

Advanced LIGO, nouvelle génération d'interféromètres pour la détection d'ondes gravitationnelles.

Présentation du projet - Isolation des sources de bruits - Focus sur les méthodes d'isolation sismique.

**Fabrice Matichard, Caltech-MIT
05 janvier 2010, à l'ENSIM, Le Mans.**



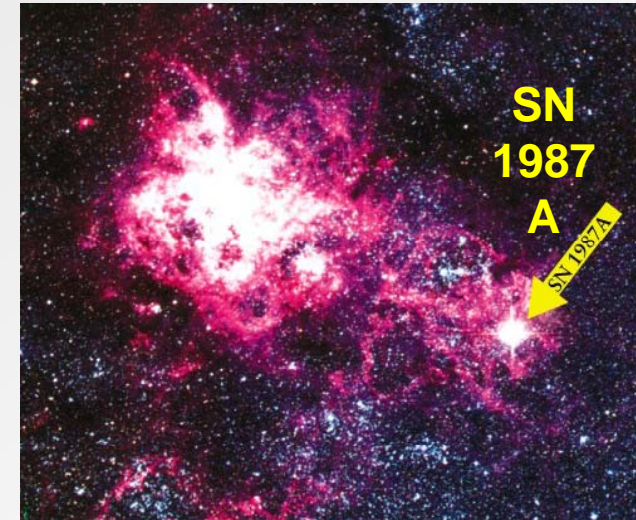
Hanford, Washington



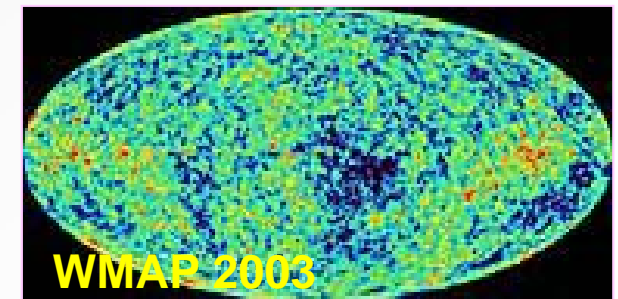
Livingston, Louisiana

Transient

- Coalescence of binary compact objects (neutron stars, black holes, primordial BH)
- Core collapse supernovae
- Black hole normal mode oscillations
- Neutron star rotational instabilities
- Gamma ray bursts
- Cosmic string cusps

**High duty cycle**

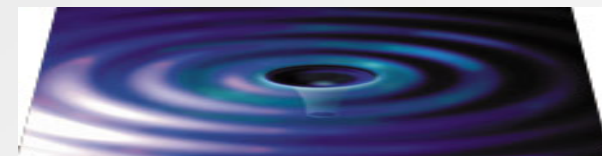
- Periodic emission from pulsars (esp. accretion driven)
- Stochastic background (incoherent sum of many sources or very early universe)
- Expect the unexpected!



**Modeled &
Unmodeled
waveforms**

Gravitational Waves
 “Ripples in space-time”
 Stretch and squeeze the space
 transverse to direction of propagation

$$\left(\nabla^2 - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) h = 0$$



Example:
 Ring of test masses responding
 to wave propagating along z



For a binary neutron star

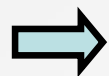
~1.4 Mo pair in Virgo cluster

$$M \approx 10^{30} \text{ kg}$$

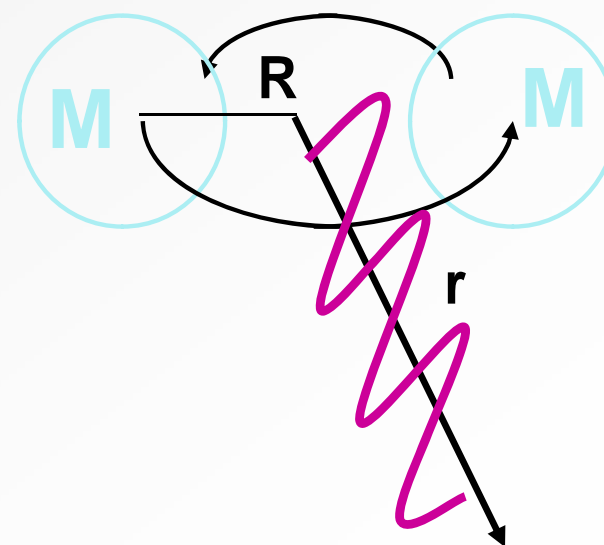
$$R \approx 20 \text{ km}$$

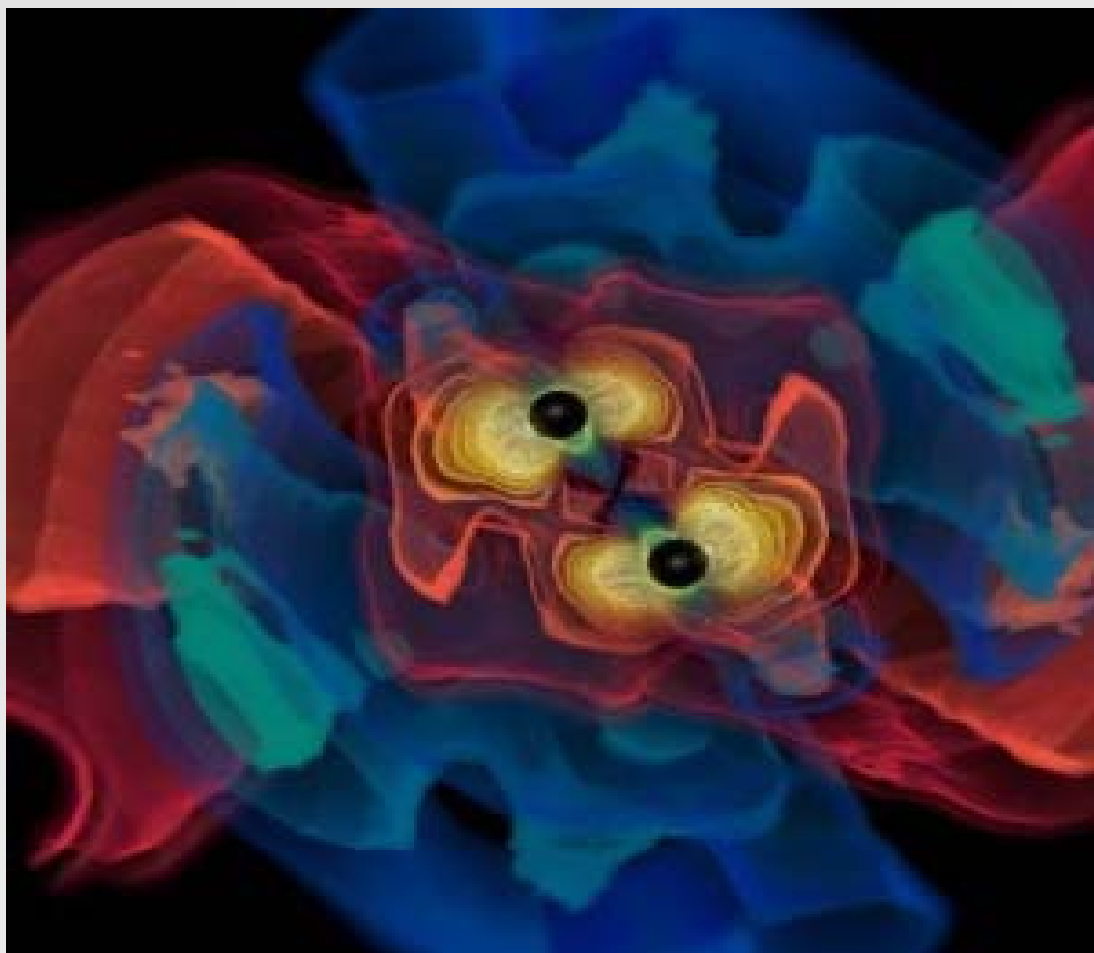
$$f \approx 400 \text{ Hz}$$

$$r \approx 10^{23} \text{ m}$$



$$h \sim 10^{-21}$$

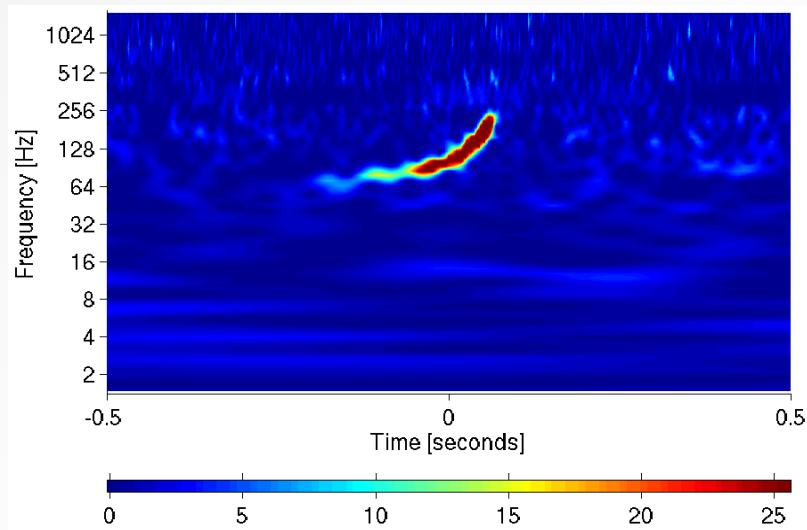


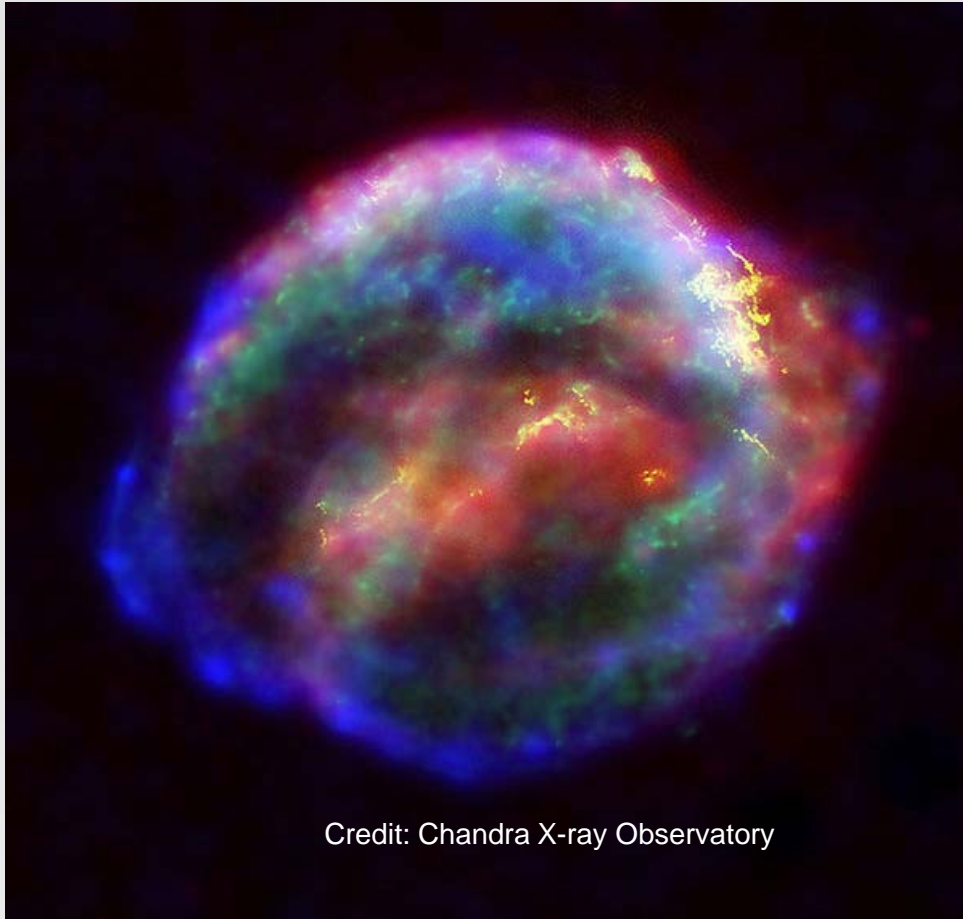


Credit: AEI, CGT, LSU

Coalescing Binary Systems

- Neutron stars,
black holes
- ‘chirped’
waveform

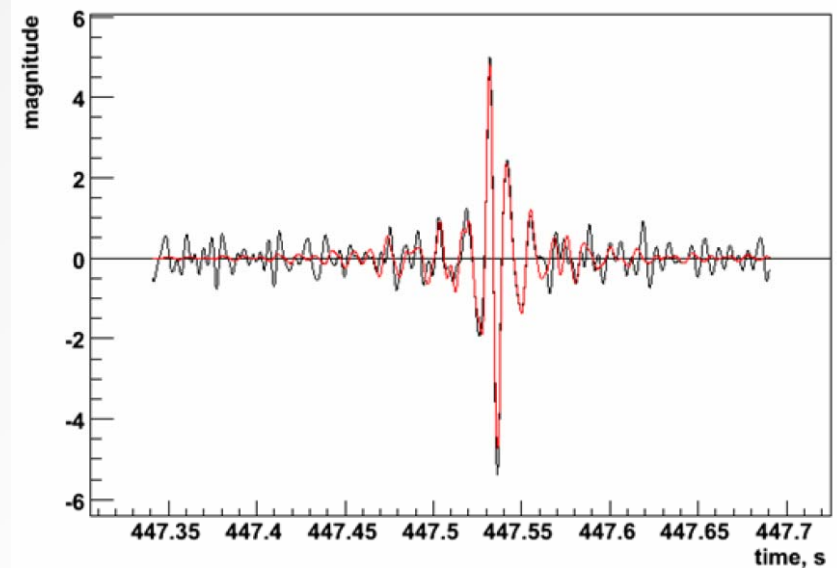


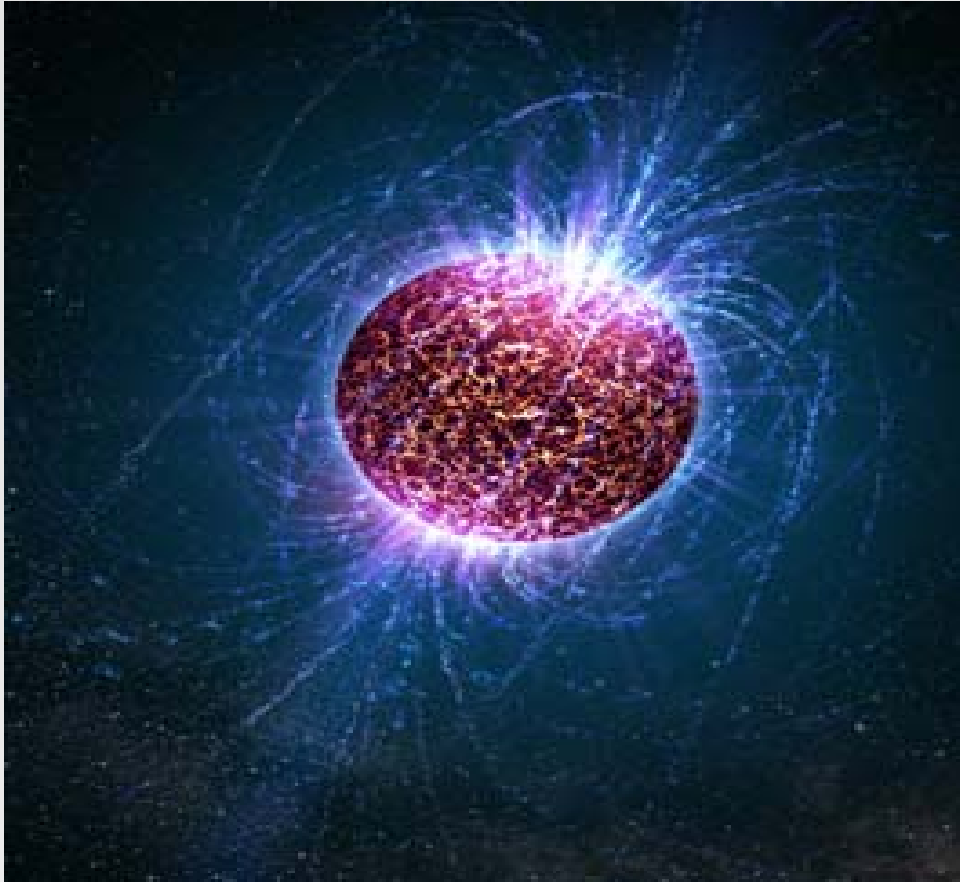


Credit: Chandra X-ray Observatory

'Bursts'

- asymmetric core collapse supernovae
 - cosmic strings
- ? (sources we haven't thought about)

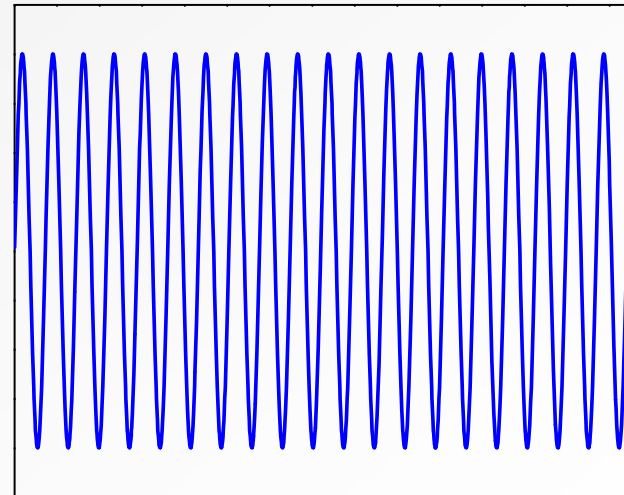


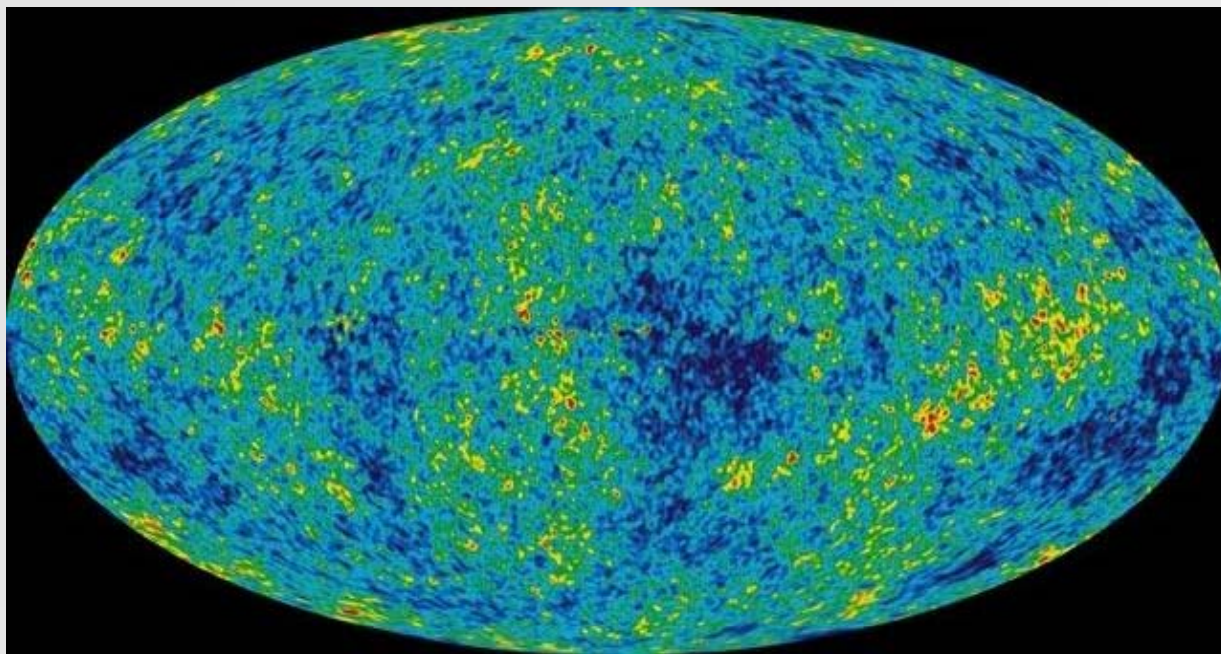


Casey Reed, Penn State

Continuous Sources

- Spinning neutron stars
- monotone waveform

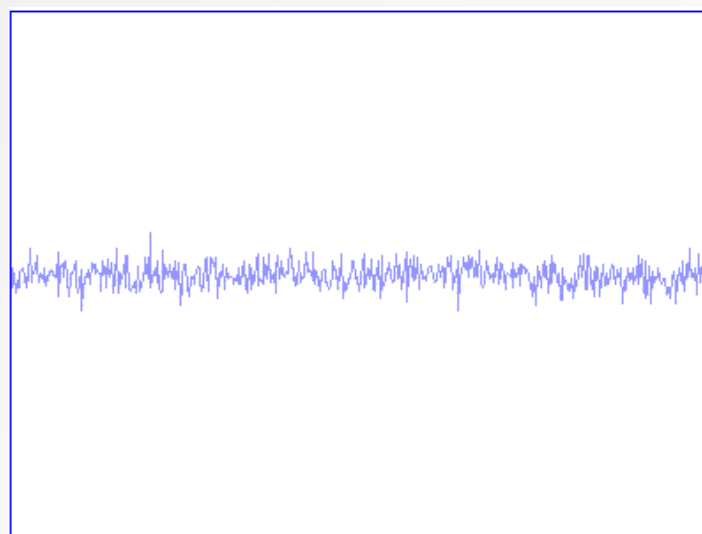




NASA/WMAP Science Team

Cosmic GW background

- residue of the Big Bang
- probes back to 10^{-21} s after the birth of the universe
- stochastic, incoherent background



LIGO



Hanford, WA
4 km interferometer
2 km interferometer

GEO



Hannover, Germany
600 m interferometer

VIRGO



Pisa, Italy
3 km interferometer

TAMA



Tokyo, Japan
300 m interferometer

AIGO

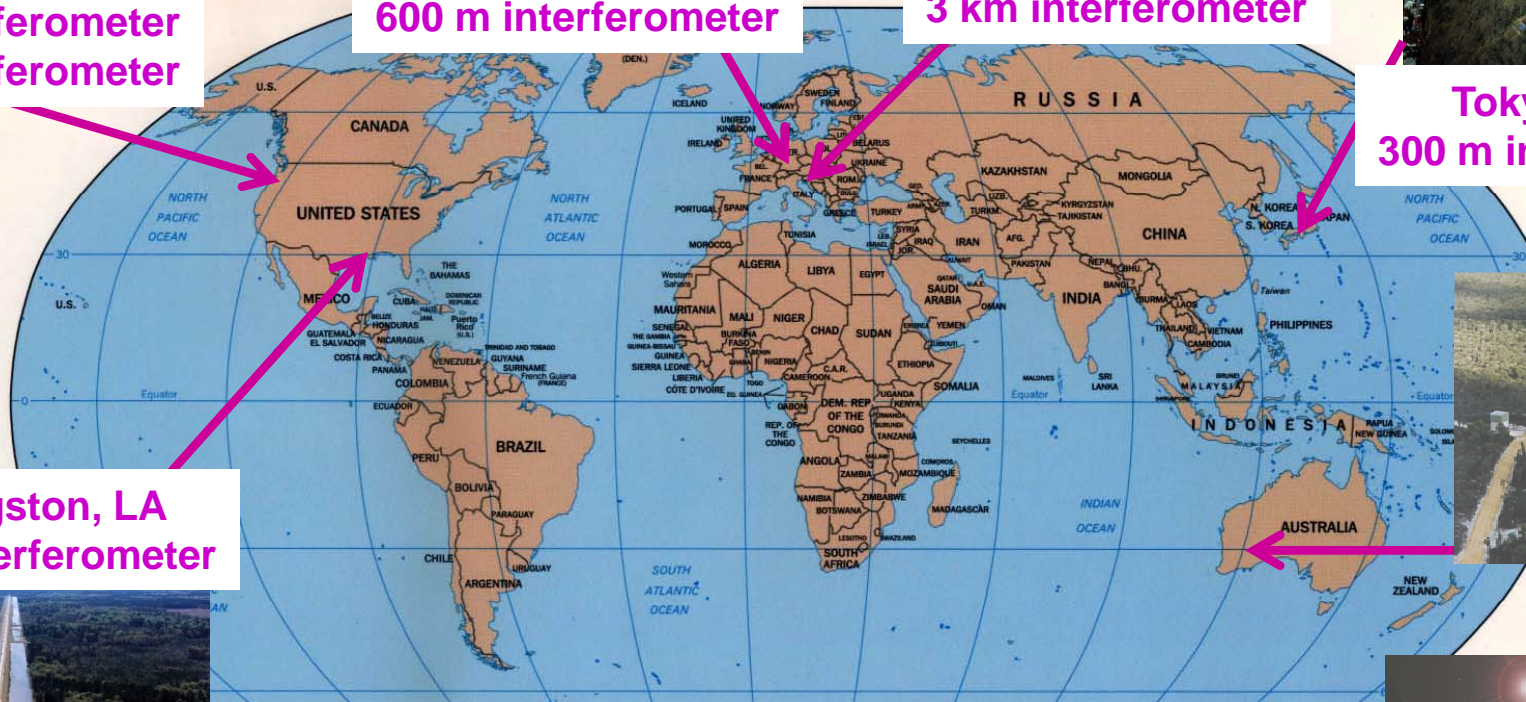


LISA



LIGO

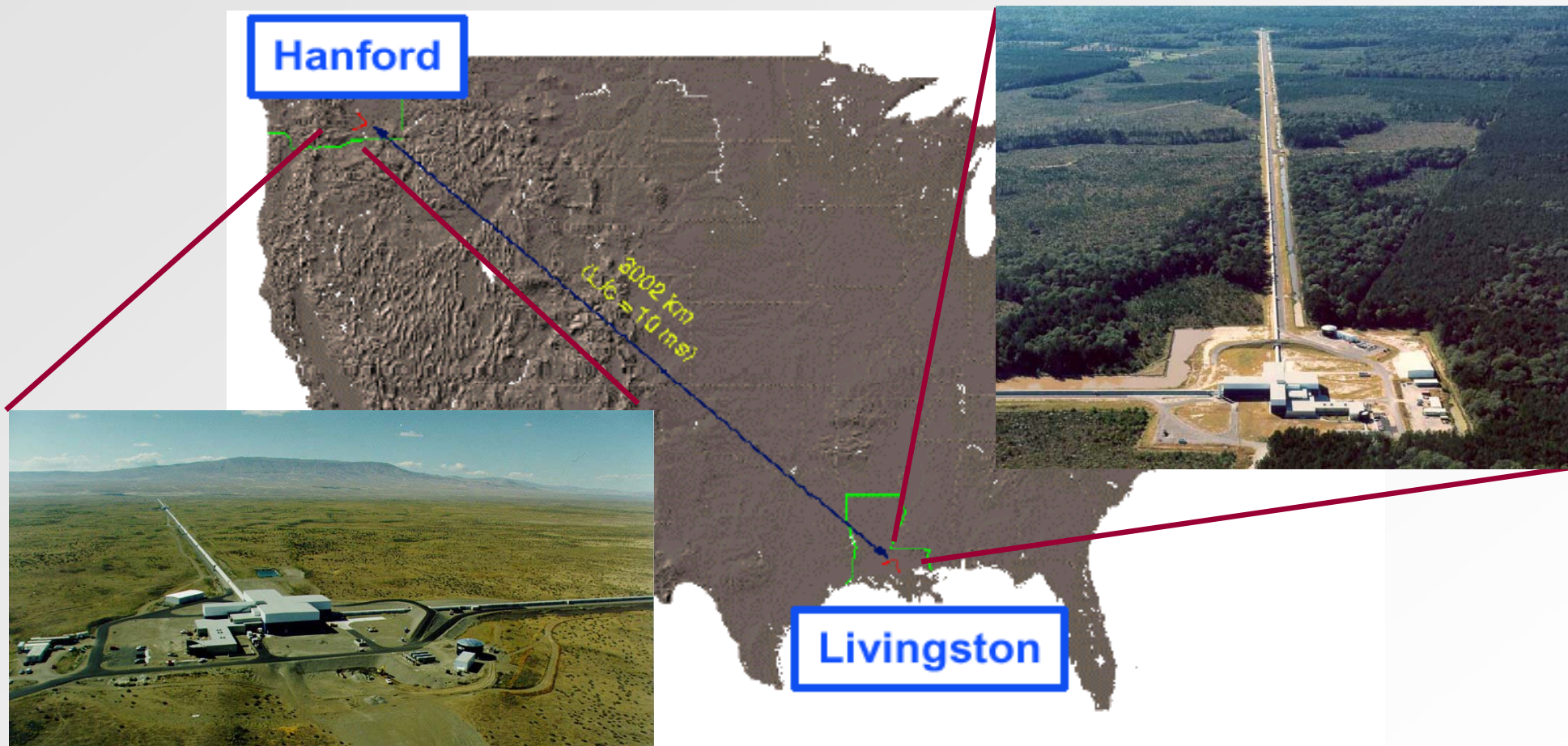
Livingston, LA
4 km interferometer



- Coincident detection to eliminate instrumental artifacts
- Source localization in the sky
- Wave polarization

