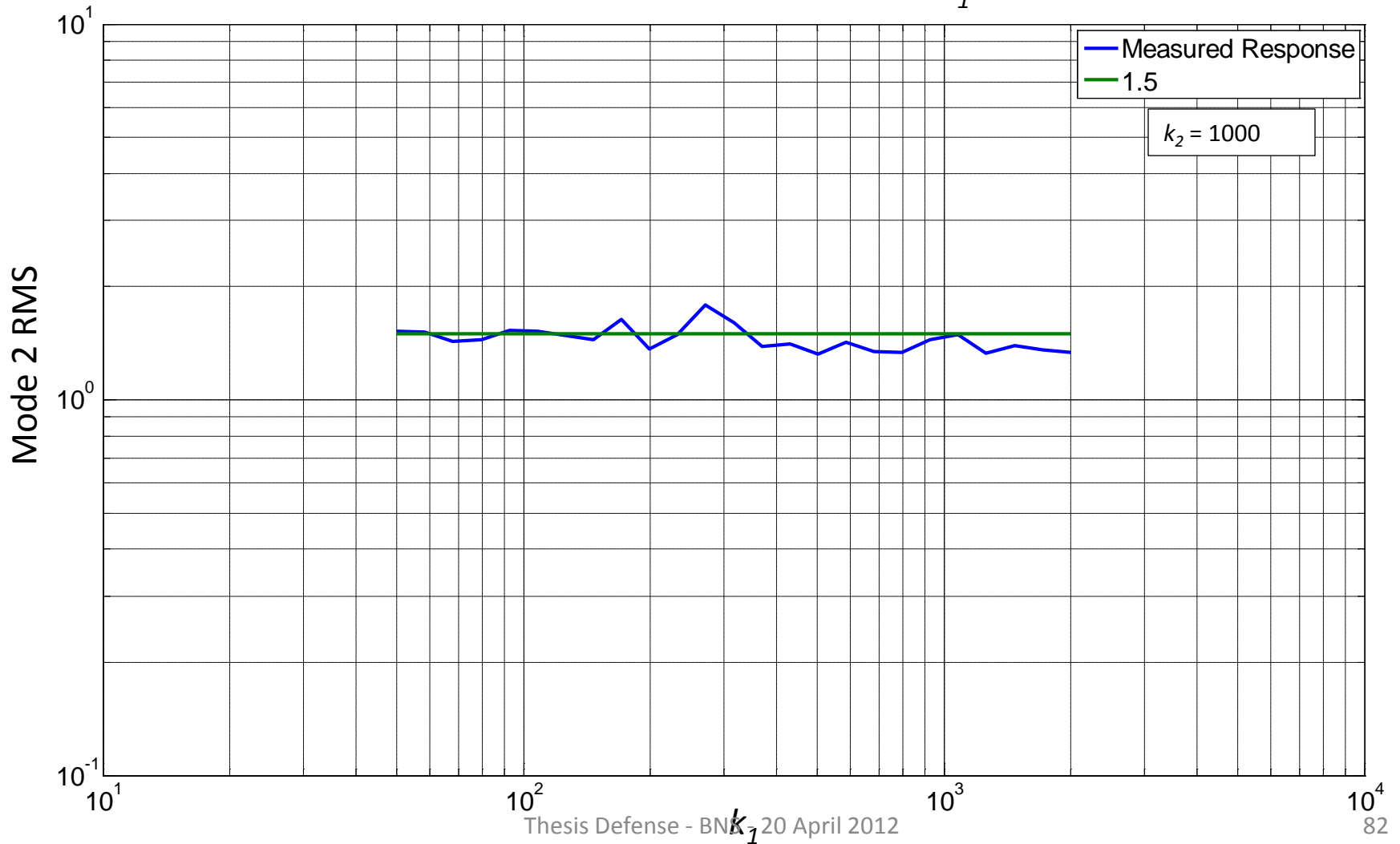
# Backups: Jacobian Measurement

Mode 2 RMS as a function of  $k_2$



# Backups: Jacobian Measurement

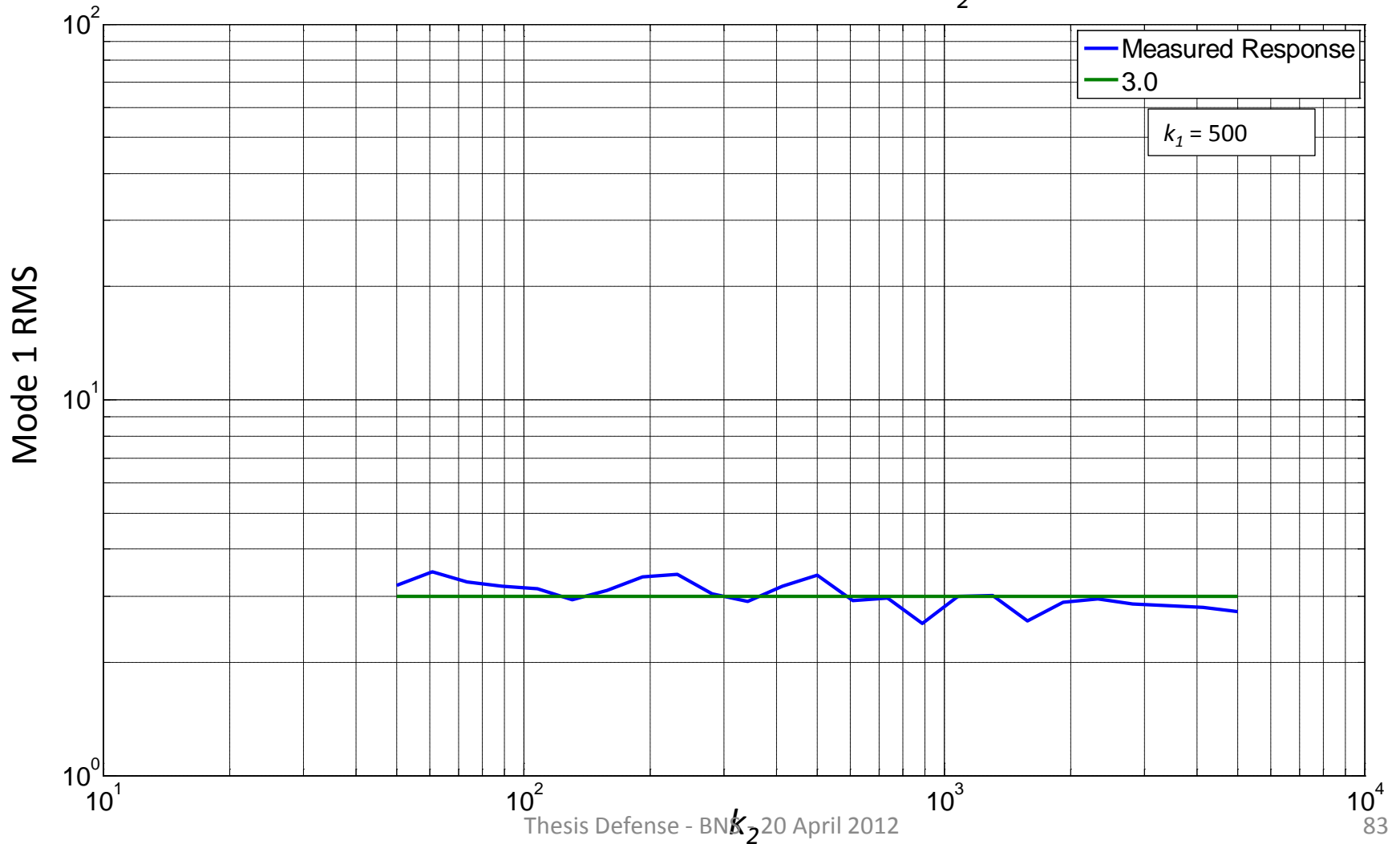
