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Advanced LIGO

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**Thermal Compensation System (TCS):
CO2 Laser Projection System (CO2P):
Final Design Document**

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1 Introduction

The purpose of this document is to provide a guided overview of the final design of the TCS CO₂ laser projection system (CO2P) for Advanced LIGO (aLIGO), making reference to external documents where necessary. With this document, the final design review (FDR) committee is to determine whether:

1. The CO2P satisfies requirements for TCS actuation on the compensator plate while performing with minimal noise
2. The procurement plan CO2P equipment is adequate
3. Installation of the CO2P can be achieved within the aLIGO Project schedule
4. Sufficiently mature plans exist to ensure continuous reliable operation of the CO2P
5. Costing has been reconciled with the baseline budget
6. Safety concerns have been addressed
7. Interfaces have been defined

All the links presented here are also accessible from the [DCC entry for this document](#).

2 Priority Issues identified for consideration

This section presents unresolved issues up front.

2.1 Outstanding issues

- **Modeling:**
 - Analytical validation of electrical and mechanical noise, for all of the actual components, has not been completed.

2.2 Risk reduction proposals

- Ongoing modeling of interferometer and signal recycling cavity. This modeling will serve to help us understand the operation of TCS and may feedback to requirements on the laser projection system to improve ease of use. [Operations and beyond]
- Use of raster scanning to reduce the effects of changing beam shape. This is difficult to implement due to noise couplings and potentially may suffer from up-conversion. [Operations and beyond]

2.3 Early approval

We request that the FDR committee approve the following items ASAP:

- One possible way to supply adequate power to the RF driver for the laser is to assembly standard 24V supplies in series. Alternatively, a vendor for a custom (linear) supply with >28V and 28A must be identified as soon as possible. In this alternative case, support from Project Systems (SYS) and Controls (CDS) is

requested. A candidate switching supply ([model 6684A, from Agilent](#)) has been identified by the CDS group; the TCS group would like to purchase and evaluate one in the lab at Caltech as early as possible. However, this implementation requires approval from the aLIGO SYStems group.

- Designs for two unique steering mirror assemblies ([D1101013-v1](#) and [D1101851-v1](#)) required for guiding the CO₂ laser onto compensation plates within BSC's 1, 2 and 3, serving H1 and L1, are on the critical path to meeting need-by dates at LLO. (Note that the hard-gold-coated copper mirror, [D1101014-v4](#), for the SM1 assembly [D1101013-v1](#) has been received from the manufacturer in December 2011; the associated machined parts have been cost-estimated, but not procured. Detailed drawings of the parts belonging to assembly [D1101851-v1](#) are currently being completed; associated cost estimations have not yet been sought.)

3 CO2P Requirements

This section summarizes requirements for the laser projection system and references documents that provide more detail.

3.1 Conceptual Design Requirements

Top-level requirements are described in detail in [T000092](#) where the primary requirements for TCS are derived from the LIGO principal science requirements. A list of these top-level requirements is given in

Table 1.

Table 1: Top level requirements (interferometer level)

Parameter	Required performance
Sideband extraction through SR cavity	>95% of nominal value (equivalent to phase error of 0.08 radians, or a round trip SR cavity loss of <0.1%)
TCS compensation profile	>112mm centered on optic
CP motion noise	< $(2 \cdot \textit{finesse} / \pi)$ times the technical noise spectrum for test mass shown in Figure 1.

No requirement is set for the CO₂P beam centering on the CP since the phase profile of the CP will be measured directly allowing for fine alignment after installation.

A detailed description of couplings between noise in the CO₂P and the interferometer can be found in [T060224](#), along with the resulting requirements for the CO₂P system. We list these requirements in this section for convenience.

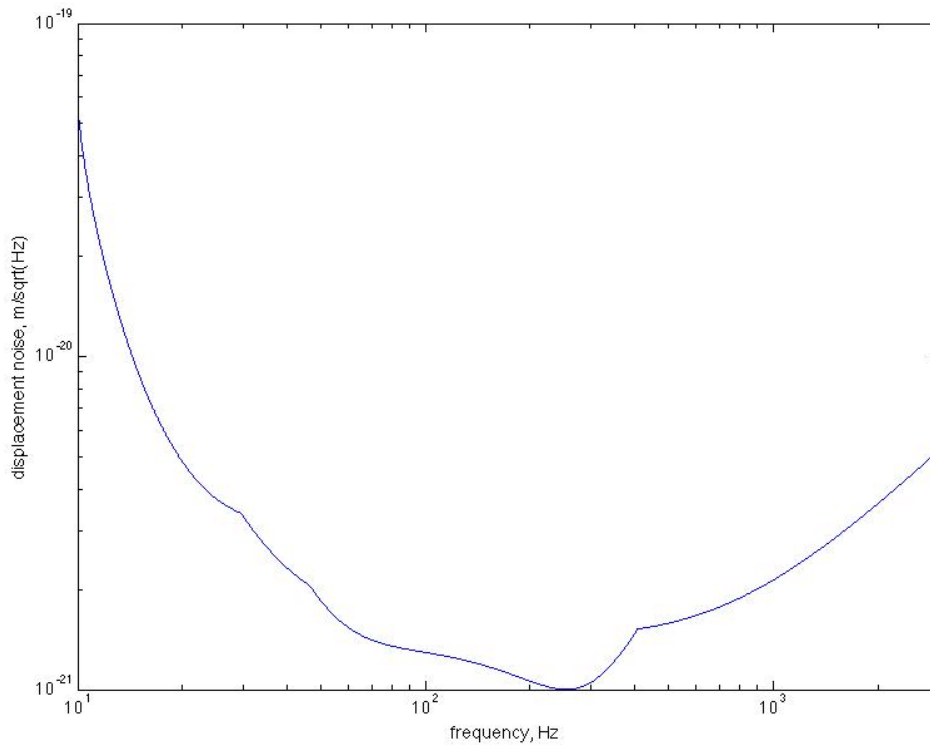


Figure 1: Maximum allowable technical displacement noise of the aLIGO test mass.

3.1.1 Amplitude noise requirement

Figure 1 shows the maximum allowable motion of the HR surface of the test mass. Since the CP is in the recycling cavity the surface motion requirement is relaxed by a factor of $2 \cdot \textit{finesse} / \pi$, where *finesse* is the finesse of the arm cavity.

The amplitude noise of the CO2P system couples to the displacement noise of the CP by two primary mechanisms – thermorefractive and thermoelastic coupling. In practice the thermorefractive effect is approximately 10 times larger than the thermoelastic coupling. There are other coupling mechanisms (flexure, elasto-optic) that have been shown to be negligible.

Calculation of the effects of absorption of a fluctuating power source with an annular spatial distribution are given in Section 5 and 6 of [T060224](#). This calculation includes the effects of both thermorefractive and thermoelastic coupling. Using this to calculate the amplitude noise spectrum requirement for the CO2P gives the curve in Figure 2.

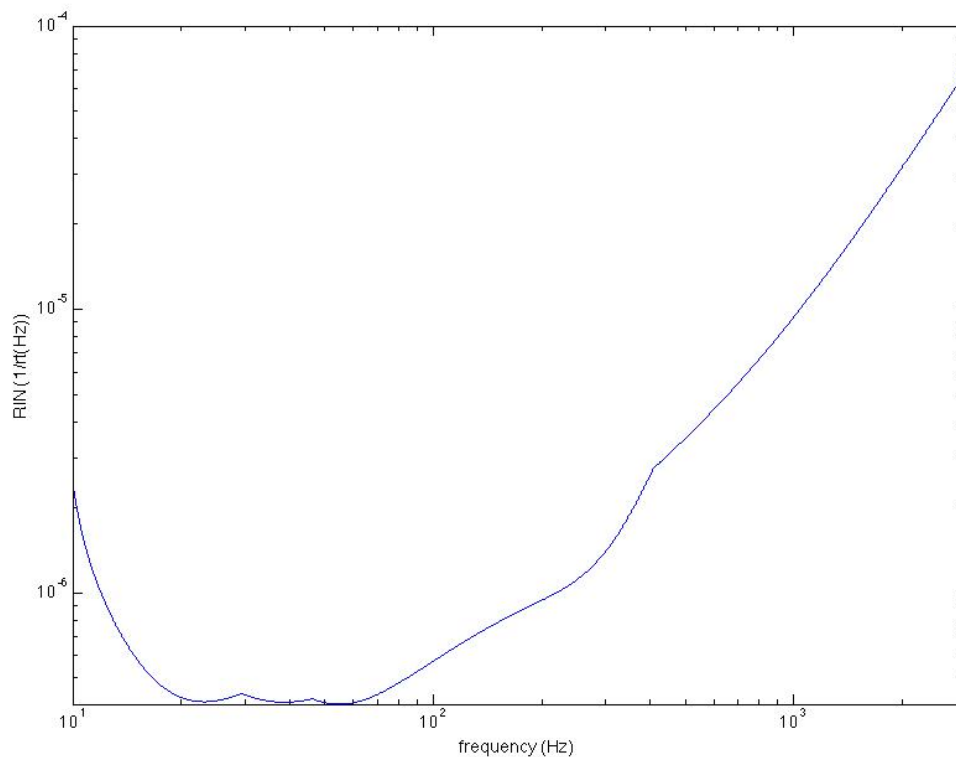


Figure 2: Amplitude noise requirement for the CO2P

To meet this requirement the laser will be followed by an intensity stabilization servo similar to that used in eLIGO, using an IntraAction AOM to modulate the amplitude.

Calculations given in [T060224](#) show it should be possible to achieve a RIN of less than 2×10^{-7} across this frequency range, based on the use of the same type of VIGO systems HgCdTe diodes used in eLIGO. Again a preamp of IF3602 FET followed by an LT1128, is proposed.

The RIN of the unstabilized Access laser has been measured and shown to be slightly lower than that of the Synrad shown in Figure 5 of [T060224](#).

3.1.2 Jitter noise requirement

Two possible jitter mechanisms are identified in [T060224](#), these being angle of incidence of the CO2P on the CP and displacement of the CO2P beam relative to the IFO beam. However for any given angular variation in the incident beam, due to the long projection distance, the effect on displacement of the beam is a far larger effect.

The effect of displacement jitter is strongly dependent on the alignment of the TCS beam. If aligned perfectly there is no coupling to first order. The displacement requirement derived in [T060224](#) is for a displacement of the TCS beam by 1mm, and is shown in Figure 3. The noise requirement must be reduced linearly with increasing offset (ie if the offset is 2mm then the requirement becomes twice as stringent).

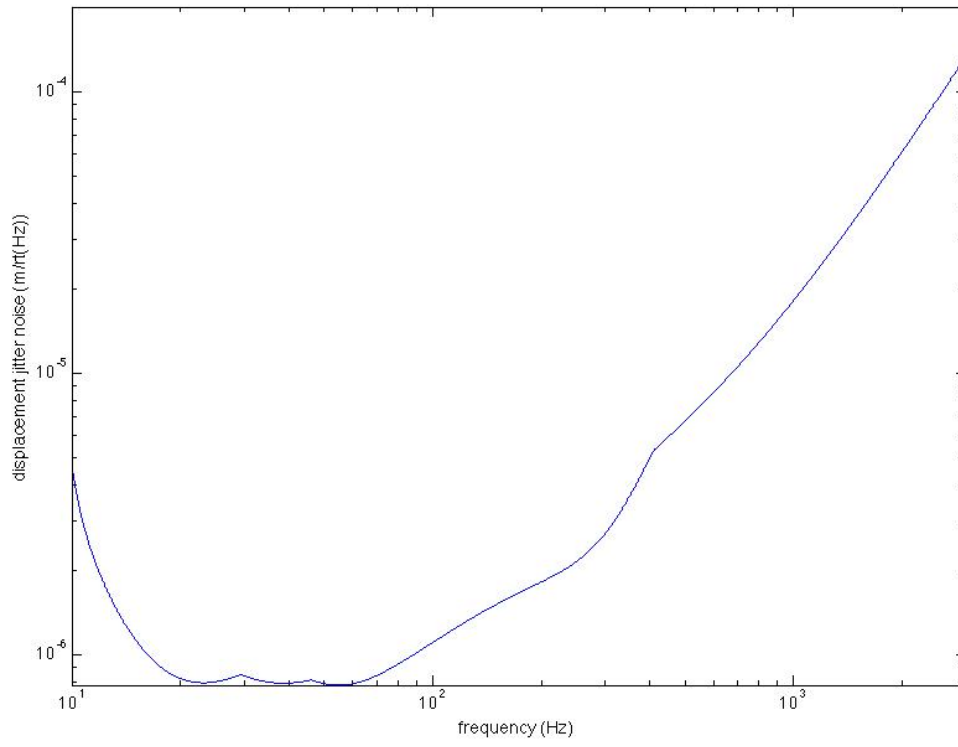


Figure 3: Jitter noise requirement for variations in overlap of TCS and IFO beams