LIGO Livingston Observatory

- 1 interferometers
- 4 km arms



LIGO Hanford Observatory

- 2 interferometers
- 4 km, 2 km arms

LIGO Observatories are operated
by Caltech and MIT

$$h = \Delta L / L$$

$$L \sim 4 \text{ km}$$

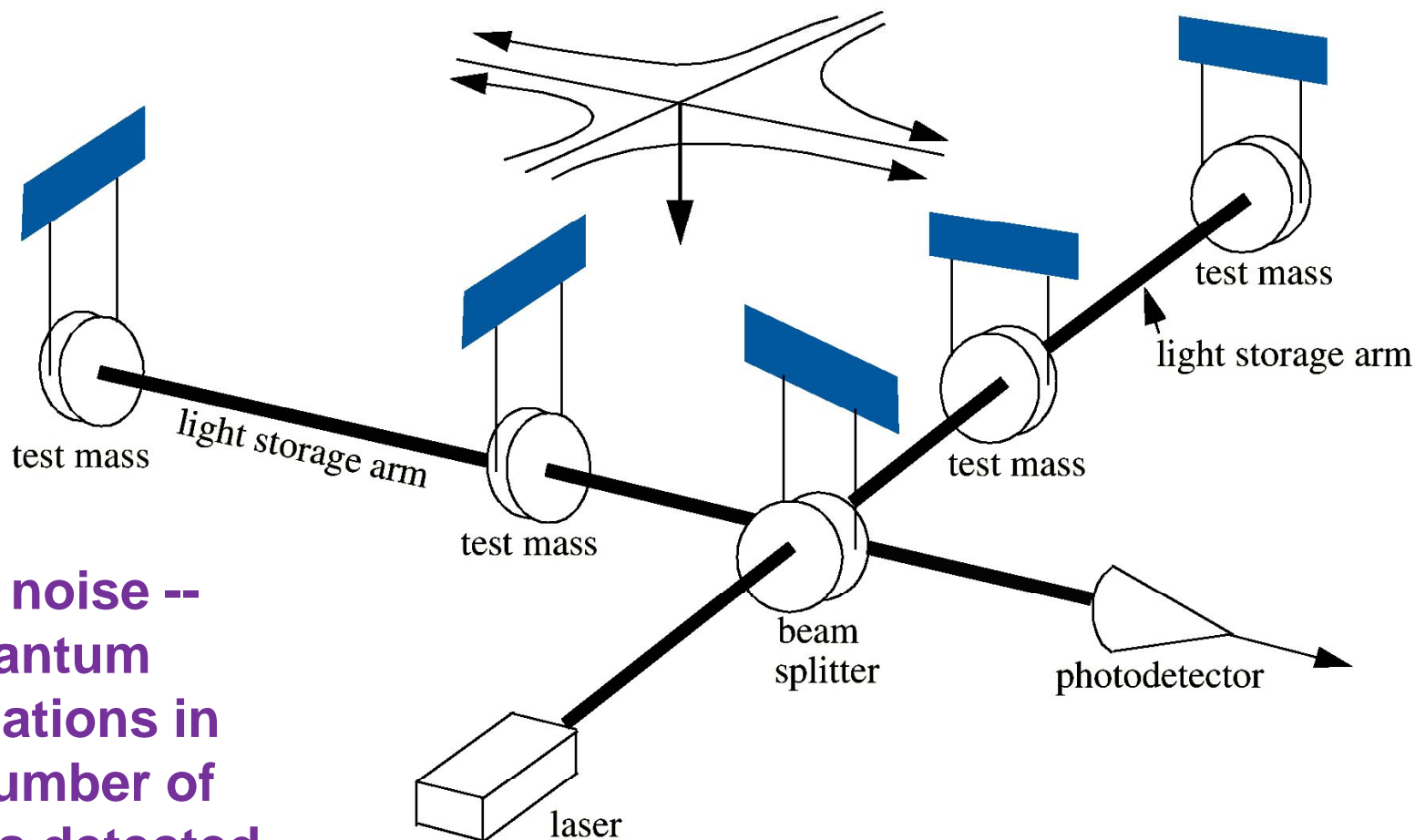
We need $h \sim 10^{-21}$

We have $L \sim 4 \text{ km}$

We see $\Delta L \sim 10^{-18} \text{ m}$

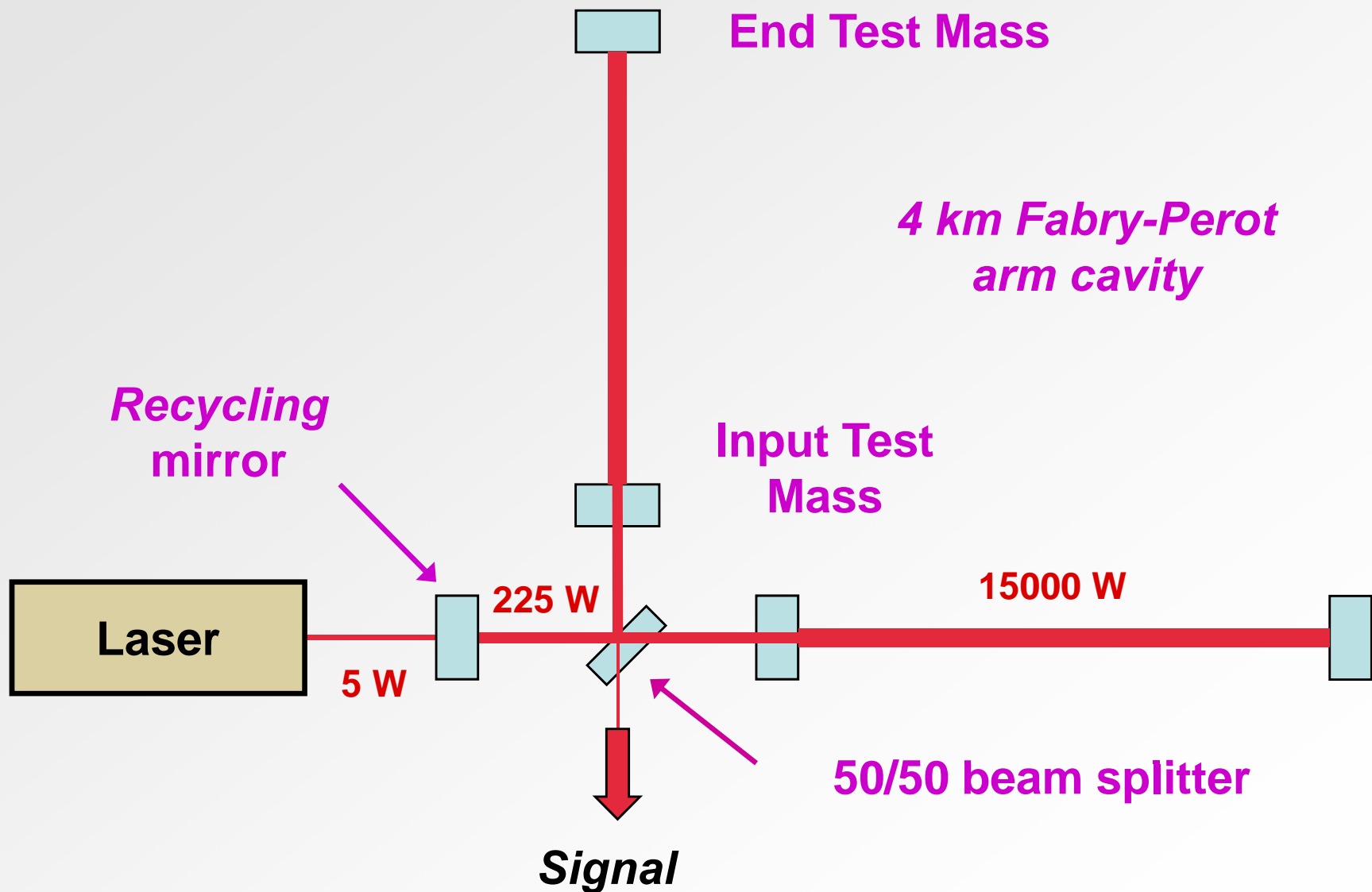
**Thermal noise --
vibrations due
to finite
temperature**

**Seismic motion --
ground motion due to
natural and
anthropogenic
sources**



**Shot noise --
quantum
fluctuations in
the number of
photons detected**

- Power Recycled
 - Michelson Interferometer
 - with Fabry-Perot Arm Cavities

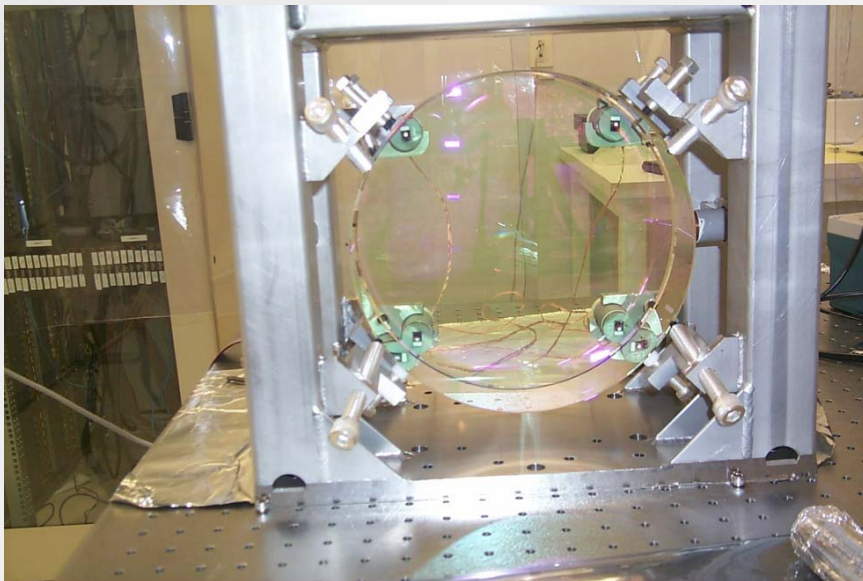


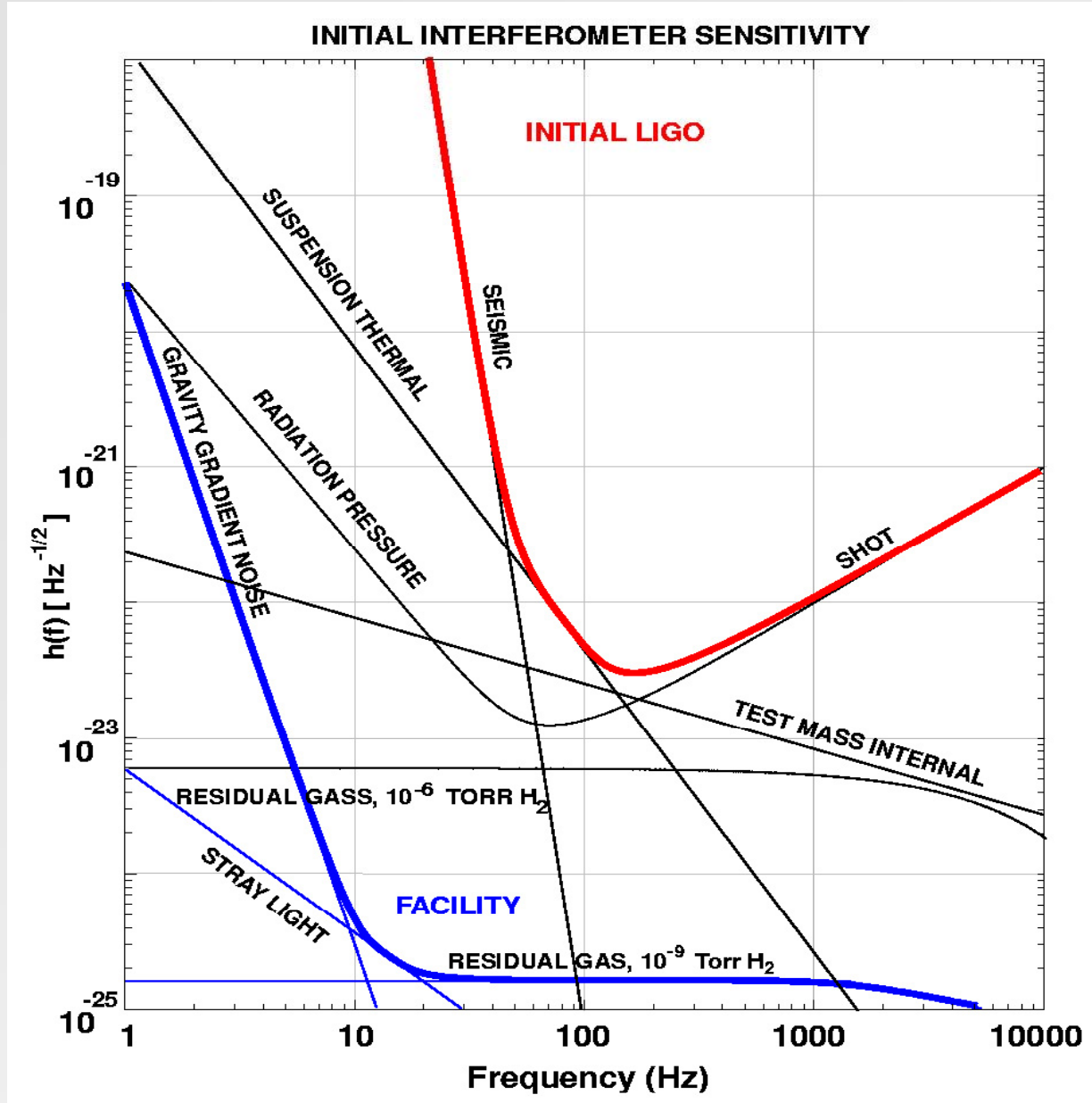


18,000 m³ of vacuum at 10⁻⁹ torr.



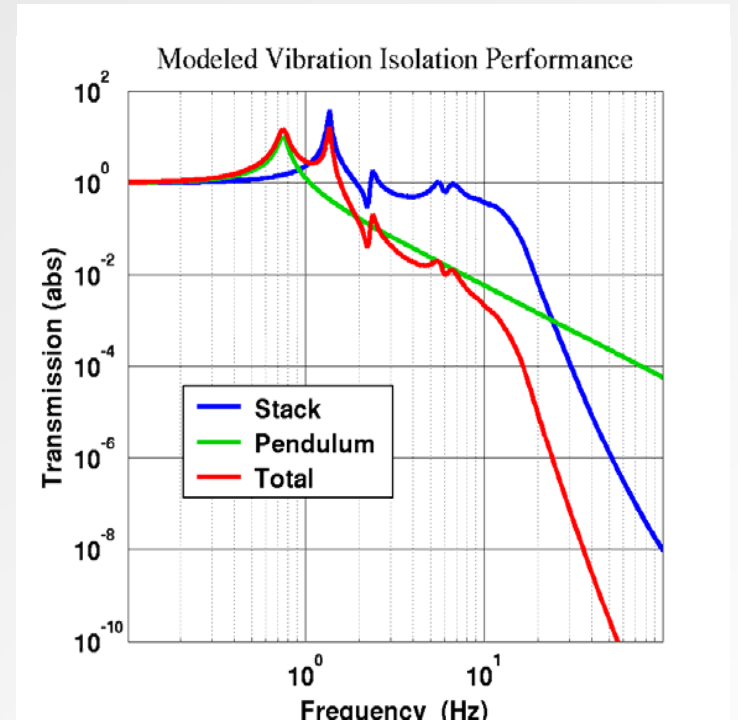
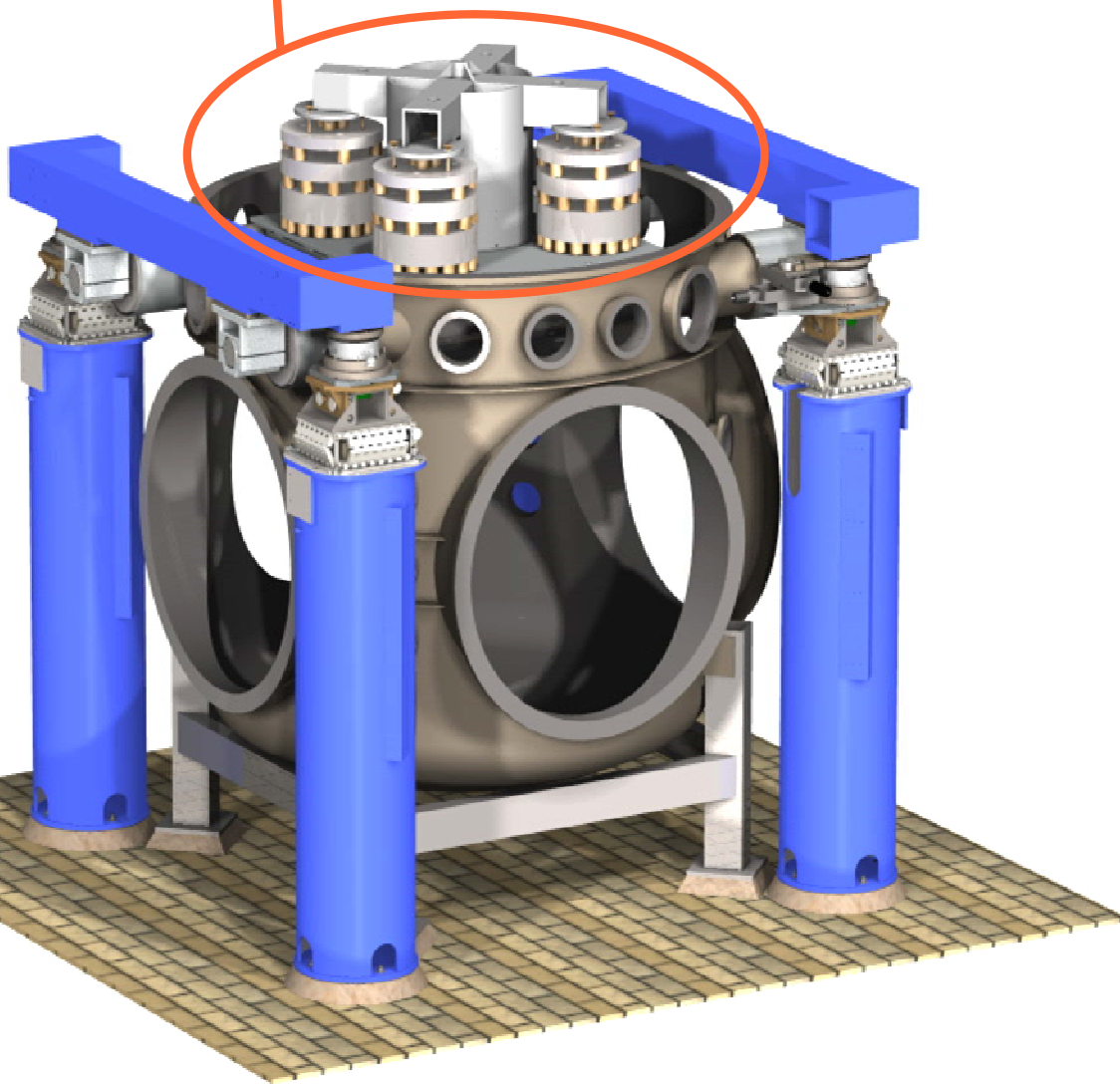
**Beam Tubes: 1.2 m diameter - 3mm stainless, 50 km of weld....
and not one leak!**

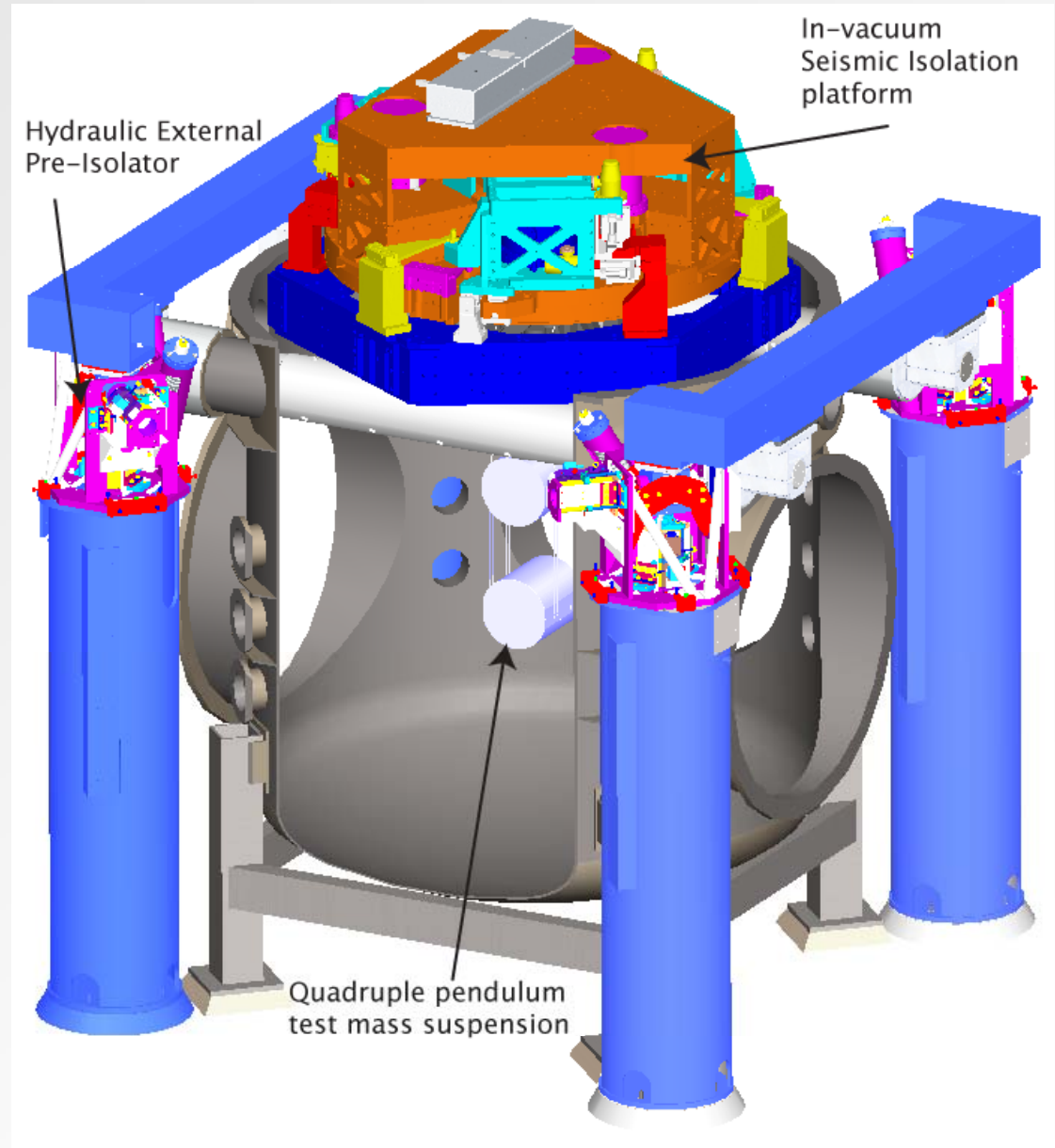
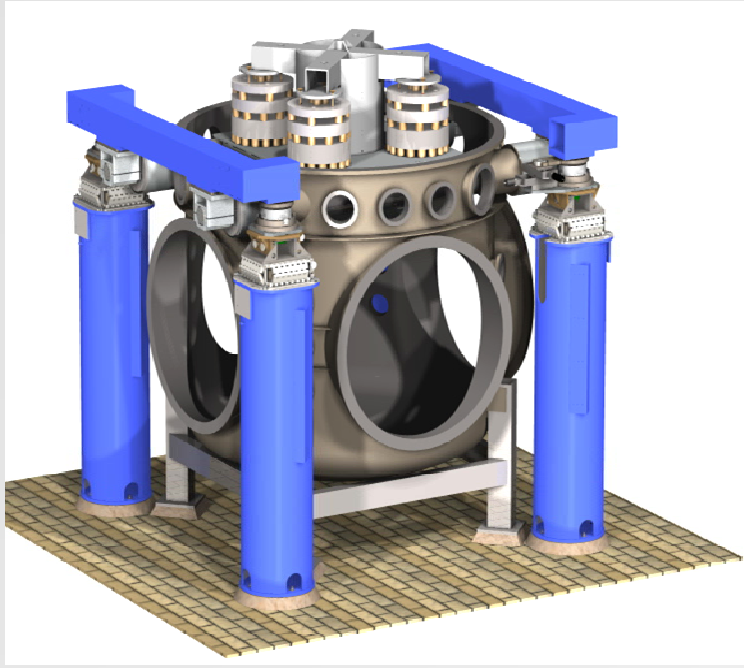




