

## VOLUME II ATTACHMENTS

### ATTACHMENT 3 *Part #* L160-C960964-01-V

TITLE	DOCUMENT NO.	REVISION
<b>I. Adapters And Spools</b>		
Spool BE-3 & BE-3A(60 in)	V049-1-049	0
Spool BE-2 (60 in)	V049-1-050	0
Spool B-5 (30 in.)	V049-1-057	1
Spool B-6 (48 in)	V049-1-058	0
Spool B-7 (48 in)	V049-1-059	0
Spool B-8 (72 in)	V049-1-060	0
Spool B-9 (72 in)	V049-1-061	0
Spool BE-4 (44 in)	V049-1-076	0
Generic Spool Design	V049-1-077	0
Spool BE-5 (44 in)	V049-1-085	1
<b>II. Supports</b>		
Design of Flexible Support for Adapter A-7	V049-1-062	1
Design of Gate Valve Support	V049-1-086	0
Support Design for Mode Cleaner Tubes (B-2/B-3/B-5)	V049-1-087	1
Support Design for Beam Tube Manifold (BE-5)	V049-1-088	1
Support Design for Beam Tube Manifold (B-9)	V049-1-089	1
Support Design for Beam Tube Manifold (B-6/B-7)	V049-1-095	1
Turbo Cart Frame Extension	V049-1-098	0
<b>III. Miscellaneous</b>		
Flange Bolting for Gate Valves	V049-1-063	0
Bellows Deflection Study	V049-1-068	0
Analysis of BSC Support Leg to Cross Beam Connection	V049-1-079	0
Analysis of Bolted Flange for Initial Out of Flatness	V049-1-080	0
Expansion Joint Tie Rod Lug Design	V049-1-084	2
Stiffener Rings At Axial Restraints	V049-1-108	0
BSC Portable Clean Room	V049-1-112	0
HAM Portable Clean Room	V049-1-113	0

## DETERMINE LOADING CONDITIONS

BEAM MANIFOLD B-9 WAS DESIGNED USING THE COMPUTER AIDED DESIGN PROGRAM COMPRESS. THE WEIGHT SUMMARY INCLUDES THE WEIGHT OF VESSEL (INCLUDING STIFFENER RIBS, SUPPORT RINGS) ADDITIONALLY FLANGES WERE MODELED TO OBTAIN THEIR RESPECTIVE WEIGHTS.

$$\text{VESSEL WEIGHT} = 6737 \text{ lbs}$$

$$\frac{6737 \text{ lbs}}{408 \text{ in}} = 16.5 \text{ lbs/in.}$$

### FLANGE WEIGHTS

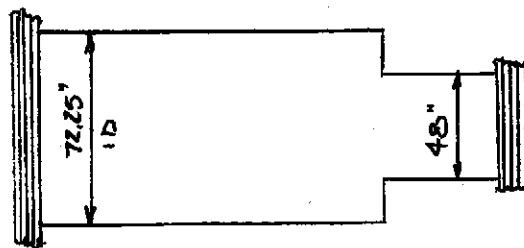
@ BE-5 BELLWS - 2 FLANGES

$$370 \text{ lbs} + 370 \text{ lbs} = 740 \text{ lbs.}$$

@ A-1 BELLWS - 2 FLANGES (ONE REDUCING)

$$1381 \text{ lbs} + 370 \text{ lbs.} = 1751 \text{ lbs.}$$

## UNBALANCED VACUUM LOAD



$$F_{72.25"} = (4.7 \text{ lb/in}^2) \left[ \frac{\pi (72.25 \text{ in})^2}{4} \right] = 60267 \text{ lbs}$$

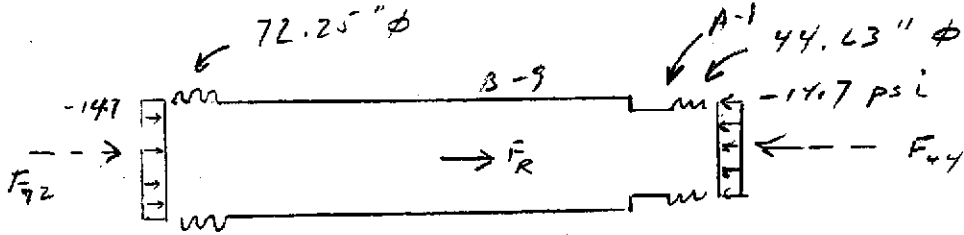
$$F_{48"} = 29500 \text{ lbs (ref. Calc V049-1-032)}$$

$$\therefore \text{UNBALANCED FORCE} = 60267 \text{ lbs} - 29500 \text{ lbs} \\ \approx 30800 \text{ lbs.}$$

SEE FOLLOWING SHEET FOR  
"EXACT" UNBAL FORCE



STOOL B-9 UNBALANCED AXIAL FORCE:



$$F_R = \text{AXIAL REACTION (TABO)}$$

$$F_{72} = 72.25" \text{ BELLOWS VAC FORCE} \\ = -64.1 \text{ K (CALL V049-1-032, P5)}$$

$$F_{44} = 44.63" \text{ BELLOWS VAC FORCE} \\ = -25.37 \text{ SAY } -25.4 \text{ K} \\ \text{(CALL V049-1-032, P.4)}$$

$$+ \rightarrow F_R + F_{72} - F_{44} = 0$$

$$F_R = F_{44} - F_{72} \\ = -25.4 - (-64.1) \\ = 38.7 \text{ K}$$

RECALCULATE USING LATEST BELLOWS DM

$$F_{72} = -62.522 \text{ K } \checkmark \text{ DM (HYDROD CALL 7/9/96)}$$

$$F_{44} = -14.7 \pi \left( \frac{45.964}{2} \right)^2 \\ = -24,392 \text{ K}$$

$$F_R = -24,392 - (-62.522) = \\ = 38.13 \text{ K}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



\*COMPRESS\* - WEIGHT SUMMARY

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



File View Title Block C:\COMPRESS\MANIFOLD\b-9.vsl:Weight summary

Component	Weight (lbs)				Contributed	
	Metal New	Metal Corr	Trays & sup	Packed Beds	Insul	Lir
Spool b-9	6737	6737	0	0	0	
Reducing flg	370	370	0	0	0	
Adapter flg	370	370	0	0	0	
	7477	7477	0	0	0	

Vessel operating weight, corroded: 7,895 lbs  
 Vessel empty weight, corroded: 7,895 lbs  
 Vessel empty weight, new: 7,895 lbs  
 Vessel test weight, new: 68,289 lbs

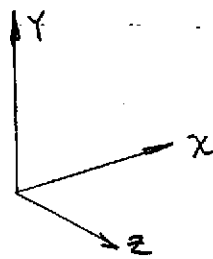
File View Title Block C:\COMPRESS\MANIFOLD\b-9.vsl:Weight summary

Component	Weight (lbs)				Contributed	
	Metal New	Metal Corr	Trays & sup	Packed Beds	Insul	Lir
Spool b-9	6737	6737	0	0	0	
Reducing flg	1381	1381	0	0	0	
Adapter flg	370	370	0	0	0	
	8488	8488	0	0	0	

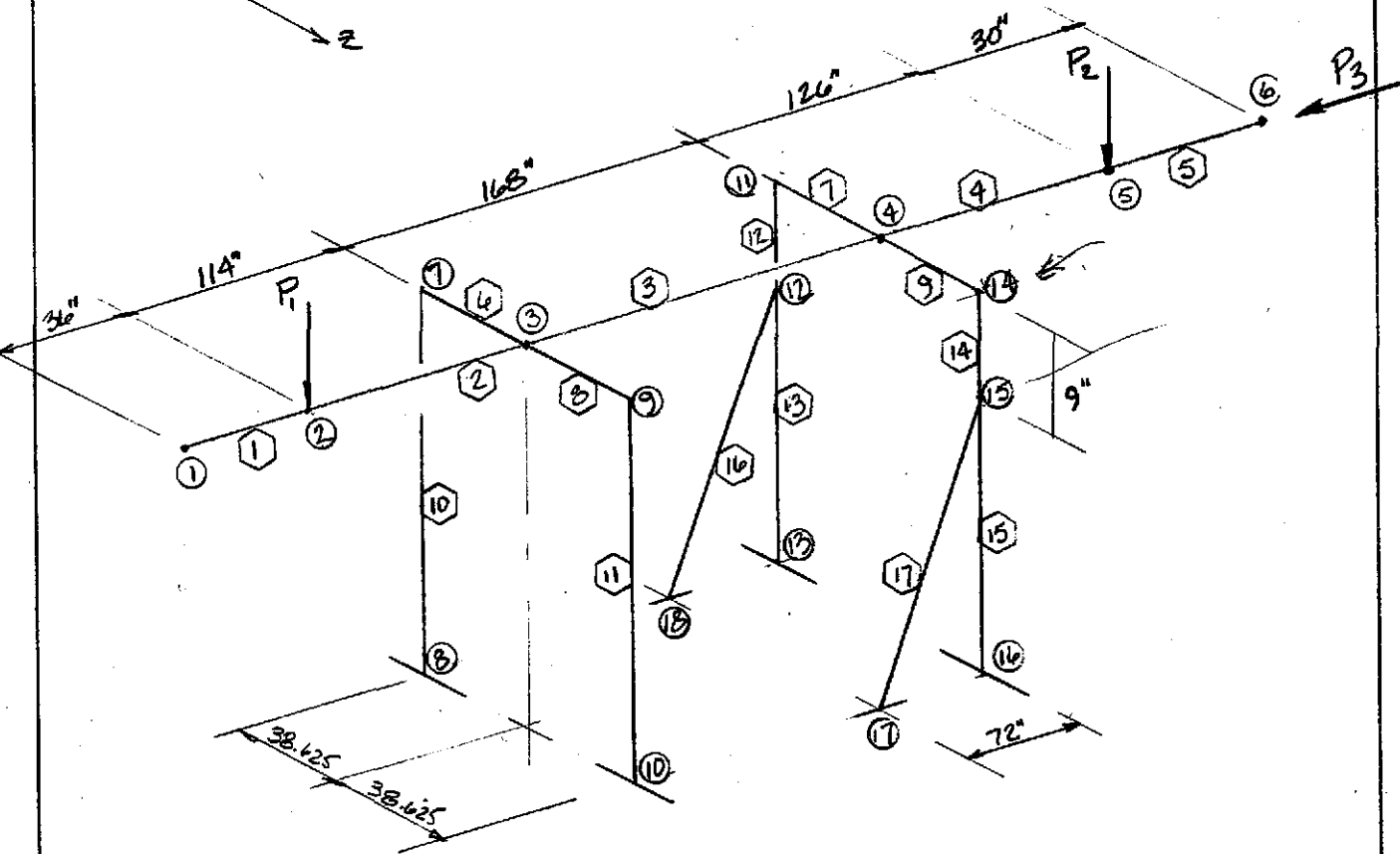
Vessel operating weight, corroded: 8,906 lbs  
 Vessel empty weight, corroded: 8,906 lbs  
 Vessel empty weight, new: 8,906 lbs  
 Vessel test weight, new: 69,300 lbs

# B-9 BEAM TUBE MANIFOLD SUPPORT SCHEME

STAAD MODEL



22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



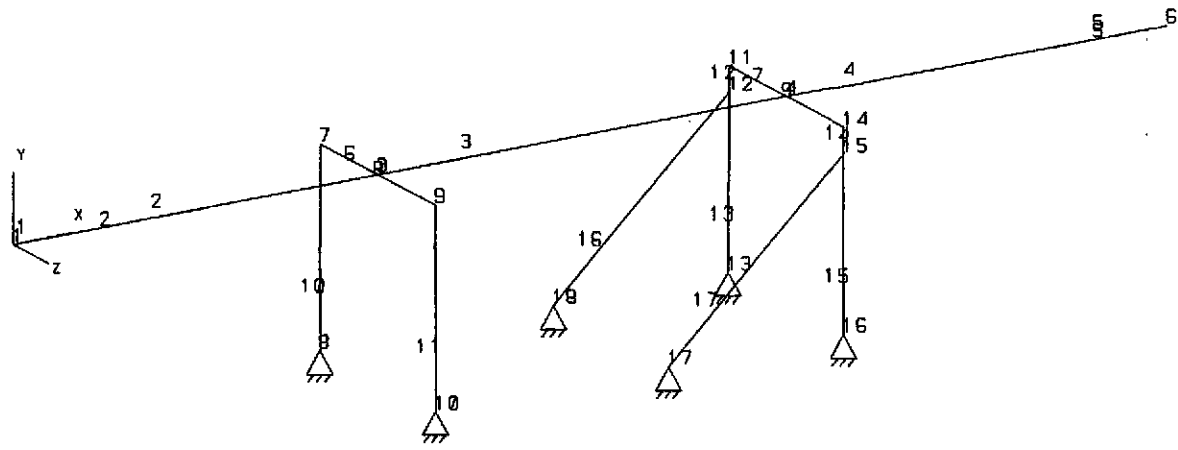
$P_1 = 740 \text{ lbs}$

$P_2 = 1751 \text{ lbs}$

$P_3 = 38130. \text{ lbs}$

STRUCTURE DATA

TYPE = SPACE  
 NJ = 18  
 NM = 17  
 NE = 0  
 NS = 6  
 NL = 4  
 XMAX = 474.0  
 YMAX = 70.0  
 ZMAX = 77.3



J=18, H=17

UNIT INC PDU

```

*****
*
*           S T A A D - III
*           Revision 21.0
*           Proprietary Program of
*           Research Engineers, Inc.
*           Date=   SEP 17, 1996
*           Time=   14:18:40
*
*           USER ID: PROCESS SYSTEMS INTERNATIONAL IN
*****

```

1. STAAD SPACE B-9 BEAM TUBE MANIFOLD SUPPORT
2. INPUT WIDTH 72
3. UNIT INCHES POUND
4. JOINT COORDINATES
  - 5. 1 0. 0. 0.; 2 36. 0. 0.; 3 150. 0. 0.; 4 318. 0. 0.; 5 444. 0. 0.
  - 6. 6 474. 0. 0.; 7 150. 0. -38.625; 8 150. -70. -38.625; 9 150. 0. 38.625
  - 7. 10 150. -70. 38.625; 11 318. 0. -38.625; 12 318. -9. -38.625
  - 8. 13 318. -70. -38.625; 14 318. 0. 38.625; 15 318. -9. 38.625
  - 9. 16 318. -70. 38.625; 17 246. -70. 38.625; 18 246. -70. -38.625
10. MEMBER INCIDENCES
  - 11. 1 1 2; 2 2 3; 3 3 4; 4 4 5; 5 5 6; 6 3 7; 7 4 11; 8 3 9; 9 4 14; 10 8 7
  - 12. 11 10 9; 12 12 11; 13 13 12; 14 15 14; 15 16 15; 16 18 12; 17 17 15
13. MEMBER PROPERTY AMER
14. 10 11 TABLE ST TUB40203
15. 1 TO 5 TABLE ST PIPE OD 72.75 ID 72.25
16. 12 TO 17 TABLE ST TUB40408
17. 6 TO 9 TABLE ST TUB1401408
18. MEMBER RELEASE
19. 10 TO 12 14 END MX MY MZ
20. CONSTANTS
21. E STEEL ALL
22. POISSON STEEL ALL
23. DENSITY STEEL ALL
24. BETA 90. MEMB 10 TO 15
25. ALPHA 0.00000919 MEMB 1 TO 9
26. SUPPORTS
27. 8 10 FIXED BUT MZ
28. 13 16 TO 18 FIXED
29. \*\*\*\*\*
30. LOAD 1 DEADWEIGHT
31. JOINT LOAD
32. 2 FY -740.
33. \* FLANGE WEIGHT
34. 5 FY -1751.
35. \* FLANGE WEIGHT
36. MEMBER LOAD
37. 1 TO 5 UNI Y -16.15
38. \* VESSEL WGHT = 6737.#/408"
39. \*\*\*\*\*
40. LOAD 2 DW+TH+VACUUM
41. JOINT LOAD

42. 2 FY -740.  
 43. 5 FY -1751.  
 44. 5 FX -38129.992.  
 45. \* UNBALANCED VACUUM LOAD @ A-1 BELLOWS  
 46. MEMBER LOAD  
 47. 1 TO 5 UNI Y -16.15  
 48. TEMPERATURE LOAD  
 49. 1 TO 5 TEMP 330.  
 50. \*\*\*\*\*  
 51. LOAD 3 DW+TH+SEIS-AXIAL  
 52. JOINT LOAD  
 53. 2 FY -740.  
 54. 5 FY -1751.  
 55. 5 FX -38129.992  
 56. 2 FX -42.  
 57. 5 FX -98.  
 58. MEMBER LOAD  
 59. 1 TO 5 UNI Y -16.15  
 60. 1 TO 5 UNI X -0.908  
 61. TEMPERATURE LOAD  
 62. 1 TO 5 TEMP 330.  
 63. \*\*\*\*\*  
 64. LOAD 4 DW+TH+SEIS-LAT  
 65. JOINT LOAD  
 66. 2 FY -740.  
 67. 5 FY -1751.  
 68. 5 FX -38129.992  
 69. 2 FZ 42.  
 70. 5 FZ 98.  
 71. MEMBER LOAD  
 72. 1 TO 5 UNI Y -16.15  
 73. 1 TO 5 UNI Z 0.908  
 74. TEMPERATURE LOAD  
 75. 1 TO 5 TEMP 330.  
 76. \*\*\*\*\*  
 77. LOAD 5 THERMAL DISPL "BAKEOUT"  
 78. TEMPERATURE LOAD  
 79. 1 TO 5 TEMP 330.  
 80. \*\*\*\*\*  
 81. PERFORM ANALYSIS

P R O B L E M   S T A T I S T I C S

---

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS = 18/ 17/ 6  
 ORIGINAL/FINAL BAND-WIDTH = 10/ 5  
 TOTAL PRIMARY LOAD CASES = 5, TOTAL DEGREES OF FREEDOM = 74  
 SIZE OF STIFFNESS MATRIX = 2664 DOUBLE PREC. WORDS  
 REQD/AVAIL. DISK SPACE = 12.05/ 954.8 MB, EXMEM = 14.83 MB

++ PROCESSING ELEMENT STIFFNESS MATRIX.	14:18:42
++ PROCESSING GLOBAL STIFFNESS MATRIX.	14:18:42
++ PROCESSING TRIANGULAR FACTORIZATION.	14:18:42
++ CALCULATING JOINT DISPLACEMENTS.	14:18:42



B-9 BEAM TUBE MANIFOLD SUPPORT

-- PAGE NO. 3

++ CALCULATING MEMBER FORCES.

14:18:42

82. PRINT MATERIAL PROPERTIES ALL

## MATERIAL PROPERTIES..

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
1	29000000.0	11153846.0	0.28299999	0.00000919
2	29000000.0	11153846.0	0.28299999	0.00000919
3	29000000.0	11153846.0	0.28299999	0.00000919
4	29000000.0	11153846.0	0.28299999	0.00000919
5	29000000.0	11153846.0	0.28299999	0.00000919
6	29000000.0	11153846.0	0.28299999	0.00000919
7	29000000.0	11153846.0	0.28299999	0.00000919
8	29000000.0	11153846.0	0.28299999	0.00000919
9	29000000.0	11153846.0	0.28299999	0.00000919
10	29000000.0	11153846.0	0.28299999	0.00000000
11	29000000.0	11153846.0	0.28299999	0.00000000
12	29000000.0	11153846.0	0.28299999	0.00000000
13	29000000.0	11153846.0	0.28299999	0.00000000
14	29000000.0	11153846.0	0.28299999	0.00000000
15	29000000.0	11153846.0	0.28299999	0.00000000
16	29000000.0	11153846.0	0.28299999	0.00000000
17	29000000.0	11153846.0	0.28299999	0.00000000

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

83. PRINT MEMBER INFORMATION ALL

## MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
1	1	2	36.000	0.00	
2	2	3	114.000	0.00	
3	3	4	168.000	0.00	
4	4	5	126.000	0.00	
5	5	6	30.000	0.00	
6	3	7	38.625	0.00	
7	4	11	38.625	0.00	
8	3	9	38.625	0.00	
9	4	14	38.625	0.00	
10	8	7	70.000	90.00	000000000111
11	10	9	70.000	90.00	000000000111
12	12	11	9.000	90.00	000000000111
13	13	12	61.000	90.00	
14	15	14	9.000	90.00	000000000111
15	16	15	61.000	90.00	
16	18	12	94.366	0.00	
17	17	15	94.366	0.00	

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

84. PRINT JOINT COORDINATES ALL

## JOINT COORDINATES

-----  
COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
1	0.000	0.000	0.000
2	36.000	0.000	0.000
3	150.000	0.000	0.000
4	318.000	0.000	0.000
5	444.000	0.000	0.000
6	474.000	0.000	0.000
7	150.000	0.000	-38.625
8	150.000	-70.000	-38.625
9	150.000	0.000	38.625
10	150.000	-70.000	38.625
11	318.000	0.000	-38.625
12	318.000	-9.000	-38.625
13	318.000	-70.000	-38.625
14	318.000	0.000	38.625
15	318.000	-9.000	38.625
16	318.000	-70.000	38.625
17	246.000	-70.000	38.625
18	246.000	-70.000	-38.625

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

85. PRINT SUPPORT INFORMATION ALL

SUPPORT INFORMATION (1=FIXED, 0=RELEASED)

-----  
UNITS FOR SPRING CONSTANTS ARE POUN INCH DEGREES

JOINT	FORCE-X/ KFX	FORCE-Y/ KFY	FORCE-Z/ KFZ	MOM-X/ KMX	MOM-Y/ KMY	MOM-Z/ KMZ
8	1	1	1	1	1	0
	0.0	0.0	0.0	0.0	0.0	0.0
10	1	1	1	1	1	0
	0.0	0.0	0.0	0.0	0.0	0.0
13	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
16	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
17	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
18	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