Mode 2 RMS as a function of  $k_1$





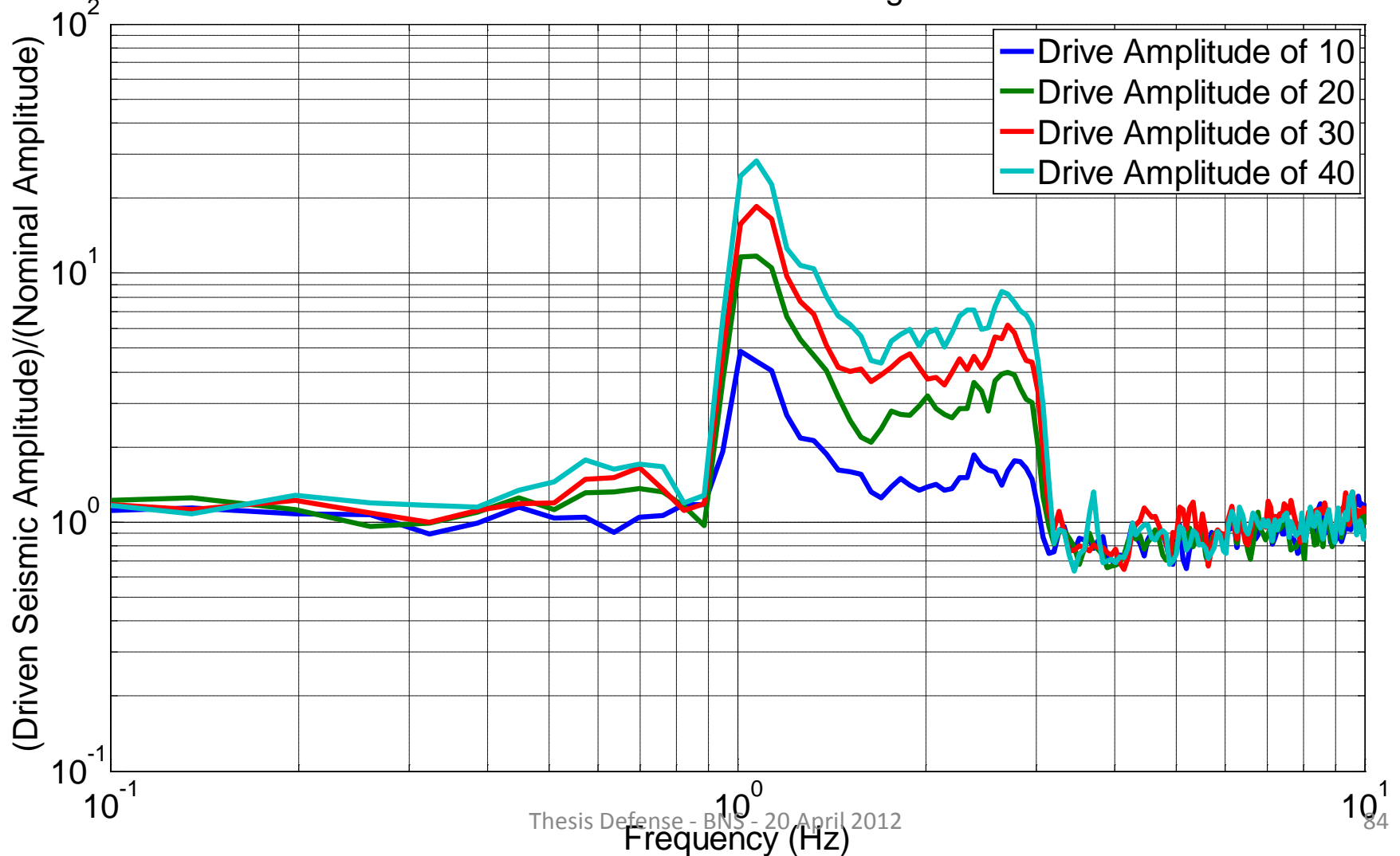
# Backups: Jacobian Measurement

Mode 1 RMS as a function of  $k_2$



# Backups: Driven Seismic Amplitudes