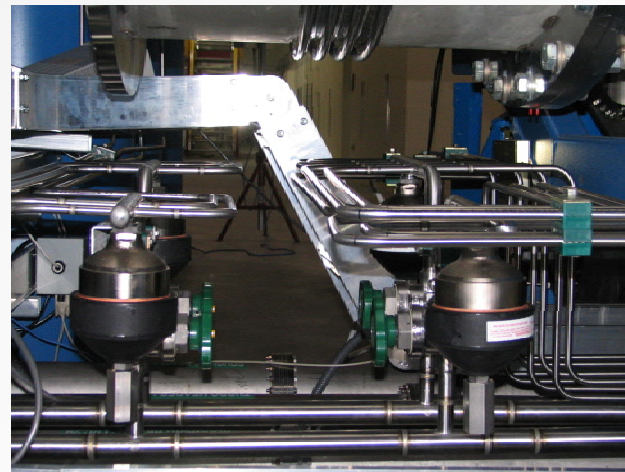
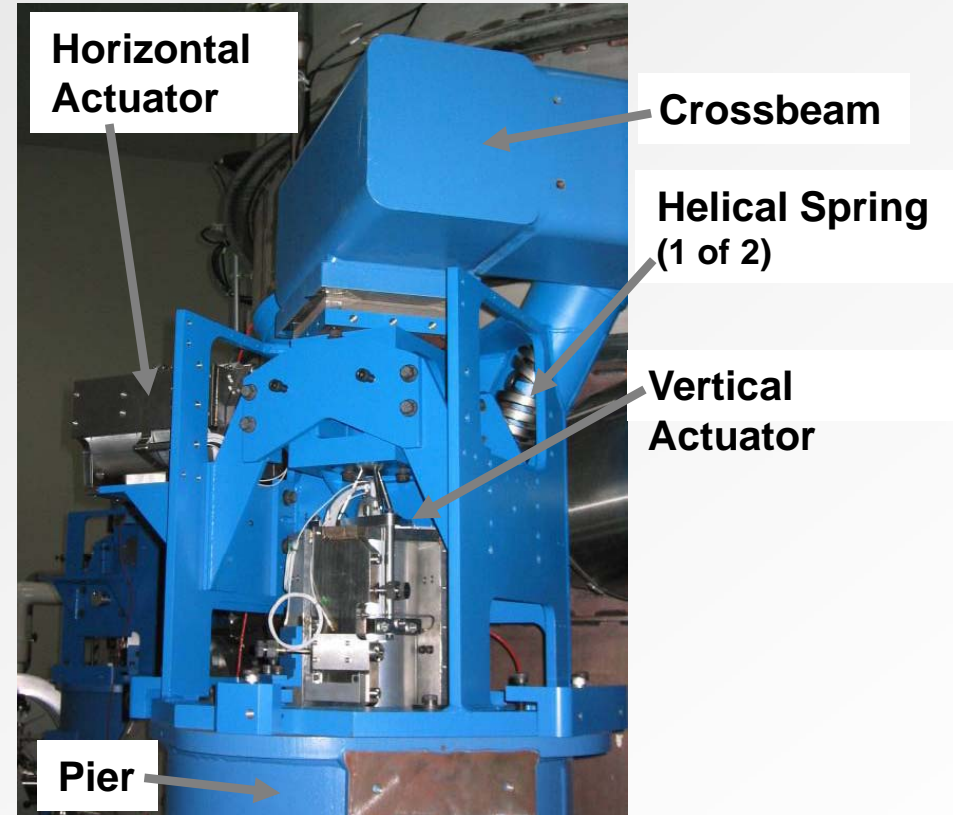
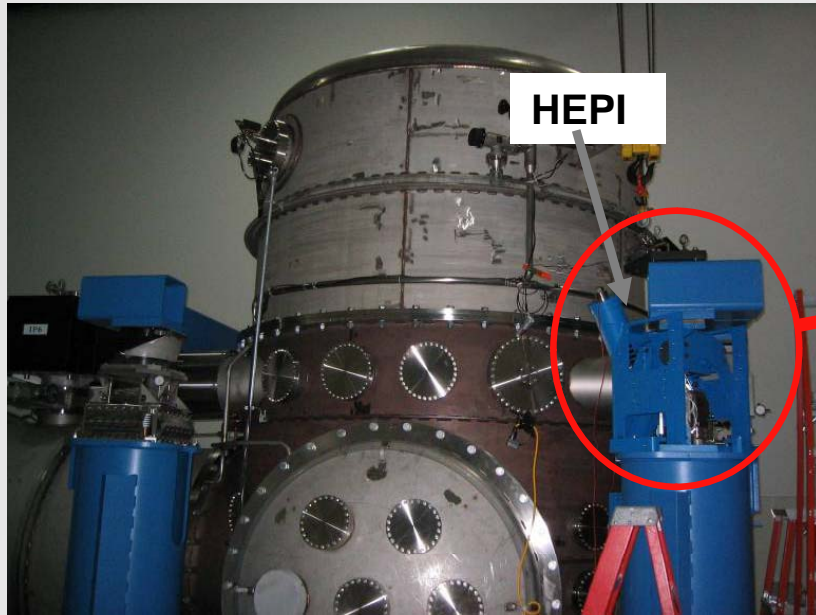
- Strain sensitivity: 10^{-21} rms in a 100 Hz bandwidth
- Instrument strain noise density: $3 \times 10^{-23} / \text{Hz}^{1/2}$ at 150 Hz
- Displacement Noise
 - Seismic motion
 - Thermal Noise
 - Radiation Pressure
- Sensing Noise
 - Photon Shot Noise
 - Residual Gas

stack of
mass-
springs



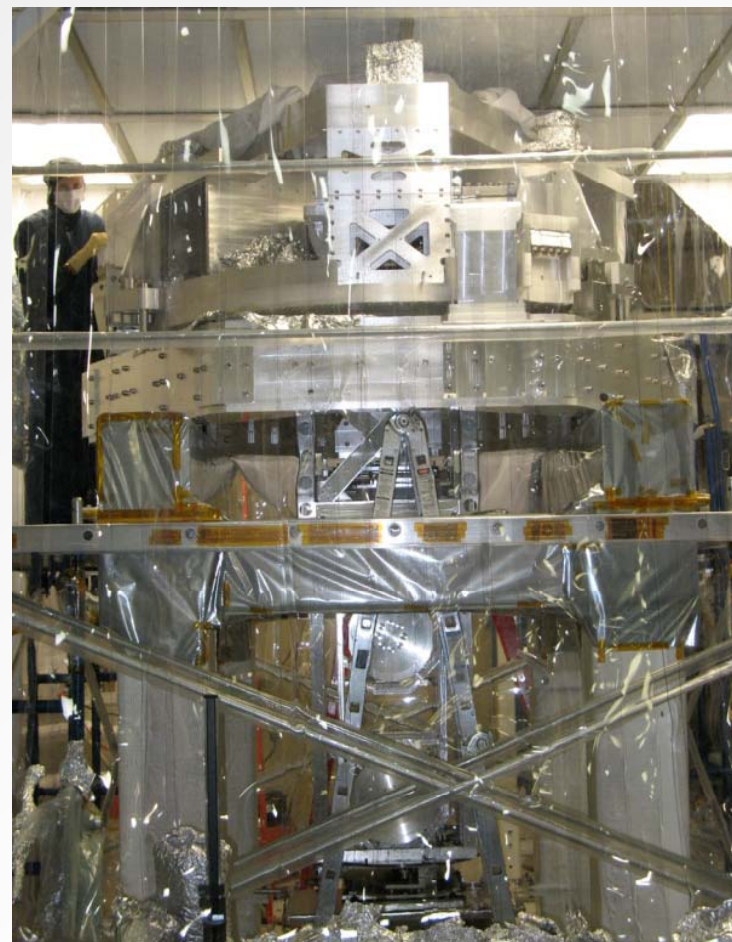
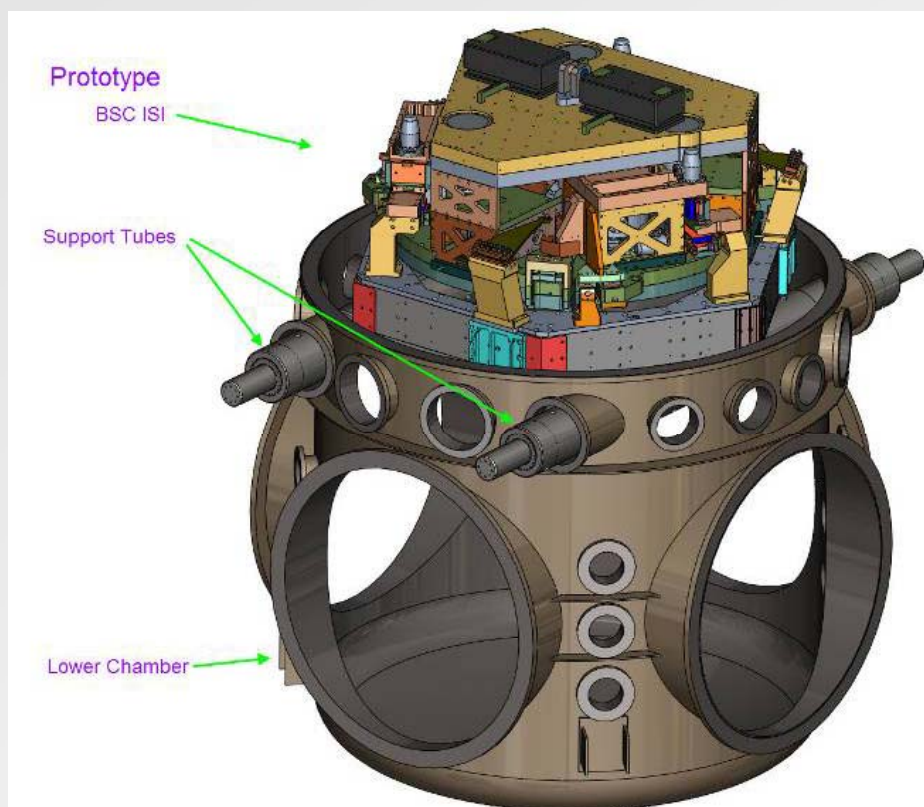


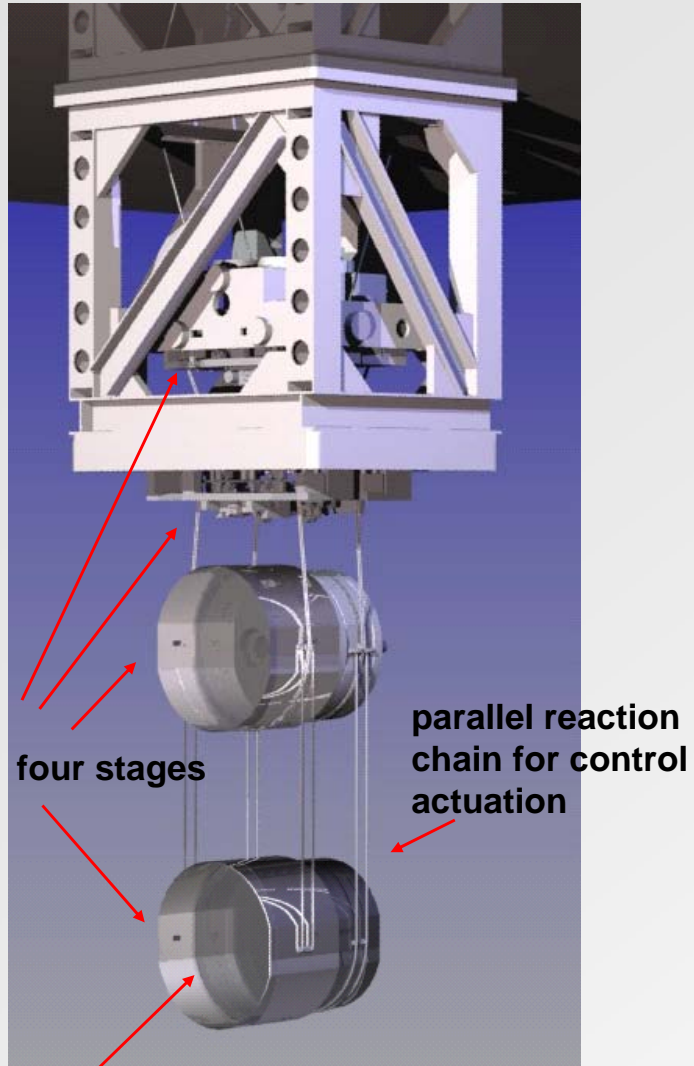
Seismic Isolation, HEPI Subsystem Installation at LIGO Livingston Observatory



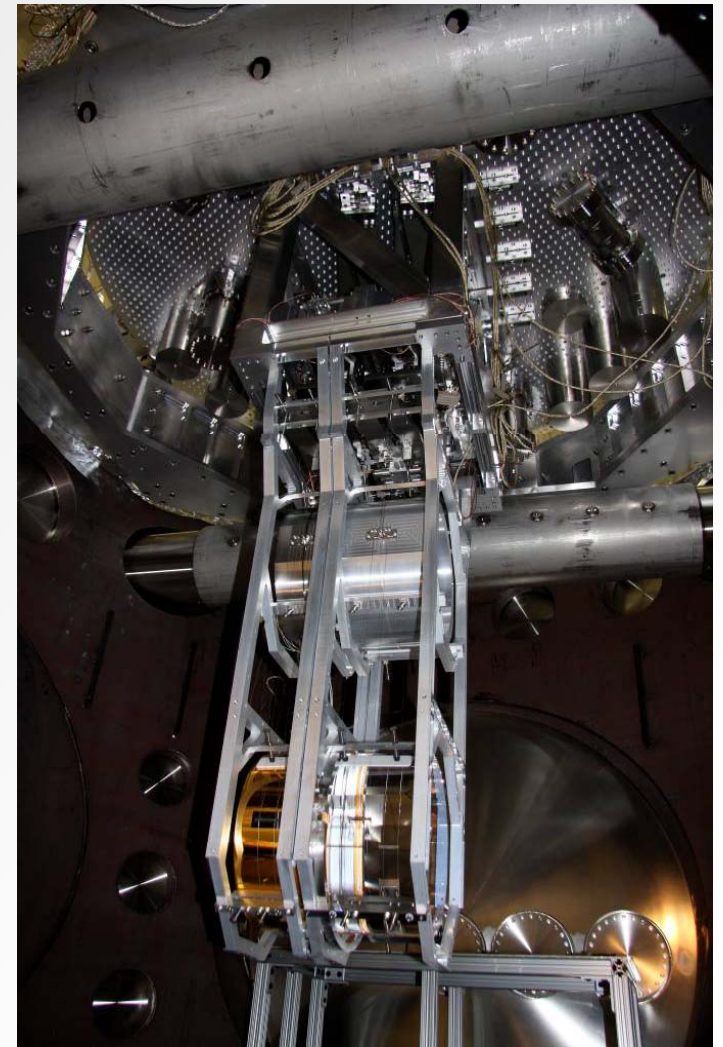
BSC Internal Seismic Isolation (BSC-ISI) system

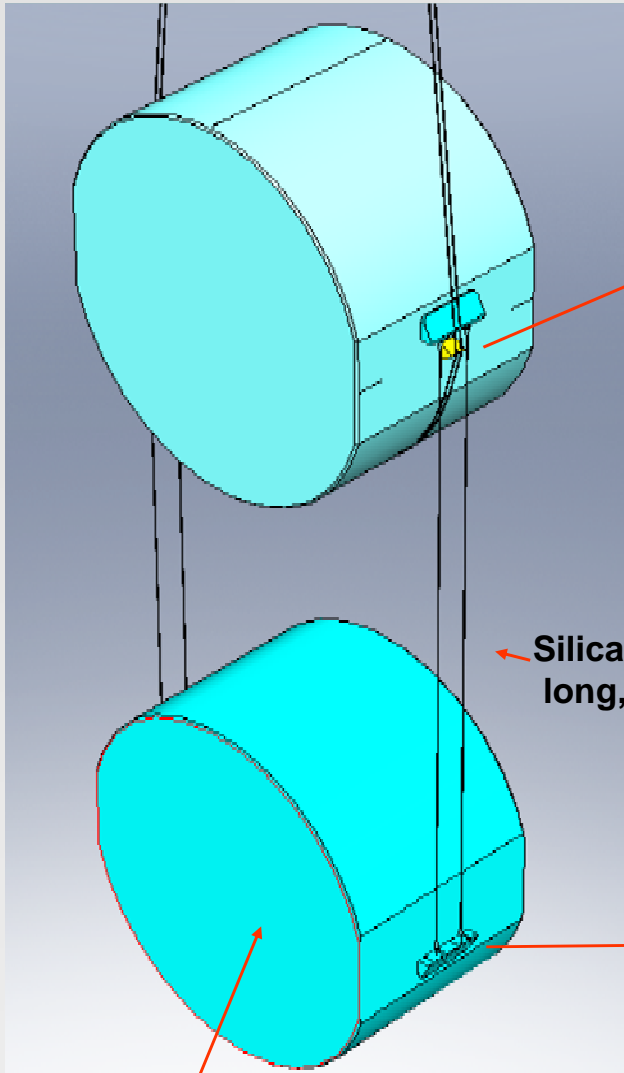
- ✓ A support structure (Stage 0) and Two suspended active stages (Stage 1 & 2).
- ✓ Will be installed for Advanced LIGO into the BSC chambers.
- ✓ A BSC-ISI system in each of the 15 BSC chambers.
- ✓ Optic table supports the test masses and beam splitters.





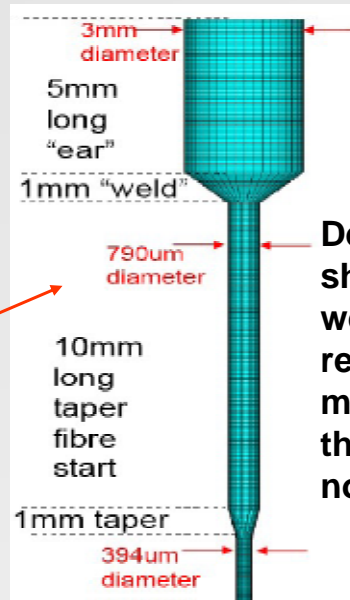
40 kg silica test mass



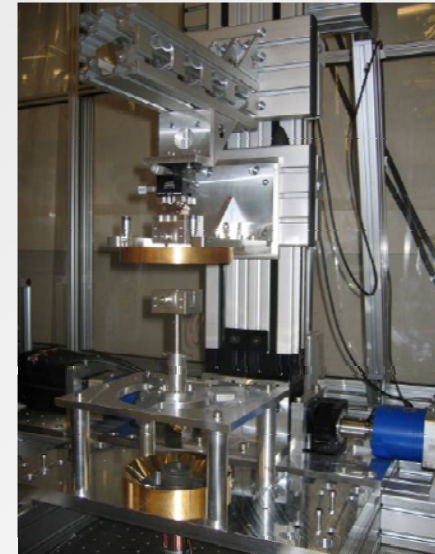


Mirror: 40 kg silica mass

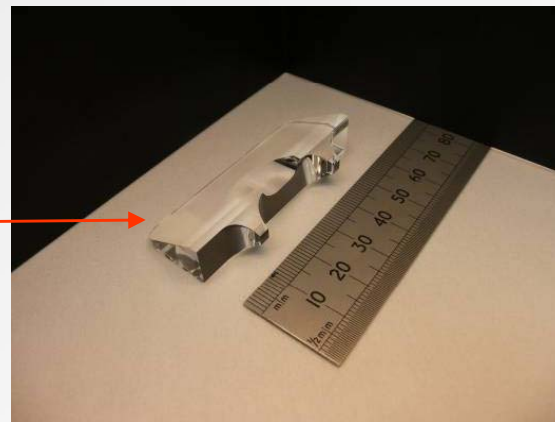
Silica fibres 600 mm long, 0.4 mm diam.



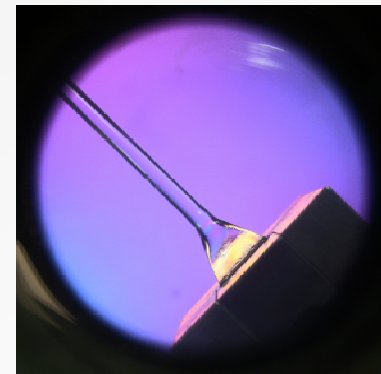
Detail of fibre shape close to weld: thick flexure region used to minimise thermoelastic noise



Fibre pulling machine at MIT



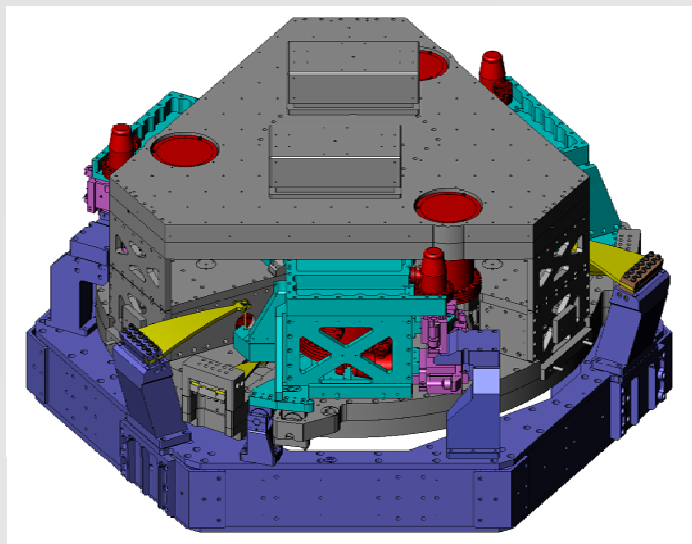
Example of ear to be bonded to silica mass



Visual inspection of test weld using crossed polarisers at Glasgow



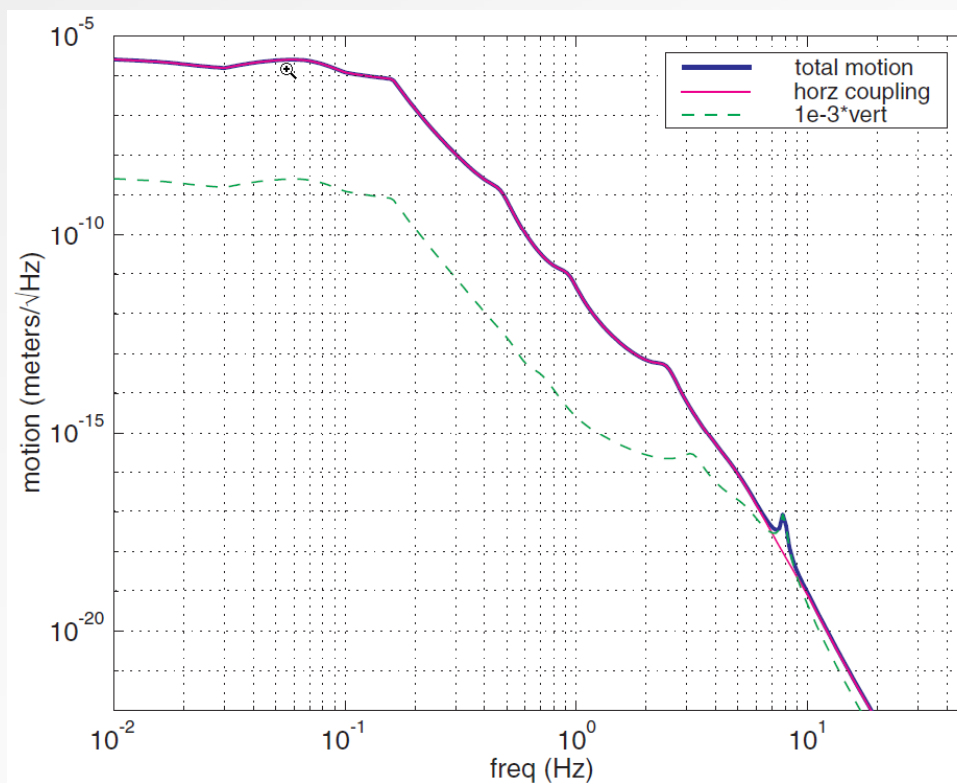
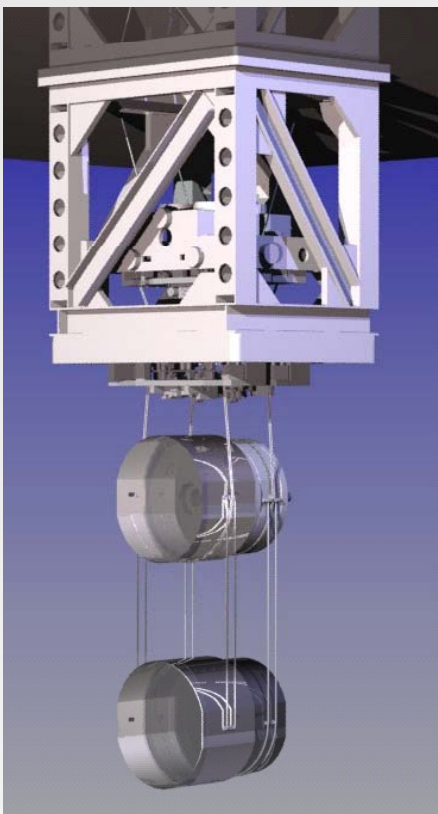
Welding test at Glasgow



Test mass suspension complements seismic isolation

All instruments using several pendulums in series for improved isolation, staging of control forces and dynamic range

Combined attenuation of seismic noise
~10 orders of magnitude at 10 Hz

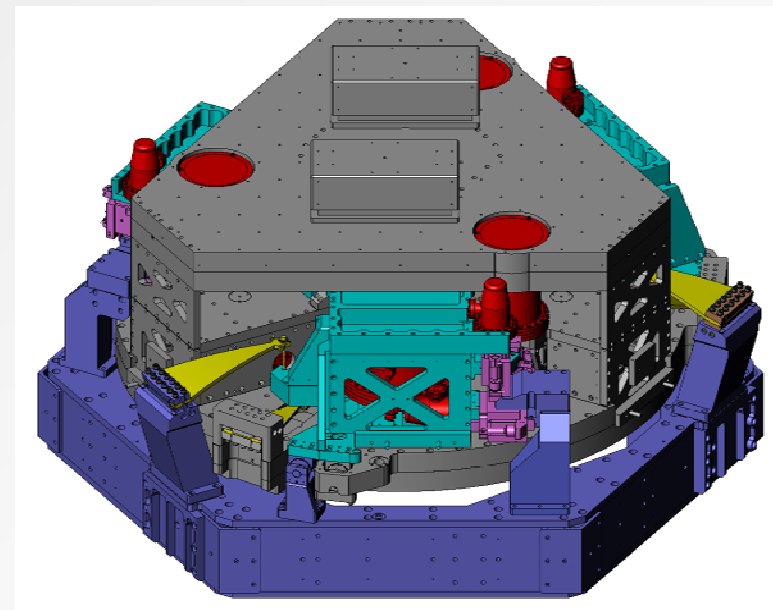


Both suspended stages and have 6 degrees of freedom:

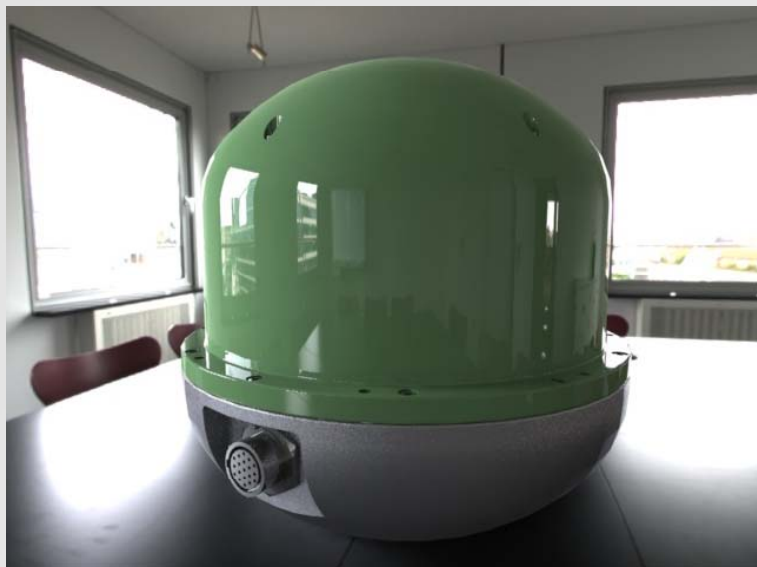
- ✓ Blades provide the vertical flexibility
- ✓ Rods provide the horizontal one
- ✓ Suspension frequencies in the 1Hz-7Hz range
- ✓ Passive isolation from few Hz to ~ 100Hz
- ✓ Active isolation in the 0.1Hz-20Hz range.
- ✓ Active control positioning