86. PRINT ANALYSIS RESULTS

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE  
 -----

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
1	1	0.00111	-0.00856	0.00000	0.00000	0.00000	0.00003
	2	-1.07093	-0.01434	0.00000	0.00000	0.00000	0.00007
	3	-1.07258	-0.01443	0.00000	0.00000	0.00000	0.00007
	4	-1.07093	-0.01434	0.06129	0.00000	0.00003	0.00007
	5	-0.96440	0.00000	0.00000	0.00000	0.00000	0.00000
2	1	0.00111	-0.00752	0.00000	0.00000	0.00000	0.00003
	2	-0.96175	-0.01192	0.00000	0.00000	0.00000	0.00007
	3	-0.96340	-0.01198	0.00000	0.00000	0.00000	0.00007
	4	-0.96175	-0.01192	0.06005	0.00000	0.00003	0.00007
	5	-0.85522	0.00000	0.00000	0.00000	0.00000	0.00000
3	1	0.00111	-0.00413	0.00000	0.00000	0.00000	0.00002
	2	-0.61603	-0.00413	0.00000	0.00000	0.00000	0.00005
	3	-0.61766	-0.00413	0.00000	0.00000	0.00000	0.00005
	4	-0.61603	-0.00413	0.05613	0.00000	0.00003	0.00005
	5	-0.50949	0.00000	0.00000	0.00000	0.00000	0.00000
4	1	0.00111	-0.00478	0.00000	0.00000	0.00000	-0.00003
	2	-0.10653	0.00170	0.00000	0.00000	0.00000	0.00001
	3	-0.10814	0.00179	0.00000	0.00000	0.00000	0.00001
	4	-0.10653	0.00170	0.05070	0.00000	0.00003	0.00001
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
5	1	0.00111	-0.01174	0.00000	0.00000	0.00000	-0.00005
	2	0.27268	-0.00041	0.00000	0.00000	0.00000	-0.00002
	3	0.27105	-0.00024	0.00000	0.00000	0.00000	-0.00001
	4	0.27268	-0.00041	0.04712	0.00000	0.00003	-0.00002
	5	0.38212	0.00000	0.00000	0.00000	0.00000	0.00000
6	1	0.00111	-0.01338	0.00000	0.00000	0.00000	-0.00005
	2	0.36366	-0.00089	0.00000	0.00000	0.00000	-0.00002
	3	0.36203	-0.00070	0.00000	0.00000	0.00000	-0.00001
	4	0.36366	-0.00089	0.04627	0.00000	0.00003	-0.00002
	5	0.47310	0.00000	0.00000	0.00000	0.00000	0.00000
7	1	0.00111	-0.00216	0.00000	0.00006	0.00000	0.00002
	2	-0.61603	-0.00216	0.00000	0.00006	0.00000	0.00005
	3	-0.61766	-0.00216	0.00000	0.00006	0.00000	0.00005
	4	-0.61732	-0.00214	0.05613	0.00006	0.00003	0.00005
	5	-0.50949	0.00000	0.00000	0.00000	0.00000	0.00000
8	1	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00002
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00880
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00882
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00882
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00728
9	1	0.00111	-0.00216	0.00000	-0.00006	0.00000	0.00002
	2	-0.61603	-0.00216	0.00000	-0.00006	0.00000	0.00005
	3	-0.61766	-0.00216	0.00000	-0.00006	0.00000	0.00005
	4	-0.61473	-0.00218	0.05613	-0.00006	0.00003	0.00005
	5	-0.50949	0.00000	0.00000	0.00000	0.00000	0.00000
10	1	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00002
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00880
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00882

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE  
 -----

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00878
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00728
11	1	0.00111	-0.00124	0.00000	0.00011	0.00000	-0.00003
	2	-0.08585	0.00524	0.00000	0.00011	-0.00062	0.00001
	3	-0.08715	0.00533	0.00000	0.00011	-0.00063	0.00001
	4	-0.08678	0.00530	0.05069	0.00011	-0.00060	0.00001
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
12	1	0.00091	-0.00108	0.00000	0.00000	0.00000	-0.00002
	2	-0.02402	0.00540	0.00000	0.00000	0.00000	0.00500
	3	-0.02440	0.00549	0.00000	0.00000	0.00000	0.00507
	4	-0.02429	0.00546	0.04139	0.00101	-0.00010	0.00505
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
13	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
14	1	0.00111	-0.00124	0.00000	-0.00011	0.00000	-0.00003
	2	-0.08585	0.00524	0.00000	-0.00011	0.00062	0.00001
	3	-0.08715	0.00533	0.00000	-0.00011	0.00063	0.00001
	4	-0.08493	0.00517	0.05069	-0.00010	0.00064	0.00001
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
15	1	0.00091	-0.00108	0.00000	0.00000	0.00000	-0.00002
	2	-0.02402	0.00540	0.00000	0.00000	0.00000	0.00500
	3	-0.02440	0.00549	0.00000	0.00000	0.00000	0.00507
	4	-0.02376	0.00533	0.04139	0.00101	-0.00010	0.00495
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
16	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
17	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
18	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

SUPPORT REACTIONS -UNIT POUN INCH      STRUCTURE TYPE = SPACE  
-----

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
8	1	0.00	1809.87	0.00	0.00	0.00	0.00
	2	0.00	1809.87	0.00	-0.10	0.00	0.00
	3	0.00	1809.87	0.00	-0.02	0.00	0.00
	4	0.00	1793.91	-55.29	-3870.62	0.00	0.00
	5	0.00	0.00	0.00	-0.08	0.00	0.00
10	1	0.00	1809.87	0.00	0.00	0.00	0.00
	2	0.00	1809.88	0.00	-0.10	0.00	0.00
	3	0.00	1809.87	0.00	-0.02	0.00	0.00
	4	0.00	1825.84	-55.29	-3870.62	0.00	0.00
	5	0.00	0.00	0.00	-0.08	0.00	0.00
13	1	-4.22	3257.23	0.00	0.00	0.00	258.77
	2	-2361.71	-16318.38	0.00	-0.01	0.00	42796.62
	3	-2396.97	-16611.12	0.00	-0.04	0.00	43432.74
	4	<del>-2386.98</del>	<del>-16512.10</del>	<del>-194.01</del>	<del>-11828.66</del>	<del>379.88</del>	<del>43253.45</del>
	5	-0.01	-0.09	0.00	-0.02	0.00	0.20
16	1	-4.22	3257.23	0.00	0.00	0.00	258.77
	2	-2361.70	-16318.28	0.00	-0.01	0.00	42796.38
	3	-2396.97	-16611.11	0.00	-0.04	0.00	43432.71
	4	-2336.43	-16124.54	-194.01	-11828.66	379.88	42339.50
	5	0.00	-0.01	0.00	-0.02	0.00	0.02
17	1	4.22	5.95	0.00	0.00	0.00	169.52
	2	21426.66	19581.45	0.00	0.00	0.00	32520.79
	3	21747.13	19874.29	0.00	-0.01	0.01	33004.74
	4	21197.19	19371.75	-35.89	-4264.39	2204.37	32173.45
	5	0.01	0.01	0.00	-0.01	0.00	0.02
18	1	4.22	5.95	0.00	0.00	0.00	169.52
	2	21426.78	19581.56	0.00	0.00	0.00	32520.97
	3	21747.14	19874.30	0.00	-0.01	0.01	33004.76
	4	21656.23	19791.24	-35.89	-4264.39	2204.37	32868.27
	5	0.10	0.09	0.00	-0.01	0.00	0.15



MEMBER END FORCES     STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	1	1	0.00	0.00	0.00	0.00	0.00	-0.03
		2	0.00	581.40	0.00	0.00	0.00	-10465.34
	2	1	0.49	-0.01	0.00	0.00	0.00	-0.16
		2	-0.49	581.41	0.00	0.00	0.00	-10465.63
	3	1	-2.93	0.00	0.00	0.00	0.00	0.03
		2	35.64	581.40	0.00	0.00	0.00	-10465.08
	4	1	2.93	0.00	0.01	0.00	0.00	-0.42
		2	-2.93	581.40	-32.70	0.00	-588.49	-10465.39
	5	1	1.95	0.00	0.00	0.00	0.00	0.00
		2	-1.95	0.00	0.00	0.00	0.00	0.00
2	1	2	0.00	-1321.40	0.00	0.00	0.00	10465.23
		3	0.00	3162.50	0.00	0.00	0.00	-266047.50
		2	0.00	-1321.40	0.00	0.00	0.00	10465.15
	2	3	0.00	3162.50	0.00	0.00	0.00	-266047.50
		3	-74.22	-1321.40	0.00	0.00	0.00	10465.20
	3	2	177.73	3162.50	0.00	0.00	0.00	-266047.50
		3	0.00	-1321.40	74.70	0.00	588.75	10465.25
	4	2	0.00	3162.50	-178.21	0.00	-15002.89	-266047.44
		3	0.00	0.00	0.00	0.00	0.00	0.00
	5	2	-0.49	0.00	0.00	0.00	0.00	0.00
3		0.49	0.00	0.00	0.00	0.00	0.00	
3	1	3	0.00	457.24	0.00	0.00	0.00	266047.53
		4	0.00	2255.96	0.00	0.00	0.00	-417139.16
	2	3	0.49	457.24	0.01	-0.30	1.46	266047.47
		4	-0.49	2255.96	-0.01	0.30	-3.82	-417139.13
	3	3	-178.22	457.24	-0.02	-0.04	2.89	266047.50
		4	330.57	2255.96	0.02	0.04	-0.19	-417139.09
	4	3	-0.49	457.24	67.66	-1233.42	14995.23	266047.47
		4	0.49	2255.96	-220.20	1233.42	-39175.46	-417139.16
	5	3	0.00	0.00	0.01	-0.24	2.37	0.00
		4	0.00	0.00	-0.01	0.24	-3.81	0.00
4	1	4	0.00	4270.40	0.00	0.00	0.00	417139.16
		5	0.00	-2235.50	0.00	0.00	0.00	-7267.55
	2	4	38130.37	4270.40	0.00	0.00	0.23	417139.16
		5	-38130.37	-2235.50	0.00	0.00	-0.11	-7267.49
	3	4	38369.63	4270.40	0.00	0.02	0.59	417139.13
		5	-38255.37	-2235.50	0.00	-0.02	-0.11	-7267.50
	4	4	38129.88	4270.40	-239.63	-0.01	23396.63	417139.16
		5	-38129.88	-2235.50	125.22	0.01	-410.18	-7267.50
	5	4	0.00	0.00	-0.02	0.00	2.59	0.00
		5	0.00	0.00	0.02	0.00	-0.29	0.00
5	1	5	0.00	484.49	0.00	0.00	0.00	7267.37
		6	0.00	0.01	0.00	0.00	0.00	0.08

MEMBER END FORCES . STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z	
2	5	5	1.95	484.50	0.00	-0.02	0.06	7267.50	
		6	-1.95	0.00	0.00	0.02	-0.08	-0.04	
	3	5	27.83	484.50	0.00	0.02	0.17	7267.52	
		6	-0.49	0.00	0.00	-0.02	-0.03	-0.05	
	4	5	-0.49	484.50	-27.34	-0.02	409.81	7267.50	
		6	0.49	0.00	0.10	0.02	1.07	-0.04	
5	5	1.95	0.00	-0.02	0.00	0.29	0.00		
	6	-1.95	0.00	0.02	0.00	0.23	0.00		
6	1	3	0.00	-1809.87	0.00	0.00	0.00	-69906.29	
		7	0.00	1809.87	0.00	0.00	0.00	0.02	
	2	3	0.01	-1809.87	0.04	0.00	-1.51	-69906.16	
		7	-0.01	1809.87	-0.04	0.00	0.41	0.00	
	3	3	0.00	-1809.87	0.04	0.00	0.01	-69906.28	
		7	0.00	1809.87	-0.04	0.00	-0.10	0.00	
	4	3	-55.36	-1793.91	-0.03	0.00	0.98	-69289.60	
		7	55.36	1793.91	0.03	0.00	1.41	0.01	
	5	3	0.02	0.00	0.05	0.00	-1.95	0.12	
		7	-0.02	0.00	-0.05	0.00	-0.01	0.00	
	7	1	4	0.00	-3263.18	0.00	0.00	0.01	-126040.25
			11	0.00	3263.18	0.00	0.00	0.01	-0.02
2		4	0.00	-3263.18	-19064.99	0.00	736386.69	-126040.35	
		11	0.00	3263.18	19064.99	0.00	-1.80	0.02	
3		4	0.00	-3263.18	-19350.11	0.00	747398.69	-126040.27	
		11	0.00	3263.18	19350.11	0.00	-0.87	-0.02	
4		4	-229.99	-3279.14	-19269.24	0.00	744275.00	-126656.92	
		11	229.99	3279.14	19269.24	0.00	-0.69	0.03	
5		4	-0.01	0.00	0.01	0.00	1.79	-0.12	
		11	0.01	0.00	-0.01	0.00	-2.02	0.00	
8		1	3	0.00	-1809.87	0.00	0.00	0.00	-69906.29
			9	0.00	1809.87	0.00	0.00	0.00	0.02
	2	3	-0.01	-1809.88	-0.16	0.00	1.57	-69906.48	
		9	0.01	1809.88	0.16	0.00	3.29	0.00	
	3	3	0.01	-1809.87	0.13	0.00	-0.66	-69906.34	
		9	-0.01	1809.87	-0.13	0.00	-1.84	0.02	
	4	3	55.36	-1825.84	-0.23	0.00	5.13	-70523.03	
		9	-55.36	1825.84	0.23	0.00	4.98	0.01	
	5	3	0.01	0.00	0.06	0.00	-0.05	-0.12	
		9	-0.01	0.00	-0.06	0.00	2.00	0.00	
	9	1	4	0.00	-3263.18	0.00	0.00	-0.01	-126040.23
			14	0.00	3263.18	0.00	0.00	0.00	-0.02
2		4	0.01	-3263.17	19064.91	0.00	-736383.00	-126040.06	
		14	-0.01	3263.17	-19064.91	0.00	0.87	0.00	
3		4	-0.01	-3263.18	19350.14	0.00	-747399.25	-126040.20	
		14	0.01	3263.18	-19350.14	0.00	-0.14	0.01	

MEMBER END FORCES     STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	4	4	229.99	-3247.21	18860.74	0.00	-728496.25	-125423.51
		14	-229.99	3247.21	-18860.74	0.00	0.54	-0.01
	5	4	0.01	0.00	0.01	0.00	-0.55	0.12
		14	-0.01	0.00	-0.01	0.00	0.18	0.00
10	1	8	1809.87	0.00	0.00	0.00	0.00	0.00
		7	-1809.87	0.00	0.00	0.00	0.00	0.00
	2	8	1809.87	0.00	0.00	0.00	0.00	-0.10
		7	-1809.87	0.00	0.00	0.00	0.00	0.00
	3	8	1809.87	0.00	0.00	0.00	0.00	-0.02
		7	-1809.87	0.00	0.00	0.00	0.00	0.00
	4	8	1793.91	-55.29	0.00	0.00	0.00	-3870.62
		7	-1793.91	55.29	0.00	0.00	0.00	0.00
	5	8	0.00	0.00	0.00	0.00	0.00	-0.08
		7	0.00	0.00	0.00	0.00	0.00	0.00
11	1	10	1809.87	0.00	0.00	0.00	0.00	0.00
		9	-1809.87	0.00	0.00	0.00	0.00	0.00
	2	10	1809.88	0.00	0.00	0.00	0.00	-0.10
		9	-1809.88	0.00	0.00	0.00	0.00	0.00
	3	10	1809.87	0.00	0.00	0.00	0.00	-0.02
		9	-1809.87	0.00	0.00	0.00	0.00	0.00
	4	10	1825.84	-55.29	0.00	0.00	0.00	-3870.62
		9	-1825.84	55.29	0.00	0.00	0.00	0.00
	5	10	0.00	0.00	0.00	0.00	0.00	-0.08
		9	0.00	0.00	0.00	0.00	0.00	0.00
12	1	12	3263.17	0.00	0.00	0.00	0.00	0.00
		11	-3263.17	0.00	0.00	0.00	0.00	0.00
	2	12	3263.19	0.00	19065.08	0.00	-171585.75	0.00
		11	-3263.19	0.00	-19065.08	0.00	0.00	0.00
	3	12	3263.16	0.00	19350.21	0.00	-174151.81	-0.01
		11	-3263.16	0.00	-19350.21	0.00	0.00	0.00
	4	12	3279.16	-229.90	19269.28	0.00	-173423.52	-2069.08
		11	-3279.16	229.90	-19269.28	0.00	0.00	0.00
	5	12	0.00	0.00	0.15	0.00	-1.39	0.00
		11	0.00	0.00	-0.15	0.00	0.00	0.00
13	1	13	3257.23	0.00	-4.22	0.00	258.77	0.00
		12	-3257.23	0.00	4.22	0.00	-1.37	0.00
	2	13	-16318.38	0.00	-2361.71	0.00	42796.62	-0.01
		12	16318.38	0.00	2361.71	0.00	101267.85	0.00
	3	13	-16611.12	0.00	-2396.97	0.00	43432.74	-0.04
		12	16611.12	0.00	2396.97	0.00	102782.24	0.00
	4	13	-16512.10	-194.01	-2386.98	379.88	43253.45	-11828.66
		12	16512.10	194.01	2386.98	-379.88	102352.40	-5.85
	5	13	-0.09	0.00	-0.01	0.00	0.20	-0.02
		12	0.09	0.00	0.01	0.00	0.48	0.00

## MEMBER END FORCES . STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
14	1	15	3263.17	0.00	0.00	0.00	0.00	0.00
		14	-3263.17	0.00	0.00	0.00	0.00	0.00
	2	15	3263.17	0.00	19064.98	0.00	-171584.78	0.00
		14	-3263.17	0.00	-19064.98	0.00	0.00	0.00
	3	15	3263.18	0.00	19350.17	0.00	-174151.56	-0.01
		14	-3263.18	0.00	-19350.17	0.00	0.00	0.00
	4	15	3247.21	-229.90	18860.77	0.00	-169746.97	-2069.08
		14	-3247.21	229.90	-18860.77	0.00	0.00	0.00
	5	15	0.00	0.00	-0.01	0.00	0.08	0.00
		14	0.00	0.00	0.01	0.00	0.00	0.00
15	1	16	3257.23	0.00	-4.22	0.00	258.77	0.00
		15	-3257.23	0.00	4.22	0.00	-1.37	0.00
	2	16	-16318.28	0.00	-2361.70	0.00	42796.38	-0.01
		15	16318.28	0.00	2361.70	0.00	101267.29	0.00
	3	16	-16611.11	0.00	-2396.97	0.00	43432.71	-0.04
		15	16611.11	0.00	2396.97	0.00	102782.19	0.00
	4	16	-16124.54	-194.01	-2336.43	379.88	42339.50	-11828.66
		15	16124.54	194.01	2336.43	-379.88	100182.63	-5.85
	5	16	-0.01	0.00	0.00	0.00	0.02	-0.02
		15	0.01	0.00	0.00	0.00	0.05	0.00
16	1	18	7.06	1.81	0.00	0.00	0.00	169.52
		12	-7.06	-1.81	0.00	0.00	0.00	1.37
	2	18	29006.15	1089.78	0.00	0.00	0.00	32520.97
		12	-29006.15	-1089.78	0.00	0.00	0.00	70317.77
	3	18	29439.81	1106.05	0.00	-0.01	0.01	33004.76
		12	-29439.81	-1106.05	0.00	0.01	0.00	71369.30
	4	18	29316.76	1101.44	-35.89	-1828.72	4438.47	32868.27
		12	-29316.76	-1101.44	35.89	1828.72	-1051.45	71070.84
	5	18	0.14	0.01	0.00	0.00	0.01	0.15
		12	-0.14	-0.01	0.00	0.00	0.00	0.34
17	1	17	7.06	1.81	0.00	0.00	0.00	169.52
		15	-7.06	-1.81	0.00	0.00	0.00	1.37
	2	17	29005.99	1089.78	0.00	0.00	0.00	32520.79
		15	-29005.99	-1089.78	0.00	0.00	0.00	70317.38
	3	17	29439.79	1106.05	0.00	-0.01	0.01	33004.74
		15	-29439.79	-1106.05	0.00	0.01	0.00	71369.26
	4	17	28695.36	1078.11	-35.89	-1828.72	4438.47	32173.45
		15	-28695.36	-1078.11	35.89	1828.72	-1051.45	69564.24
	5	17	0.02	0.00	0.00	0.00	0.01	0.02
		15	-0.02	0.00	0.00	0.00	0.00	0.04

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

87. PRINT MEMBER STRESSES ALL

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z	
1	1	.0	0.0 T	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 T	0.0	10.2	10.2	17.0	0.0	
	2	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	10.2	10.2	17.0	0.0	
	3	.0	0.1 T	0.0	0.0	0.1	0.0	0.0	
		1.00	0.6 T	0.0	10.2	10.8	17.0	0.0	
	4	.0	0.1 C	0.0	0.0	0.1	0.0	0.0	
		1.00	0.1 C	0.6	10.2	10.2	17.0	1.0	
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0	
	2	1	.0	0.0 T	0.0	10.2	10.2	38.7	0.0
			1.00	0.0 T	0.0	258.7	258.7	92.6	0.0
		2	.0	0.0	0.0	10.2	10.2	38.7	0.0
			1.00	0.0	0.0	258.7	258.7	92.6	0.0
		3	.0	1.3 T	0.0	10.2	11.5	38.7	0.0
1.00			3.1 T	0.0	258.7	261.8	92.6	0.0	
4		.0	0.0	0.6	10.2	10.2	38.7	2.2	
		1.00	0.0	14.6	258.7	259.1	92.6	5.2	
5		.0	0.0 T	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 T	0.0	0.0	0.0	0.0	0.0	
3		1	.0	0.0 T	0.0	258.7	258.7	13.4	0.0
			1.00	0.0 T	0.0	405.6	405.6	66.0	0.0
		2	.0	0.0 C	0.0	258.7	258.7	13.4	0.0
			1.00	0.0 C	0.0	405.6	405.6	66.0	0.0
		3	.0	3.1 T	0.0	258.7	261.8	13.4	0.0
	1.00		5.8 T	0.0	405.6	411.4	66.0	0.0	
	4	.0	0.0 T	14.6	258.7	259.1	13.4	2.0	
		1.00	0.0 T	38.1	405.6	407.4	66.0	6.4	
	5	.0	0.0	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0	0.0	0.0	0.0	0.0	0.0	
	4	1	.0	0.0 T	0.0	405.6	405.6	125.0	0.0
			1.00	0.0 T	0.0	7.1	7.1	65.4	0.0
		2	.0	669.6 C	0.0	405.6	1075.2	125.0	0.0
			1.00	669.6 C	0.0	7.1	676.7	65.4	0.0
		3	.0	673.8 C	0.0	405.6	1079.4	125.0	0.0
1.00			671.8 C	0.0	7.1	678.9	65.4	0.0	
4		.0	669.6 C	22.7	405.6	1075.8	125.0	7.0	
		1.00	669.6 C	0.4	7.1	676.7	65.4	3.7	
5		.0	0.0	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0	0.0	0.0	0.0	0.0	0.0	
5		1	.0	0.0 T	0.0	7.1	7.1	14.2	0.0
			1.00	0.0 T	0.0	0.0	0.0	0.0	0.0
		2	.0	0.0 C	0.0	7.1	7.1	14.2	0.0
			1.00	0.0 C	0.0	0.0	0.0	0.0	0.0

