

## Material Loss Angles from Direct Measurements of Broadband Thermal Noise: Statistical Analysis and Preliminary Comparison with Results from Mixture Theory

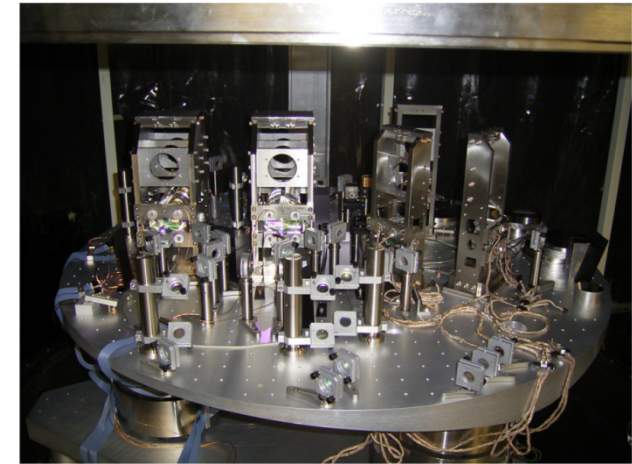
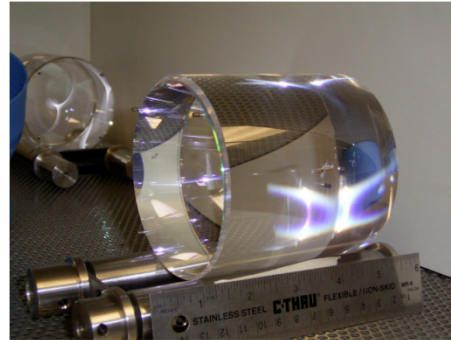
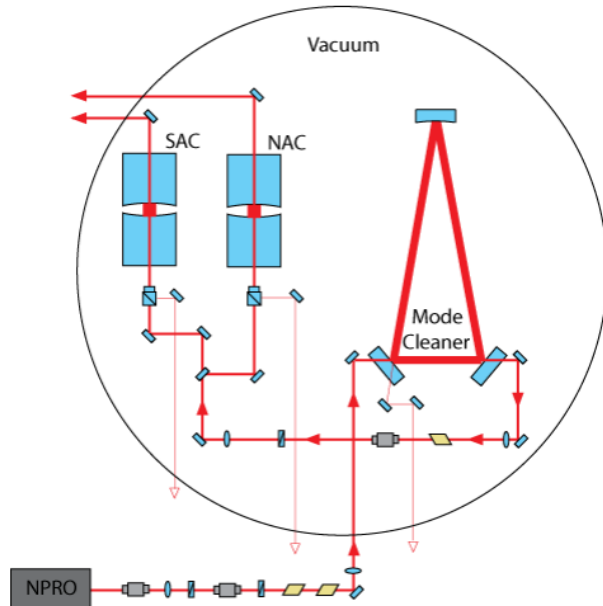
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**LIGO-G1101096**



fit data to model

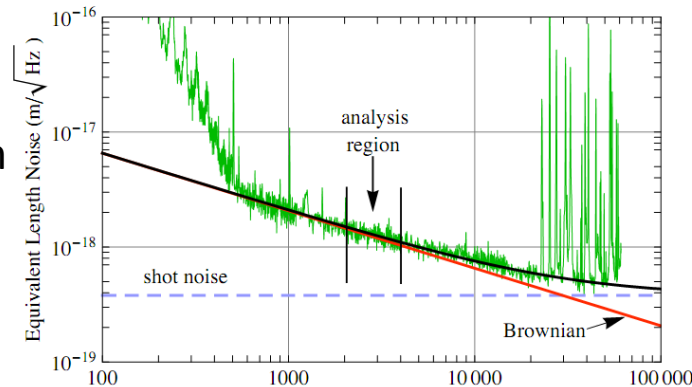
[G. Harry et al., CQG 19 (2002) 897]

$$S_B(f) = \frac{2k_B T}{\pi^{3/2} f} \frac{(1 - \sigma^2)}{wY} \phi_c$$

→  $\phi_c$

Spectrum Analyzer

calibration →





# Individual loss angles



Measurements on different coatings give 2 equations and 2 unknowns, relating Quarter-Wave (QWL) and Optimized (OPT) coating loss to the losses of Silica and Tantalum layers