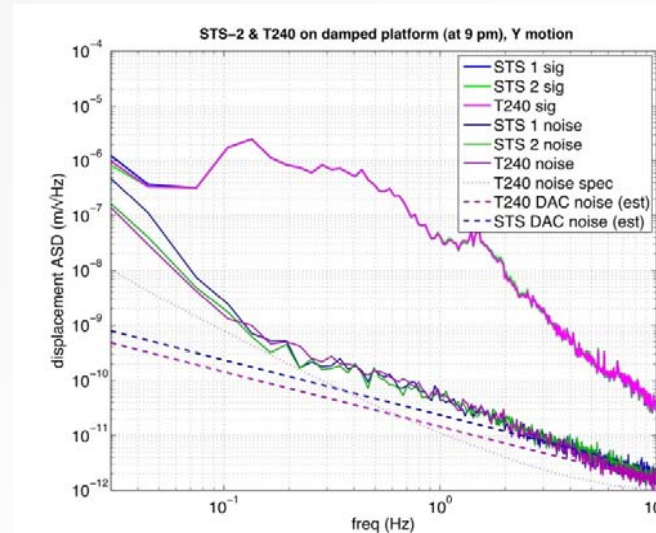
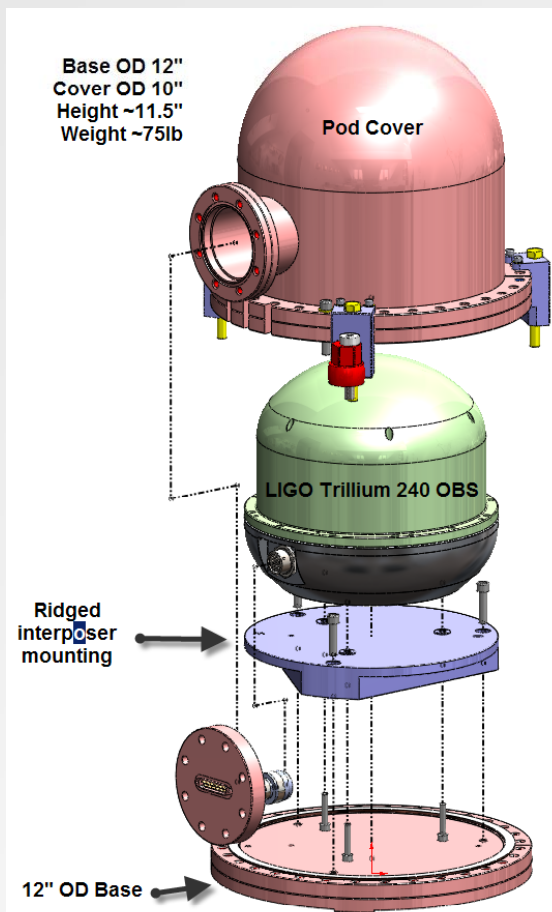
BSC-ISI as built for the prototype installed at MIT

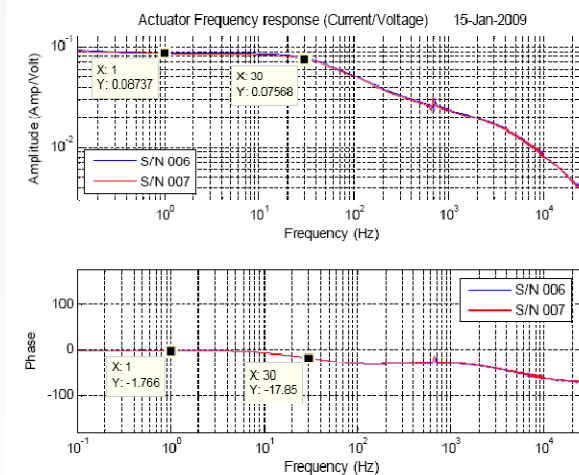
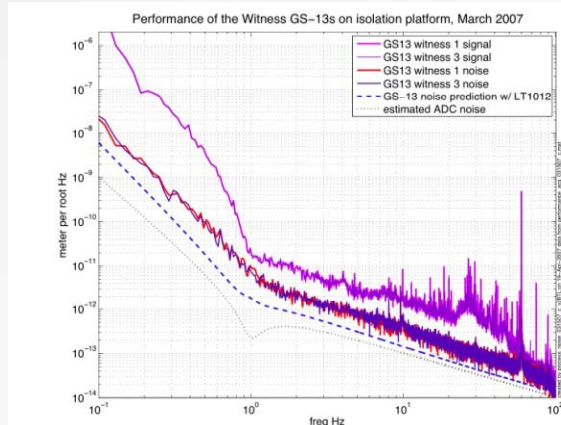
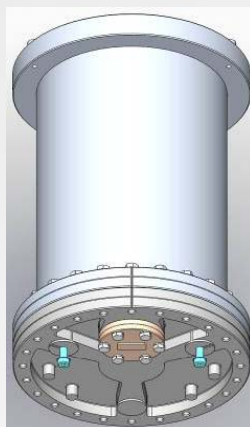
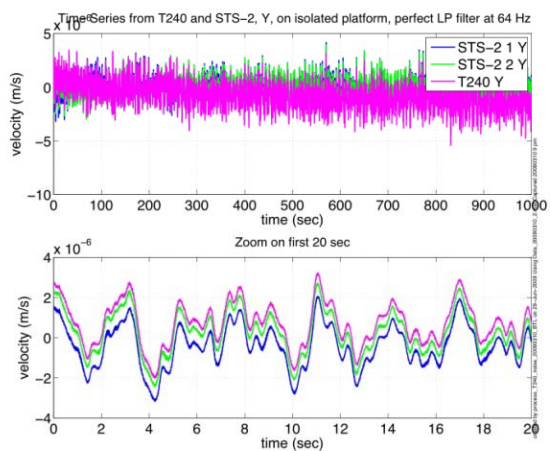
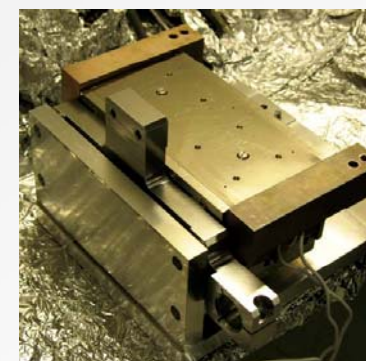
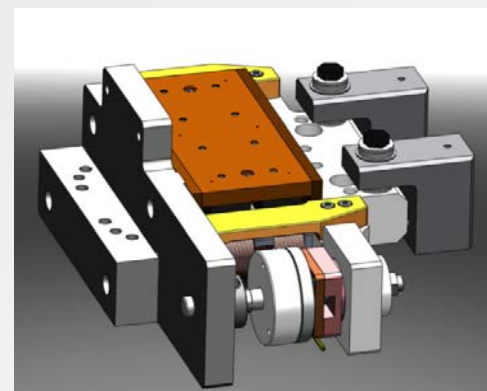
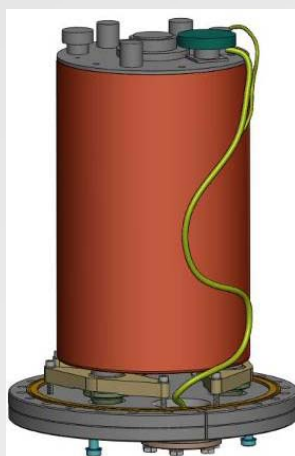


- Stage 0 in violet
- Stage 1 in cyan
- Stage 2 in grey
- Blades and flexure in yellow
- Sensors in Red
- Actuators in Pink



Trillium Diameter: 9.5 in
 Height: 8.9 in
 Weight: 21 lb
 (No Locker needed)



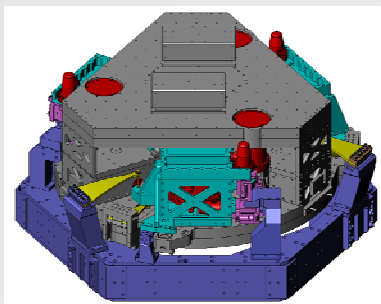


1- Cahier des charges

LIGO Design Requirements Summary Structure

Paragraph	Parameter	SR Requirements	Units	Status
C.1	Material	Major structural elements shall be made from aluminum	N/A	Comply
K.1	Prototype Mass	8200 lbs (370 kg)	lb mass	Comply
K.2	Payload Mass Total	1764 lbs	lb mass	Comply
K.3	Center of Gravity (Stage 1)	The CG of Stage 1 shall be within 1.25" vertically with respect to the horizontal actuator plane at the stage cut	inches	Comply
K.4	Center of Gravity (Stage 2)	The CG of combined stage 2 and the non-suspension portion of the payload for each of the support tubes	inches	Comply
C.2	Interface	Hardly 1000 holes on each of four support tubes (200x100)	319 - 24 UNF	Comply
C.4	Shakeout	Hardware mounted to the support tubes shall not protrude more than 1.5" beyond the raised interface bosses	inches	Comply
C.5	Critical Clearance	Minimum clearance of 0.5" between assembly and interface; minimum inter-stage clearance of 2.2"	inches	Comply
G.1	Optical Table Configuration	Optical table with a 1920x1920 mm	inches	Comply
G.2	Optical Table Location	The laser tables ensuring guiding total for 14.5" above the BSC chamber support tubes	inches	Comply
C.5	System Mobility	Assembly shall include means for lifting with a crane hook, since its center of gravity, with the dimensions from the position of the axis of the support tube to the center of the hook pin shall not be greater than 25.0"	inches	Comply

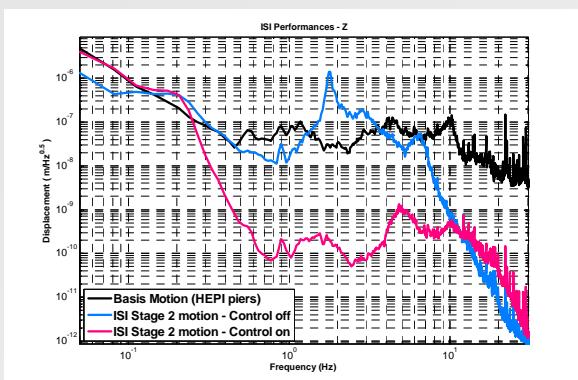
2- Conception



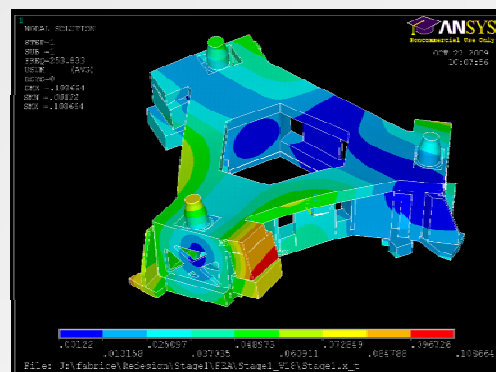
3- Prototypage



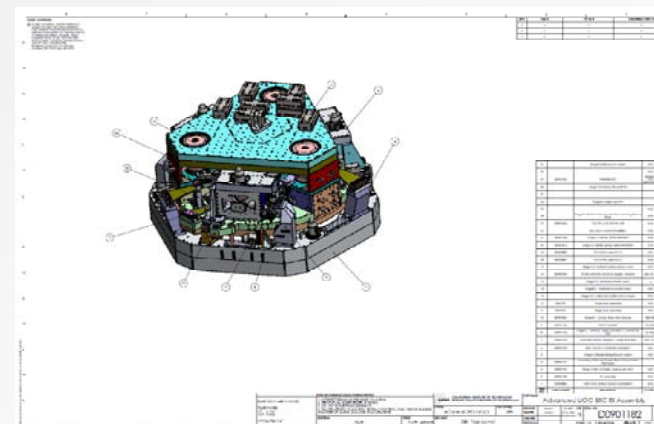
4- Test



5- Developpement



6- Fabrication en serie



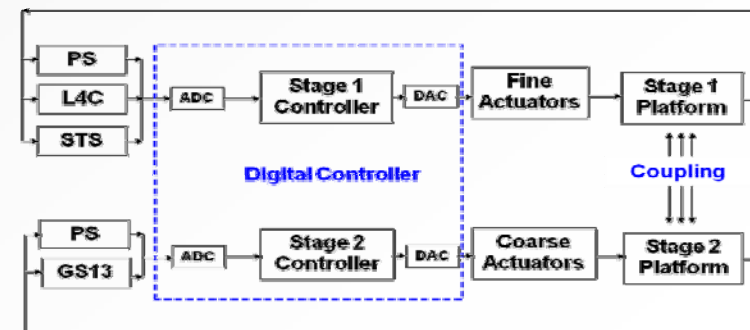
7- Assemblage

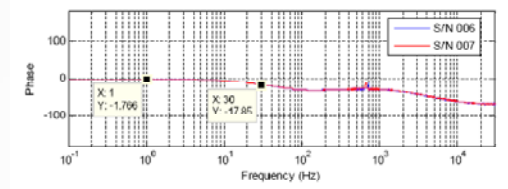
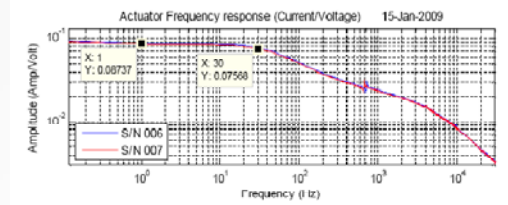
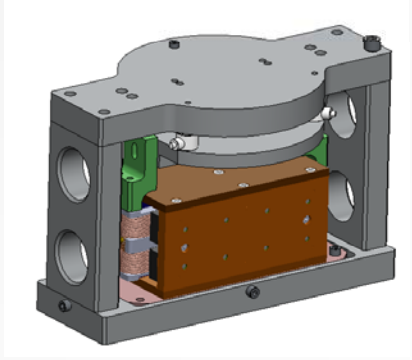
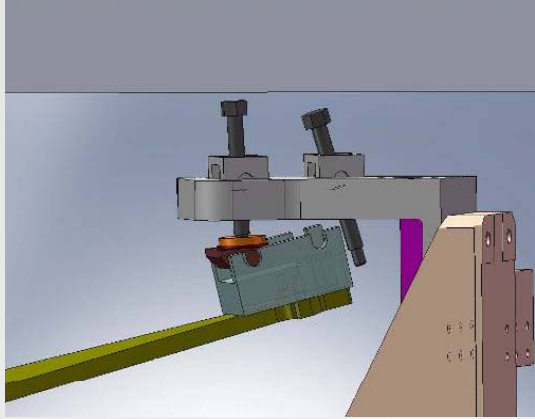
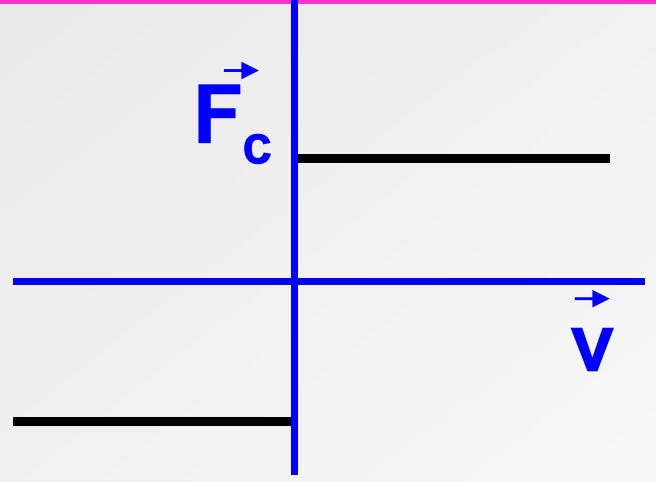
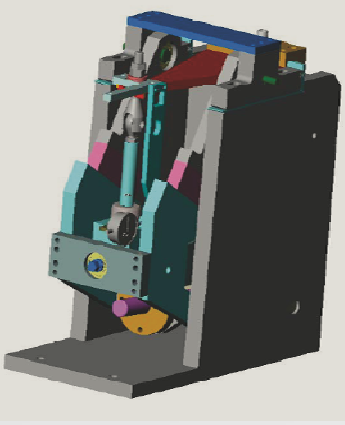


8- Installation

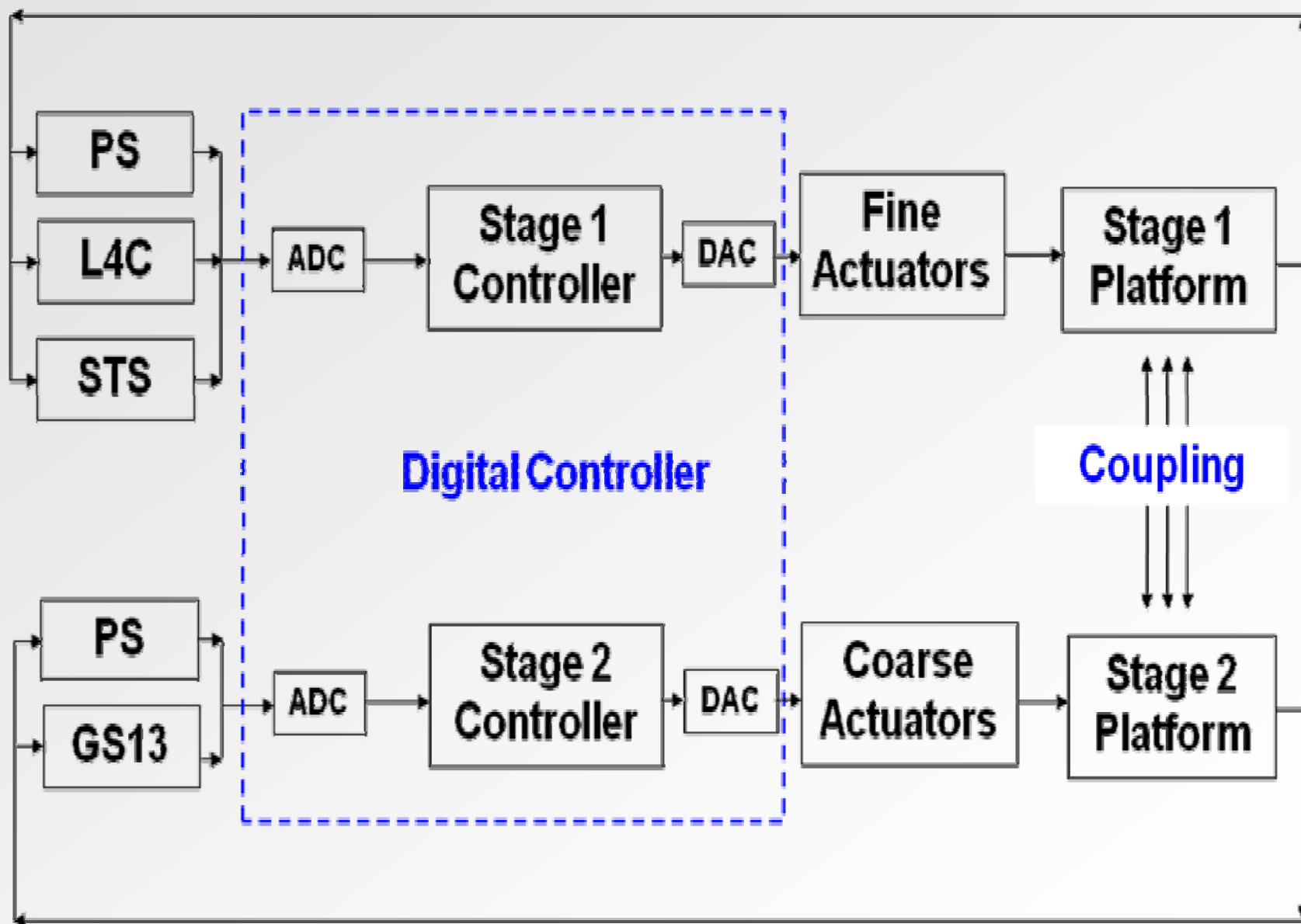


9- Mise en service

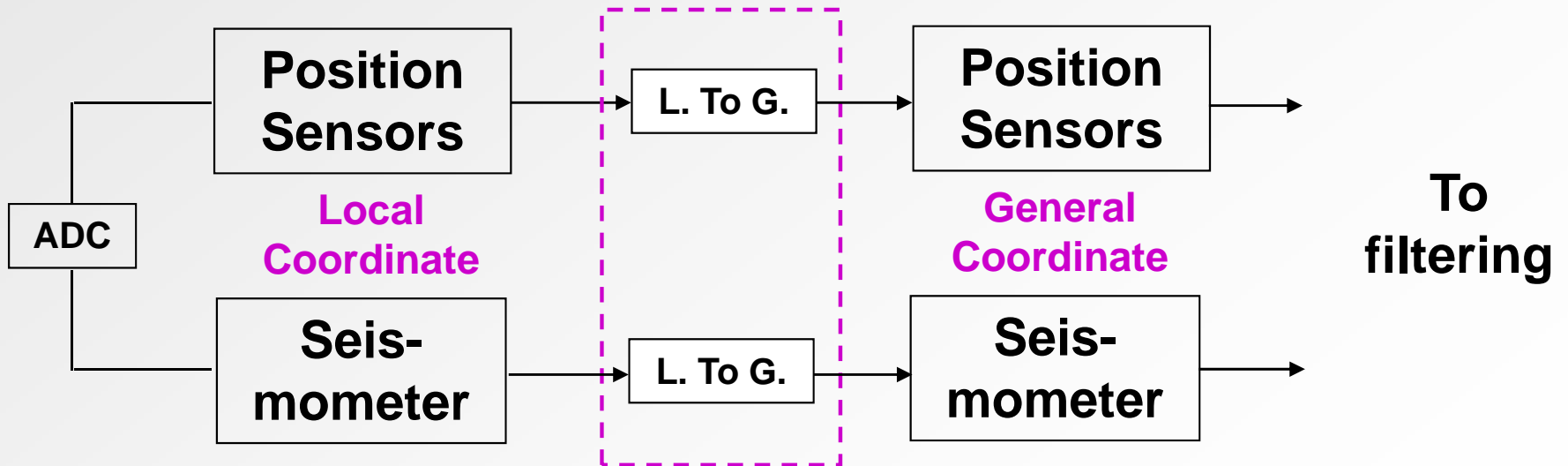
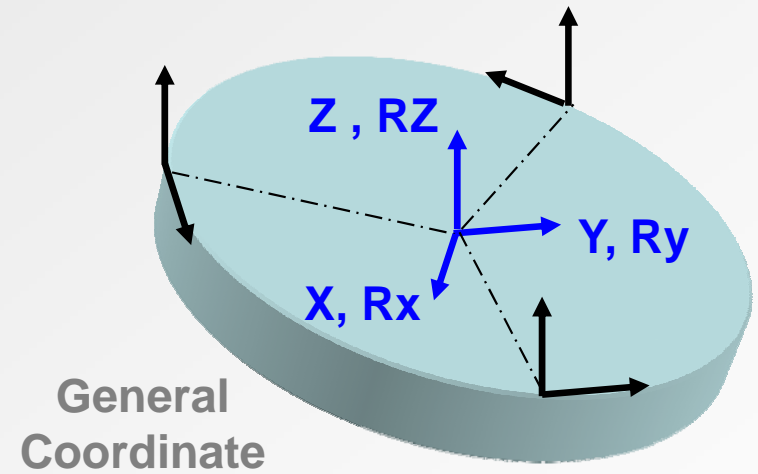
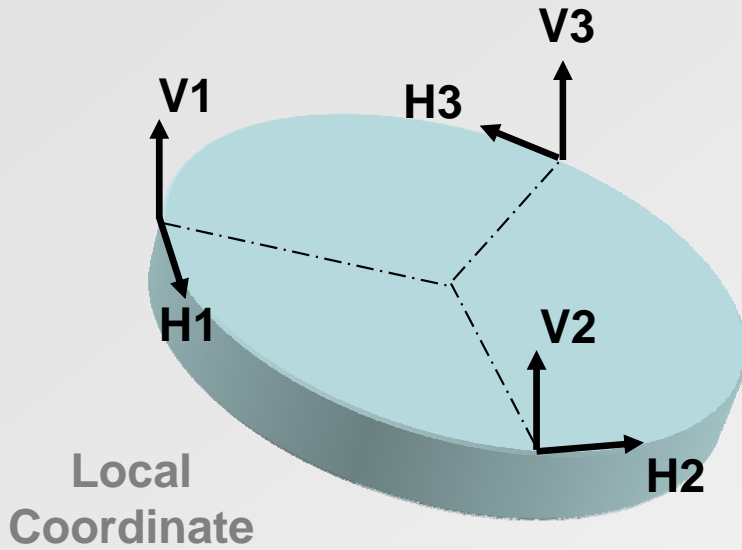