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z	
		3	.0	0.5 C	0.0	7.1	7.6	14.2	0.0
			1.00	0.0 C	0.0	0.0	0.0	0.0	0.0
		4	.0	0.0 T	0.4	7.1	7.1	14.2	0.8
			1.00	0.0 T	0.0	0.0	0.0	0.0	0.0
		5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0
			1.00	0.0 C	0.0	0.0	0.0	0.0	0.0
6	1	.0	0.0 T	0.0	618.6	618.6	129.3	0.0	
		1.00	0.0 T	0.0	0.0	0.0	129.3	0.0	
	2	.0	0.0 C	0.0	618.6	618.7	129.3	0.0	
		1.00	0.0 C	0.0	0.0	0.0	129.3	0.0	
	3	.0	0.0 T	0.0	618.6	618.6	129.3	0.0	
		1.00	0.0 T	0.0	0.0	0.0	129.3	0.0	
	4	.0	2.1 T	0.0	613.2	615.3	128.1	0.0	
		1.00	2.1 T	0.0	0.0	2.1	128.1	0.0	
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0	
7	1	.0	0.0 C	0.0	1115.4	1115.4	233.1	0.0	
		1.00	0.0 C	0.0	0.0	0.0	233.1	0.0	
	2	.0	0.0 T	6516.7	1115.4	7632.1	233.1	1361.8	
		1.00	0.0 T	0.0	0.0	0.0	233.1	1361.8	
	3	.0	0.0 C	6614.1	1115.4	7729.5	233.1	1382.2	
		1.00	0.0 C	0.0	0.0	0.0	233.1	1382.2	
	4	.0	8.7 T	6586.5	1120.9	7716.1	234.2	1376.4	
		1.00	8.7 T	0.0	0.0	8.7	234.2	1376.4	
	5	.0	0.0 T	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 T	0.0	0.0	0.0	0.0	0.0	
8	1	.0	0.0 T	0.0	618.6	618.6	129.3	0.0	
		1.00	0.0 T	0.0	0.0	0.0	129.3	0.0	
	2	.0	0.0 T	0.0	618.6	618.7	129.3	0.0	
		1.00	0.0 T	0.0	0.0	0.0	129.3	0.0	
	3	.0	0.0 C	0.0	618.6	618.6	129.3	0.0	
		1.00	0.0 C	0.0	0.0	0.0	129.3	0.0	
	4	.0	2.1 C	0.0	624.1	626.2	130.4	0.0	
		1.00	2.1 C	0.0	0.0	2.1	130.4	0.0	
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0	
9	1	.0	0.0 T	0.0	1115.4	1115.4	233.1	0.0	
		1.00	0.0 T	0.0	0.0	0.0	233.1	0.0	
	2	.0	0.0 C	6516.7	1115.4	7632.1	233.1	1361.8	
		1.00	0.0 C	0.0	0.0	0.0	233.1	1361.8	
	3	.0	0.0 T	6614.2	1115.4	7729.6	233.1	1382.2	
		1.00	0.0 T	0.0	0.0	0.0	233.1	1382.2	
	4	.0	8.7 C	6446.9	1109.9	7565.5	231.9	1347.2	
		1.00	8.7 C	0.0	0.0	8.7	231.9	1347.2	
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0	

MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
10	1	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	2	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	3	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	4	.0	888.1 C	0.0	1984.9	2873.0	36.9	0.0
		1.00	888.1 C	0.0	0.0	888.1	36.9	0.0
	5	.0	0.0 T	0.0	0.0	0.0	0.0	0.0
1.00		0.0 T	0.0	0.0	0.0	0.0	0.0	
11	1	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	2	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	3	.0	896.0 C	0.0	0.0	896.0	0.0	0.0
		1.00	896.0 C	0.0	0.0	896.0	0.0	0.0
	4	.0	903.9 C	0.0	1984.9	2888.8	36.9	0.0
		1.00	903.9 C	0.0	0.0	903.9	36.9	0.0
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0
1.00		0.0 C	0.0	0.0	0.0	0.0	0.0	
12	1	.0	513.1 C	0.0	0.0	513.1	0.0	0.0
		1.00	513.1 C	0.0	0.0	513.1	0.0	0.0
	2	.0	513.1 C	27900.1	0.0	28413.2	0.0	4766.3
		1.00	513.1 C	0.0	0.0	513.1	0.0	4766.3
	3	.0	513.1 C	28317.4	0.0	28830.4	0.0	4837.6
		1.00	513.1 C	0.0	0.0	513.1	0.0	4837.6
	4	.0	515.6 C	28198.9	336.4	29051.0	57.5	4817.3
		1.00	515.6 C	0.0	0.0	515.6	57.5	4817.3
	5	.0	0.0 C	0.2	0.0	0.2	0.0	0.0
1.00		0.0 C	0.0	0.0	0.0	0.0	0.0	
13	1	.0	512.1 C	42.1	0.0	554.2	0.0	1.1
		1.00	512.1 C	0.2	0.0	512.4	0.0	1.1
	2	.0	2565.8 T	6958.8	0.0	9524.6	0.0	590.4
		1.00	2565.8 T	16466.3	0.0	19032.1	0.0	590.4
	3	.0	2611.8 T	7062.2	0.0	9674.1	0.0	599.2
		1.00	2611.8 T	16712.6	0.0	19324.4	0.0	599.2
	4	.0	2596.2 T	7033.1	1923.4	11552.7	48.5	596.7
		1.00	2596.2 T	16642.7	1.0	19239.9	48.5	596.7
	5	.0	0.0 T	0.0	0.0	0.0	0.0	0.0
1.00		0.0 T	0.1	0.0	0.1	0.0	0.0	
14	1	.0	513.1 C	0.0	0.0	513.1	0.0	0.0
		1.00	513.1 C	0.0	0.0	513.1	0.0	0.0
	2	.0	513.1 C	27900.0	0.0	28413.0	0.0	4766.2
		1.00	513.1 C	0.0	0.0	513.1	0.0	4766.2



MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
	3	.0	513.1 C	28317.3	0.0	28830.4	0.0	4837.5
		1.00	513.1 C	0.0	0.0	513.1	0.0	4837.5
	4	.0	510.6 C	27601.1	336.4	28448.1	57.5	4715.2
		1.00	510.6 C	0.0	0.0	510.6	57.5	4715.2
	5	.0	0.0 T	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 T	0.0	0.0	0.0	0.0	0.0
15	1	.0	512.1 C	42.1	0.0	554.2	0.0	1.1
		1.00	512.1 C	0.2	0.0	512.4	0.0	1.1
	2	.0	2565.8 T	6958.8	0.0	9524.5	0.0	590.4
		1.00	2565.8 T	16466.2	0.0	19032.0	0.0	590.4
	3	.0	2611.8 T	7062.2	0.0	9674.0	0.0	599.2
		1.00	2611.8 T	16712.6	0.0	19324.4	0.0	599.2
	4	.0	2535.3 T	6884.5	1923.4	11343.1	48.5	584.1
		1.00	2535.3 T	16289.9	1.0	18826.1	48.5	584.1
	5	.0	0.0 T	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 T	0.0	0.0	0.0	0.0	0.0
16	1	.0	1.1 C	0.0	27.6	28.7	0.5	0.0
		1.00	1.1 C	0.0	0.2	1.3	0.5	0.0
	2	.0	4560.7 C	0.0	5288.0	9848.7	272.4	0.0
		1.00	4560.7 C	0.0	11433.8	15994.5	272.4	0.0
	3	.0	4628.9 C	0.0	5366.6	9995.5	276.5	0.0
		1.00	4628.9 C	0.0	11604.8	16233.7	276.5	0.0
	4	.0	4609.6 C	721.7	5344.4	10675.7	275.4	9.0
		1.00	4609.6 C	171.0	11556.2	16336.8	275.4	9.0
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 C	0.0	0.1	0.1	0.0	0.0
17	1	.0	1.1 C	0.0	27.6	28.7	0.5	0.0
		1.00	1.1 C	0.0	0.2	1.3	0.5	0.0
	2	.0	4560.7 C	0.0	5287.9	9848.6	272.4	0.0
		1.00	4560.7 C	0.0	11433.7	15994.4	272.4	0.0
	3	.0	4628.9 C	0.0	5366.6	9995.5	276.5	0.0
		1.00	4628.9 C	0.0	11604.8	16233.7	276.5	0.0
	4	.0	4511.8 C	721.7	5231.5	10465.0	269.5	9.0
		1.00	4511.8 C	171.0	11311.3	15994.1	269.5	9.0
	5	.0	0.0 C	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

- 88. PARAMETER
- 89. CODE AISC
- 90. PUNCH 3. MEMB 12 TO 17
- 91. FYLD 45999.969 MEMB 10 TO 17
- 92. WSTR 21000. MEMB 10 TO 17

B-9 BEAM TUBE MANIFOLD SUPPORT

-- PAGE NO. 20

- 93. WMIN 0.188 MEMB 10 TO 17
- 94. CB 1. MEMB 10 TO 17
- 95. GMY 1. MEMB 10 TO 17.
- 96. MAIN 0. MEMB 10 TO 17
- 97. RATIO 1. MEMB 10 TO 17
- 98. CHECK CODE MEMB 10 TO 17

STAAD-III CODE CHECKING - (AISC)  
 \*\*\*\*\*

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
10	ST TUB 40203	PASS 1793.91 C	AISC- H1-3 0.00	0.125 -3870.62	4 0.00
11	ST TUB 40203	PASS 1825.84 C	AISC- H1-3 0.00	0.126 -3870.62	4 0.00
* 12	ST TUB 40408	FAIL 3279.16 C	AISC- H1-3 -173423.52	1.053** -2069.08	4 0.00
13	ST TUB 40408	PASS 16611.12 T	AISC- H2-1 102782.24	0.700 0.00	3 61.00
* 14	ST TUB 40408	FAIL 3263.18 C	AISC- H1-3 -174151.56	1.045** -0.01	3 0.00
15	ST TUB 40408	PASS 16611.11 T	AISC- H2-1 102782.19	0.700 0.00	3 61.00
16	ST TUB 40408	PASS 29316.76 C	AISC- H1-1 -1051.45	0.652 71070.84	4 94.37
17	ST TUB 40408	PASS 29439.79 C	AISC- H1-1 0.00	0.647 71369.26	3 94.37
99. SELECT WELD MEMB 10 TO 17					

\*\* NOTE: STRESS RATIO IS ACCEPTABLE BASED ON CONSERVATIVE LOADING. APPLIED LOAD DOES NOT TAKE INTO ACCOUNT STIFFENER RINGS BEHAVIOR DURING LOADING. ADDITIONALLY ACCEPTANCE RATIO CAN BE INCREASED BY 1.33 DUE TO SEISMIC LOAD CONDITION.

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
10	STA 4	1 0.00	3/16 24.58	2345.67 2345.54
10	END 3	1 0.00	3/16 0.00	804.39 804.39
11	STA 4	1 0.00	3/16 24.58	2359.86 2359.73
11	END 4	1 0.00	3/16 24.58	811.86 811.48
12	STA 4	1 2752.75	7/16 32.84	19466.87 19271.23
12	END 3	1 6450.07	3/16 0.00	6541.14 1087.72
13	STA 4	1 843.15	3/16 112.15	19293.32 19274.56
13	END 3	1 479.39	5/16 0.00	18745.69 18739.56
14	STA 3	1 2764.31	7/16 0.00	19324.00 19125.27
14	END 3	1 6450.06	3/16 0.00	6541.13 1087.73
15	STA 4	1 826.29	3/16 112.15	18935.26 18916.89
15	END 3	1 479.39	5/16 0.00	18745.68 18739.55
16	STA 4	1 240.55	3/16 595.74	19109.74 19098.94
16	END 4	1 180.42	4/16 446.80	20857.69 20852.12
17	STA 4	1 240.55	3/16 587.96	18728.88 18718.10
17	END 3	1 0.00	4/16 276.51	20743.53 20741.69

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

---

\*\*\*\*\* END OF TABULATED WELD DESIGN \*\*\*\*\*

100. STEEL TAKEOFF

STEEL TAKE-OFF  
-----

PROFILE	LENGTH (INCH)	WEIGHT (POUN)
ST PIP E	474.00	7638.229
ST TUB 1401408	154.50	1154.300
ST TUB 40203	140.00	80.032
ST TUB 40408	328.73	591.679
	-----	-----
	TOTAL =	9464.24

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

101. FINISH

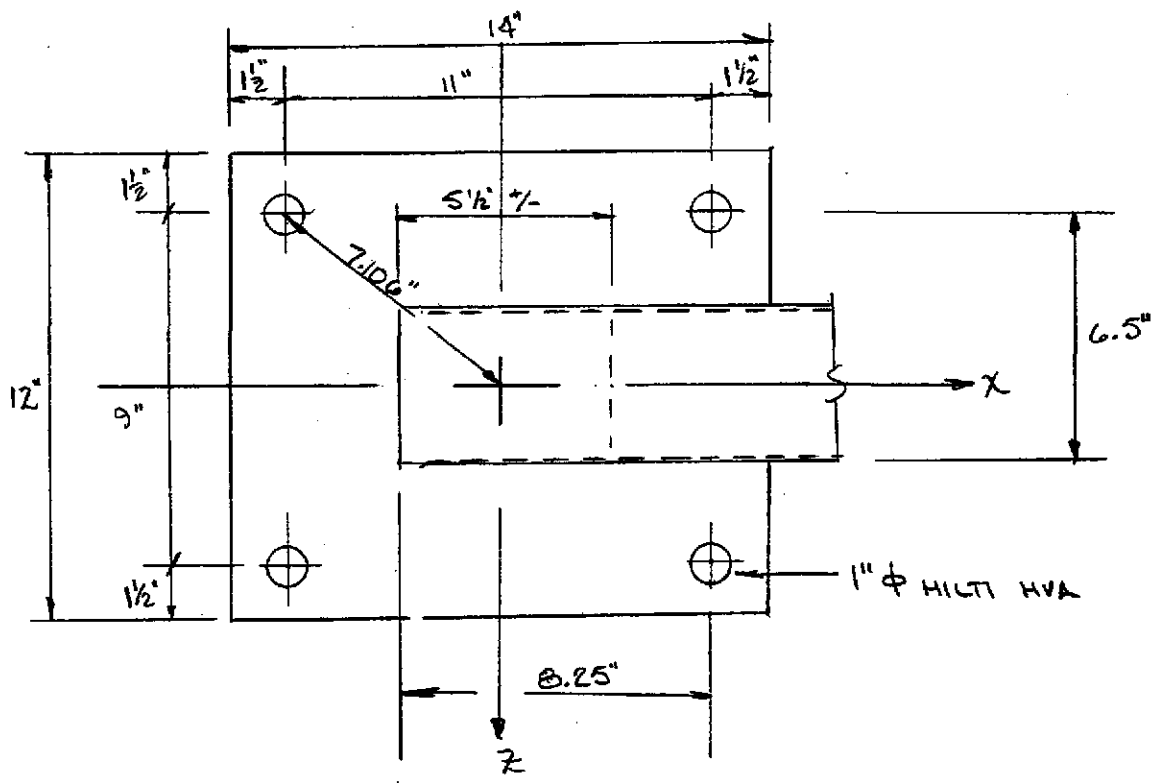
\*\*\*\*\* END OF STAAD-III \*\*\*\*\*

\*\*\*\* DATE= SEP 17,1996 TIME= 14:18:44 \*\*\*\*

\*\*\*\*\*  
\* For questions on STAAD-III, contact: \*  
\* Research Engineers, Inc at \*  
\* Ph: (714) 974-2500 Fax: (714) 921-2543 \*  
\*\*\*\*\*

14" x 12" x 1"

BASEPLATE @ KICKER LEGS. (JOINTS 17/18)



$$F_x = 21656 \text{ lbs}$$

$$M_x = 4264 \text{ in-lbs}$$

$$F_y = 19791 \text{ lbs (compression)}$$

$$M_y = 2204 \text{ in-lbs}$$

$$F_z = 36 \text{ lbs}$$

$$M_z = 32868 \text{ in-lbs}$$

BOLT TENSION

$$T = \frac{4264 \text{ in-lbs}}{(2 \text{ BOLTS})(6.5 \text{ in})} + \frac{32868 \text{ in-lbs}}{(2 \text{ BOLTS})(8.25 \text{ in})}$$

$$= 2320 \text{ lbs/BOLT (1.2)} = 2784 \text{ #/BOLT}$$

↑ PERIOD

BOLT SHEAR

$$V = \frac{21656 \text{ lbs.} + 36 \text{ lbs.}}{4 \text{ BOLTS}} + \frac{2204}{(4 \text{ BOLTS})(7.106 \text{ in})}$$

$$= 5501 \text{ lbs/BOLT.}$$

BOLT INTERACTION

1"  $\phi$  HILTI HVA @ 8 1/4" EMBED

$T_{ALL} = 10960 \text{ lbs.}$      $V_{ALL} = 7630 \text{ lbs.}$

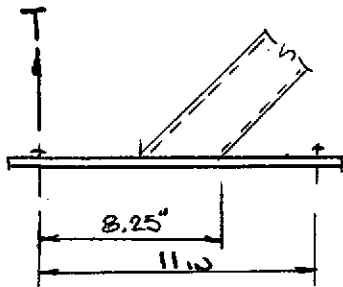
$$\frac{2784 \text{ lbs/BOLT}}{10960 \text{ lbs/BOLT}} + \frac{5501 \text{ lbs/BOLT}}{7630 \text{ lbs/BOLT}} = .975 < 1.0 \text{ : OK}$$

USE 1"  $\phi$  HILTI HVA @ 8 1/4" EMBED

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



BASEPLATE    14" x 12"



$T = 2784 \text{ lbs}$

$F_y = 36000 \text{ */in}^2$

$F_{by} = .75(F_y) = 27000 \text{ */in}^2$

$f_b = \frac{M}{S} = \frac{T(8.25)}{S}$

$S_{REQ'D} = \frac{M}{f_b} = \frac{M}{F_{yb}}$

$S = \frac{(2784 \text{ lbs.})(8.25 \text{ in.})}{27000 \text{ lbs/in}^2} = .851 \text{ in}^3$

$S = \frac{bd^2}{6} \Rightarrow d = \sqrt{\frac{6S}{b}}$

$d = \sqrt{\frac{6(.851 \text{ in}^3)}{11 \text{ in.}}} = .68 \text{ in}$

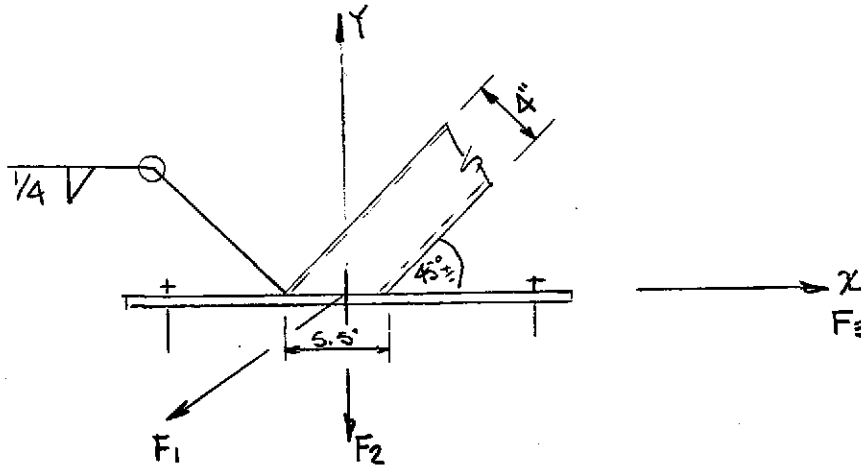
$t = 1 3/8$  will be used

USE 1" THK PL X 14" X 12"



ALL AROUND RECTANGULAR OR SQUARE FILLET WELD

Between part MEM 16 & 17 and BASEPLTS



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
36.00	0.00	21656.00	4264.00	2204.00	32868.00

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)	SKEWED ANGLE (90° < α < 120°)
5.500	4.000	21000	45.000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
19.000	32.083	27.333	142.896	2.750	2.000

EFFECTIVE THROAT CORRECTION FACTOR

Mf  
0.54

MAXIMUM WELD LOAD (f) - #/INCH

f=  
1776

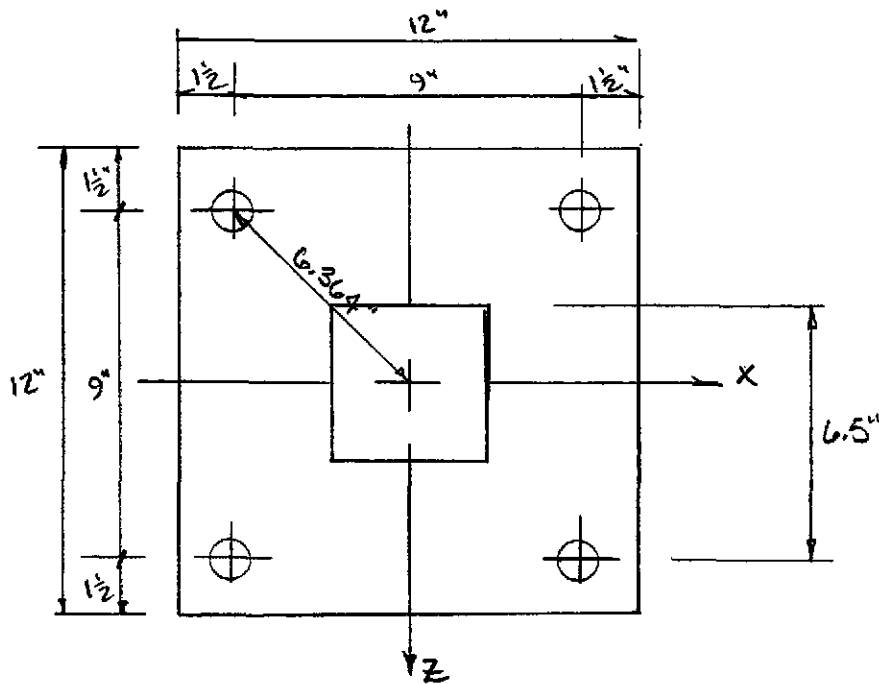
REQUIRED FILLET WELD SIZE (INCHES)

w=  
0.065

*USE 1/4" fillet*

PLATE 12" x 12"

(JOINTS 13 & 16)



$$\begin{aligned} F_x &= 2387. \text{ lbs.} & M_x &= 11829. \text{ in-lbs} \\ F_y &= 16512. \text{ lbs} & M_y &= 380. \text{ in-lbs} \\ F_z &= 194. \text{ lbs} & M_z &= 43253. \text{ in-lbs.} \end{aligned}$$

BOLT TENSION

$$\begin{aligned} T &= \frac{16512 \text{ lbs}}{4 \text{ BOLTS}} + \frac{11829 \text{ in-lbs}}{2(6.5 \text{ in})} + \frac{43253 \text{ in-lbs}}{2(6.5 \text{ in})} \\ &= 4128. + 910. + 3327 \\ &= 8365 \text{ lbs. (1.2) } = 10038. \text{ lbs/BOLT} \\ &\quad \uparrow \text{ PLYING} \end{aligned}$$

BOLT SHEAR

$$\begin{aligned} V &= \frac{2387 + 194}{4 \text{ BOLTS}} + \frac{380}{(4 \text{ BOLTS})(6.364 \text{ in})} \\ &= 660 \text{ lbs/BOLT} \end{aligned}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



BOLT INTERACTION

FOR 1"  $\phi$  HILTI HVA @ 8/4" EMB'D

T<sub>ALL</sub> = 10960 lbs      V<sub>ALL</sub> = 7630 lbs.