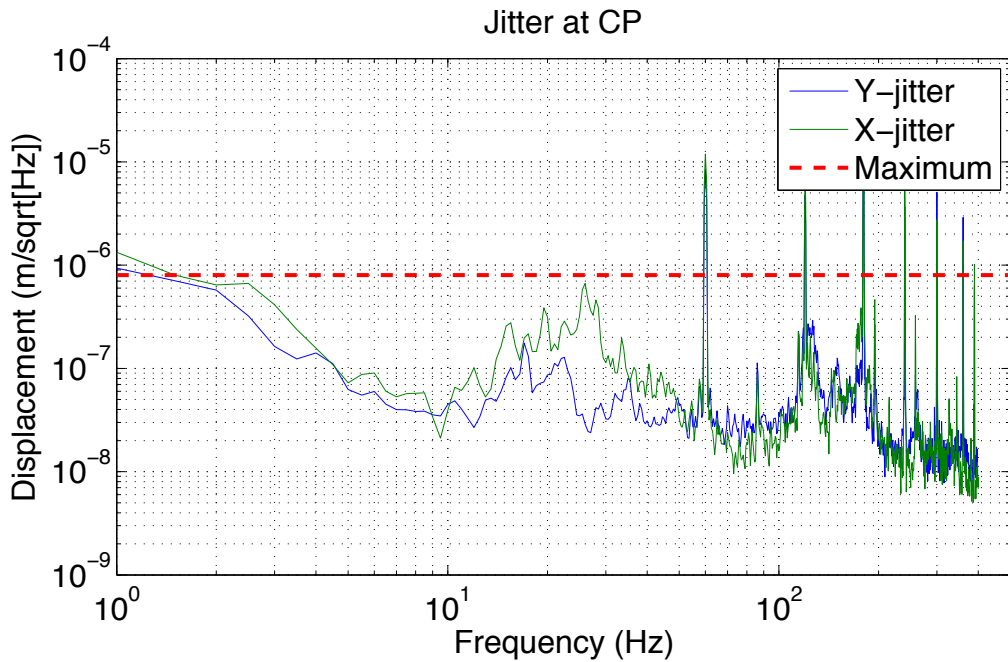
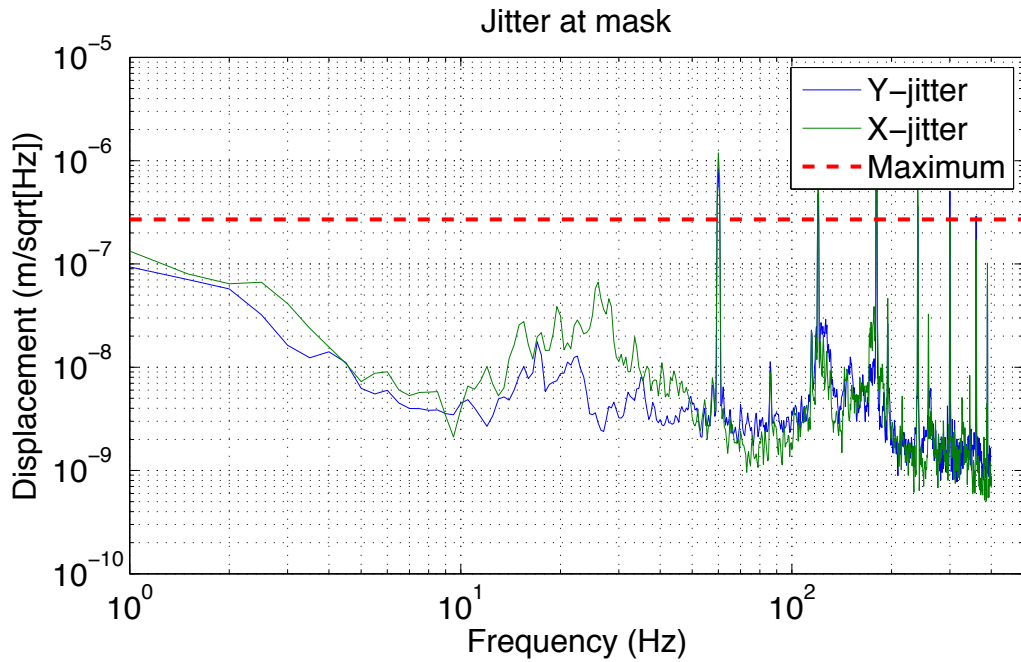
With a significant projection distance, we convert this into an angular jitter requirement for the CO2P. For H2 with a projection distance of approximately 30m, this becomes a requirement of 1×10^{-7} m at 10Hz.

Please note that the baseline final design contains no active jitter control system.

The jitter noise can however be nulled by aligning the input beam using a shaker on the TCS table and moving the alignment until the peak is no longer visible in DARM. This method has been previously used in eLIGO. Any drift in alignment from the laser or AOM will be removed on with the pico-motor and QPD system periodically when the detector is not in science mode.

The measured angular resolution for steering the beam reflected of the picomotor mirrors is 400 nano-radians. When the picomotor mirrors are placed approximately 800mm away from the mask, the smallest beam motion on the mask is approximately 300nm which is approximately 2000x finer resolution necessary than the maximum tolerable 0.6mm beam-mask displacement. Therefore, the picomotor have sufficient resolution to optimize the beam position on the mask.

The jitter noise for the aLIGO CO2 lasers was measured and was determined to be smaller than the minimum acceptable level across the entire audio band, as illustrated in Figure 4. Therefore, no active jitter control system is needed for baseline aLIGO TCS.



/Users/aidanbrooks/Documents/LIGO/documents/Advanced_LIGO/TCS/TCS_SVN/LIGO/test data/CO2/jitter/cit/access_laser_SN_12752-13234D/plot_beam_jitter_data.m

Figure 4: Measured beam jitter from Access Laser SN 12752-13234D

3.2 Requirements for the optical design

There are no substantive changes to the requirements for the optical design described in Section 4.2 of the [T0900304 - aLIGO Thermal Compensation System Preliminary Design](#).

Those requirements are summarized here:

- The amount of TCS power delivered to the Compensation Plate required for optimal compensation of 0.5 ppm absorption at full power is 7.5W; with the factor of two excess capacity specified in the Design Requirements, this rises to 15W.
- The projector must be capable of producing an annular heating pattern that produces a thermal lens that, when combined with the thermal lens from the ring heater, results in a residual optical path distortion that scatters less than 0.1% of the Gaussian TEM00 mode from itself on one round trip through the ITM+CP. The idealized heating pattern is described in Section 4.1.2 of [T060083 - Auxiliary Optics Support System Conceptual Design Document, Vol. 1: Thermal Compensation System](#).

3.2.1 DC requirements

3.2.1.1 Power resolution

The power projected onto the compensator plate by the CO2P is measured using two power meters, one in each beam shaping path. The total power must correct the thermal lens of the ITM+CP such that the residual optical distortion meets the 0.1% scatter in one round trip requirement, as described above. Figure 5 shows results of modeling of scattered power as a function of CO2P power for the case of an ideal correction pattern requiring 5W of annular heating power¹. From this we see that the power must be set to better than $\pm 1.5\%$. The power meters that are planned for use in the CO2P are Thorlabs S302C 2W units with a manufacturer specified resolution of $1\mu\text{W}$. This resolution is reduced when viewing the power on the controller, however the analogue output of the PM100D gives a direct amplified signal from the power meter head. In practice the resolution will be limited by our ADC to around 0.6mW, though further amplification and subtraction of offsets would reduce this. The resolution required for a measured power of 2W is $\pm 30\text{mW}$.

¹ The ideal pattern was created by subtracting the thermal lens from 0.4W of self-absorption from a flat wavefront. It was then assumed that 5.0W of annular power were required to create that ideal pattern. This ideal pattern was then scaled accordingly to determine its size at different annular power levels.

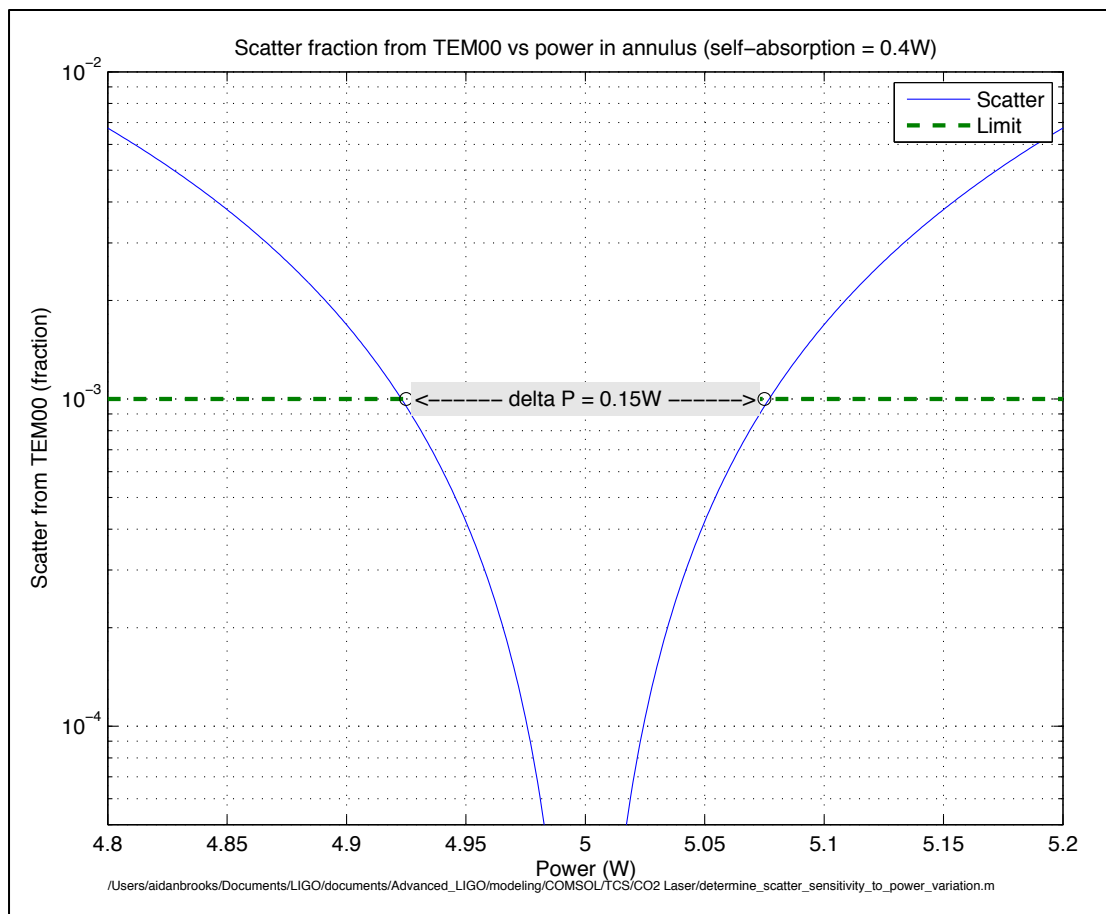


Figure 5: Scatter from TEM00 mode vs power in ideal annulus

3.2.1.2 Beam centering

As specified in Section 3.1.4.1 in [T000092-v2 Auxiliary Optics Support System Design Requirements Document, Vol. 1: Thermal Compensation System](#), “the compensated phase profile can then be sensed and used to improve the CO2 laser projector profile and alignment. For this reason, no requirement on the CO2 laser projector centering is specified”.

To expand on this:

- The picomotor mirrors on the upper periscope mirror have an angular resolution of approximately 220nrad and this corresponds to 440nrad resolution for the reflected beam.
- With the 12m projection onto the CP, this corresponds to a alignment resolution of 5 μm . This is much smaller than the necessary spatial resolution $\sim 0.5\text{mm}$ and is therefore an acceptable level of correction
- The alignment to the center of the IFO beam can be achieved in a two stage process
 - First by aligning the center of the test mass as determined by the HWS (with an uncertainty of 2 or 3mm).
 - Secondly, by actuating with TCS and measuring the induced DC tilt in the main IFO beam with the ASC system.
 - This signal is sufficient to realign the TCS system to zero the DC induced tilt (as it must be sufficient for operation of the ASC system).

3.2.1.3 Annular beam diameter and width

We used a COMSOL model to determine the required spatial resolution of a CO2 laser beam profiler. We began by first applying a Gaussian annulus to a compensation plate (CP) and determining the optical path distortion (OPD). The Gaussian annulus is described by the following equation:

$$I(r) = \frac{P_{annulus}}{C_{normalization}} \exp\left(-2\left(\frac{r - r_{ann}}{w_{ann}}\right)^2\right),$$

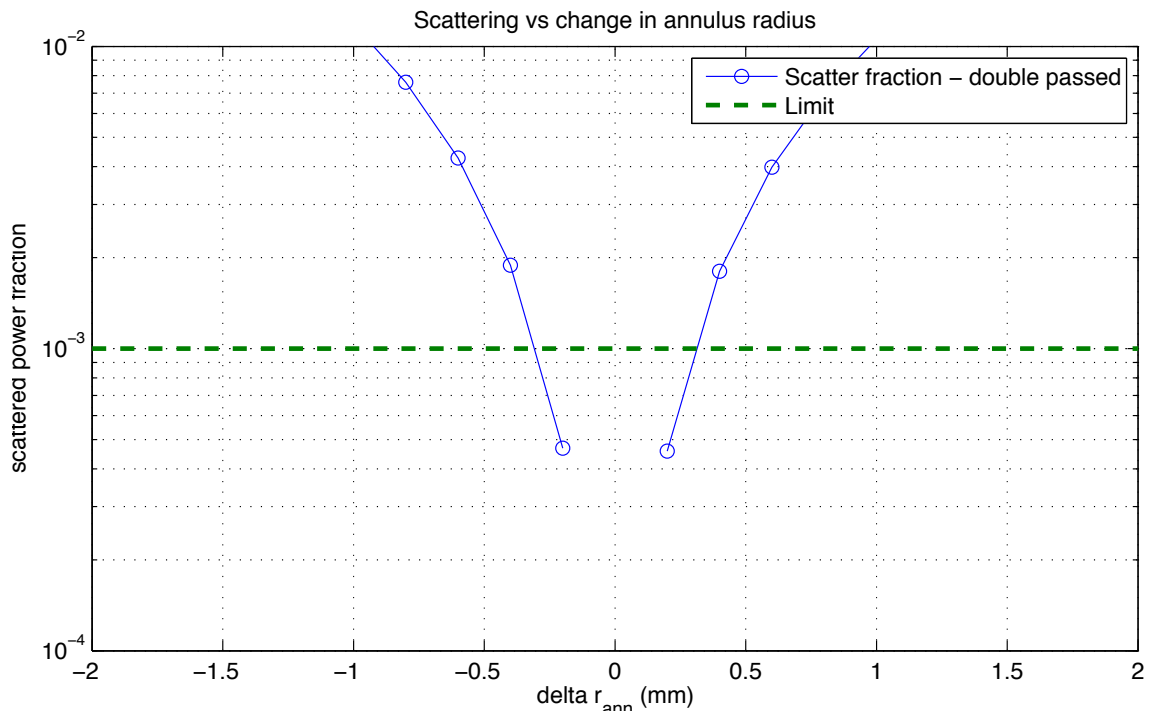
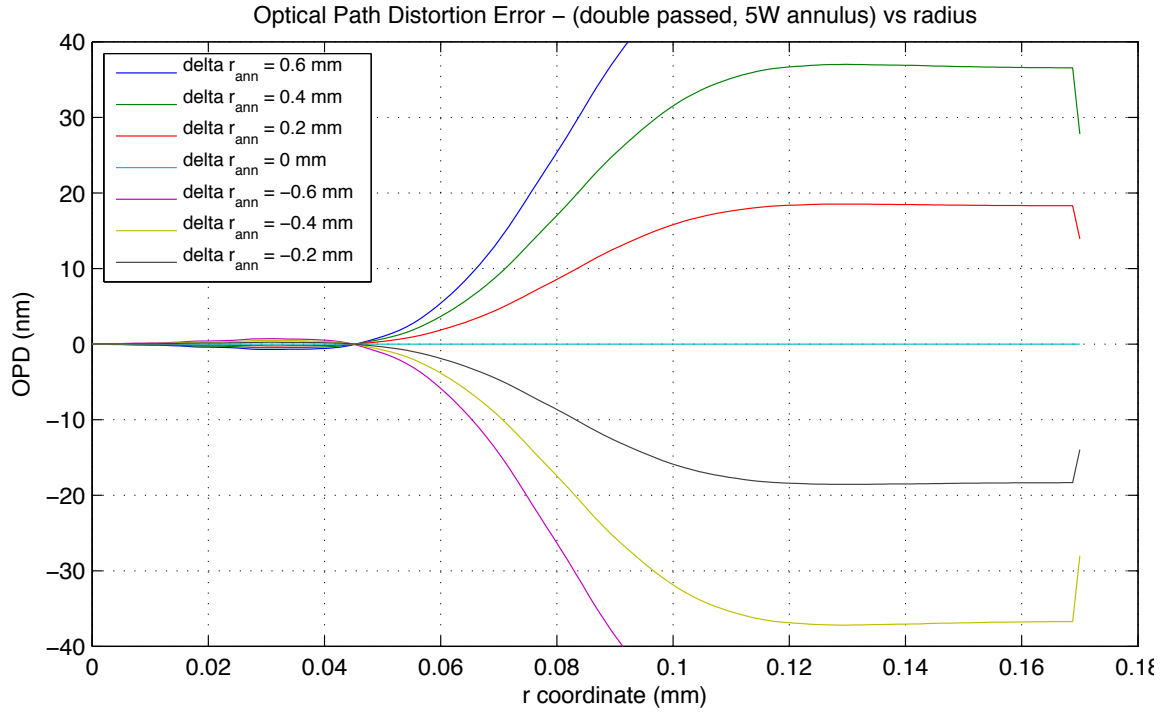
where the nominal parameters are $r_{ann} = 81\text{mm}$, $w_{ann} = 37.5\text{mm}$ and $P_{annulus} = 5.0\text{W}$.