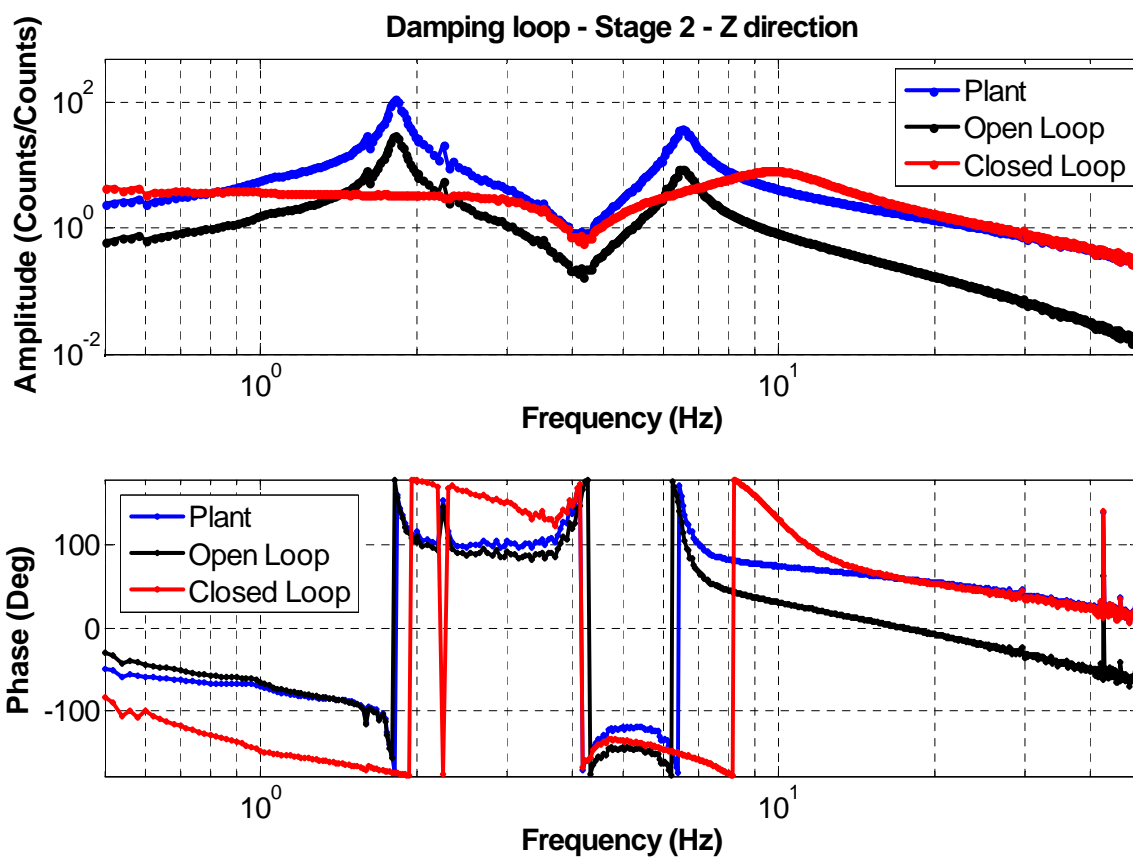
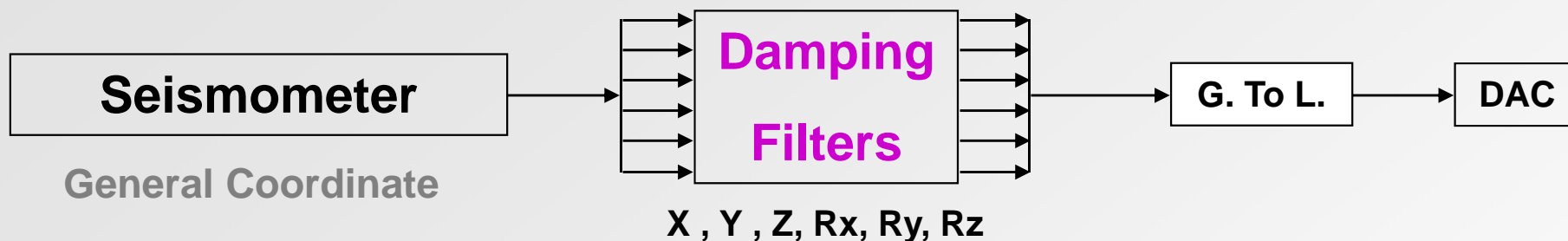
Control Strategy



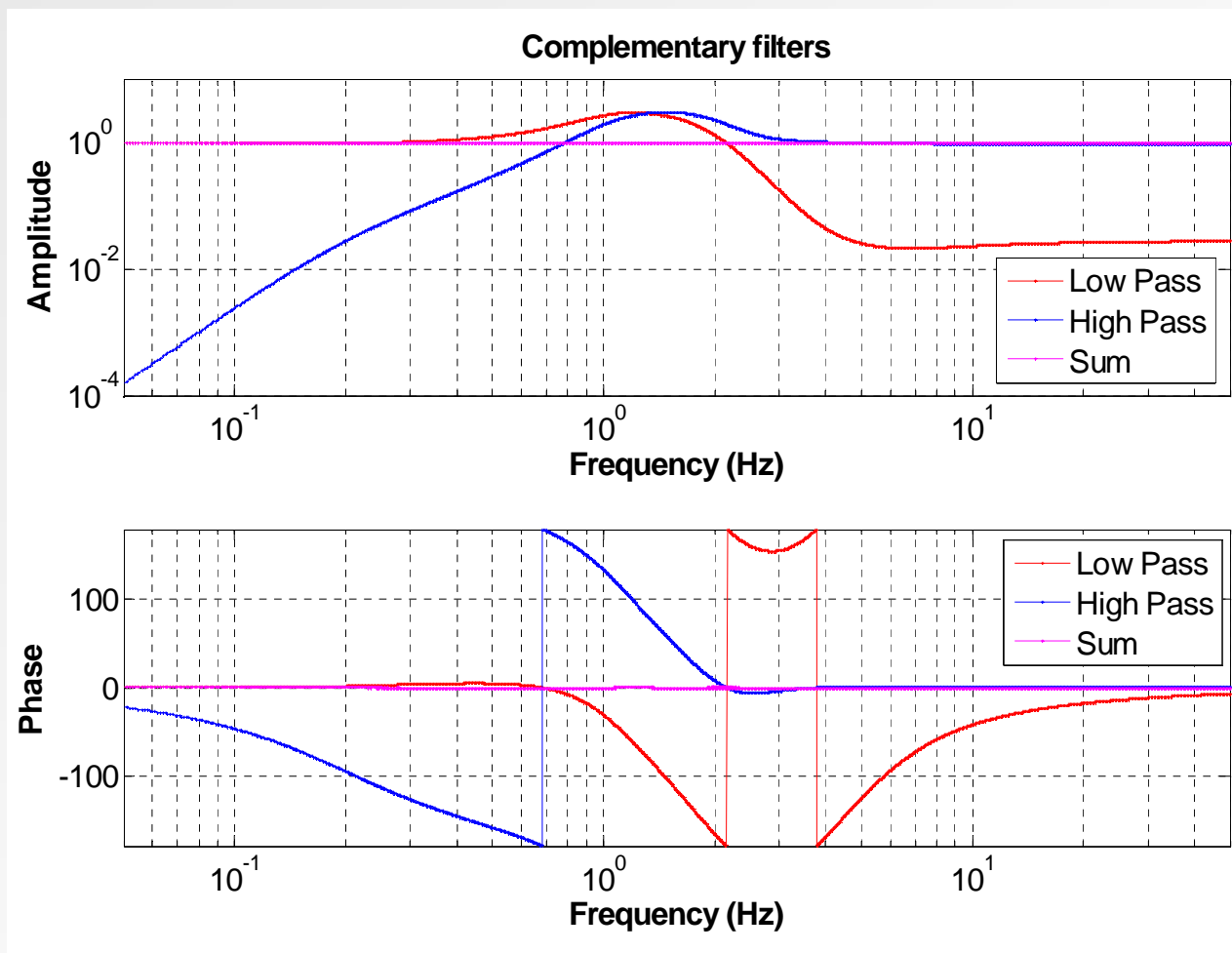
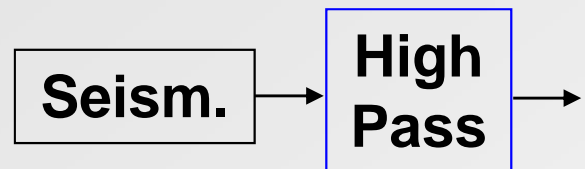
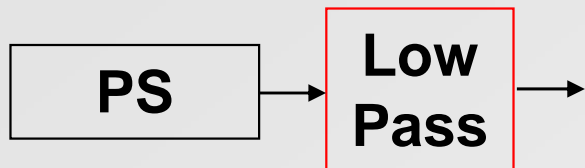
1st Step: Local to General coordinates



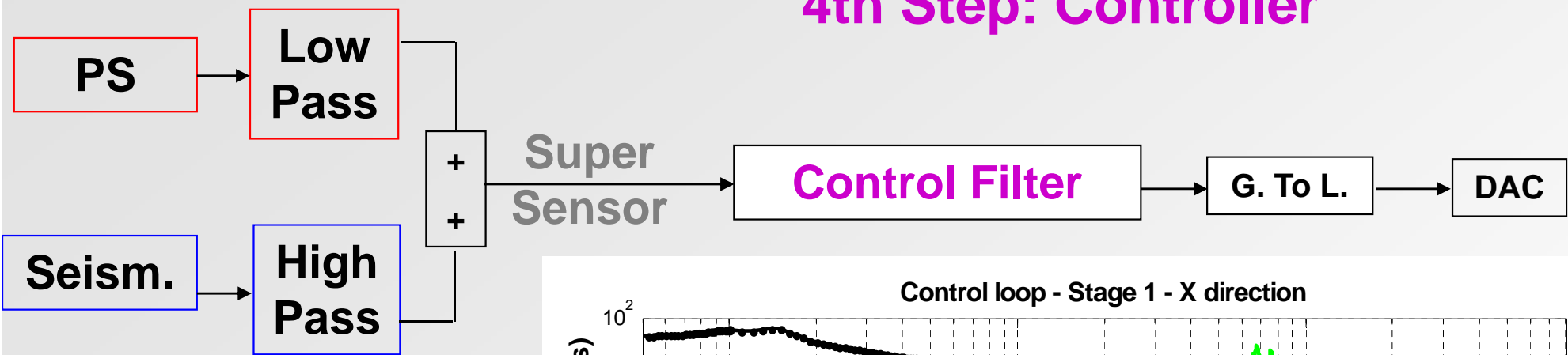
2nd Step: Damping loops



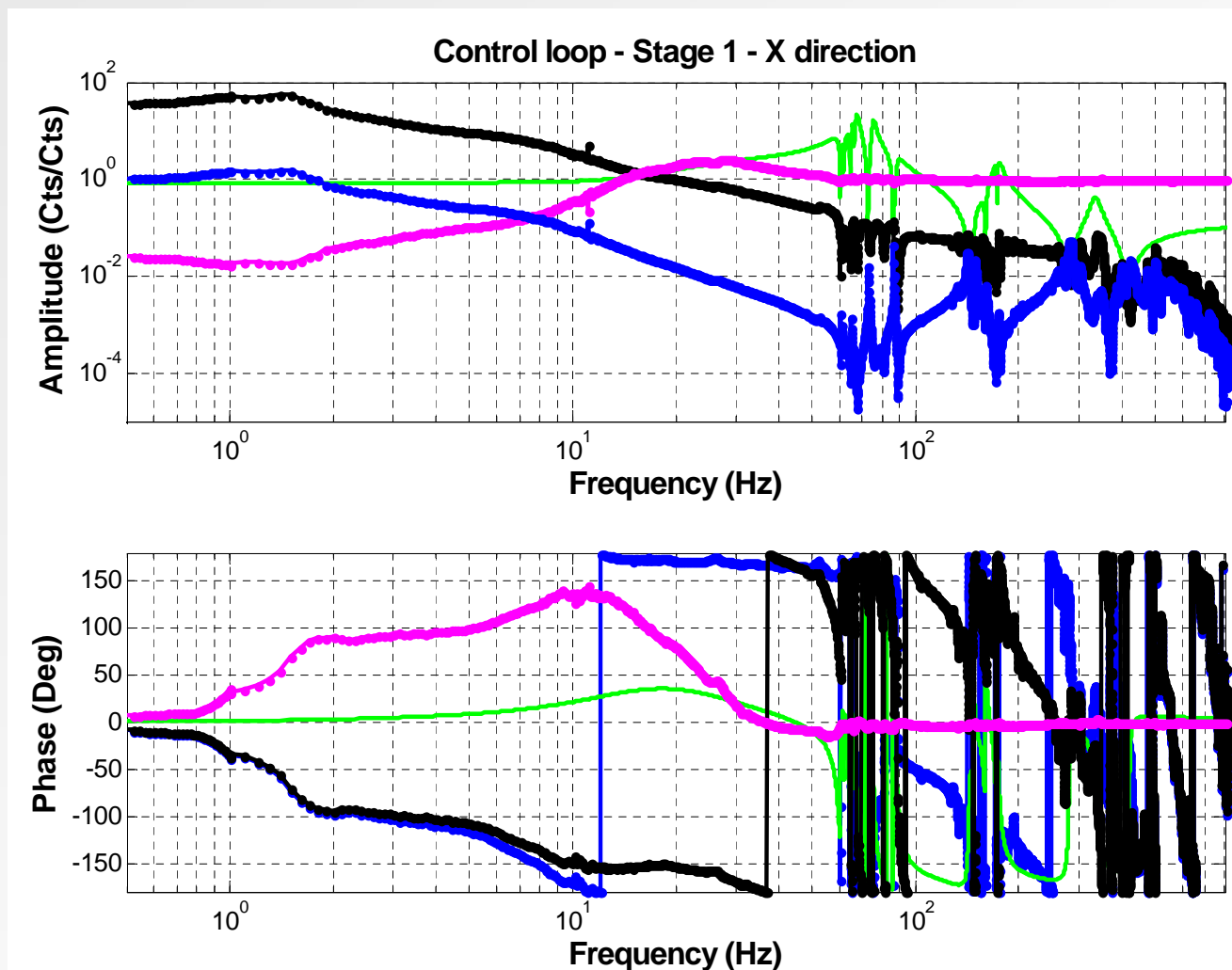
3rd step: Sensor Blend



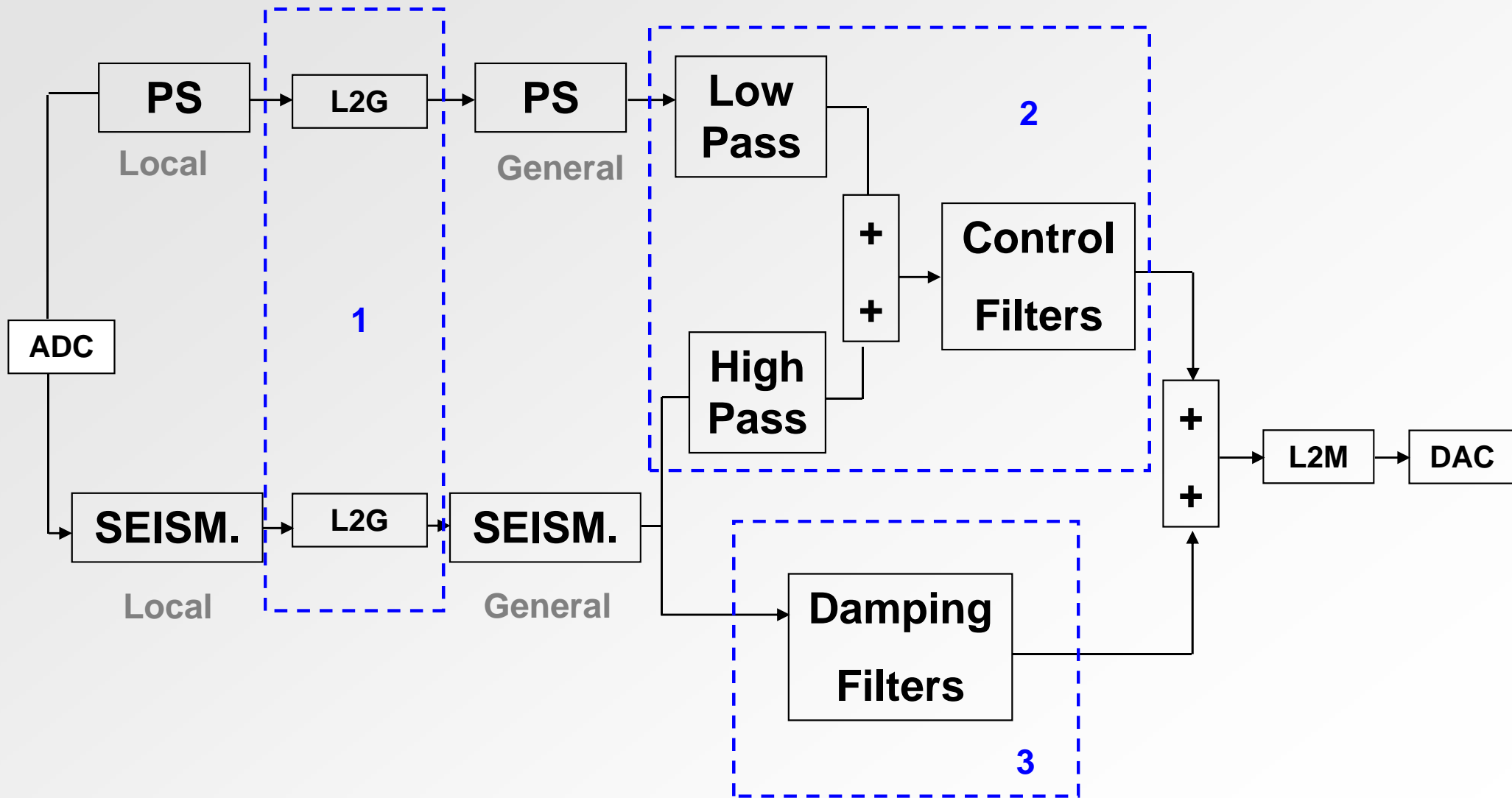
4th Step: Controller



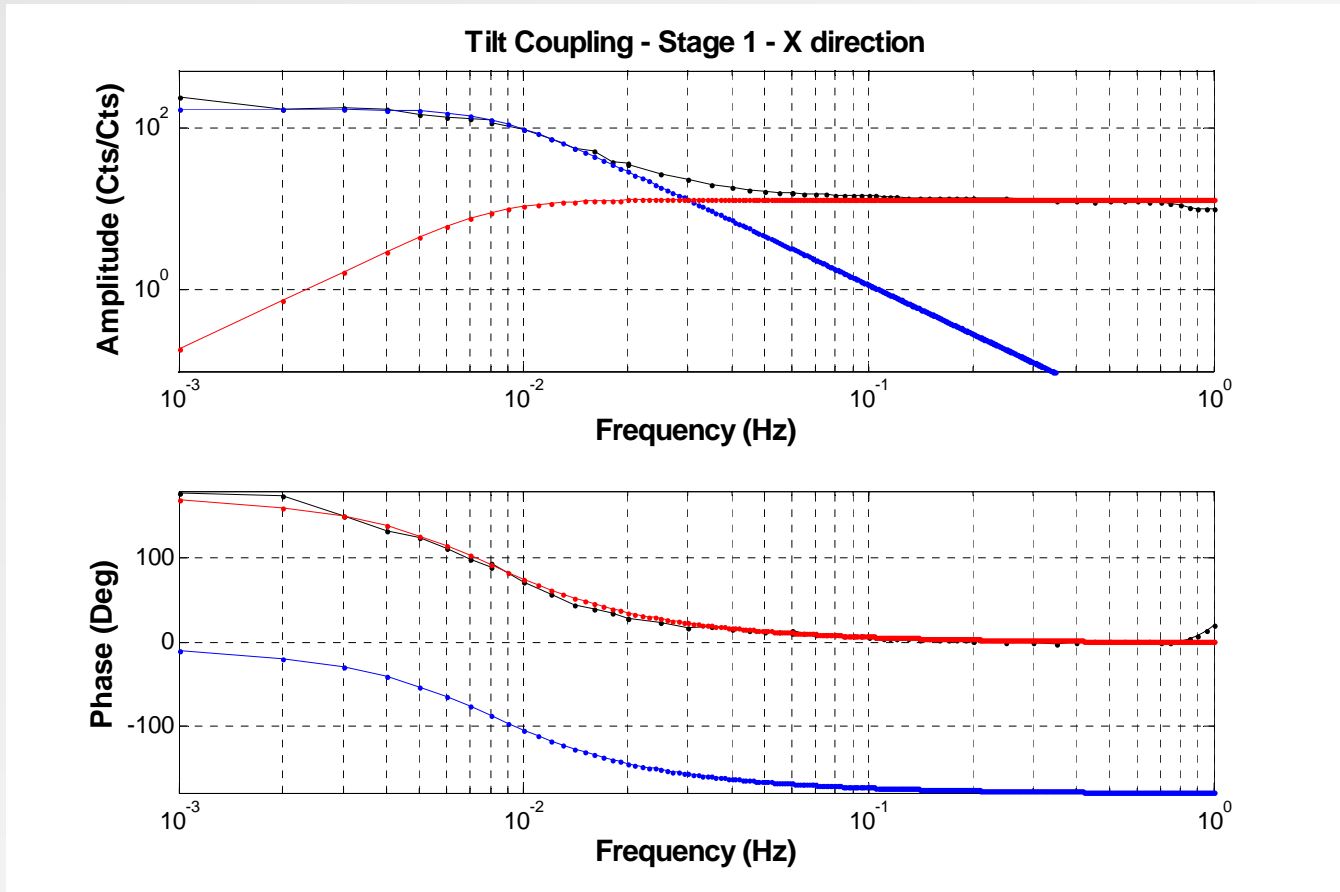
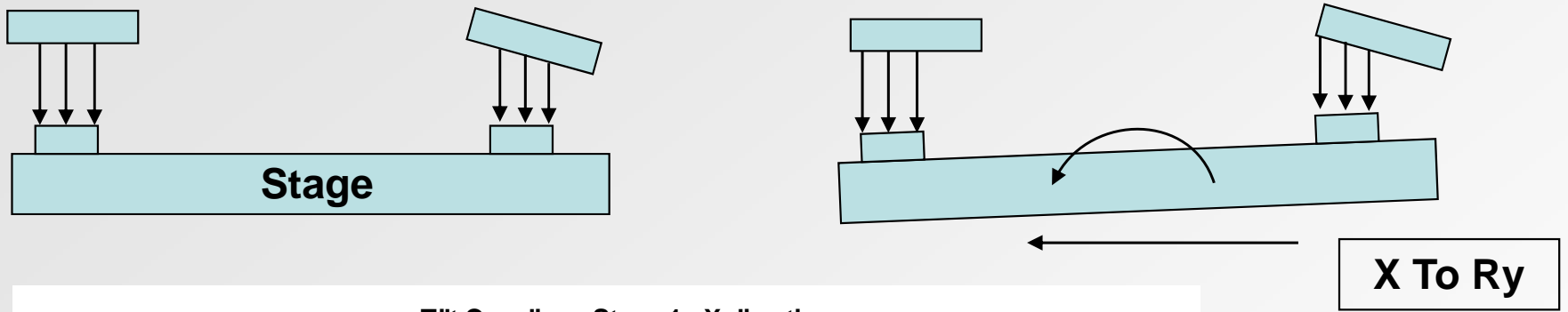
- Plant
- Compensator
- Open Loop
- Isolation



Control Strategy for each degree of freedom:

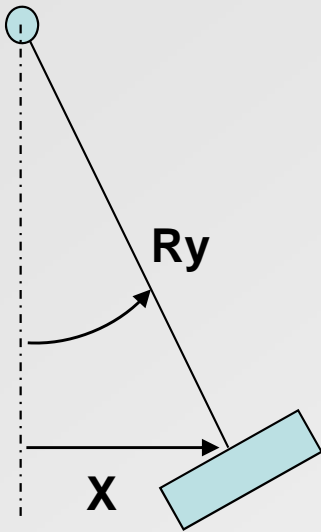


5th Step: Tilt decoupling



5th Step: Tilt decoupling

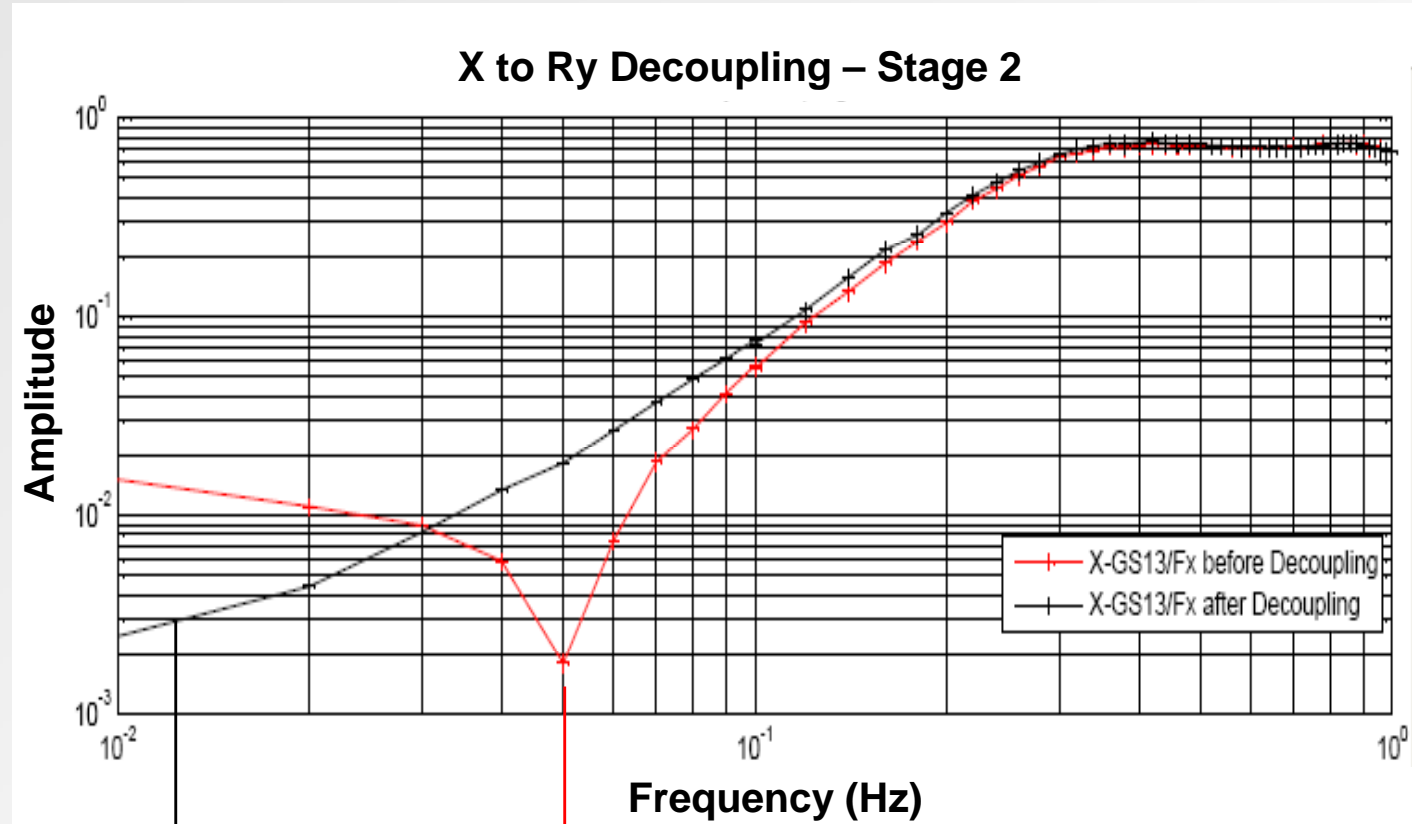
$$\frac{Ry}{X} \text{ (Rad / m)}$$



$$L = \frac{X}{Ry} \text{ (m / Rad)}$$

$$\omega_0 = \omega_{\text{tilt}} = \sqrt{\frac{g}{L}} \text{ (Rad / s)}$$

Tilt decoupling Matrix

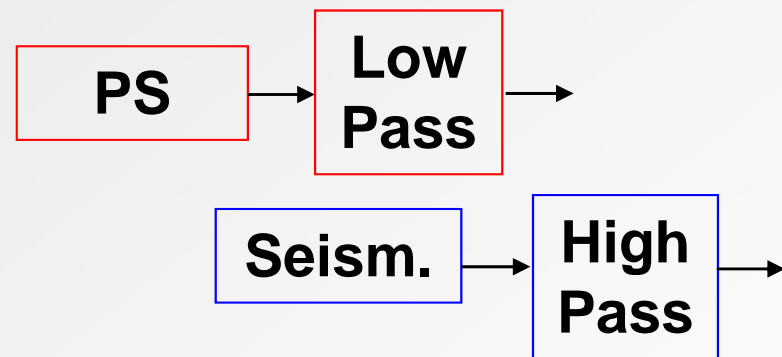
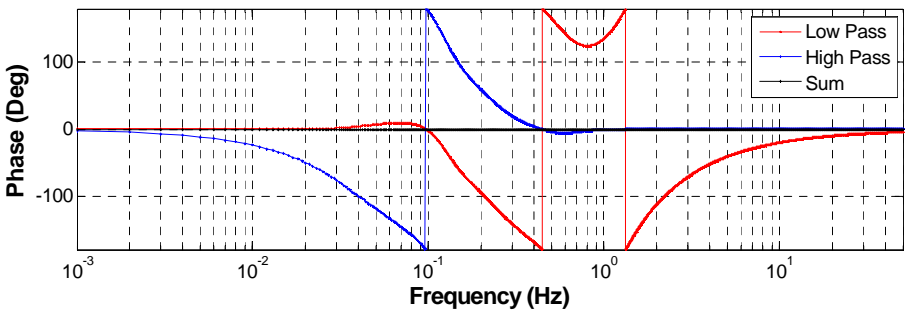
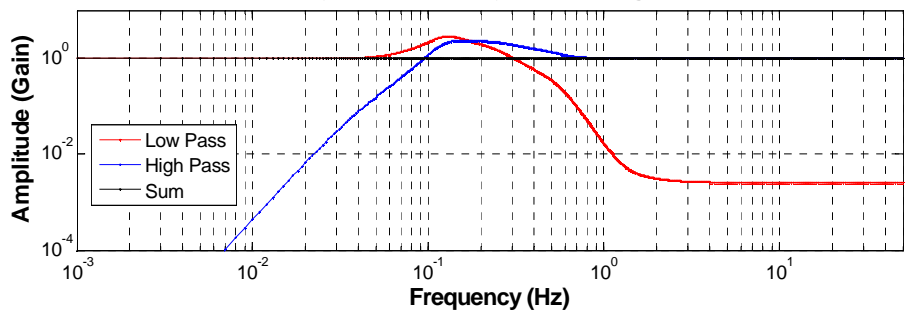