$$\phi_C^{(QWL)} = A\phi_{SiO_2} + B\phi_{Ta_2O_5}$$

$$\phi_C^{(OPT)} = C\phi_{SiO_2} + D\phi_{Ta_2O_5}$$

$$A = b_{SiO_2} d_{SiO_2}^{(QWL)} \quad B = b_{Ta_2O_5} d_{Ta_2O_5}^{(QWL)}$$

$$C = b_{SiO_2} d_{SiO_2}^{(OPT)} \quad D = b_{Ta_2O_5} d_{Ta_2O_5}^{(OPT)}$$

$$b_X = \frac{1}{\sqrt{\pi}} \left( \frac{Y_X}{Y_S} + \frac{Y_S}{Y_X} \right)$$

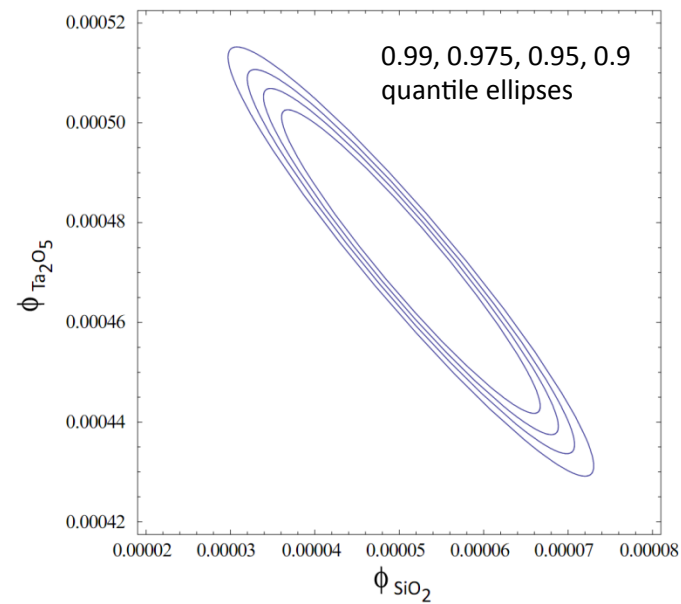
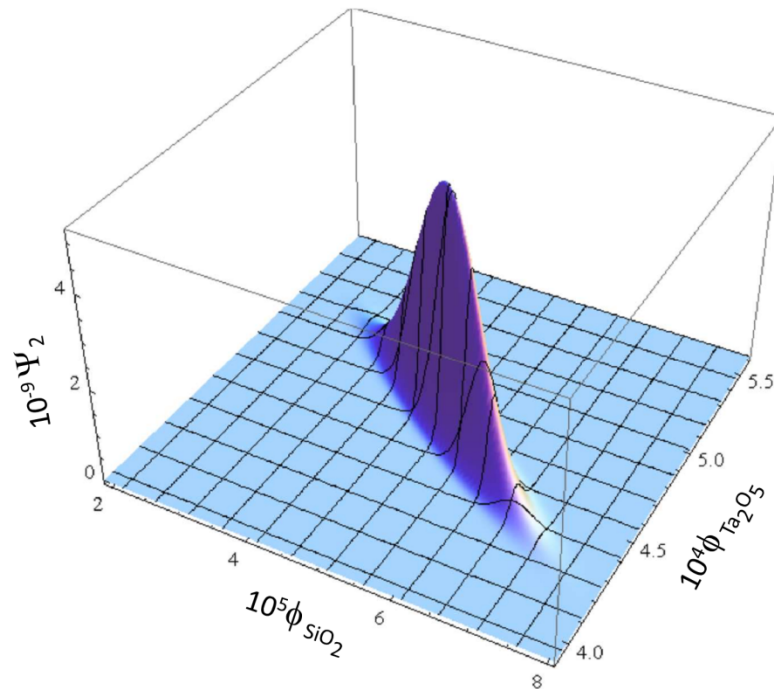
Fastest way to do this is with matrix algebra:

$$\mathbf{M} \cdot \phi = \Phi_c \quad , \text{ with } \left\{ \begin{array}{l} \Phi_c = \{ \Phi_c^{(QWL)}, \Phi_c^{(OPT)} \} \\ \phi = \{ \phi_{SiO_2}, \phi_{Ta_2O_5} \} \\ \mathbf{M} = \begin{bmatrix} b_{SiO_2} d_{SiO_2}^{(QWL)} & b_{Ta_2O_5} d_{Ta_2O_5}^{(QWL)} \\ b_{SiO_2} d_{SiO_2}^{(OPT)} & b_{Ta_2O_5} d_{Ta_2O_5}^{(OPT)} \end{bmatrix} \end{array} \right.$$

Error bars (assumed independent and Gaussian) are handled consistently, resulting into correlated, Gaussian-distributed material loss angles ...