We assumed that this OPD, which is close to the ideal correction pattern, was, in fact, the ideal correction pattern². That is, we assumed that this correction plus the 0.4W self-absorption of the interferometer resulted in a flat OPD (wavefront error) on the interferometer beam.

Next, we perturbed the diameter ($2 r_{ann}$) and diameter ($2 w_{ann}$) parameters of the annulus from the nominal values and determined the difference in the wavefront error between the two cases (for a beam that is double passed through the ITM+CP). This difference represented the residual wavefront error left on the interferometer beam. Finally, we worked out the scatter from the interferometer TEM00 mode given this wavefront error. The residual OPDs (double-passed through the optic) and the corresponding scatter for the two cases are plotted in Figure 6 and Figure 7.

The results show that the resolution of the beam profiler is limited by the radial variations in the annulus and we need a spatial resolution of better than 0.6 mm at the ITM.

² In fact, this annular pattern in the gold-barreled compensation plate will yield 2% scatter from the TEM00 on one round-trip through the residual distortion. Scatter = 2%*(P_{absorbed}/0.4W)².



/Users/aidanbrooks/Documents/LIGO/documents/Advanced_LIGO/modeling/COMSOL/TCS/CO2 Laser/data/analyze_annulus_variations.m

Figure 6: (top) Variation in OPD (wavefront error) as the annulus *radius* is varied, (bottom) scatter from TEM00 mode due to residual OPD.

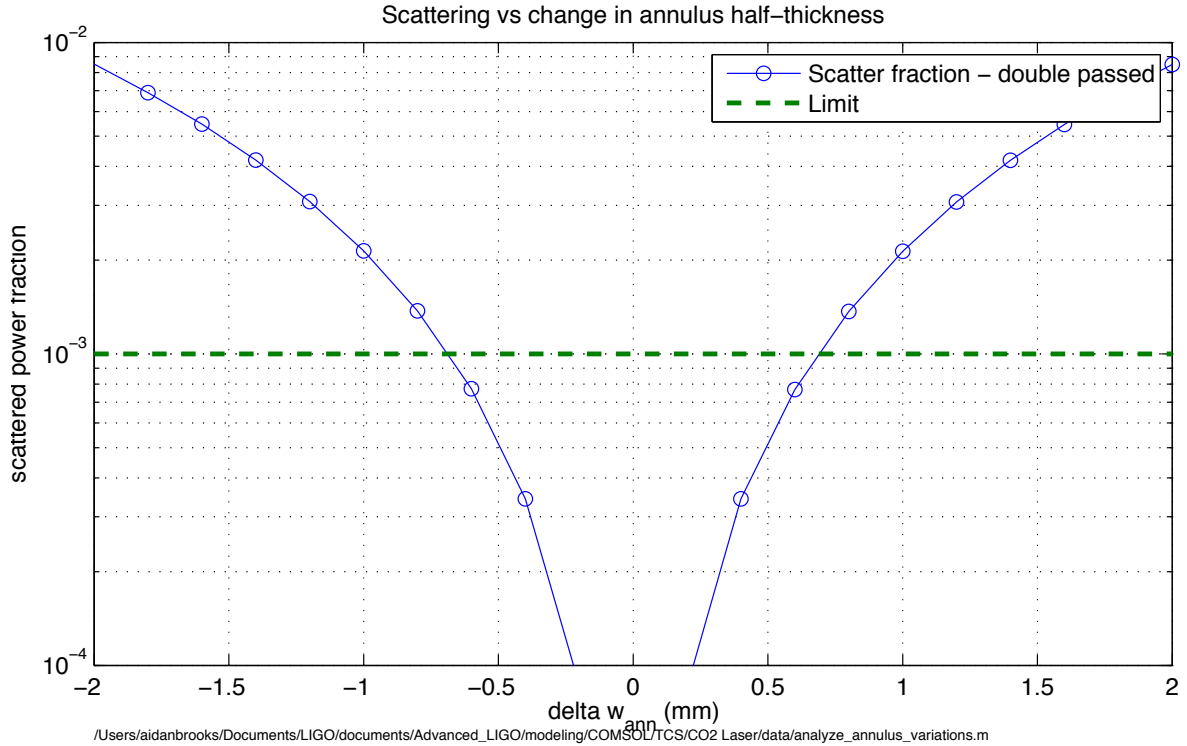
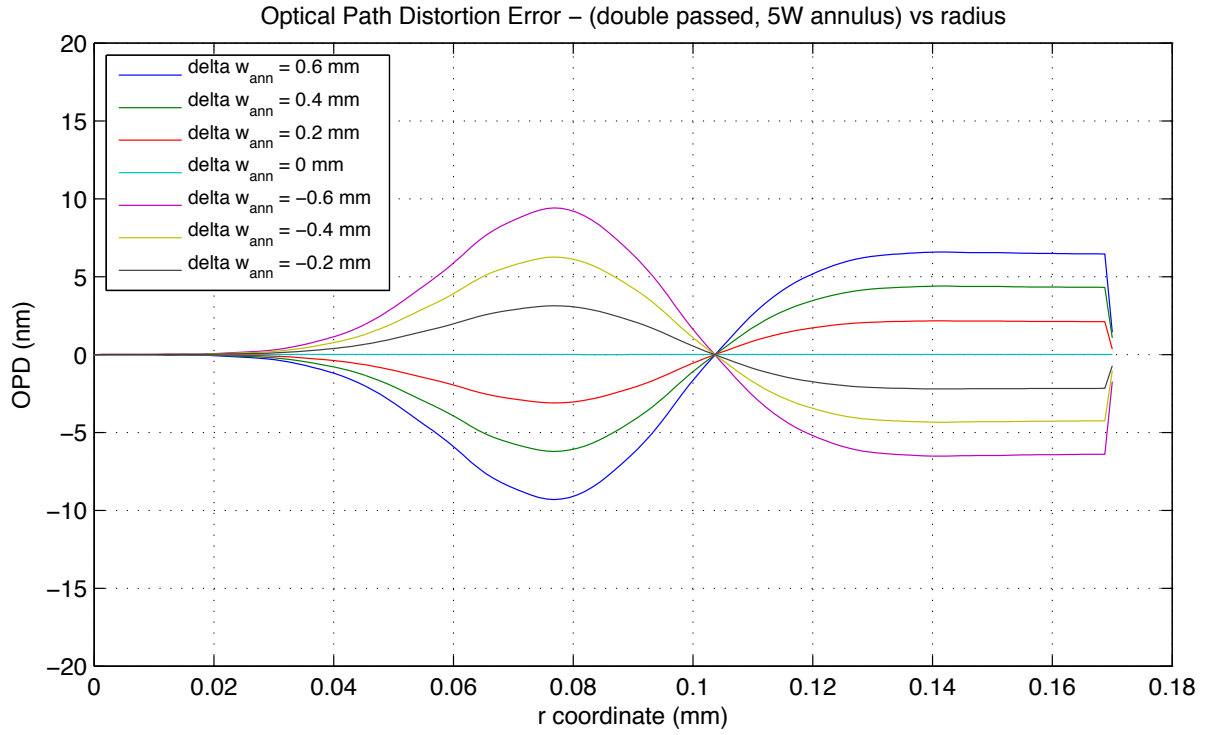


Figure 7: (top) Variation in OPD (wavefront error) as the annulus *half-thickness* is varied, (bottom) scatter from TEM00 mode due to residual OPD.

3.2.2 Requirements to prevent degradation of aLIGO performance

3.2.2.1 Reliability

The reliability of the TCS laser can be inferred from the Availability Requirements for Advanced LIGO that are specified in Section 2.3 of [T010075 - Advanced LIGO Systems Design](#):

- Single interferometer operation: 90% availability (annually integrated), minimum lock duration of 40 hours

From this requirement, we can set a limit on the reliability of each projector such that they require no more than 1 hour of maintenance/downtime every 400 hours (roughly 2 weeks).

3.2.2.2 Beam pointing

A beam pointing drift correction may will require ~30 minutes to tune the alignment of the projector system using the signals from the Hartmann sensor (due to the long thermal time constant of the fused silica CP). Therefore, this should not be required more frequently than 1 correction every 200 hours (roughly once per week).

3.2.2.3 Glitches/mode-hops

The dynamical optical requirements for the CO₂ laser were specified in [E1000065-v6 - TCS CO₂ Laser Specification](#). Requirement 3.4.1 states:

- After initial warm-up and selection of operating point, laser emission shall maintain a single longitudinal mode over time, with not more than one mode hop per 24 hours, averaged over at least 100 hours.

Based on observation of glitches in the TCS lasers in eLIGO, a mode-hop in the laser results in 10-20s of contaminated data at the output of the GW interferometer but does not, typically, cause a lock-loss. This requirement translates to a reduction on ~0.02% in the availability of the interferometer.

4 Architecture of the CO₂ Laser Projection System

A comprehensive description of the CO₂P architecture can be found in [T0900217](#). Figure 1 provides key details of the system, which are explained in sections below.

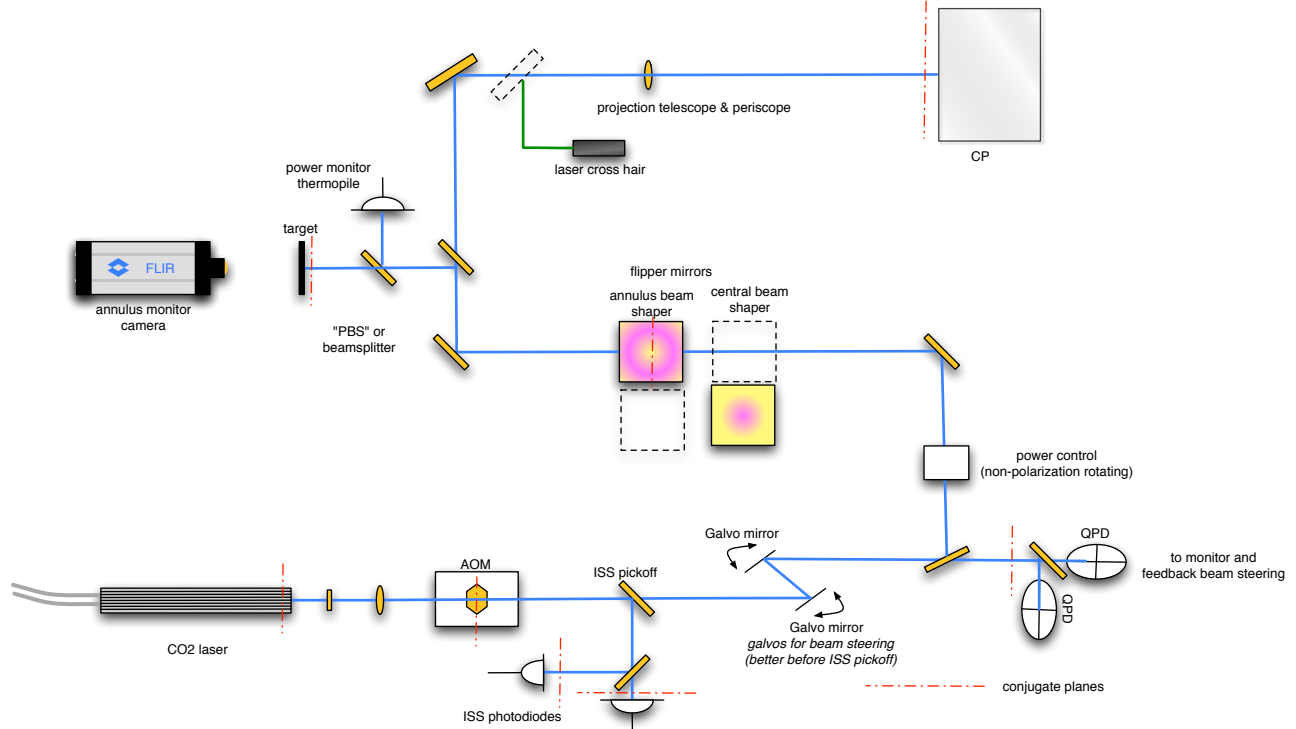


Figure 8: Schematic of main features of CO2P system (AdvLIGO TCS tables.graffle)

4.1 Power stabilized 50W CO₂ laser

The laser chosen to actuate on the compensation plate is a power stabilized CO₂ laser by Access. Power is stabilized at the output of the laser using a pickoff beam on a thermopile. The cavity length is controlled using a piezo mounted mirror, and the cavity length is effectively offset locked. Stability has been measured at $\pm 0.5\%$ over 12 days with no mode hops seen.

The laser cooling water will be actuated on to give low frequency stability using a similar system to that used in eLIGO. By measuring the voltage applied to the piezo the water temperature will be used to keep the piezo in the middle of its range. This will be done with a loop in the real-time system.

4.2 Intensity stabilization

The laser intensity will be further stabilized using an AOM and in-loop and out-of-loop HgCdTe photodiodes. These photodiodes will be the same VIGO Systems type used in eLIGO. A servo based on the same LT1128 opamp and Interfet IF3602 input stage used in eLIGO is planned. A detailed analysis of this servo can be found in [T070224](#).

4.3 Beam pointing control

Consisting of two pico-motor controlled mirrors, followed by near and far-field quadrant photodiodes. The pico-motors will operate at frequencies below 1Hz and the pointing can be corrected using the realtime system. In practice there are likely to be glitches in the picomotor

motion that will require this alignment to be done out of science mode. For this reason we do not intend to servo this alignment while in science mode.

4.4 Power control

Relative heating power for center and edge heading will be controlled using a motorized (Newport URS-50) half-wave plate and polarizer. The total heating power is controlled using a separate half-wave plate and polarizer. Since a small amount of power will be transmitted through the polarizer when it is set to zero power, there will also be flipper mirrors to direct the residual beam onto a beam dump to give a true zero intensity.