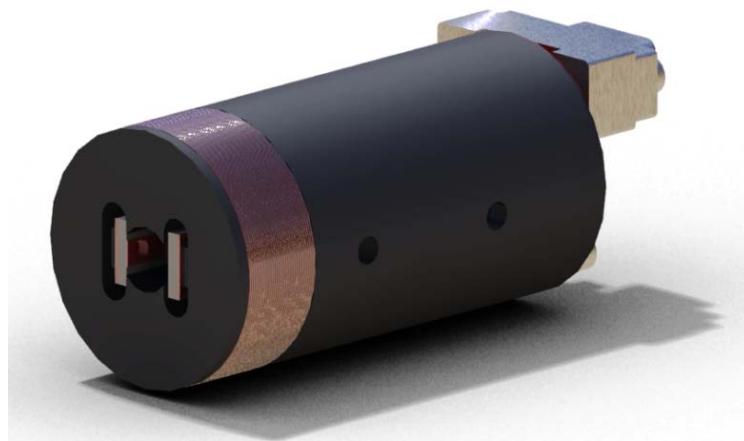
Measured Seismic Enhancement Factor Driving the Table: 17 June 2011



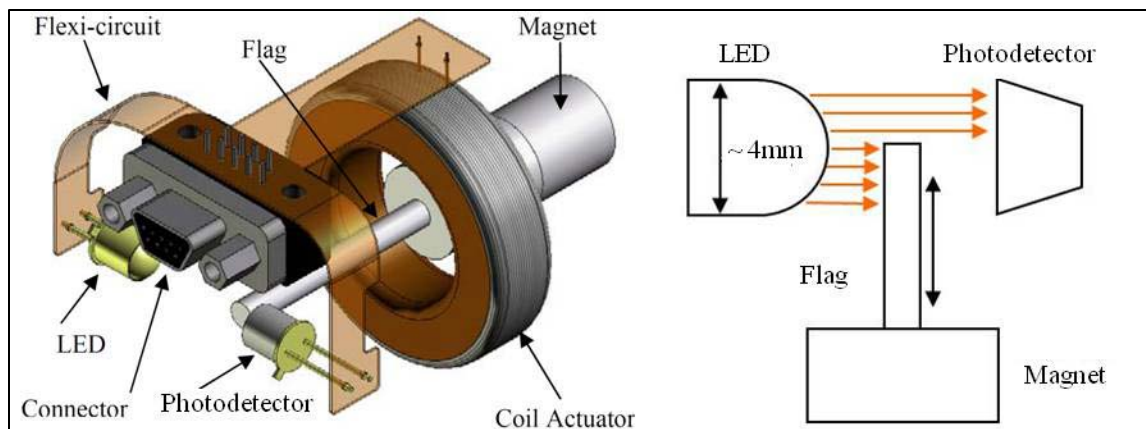
# Backups: Optical Sensor ElectroMagnet (OSEM)