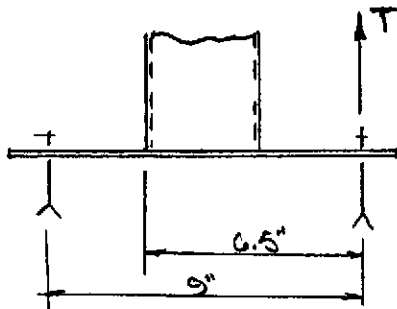
$$\frac{10038}{10960} + \frac{660}{7630} = .91 + .08 \approx 1.0 \approx 1.0 \quad \therefore \text{O.K.}$$

USE

1"  $\phi$  HILTI HVA @ 8/4" EMB'D

BASE PLATE

12" x 12"



$$F_T = 36000$$

$$F_{yb} = .75 (F_y) = 27000 \text{ */in}^2$$

$$f_b = \frac{M}{S} = \frac{T (6.5 \text{ in})}{S}$$

$$S_{REQ'D} = \frac{M}{f_b} = \frac{M}{F_{yb}} = \frac{10038 (6.5 \text{ in})}{27000 \text{ */in}} = 2.42 \text{ in}^3$$

$$S = \frac{bd^2}{6} \Rightarrow d = \sqrt{\frac{6S}{b}}$$

$$= \sqrt{\frac{6 (2.42 \text{ in}^3)}{9 \text{ in}}}$$

$$d = 1.27 \text{ in}$$

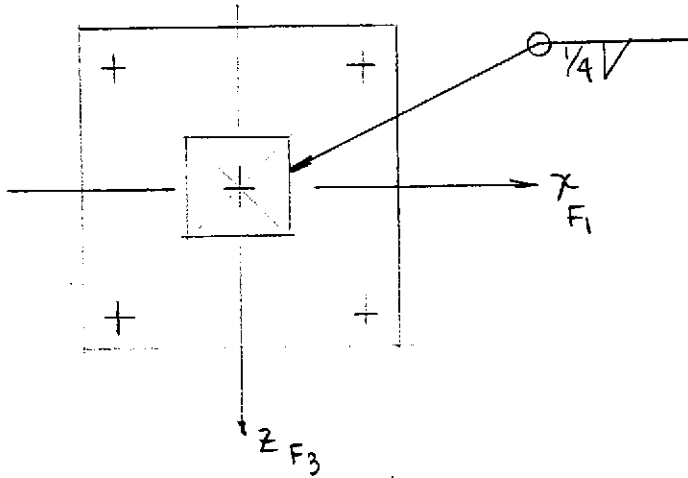
USE PL 1 3/8" THK X 12" X 12"

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



ALL AROUND RECTANGULAR OR SQUARE FILLET WELD

Between part MEM 13 & 15 and BASEPLTS



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
2387.00	16512.00	194.00	11829.00	380.00	43253.00

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)	SKEWED ANGLE (90° < α < 120°)
4.000	4.000	21000	90.000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
16.000	21.333	21.333	85.333	2.000	2.000

EFFECTIVE THROAT CORRECTION FACTOR

Mf  
1.00

MAXIMUM WELD LOAD (f) - #/INCH

f=  
3617

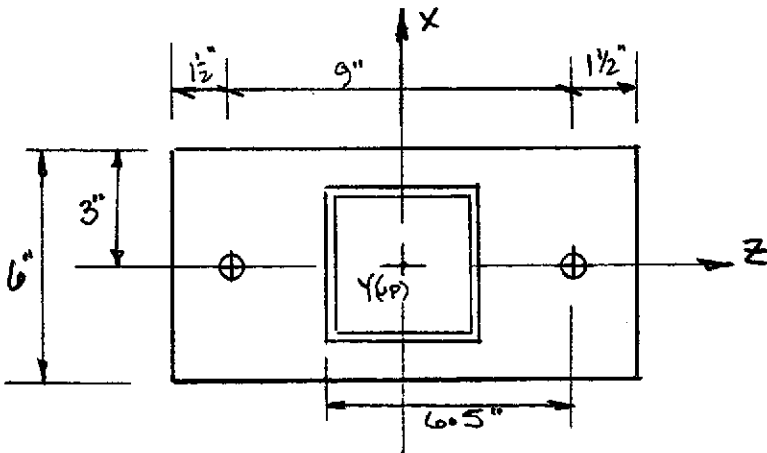
REQUIRED FILLET WELD SIZE (INCHES)

w=  
0.244

*USE 1/4" fillet*

FL 6" x 12"

JTS 8 & 10



1"  $\phi$  HILTI HVA

$T_{ALL} = 10960. \text{ lbs}$

$V_{ALL} = 7630. \text{ lbs}$

ENVELOPE OF LOADS @ JTS 8, 10, 13 & 16 (MEMBERS 10, 11, 13 & 15)

$$\begin{array}{l}
 F_x = 0. \\
 F_y = 1826 \text{ (compression)} \\
 F_z = 55.0 \\
 M_x = 3871. \\
 M_y = 0. \\
 M_z = 0.
 \end{array}$$

BOLT TENSION

$$T = \frac{1826 \text{ lbs}}{2 \text{ BOLTS}} + \frac{3871.10 \text{ lbs}}{(1 \text{ BOLT})(6.5 \text{ in})}$$

$$= 1508.5 \text{ lbs (1.2)} = 1810 \text{ lbs}$$

↑ PULLING

BOLT SHEAR

$$V = \frac{55 \text{ lbs}}{2 \text{ BOLTS}}$$

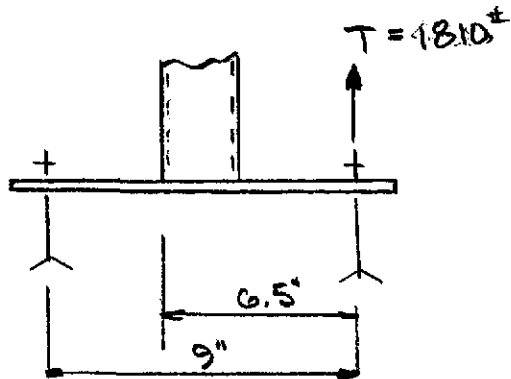
$$= 27.5 \text{ lbs/BOLT}$$

BOLT INTERACTION

$$\frac{1810 \text{ lbs}}{10960. \text{ lbs}} + \frac{27.5 \text{ lbs}}{7630. \text{ lbs}} = .17 < 1.0 \therefore \text{O.K.}$$

USE 1"  $\phi$  HILTI HVA @ 8 1/4" SPAC.

BASEPLATE



$$F_1 = 36000 \text{ psi}$$

$$F_{by} = .75(36000 \text{ psi}) \\ = 27000 \text{ psi}$$

$$f_b = \frac{M}{S} = \frac{T(6.5 \text{ in})}{S}$$

$$S_{req'd} = \frac{M}{f_b} = \frac{M}{F_{by}}$$

$S_{req'd}$

$$S = \frac{1810 \text{ lbs}(6.5 \text{ in})}{27000 \text{ psi}}$$

$$S_{req'd} = 0.436 \text{ in}^3$$

$$S = \frac{bd^2}{6} \Rightarrow d = \sqrt{\frac{6(S)}{b}}$$

$$d = \sqrt{\frac{6(0.436 \text{ in}^3)}{9 \text{ in}}}$$

$$d = .54 \text{ in}$$

**USE 1" THK PLATE x 12" x 6"**

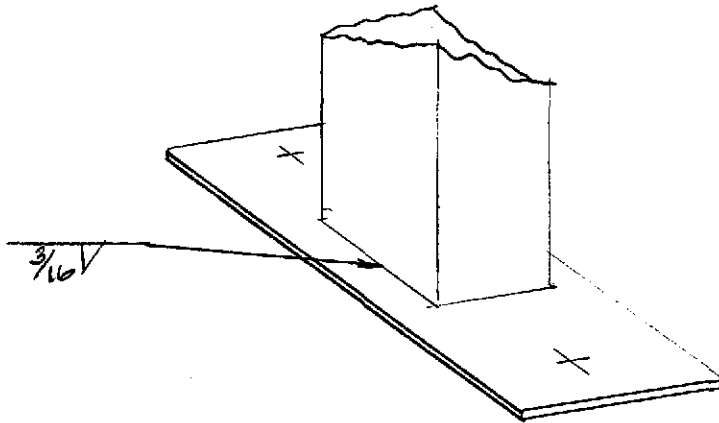
22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



Filename: B-9 SUPPORT

ALL AROUND RECTANGULAR OR SQUARE FILLET WELD

Between part\_ MEM 10 & 11 and BASEPLTS



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
0.00	1826.00	55.00	3871.00	0.00	0.00

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)	SKEWED ANGLE(90°<math>\leq \alpha < 120^\circ </math>)
4.000	4.000	21000	90.000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
16.000	21.333	21.333	85.333	2.000	2.000

EFFECTIVE THROAT CORRECTION FACTOR

Mf  
1.00

MAXIMUM WELD LOAD (f) - #/INCH

f=  
296

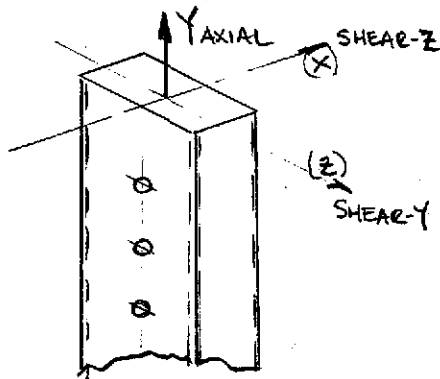
REQUIRED FILLET WELD SIZE (INCHES)

w=  
0.020

*USE 3/16 in fillet all around*

DESIGN BOLTED CONNECTIONS

MEMBER END FORCES @ 10, 11, 12 & 14



ENVELOPE (WORST CASE) LOADS

$$F_y = \text{Axial} = 3279 \quad (\text{MEM 12})$$

$$F_x = \text{Shear-Z} = 19350 \quad (\text{MEM 12/14})$$

$$F_z = \text{Shear-Y} = 230 \quad (\text{MEM 12/14})$$

$$\text{MAX SHEAR} = V_{\text{MAX}} = \frac{3279 \text{ lbs} + 230 \text{ lbs}}{3 \text{ BOLTS}}$$

$$V_{\text{MAX}} = 1170 \text{ #/BOLT}$$

$$\text{MAX TENSION} = T_{\text{MAX}} = 19350 \text{ lbs} / 3 \text{ BOLTS} = 6450 \text{ #/BOLT}$$

USE 5/8" φ A325 BOLTS

$$\text{ALLOWABLE} = V_{\text{MAX}} = 5220 \text{ lbs}$$

$$\text{ALLOWABLE} = T_{\text{MAX}} = 13500 \text{ lbs}$$

BOLT INTERACTION

$$\frac{V_{\text{MAX}}}{V_{\text{MAX ALLOW}}} + \frac{T_{\text{MAX}}}{T_{\text{MAX ALLOW}}} = \frac{1170}{5220} + \frac{6450(1.2) \text{ PRYING}}{13500}$$

$$= 0.80 < 1.0 \therefore \text{OK}$$

NOTE: TO ACCOUNT FOR ANY LOCAL PRYING EFFECTS AT THE BOLTED CONNECTIONS USE 1.2 FACTOR.

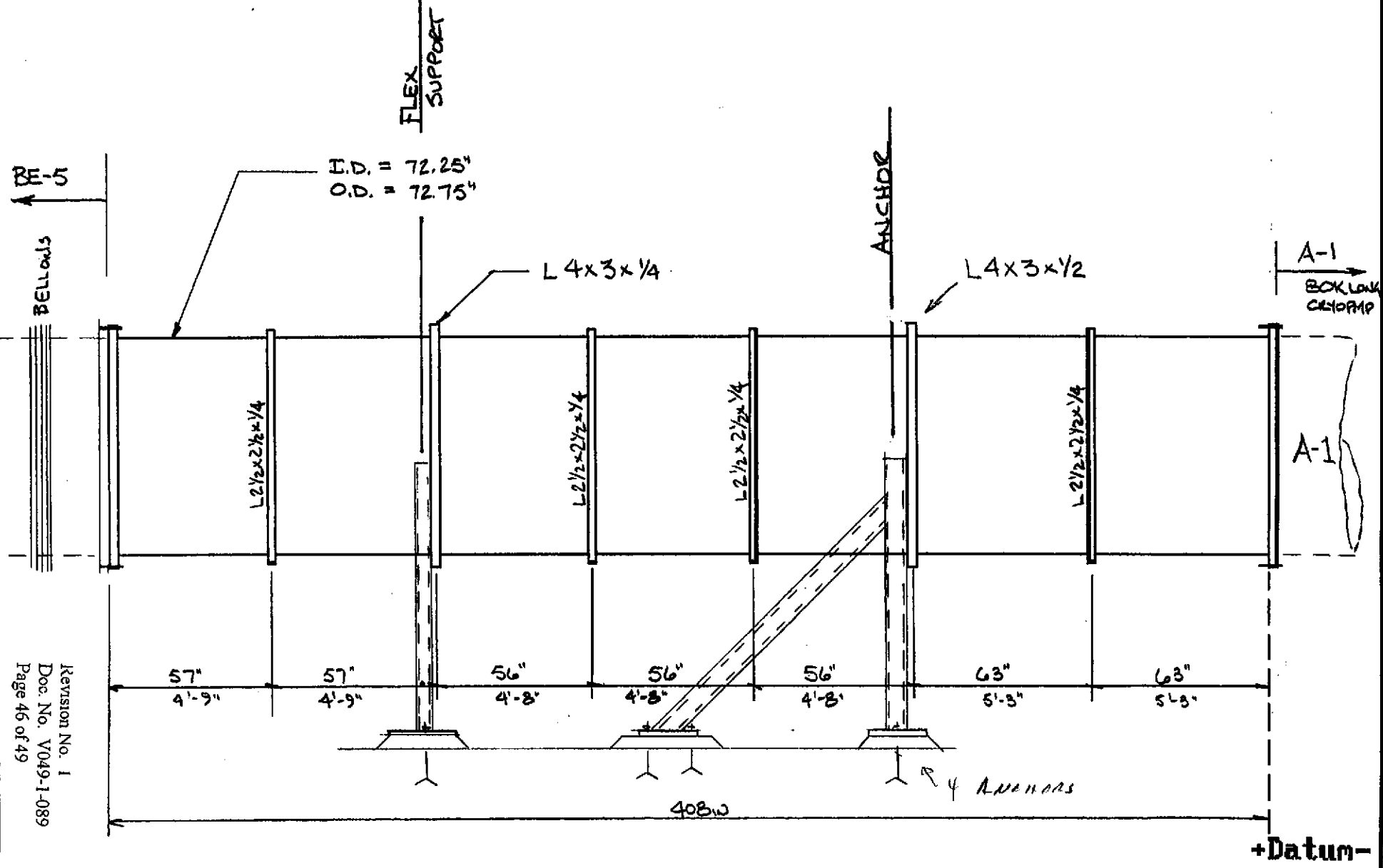
USE 5/8" φ A325 BOLTS

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



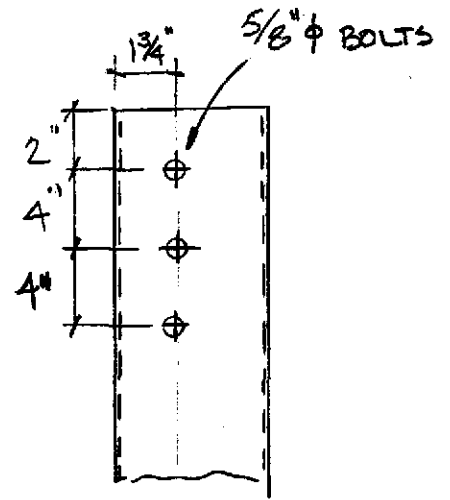
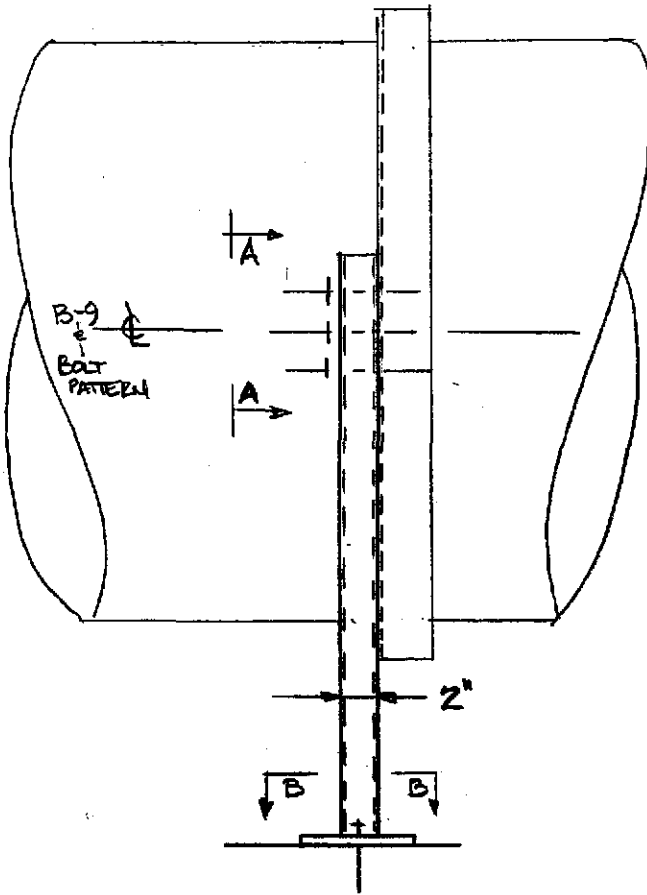
Revision No. 1  
Doc. No. V049-1-089  
Page 45 of 49



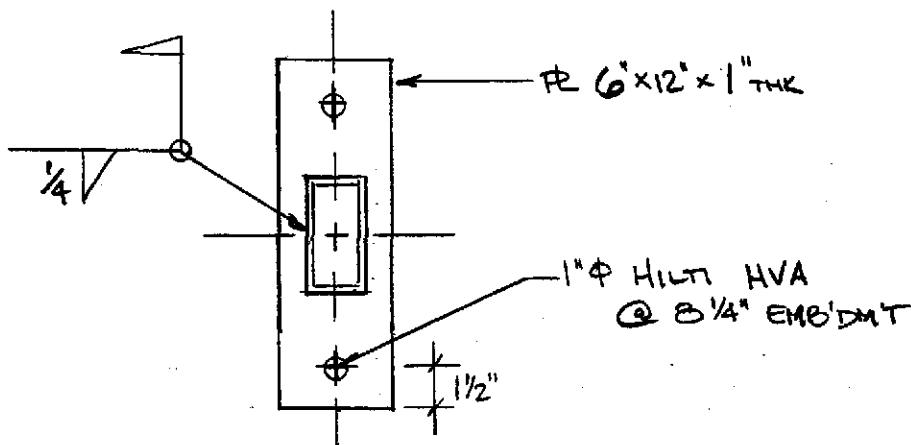


Revision No. 1  
 Doc. No. V049-1-089  
 Page 46 of 49

B-9 FLEX SUPPORT



SECTION A-A



SECTION B-B

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

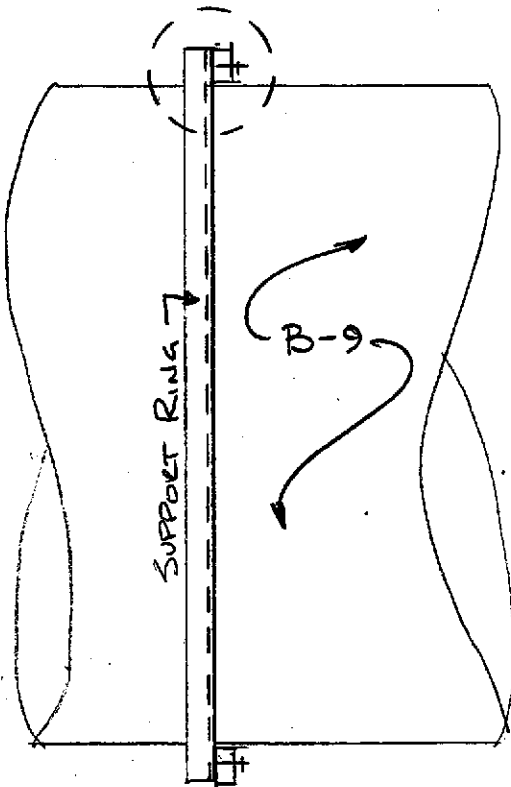


# BEAM TUBE MANIFOLD SUPPORTS

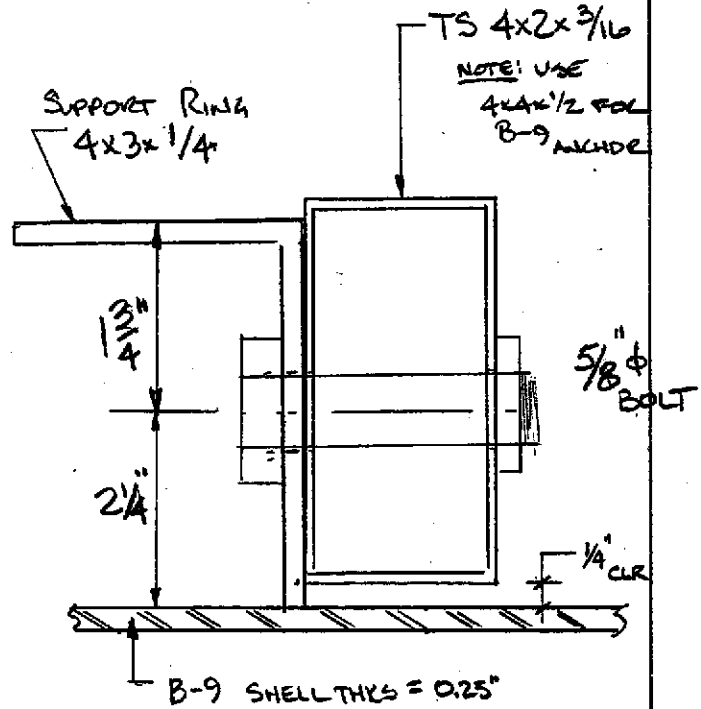
B-9

FLEX SUPPORT

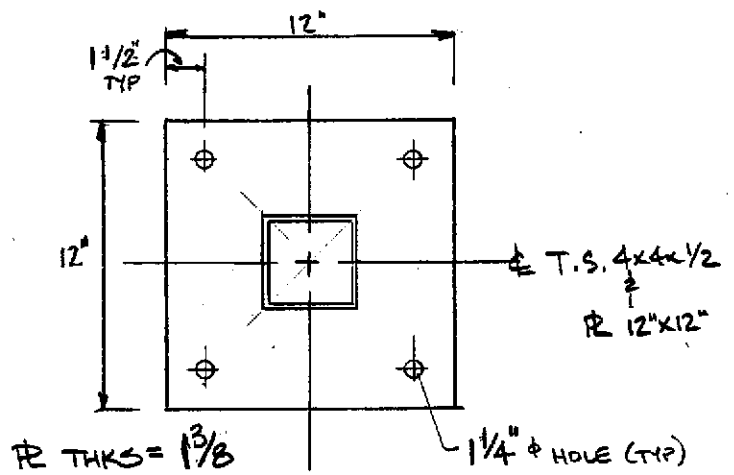
DET 'A'



PLAN VIEW



DETAIL 'A'