4.5 Heat management, temperature control

Cooling of the laser projector system will be handled by a separate chiller for each laser bench. The specification derived for this chiller is given in [E1101107](#). A tool to help calculate pipe diameters and design manifolds has been developed but not yet implemented. The chiller will be used to cool the laser, the laser RF driver, the AOM, the AOM driver and two beam dumps.

The temperature of the cooling water will be actuated on to keep the laser piezo in the center of its range and reduce the likelihood that the laser will mode hop.

Since the length of tubing used in the cooling system affects the unity gain of the servo, it is planned that a test be done at Caltech using similar pipe length to those planned for the sites in order to verify that the servo has sufficient gain.

4.6 Beam shaping

There is a single beam shaping path that contains two masks in individual flipper mirror mounts. The masks can be individually inserted into the beam to shape the resulting output. The initial masks will be a central heating mask and a simple annular heating mask.

4.6.1 Optimum beam profile using a mask

When a binary mask is used to correct for thermal lensing, that mask will be constructed by laser drilling a sheet of AISI 316 Stainless Steel, see D1400006 Mask for aLIGO TCS CO2P Central Heating for example.

The optimum mask design to correct for a thermal lens is found using code that iterates through mask designs in COMSOL to converge to a model that provides the appropriate level of correction. The Beam Shape Servo (BeSS), T1200103³, that accomplishes this is illustrated in Figure 9. The code to run this mask design program resides on the TCS SVN:

```
svn.ligo.caltech.edu/TCS_Components/aLIGO/modeling/models/BeSS
```

COMSOL modeling with this system finds that:

- at full IFO power with 0.5ppm absorption in the ITM HR surface,
- optimum RH correction for surface effects,
- annular correction with the CO2 laser beam and,

³ “TCS beam shaping: optimum and achievable beam profiles for correcting thermo-refractive lensing (not thermo-elastic surface deformation)”

- annular mask designed with BeSS,

the residual thermal lens is around 2nm RMS double passed vs a maximum allowed residual of 3.8nm RMS (G1201041). Therefore, the BeSS mask can correct for nominal distortion at full IFO power.

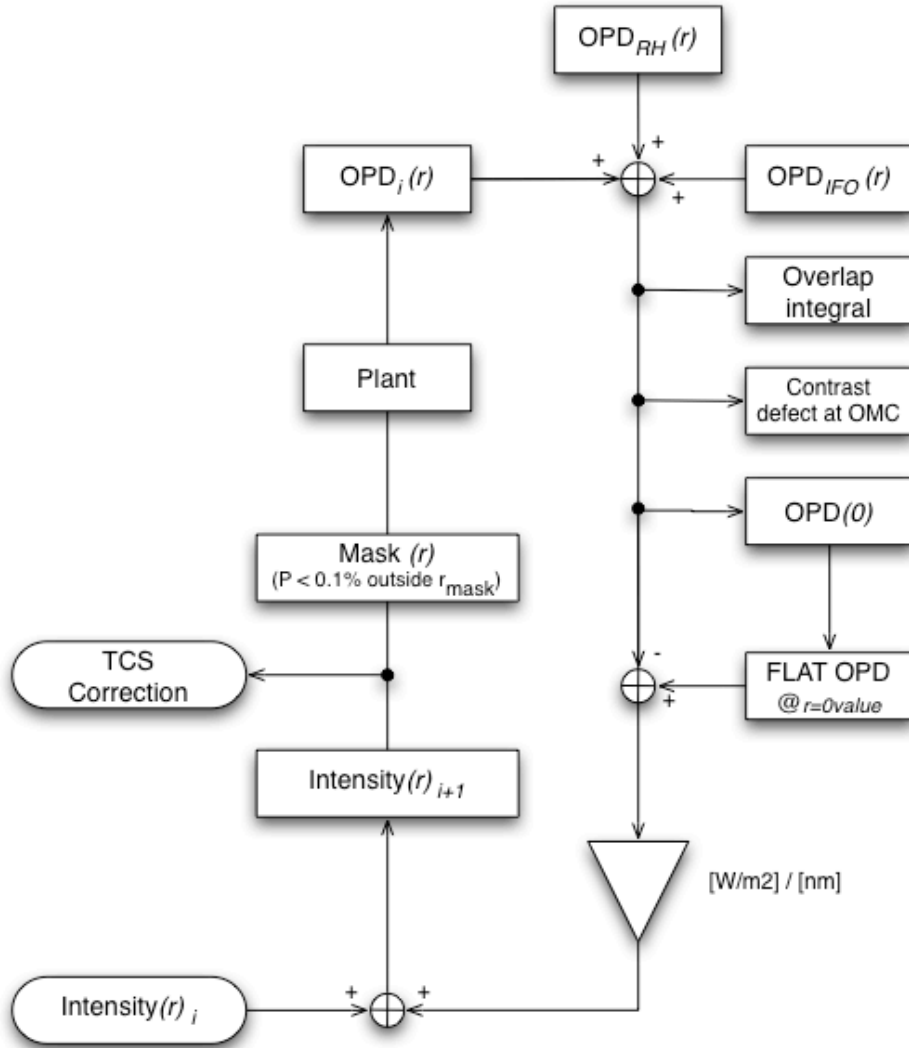


Figure 9: Beam Shape Servo for designing masks. LIGO-T1200103-v2

The calculated optimum mask + Gaussian beam to correct for maximum thermal lensing from 0.5ppm uniform absorption in the ITM HR surface at full power and RH actuation is shown in Figure 10. The residual OPD after this heat pattern has been applied is ~ 2.1 nm RMS which is lower than the required 3.8nm RMS distortion and is illustrated in Figure 11.

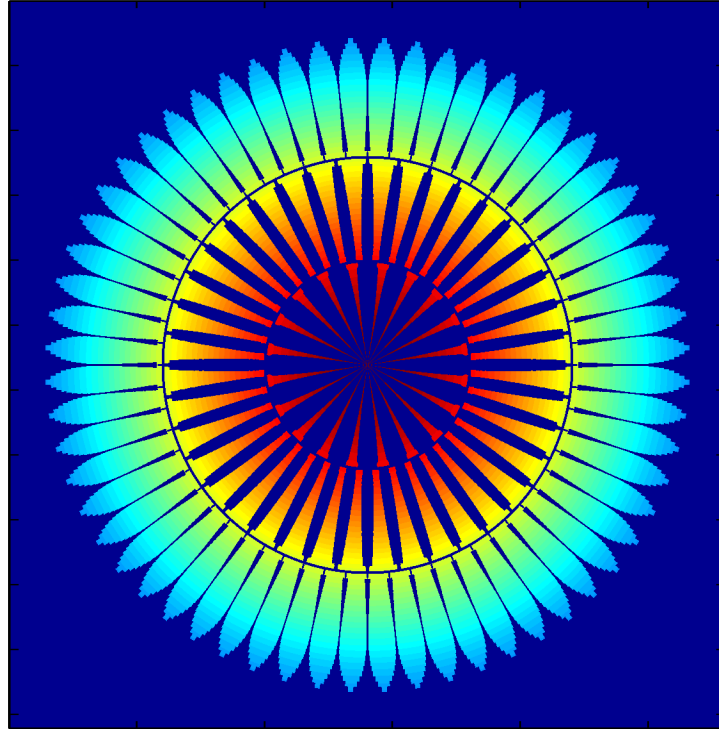


Figure 10: Illuminated optimum mask ($P= 4.7\text{W}$) to compensate for residual optical path distortion after 0.4W of self induced thermal lensing and RH applied to correct thermo-elastic effects.

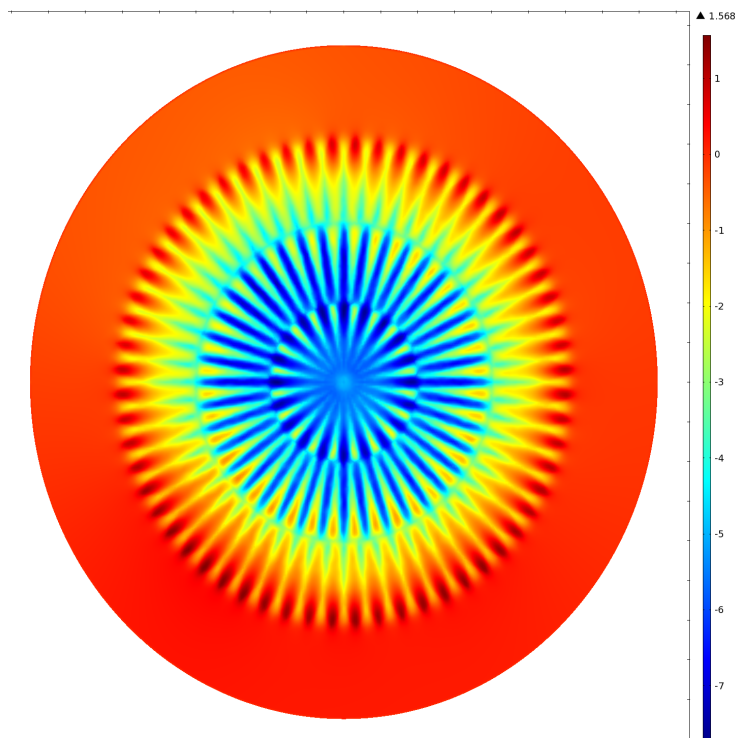


Figure 11: Residual OPD after self-absorption, RH and CO2 laser applied. RMS = 2.1nm vs maximum of 3.8nm .

4.7 Beam imaging

The annular mask is placed at a conjugate plane of the ITM with a magnification factor of approximately 23x. The central heating mask is placed as close to this plane as practical (about 1.5” away).

4.8 Beam quality monitoring

A pick-off after the masks will be imaged using a camera/beam imager. The image from the beam imager will give continuous monitoring of the projected beam. In eLIGO this was not possible and the annular beam shape could only be checked periodically. Drift in the system was found to cause uneven heat distributions. For aLIGO we will continuously monitor the projected beam shape and the applied phase front changes using the HWS to give more complete information about the system. The data from this system can also be used to track long term drifts.

4.9 Imaging optics and periscope

A final telescope is used to image the beam onto the compensator plate. The beam then passes through a periscope containing pico-motor controlled mirrors to allow for remote beam steering onto the CP.

4.10 Interlocks and control loops

The following control loops will be used

- Laser internal control loop – runs through a LIGO real-time front end model.
- Water temperature – uses error signal from laser internal control loop. Low frequency loop that can be run using frontend system. Also LIGO real-time front end model.
- Intensity stabilization servo – An analog control servo. [Alastair looking into this](#)

The laser projector will have its own dedicated interlock board to protect the laser against low water flow rates, and to shut off the laser if its internal temperature rises above a setpoint. This interlock will integrate with the site interlock to shut down the TCS laser in the event that a site kill switch is activated. In addition there will be a clearly labeled TCS laser only kill switch located on the outside of each laser enclose.

4.11 Visible alignment lasers

There is a visible alignment lasers in the CO2 projector optical layout.

The laser is a cross-hairs coupled into the final stage of the projection system using a mirror that is temporarily inserted to align the visible laser to a pair of irises that are aligned to the optical axis. The purpose of this laser is to provide an initial alignment of the optical axis to the compensation plate.

5 Optical Design

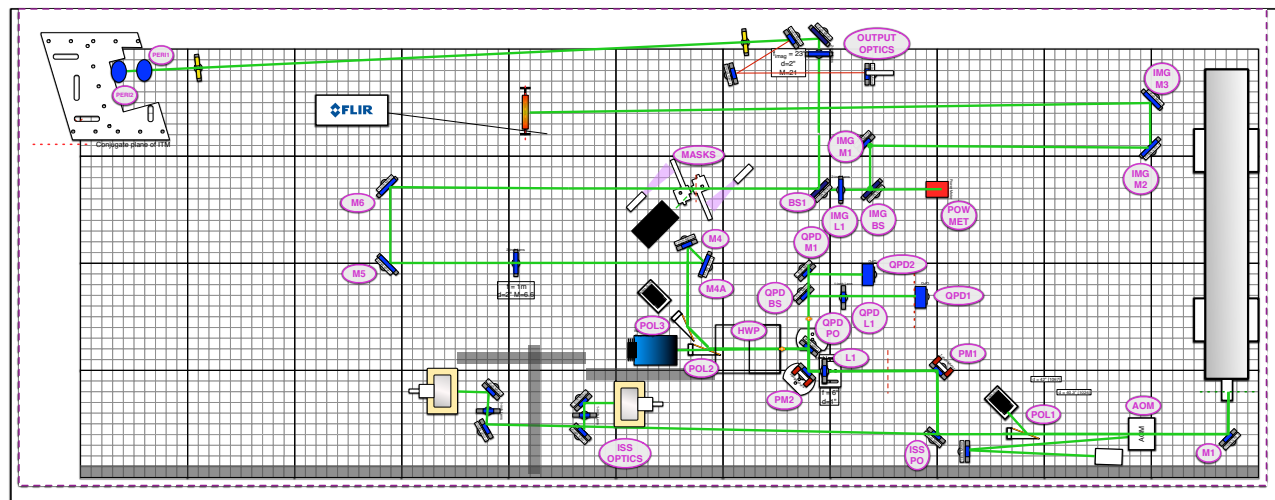
The optical layout consists of in-vacuum mirrors, an in-air periscope containing pico-motor controlled mirrors, and an enclosed optical table. The top-level systems diagram for all aLIGO TCS elements is given by D1001227. Version 3 (-v3) of this document isolates only the CO2P components. Sheet 1 of this drawing illustrates H1 and L1 configurations.

The optical layout is drawn in T1200007.

The ABCD calculation reflecting this layout is described in T1500034.

5.1 Table layout, in air

Figure 5 shows the planned table layout for the CO2P.



T1200007-v13 - TCS CO2 laser table

Figure 12: Optical layout T1200007-v13 for CO2P on a 1" grid.

5.2 In vacuum steering

5.2.1 H1 and L1

As stated in Section 2 (above), designs for two unique steering mirror assemblies ([D1101013-v1](#) and [D1101851-v1](#)) required for guiding the CO2 laser onto compensation plates within BSC's 1, 2 and 3, serving H1 and L1, have not yet been reviewed. However, the hard-gold-coated copper mirror for the SM1 assembly ([D1101013-v1](#)) has been received from the manufacturer in December 2011.

Two packages documenting the detailed analysis of each of these assemblies are given by [G1101230-v3](#) (for SM1 in BSC's 1 and 3) and [G1200016-v1](#) (for SM2 in BSC 2). Note that the hard-gold-coated copper mirror ([D1101014-v4](#)) for the SM1 assembly ([D1101013-v1](#)) has been received from the manufacturer in December 2011.