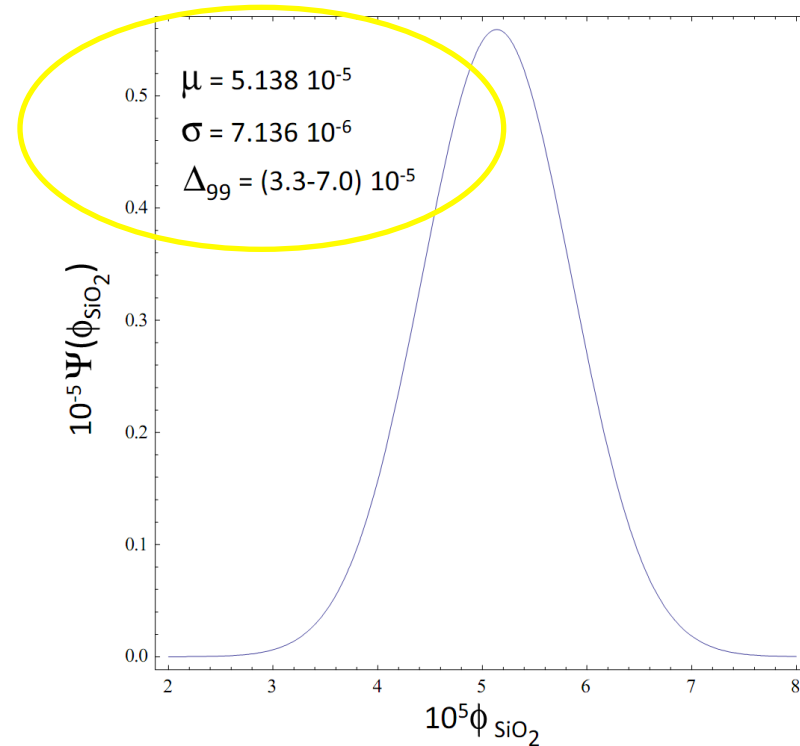
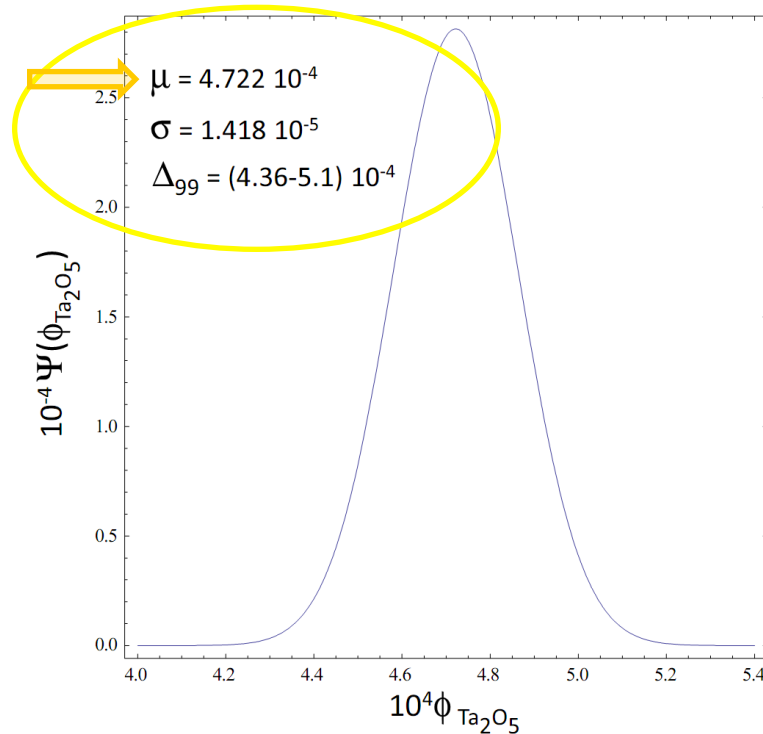
$$\underline{E(\phi)} = \mathbf{M}^{-1} \underline{E(\Phi_c)}, \quad \text{cov}(\phi) = \mathbf{M}^{-1} \cdot \begin{bmatrix} \sigma_{\Phi_c^{(QWL)}}^2 & 0 \\ 0 & \sigma_{\Phi_c^{(OPT)}}^2 \end{bmatrix} \cdot [\mathbf{M}^{-1}]^T$$

Hence, the TNI measurements of QWL and OPT coatings based on plain Tantalum give:



The *marginal* distributions (which take into account uncertainties in *both* numbers) of Silica and plain Tantalum loss angles are easily computed

$$\Psi(\phi_{SiO_2}) = \int_{-\infty}^{\infty} d\phi_{Ta_2O_5} \Psi_2(\phi_{SiO_2}, \phi_{Ta_2O_5}), \quad \Psi(\phi_{Ta_2O_5}) = \int_{-\infty}^{\infty} d\phi_{SiO_2} \Psi_2(\phi_{SiO_2}, \phi_{Ta_2O_5})$$





# Doped Tantalum



Doped Tantalum is harder because the system is *ill-conditioned*, or

$$\det M \approx 0$$

However, the low-index layers here are made from fused silica, i.e., the same material used in the undoped coatings. This means we can use the previous value for the fused-silica loss,