$$\omega_0 = \omega_{\text{tilt}} = 50 \text{ mHz}$$

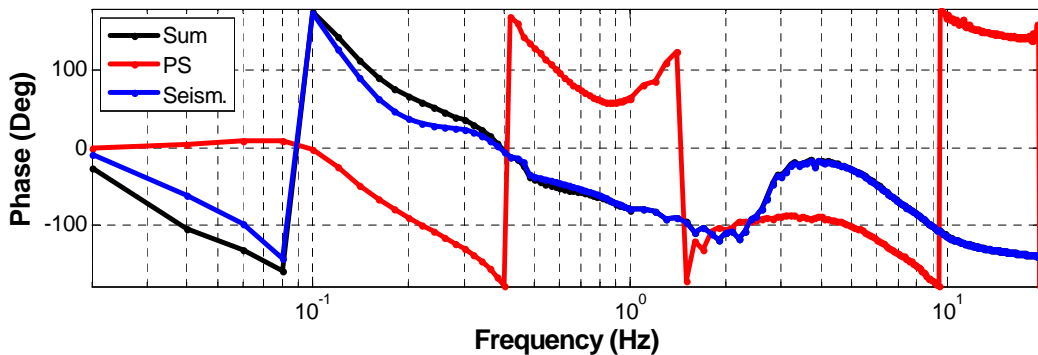
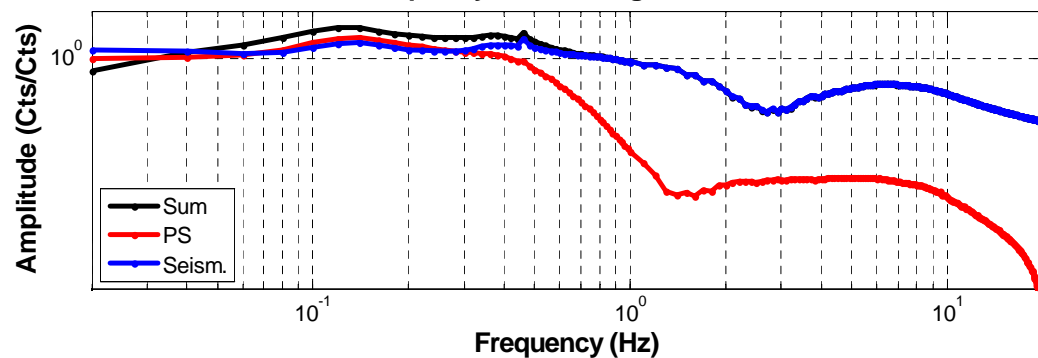
$$\omega_0 = \omega_{\text{tilt}} \approx 10 \text{ mHz}$$

6th Step: Low-Frequency Blend

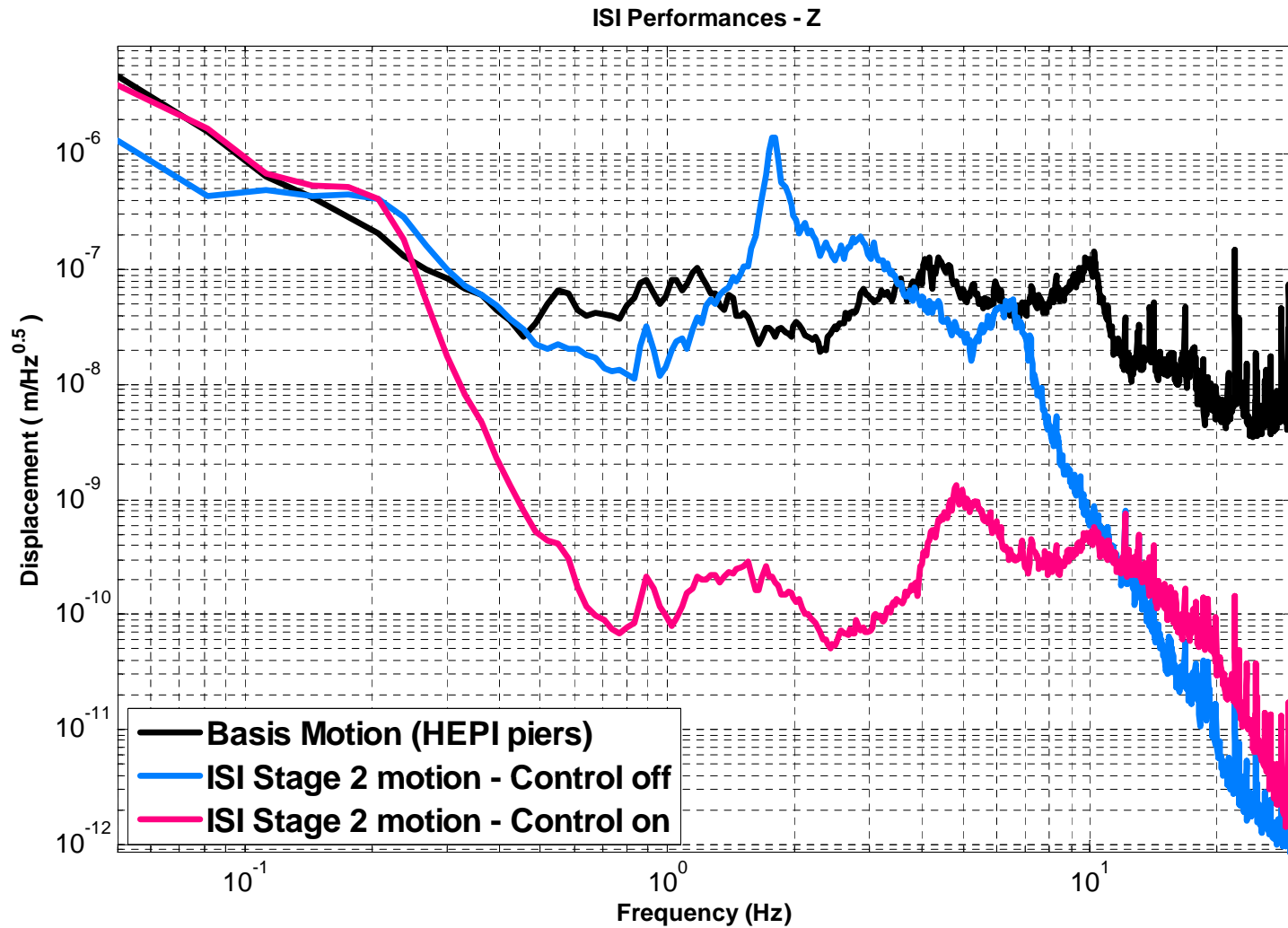
Low Frequency Complementary Filters - Stage 2 - X direction



Low Frequency Blend - Stage 2 - X direction

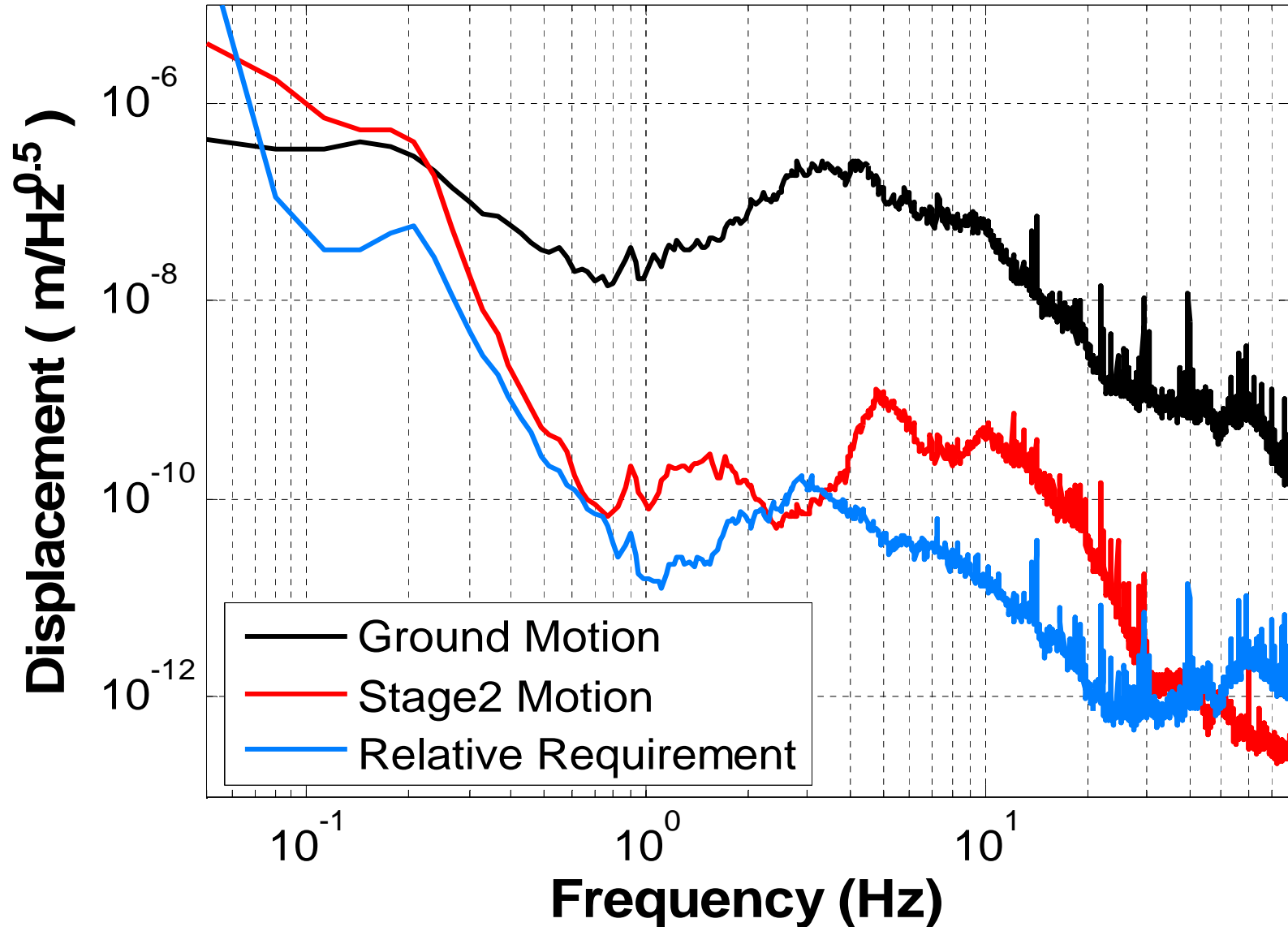


ISI System Performance



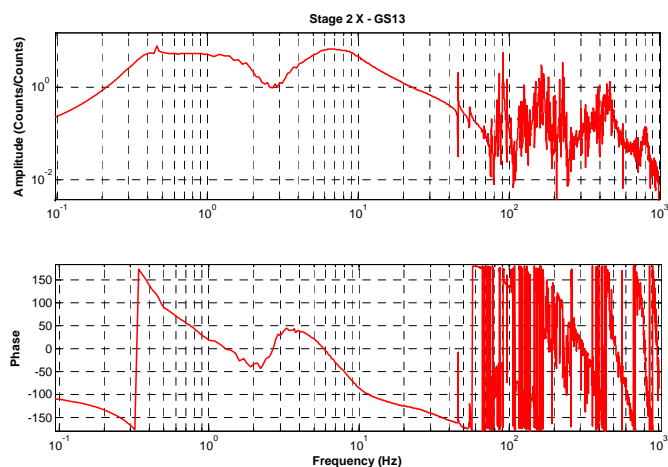
BSC Global Performance

BSC-ISI Performances - Z

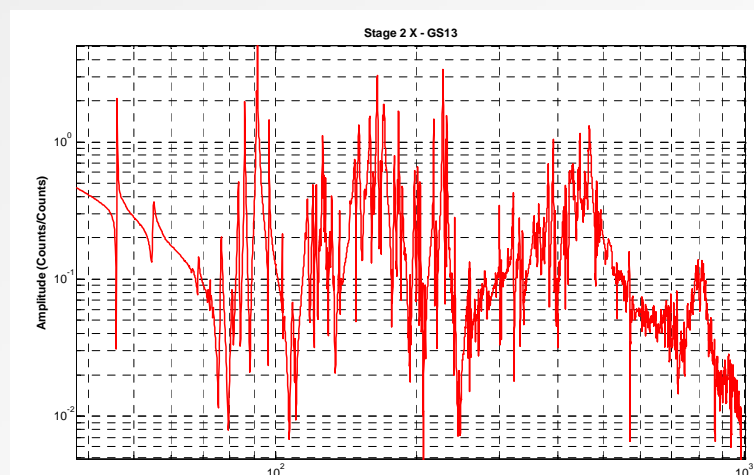


Three major problems identified:

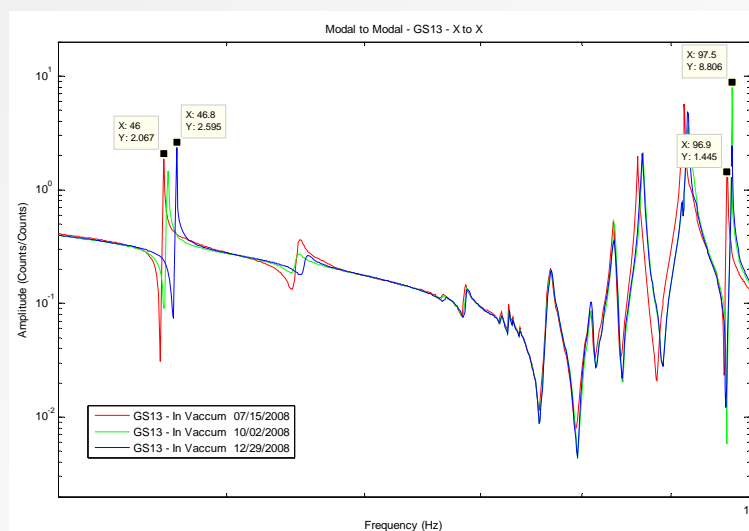
- ✓ The first deformation resonances were much lower in frequencies than required.
- ✓ The modal density at high frequencies was higher than expected.
- ✓ The plant was variant in time.