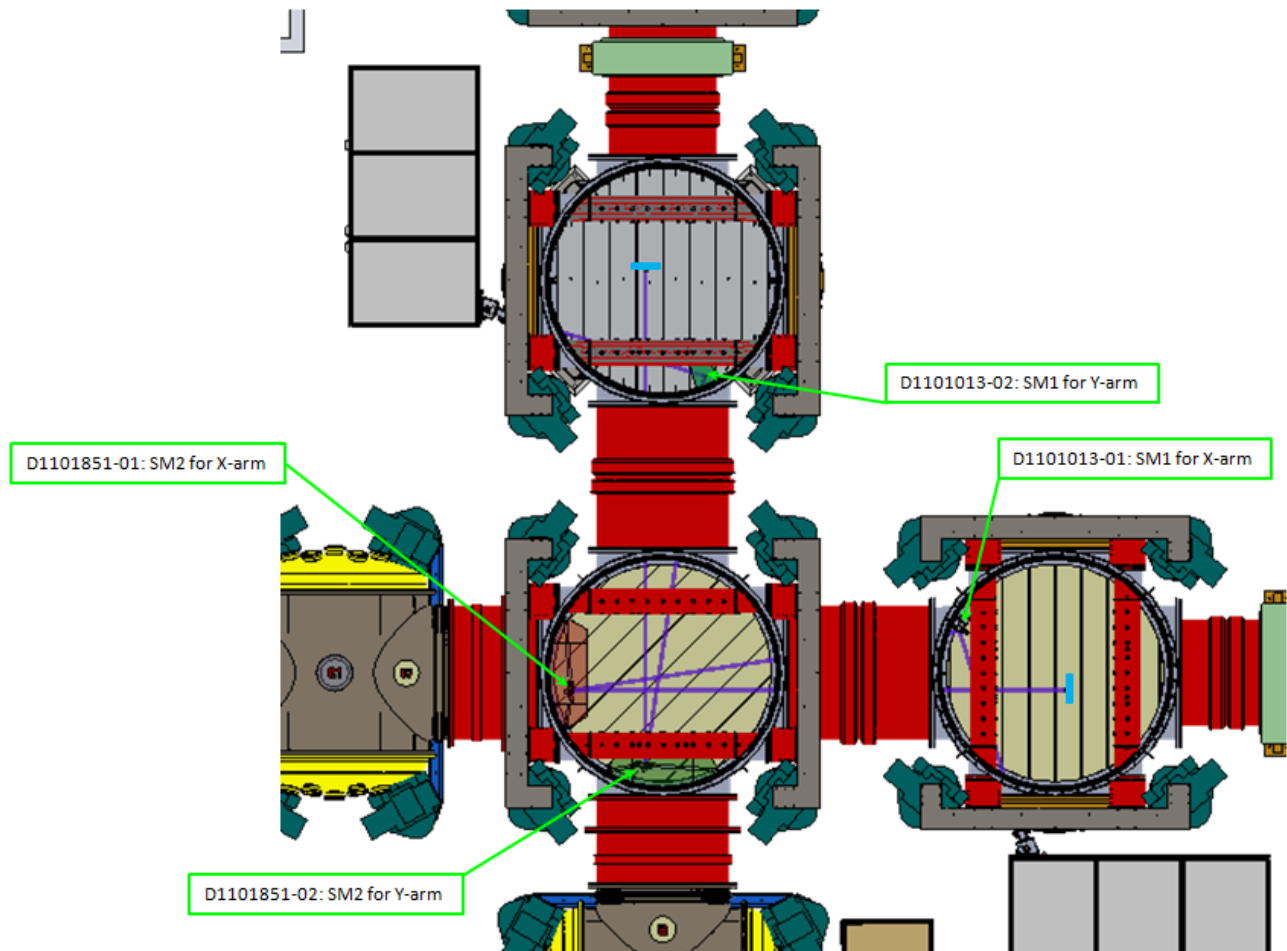


Figure 13: View of injection path for H1 or L1 CO2P beam.

Precise angular projections of beams, in vacuum, are illustrated on Sheet 1 of [D1001227-v3](#).

5.3 Custom Optics and opto-mechanics

We describe here only the custom optics and opto-mechanics. Section 13.2 contains a more complete list of optics to be purchased.

5.3.1 Periscope and mirrors

A custom designed periscope is used to take the beam from the table up to the ZnSe viewport where it is injected into the vacuum system. The periscope has two 4" mirrors, mounted in SL series Newport mirror mounts that have been customized to accommodate pico-motor control. This gives remote beam steering for the final alignment of the beam onto the CP. Implementation of this periscope is most difficult for H2, due to location of the table. This is illustrated in the following figure.

The mirrors used are silicon substrate with a dielectric coating of ZnSe/ThF4. The reflectivity of this coating has been measured at Caltech to be 99% for an S-polarized 10.6 μ m beam.

5.3.2 Optical table

The optics used on the optical table are all standard parts that will be purchased. Some partially transmitting mirrors are required at points for photodiodes and beam monitoring, and for larger numbers of optics it will be more cost effective to have these coated specially.

There are a number of custom opto-mechanical parts required. These include:

- Laser mount (for rigidity of base): D1201510
- Periscope from laser to bench (rotates output polarization from P to S): D1200953
- Mounts for the HgCdTe photodiodes (for high frequency stability): D1201065
- Rotation stage (URS-50) mount for the half-wave plate: D1000791

Documentation of analysis for the design for the custom mount of the rotation stage can be found in [G1100567-v2](#), which is also referenced by the Input Optics (IO) layout. The associated modal test data can be found in [T1100348-v1](#).

6 Enclosures / VEA Layout

6.1 Floor plan

The corner station floor plan [[D1001227-v3](#): aLIGO TCS Envelopes, Corner Station, LLO, LHO] shows the size and locations of the tables. Table locations in this document can be related to rack and cable tray layouts in the Systems (SYS) layout given by documents related to [D1003142](#).

6.2 Table enclosures

Enclosures for tables adjacent to BSC's 1 and 3 have been designed so that the periscope is completely enclosed, and the viewport enclosure is integral to the design of one wall. Detailed mechanical drawings are being prepared; the top-level bill of materials is given in the Appendix.

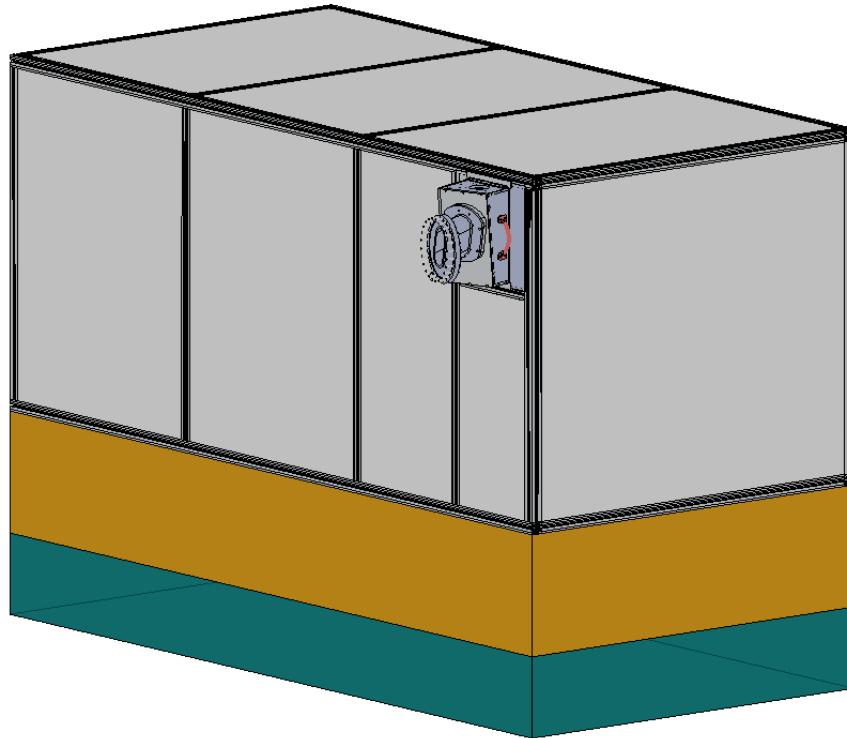


Figure 14: Isometric view of the top level Table assembly for H1 and L1; the viewport enclosure ([D1101627-v1](#)) is integral to one panel of the table enclosure.

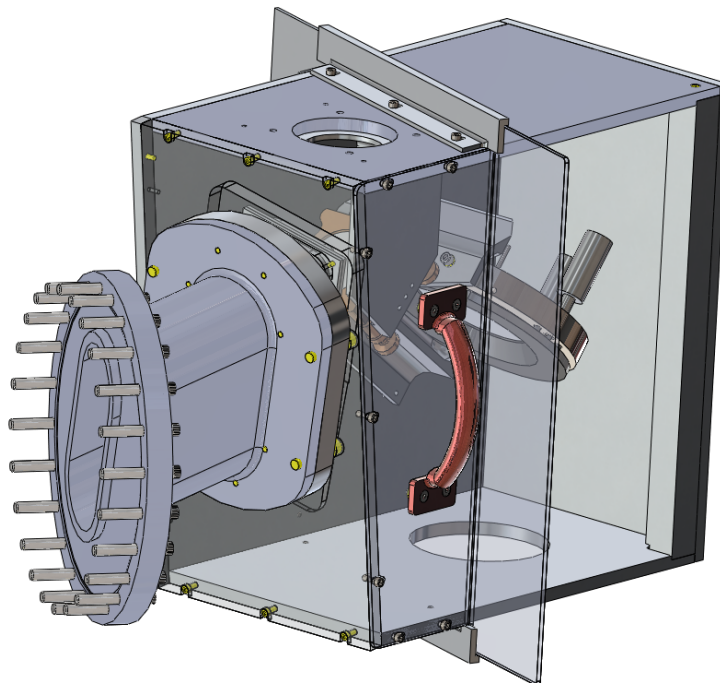


Figure 15: Isometric view of the H1-L1 viewport enclosure [D1101627-v1](#), Type -01.

6.3 Viewport enclosures

For H1 and L1, assembly [D1101627-v1](#) has types -01 and -02 for the X- and Y-arm injections into BSC's 3 and 1, respectively. Detailed mechanical drawings are being prepared; the top-level bill of materials is given in the Appendix.

One element of this enclosure is the Primary Flange Viewport Assembly, [D1101630-v1](#), which incorporates one part ([D1003209-v2](#), a Clamping Flange)

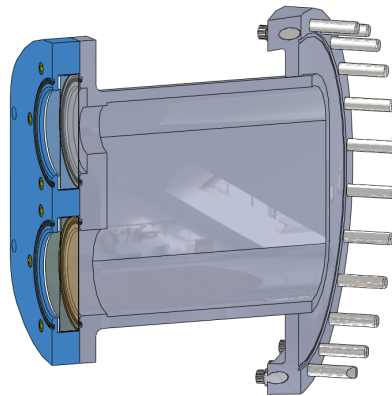


Figure 16: Common use of a *Clamping Flange* ([D1003209-v2](#)) for Primary Viewport Assembly in H1-L1

There are two primary viewports, at the vacuum interface, for alignments using a visible camera as well as for injection of the CO₂ laser beam. The designs for these ZnSe viewports are the same for both the H1-L1 assemblies. As part of the hazard analysis for TCS, overall, an analysis of ZnSe viewport operating stresses, under vacuum, has been performed. An unapproved report associated with this analysis is given by [E1100379-v3](#).

There are also two secondary viewports, half the thickness of the primary viewports, which are common to the H1-L1. IR sensors are incorporated into the designs. The sensors monitor stray IR light and are a key part of the equipment safety interlock circuitry.

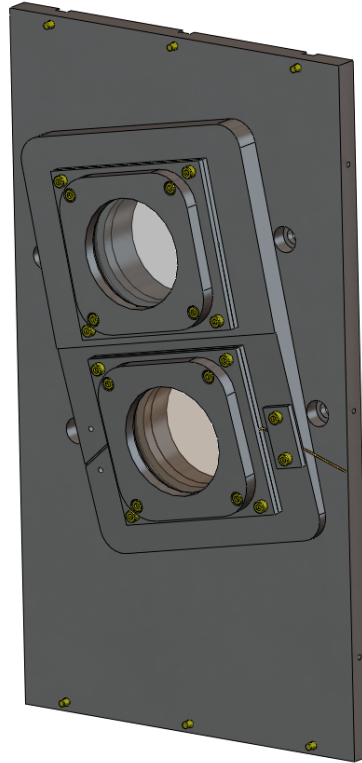


Figure 17: Common use of secondary viewports with temperature sensing for the H1-L1, in sub-assembly [D1101631-v1](#).

7 Electronics

Corner station block diagrams for each of the three major elements of TCS (CO₂ laser projection, Ring Heaters and Hartmann Sensors) are given on separate sheets in the document [E1100892](#).

7.1 Overview - Block Diagram

E1100892-v25 (page 1 of 3)
 Corner Station (H1, L1) CO2 Laser projector (X & Y).
 Cables for Laser are listed in BOM E1400342

8-Aug-2014

This page shows the electronics layout for one TCS CO2 Laser projector table. There are 2 such tables at each site, one for X arms and one for Y arms. These are identical, each being 6' wide and 10' high and 10' deep. The 6' dimension is the size of the main control rack and 10' is the size of the laser table.
 The X and Y arms share one DAC (distributed in shared). The X and Y arms have separate ADC (shown here in block for X arm and not for Y arm).