Birmingham OSEM (BOSEM)



Advanced LIGO OSEM (AOSEM)  
- modified iLIGO OSEM



BOSEM Schematic

## Magnet Types (M0900034)

- BOSEM – 10 X 10 mm, NdFeB , SmCo

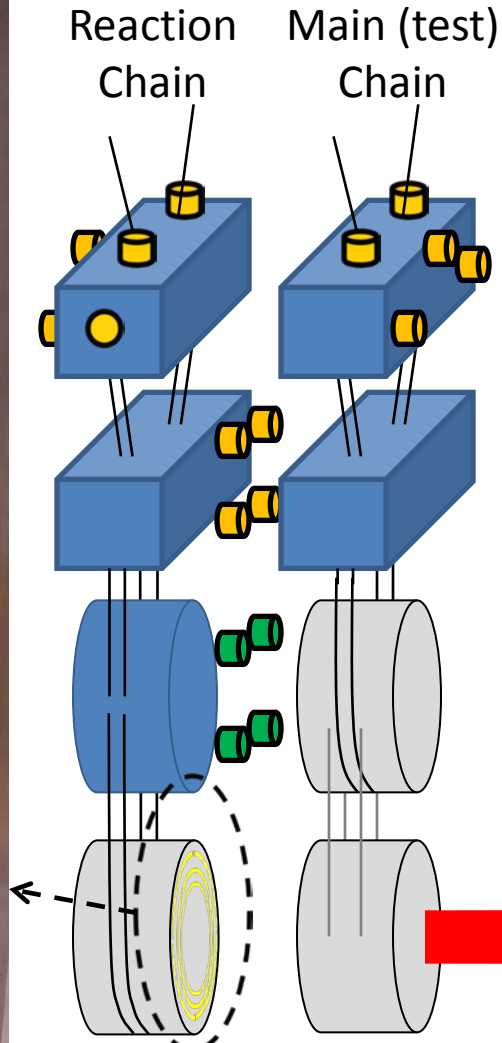
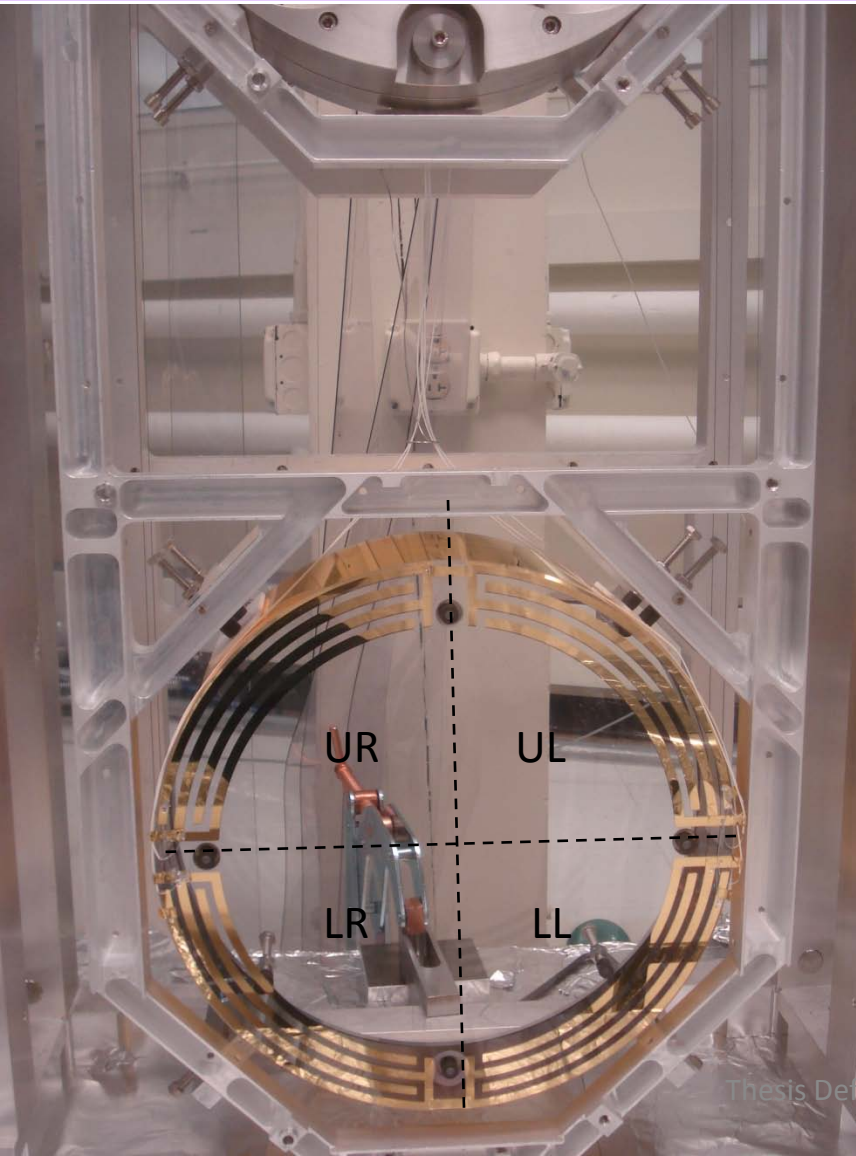
10 X 5 mm, NdFeB, SmCo