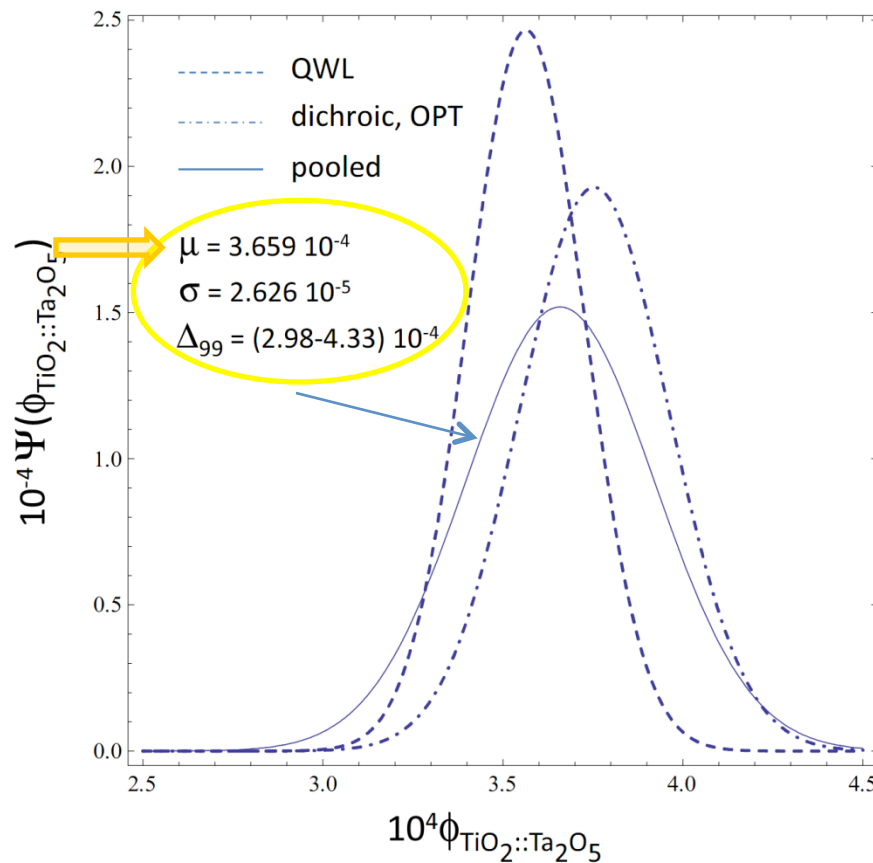
$$\phi_{SiO_2} = (5.138 \pm 0.714) \times 10^{-5}$$

leaving us with only one unknown. We still have two equations, and we can use this previous value for the silica loss to get two (Gaussian) distributions for the doped-tantalum loss. We expect them to agree, and they do, yielding

$$\phi_{Ta_2O_5:TiO_2} = (3.56 \pm 0.16) \times 10^{-4}$$

$$\phi_{Ta_2O_5:TiO_2} = (3.75 \pm 0.21) \times 10^{-4}$$

We may pool (combine) the two distributions of the doped-Tantala loss. Average and uncertainties propagate in the usual way.



$$\langle \phi_{TiO_2::Ta_2O_5} \rangle = \frac{\langle \phi_{TiO_2::Ta_2O_5} \rangle_1 + \langle \phi_{TiO_2::Ta_2O_5} \rangle_2}{2}$$

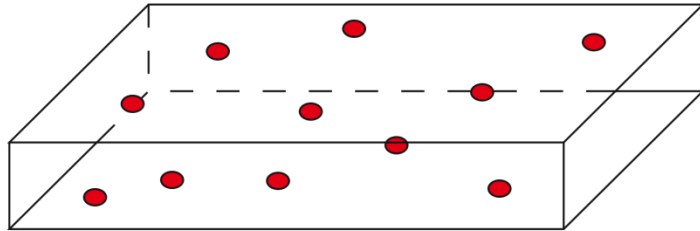
$$\sigma_{\phi_{TiO_2::Ta_2O_5}} = \left( \sigma_{\phi_{TiO_2::Ta_2O_5},1}^2 + \sigma_{\phi_{TiO_2::Ta_2O_5},2}^2 \right)^{1/2}$$

$$\phi_{Ta_2O_5::TiO_2} = (3.66 \pm 0.26) \times 10^{-4}$$



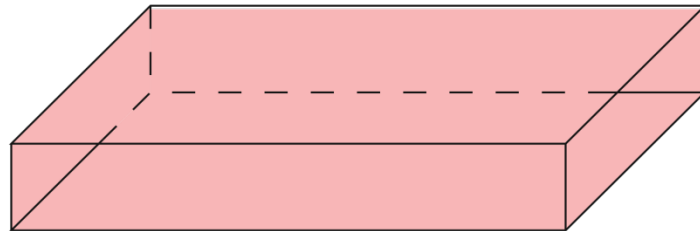


# Effective-Medium Theory



Composite materials (mixtures) can be modeled by an appropriately-weighted average of macroscopic properties of both components.

Replace actual, “composite” system with a homogeneous, “effective” medium.



Effective for a wide variety of properties  
dielectric constant  
index of refraction  
elastic modulus  
loss angle  
etc.

Results depend somewhat on inclusion concentration, morphology, orientation.