SECTION D-D

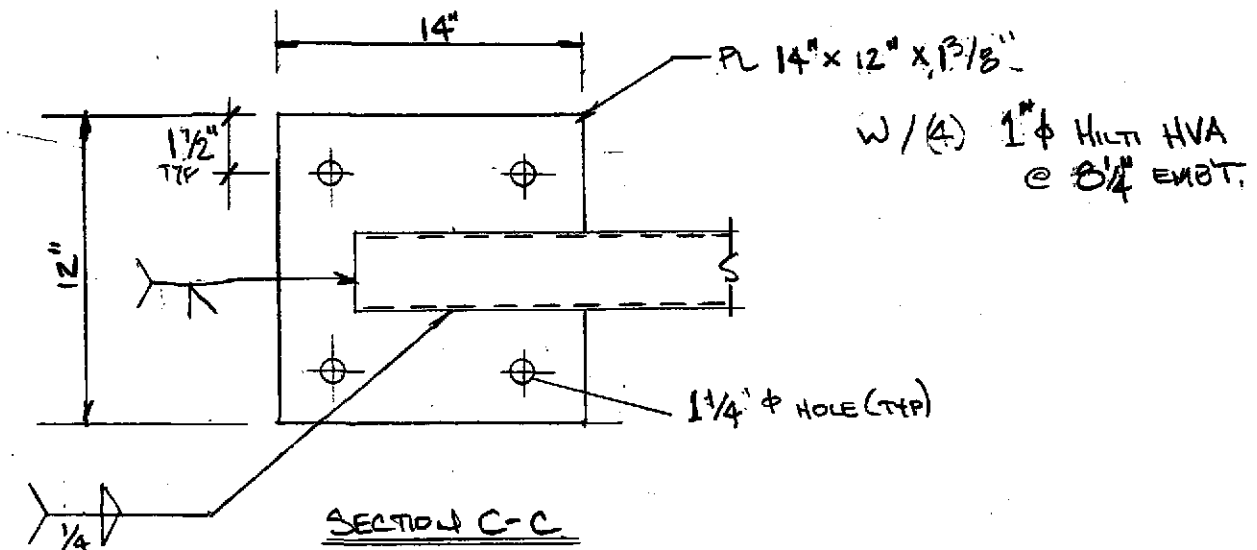
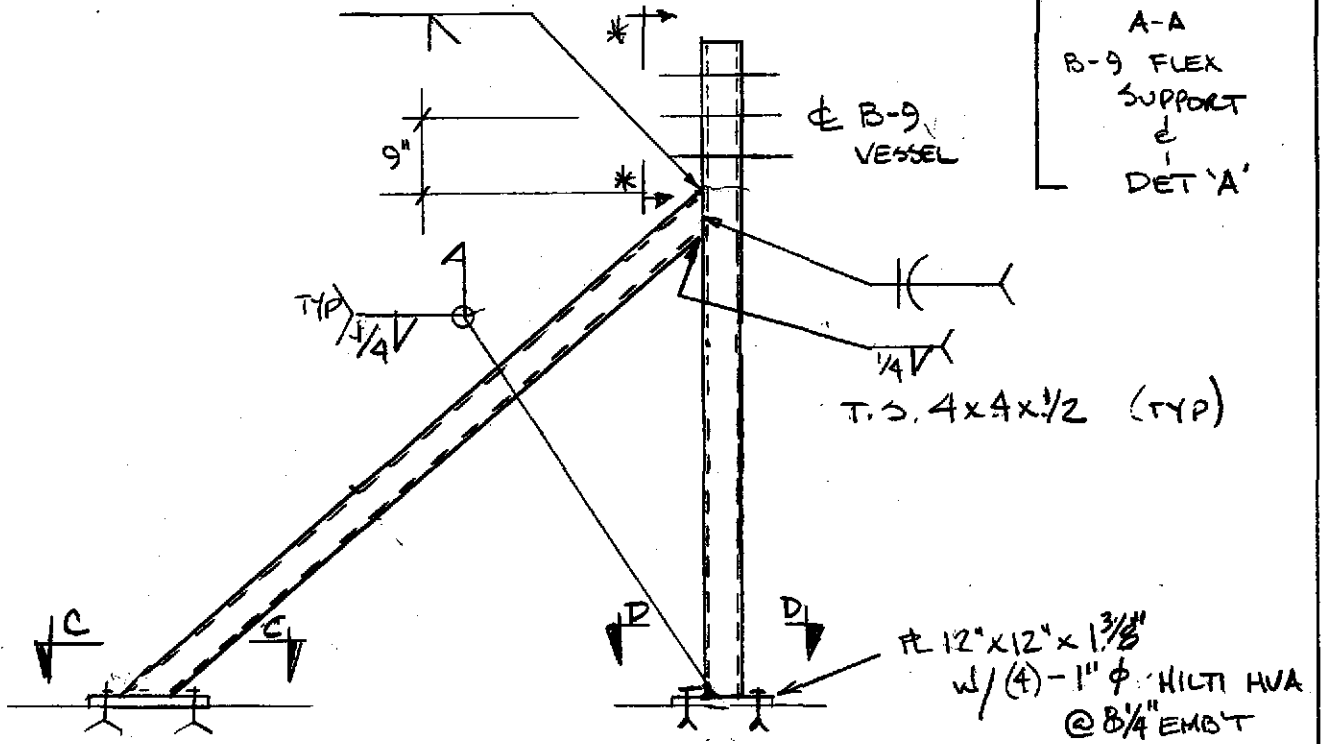
22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



BEAM TUBE MANIFOLD SUPPORTS

B-9 ANCHOR

\* SEE SECTION  
A-A  
B-9 FLEX  
SUPPORT  
DET 'A'



22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

AMIPAD

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-095 PAGE 1 OF 46
REV.	DEO #	DATE	BY:	CHECK	TITLE: Design of Generic Support Scheme for; Beam Tube Manifold B-6 & B-7	
0	0139	4/24/96	WDB	AGR		
1	0293	9/23/96	WDB	ROC		
					BY: W. Bilynsky	DEPT.: 744
<b>PROJECT: LIGO Vacuum Equipment</b>					<b>PROJECT NO: V59049</b>	
<p><b>PURPOSE:</b> The purpose of this calculation is to design a generic support for B-6/B-7 Beam Tube Manifolds (BTM). The design of BTM B-6/B-7 is governed by the gate valve's vacuum load which occurs during system regeneration.</p>						
<p><b>METHOD:</b> A STAAD model of BTM B-6/B-7 was generated and used for design. Baseplates, anchor bolts and thru-bolted connections were designed using AISC standards and STAAD computer output. Load cases included; DW, Thermal, Vacuum and Seismic (static g load). DW included the weight of the vessel and its flanges. Thermal included a temperature load along the length of the vessel. Vacuum loads occur from the gate valves opening/closing. An additional unbalanced vacuum load occurs at the turbo pump nozzle opening.</p>						
<p><b>ASSUMPTIONS</b> See Calculation</p>						
<p><b>INPUTS:</b> Vessel weight = 1083.0 lbs, Flange weight = 253.0 lbs Seismic Acceleration = 0.05625 g. Vacuum Load @ Gate Valve = 32170.0 lbs Vacuum Load @ Turbo Pump = 1155.0 lbs. (B-7)</p>						
<p><b>REFERENCES:</b></p> <ol style="list-style-type: none"> <li>1. STAAD-III release 21, Research Engineers</li> <li>2. ASD - AISC 9th edition</li> <li>3. Doc. No. V049-1-066 - LIGO Vacuum Equipment Structural Design Criteria</li> </ol>						
<p><b>CALCULATIONS:</b></p> <p>V049-1- 058 Design of Spool B-6 V049-1- 059 Design of Spool B-7</p>						
<p><b>CONCLUSIONS:</b> The requirements of the AISC Code and the LIGO Vacuum Equipment Structural Design Criteria are met.</p>						
<p><b>NOTES:</b> STAAD-III Computer file: B67BTMR1.*</p>						

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-095
		Rev. No. 1
		Page 2 of 46
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Design of Generic Support Scheme for Beam Tube Manifold B-6 & B-7		

TABLE OF CONTENTS

Revision History	3
Spool B-6/B-7 (48 in dia) COMPRESS Plot	4
Loading Conditions	6
Input Model (B-6/B-7)	8
STAAD Model	9
STAAD Output File	10
Support Reactions	21
Code Checking	36
Anchorage Design	39
Anchor Bolts	
Baseplates	
Welded Connections @ Baseplate	
Bolted Connections	45
B-6/B-7 Support Detail	46

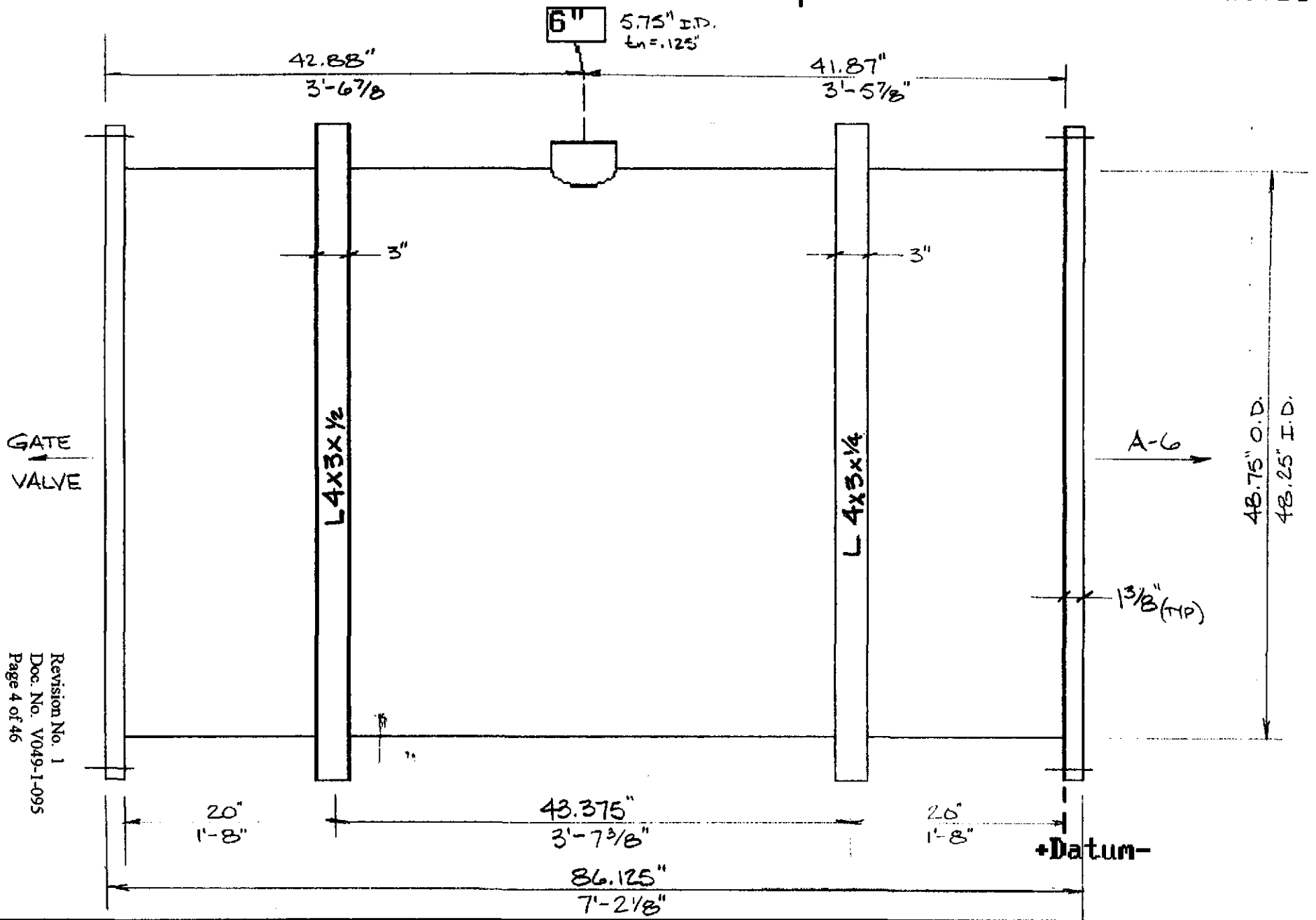
PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-095
		Rev. No. 1
		PAGE 3 OF 46
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Design of Generic Support Scheme for Beam Tube Manifolds B-6 & B-7		

### REVISION HISTORY

Rev. 0            Original Issue  
                         April 24, 1996

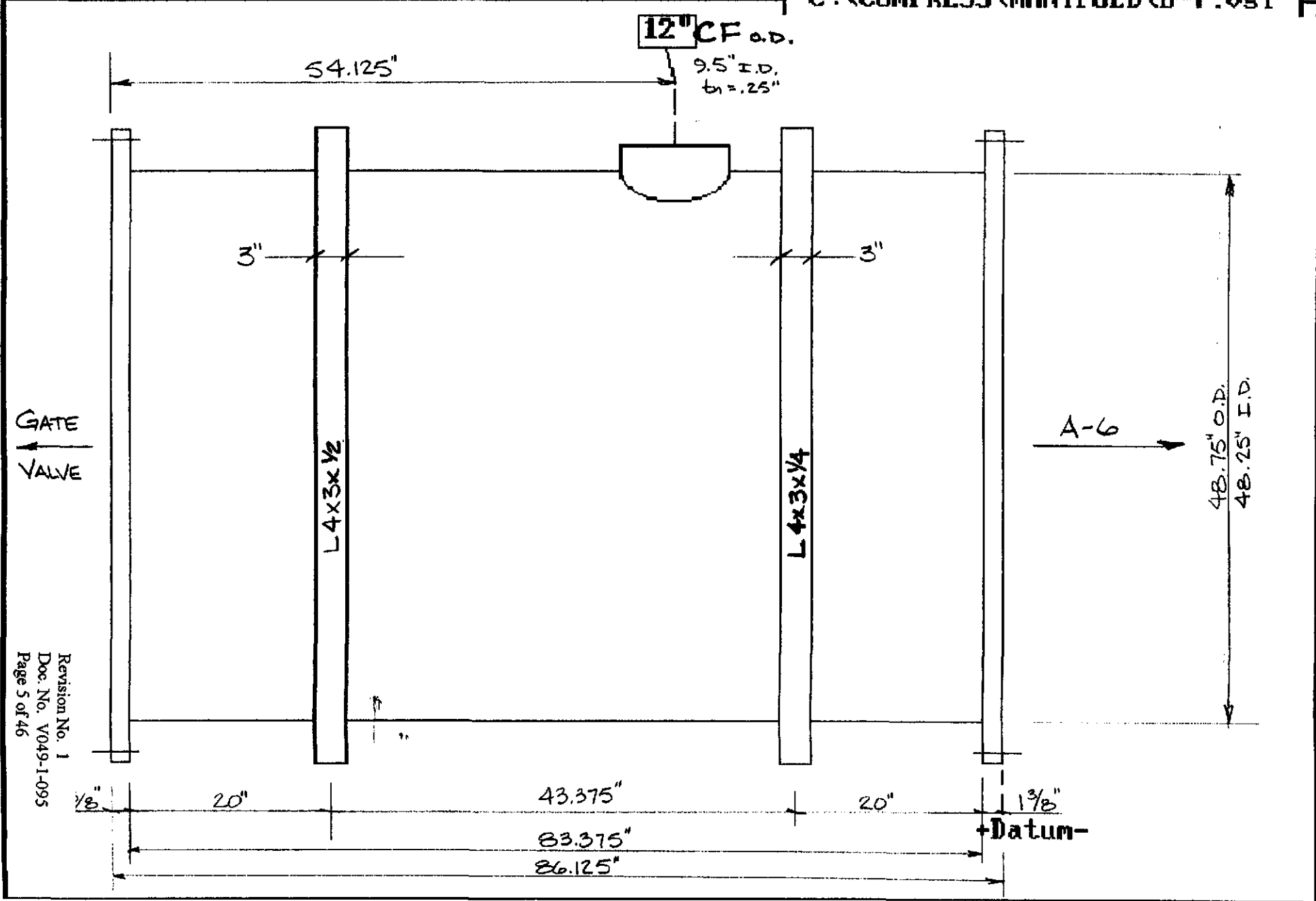
Rev. 1            Issue Date  
                         September 23, 1996

- Revised the unbalanced vacuum load at the gate valve (32.17k).
- Revised the baseplate thickness.
- Revised the anchor bolts.
- Revised body of calc to reflect changes due to new vacuum load.
- Added weld calculations.
- Revised design details to reflect change in members.
- Checked for punching shear at the tube steel connections using *STAAD*.



Revision No. 1  
Doc. No. V049-1-095  
Page 4 of 46





Revision No. 1  
Doc. No. V049-1-095  
Page 5 of 46

## LOAD CONDITIONS

### • DEADWEIGHT

VESSEL WEIGHT - REF COMPRESS OUTPUT  
CALC No. V049-1-058 & 059

$$1589\# - (2)(253\#) = 1083 \text{ lbs}$$

$$\text{uniform load} = \frac{1083 \text{ lbs}}{83.375 \text{ in}} = 12.99 \approx 13.0 \#/\text{in}$$

$$\text{FLANGE WEIGHT} = 253 \text{ lbs.} \\ (2 \text{ FLANGES})$$

$$\text{VALVE} = 150 \text{ lbs.}$$

### • THERMAL

$$\text{"BAKEOUT" @ } 400^\circ\text{F} \Rightarrow \Delta T = 400^\circ\text{F} - 70^\circ\text{F}$$

$$\Delta T = 330^\circ\text{F}$$

### • VACUUM

$$\text{VACUUM LOAD FROM GATE VALVE} = 32170 \text{ lbs} \\ (\text{see following page})$$

VACUUM LOAD FROM UNBALANCED CONDITION  
@ TURBO PUMP (10"  $\phi$ ).

$$F = PA$$

$$= (14.7 \#/\text{in}^2) \frac{(10 \text{ in})^2 \pi}{4}$$

$$= 1155. \text{ lbs.}$$

### • SEISMIC -

SEISMIC (HORIZONTAL ONLY) - ONE DIRECTION

$$\text{VESSEL} = F_H = (13.0 \#/\text{in}) (0.05625 \text{ g}) = 0.73 \#/\text{in}$$

$$\text{FLANGE} = 253. \text{ lbs} (0.05625 \text{ g}) = 14.23 \text{ lbs} = F_{\text{HOR.}}$$

$$\text{VALVE} = 150. \text{ lbs} (0.05625 \text{ g}) = 8.4 \text{ lbs} = F_{\text{HOR.}}$$

UNBALANCED FORCE AT 48.25 IN VALVE

$$D_m = 49.589 \text{ IN} \quad (\text{HYSCAN CALC. } 7/9/96)$$

VACUUM FORCE

$$F = \pi \frac{D_m^2}{4} (14.7) \\ = 28.4 \text{ K}$$

PURGE PRESSURE = 2 PSIG

$$F' = \pi \frac{G^2}{4} (2)$$

$$G = \text{INNER O-RING DIAM} * \\ = 49 \text{ IN}$$

$$F' = \pi \frac{49^2}{4} (2) = 3.77 \text{ K}$$

TOTAL FORCE

$$F = 28.4 + 3.77 = 32.17$$

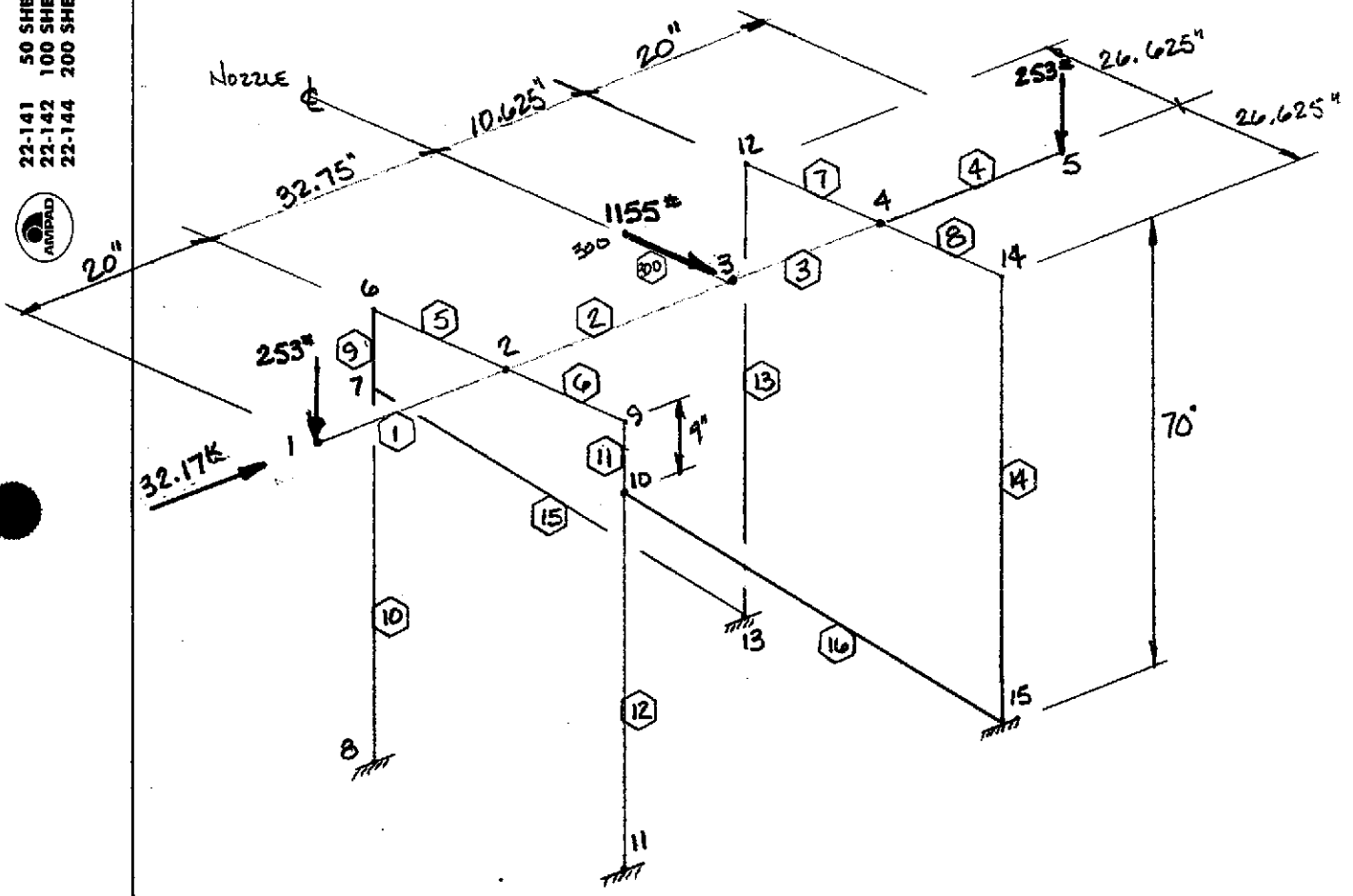
\* REF CALL 042, P. 25 - DEFLATION UNDER POS PRESSURE WILL NOT UNSAT THE INNER O-RING.  $\therefore$  PRESSURE ACTS TO THE INNER O-RING. CALLS 019 & 042 CONSERVATIVELY ASSUMED THAT PRESSURE ACTS TO THE OUTER O-RING.