- AOSEM – 2 X 3 mm, SmCo

2 X 6 mm, SmCo

2 X 0.5 mm, SmCo

# Backups: Quadruple Suspension ESD

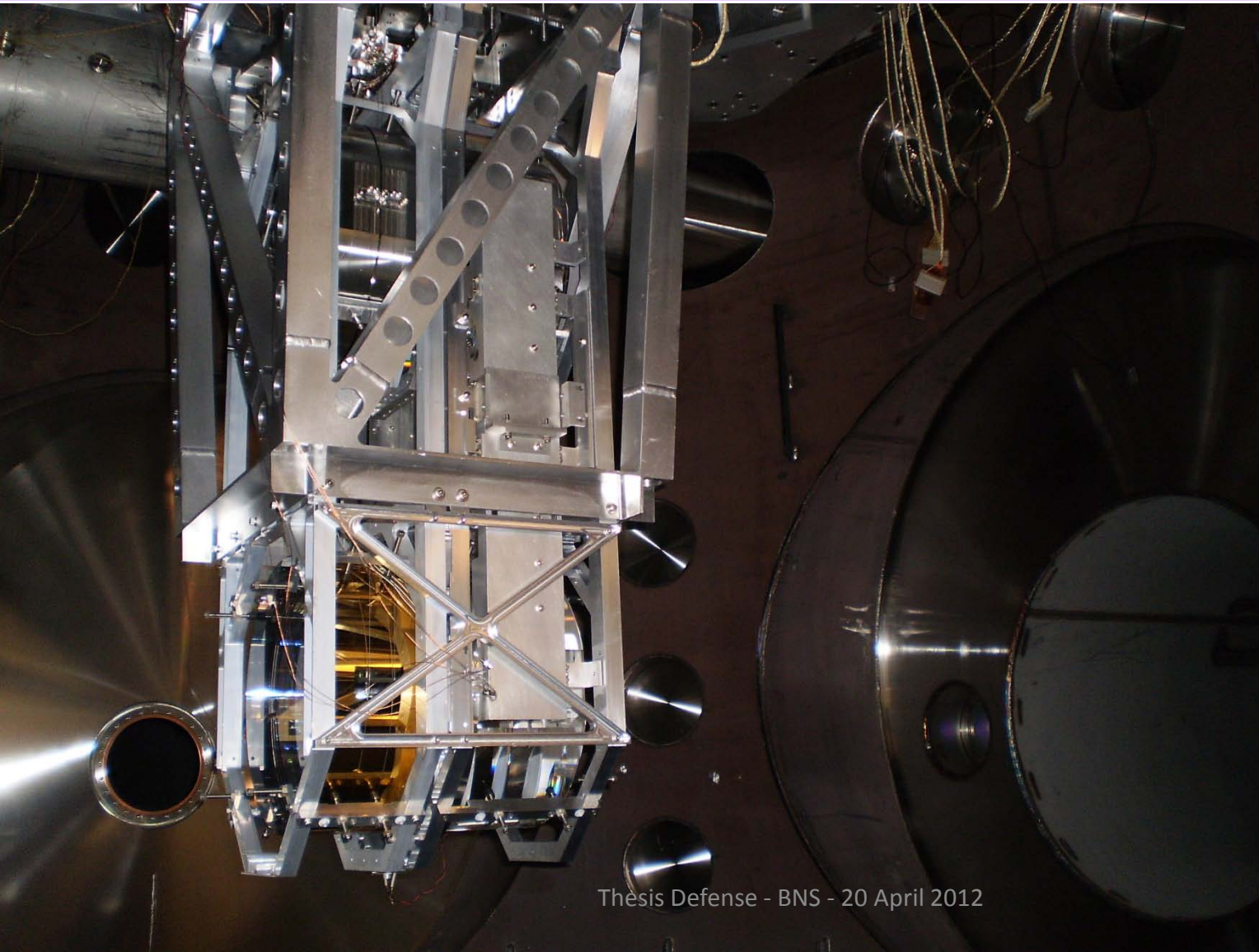


The electrostatic drive (ESD) acts directly on the test ITM and ETM test masses.