First model the index of refraction and check the Titania volume fraction.  
(Use Bruggemann formula for modeling the effective medium.)

$$\eta_2 \frac{\epsilon_2 - \epsilon_{mix}}{\gamma \epsilon_2 + (1 - \gamma) \epsilon_{mix}} + (1 - \eta_2) \frac{\epsilon_1 - \epsilon_{mix}}{\gamma \epsilon_1 + (1 - \gamma) \epsilon_{mix}} = 0, \quad \epsilon = n^2$$

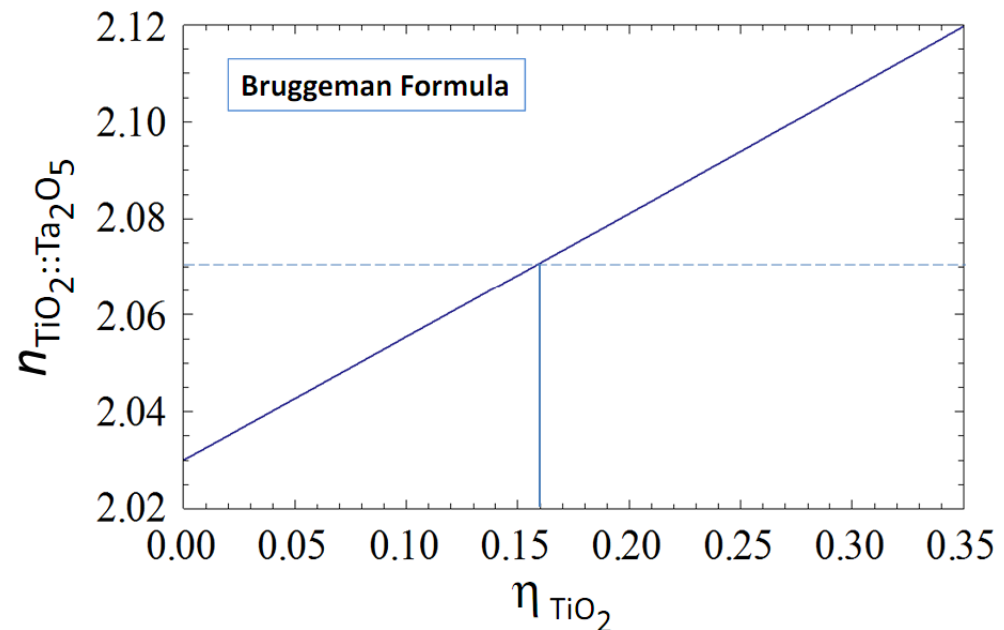
using (LIGO) reference values for  
pertinent optical indexes

$$n_{Ta_2O_5} = 2.03$$

$$n_{TiO_2} = 2.29$$

$$n_{TiO_2::Ta_2O_5} = 2.07$$

➔  $\eta = 0.16$



Next calculate Young's modulus and Poisson's ratio.


Barta's microscopic derivation of Bruggeman-like mixture formulas for viscoelastic parameters of a glassy-oxide composite yields

$$\left\{ \begin{array}{l} (1 - \eta_2) \frac{X - X_1}{2X + (X_1/y_1)(\sigma_1 + 1)} + \eta_2 \frac{X - X_2}{2X + (X_2/y_2)(\sigma_2 + 1)} = 0 \\ (1 - \eta_2) \frac{(X/y) - (X_1/y_1)}{2X + (X_1/y_1)(\sigma_1 + 1)} + \eta_2 \frac{(X/y) - (X_2/y_2)}{2X + (X_2/y_2)(\sigma_2 + 1)} = 0 \end{array} \right. ,$$

$$X = \frac{\sigma Y}{\sigma + 1}, \quad y = \sigma - 2$$

System can be solved in closed form . [S. Barta, «Effective Young modulus and Poisson's ratio for the particulate composite," J. Appl. Phys. 75 (1994) 3258].

Frequently quoted values must be handled w. care, especially for Titania ...



	SiO <sub>2</sub>	TiTa <sub>2</sub> O <sub>5</sub>	Ta <sub>2</sub> O <sub>5</sub>	TiO <sub>2</sub>
Loss angle	0.4×10 <sup>-4</sup> [37] 0.5×10 <sup>-4</sup> [46] 10 <sup>-3</sup> on sapphire [47]	2.3×10 <sup>-4</sup> [37] 2×10 <sup>-4</sup> [36]	3.8×10 <sup>-4</sup> [1]	6.3×10 <sup>-3</sup> deduced from [48]
Young's modulus (GPa)	72 [1, 10, 37] 40-60 [14]	140 [37]	140 [37]	290 [12]
Poisson's ratio	0.17 [1, 10]	0.23 [6]	0.23 [37]	0.28 [12]

J. Franc et al., ET-021-09 (2009).

Values from a *single* experiment: 25-doublers QWL Silica/Titania coating [P. Amico et al., J. Phys. Conf. Ser. 32 (2006) 413]. Thickness of Titania layers was 116nm. Well above limit-thickness for preventing crystallization upon annealing [S. Chao et al., J. Opt. Soc. Am. A16 (1999) 1477]. Reported loss angle most likely due to crystallization.

In the amorphous phase  $Y_{TiO_2}$  is 160 - 170 Gpa. [T. Modes et al., Surf. Coat. Technol. 200 (2005) 306] Quoted  $Y = 290$  Gpa is OK for the *crystalline* (Rutile) phase [O. Zywitzki, et al., Surf. Coat. Technol. 180 (2004) 538].