# B6 & B7 STAAD MODEL

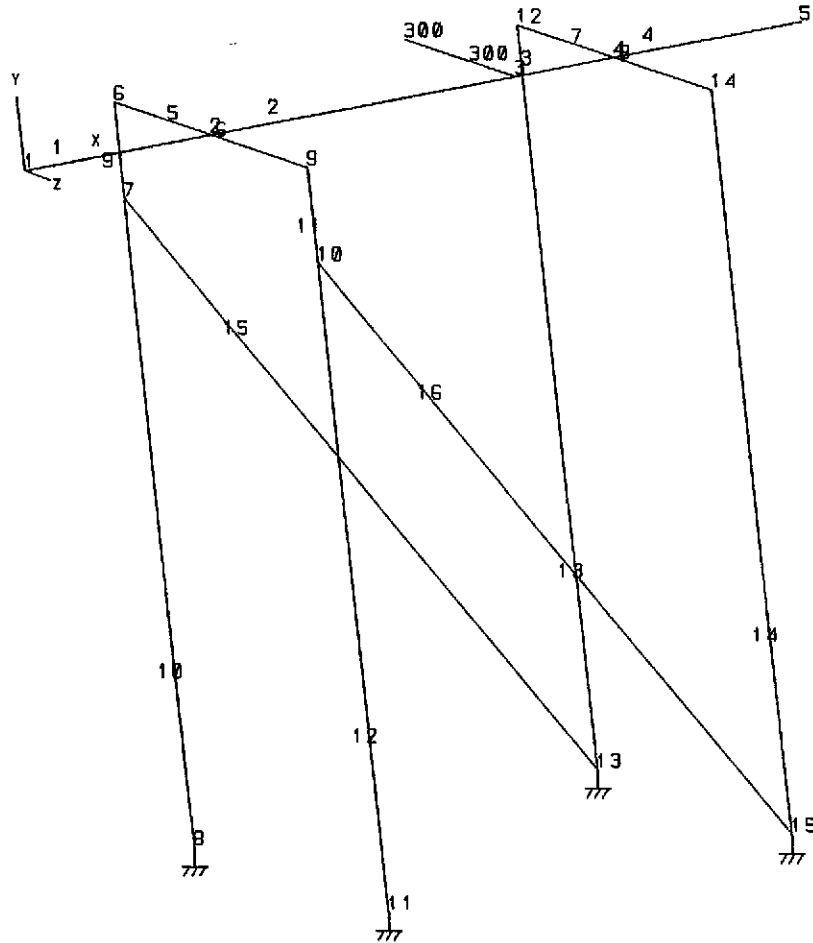
B6 & B7 = 48 in  $\phi$  = 48.25 in I.D. / 48.75 in. O.D.

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



STRUCTURE DATA

TYPE = SPACE  
 NJ = 16  
 NM = 17  
 NE = 0  
 NS = 4  
 NL = 8  
 XMAX = 83.4  
 YMAX = 70.0  
 ZMAX = 57.0



J=16, M=17

UNIT INC POU

```

*****
*
*           S T A A D - III
*           Revision 21.0
*           Proprietary Program of
*           Research Engineers, Inc.
*           Date=   SEP 25, 1996
*           Time=   16:11: 3
*
*           USER ID: PROCESS SYSTEMS INTERNATIONAL IN
*****

```

1. STAAD SPACE B6 & B7 MANIFOLD SUPPORT
2. \*\*\* ( B-7 BOUNDING CASE )
3. INPUT WIDTH 72
4. UNIT INCHES POUND
5. JOINT COORDINATES
6. 1 0. 0. 0.; 2 20. 0. 0.; 3 52.75 0. 0.; 4 63.375 0. 0.; 5 83.375 0. 0.
7. 6 20. 0. -26.625; 7 20. -9. -26.625; 8 20. -70. -26.625; 9 20. 0. 26.625
8. 10 20. -9. 26.625; 11 20. -70. 26.625; 12 63.375 0. -26.625
9. 13 63.375 -70. -26.625; 14 63.375 0. 26.625; 15 63.375 -70. 26.625
10. 300 52.75 0. -30.375
11. MEMBER INCIDENCES
12. 1 1 2; 2 2 3; 3 3 4; 4 4 5; 5 2 6; 6 2 9; 7 4 12; 8 4 14; 9 7 6; 10 8 7
13. 11 10 9; 12 11 10; 13 13 12; 14 15 14; 15 7 13; 16 10 15; 300 3 300
14. MEMBER PROPERTY AMER
15. 9 TO 12 15 16 TABLE ST TUB40408
16. 13 14 TABLE ST TUB40203
17. 5 TO 8 TABLE ST TUB80805
18. 1 TO 4 TABLE ST PIPE OD 48.75 ID 48.25
19. 300 TABLE ST PIPE OD 10. ID 9.5
20. MEMBER RELEASE
21. 9 11 13 14 END MX MY MZ
22. CONSTANTS
23. E STEEL ALL
24. POISSON STEEL ALL
25. DENSITY STEEL ALL
26. BETA 90. MEMB 13 14
27. ALPHA 0.00000919 MEMB 1 TO 8
28. SUPPORTS
29. 8 11 13 15 FIXED
30. \*\*\*\*\*
31. LOAD 1 DEADWEIGHT
32. JOINT LOAD
33. 1 5 FY -506.
34. \* FLANGE WEIGHT = 2 @ 253 LBS.
35. 300 FY -150.
36. \* VALVE WEIGHT
37. MEMBER LOAD
38. 1 TO 4 UNI Y -13.
39. \* UNIFORM 1083.#/83.375" = 13.0
40. \*\*\*\*\*
41. LOAD 2 DW+TH+VACUUM(+)

- B6 & B7 MANIFOLD SUPPORT
- \*\*\* ( B-7 BOUNDING CASE )
- 42. JOINT LOAD
- 43. 1 FX 32170.
- 44. \* UNBALANCED (+) VACUUM LOAD @ GATE VALVE
- 45. 1 5 FY -506.
- 46. 300 FY -150.
- 47. 300 FZ 1155.
- 48. \* UNBALANCED VACUUM LOAD @ TURBO PMP
- 49. MEMBER LOAD
- 50. 1 TO 4 UNI Y -13.
- 51. TEMPERATURE LOAD
- 52. 1 TO 8 300 TEMP 330.
- 53. \*\*\*\*\*
- 54. LOAD 3 DW+TH+VACUUM(-)
- 55. JOINT LOAD
- 56. 1 FX -32170.
- 57. \* UNBALANCED (-) VACUUM LOAD @ GATE VALVE
- 58. 1 5 FY -506.
- 59. 300 FY -150.
- 60. 300 FZ 1155.
- 61. \* UNBALANCED VACUUM LOAD @ TURBO PMP
- 62. MEMBER LOAD
- 63. 1 TO 4 UNI Y -13.
- 64. TEMPERATURE LOAD
- 65. 1 TO 8 300 TEMP 330.
- 66. \*\*\*\*\*
- 67. LOAD 4 DW+TH+VACUUM(+)+SEIS-AXIAL(+)
- 68. JOINT LOAD
- 69. 1 FX 32170.
- 70. \* UNBALANCED (+) VACUUM LOAD @ GATE VALVE
- 71. 1 5 FY -506.
- 72. 300 FY -150.
- 73. 1 5 FX 14.23
- 74. \* FLANGE WEIGHT X 0.05625
- 75. 300 FX 8.5
- 76. \* VALVE WEIGHT X 0.05625
- 77. 300 FZ 1155.
- 78. \* UNBALANCED VACUUM LOAD @ TURBO PMP
- 79. MEMBER LOAD
- 80. 1 TO 4 UNI Y -13.
- 81. 1 TO 4 UNI X 0.73
- 82. \* UNIFORM WEIGHT X 0.05625
- 83. TEMPERATURE LOAD
- 84. 1 TO 8 300 TEMP 330.
- 85. \*\*\*\*\*
- 86. LOAD 5 DW+TH+VACUUM(-)+SEIS-AXIAL(-)
- 87. JOINT LOAD
- 88. 1 FX -32170.
- 89. \* UNBALANCED (-) VACUUM LOAD @ GATE VALVE
- 90. 1 5 FY -506.
- 91. 300 FY -150.
- 92. 1 5 FX -14.23
- 93. \* FLANGE WEIGHT X 0.05625
- 94. 300 FX -8.5
- 95. \* VALVE WEIGHT X 0.05625
- 96. 300 FZ 1155.
- 97. \* UNBALANCED VACUUM LOAD @ TURBO PMP

- B6 & B7 MANIFOLD SUPPORT
- \*\*\* ( B-7 BOUNDING CASE )
- 98. MEMBER LOAD
- 99. 1 TO 4 UNI Y -13.
- 100. 1 TO 4 UNI X -0.73
- 101. \* UNIFORM WEIGHT X 0.05625
- 102. TEMPERATURE LOAD
- 103. 1 TO 8 300 TEMP 330.
- 104. \*\*\*\*\*
- 105. LOAD 6 DW+TH+VACUUM(+)+SEIS-LAT(+)
- 106. JOINT LOAD
- 107. 1 FX 32170.
- 108. \* UNBALANCED (+)VACUUM LOAD @ GATE VALVE
- 109. 1 5 FY -502.
- 110. 300 FY -150.
- 111. 1 5 FZ 14.23
- 112. 300 FZ 8.5
- 113. 300 FZ 1155.
- 114. \* UNBALANCED VACUUM LOAD @ TURBO PMP
- 115. MEMBER LOAD
- 116. 1 TO 4 UNI Y -13.
- 117. 1 TO 4 UNI Z 0.73
- 118. TEMPERATURE LOAD
- 119. 1 TO 8 300 TEMP 330.
- 120. \*\*\*\*\*
- 121. LOAD 7 DW+TH+VACUUM(-)+SEIS-LAT(-)
- 122. JOINT LOAD
- 123. 1 FX -32170.
- 124. \* UNBALANCED (-)VACUUM LOAD @ GATE VALVE
- 125. 1 5 FY -502.
- 126. 300 FY -150.
- 127. 1 5 FZ -14.23
- 128. 300 FZ -8.5
- 129. 300 FZ 1155.
- 130. \* UNBALANCED VACUUM LOAD @ TURBO PMP
- 131. MEMBER LOAD
- 132. 1 TO 4 UNI Y -13.
- 133. 1 TO 4 UNI Z -0.73
- 134. TEMPERATURE LOAD
- 135. 1 TO 8 300 TEMP 330.
- 136. \*\*\*\*\*
- 137. LOAD 8 THERMAL "BAKEOUT"
- 138. TEMPERATURE LOAD
- 139. 1 TO 8 300 TEMP 330.
- 140. PERFORM ANALYSIS

P R O B L E M   S T A T I S T I C S

---

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS = 16/ 17/ 4  
 ORIGINAL/FINAL BAND-WIDTH = 13/ 4  
 TOTAL PRIMARY LOAD CASES = 8, TOTAL DEGREES OF FREEDOM = 72  
 SIZE OF STIFFNESS MATRIX = 2160 DOUBLE PREC. WORDS  
 REQD/AVAIL. DISK SPACE = 12.05/ 952.1 MB, EXMEM = 14.83 MB

++ PROCESSING ELEMENT STIFFNESS MATRIX. 16:11: 5



B6 & B7 MANIFOLD SUPPORT

-- PAGE NO. 4

\*\*\* ( B-7 BOUNDING CASE )

++ PROCESSING GLOBAL STIFFNESS MATRIX.  
++ PROCESSING TRIANGULAR FACTORIZATION.  
++ CALCULATING JOINT DISPLACEMENTS.  
++ CALCULATING MEMBER FORCES.

16:11: 5  
16:11: 5  
16:11: 5  
16:11: 6

141. PRINT MATERIAL PROPERTIES ALL

MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
1	29000000.0	11153846.0	0.28299999	0.00000919
2	29000000.0	11153846.0	0.28299999	0.00000919
3	29000000.0	11153846.0	0.28299999	0.00000919
4	29000000.0	11153846.0	0.28299999	0.00000919
5	29000000.0	11153846.0	0.28299999	0.00000919
6	29000000.0	11153846.0	0.28299999	0.00000919
7	29000000.0	11153846.0	0.28299999	0.00000919
8	29000000.0	11153846.0	0.28299999	0.00000919
9	29000000.0	11153846.0	0.28299999	0.00000000
10	29000000.0	11153846.0	0.28299999	0.00000000
11	29000000.0	11153846.0	0.28299999	0.00000000
12	29000000.0	11153846.0	0.28299999	0.00000000
13	29000000.0	11153846.0	0.28299999	0.00000000
14	29000000.0	11153846.0	0.28299999	0.00000000
15	29000000.0	11153846.0	0.28299999	0.00000000
16	29000000.0	11153846.0	0.28299999	0.00000000
300	29000000.0	11153846.0	0.28299999	0.00000000

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

142. PRINT MEMBER INFORMATION ALL

MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
1	1	2	20.000	0.00	
2	2	3	32.750	0.00	
3	3	4	10.625	0.00	
4	4	5	20.000	0.00	
5	2	6	26.625	0.00	
6	2	9	26.625	0.00	
7	4	12	26.625	0.00	
8	4	14	26.625	0.00	
9	7	6	9.000	0.00	000000000111
10	8	7	61.000	0.00	
11	10	9	9.000	0.00	000000000111
12	11	10	61.000	0.00	
13	13	12	70.000	90.00	000000000111
14	15	14	70.000	90.00	000000000111
15	7	13	74.849	0.00	
16	10	15	74.849	0.00	
300	3	300	30.375	0.00	

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

143. PRINT JOINT COORDINATES ALL

JOINT COORDINATES

COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
1	0.000	0.000	0.000
2	20.000	0.000	0.000
3	52.750	0.000	0.000
4	63.375	0.000	0.000
5	83.375	0.000	0.000
6	20.000	0.000	-26.625
7	20.000	-9.000	-26.625
8	20.000	-70.000	-26.625
9	20.000	0.000	26.625
10	20.000	-9.000	26.625
11	20.000	-70.000	26.625
12	63.375	0.000	-26.625
13	63.375	-70.000	-26.625
14	63.375	0.000	26.625
15	63.375	-70.000	26.625
300	52.750	0.000	-30.375

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

144. PRINT SUPPORT INFORMATION ALL

SUPPORT INFORMATION (1=FIXED, 0=RELEASED)

UNITS FOR SPRING CONSTANTS ARE POUN INCH DEGREES

JOINT	FORCE-X/ KFX	FORCE-Y/ KFY	FORCE-Z/ KFZ	MOM-X/ KMX	MOM-Y/ KMY	MOM-Z/ KMZ
8	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
11	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
13	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0
15	1	1	1	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0

B6 & B7 MANIFOLD SUPPORT  
\*\*\* ( B-7 BOUNDING CASE )

-- PAGE NO. 8

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

145. PRINT ANALYSIS RESULTS

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
1	1	-0.00030	-0.00155	0.00003	-0.00001	0.00000	-0.00001
	2	0.07282	0.01153	0.08897	0.00000	-0.00017	-0.00022
	3	-0.19546	-0.01470	0.08897	0.00000	-0.00017	0.00019
	4	0.07323	0.01157	0.08893	0.00000	-0.00017	-0.00022
	5	-0.19586	-0.01474	0.08901	0.00000	-0.00017	0.00020
	6	0.07282	0.01154	0.09666	0.00000	-0.00018	-0.00022
	7	-0.19545	-0.01470	0.08129	0.00000	-0.00016	0.00019
	8	-0.06101	-0.00004	0.00000	0.00000	0.00000	0.00000
2	1	-0.00030	-0.00176	0.00001	-0.00001	0.00000	-0.00001
	2	0.13290	0.00719	0.09236	0.00000	-0.00017	-0.00022
	3	-0.13422	-0.01076	0.09236	0.00000	-0.00017	0.00019
	4	0.13330	0.00722	0.09235	0.00000	-0.00017	-0.00022
	5	-0.13462	-0.01079	0.09238	0.00000	-0.00017	0.00020
	6	0.13290	0.00720	0.10022	0.00000	-0.00018	-0.00022
	7	-0.13422	-0.01075	0.08451	0.00000	-0.00016	0.00019
	8	-0.00036	-0.00002	0.00000	0.00000	0.00000	0.00000
3	1	-0.00030	-0.00222	-0.00002	-0.00001	0.00000	-0.00001
	2	0.23221	-0.00003	0.09807	0.00000	-0.00017	-0.00022
	3	-0.03490	-0.00442	0.09808	0.00000	-0.00017	0.00019
	4	0.23262	-0.00002	0.09811	0.00000	-0.00017	-0.00022
	5	-0.03531	-0.00443	0.09804	0.00000	-0.00017	0.00019
	6	0.23221	-0.00002	0.10623	0.00000	-0.00018	-0.00022
	7	-0.03490	-0.00442	0.08992	0.00000	-0.00016	0.00019
	8	0.09896	-0.00001	0.00000	0.00000	0.00000	0.00000
4	1	-0.00030	-0.00236	-0.00004	-0.00001	0.00000	-0.00001
	2	0.26443	-0.00236	0.09988	0.00000	-0.00017	-0.00022
	3	-0.00268	-0.00236	0.09989	0.00000	-0.00017	0.00019
	4	0.26484	-0.00236	0.09994	0.00000	-0.00017	-0.00022
	5	-0.00308	-0.00236	0.09983	0.00000	-0.00017	0.00019
	6	0.26443	-0.00235	0.10814	0.00000	-0.00018	-0.00022
	7	-0.00267	-0.00235	0.09164	0.00000	-0.00016	0.00019
	8	0.13118	0.00000	0.00000	0.00000	0.00000	0.00000
5	1	-0.00030	-0.00270	-0.00005	-0.00001	0.00000	-0.00001
	2	0.32509	-0.00683	0.10330	0.00000	-0.00017	-0.00022
	3	0.05798	0.00145	0.10331	0.00000	-0.00017	0.00019
	4	0.32550	-0.00684	0.10339	0.00000	-0.00017	-0.00022
	5	0.05757	0.00146	0.10322	0.00000	-0.00017	0.00019
	6	0.32509	-0.00682	0.11174	0.00000	-0.00018	-0.00022
	7	0.05798	0.00146	0.09488	0.00000	-0.00016	0.00019
	8	0.19184	0.00001	0.00000	0.00000	0.00000	0.00000
6	1	-0.00033	-0.00022	0.00001	0.00007	0.00000	-0.00001
	2	0.09002	0.00902	0.01161	0.00009	0.00206	-0.00022
	3	-0.08521	-0.00893	0.01161	0.00009	-0.00226	0.00019
	4	0.09032	0.00905	0.01160	0.00009	0.00206	-0.00022
	5	-0.08550	-0.00896	0.01162	0.00009	-0.00226	0.00020
	6	0.09018	0.00904	0.01947	0.00009	0.00205	-0.00022
	7	-0.08536	-0.00895	0.00376	0.00008	-0.00225	0.00019
	8	-0.00024	-0.00002	-0.08070	0.00000	-0.00001	0.00000

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
7	1	-0.00027	-0.00019	0.00001	0.00000	0.00000	0.00001
	2	0.03615	0.00905	0.00946	0.00023	0.00003	-0.00436
	3	-0.03450	-0.00890	0.00946	0.00023	0.00003	0.00411
	4	0.03627	0.00908	0.00945	0.00023	0.00003	-0.00438
	5	-0.03462	-0.00893	0.00947	0.00023	0.00003	0.00412
	6	0.03621	0.00907	0.01585	0.00039	0.00005	-0.00437
	7	-0.03456	-0.00892	0.00306	0.00008	0.00001	0.00412
	8	-0.00009	-0.00002	-0.06572	-0.00162	-0.00019	0.00001
8	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	6	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	7	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	8	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
9	1	-0.00028	-0.00019	0.00001	-0.00007	0.00000	-0.00001
	2	0.08413	0.00847	0.17302	-0.00006	-0.00225	-0.00022
	3	-0.09110	-0.00948	0.17302	-0.00006	0.00207	0.00019
	4	0.08437	0.00850	0.17301	-0.00006	-0.00225	-0.00022
	5	-0.09134	-0.00950	0.17303	-0.00006	0.00207	0.00020
	6	0.08398	0.00846	0.18088	-0.00006	-0.00225	-0.00022
	7	-0.09095	-0.00946	0.16517	-0.00006	0.00207	0.00019
	8	-0.00024	-0.00002	0.08070	0.00000	0.00001	0.00000
10	1	-0.00023	-0.00016	0.00001	0.00000	0.00000	0.00001
	2	0.03381	0.00850	0.14089	0.00348	0.00041	-0.00407
	3	-0.03684	-0.00946	0.14089	0.00348	0.00041	0.00440
	4	0.03391	0.00852	0.14088	0.00348	0.00041	-0.00409
	5	-0.03693	-0.00948	0.14090	0.00348	0.00041	0.00441
	6	0.03375	0.00848	0.14729	0.00364	0.00042	-0.00407
	7	-0.03678	-0.00944	0.13450	0.00332	0.00039	0.00439
	8	-0.00009	-0.00002	0.06572	0.00162	0.00019	0.00001
11	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	6	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	7	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	8	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
12	1	-0.00033	-0.00074	-0.00004	0.00008	0.00000	-0.00001
	2	0.26873	-0.00069	0.01914	0.00008	-0.00016	-0.00022
	3	0.00188	-0.00069	0.01914	0.00008	-0.00017	0.00019
	4	0.26918	-0.00069	0.01919	0.00008	-0.00016	-0.00022
	5	0.00143	-0.00069	0.01908	0.00008	-0.00017	0.00019
	6	0.26897	-0.00069	0.02739	0.00008	-0.00017	-0.00022
	7	0.00164	-0.00069	0.01089	0.00008	-0.00016	0.00019
	8	0.13106	0.00000	-0.08074	0.00000	0.00001	0.00000

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
13	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	6	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	7	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	8	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
14	1	-0.00028	-0.00065	-0.00004	-0.00008	0.00000	-0.00001
	2	0.25963	-0.00070	0.18061	-0.00008	-0.00018	-0.00022
	3	-0.00722	-0.00070	0.18061	-0.00008	-0.00017	0.00019
	4	0.26000	-0.00070	0.18067	-0.00008	-0.00018	-0.00022
	5	-0.00759	-0.00070	0.18056	-0.00008	-0.00017	0.00019
	6	0.25940	-0.00070	0.18886	-0.00008	-0.00019	-0.00022
	7	-0.00698	-0.00069	0.17236	-0.00008	-0.00016	0.00019
	8	0.13106	0.00000	0.08074	0.00000	-0.00001	0.00000
15	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	2	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	3	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	4	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	5	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	6	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	7	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
	8	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
300	1	-0.00033	-0.00302	-0.00002	-0.00003	0.00000	-0.00001
	2	0.23741	-0.00064	0.09823	-0.00003	-0.00017	-0.00022
	3	-0.02970	-0.00503	0.09823	-0.00003	-0.00017	0.00019
	4	0.23790	-0.00063	0.09827	-0.00003	-0.00017	-0.00022
	5	-0.03019	-0.00504	0.09820	-0.00003	-0.00017	0.00019
	6	0.23768	-0.00062	0.10639	-0.00003	-0.00018	-0.00022
	7	-0.02997	-0.00504	0.09008	-0.00003	-0.00016	0.00019
	8	0.09896	-0.00001	0.00000	0.00000	0.00000	0.00000