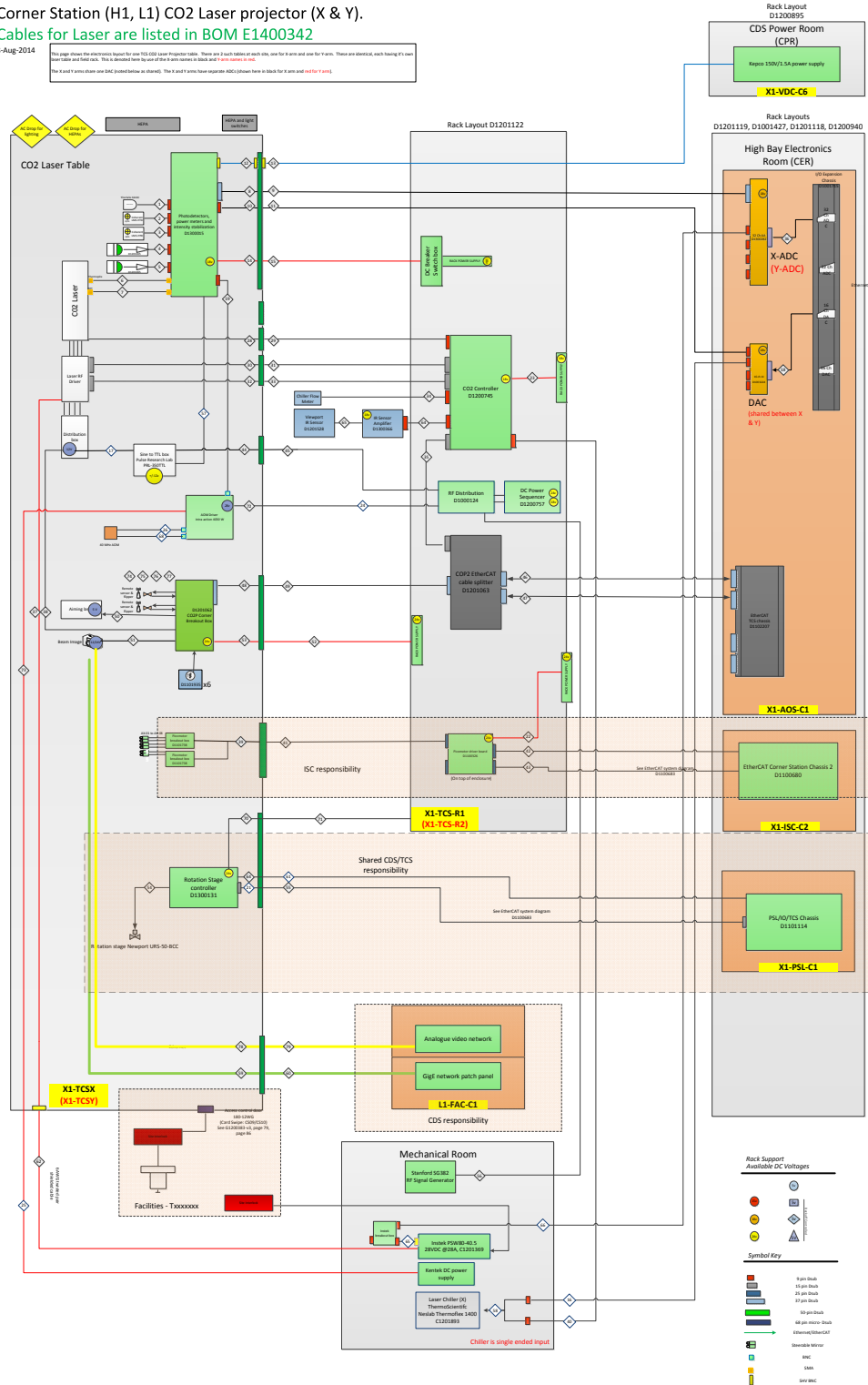


Figure 18: Block diagram of electronics for TCS CO2P system, Sheet 1 of E1100892-v26

7.2 EtherCAT control

The Beckhoff EtherCAT system described in [G1100098](#) will be used for slow control and measurement. Currently we plan to use this for flipper mirrors and temperature sensors.

7.3 Custom electronics

7.3.1 aLIGO TCS ISS SERVO DRIVER [ACTS ON AOM]

The aLIGO TCS ISS servo is show in D1300015. This interfaces with the ISS photodiodes, D1201065.

7.3.2 aLIGO TCS CO2P QPD [D1300650]

The buffer circuitry for the QPDs is on D1300650, aLIGO TCS ISS Interface Board.

7.3.3 aLIGO TCS CO2P CHILLER FLOWMETER SENSING & INTERLOCK CIRCUITRY [D1200745]

The local interlock for the TCS CO₂ laser has been designed, D1200745. It is used to protect the laser against low water flow, or if the internal temperature of the laser increases. The action of the interlock is to trip a relay that disables the enable input of the RF driver of the laser. This interlock is still to be integrated into the LIGO site interlock, however the use of relays in this circuit allows another interlock signal to be routed through the device. The optical table also has its own limited access system that will be integrated with this interlock. IR sensors on the ZnSe viewports are be integrated into this .

The interlock has analogue outputs for flow rate and temperature. It also has digital outputs to give information on latched status.

7.3.3.1 aLIGO TCS CO2P LASER TEMP. SENSING CIRCUITRY

The temperature sensing of the laser is done using an RTD device built into the laser. The readout for this is done in the interlock circuit since this temperature is used to protect the laser. An analogue output from the interlock allows the temperature to be recorded using the EtherCAT system.

7.3.3.2 aLIGO TCS CO2P LASER ENABLE ON/OFF

The laser is turned on and off using an enable input that must be set high to give continuous wave operation. This will be done using a small control box mounted next to the laser on the bench. The laser power can be reduced for alignment procedures by modulating this input with a square wave. The Synrad power controllers used for eLIGO can be used to control the Access laser for this purpose. The laser controller can be switched into use using the laser enable on/off box.

7.3.4 aLIGO TCS CO2P LASER POWER SUPPLY

The power supply for the Access laser requires 28V at 28A. This can be split by driving the two sides of the RF driver with separate supplies at 28V and 14A. The power supply is an Instek PSW80-40.5.

7.3.5 aLIGO TCS CO2P AOM DRIVER

The AOM driver will remain the same water cooled version of the IntraAction GE-4030 used for eLIGO. It will be powered using an external DC supply at 28V. It is proposed to use the same 40.68MHz clock to drive this as for the Access CO₂ laser. This clock will be synchronized to the site clock.

7.3.6 aLIGO TCS CO2P ROTATION STAGE DRIVER

The rotation stage, URS-50-BCC, is controlled through the Beckhoff system via D1300131.

7.3.7 PICO MOTOR DRIVER BOARD

The pico motor driver board will be Daniel Sigg's design [D1100326](#). It will connect to the driver breakout box [D1101738](#).

7.3.8 aLIGO TCS CO2P FLIPPER MIRROR DRIVER

The flipper mirrors will be driven using a New Focus off the shelf driver. This takes a TTL input to operate the flipper mirror. A separate sensor will be used to monitor the status of the flipper mirror.

7.3.9 aLIGO TCS CO2P THERMAL IMAGING CAMERA [FLIR A325c]

The thermal imaging camera will use GigE for both control and to transmit images to a TCS computer. These images will be stored for off-line analysis of beam shape.

7.3.10 aLIGO TCS CO2P IN-AIR TABLE OPTICAL POWER METER

The power from both paths of the CO₂P will be monitored using Thorlabs S302C power meter heads. These can take 2W and give a 1uW resolution. The power meter heads will be connected to Thorlabs PM100D power meters which gives an analogue output as well as a local user display. The analogue output will be connected to EtherCAT to record data.

7.3.11 aLIGO TCS CO2P VIEWPORT IR SENSING CIRCUITRY [D1201528]

The ZnSe viewports will use an IR sensor to look for stray IR reflections (caused by sudden large scattering sources on the viewports, for example, insects settling on the ZnSe). This unit has a setpoint above which the laser interlock will be triggered.

7.3.12 aLIGO TCS CO2P IN-AIR TABLE 3-AXIS ACCEL SENSING CIRCUITRY

A 3-axis accelerometer will be used to measure the acceleration created by the shaker. A sensing circuit for this accelerometer is to either be purchased off the shelf or designed.

PEM is responsible for providing this.

8 Software

Software for the CO2P can be split into subcomponents (yet to be developed). There can be a realtime code model for control. In addition there will be a PC collecting data from the GigE camera link used for beam profiling. There will also be an EtherCAT system, though this will be integrated with the system used for the Hartmann wavefront sensors. There will also be some further scripts required. We discuss requirements for each of these below.

8.1 Realtime code

The realtime model for the CO2P (on the CDS SVN under `userapps/release/tcs/common/models`) will cover the following items:

- Collection of fast channel data from intensity stabilization photodiodes
- Control of the ISS
- Slow data related to the laser (thermopile output, piezo, locking status)
- QPD data
- Picomotor control
- Power control using the half-wave plates
- Power monitoring using power meters
- Servo for controlling the chillers

We intend to combine these functions in one model to reduce interdependencies in the TCS system

8.2 GigE beam imaging cameras

The beam profiler will use GigE for both data transfer and control of the camera. It is likely that the data from these cameras, which will be in image format, will not be recorded in the frames. Instead it will be recorded to a dedicated PC to be stored locally. This data is used for long term beam monitoring, not for any form of real time control.

8.3 Other scripts

RS232 monitoring of the chillers is an optional upgrade but not part of the baseline design.

8.4 Computing hardware/software requirements

In total the CO2P should require two computers per interferometer. One multi-core machine is needed to run the realtime system and scripts; a second machine is needed to collect image data from GigE cameras. This second machine may be shared with the Hartmann Sensor computer.

8.5 DAQ/Storage requirements

The following is a brief summary of the data acquisition storage requirements.

8.5.1 Fast channels

The fast channels to be recorded in the DAQ are listed in taken from the `TCS_MASTER.mdl` Simulink file.

#DAQ Channels	
ISS_IN_AC_OUT*	2048
ISS_OUT_AC_OUT*	2048
ISS_CTRL1_OUT	1024
ISS_CTRL2_OUT	1024
PWR_SUPPLY_V_OUT	1024
PWR_SUPPLY_I_OUT	1024
AOM_OUT_GAIN_IN2	1024
PZT_OUT_GAIN_IN2	1024

Figure 19: The fast CO2P DAQ channels to be stored

Two CO2 laser projectors per interferometer yield a total of $4 \times 2\text{KHz} + 12 \times 1\text{KHz}$ channels per IFO. The data rate is, thus, $10 \times 2\text{KHz} \times 2 \text{ Bytes} = 40 \text{ KB/s}$.

8.5.2 Slow channels ($\leq 16\text{Hz}$)

The following is a list of the slow channels required for storage per CO2P.

- Shutters: (2× binary actuators, 2× binary read-backs)
- Power meters: (2× analogue readbacks)
- AOM: (1× DC analogue level set)
- ISS: (2× DC analogue level readback, 1× on/off switch, 1× analogue gain set)
- QPD: (8× analogue level readback)
- Polarizers: (2× angle set value, 2× actual value)
- Pico-motors: (6× set-point change request)
- Aiming lasers: (2× binary on/off actuators)
- Temperature sensors: (4× analogue readbacks)
- Flow meter: (1× analogue readback)

This yields a total of 34 slow channels to store at 16 Hz and 16 bits = 1KB/s. This does not include additional slow channels to be stored for other values such as set-points in PID loops, etc. To allow for plenty of head-room in slow channel storage multiply this by a factor of 3 = 3KB/s per CO2P.

This results in 6KB/s per IFO in slow channel storage.

8.5.3 Images

The method for storing images from the GigE beam imaging cameras has not been determined. The images themselves will be no greater than 640×480 pixels at 16-bit resolution = 600KB. They will not need to be stored very often (the shortest thermal time constant of the test mass is approximately 40s). A rate of 2 per minute will suffice. This yields an average rate of 20KB/s per camera, or 40KB/s per IFO.

9 Interfaces

9.1 Corner Station Mechanical Interfaces

Provided by TCS:

- [\[D1001227-v3: aLIGO TCS Envelopes, Corner Station, LLO, LHO\]](#)

It is known that the optical table supports for each of the TCS tables must allow for easy transportation of each of the tables, away from the vicinity of each of the BSC doors. The supports may be of a custom design, yet to be detailed. Tables are the standard RS4000 series, 18" thick, from Newport. Advertised performance for this type of table is shown below.

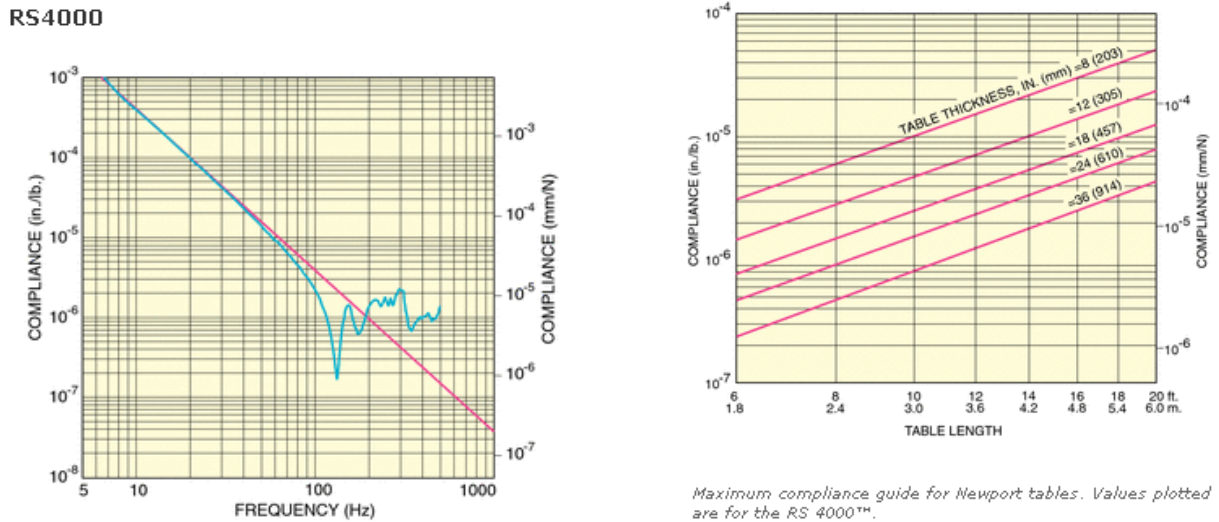


Figure 20: Advertised performance of RS4000 series tables from Newport

9.2 Corner Station Cabling/Plumbing Interfaces

Provided by Systems (SYS):

- [\[D1002704: Rack and Cable Tray Layout, LVEA, H1& H2\]](#)
- [\[D1003141: Rack and Cable Tray Layout, LVEA, L1\]](#)
- [\[E1000760: Cable Lengths, Corner Station, H1& H2\]](#)

10 Verification Testing and Modeling

10.1 Verification Plan

In order to verify expected performance of the laser projection system, a broad collaboration of modeling efforts is necessary. In recognition of this, ad-hoc collaborative modeling discussions have been held in the months leading up to this Final Design Review. In these discussions, it has

been acknowledged, by attendants, that the top level modeling tools (for the interferometer) are not yet robust enough for complete correlation of building-block style modeling efforts, using a bottoms-up approach to the verification task. To track the roots of this discussion, visit the [wiki page](#) for minutes from the initial meeting.

Acceptance testing of TCS components is described in T1300495, [Acceptance Testing of TCS Components](#).

10.2 Modeling

10.2.1 Requirement on annulus uniformity

Modeling of absorption of an annular beam on the CP has been used to show that phase front can be corrected sufficiently to meet the requirements set in Section 3. One extension of this model that is yet to be investigated is to look at the effect of a non-uniform annulus. The effect of offsetting the annulus has previously been looked at, as have the effects of altering annulus diameter and width. Here we are interested in understanding the effect of having a non-ideal alignment through the mask, which produces an annular beam with a higher power density on one side.

The aim of this modeling is to produce a requirement on beam uniformity that can be used to inform our interpretation of annular beam images that will be coming from the CO2P. This could be used either offline to interpret long term trends, or it could be done in real time to give information on whether the alignment of the system has drifted out with a required range.

10.3 Testing

What follows are descriptions of component tests that can produce data that will be used to verify CO2P once the full interferometer is operational.

10.3.1 Pointing from AOM and Laser

We will measure pointing effects from the laser and AOM using QPDs. Beam steering after the AOM will be used to correct for drifts in pointing.

Alternative AOMs could be tested if beam pointing is an issue from the IntraAction unit.