Large spreads among values obtained from different measurement techniques...

Conjectured values - No direct measurements of  $Y$  or  $\sigma$  on doped Tantalum reported yet.

## Apparatus for Mechanical Loss Measurements in Low Loss Materials at Audio Frequencies and Low Temperatures\*

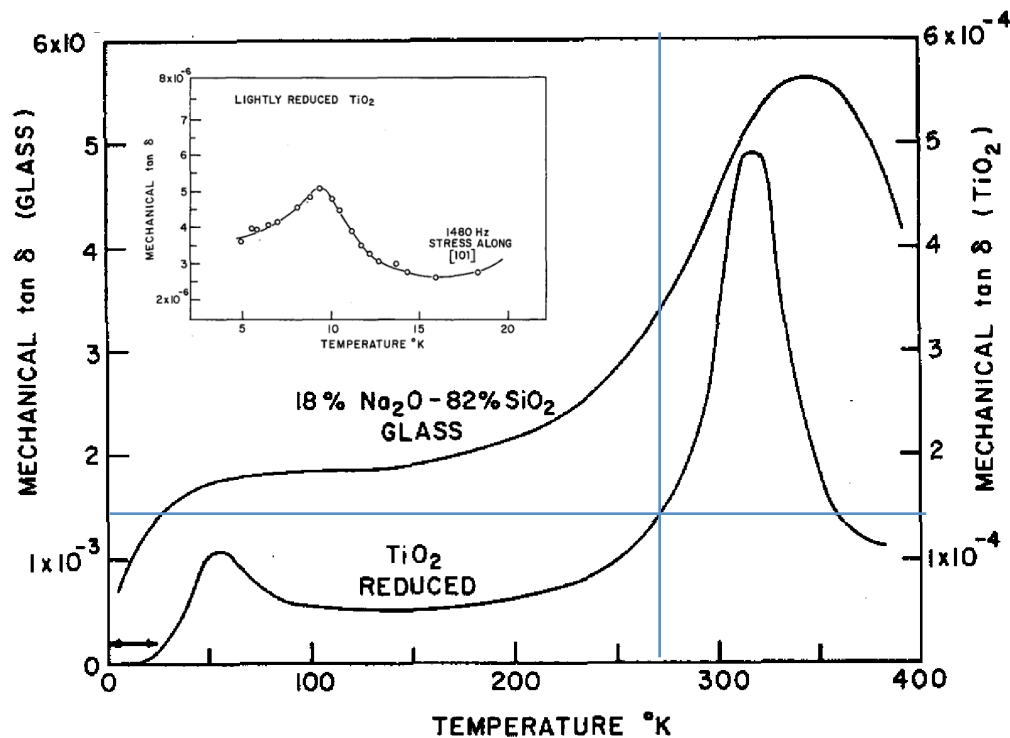
W. W. SCOTT AND R. K. MACCRONE\*\*

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(Received 8 January 1968; and in final form, 14 February 1968)

A new apparatus for measuring mechanical loss in low loss materials at low temperatures is described. The method has several advantages over existing techniques. Using this apparatus, losses as low as  $2 \times 10^{-6}$  with a resolution of  $10^{-7}$  have been reproducibly measured at 4.2°K in TiO<sub>2</sub> (rutile).

- Introduces an apparatus *conceptually similar* to the familiar «cantilever».
- Reported results over a wide range of temperatures from 5K to 400K...
- Little details about tested material.