Low frequency modes

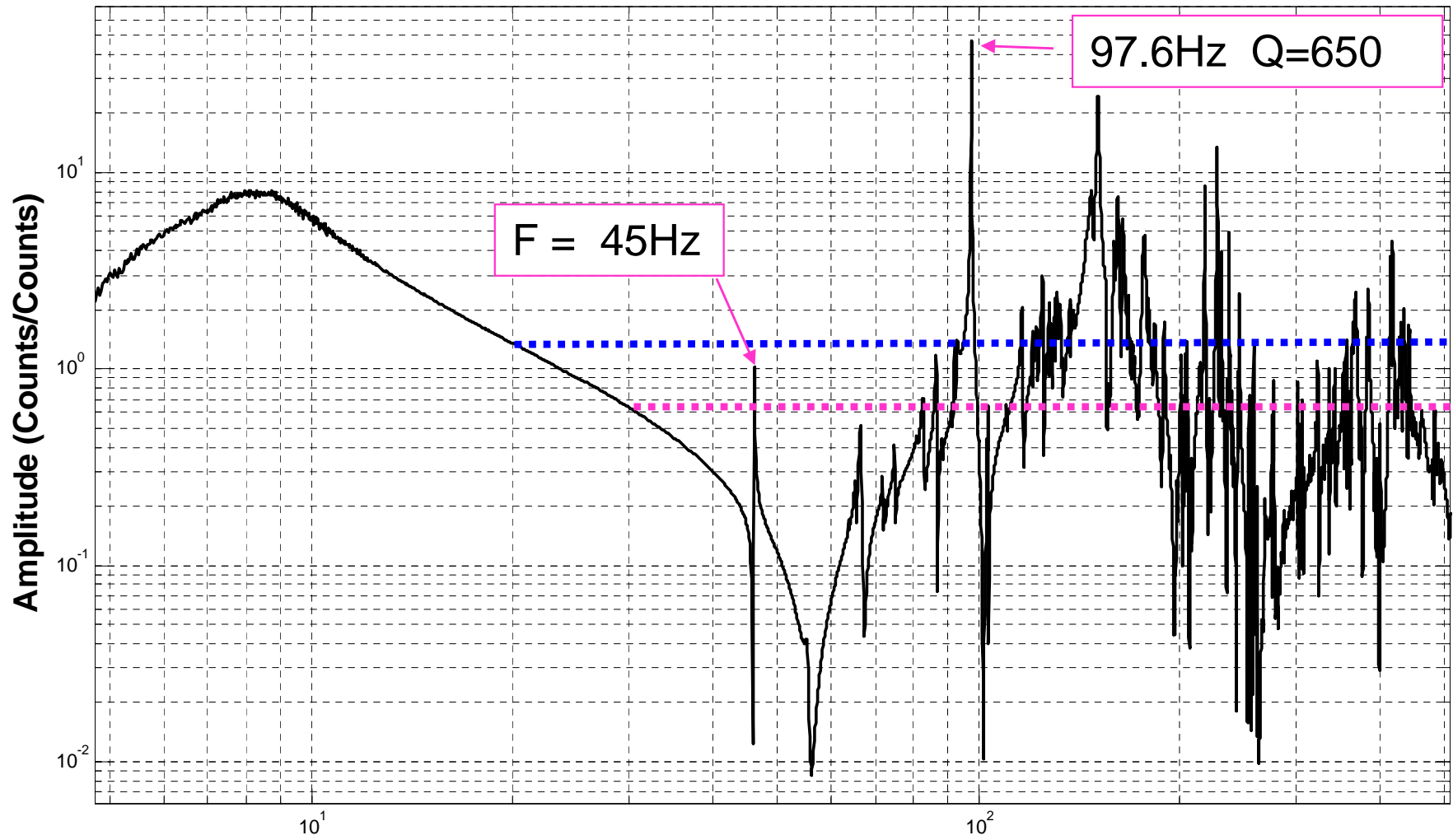


High modal density

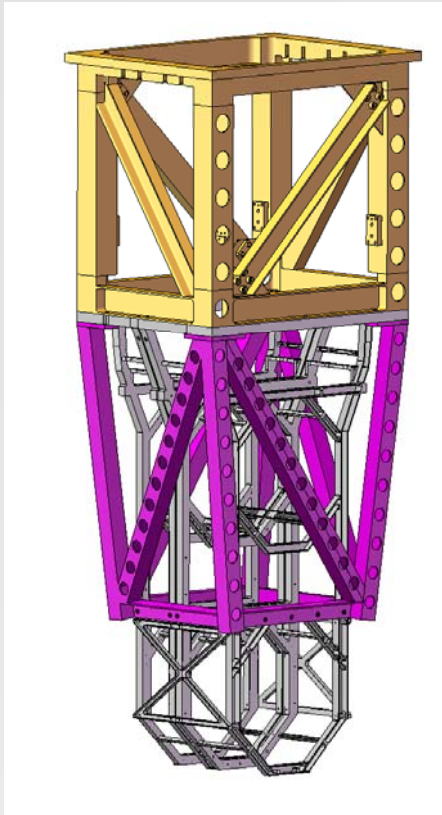


Plant variation

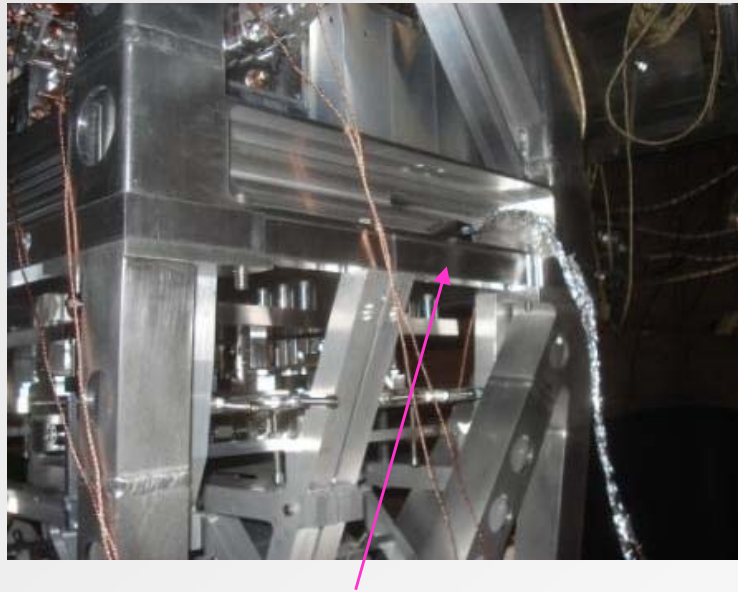
Stage 2 - Ry - GS13



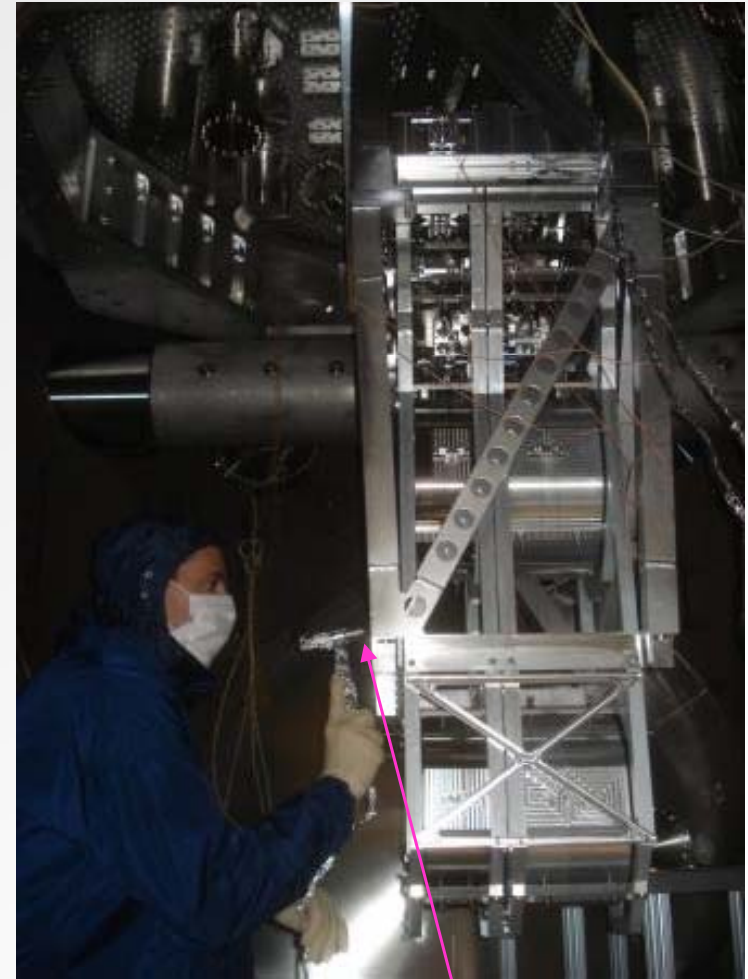
Quad Modal Testing



The Quad Structure

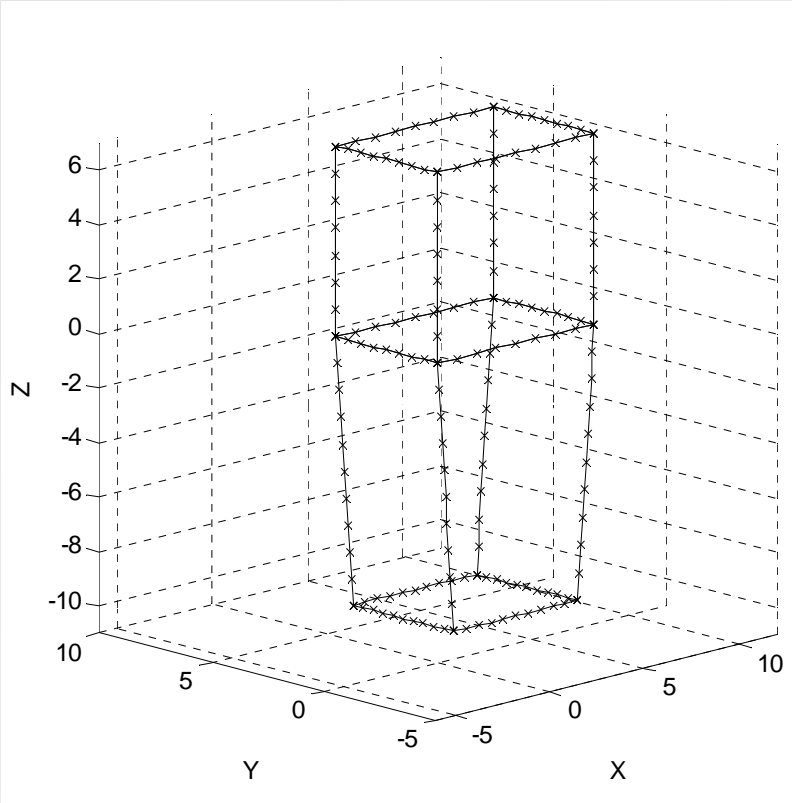


3 Axis Accelerometer

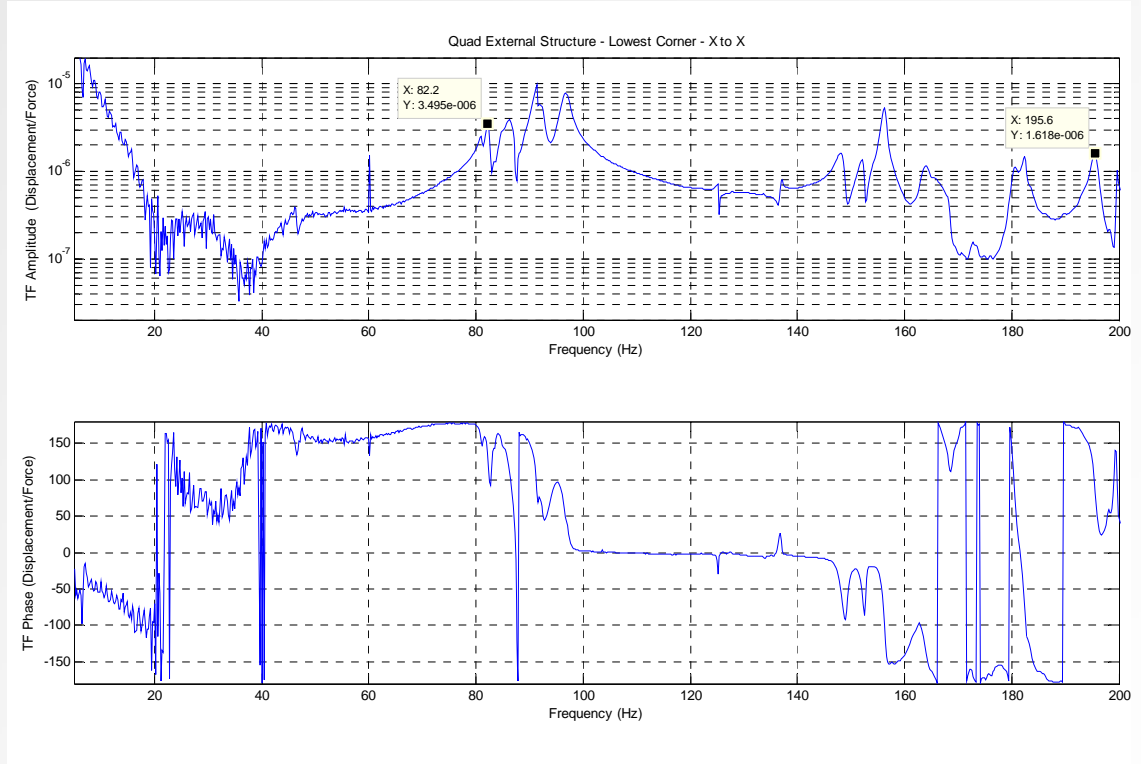


Impact Force Sensor

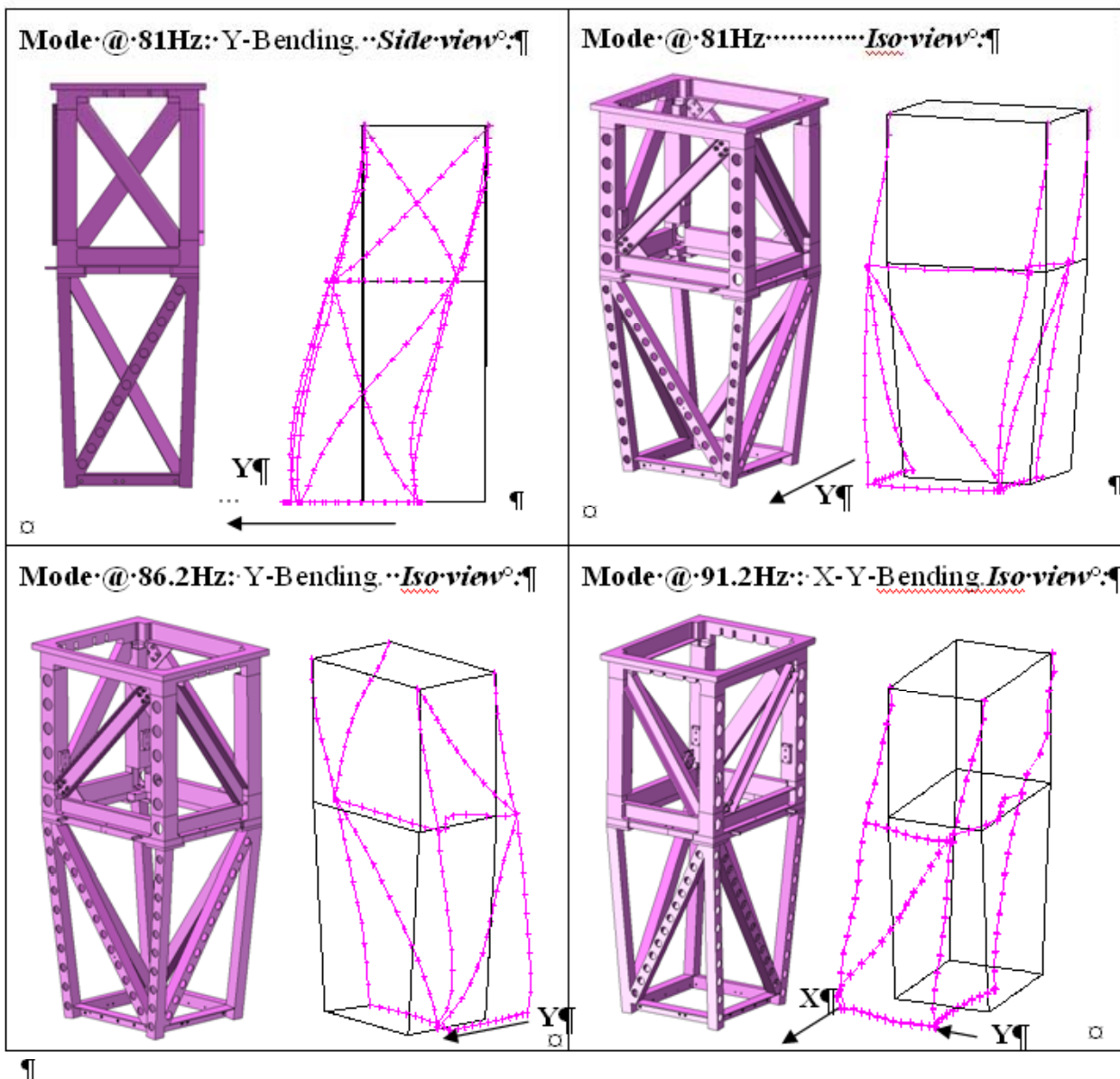
Experimental Meshing



Transfer Functions

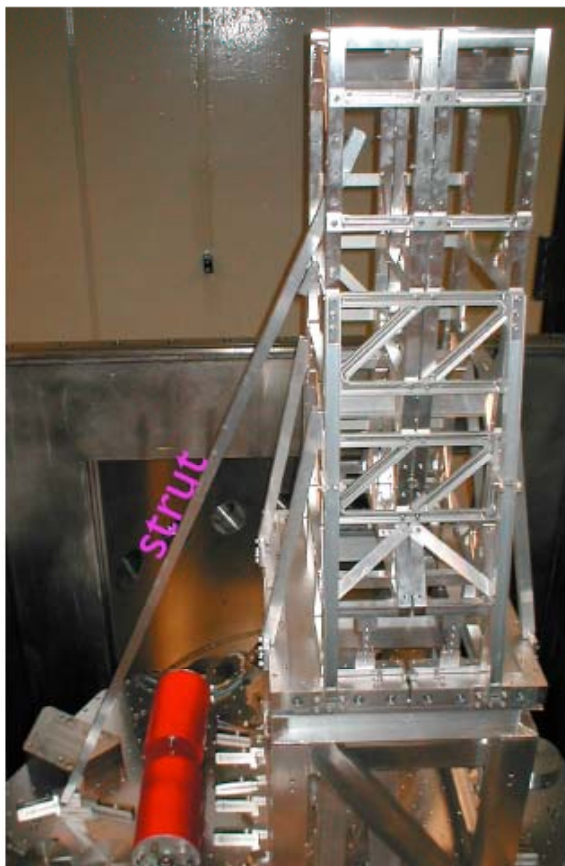


**First
modes
measured
on the Quad
structure :**

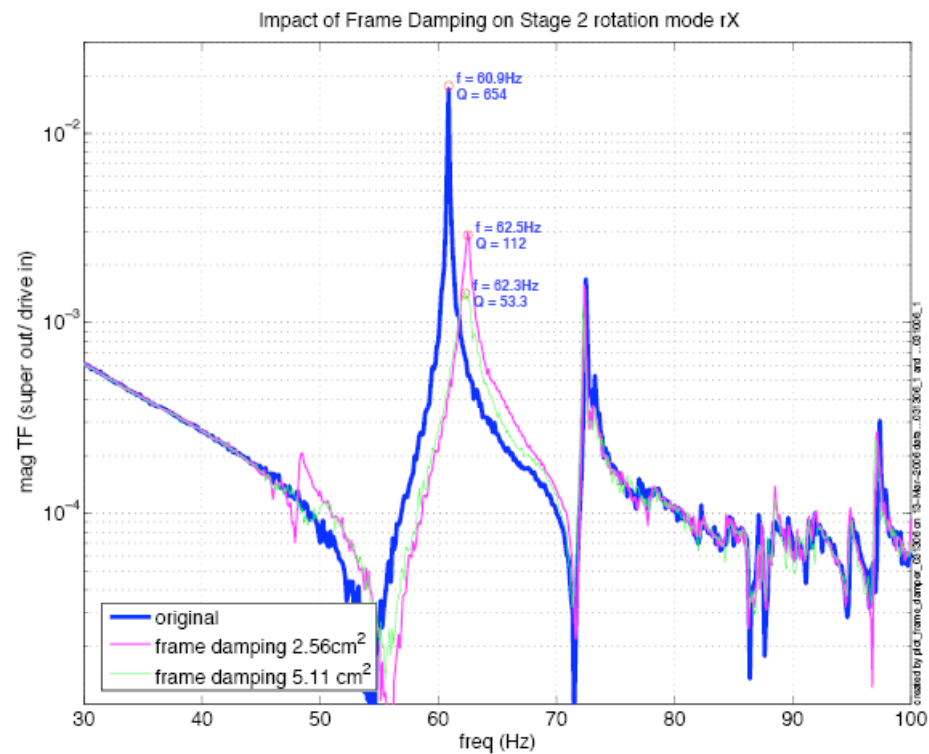




Setup

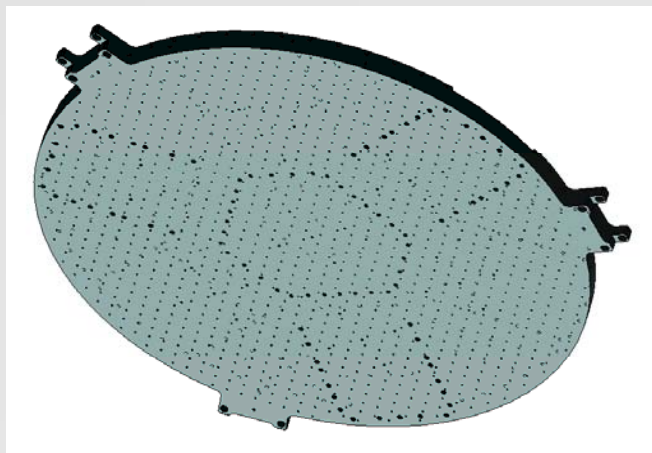


Results

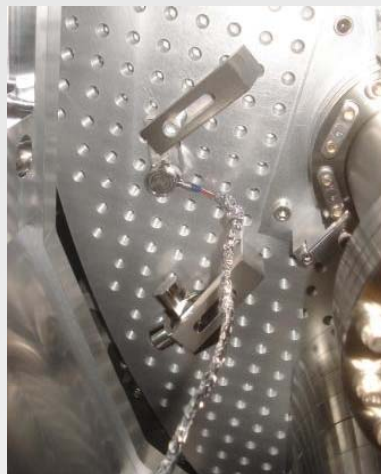


B.Lantz - Tech Demo - Stanford

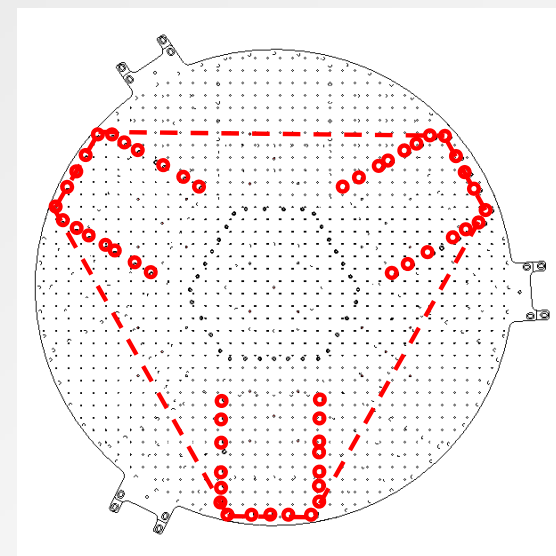
ISI Modal Testing :



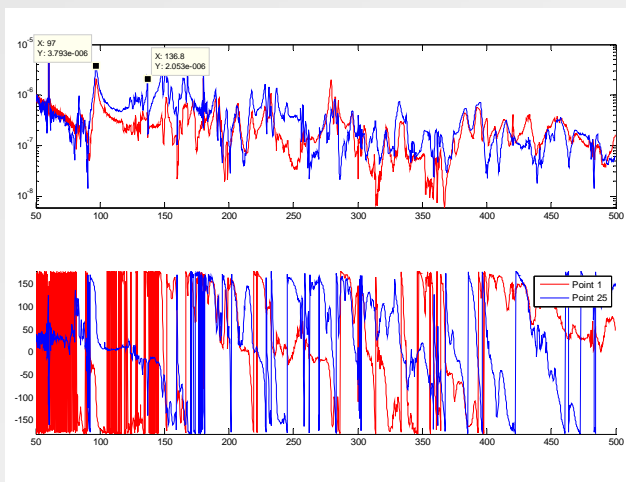
Optical Table



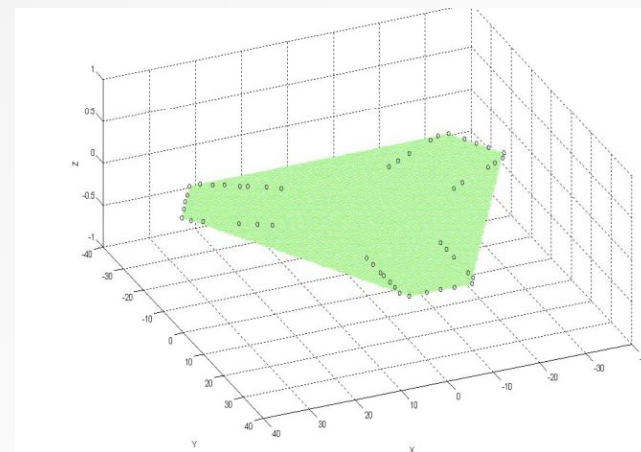
Instrumentation



Experimental Meshing



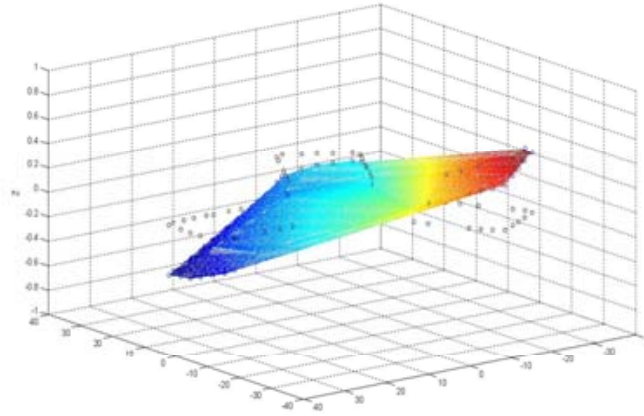
Transfer Functions



Domain of Interpolation

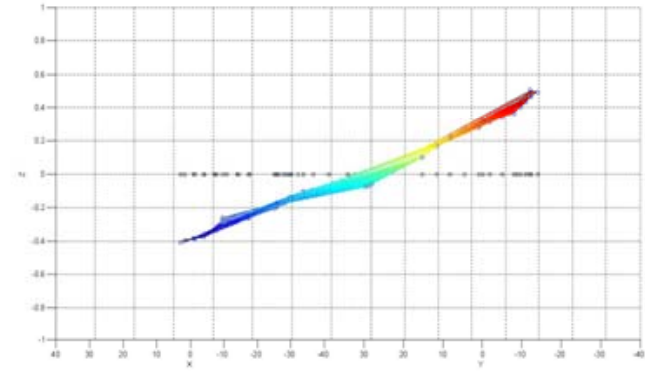
First modes measured on the optical table:

Mode @ 97 Hz:



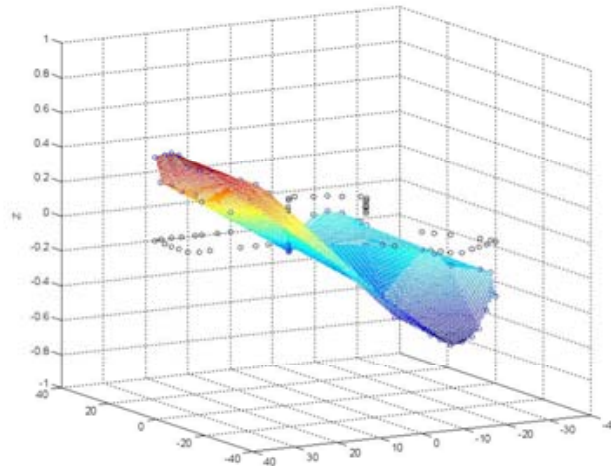
Isometric view

Mode @ 97 Hz:



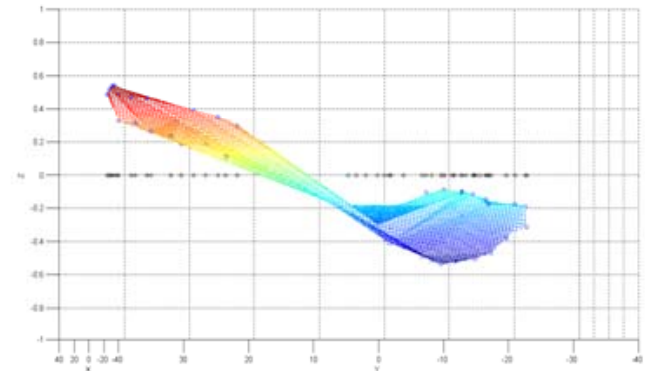
Side view

Mode @ 137 Hz:



Isometric view

Mode @ 137 Hz:



Side view

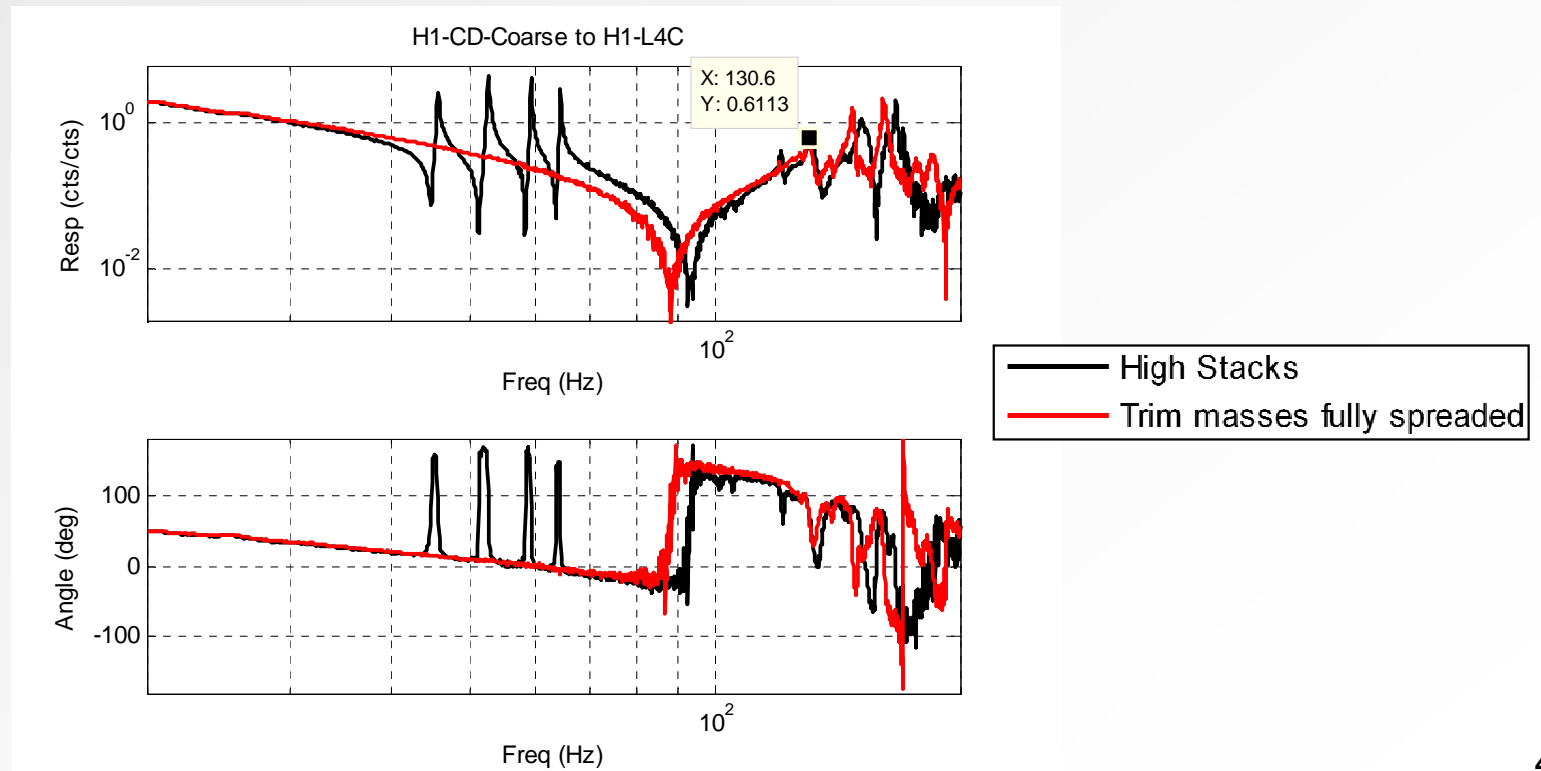
GS13 Attachment

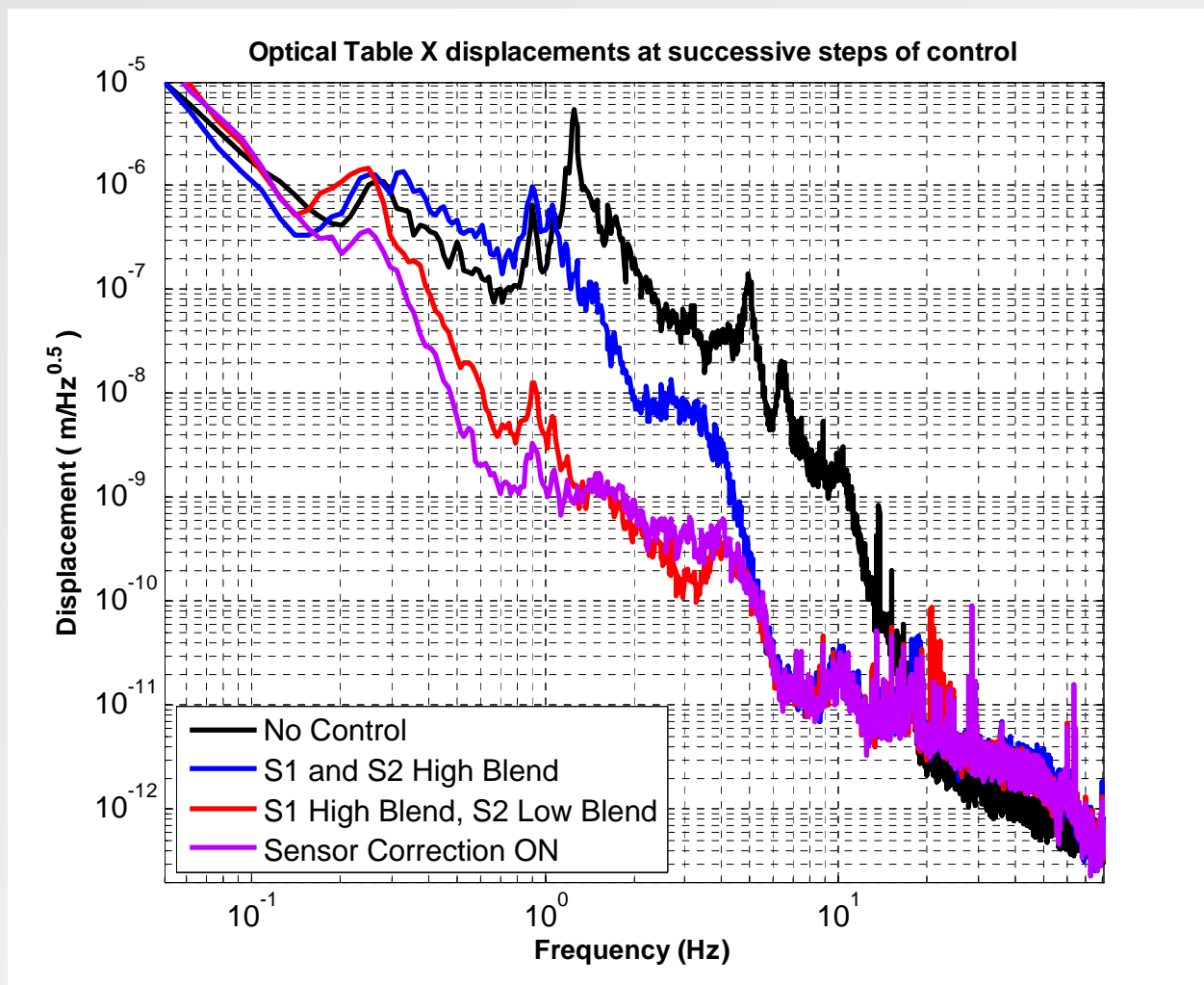


Counter weights



Transfer function

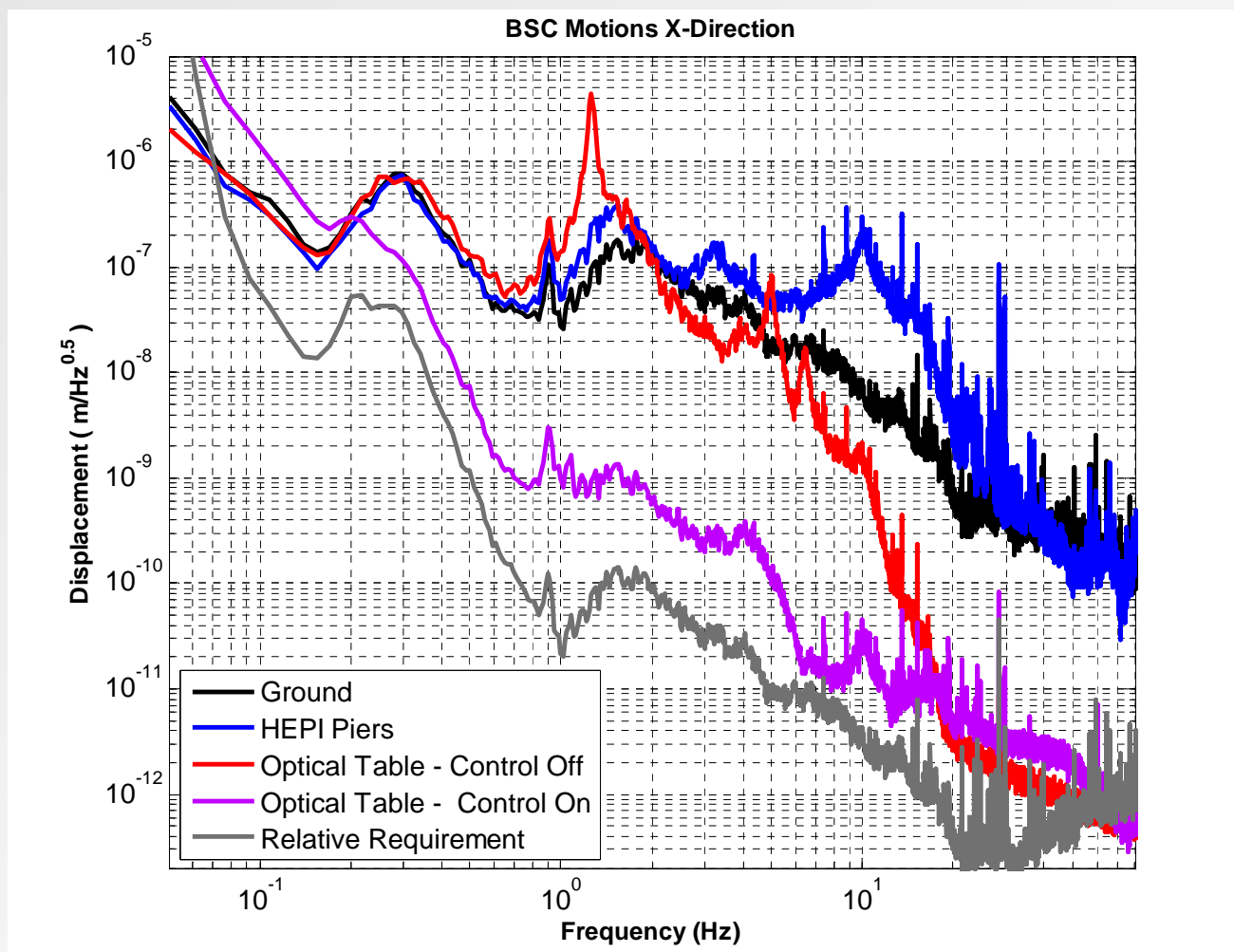




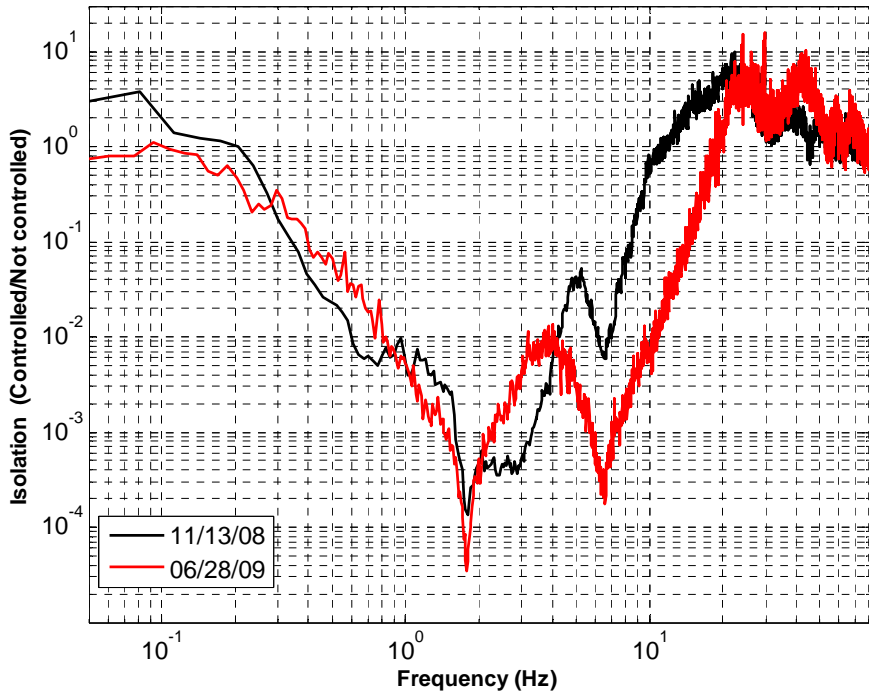
- ✓ At low frequencies (around 0.1Hz) there is very little motion amplification.
- ✓ The isolation starts as low as 0.1Hz which is good.
- ✓ The isolation at 1Hz is close to a factor of 100.
- ✓ The control provides isolation up to 20Hz, which is good.

Global isolation (Active & Passive)

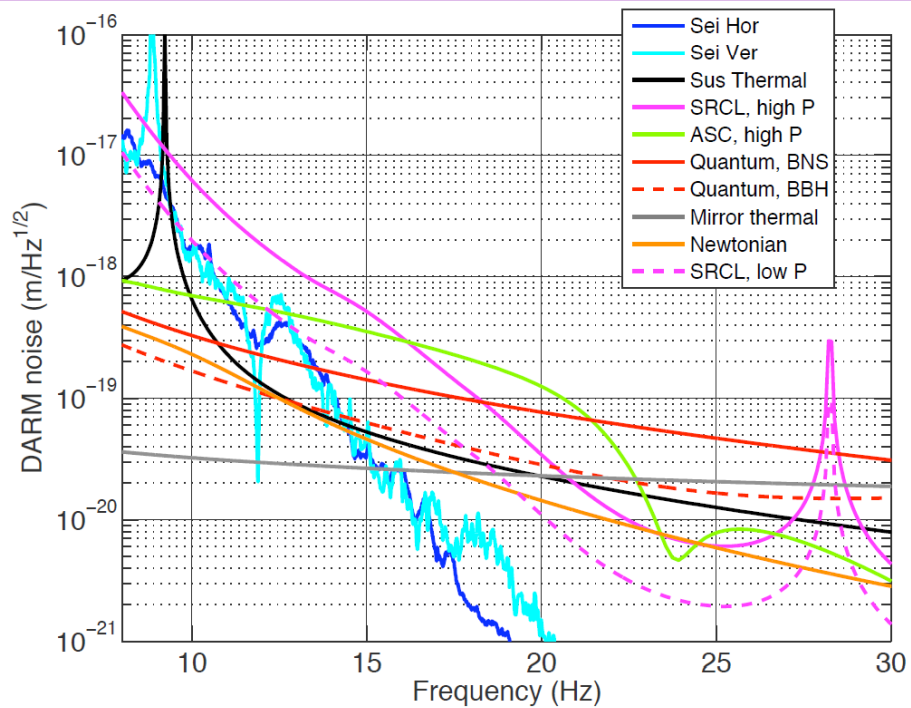
- The ground motion is shown in Black. It is measured with a STS.
- The HEPI motion is shown in Blue. It is measured with HEPI L4Cs.
- The motion of stage2 when the control is off is presented in Red
- The motion of stage2 when the control is on is presented in Purple
- The relative requirements are presented in Grey



Evolution of control performances since November 2008 - Z Direction



Low frequency noises

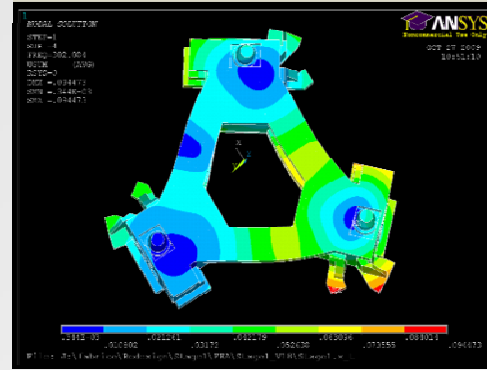
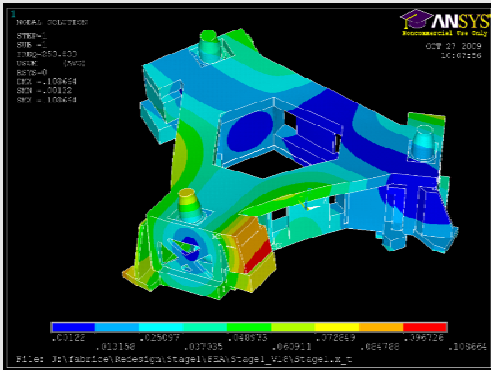


G0810021-v1

9

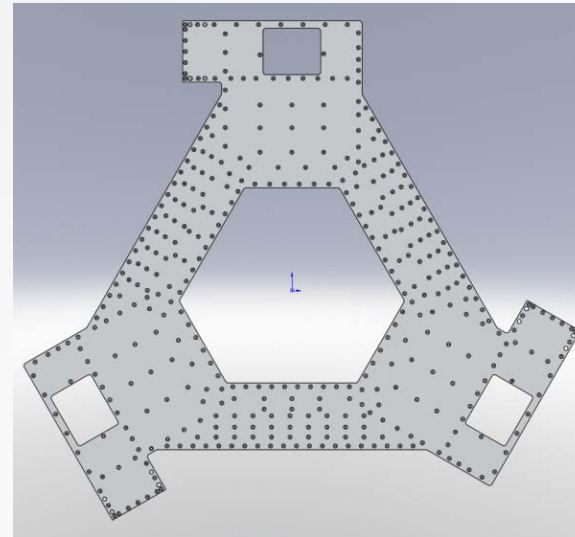
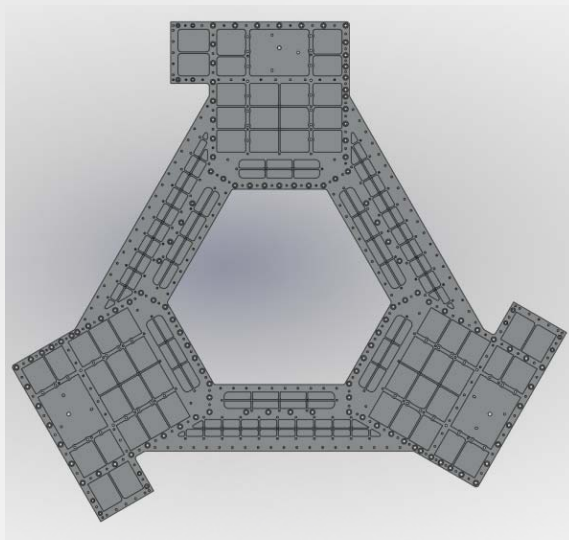
Stage1

- The close out plate studied and analyzed to optimize the stiffness of Stage1
- Successive conceptual design and Finite Element analysis.
- 18 iterations led to the design presented below.
- All analysis and concepts presented E0900389



	V1, 237 Lbs	V18, 376 Lbs
1	195 Hz	254 Hz
2	195 Hz	254 Hz
3	229 Hz	302 Hz
4	229 Hz	302 Hz
5	287 Hz	326 Hz
6	319 Hz	364 Hz

- The first two modes at 195Hz were in plane bending modes. They have moved to 302Hz.
- The next modes at 229Hz were torsion modes. They have moved to 254Hz.



The final design of the close plate and its new plate cover.

D0901182, Top Assembly Drawing:

NOTES CONTINUED:

① SCRIBE, ENGRAVE, OR MECHANICALLY STAMP INTO INKS OR DYES DRAWING PART NUMBER AND REVISION ON HOLED SURFACE FOLLOWED ON THE NEXT LINE BY A THREE DOT SERIAL NUMBER, SERIAL NUMBERS START AT 001 FOR THE FIRST ARTICLE AND PROCEED CONSECUTIVELY. USE 07" HIGH CHARACTERS. EXAMPLE: 000000001.V1 IN 001. A VIBRATORY TOOL MAY BE USED.

REV.	DATE	DCN #	DRAWING TREE #
-	-	-	-
-	-	-	-
-	-	-	-

① INTERPRET DRAWING PER ASME Y14.5-1994.
 ② REMOVE ALL SHARP EDGES, R.02 MIN.
 ③ DO NOT SCALE FROM DRAWING.
 ④ ALL MACHINING FLUIDS MUST BE FULLY SYNTHETIC, FULLY WATER SOLUBLE AND FREE OF SULFUR, SILICONE, AND CHLORINE.

ITEM NO. PART NUMBER DESCRIPTION MATERIAL REQ

31		Stage0 Vertical L4-C Assem	N/A	3
30			N/A	3
29	D0901282	breadboard	Metallic (not specified)	4
28		Stage1-2 Tooling Standoff Pin		3
27				3
26		Stage0-2 Alignment Pin		3
25			N/A	4
24		Stage0-1 Blade Pusher Assembly for loading Flexure Rods	N/A	3
23	D0902454	STAGE 1-2 BLADE FULLER	N/A	3
22		BSC ISLIFT HOOK ASSEMBLY	N/A	1
21	D0902164	Stage 1-2 Blade Safety Restraint	N/A	1
20	D0901872	Stage 01 Blade Spring Safety Restraint	N/A	3
19	D0900857	GS-13 Pod and GS-13	N/A	3
18	D0900857	GS-13 Pod and GS-13	N/A	3
17		Stage1-2, Vertical Position Sensor Asm	N/A	3
16	D0902236	Small Actuator, Vertical, Stage1, bracket	6061-T6 Al	3
15		Stage1-2, Vertical Actuator Asm	-	3
14		Stage0-1, Horizontal Actuator Asm	N/A	3
13		Stage1-2, Horizontal, Position Sensor Asm	N/A	3
12	D047941	Stage lock assembly	N/A	3
11	D047941	Stage lock assembly	N/A	3
10	D0901805	Stage0-1, Locker, Base Shim Spacer	304 STL	4
9	D0901102	Asm, Actuator	As Req.	3
8	D0901103	Stage0-1, Vertical, Large Actuator, I Connector, Left	As Req.	3
7	D0901554	Actuator Post for Stage0-1, Large Actuator	6061-T6 Al	3
6	D0901748	BSC, STAGE 1-2 FLEXURE ASSEMBLY	N/A	3
5		Stage1-2 Blade Spring Flexure Assem	N/A	3
4	D0901197	Assembly of Flexure, Blade, Rod and post with hardware		3
3	D0901181	Stage 2 BSC ISITable, Advanced LIGO	N/A	1
2	D0901180	S1 Assembly	N/A	1
1	D0900896	ADV LIGO SEI BSC STAGE 0 ASSEMBLY	N/A	1

Part Name: **Advanced LIGO BSC ISI Assembly**

DESIGNER: eorum July 2009
 DRAFTER: nullbard 30 Oct. 2009
 CHECKER:
 APPROVAL:

SCALE: 1:5 PROJECTION:

SHEET 1 OF 2

DIMENSIONS ARE IN INCHES

TOLERANCES:
 .XX: ± n/a
 .XXX: ± n/a
 ANGULAR ± n/a°

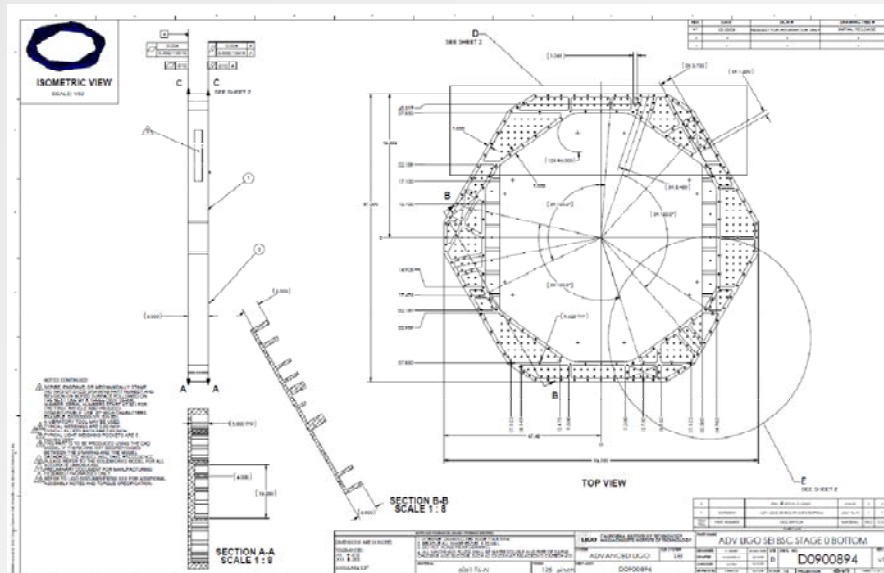
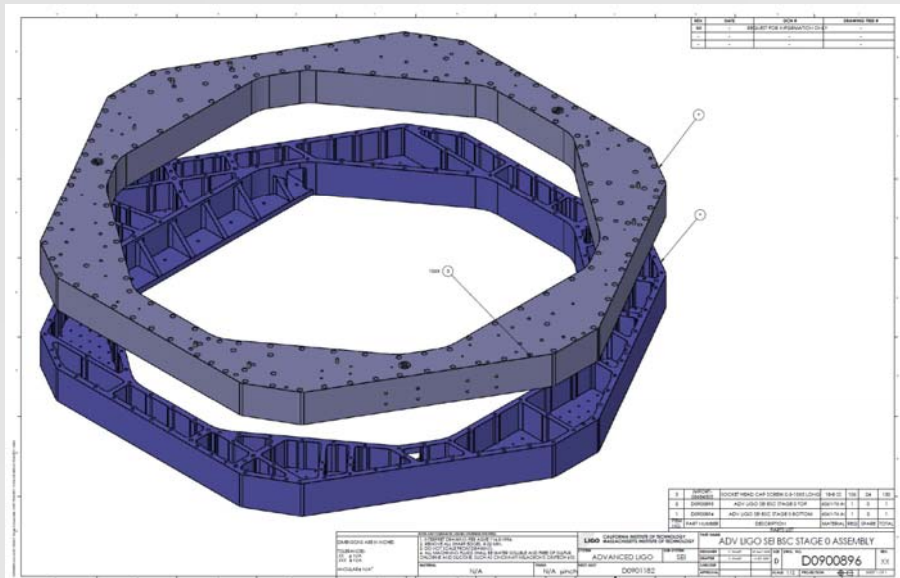
NOTES AND TOLERANCES (UNLESS OTHERWISE SPECIFIED)

MATERIAL: N/A FINISH: N/A μinch

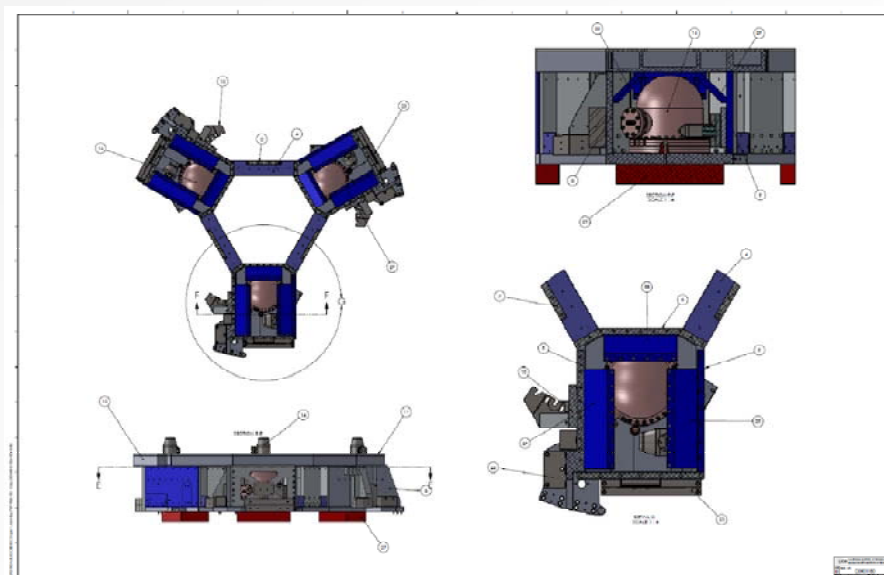
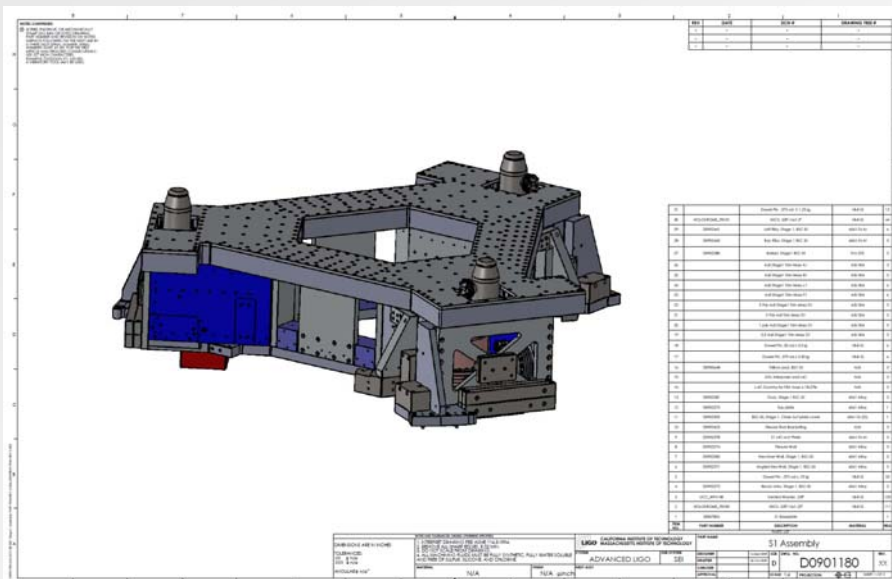
SYSTEM: ADVANCED LIGO SUB-SYSTEM: SEI

NEXT ASSY: SEI Top Level

D09000896, Stage 0 Assembly and D09000895, Stage 0 Bottom part



D0901180, Stage 1 Assembly



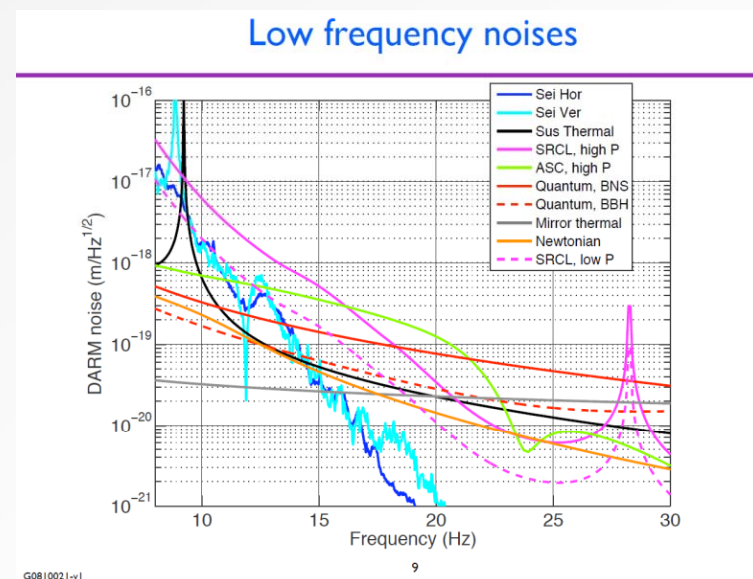
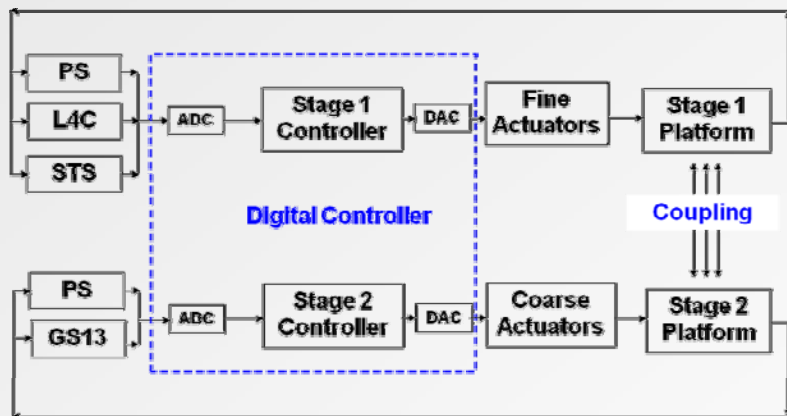
7- Assemblage



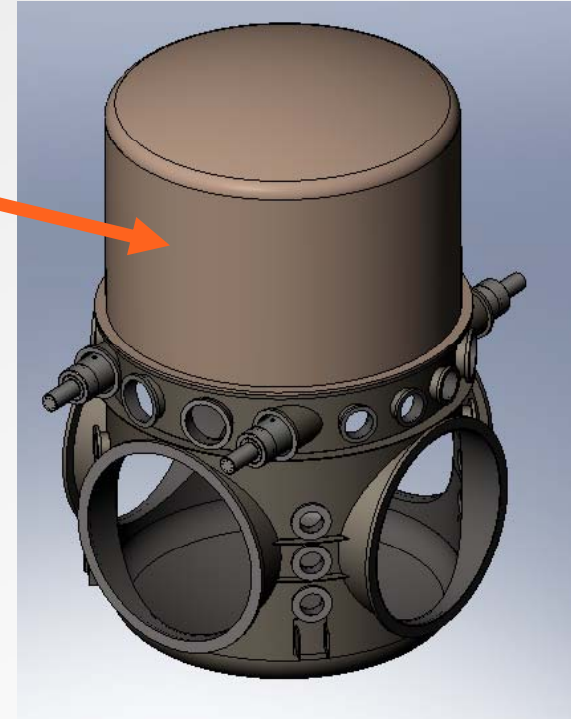
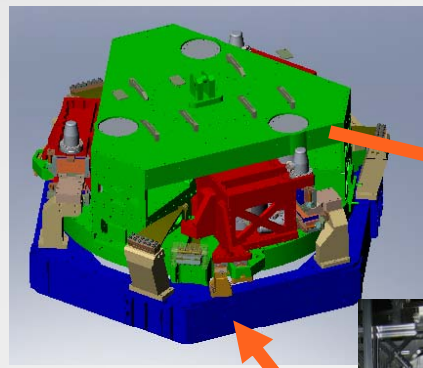
8- Installation



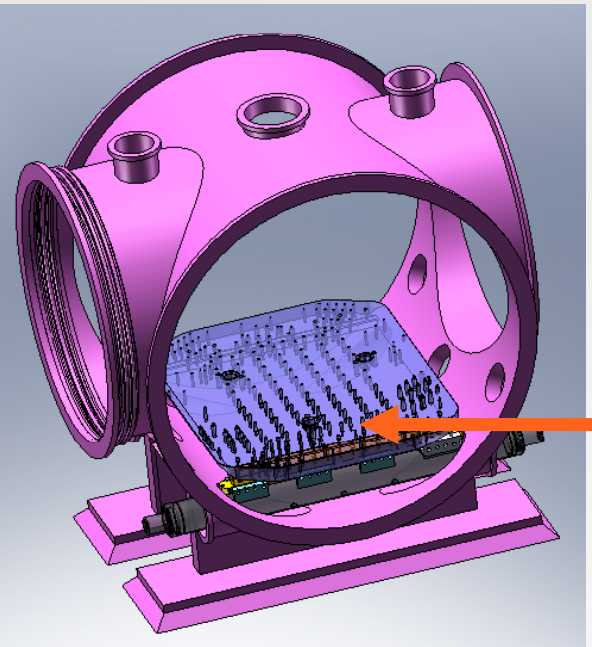
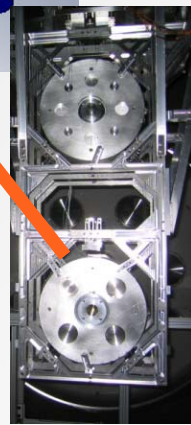
9- Mise en service



Triple Quad Cavity With BSC and HAM ISI



LASTI BSC



LASTI HAM X-End