- $\pm 400 \text{ V}$  ( $\Delta V 800 \text{ V}$ )  
 $\approx 100 \mu\text{N}$
- Each quadrant has an independent control channel
- Common bias channel over all quadrants



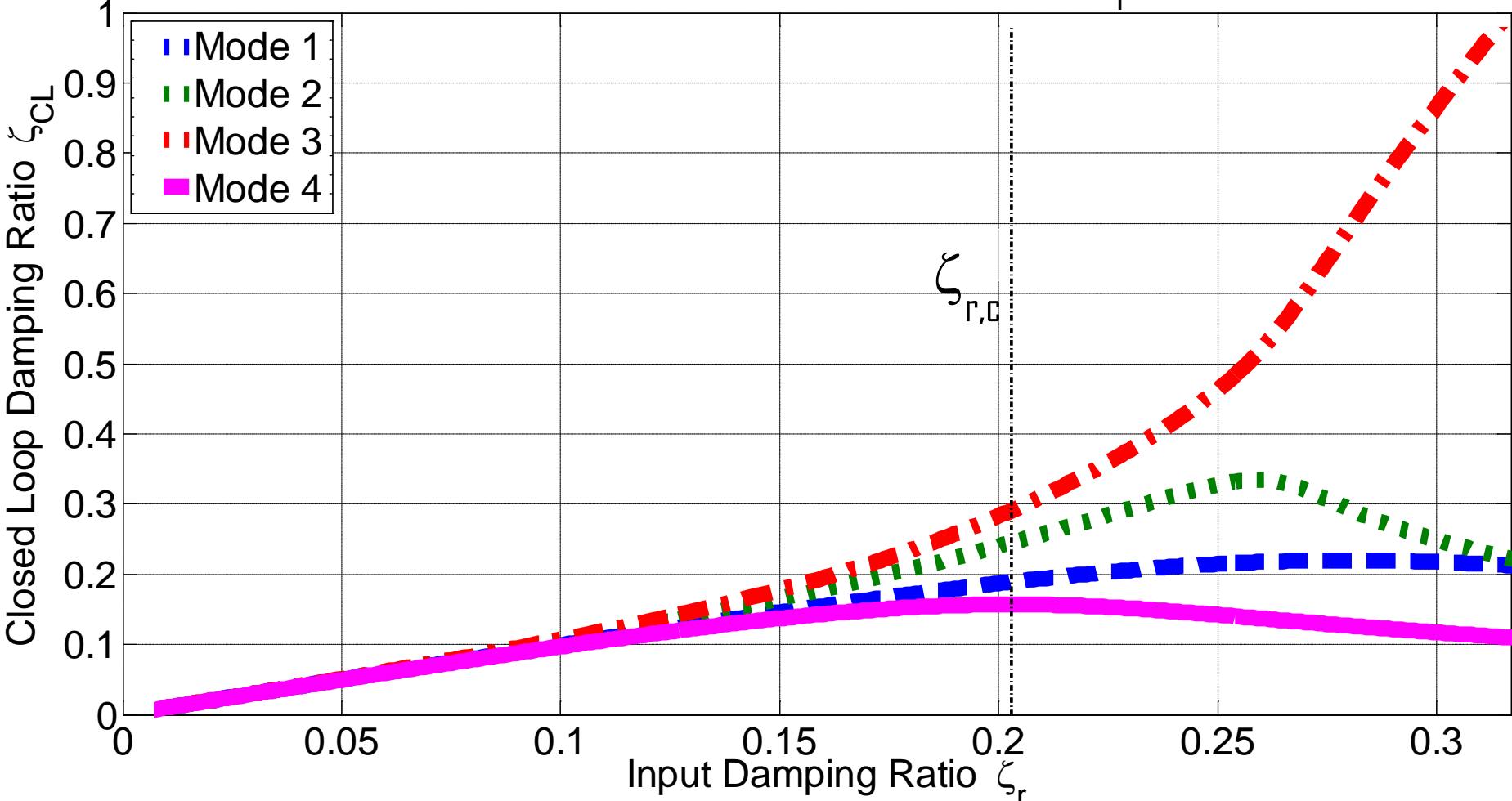
# Backups: Quadruple Suspension



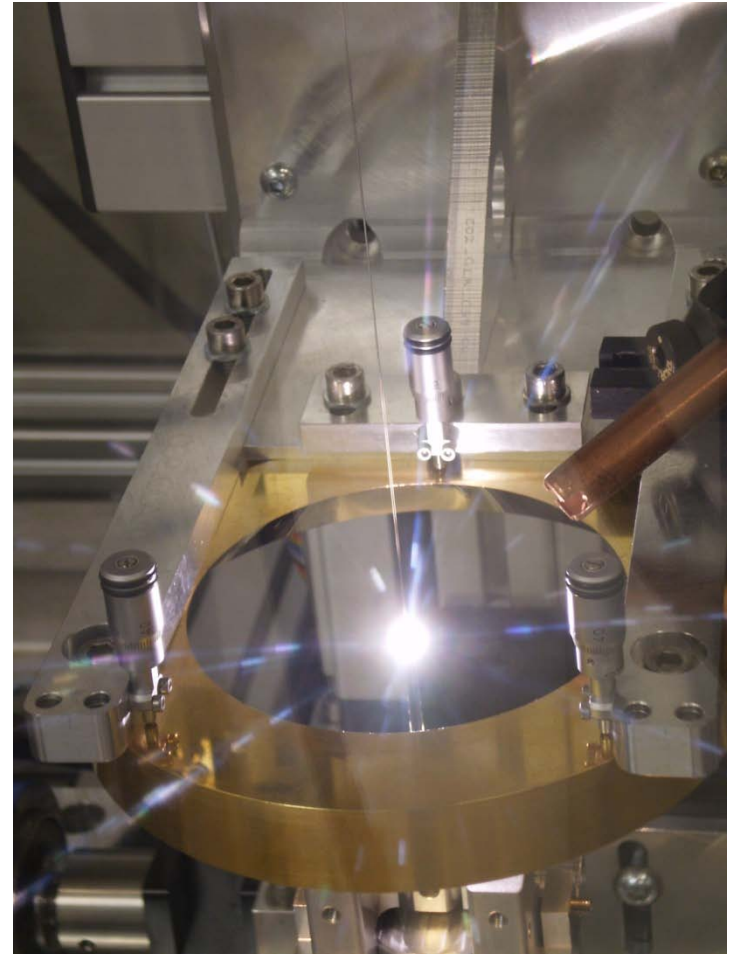
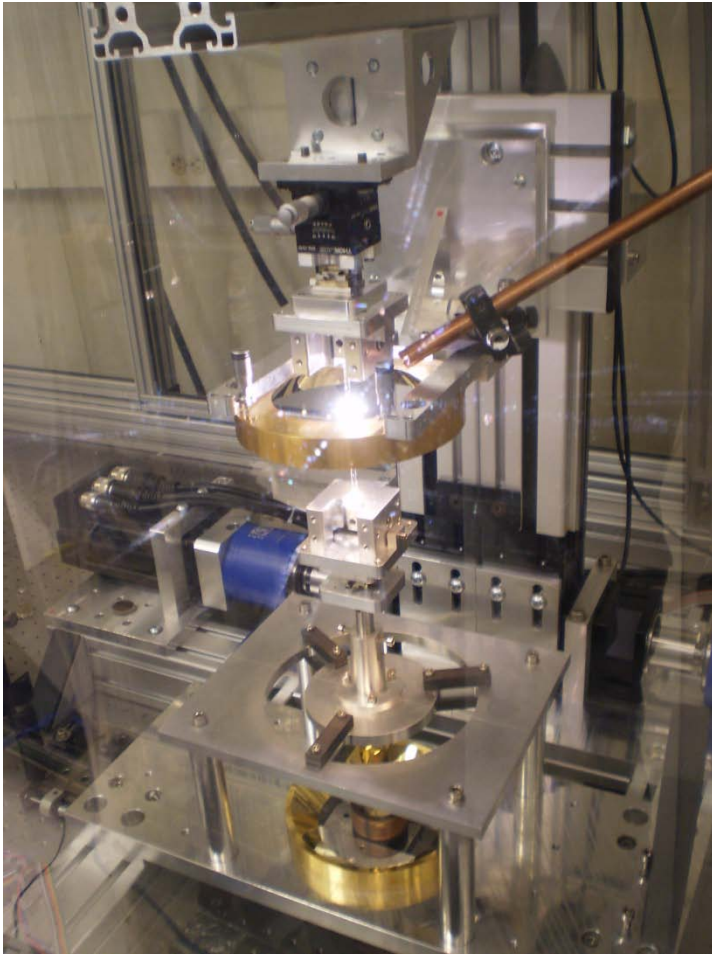
MIT  
monolithic  
quad in BSC