10.3.2 Investigation of laser stability

As part of the ISS system we will be acting on the laser chiller as well as the AOM. The chiller type and pipe lengths should be setup to closely mimic the situation at the sites. The chiller feedback loop must be setup and analyzed. Due to the latency of such long pipe lengths the unity gain frequency will be low, and the gain limited. It is also possible to improve the temperature stability of the laser using a thermally stabilized enclosure, and this will be considered if sufficient gain cannot be achieved using the chiller alone.

It is possible that the internal intensity stabilization for the laser may also be improved. We will investigate the possibility of implementing our own laser stabilization servo, possibly using photodiodes instead of the internal thermopile to increase bandwidth. We may investigate using separate chillers for the laser and the rest of the heat load.

10.3.3 Quantum efficiency of HgCdTe photodiodes in ISS

We will investigate the effects of spatial variation of the quantum efficiency of the HgCdTe photodiodes on power stability. This QE variation can couple jitter noise to intensity noise.

Approximate measurements of the QE of the HgCdTe photodiodes give 20% variation over mm distances ([T0900428](#)), though these values are approximate. The manufacturer does not provide data on QE.

The primary sources of jitter noise in initial LIGO were the laser and AOM. To reach the required ISS level we must have less than 1×10^{-9} m/ $\sqrt{\text{Hz}}$ of jitter on the photodiode.

10.4 Validity in context of all TCS

In order to validate the architecture of the laser projection system, it is necessary to consider, serially, the expected magnitude of all noise sources within the laser projection system once all components have been completely designed. Outstanding designs are listed in Section 2, above.

Fundamentally, noise associated with operations of the CO₂ laser, itself, are to be validated in context of the specification ([E1000065-v6](#)). A detailed report of as-delivered performance of the first article *Lasy-50* device obtained from Access Laser Co. is presented in [T1100508-v2](#). The following figures present some data gathered from operations of this device at Caltech.

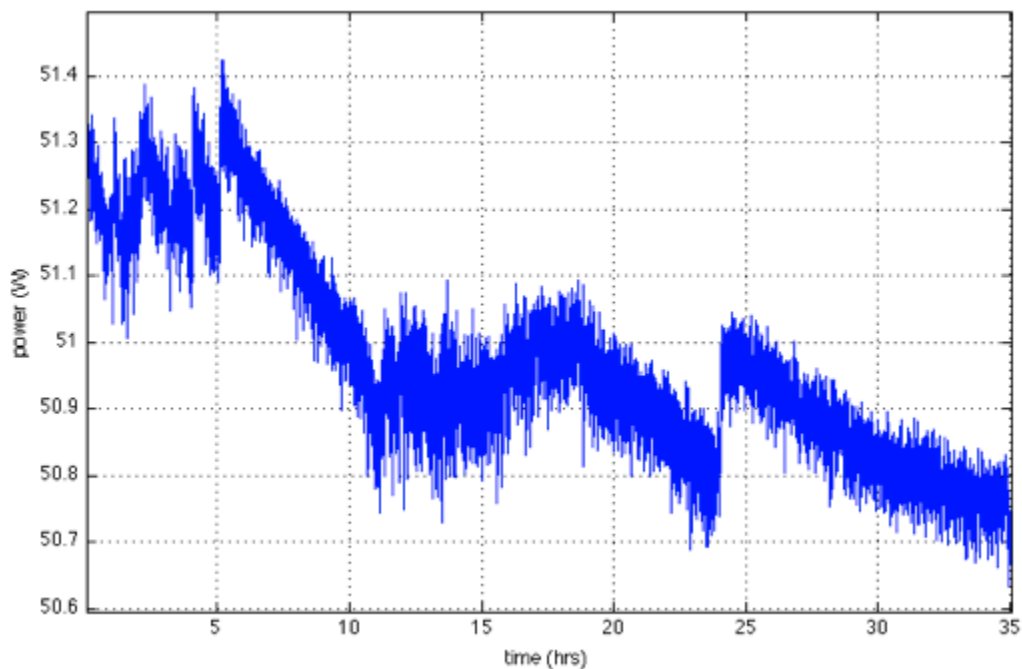


Figure 21: Short term power stability of Access *Lasy-50*

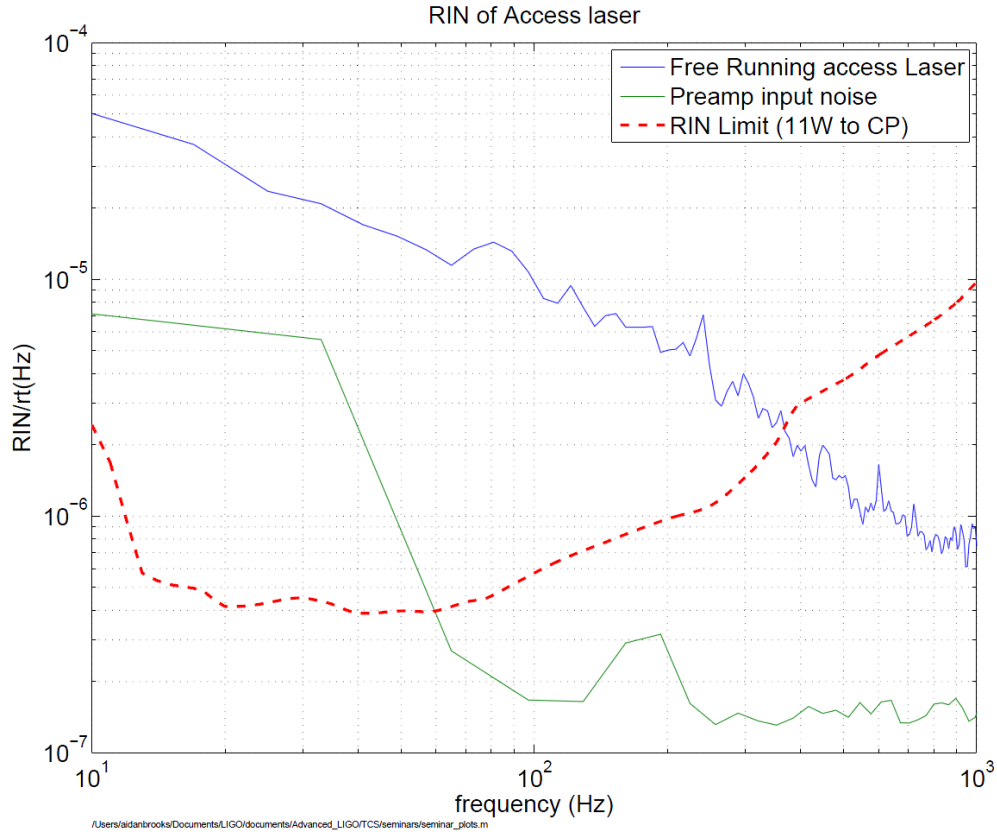


Figure 22: RIN of Access *Lasy-50*

Long term power stability of the laser is being monitored continuously in the Caltech laboratory. 12 days of continuous data are plotted, for example, in Figure 23 below. The laser exhibits a daily variation of approximately $\pm 0.5\%$. No glitches were observed over the 12-day period.

This easily satisfies the glitch requirement in Section 3.2.2.3.

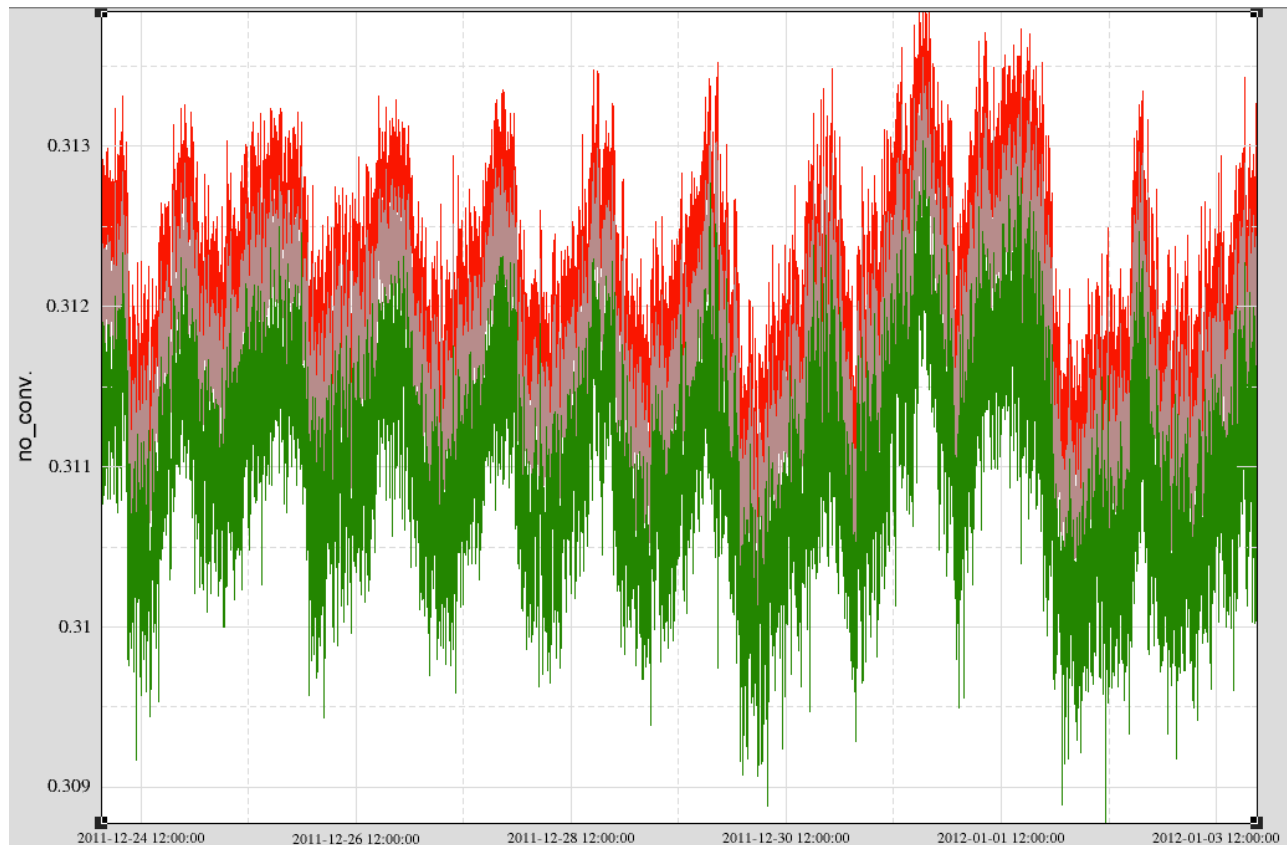


Figure 23: Power of Access laser over 12days, measured with 0.3W pickoff beam. Red trace shows maximum and green curve shows minimum of hourly trend data.

11 Procedures

11.1 Cleaning

The custom $\varnothing 4$ " periscope mirrors described in section 5.3.1 should be cleaned in accordance with the procedure given by [T1100596](#).

The custom $\varnothing 12$ " mirror, installed in vacuum for H2 laser projections onto the compensation plates in BSC's 7 & 8, are to be cleaned in accordance with the approved procedure given by [T1100179-v13](#).

11.2 Alignments

The alignment procedure for the in-vacuum steering mirrors is described in [E1400137, Punch List for Re-Aligning aLIGO TCS CO2P-X UHV Steering Mirror #1 \(BSC3\)](#).

11.3 Operations

The CO2P Operations Manual is on the DCC under [E1300233](#).

12 Safety

The hazards associated with the aLIGO TCS CO2P are discussed in detail in [E1000205 - aLIGO TCS Hazard Analysis](#).

For all activities conducted in the laboratory at Caltech, the approved standard operating procedure ([M1000024-V12](#)) must be followed.

As the design of the CO2P for aLIGO is conceptually very similar to the eLIGO design (the peak laser power and thermal power in the system is roughly 2× that of eLIGO), the identification of hazards and mitigation has not changed significantly from that system, the hazard analyses for which are linked below.

- [E080206 - LHO ELIGO TCS Hazard Analysis](#)
- [E080501 - ELIGO TCS Hazard Analysis, Volume 2](#)

The greatest hazards regarding this subsystem remain the same as eLIGO and are as follows:

- 1) Class IV radiation directed into an operators eyes [Personnel hazard],
- 2) Personnel burns (on hands) due to infrared radiation [Personnel hazard],
- 3) Power supply grounding faults [Equipment hazard];
- 4) Handling of heavier parts by hand and lifting them under the manifolds (i.e., power supplies, chillers) [Personnel hazard]
- 5) failure of the ZnSe vacuum viewport window under intense illumination if contaminated by a highly absorbing material. [Equipment hazard]
- 6) Overheating and damage of equipment that handles high power (electrical or thermal). [Equipment hazard]

More detail on these hazards is briefly summarized in the following two subsections. For full details, see [E1000205 - aLIGO TCS Hazard Analysis](#).

12.1 Equipment Hazards

The following hazards have been identified that may damage equipment:

- **Fire**
 - Fire hazard due to equipment/cable burn through.
- **Heat.**
 - Coolant failure: Should the liquid coolant supply to the TCS table fail, the laser and acousto-optical modulator (Figure 5, Right) could overheat. There is no personnel risk due to this eventuality. Both these devices contain internal fail-safe devices that sense temperature increases and shut themselves down when overheating occurs.
- **Laser**
 - The 50W laser has the potential to damage optics and equipment on the table, including the viewport to the vacuum, if it is improperly used or aligned or if the absorption on a particular optic becomes very high. To alleviate this:
 - gold-coated copper mirrors are used wherever possible for beam steering (the high thermal conductivity makes it next to impossible to damage these with 35W of laser power as repeated damage tests have shown).

- The optics will be enclosed in HEPA filtered enclosure to help prevent contamination
- Failure of ZnSe viewports: A viewport cover will prevent contamination of the primary viewport to the vacuum system. This viewport will be temperature interlocked to shutdown the laser in the event that it becomes contaminated and overheats.
- **Misc. hazards**
 - Equipment, especially the laser, can be damaged as it is being transported if it is mishandled.
 - Electronics failure, specifically failure of the laser power supply.

12.2 Personnel hazards

The primary hazard to humans is the Class 4W 50W CO2 laser. This poses both eye and skin hazards. Specifically, there are hazards associated with:

- TCS 30m Laser Alignment: there are unique personnel hazards associated with projecting the laser beam across the LVEA floor.
- Bodily laser burn to personnel: during regular operation and maintenance
- Laser burn to eye: during regular operation and maintenance
- Fire hazard due to equipment burn through
- Electronics failure: failure of the power supply chassis grounding
- Laser power control failure: during alignment

Standard Class 4 laser protocol will be employed when human interference with this laser is required. Due to the safe and continuous operation of the eLIGO lasers and the large similarities between the aLIGO CO2 projector and the eLIGO CO2 projector, the aLIGO standard operating procedure (SOP) will be as close as possible to the eLIGO SOP:

[“Standard Operating Procedure Aligning the Thermal Compensation Laser Operating in LVEA,” LIGO-M080080-00-W](#)

[“Standard Operating Procedure Thermal Compensation Laser Operating in LVEA,” LIGO-M080082-00-W](#)

13 Project Planning

13.1 Schedules

Activities associated with the production and installation phases for all elements of aLIGO TCS are linked to formal (INS) activity identifiers in [M1200009](#).