# Doped Tantalum from EMT



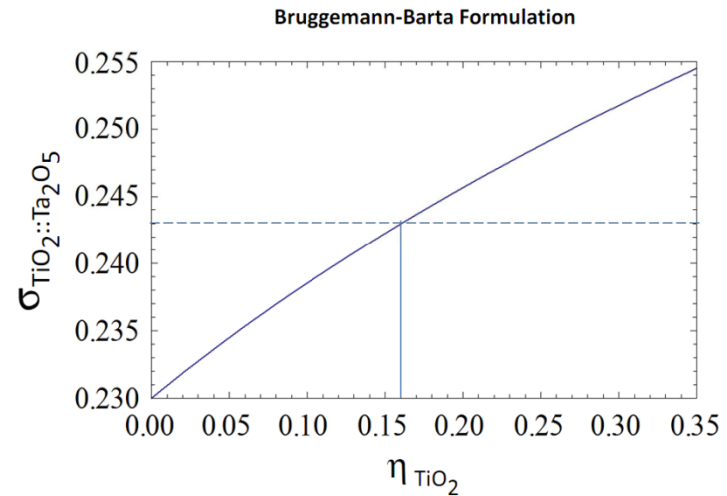
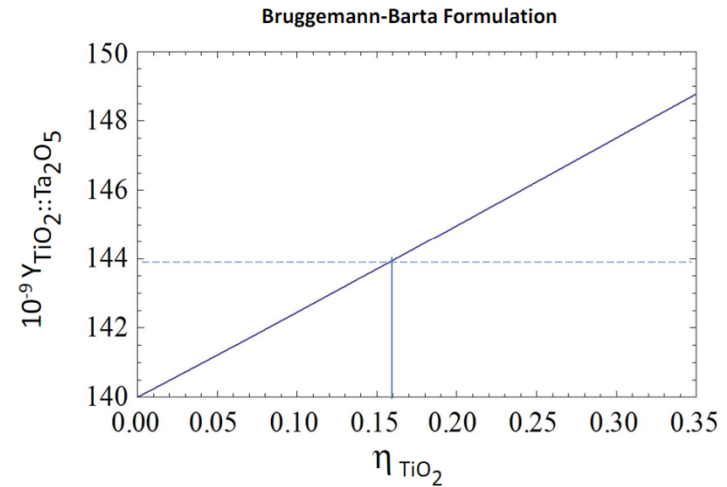
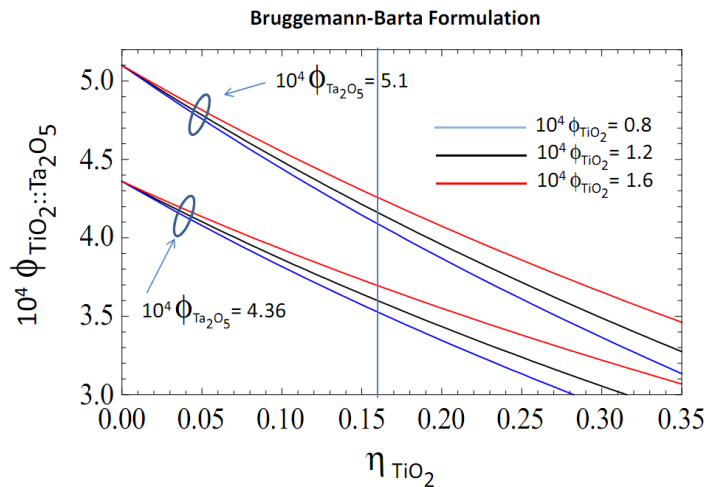
We use Barta-Bruggemann formula to estimate the viscoelastic params of doped Tantalum, using reference values for Titania and plain Tantalum

$$Y_{TiO_2} = 165 GPa$$

$$Y_{Ta_2O_5} = 140 GPa$$

$$\sigma_{Ta_2O_5} = 0.23$$

$$\sigma_{TiO_2} = 0.28$$





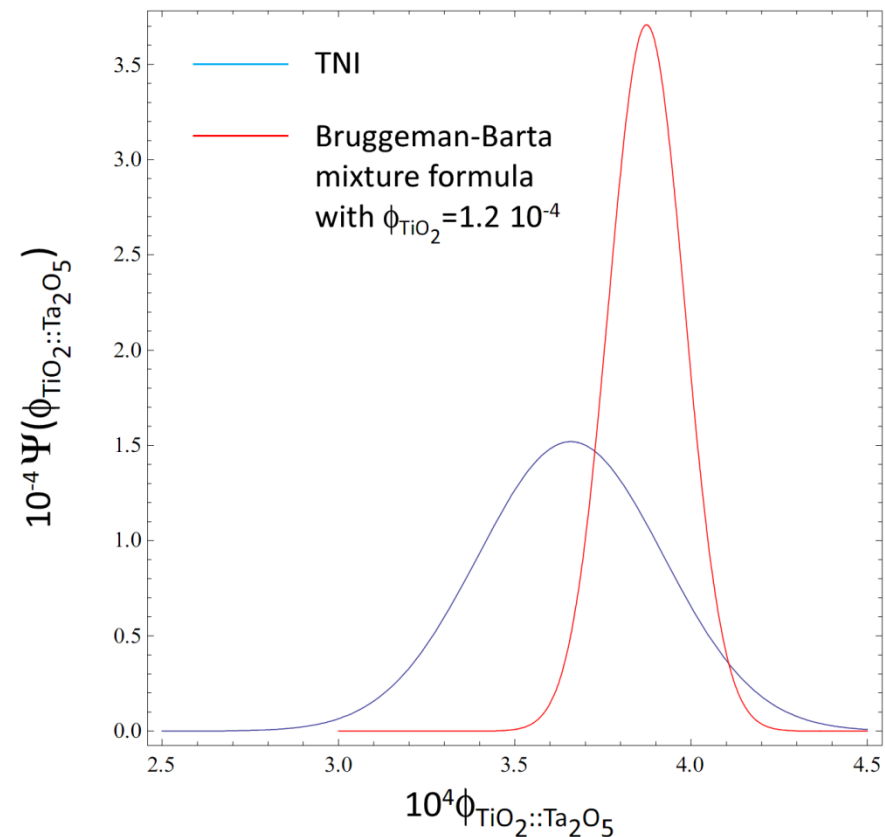
# Mixtures vs Measured



We can compare the doped Tantalum loss angle distribution obtained from TNI measurements to the prediction of EMT, using Scott-MacCrone loss angle for Titania, and the TNI result for plain Tantalum

**TNI : distribution deduced from doped coating measurement, using the marginal distribution of Silica loss angle from the undoped coating measurements.**

**Bruggeman-Barta : distribution deduced using Scott-MacCrone value for Titania loss angle, with plain Tantalum loss-angle distribution from undoped coating measurements.**





# Conclusions



- 
1. First extraction of individual-material loss angles from direct observations of thermal noise.
  2. Simple predictive model for composite material properties including elastic moduli, loss angle.
  3. Loss angles derived from direct noise measurements not entirely in agreement with  $Q_s$ .
  4. Loss-angle ratios between doped and undoped are consistent.