June 2010

Closed Loop Damping Ratios vs.  $\zeta_r$

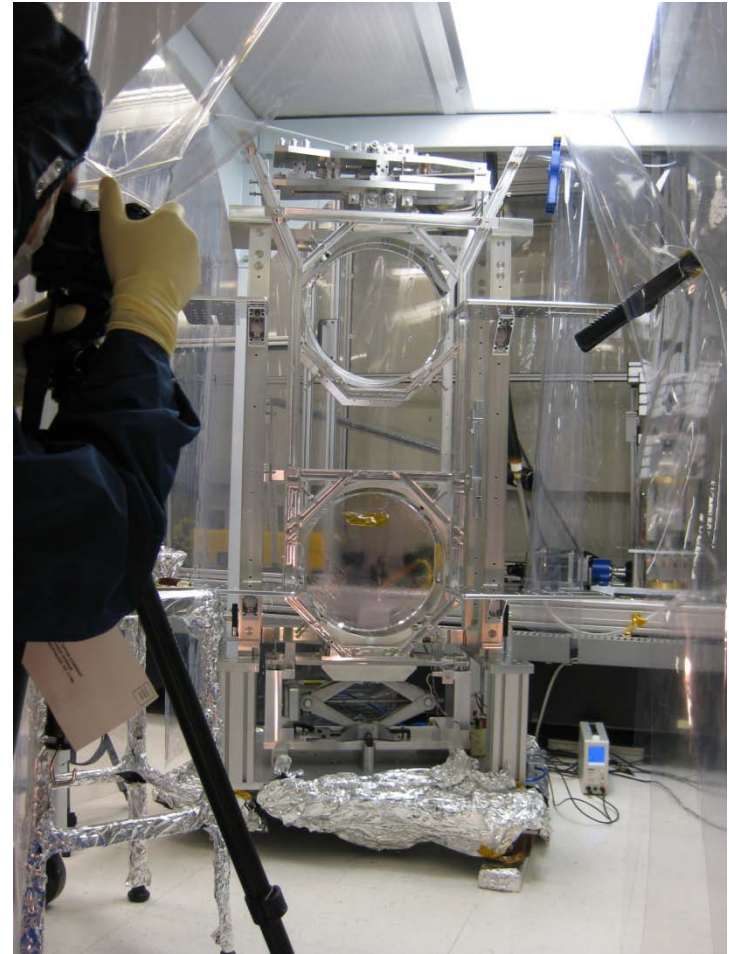


# Pulling Fibers

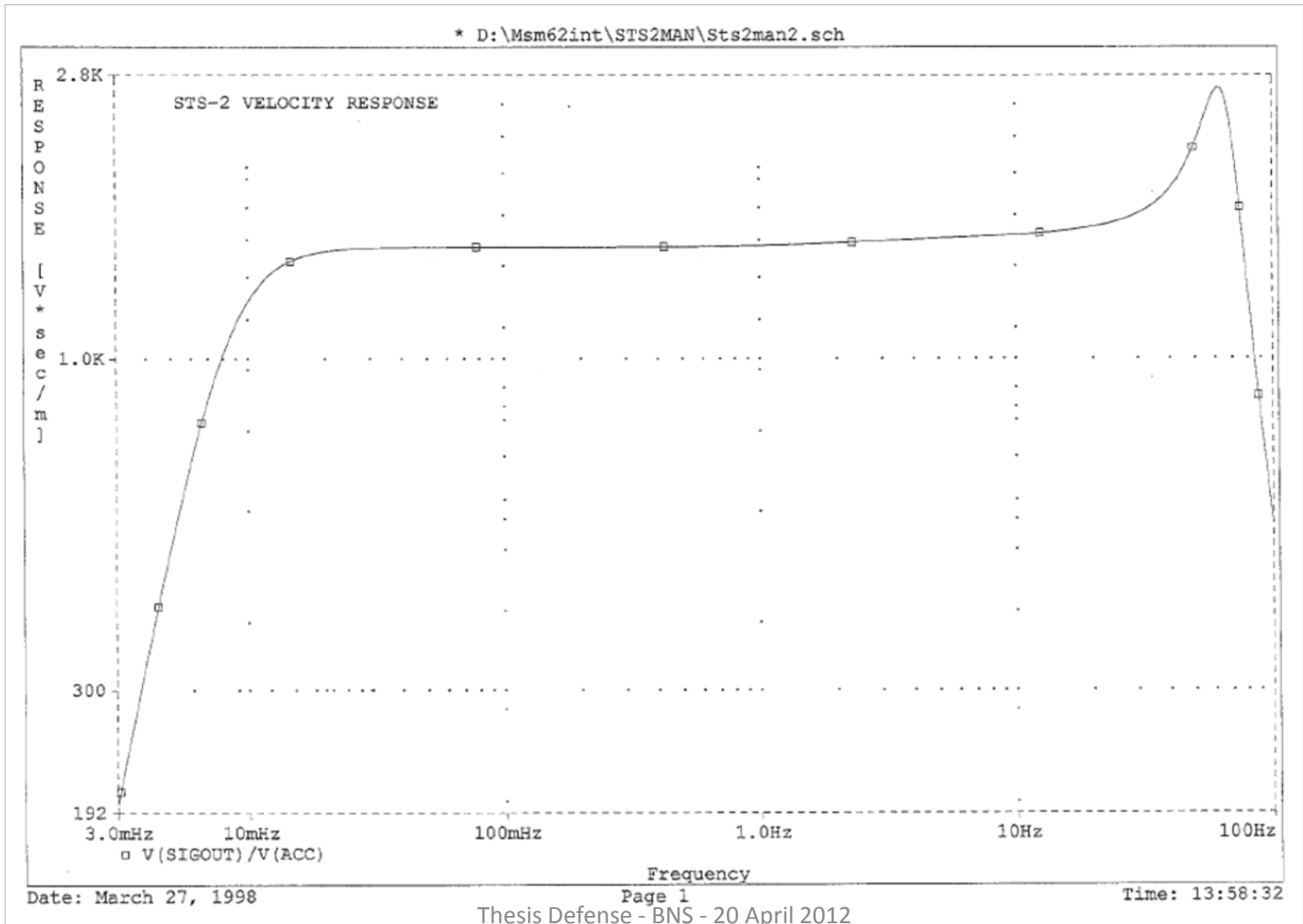




# Quad Monolithic Stages



# Streckeisen STS-2 Seismometer



# Scratch

LIGO GW sources with sound files  
<http://www.ligo.org/science//GW-Burst.php>