SUPPORT REACTIONS -UNIT POUN INCH      STRUCTURE TYPE = SPACE  
 -----

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
8	1	1.27	585.53	-0.02	-1.53	-0.06	-77.30
	2	1781.52	-27372.30	-42.82	-2672.16	-108.57	-28826.29
	3	-1670.06	26914.09	-42.82	-2672.54	-108.59	26905.35
	4	1787.30	-27462.96	-42.78	-2669.78	-108.47	-28919.76
	5	-1675.81	27004.16	-42.86	-2675.17	-108.69	26998.22
	6	1784.55	-27419.98	-71.79	-4480.21	-182.03	-28875.35
	7	-1673.10	26957.66	-13.86	-864.90	-35.14	26954.80
	8	-4.63	72.86	297.58	18572.61	754.62	74.80
11	1	1.06	492.85	-0.02	-1.53	-0.06	-64.86
	2	1663.11	-25689.65	-637.99	-39817.56	-1617.81	-26897.57
	3	-1788.46	28596.71	-637.99	-39817.92	-1617.83	28834.03
	4	1667.88	-25765.04	-637.95	-39815.16	-1617.71	-26974.55
	5	-1793.19	28671.43	-638.03	-39820.54	-1617.93	28910.34
	6	1660.06	-25645.91	-666.96	-41625.59	-1691.27	-26847.94
13	7	-1785.41	28548.74	-609.03	-38010.27	-1544.38	28784.69
	8	-4.64	72.92	-297.59	-18572.77	-754.62	74.87
	1	-1.33	622.97	0.02	1.53	-0.37	-71.20
	2	-18416.44	28580.80	-36.30	-2865.68	-648.09	-21316.82
	3	17205.11	-25705.59	-36.30	-2866.00	-648.18	25725.86
	4	-18476.16	28671.46	-36.33	-2868.02	-647.51	-21395.66
	5	17264.44	-25795.66	-36.27	-2863.85	-648.82	25804.20
	6	-18447.80	28624.49	-56.23	-4480.72	-1086.60	-21358.15
15	7	17236.38	-25753.16	-16.37	-1251.28	-209.77	25767.56
	8	4.65	-72.86	200.78	16313.16	4504.46	3083.94
	1	-1.01	544.52	0.02	1.53	-0.37	-59.76
	2	-17197.91	26727.02	-437.87	-35492.18	-9657.06	-19688.66
	3	18423.61	-27559.33	-437.87	-35492.49	-9657.14	27353.99
	4	-17247.15	26802.41	-437.90	-35494.52	-9656.48	-19753.61
	5	18472.41	-27634.05	-437.84	-35490.34	-9657.78	27418.36
	6	-17166.52	26679.27	-457.80	-37107.22	-10095.57	-19646.81
7	18392.07	-27515.37	-417.94	-33877.77	-9218.73	27312.42	
8	4.70	-72.92	-200.79	-16313.33	-4504.50	3084.00	

MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	1	1	0.00	-506.00	0.00	0.00	0.00	-0.01
		2	0.00	766.00	0.00	0.00	0.00	-12720.00
	2	1	32169.43	-506.00	-0.15	-0.02	0.85	-0.24
		2	-32169.43	766.00	0.15	0.02	0.47	-12720.14
	3	1	-32169.92	-505.99	-0.12	-0.01	1.37	-0.07
		2	32169.92	765.99	0.12	0.01	0.57	-12719.61
	4	1	32185.06	-505.99	-0.01	0.00	-0.33	0.05
		2	-32199.71	765.99	0.01	0.00	-0.28	-12720.37
	5	1	-32183.35	-506.00	0.05	0.00	-0.06	0.23
		2	32198.00	766.00	-0.05	0.00	-0.39	-12719.91
	6	1	32169.19	-501.99	14.32	0.02	-2.41	0.21
		2	-32169.19	761.99	-28.92	-0.02	-431.33	-12640.07
	7	1	-32170.41	-502.00	-14.21	0.01	-0.65	0.09
		2	32170.41	762.00	28.81	-0.01	428.68	-12639.51
	8	1	0.24	0.00	0.01	0.00	-0.17	-0.01
		2	-0.24	0.00	-0.01	0.00	-0.05	0.00
2	1	2	-0.20	318.68	-0.07	2487.18	3.44	12720.03
		3	0.20	107.07	0.07	-2487.18	-1.18	-9254.86
	2	2	174.07	318.68	-958.27	4653.05	29209.49	12720.15
		3	-174.07	107.07	958.27	-4653.05	2174.12	-9255.10
	3	2	-1.71	318.69	-958.16	4652.99	29210.20	12720.23
		3	1.71	107.06	958.16	-4652.99	2169.84	-9254.59
	4	2	104.98	318.68	-958.00	4671.68	29462.71	12719.96
		3	-128.91	107.07	958.00	-4671.68	1914.44	-9254.76
	5	2	66.89	318.68	-958.37	4634.29	28957.67	12719.72
		3	-42.97	107.07	958.37	-4634.29	2428.08	-9254.89
	6	2	174.07	318.68	-1010.87	4764.58	31146.25	12639.84
		3	-174.07	107.07	986.97	-4764.58	1570.24	-9174.68
	7	2	-1.95	318.69	-905.59	4541.29	27274.61	12640.17
		3	1.95	107.06	929.50	-4541.29	2773.61	-9175.02
	8	2	86.43	0.00	-0.02	0.08	0.73	0.00
		3	-86.43	0.00	0.02	-0.08	0.07	0.01
3	1	3	-0.20	-257.06	-0.07	-2069.07	1.18	9254.93
		4	0.20	395.19	0.07	2069.07	-0.44	-12719.99
	2	3	173.10	-257.07	196.73	96.83	-2172.25	9255.08
		4	-173.10	395.19	-196.73	-96.83	81.89	-12720.37
	3	3	-2.69	-257.08	196.63	96.73	-2167.61	9254.34
		4	2.69	395.20	-196.63	-96.73	76.74	-12719.59
	4	3	136.96	-257.07	196.93	115.42	-2171.04	9254.42
		4	-144.78	395.19	-196.93	-115.42	78.05	-12719.78
	5	3	33.45	-257.07	196.56	78.04	-2170.85	9254.05
		4	-25.63	395.20	-196.56	-78.04	82.14	-12719.35

MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z	
6	3	4	175.29	-257.07	176.79	208.31	-1571.44	9174.91	
		4	-175.29	395.19	-184.54	-208.31	-349.56	-12639.68	
7	3	4	-2.20	-257.06	217.40	-14.96	-2777.10	9175.06	
		4	2.20	395.19	-209.64	14.96	508.45	-12640.69	
8	3	4	87.40	0.00	-0.02	0.08	-0.44	-0.02	
		4	-87.40	0.00	0.02	-0.08	0.61	0.02	
4	1	4	0.00	766.00	0.00	-0.01	0.00	12720.01	
		5	0.00	-506.00	0.00	0.01	0.00	0.01	
	2	4	5	2.69	766.00	0.20	0.00	-2.14	12720.33
			5	-2.69	-506.00	-0.20	0.00	-1.89	-0.21
	3	4	5	-0.24	766.00	0.12	0.00	0.26	12720.09
			5	0.24	-506.00	-0.12	0.00	-1.87	-0.14
	4	4	5	-28.08	765.99	-0.08	0.00	3.00	12719.55
			5	13.43	-505.99	0.08	0.00	1.25	0.35
	5	4	5	28.56	766.00	-0.04	0.01	-1.65	12720.41
			5	-13.92	-506.00	0.04	-0.01	0.92	-0.67
	6	4	5	2.20	762.00	-28.84	-0.01	429.89	12640.05
			5	-2.20	-502.00	14.24	0.01	-0.15	0.08
	7	4	5	0.00	762.00	28.96	-0.01	-431.15	12639.84
			5	0.00	-502.00	-14.36	0.01	-1.56	0.11
	8	4	5	0.98	0.00	-0.02	0.00	-0.03	0.02
			5	-0.98	0.00	0.02	0.00	0.33	-0.01
5	1	2	-0.03	-589.05	0.16	0.00	-4.36	-15683.40	
		6	0.03	589.05	-0.16	0.00	0.00	0.00	
	2	2	6	-60.24	-629.72	16546.68	0.00	-440555.34	-16766.36
			6	60.24	629.72	-16546.68	0.00	-0.02	0.00
	3	2	6	-60.30	-629.72	15535.66	0.00	413636.94	-16766.28
			6	60.30	629.72	-15535.66	0.00	-0.15	-0.01
	4	2	6	-60.24	-630.07	16600.46	0.00	-441987.34	-16775.63
			6	60.24	630.07	-16600.46	0.00	-0.01	0.00
	5	2	6	-60.30	-629.37	15589.10	0.00	415059.91	-16756.95
			6	60.30	629.37	-15589.10	0.00	0.00	0.00
	6	2	6	-101.01	-629.82	16574.91	0.00	-441307.16	-16768.88
			6	101.01	629.82	-16574.91	0.00	0.01	0.01
	7	2	6	-19.47	-625.62	15563.82	0.00	414386.72	-16657.22
			6	19.47	625.62	-15563.82	0.00	-0.02	0.01
	8	2	6	418.82	0.00	-43.06	0.00	1146.41	-0.05
			6	-418.82	0.00	43.06	0.00	0.00	0.00
6	1	2	0.03	-495.63	-0.03	0.00	0.92	-13196.22	
		9	-0.03	495.63	0.03	0.00	0.00	0.00	
	2	2	9	897.95	-454.96	15449.57	0.00	411344.75	-12113.29
			9	-897.95	454.96	-15449.57	0.00	0.14	0.01
	3	2	9	897.89	-454.96	16632.78	0.00	-442847.53	-12113.30
			9	-897.89	454.96	-16632.78	0.00	-0.09	0.01

MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
 ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	4	2	897.89	-454.61	-15493.90	0.00	412525.09	-12103.95
		9	-897.89	454.61	15493.90	0.00	-0.11	0.01
	5	2	898.01	-455.31	16676.73	0.00	-444017.81	-12122.67
		9	-898.01	455.31	-16676.73	0.00	-0.05	0.01
	6	2	938.66	-450.87	-15421.33	0.00	410592.50	-12004.32
		9	-938.66	450.87	15421.33	0.00	0.48	-0.01
	7	2	857.18	-455.06	16604.39	0.00	-442091.63	-12115.92
		9	-857.18	455.06	-16604.39	0.00	-0.08	-0.03
	8	2	418.82	0.00	43.08	0.00	-1147.10	0.03
		9	-418.82	0.00	-43.08	0.00	0.04	0.00
7	1	4	0.03	-619.45	-0.11	0.00	2.87	-16492.93
		12	-0.03	619.45	0.11	0.00	0.00	0.00
	2	4	-18.86	-578.78	88.25	0.00	-2349.54	-15410.01
		12	18.86	578.78	-88.25	0.00	-0.01	0.00
	3	4	-18.86	-578.78	0.62	0.00	-16.40	-15410.02
		12	18.86	578.78	-0.62	0.00	0.00	0.00
	4	4	-18.92	-578.43	88.37	0.00	-2353.33	-15400.70
		12	18.92	578.43	-88.37	0.00	0.27	0.00
	5	4	-18.80	-579.13	0.47	0.00	-12.49	-15419.39
		12	18.80	579.13	-0.47	0.00	0.00	0.00
	6	4	-26.92	-574.69	88.34	0.00	-2351.57	-15300.99
		12	26.92	574.69	-88.34	0.00	0.09	0.00
	7	4	-10.80	-578.88	0.54	0.00	-14.34	-15412.61
		12	10.80	578.88	-0.54	0.00	0.00	0.00
	8	4	79.47	0.00	43.02	0.00	-1145.78	0.03
		12	-79.47	0.00	-43.02	0.00	0.04	0.00
8	1	4	-0.03	-541.74	0.09	0.00	-2.42	-14423.86
		14	0.03	541.74	-0.09	0.00	0.00	0.00
	2	4	178.10	-582.41	-85.29	0.00	2270.58	-15506.78
		14	-178.10	582.41	85.29	0.00	0.56	0.00
	3	4	178.04	-582.41	2.38	0.00	-63.28	-15506.77
		14	-178.04	582.41	-2.38	0.00	-0.14	0.00
	4	4	177.86	-582.76	-85.38	0.00	2273.27	-15516.11
		14	-177.86	582.76	85.38	0.00	0.11	-0.01
	5	4	177.86	-582.06	2.49	0.00	-66.37	-15497.41
		14	-177.86	582.06	-2.49	0.00	0.02	-0.01
	6	4	185.97	-582.51	-85.23	0.00	2268.70	-15509.30
		14	-185.97	582.51	85.23	0.00	0.81	0.00
	7	4	169.92	-578.32	2.30	0.00	-61.16	-15397.67
		14	-169.92	578.32	-2.30	0.00	-0.11	0.01
	8	4	79.53	0.00	-43.05	0.00	1146.12	-0.04
		14	-79.53	0.00	43.05	0.00	0.25	0.00
9	1	7	589.05	0.16	-0.03	0.00	0.31	1.48
		6	-589.05	-0.16	0.03	0.00	0.00	0.00

MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
2	7	6	629.73	16546.68	-60.26	0.00	542.34	148920.14
		6	-629.73	-16546.68	60.26	0.00	0.00	0.00
3	7	6	629.72	-15535.66	-60.27	0.00	542.41	-139820.94
		6	-629.72	15535.66	60.27	0.00	0.00	0.00
4	7	6	630.06	16600.47	-60.21	0.00	541.86	149404.19
		6	<u>-630.06</u>	<u>-16600.47</u>	60.21	0.00	0.00	0.00
5	7	6	629.37	-15589.10	-60.33	0.00	542.95	-140301.88
		6	-629.37	15589.10	60.33	0.00	0.00	0.00
6	7	6	629.82	16574.92	-101.03	0.00	909.31	149174.25
		6	-629.82	-16574.92	101.03	0.00	0.00	0.00
7	7	6	625.62	-15563.83	-19.50	0.00	175.54	-140074.48
		6	-625.62	15563.83	19.50	0.00	0.00	0.00
8	7	6	0.00	-43.06	418.83	0.00	-3769.48	-387.52
		6	0.00	43.06	<u>-418.83</u>	0.00	0.00	0.00
10	1	8	585.53	-1.27	-0.02	-0.06	1.53	-77.30
		7	-585.53	1.27	0.02	0.06	-0.03	-0.44
2	8	7	-27372.30	-1781.52	-42.82	-108.57	2672.16	-28826.29
		7	27372.30	1781.52	42.82	108.57	-60.42	-79846.21
3	8	7	26914.09	1670.06	-42.82	-108.59	2672.54	26905.35
		7	-26914.09	-1670.06	42.82	108.59	-60.43	74968.27
4	8	7	-27462.96	-1787.30	-42.78	-108.47	2669.78	-28919.76
		7	27462.96	1787.30	42.78	108.47	-60.37	-80105.75
5	8	7	27004.16	1675.81	-42.86	-108.69	2675.17	26998.22
		7	-27004.16	-1675.81	42.86	108.69	-60.49	75226.13
6	8	7	-27419.98	-1784.55	-71.79	-182.03	4480.21	-28875.35
		7	27419.98	1784.55	71.79	182.03	-101.31	-79982.47
7	8	7	26957.66	1673.10	-13.86	-35.14	864.90	26954.80
		7	-26957.66	-1673.10	13.86	35.14	-19.56	75104.15
8	8	7	72.86	4.63	297.58	754.62	-18572.61	74.80
		7	-72.86	-4.63	-297.58	-754.62	419.97	207.78
11	1	10	495.63	0.03	-0.03	0.00	0.31	0.31
		9	<u>-495.63</u>	-0.03	0.03	0.00	0.00	0.00
2	10	9	454.98	15449.55	-897.89	0.00	8081.00	139045.97
		9	-454.98	-15449.55	897.89	0.00	0.00	0.00
3	10	9	454.95	-16632.78	-897.98	0.00	8081.87	-149695.08
		9	-454.95	16632.78	897.98	0.00	0.00	0.00
4	10	9	454.61	15493.89	-897.87	0.00	8080.79	139445.05
		9	-454.61	-15493.89	897.87	0.00	0.00	0.00
5	10	9	455.33	-16676.73	-898.01	0.00	8082.13	-150090.58
		9	-455.33	<u>16676.73</u>	898.01	0.00	0.00	0.00
6	10	9	450.85	15421.30	-938.72	0.00	8448.36	138791.64
		9	-450.85	-15421.30	<u>938.72</u>	0.00	0.00	0.00
7	10	9	455.02	-16604.37	-857.18	0.00	7714.52	-149439.33
		9	-455.02	16604.37	857.18	0.00	0.00	0.00
8	10	9	0.00	-43.09	-418.84	0.00	3769.54	-387.77
		9	0.00	43.09	418.84	0.00	0.00	0.00

MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
12	1	11	492.85	-1.06	-0.02	-0.06	1.53	-64.86
		10	-492.85	1.06	0.02	0.06	-0.03	0.13
	2	11	-25689.65	-1663.11	-637.99	-1617.81	39817.56	-26897.57
		10	25689.65	1663.11	637.99	1617.81	-900.35	-74552.06
	3	11	28596.71	1788.46	-637.99	-1617.83	39817.92	28834.03
		10	-28596.71	-1788.46	637.99	1617.83	-900.38	80262.31
	4	11	-25765.04	-1667.88	-637.95	-1617.71	39815.16	-26974.55
		10	25765.04	1667.88	637.95	1617.71	-900.32	-74766.05
	5	11	28671.43	1793.19	-638.03	-1617.93	39820.54	28910.34
		10	-28671.43	-1793.19	638.03	1617.93	-900.45	80474.39
	6	11	-25645.91	-1660.06	-666.96	-1691.27	41625.59	-26847.94
		10	25645.91	1660.06	666.96	1691.27	-941.26	-74415.70
7	11	28548.74	1785.41	-609.03	-1544.38	38010.27	28784.69	
	10	-28548.74	-1785.41	609.03	1544.38	-859.52	80125.26	
8	11	72.92	4.64	-297.59	-754.62	18572.77	74.87	
	10	-72.92	-4.64	297.59	754.62	-419.98	207.96	
13	1	13	619.45	0.03	0.11	0.00	-7.54	2.42
		12	-619.45	-0.03	-0.11	0.00	0.00	0.00
	2	13	578.78	-18.85	-88.25	0.00	6177.23	-1319.65
		12	-578.78	18.85	88.25	0.00	0.00	0.00
	3	13	578.78	-18.85	-0.62	0.00	43.12	-1319.75
		12	-578.78	18.85	0.62	0.00	0.00	0.00
	4	13	578.43	-18.91	-88.39	0.00	6187.57	-1323.37
		12	-578.43	18.91	88.39	0.00	0.00	0.00
	5	13	579.13	-18.80	-0.47	0.00	32.85	-1316.08
		12	-579.13	18.80	0.47	0.00	0.00	0.00
	6	13	574.69	-26.98	-88.32	0.00	6182.71	-1888.61
		12	-574.69	26.98	88.32	0.00	0.00	0.00
	7	13	578.88	-10.73	-0.54	0.00	37.70	-750.88
		12	-578.88	10.73	0.54	0.00	0.00	0.00
	8	13	0.00	79.54	-43.04	0.00	3012.57	5567.60
		12	0.00	-79.54	43.04	0.00	0.00	0.00
14	1	15	541.74	0.03	0.09	0.00	-6.36	2.42
		14	-541.74	-0.03	-0.09	0.00	0.00	0.00
	2	15	582.41	-177.93	-85.26	0.00	5968.08	-12454.92
		14	-582.41	177.93	85.26	0.00	0.00	0.00
	3	15	582.41	-177.93	2.37	0.00	-166.03	-12455.03
		14	-582.41	177.93	-2.37	0.00	0.00	0.00
	4	15	582.76	-177.98	-85.38	0.00	5976.59	-12458.65
		14	-582.76	177.98	85.38	0.00	0.00	0.00
	5	15	582.06	-177.88	2.49	0.00	-174.46	-12451.36
		14	-582.06	177.88	-2.49	0.00	0.00	0.00
	6	15	582.51	-186.06	-85.18	0.00	5962.64	-13023.89
		14	-582.51	186.06	85.18	0.00	0.00	0.00

MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
	7	15	578.32	-169.80	2.29	0.00	-160.51	-11886.16
		14	-578.32	169.80	-2.29	0.00	0.00	0.00
	8	15	0.00	-79.54	-43.04	0.00	3012.56	-5567.68
		14	0.00	79.54	43.04	0.00	0.00	0.00
15	1	7	3.70	-0.86	0.01	0.21	0.19	-1.03
		13	-3.70	0.86	-0.01	-0.21	-0.94	-63.67
	2	7	33442.06	-1290.17	17.44	367.75	329.83	-69073.90
		13	-33442.06	1290.17	-17.44	-367.75	-1635.54	-27494.05
	3	7	-31391.75	1209.57	17.45	367.80	329.88	64852.72
		13	31391.75	-1209.57	-17.45	-367.80	-1635.77	25682.74
	4	7	33550.75	-1294.36	17.43	367.42	329.54	-69298.42
		13	-33550.75	1294.36	-17.43	-367.42	-1634.08	-27583.23
	5	7	-31499.74	1213.74	17.46	368.17	330.20	65075.79
		13	31499.74	-1213.74	-17.46	-368.17	-1637.38	25771.35
	6	7	33499.13	-1292.37	29.25	616.58	553.00	-69191.77
		13	-33499.13	1292.37	-29.25	-616.58	-2742.19	-27540.86
	7	7	-31448.68	1211.77	5.65	119.03	106.76	64970.27
		13	31448.68	-1211.77	-5.65	-119.03	-529.37	25729.86
	8	7	-87.01	3.35	-121.25	-2556.03	-2292.46	179.74
		13	87.01	-3.35	121.25	2556.03	11367.67	71.37
16	1	10	2.90	-0.72	0.01	0.21	0.19	-0.44
		15	-2.90	0.72	-0.01	-0.21	-0.94	-53.40
	2	10	31223.92	-1204.43	259.94	5479.83	4914.75	-64493.86
		15	-31223.92	1204.43	-259.94	-5479.83	-24371.00	-25656.74
	3	10	-33609.85	1295.31	259.94	5479.88	4914.81	69432.66
		15	33609.85	-1295.31	-259.94	-5479.88	-24371.21	27520.02
	4	10	31313.53	-1207.89	259.92	5479.50	4914.46	-64678.97
		15	-31313.53	1207.89	-259.92	-5479.50	-24369.53	-25730.20
	5	10	-33698.66	1298.73	259.96	5480.24	4915.14	69616.13
		15	33698.66	-1298.73	-259.96	-5480.24	-24372.82	27592.83
	6	10	31166.78	-1202.22	271.74	5728.66	5137.93	-64375.89
		15	-31166.78	1202.22	-271.74	-5728.66	-25477.63	-25609.46
	7	10	-33552.45	1293.10	248.14	5231.11	4691.70	69314.11
		15	33552.45	-1293.10	-248.14	-5231.11	-23264.81	27472.94
	8	10	-87.09	3.36	121.25	2556.05	2292.48	179.90
		15	87.09	-3.36	-121.25	-2556.05	-11367.77	71.43
300	1	3	0.00	150.00	0.00	0.00	0.00	4556.26
		300	0.00	-150.00	0.00	0.00	0.00	0.01
	2	3	1154.90	150.00	0.02	0.00	-0.68	4556.25
		300	-1154.90	-150.00	-0.02	0.00	-0.52	0.00
	3	3	1155.03	150.00	-0.02	0.00	0.26	4556.25
		300	-1155.03	-150.00	0.02	0.00	0.25	0.00
	4	3	1155.04	150.00	-8.46	0.00	257.75	4556.25
		300	-1155.04	-150.00	8.46	0.00	-0.41	0.00

B6 & B7 MANIFOLD SUPPORT  
\*\*\* ( B-7 BOUNDING CASE )

-- PAGE NO. 19

MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
5		3	1154.94	150.00	8.49	0.00	-258.07	4556.25
		300	-1154.94	-150.00	-8.49	0.00	0.10	0.00
6		3	1163.53	150.00	0.03	0.00	-0.43	4556.25
		300	-1163.53	-150.00	-0.03	0.00	-0.52	0.00
7		3	1146.31	150.00	-0.01	0.00	0.09	4556.25
		300	-1146.31	-150.00	0.01	0.00	0.08	0.01
8		3	0.03	0.00	0.02	0.00	-0.26	0.00
		300	-0.03	0.00	-0.02	0.00	-0.30	0.00