## Caveats:

- a) Agreement is good, but only one material (doped tantala) tested.
- b) Reliable values for pure materials (components) still needed.

Next: predict and test other materials, and/or other morphologies (subwavelength films)



***Back Up Material***



## Conclusions/Issues



TNI allows the direct measurement of coating noise spectra, and the estimation of coating loss and material loss angles. Experiments were carried out on four different Prototypes, two of which used Titania doped Tantalum.

Estimated loss angles are fully consistent with early results in [S.D. Penn et al., CQG 20, 2917 (2003)], but e.g. differ from those by LMA [Ch. Comtet, L-V thermal Noise Workshop, Cascina, 2007] and Glasgow [I. Martin, PhD Thesis, 2009], based on different setups, which yield losses larger for Silica and smaller for (doped) Tantalum. The loss-angle ratio between the doped and undoped material is nonetheless almost the same.

The estimated loss angle distribution for doped Tantalum is consistent with that predicted by EMT, using the estimated loss angle distribution of plain Tantalum, and a fiducial value for Titania loss angle from Scott-MacCrone.

D. Crooks et al., CQG 23 (2006), 4953.

G. Harry et al., CQG 24 (2007) 405.

Material	Loss Angle ( $\times 10^4$ )
SiO <sub>2</sub>	1.0 ± 0.2
Ta <sub>2</sub> O <sub>5</sub>	3.8 ± 0.2 ; 3.0 ± 0.2 (  )
LMA no. 5	2.0 ± 0.1 (  )

76.2 mm Ø x 25.4mm substrate + 30 QWL doublets

C. Comtet, LV –TNW 07, Cascina (2007).

Material	Loss Angle ( $\times 10^4$ )
Ta <sub>2</sub> O <sub>5</sub>	3.02 ± 0.15
LMA no. 5	2.47 ± 0.05
LMA no. 5**	1.93 ± ?

LMA cantilever testbench

P.G. Murray, PhD Thesis, Glasgow (2008).

Dopant (cation conc.)	Mixture	Loss Angle ( $\times 10^4$ )	
		CSIRO	LMA
none	Ta <sub>2</sub> O <sub>5</sub>	3.8 ± 0.1	4.4 ± 0.2
15% TiO <sub>2</sub>	TiO <sub>2</sub> ::Ta <sub>2</sub> O <sub>5</sub>	2.4 ± 0.2	2.0 ± 0.2
35% SiO <sub>2</sub>	SiO <sub>2</sub> ::Ta <sub>2</sub> O <sub>5</sub>	2.5 ± 0.4	-
35% TiO <sub>2</sub>	TiO <sub>2</sub> ::Si <sub>2</sub> O <sub>2</sub>	1.7 ± 0.4	-

76.2 mm Ø x 25.4mm substrate + 30 QWL mixture/silica doublets

**Warning:** - uses naive mixture formulas for  $Y$  and  $\sigma$ ;  
- assumes  $Y_{\text{TiO}_2} \approx 290$  Gpa.

I. Martin, PhD Thesis, Glasgow (2009).

Coating (LMA)	Cantilever	Loss Angle ( $\times 10^4$ )
Ta <sub>2</sub> O <sub>5</sub>	unwelded	4.2 ± 0.3
LMA no. 5*	unwelded	3.0 ± 0.01
LMA no. 5**	welded	1.5 ± 0.1
LMA no. 5***	welded	2.0 ± 0.4
SiO <sub>2</sub>	unwelded	0.97 ± 0.02

110 µm thick cantilever + 0.5 µm single layer



# TNI Coating Prototypes



Coating	Type	Low Index	High Index	Mfr.	$\phi_s \times 10^6$
1	QWL	Silica	Tantala	REO	$8.25 \pm 0.3$
2	Optimized	Silica	Tantala	LMA	$6.85 \pm 0.2$
3	QWL	Silica	Doped Tantala	LMA	$6.0 \pm 0.25$
4	Dichroic	Silica	Doped Tantala	LMA	$5.5 \pm 0.5$

Coating #	$d_L$	$d_H$
1	2.72 $\mu\text{m}$	1.83 $\mu\text{m}$
2	4.05 $\mu\text{m}$	1.36 $\mu\text{m}$
3	2.54 $\mu\text{m}$	1.67 $\mu\text{m}$
3	2.36 $\mu\text{m}$	1.45 $\mu\text{m}$

A. Villar et al., LIGO-G1000937 (2010)