As stated in Section 2.3, above, laser projection system items on the critical path to meeting (INS) need-by dates are the two steering mirror assemblies for BSCs 1, 2 and 3 ([D1101013-v1](#) and [D1101851-v1](#)).

13.2 Costs

The most recent costing baseline is documented in [M1000349-v2](#). Since the time of this ACR ([#110012](#)), the CO2P bills of materials (BOMs) for all components have been matured and detailed, though not finalized. The Appendix includes detailed BOMs

- i. for items installed in air
- ii. for electronics
- iii. for items to be installed in the vacuum system (or at the vacuum interface)

From these, updating completion estimates can be an on-going activity. The current (unapproved) cost book is given by [M1000349-v5](#).

The CO2 power supply was evaluated using the bid-evaluation matrix in [C1201369](#).

13.3 Procurements

The "notes" column in each of the BOMs includes vendor information. In the case of CO2P, most items to be used for installations in air are readily available from commercial catalogs.

The CO2 laser procurement has been concluded; see procurement activity "[AO-214b TCS - CO2 Laser](#)" for details.

Many custom items, for installations in vacuum or at the vacuum interface, have been procured due to early need-by dates and long-lead times. Examples are:

- Assemblies [D1002431-v3](#) and [D1001742-v3](#)
- Handling fixture ([D1100263-v3](#)) for the Ø12" mirror in each of the above assemblies
- Assembly Type -01 of [D1003193-v3](#)
- ZnSe viewports, both primary and secondary ([D1100439](#) and [D1100485](#), respectively)

Custom optics which may have long-lead times but have not been procured include:

- Ø3" optical viewports (see section 6.3)
- Ø10" hard-gold coated copper mirrors for H1-L1 SM2 assemblies ([D1101851-v1](#))
- anamorphic prisms
- Ø4" periscope mirrors (see section 5.3.1)

Associated costs and vendors for each of these have, however, been identified.

Procurement plans associated with custom electronics are not yet mature, due to immature designs.

Beam quality monitoring can be performed by commercially available devices. Several particular vendors and product types have already been investigated, in terms of cost, lead time and technical capabilities. (See, for example, [C1107040-v3](#) and [C1107005-v2](#).) A specification for requirements of these devices in context of operation within the laser projection system, however, have not been fully documented. These requirements will be used to complete systematic rankings of all possible commercial devices.

Similarly, a specification ([E1101107-v3](#)) for requirements of a chiller has been drafted. This is to be used to help identify the most optimal chiller for use in conjunction with each laser. To ensure consistent operations *within* any single interferometer (IFO), all chillers should be the same make and model.

13.4 Receiving Inspections

All custom optics used in the laser projection system are going through 100% inspection upon receipt.

Custom machined parts are being inspected with respect to critical dimensions, which are identified on detailed drawings, by vendors' in-house quality assurance departments whenever possible.

Each laser is shipped with data associated with the awarded Statement of Work ([C1000270-v7](#)). Upon receipt, data are to be verified on site. In addition, it has been determined that circuit boards internal to each RF driver, which are supplied by Access Laser Co. (together with each CO2 laser), must be tested rigorously to determine robustness in functionality. There have been two failures encountered during operational tests of the first article.



LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY

14 Project Planning - Appendix

(i) - Items installed in air

Subsystem	DCN	NOTES	Level	INDENTURE CHART	QUANTITY			ECC No.	TYPE [config.]	NAME	TYPE	MODEL STATUS	DWG STATUS	REV	REV	REV		
					REQ'd	SPARE	TOT UNITS											
COSP System Mihir Jacobson 7-Jan-18 Total No. [MTS] Dwg# = 325 Aggregate %-complete = 45%	{} (QTY) TEA TYPE I X2 IFOs	VACUUM INTERFACE	0			2	0	2	EA									
			1			2	0	2	EA									
EXTERNAL TO VACUUM	{} (QTY) TEA TYPE I X2 IFOs	VACUUM INTERFACE	1			1	0	1	EA	D1000634	-01	aLIGO TCS CO2P TABLE ASSY, H1L1	TopAssy	20	0	MTS	MA	
			2			1	0	1	EA	D1001627	-01	VIEWPORT ENCLOSURE ASSY, H1L1 CO2P TCS	PRIT	100	0	MTS	MA	
			2			1	0	1	EA	D1000439		TCS CO2P OPTICS TABLE ENVELOPE	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000439		aLIGO TCS CO2P SUPPORTS, H1L1	PRIT	100	0	MTS	MA	
			2			1	0	1	EA	D1000439		TCS CO2P ENCLOSURE, H1L1	PRIT	100	0	MTS	MA	
			2			1	0	1	EA	D1001863		aLIGO TCS CO2P TABLE ENVELOPE	PRIT	100	0	MTS	MA	
			1			1	0	1	EA	D1001834		aLIGO TCS CO2P LASER, Access Lspn-50	ASSY	100	100	MTS	MA	
			2			1	0	1	EA	D1000439		aLIGO TCS CO2P MECH OPTICS LAYOUT, H1L1	ASSY	0	0	MTS	MA	
			2			1	0	1	EA	D1000439		aLIGO TCS CO2P H1L1 OPTIC, n-1	PRIT	0	0	MTS	MA	
			2			1	0	1	EA	D1000439		aLIGO TCS CO2P H1L1 OPTIC, n	PRIT	0	0	MTS	MA	
			2			1	0	1	EA	D1000791		aLIGO TCS CO2P H1L1 OPTIC, n-1	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P H1L1 OPTIC, n	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		ROTATION STAGE ASSEMBLY	ASSY	100	100	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n-1	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n-1	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n	PRIT	0	0	MTS	MA	
			1			1	0	1	EA	D1000791		ROTATION STAGE ASSEMBLY	ASSY	100	100	MTS	MA	
			1			1	0	1	EA	D1000791		aLIGO TCS CO2P LASER, Access Lspn-50	ASSY	100	100	MTS	MA	
			{} (QTY) TEA TYPE I X2 IFOs		VACUUM INTERFACE	0			2	0	2	EA						
{} (QTY) TEA TYPE I X2 IFOs	VACUUM INTERFACE	1			1	0	1	EA	D1000630	-01	aLIGO TCS CO2P TABLE ASSY, H2	TopAssy	25	0	MTS	MA		
		2			1	0	1	EA	D1000630	-01	VIEWPORT ENCLOSURE ASSY, CO2P	ASSY	100	100	MTS	MA		
		2			1	0	1	EA	D1000437		TCS VIEWPORTS SPHERICAL BEARING REFLECTOR ASSY	ASSY	30	75	MTS	MA		
		2			1	0	1	EA	D1002439		SPHERICAL BEARING, CO2P VP ENCLOSURE	PRIT	30	75	MTS	MA		
		2			1	0	1	EA	D1000416		SET SCREW	HV	30	25	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P TABLE, H2	PRIT	0	0	MTS	MA		
		1			1	0	1	EA	D1000439		TCS CO2P OPTICS TABLE ENVELOPE	PRIT	100	0	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P SUPPORTS, H2	PRIT	0	0	MTS	MA		
		1			1	0	1	EA	D1000900		TCS CO2P TABLE SUPPORTS ENVELOPE	PRIT	100	0	MTS	MA		
		1			1	0	1	EA	D1000900		aLIGO TCS CO2P ENCLOSURE, H2	PRIT	100	0	MTS	MA		
		1			1	0	1	EA	D1001863		aLIGO TCS CO2P TABLE ENVELOPE	PRIT	100	0	MTS	MA		
		1			1	0	1	EA	D1001863		aLIGO TCS CO2P LASER, Access Lspn-50	ASSY	100	100	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P H2 OPTIC, n-1	PRIT	0	0	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P H2 OPTIC, n	PRIT	0	0	MTS	MA		
		2			1	0	1	EA	D1000791		ROTATION STAGE ASSEMBLY	ASSY	60	60	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n-1	PRIT	0	0	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P ISS ELECTRONICS MECH SUPPORT, n-1	PRIT	0	0	MTS	MA		
		1			1	0	1	EA	D1000439		aLIGO TCS CO2P TABLE HARDWARE, H2	HV	0	0	MTS	MA		
		{} (QTY) TEA TYPE I X2 IFOs		VACUUM INTERFACE	0			2	2	4	EA							
		{} (QTY) TEA TYPE I X2 IFOs	VACUUM INTERFACE	1			1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER INSTALL ASSY, H1L1	TopAssy	0	0	MTS	MA
2					1	0	1	EA	D1000630	-01	VIEWPORT ENCLOSURE ASSY, H1L1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMBING, H1L1	ASSY	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n-1	PRIT	0	0	MTS	MA		
2					1	0	1	EA	D1000630	-01	aLIGO TCS CO2P CHILLER PLUMB ITEM, n	PRIT	0	0	MTS	MA		



LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY

(ii)a - Electronics

Subsystem Reporter Date	DCN No.	NOTES	Level	INDENTURE CHART	REQ'd	QUANTITY			EOM Item no.	DCC No.	TYPE (conting.)	NAME	TYPE	MODEL STATUS	DVG STATUS	SRC	REV	REY	FDR
						SPARE	TOT	UNITS											
CO2P Supply Micky Johnson Date: _____ Total No. (MTS) Drawn = 335 Aggregate % complete = 45%																			
ELECTRONICS																			
			0		?		EA					alIGO TCS ISS SERVO DRIVER (ACTS ON ADM)	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			1				EA		DXXXXXXXX			ISS DRIVER ASSY CHASSIS (HARDWARE)	PRT	0	0				
			0		?		EA					alIGO TCS CO2P OPD SENSING CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P OPD AMPLIFIER CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P CHILLER FLOWMETER SENSING & INTERLOCK C	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P CHILLER FLOWMETER SENSING CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P LASER TEMP. SENSING CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P LASER FORWARD TEMP. CONTROL SERVO	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P LASER ENABLING (INTERLOCK) CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P LASER POWER SUPPLY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P LASER PZT DRIVER (100V SUPPLY)	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P ADM DRIVER	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				
			0		?		EA					alIGO TCS CO2P ADM FREQUENCY SYNCHRONIZATION CIRCUITRY	ASSY	0	0				
			1				EA		DXXXXXXXX			BOARD LAYOUT		0	0				
			1				EA					GERBER FILES		0	0				
			1				EA		DXXXXXXXX			WIRING DIAGRAMS		0	0				



LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY

(iii)a - Items installed in the vacuum system or at the vacuum interface

Subsystem:	DCN	Notes	Level	INVENTORY CHART	REQ	QUANTITY			DCC No.	TYPE [Config]	NAME	TYPE	MODEL STATUS	DWG STATUS	SRC	REV	REV	REV
						PAR	DELTA-PDR	FDR										
INTERNAL TO VACUUM																		
E101043	BSC1	mirror BSC3	0		2	0	2	EA	E101044	-01	ALIGO TCS CO2P STEERING MIRROR T ASSY, HLL1	TopAssy	100	100	MIS	N/A	N/A	N/A
E101043			1		1	0	1	EA	D101013		CO2P M1 ASSSEMBLY ENVELOPE, BSC3	PRT	100	0	MIS	N/A	N/A	N/A
E101043			1		1	0	1	EA	D101014		CO2P TCS MIRROR ASSY	ASSY	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		ALIGO TCS CO2P STEERING MIRROR, HLL1	PRT	100	100	MIS	N/A	N/A	v1
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HLL1 STEER M1 SUPPORT	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HLL1 STEER M1A2 BRACKET	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHCS 8-32 X 4.33 LONG, VENTED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HEX NUT, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SHLDR SCREW, 1/4, HEX, HD, 00-32, VENTED, 3003 SS	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		ALIGO TCS CO2P STEERING MIRROR 1	ASSY	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HLL1 STEER M1A2 BRACKET	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HELI COIL (M60, 10-32 X 1.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHLDR SCREW, 1/4, HEX, HD, 00-32, VENTED, 3003 SS	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SHCS 8-32 X 7.0 LONG, VENTED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHCS 8-32 X 5.0 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		FLAT WASHER, #8, AN PLATED	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HLL1 STEER M1 BRACKET	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 14-20 X 2.0 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HELI COIL (M60, 8-32 X 3.0 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SHCS 8-32 X 7.0 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		TCS 3/4 HLL INTERFACE DIAPHR	PRT	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		STANDARD T SECTION, SS 304, 2 X 2 X .25	PRT	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHCS 8-32 X 7.0 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HEX NUT, #8	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHCS 14-20 X 1.75 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SS HEX JAM NUT, 14-20	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		FLAT WASHER, #8	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		TCS 3/4 HLL STRONG BACK	PRT	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		HELI COIL (M60, 8-32 X 2.50 LONG)	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		STANDARD ANGLE SECTION, SS 316, 1.25 X 1.25 X .25	PRT	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		ALIGO WEDGE SUPPORT ASSY, TCS STEER MIRROR 1	ASSY	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SHCS 14-20 X 1.75 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		STANDARD T SECTION, SS 304, 2 X 2 X .25	PRT	100	100	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		HEX NUT, #8	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SHCS 14-20 X 1.5 LONG	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		SS NUT, HEX, HD, 14-20, AN PLTD	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101014		SS HEX JAM NUT, 14-20	PRT	100	0	MIS	N/A	N/A	N/A
E101043			3		3	0	3	EA	D101013		FLAT WASHER, #8	PRT	100	0	MIS	N/A	N/A	N/A



LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY

(iii)d - Items installed in the vacuum system or at the vacuum interface

Table with columns: Subsystem, Reporter, Date, DCM No., Notes, Level, Inventory Chart, Ref ID, Spares, Qty, Units, BOM Ref No., DCC No., Type, Name, Type, Model, Divg Status, SPC, REV, PDR, deka-PDR, FDR, REV, REV, First Article, REV. Includes a detailed list of components like BSC7, BSC8, mirrors, and optics assemblies.

Total No. (MFG) Drawz : 526
Approved & Complete : 454

Subsystem: COSE System
Reporter: Mikko Jacobsson
Date: 1-Jan-02



LASER INTERFEROMETER GRAVITATIONAL WAVE OBSERVATORY

(iii)e - Items installed in the vacuum system or at the vacuum interface

Table with columns: Subsystem, Reporter, Date, DCN, No., Notes, Level, Incidence Chart, Ref, Spare, Quantity, E, Tot, Units, BOM Item No., DCC No., Type (Config), Name, Type, Model Status, SPC, Rev, PDR, FDR, REV, First Article

COBP System
Mingyi Jacobson
E-Jacob-02
Total No. (MIS) Drawn: 325
Aggregates & complete: 45%