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

146. PRINT MEMBER STRESSES ALL



MEMBER STRESSES

-----  
 ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
1	1	.0	0.0 C	0.0	0.0	0.0	22.1	0.0
		1.00	0.0 C	0.0	27.7	27.7	33.5	0.0
	2	.0	844.5 C	0.0	0.0	844.5	22.1	0.0
		1.00	844.5 C	0.0	27.7	872.2	33.5	0.0
	3	.0	844.5 T	0.0	0.0	844.5	22.1	0.0
		1.00	844.5 T	0.0	27.7	872.2	33.5	0.0
	4	.0	844.9 C	0.0	0.0	844.9	22.1	0.0
		1.00	845.3 C	0.0	27.7	873.0	33.5	0.0
	5	.0	844.9 T	0.0	0.0	844.9	22.1	0.0
		1.00	845.3 T	0.0	27.7	873.0	33.5	0.0
	6	.0	844.5 C	0.0	0.0	844.5	22.0	0.6
		1.00	844.5 C	0.9	27.5	872.0	33.3	1.3
	7	.0	844.5 T	0.0	0.0	844.6	22.0	0.6
		1.00	844.5 T	0.9	27.5	872.1	33.3	1.3
	8	.0	0.0 C	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0
2	1	.0	0.0 T	0.0	27.7	27.7	13.9	0.0
		1.00	0.0 T	0.0	20.1	20.1	4.7	0.0
	2	.0	4.6 C	63.6	27.7	73.9	13.9	41.9
		1.00	4.6 C	4.7	20.1	25.3	4.7	41.9
	3	.0	0.0 T	63.6	27.7	69.4	13.9	41.9
		1.00	0.0 T	4.7	20.1	20.7	4.7	41.9
	4	.0	2.8 C	64.1	27.7	72.6	13.9	41.9
		1.00	3.4 C	4.2	20.1	24.0	4.7	41.9
	5	.0	1.8 C	63.0	27.7	70.6	13.9	41.9
		1.00	1.1 C	5.3	20.1	22.0	4.7	41.9
	6	.0	4.6 C	67.8	27.5	77.7	13.9	44.2
		1.00	4.6 C	3.4	20.0	24.8	4.7	43.2
	7	.0	0.1 T	59.4	27.5	65.5	13.9	39.6
		1.00	0.1 T	6.0	20.0	20.9	4.7	40.7
	8	.0	2.3 C	0.0	0.0	2.3	0.0	0.0
		1.00	2.3 C	0.0	0.0	2.3	0.0	0.0
3	1	.0	0.0 T	0.0	20.1	20.1	11.2	0.0
		1.00	0.0 T	0.0	27.7	27.7	17.3	0.0
	2	.0	4.5 C	4.7	20.1	25.2	11.2	8.6
		1.00	4.5 C	0.2	27.7	32.2	17.3	8.6
	3	.0	0.1 T	4.7	20.1	20.8	11.2	8.6
		1.00	0.1 T	0.2	27.7	27.8	17.3	8.6
	4	.0	3.6 C	4.7	20.1	24.3	11.2	8.6
		1.00	3.8 C	0.2	27.7	31.5	17.3	8.6
	5	.0	0.9 C	4.7	20.1	21.6	11.2	8.6
		1.00	0.7 C	0.2	27.7	28.4	17.3	8.6
	6	.0	4.6 C	3.4	20.0	24.9	11.2	7.7
		1.00	4.6 C	0.8	27.5	32.1	17.3	8.1
	7	.0	0.1 T	6.0	20.0	20.9	11.2	9.5
		1.00	0.1 T	1.1	27.5	27.6	17.3	9.2

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z	
		8	.0	2.3 C	0.0	0.0	2.3	0.0	0.0
			1.00	2.3 C	0.0	0.0	2.3	0.0	0.0
4	1	.0	0.0 C	0.0	27.7	27.7	33.5	0.0	
		1.00	0.0 C	0.0	0.0	0.0	22.1	0.0	
	2	.0	0.1 C	0.0	27.7	27.8	33.5	0.0	
		1.00	0.1 C	0.0	0.0	0.1	22.1	0.0	
	3	.0	0.0 T	0.0	27.7	27.7	33.5	0.0	
		1.00	0.0 T	0.0	0.0	0.0	22.1	0.0	
	4	.0	0.7 T	0.0	27.7	28.4	33.5	0.0	
		1.00	0.4 T	0.0	0.0	0.4	22.1	0.0	
	5	.0	0.7 C	0.0	27.7	28.4	33.5	0.0	
		1.00	0.4 C	0.0	0.0	0.4	22.1	0.0	
	6	.0	0.1 C	0.9	27.5	27.6	33.3	1.3	
		1.00	0.1 C	0.0	0.0	0.1	22.0	0.6	
	7	.0	0.0	0.9	27.5	27.5	33.3	1.3	
		1.00	0.0	0.0	0.0	0.0	22.0	0.6	
	8	.0	0.0 C	0.0	0.0	0.0	0.0	0.0	
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0	
5	1	.0	0.0 T	0.2	690.1	690.3	117.8	0.0	
		1.00	0.0 T	0.0	0.0	0.0	117.8	0.0	
	2	.0	6.4 T	19386.4	737.8	20130.6	125.9	3309.3	
		1.00	6.4 T	0.0	0.0	6.4	125.9	3309.3	
	3	.0	6.4 T	18201.8	737.8	18946.1	125.9	3107.1	
		1.00	6.4 T	0.0	0.0	6.4	125.9	3107.1	
	4	.0	6.4 T	19449.4	738.2	20194.0	126.0	3320.1	
		1.00	6.4 T	0.0	0.0	6.4	126.0	3320.1	
	5	.0	6.4 T	18264.5	737.4	19008.3	125.9	3117.8	
		1.00	6.4 T	0.0	0.0	6.4	125.9	3117.8	
	6	.0	10.8 T	19419.5	737.9	20168.2	126.0	3315.0	
		1.00	10.8 T	0.0	0.0	10.8	126.0	3315.0	
	7	.0	2.1 T	18234.8	733.0	18969.9	125.1	3112.8	
		1.00	2.1 T	0.0	0.0	2.1	125.1	3112.8	
	8	.0	44.7 C	50.4	0.0	95.2	0.0	8.6	
		1.00	44.7 C	0.0	0.0	44.7	0.0	8.6	
6	1	.0	0.0 C	0.0	580.7	580.7	99.1	0.0	
		1.00	0.0 C	0.0	0.0	0.0	99.1	0.0	
	2	.0	95.9 C	18101.0	533.0	18730.0	91.0	3089.9	
		1.00	95.9 C	0.0	0.0	95.9	91.0	3089.9	
	3	.0	95.9 C	19487.2	533.0	20116.2	91.0	3326.6	
		1.00	95.9 C	0.0	0.0	95.9	91.0	3326.6	
	4	.0	95.9 C	18152.9	532.6	18781.5	90.9	3098.8	
		1.00	95.9 C	0.0	0.0	95.9	90.9	3098.8	
	5	.0	95.9 C	19538.7	533.5	20168.1	91.1	3335.3	
		1.00	95.9 C	0.0	0.0	95.9	91.1	3335.3	
	6	.0	100.3 C	18067.9	528.2	18696.4	90.2	3084.3	
		1.00	100.3 C	0.0	0.0	100.3	90.2	3084.3	

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
		7 .0	91.6 C	19454.0	533.2	20078.7	91.0	3320.9
		1.00	91.6 C	0.0	0.0	91.6	91.0	3320.9
		8 .0	44.7 C	50.5	0.0	95.2	0.0	8.6
		1.00	44.7 C	0.0	0.0	44.7	0.0	8.6
7	1	.0	0.0 C	0.1	725.8	725.9	123.9	0.0
		1.00	0.0 C	0.0	0.0	0.0	123.9	0.0
	2	.0	2.0 T	103.4	678.1	783.5	115.8	17.7
		1.00	2.0 T	0.0	0.0	2.0	115.8	17.7
	3	.0	2.0 T	0.7	678.1	680.8	115.8	0.1
		1.00	2.0 T	0.0	0.0	2.0	115.8	0.1
	4	.0	2.0 T	103.6	677.7	783.3	115.7	17.7
		1.00	2.0 T	0.0	0.0	2.0	115.7	17.7
	5	.0	2.0 T	0.5	678.5	681.1	115.8	0.1
		1.00	2.0 T	0.0	0.0	2.0	115.8	0.1
	6	.0	2.9 T	103.5	673.3	779.7	114.9	17.7
		1.00	2.9 T	0.0	0.0	2.9	114.9	17.7
	7	.0	1.2 T	0.6	678.2	680.0	115.8	0.1
		1.00	1.2 T	0.0	0.0	1.2	115.8	0.1
	8	.0	8.5 C	50.4	0.0	58.9	0.0	8.6
		1.00	8.5 C	0.0	0.0	8.5	0.0	8.6
8	1	.0	0.0 T	0.1	634.7	634.8	108.3	0.0
		1.00	0.0 T	0.0	0.0	0.0	108.3	0.0
	2	.0	19.0 C	99.9	682.4	801.3	116.5	17.1
		1.00	19.0 C	0.0	0.0	19.1	116.5	17.1
	3	.0	19.0 C	2.8	682.4	704.2	116.5	0.5
		1.00	19.0 C	0.0	0.0	19.0	116.5	0.5
	4	.0	19.0 C	100.0	682.8	801.8	116.6	17.1
		1.00	19.0 C	0.0	0.0	19.0	116.6	17.1
	5	.0	19.0 C	2.9	682.0	703.9	116.4	0.5
		1.00	19.0 C	0.0	0.0	19.0	116.4	0.5
	6	.0	19.9 C	99.8	682.5	802.2	116.5	17.0
		1.00	19.9 C	0.0	0.0	19.9	116.5	17.0
	7	.0	18.2 C	2.7	677.6	698.4	115.7	0.5
		1.00	18.2 C	0.0	0.0	18.2	115.7	0.5
	8	.0	8.5 C	50.4	0.0	58.9	0.0	8.6
		1.00	8.5 C	0.0	0.0	8.5	0.0	8.6
9	1	.0	92.6 C	0.1	0.2	92.9	0.0	0.0
		1.00	92.6 C	0.0	0.0	92.6	0.0	0.0
	2	.0	99.0 C	88.2	24214.7	24401.9	4136.7	15.1
		1.00	99.0 C	0.0	0.0	99.0	4136.7	15.1
	3	.0	99.0 C	88.2	22735.1	22922.3	3883.9	15.1
		1.00	99.0 C	0.0	0.0	99.0	3883.9	15.1
	4	.0	99.1 C	88.1	24293.4	24480.5	4150.1	15.1
		1.00	99.1 C	0.0	0.0	99.1	4150.1	15.1
	5	.0	99.0 C	88.3	22813.3	23000.6	3897.3	15.1
		1.00	99.0 C	0.0	0.0	99.0	3897.3	15.1

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
		6 .0	99.0 C	147.9	24256.0	24502.9	4143.7	25.3
		1.00	99.0 C	0.0	0.0	99.0	4143.7	25.3
		7 .0	98.4 C	28.5	22776.3	22903.3	3891.0	4.9
		1.00	98.4 C	0.0	0.0	98.4	3891.0	4.9
		8 .0	0.0 C	612.9	63.0	675.9	10.8	104.7
		1.00	0.0 C	0.0	0.0	0.0	10.8	104.7
10		1 .0	92.1 C	0.2	12.6	104.9	0.3	0.0
		1.00	92.1 C	0.0	0.1	92.1	0.3	0.0
		2 .0	4303.8 T	434.5	4687.2	9425.5	445.4	10.7
		1.00	4303.8 T	9.8	12983.1	17296.8	445.4	10.7
		3 .0	4231.8 C	434.6	4374.9	9041.2	417.5	10.7
		1.00	4231.8 C	9.8	12190.0	16431.6	417.5	10.7
		4 .0	4318.1 T	434.1	4702.4	9454.6	446.8	10.7
		1.00	4318.1 T	9.8	13025.3	17353.2	446.8	10.7
		5 .0	4245.9 C	435.0	4390.0	9070.9	419.0	10.7
		1.00	4245.9 C	9.8	12231.9	16487.7	419.0	10.7
		6 .0	4311.3 T	728.5	4695.2	9735.0	446.1	17.9
		1.00	4311.3 T	16.5	13005.3	17333.1	446.1	17.9
		7 .0	4238.6 C	140.6	4382.9	8762.2	418.3	3.5
		1.00	4238.6 C	3.2	12212.1	16453.9	418.3	3.5
		8 .0	11.5 C	3019.9	12.2	3043.6	1.2	74.4
		1.00	11.5 C	68.3	33.8	113.5	1.2	74.4
11		1 .0	77.9 C	0.1	0.1	78.0	0.0	0.0
		1.00	77.9 C	0.0	0.0	77.9	0.0	0.0
		2 .0	71.5 C	1314.0	22609.1	23994.6	3862.4	224.5
		1.00	71.5 C	0.0	0.0	71.5	3862.4	224.5
		3 .0	71.5 C	1314.1	24340.7	25726.3	4158.2	224.5
		1.00	71.5 C	0.0	0.0	71.5	4158.2	224.5
		4 .0	71.5 C	1313.9	22674.0	24059.4	3873.5	224.5
		1.00	71.5 C	0.0	0.0	71.5	3873.5	224.5
		5 .0	71.6 C	1314.2	24405.0	25790.7	4169.2	224.5
		1.00	71.6 C	0.0	0.0	71.6	4169.2	224.5
		6 .0	70.9 C	1373.7	22567.7	24012.4	3855.3	234.7
		1.00	70.9 C	0.0	0.0	70.9	3855.3	234.7
		7 .0	71.5 C	1254.4	24299.1	25625.0	4151.1	214.3
		1.00	71.5 C	0.0	0.0	71.5	4151.1	214.3
		8 .0	0.0 T	612.9	63.1	676.0	10.8	104.7
		1.00	0.0 T	0.0	0.0	0.0	10.8	104.7
12		1 .0	77.5 C	0.2	10.5	88.3	0.3	0.0
		1.00	77.5 C	0.0	0.0	77.5	0.3	0.0
		2 .0	4039.3 T	6474.4	4373.6	14887.2	415.8	159.5
		1.00	4039.3 T	146.4	12122.3	16307.9	415.8	159.5
		3 .0	4496.3 C	6474.5	4688.5	15659.3	447.1	159.5
		1.00	4496.3 C	146.4	13050.8	17693.5	447.1	159.5
		4 .0	4051.1 T	6474.0	4386.1	14911.2	417.0	159.5
		1.00	4051.1 T	146.4	12157.1	16354.6	417.0	159.5

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z	
		5	.0	4508.1 C	6474.9	4700.9	15683.8	448.3	159.5
			1.00	4508.1 C	146.4	13085.3	17739.8	448.3	159.5
		6	.0	4032.4 T	6768.4	4365.5	15166.3	415.0	166.7
			1.00	4032.4 T	153.1	12100.1	16285.5	415.0	166.7
		7	.0	4488.8 C	6180.5	4680.4	15349.8	446.4	152.3
			1.00	4488.8 C	139.8	13028.5	17657.1	446.4	152.3
		8	.0	11.5 C	3020.0	12.2	3043.6	1.2	74.4
			1.00	11.5 C	68.3	33.8	113.6	1.2	74.4
13		1	.0	306.7 C	5.8	1.2	313.7	0.0	0.2
			1.00	306.7 C	0.0	0.0	306.7	0.0	0.2
		2	.0	286.5 C	4751.7	676.7	5715.0	12.6	176.5
			1.00	286.5 C	0.0	0.0	286.5	12.6	176.5
		3	.0	286.5 C	33.2	676.8	996.5	12.6	1.2
			1.00	286.5 C	0.0	0.0	286.5	12.6	1.2
		4	.0	286.4 C	4759.7	678.7	5724.7	12.6	176.8
			1.00	286.4 C	0.0	0.0	286.4	12.6	176.8
		5	.0	286.7 C	25.3	674.9	986.9	12.5	0.9
			1.00	286.7 C	0.0	0.0	286.7	12.5	0.9
		6	.0	284.5 C	4755.9	968.5	6008.9	18.0	176.6
			1.00	284.5 C	0.0	0.0	284.5	18.0	176.6
		7	.0	286.6 C	29.0	385.1	700.6	7.2	1.1
			1.00	286.6 C	0.0	0.0	286.6	7.2	1.1
		8	.0	0.0 T	2317.4	2855.2	5172.5	53.0	86.1
			1.00	0.0 T	0.0	0.0	0.0	53.0	86.1
14		1	.0	268.2 C	4.9	1.2	274.3	0.0	0.2
			1.00	268.2 C	0.0	0.0	268.2	0.0	0.2
		2	.0	288.3 C	4590.8	6387.1	11266.3	118.6	170.5
			1.00	288.3 C	0.0	0.0	288.3	118.6	170.5
		3	.0	288.3 C	127.7	6387.2	6803.2	118.6	4.7
			1.00	288.3 C	0.0	0.0	288.3	118.6	4.7
		4	.0	288.5 C	4597.4	6389.1	11274.9	118.7	170.8
			1.00	288.5 C	0.0	0.0	288.5	118.7	170.8
		5	.0	288.1 C	134.2	6385.3	6807.7	118.6	5.0
			1.00	288.1 C	0.0	0.0	288.1	118.6	5.0
		6	.0	288.4 C	4586.6	6678.9	11553.9	124.0	170.4
			1.00	288.4 C	0.0	0.0	288.4	124.0	170.4
		7	.0	286.3 C	123.5	6095.5	6505.2	113.2	4.6
			1.00	286.3 C	0.0	0.0	286.3	113.2	4.6
		8	.0	0.0 C	2317.4	2855.2	5172.6	53.0	86.1
			1.00	0.0 C	0.0	0.0	0.0	53.0	86.1
15		1	.0	0.6 C	0.0	0.2	0.8	0.2	0.0
			1.00	0.6 C	0.2	10.4	11.1	0.2	0.0
		2	.0	5258.2 C	53.6	11231.5	16543.3	322.5	4.4
			1.00	5258.2 C	265.9	4470.6	9994.7	322.5	4.4
		3	.0	4935.8 T	53.6	10545.2	15534.6	302.4	4.4
			1.00	4935.8 T	266.0	4176.1	9377.8	302.4	4.4

MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
		4 .0	5275.3 C	53.6	11268.0	16596.9	323.6	4.4
		1.00	5275.3 C	265.7	4485.1	10026.1	323.6	4.4
		5 .0	4952.8 T	53.7	10581.4	15587.9	303.4	4.4
		1.00	4952.8 T	266.2	4190.5	9409.5	303.4	4.4
		6 .0	5267.2 C	89.9	11250.7	16607.8	323.1	7.3
		1.00	5267.2 C	445.9	4478.2	10191.2	323.1	7.3
		7 .0	4944.8 T	17.4	10564.3	15526.4	302.9	1.4
		1.00	4944.8 T	86.1	4183.7	9214.6	302.9	1.4
		8 .0	13.7 T	372.8	29.2	415.7	0.8	30.3
		1.00	13.7 T	1848.4	11.6	1873.7	0.8	30.3
16		1 .0	0.5 C	0.0	0.1	0.6	0.2	0.0
		1.00	0.5 C	0.2	8.7	9.3	0.2	0.0
		2 .0	4909.4 C	799.1	10486.8	16195.4	301.1	65.0
		1.00	4909.4 C	3962.8	4171.8	13044.0	301.1	65.0
		3 .0	5284.6 T	799.2	11289.9	17373.6	323.8	65.0
		1.00	5284.6 T	3962.8	4474.8	13722.2	323.8	65.0
		4 .0	4923.5 C	799.1	10516.9	16239.5	302.0	65.0
		1.00	4923.5 C	3962.5	4183.8	13069.8	302.0	65.0
		5 .0	5298.5 T	799.2	11319.7	17417.4	324.7	65.0
		1.00	5298.5 T	3963.1	4486.6	13748.2	324.7	65.0
		6 .0	4900.4 C	835.4	10467.6	16203.5	300.6	67.9
		1.00	4900.4 C	4142.7	4164.1	13207.3	300.6	67.9
		7 .0	5275.5 T	762.9	11270.6	17309.0	323.3	62.0
		1.00	5275.5 T	3782.9	4467.1	13525.6	323.3	62.0
		8 .0	13.7 T	372.8	29.3	415.7	0.8	30.3
		1.00	13.7 T	1848.4	11.6	1873.7	0.8	30.3
300		1 .0	0.0 T	0.0	250.2	250.2	32.6	0.0
		1.00	0.0 T	0.0	0.0	0.0	32.6	0.0
		2 .0	150.8 C	0.0	250.2	401.0	32.6	0.0
		1.00	150.8 C	0.0	0.0	150.8	32.6	0.0
		3 .0	150.8 C	0.0	250.2	401.0	32.6	0.0
		1.00	150.8 C	0.0	0.0	150.8	32.6	0.0
		4 .0	150.8 C	14.2	250.2	401.4	32.6	1.8
		1.00	150.8 C	0.0	0.0	150.9	32.6	1.8
		5 .0	150.8 C	14.2	250.2	401.4	32.6	1.8
		1.00	150.8 C	0.0	0.0	150.8	32.6	1.8
		6 .0	151.9 C	0.0	250.2	402.1	32.6	0.0
		1.00	151.9 C	0.0	0.0	152.0	32.6	0.0
		7 .0	149.7 C	0.0	250.2	399.9	32.6	0.0
		1.00	149.7 C	0.0	0.0	149.7	32.6	0.0
		8 .0	0.0 C	0.0	0.0	0.0	0.0	0.0
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

B6 & B7 MANIFOLD SUPPORT  
\*\*\* ( B-7 BOUNDING CASE )

-- PAGE NO. 26

147. PARAMETER  
148. CODE AISC  
149. FYLD 45999.969 MEMB 9 TO 16  
150. WSTR 21000. MEMB 9 TO 16  
151. WMIN 0.188 MEMB 9 TO 16  
152. PUNCH 2.0 MEMB 9 TO 14  
153. CB 1. MEMB 9 TO 16  
154. CMY 1. MEMB 9 TO 16  
155. MAIN 0. MEMB 9 TO 16  
156. RATIO 1. MEMB 9 TO 16  
157. CHECK CODE MEMB 9 TO 16

STAAD-III CODE CHECKING - (AISC)  
 \*\*\*\*\*

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
9	ST TUB 40408	PASS 629.82 C	AISC- H1-3 909.31	0.888 149174.25	6 0.00
10	ST TUB 40408	PASS 27462.96 T	AISC- H2-1 -60.37	0.629 -80105.75	4 61.00
11	ST TUB 40408	PASS 455.33 C	AISC- H1-3 8082.13	0.934 -150090.58	5 0.00
12	ST TUB 40408	PASS 28671.43 C	AISC- H1-2 -900.45	0.643 80474.39	5 61.00
13	ST TUB 40203	PASS 578.43 C	PUNCHING SHR 6187.57	0.689 -1323.37	4 0.00
14	ST TUB 40203	PASS 582.06 C	PUNCHING SHR -174.46	0.694 -12451.36	5 0.00
15	ST TUB 40408	PASS 33499.13 C	AISC- H1-1 553.00	0.627 -69191.77	6 0.00
16	ST TUB 40408	PASS 33698.66 T	AISC- H2-1 4915.14	0.631 69616.13	5 0.00
158. SELECT WELD MEMB 9 TO 16					



STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
9	STA 6	1 16.84	6/16 2762.49	19066.61 18865.41
9	END 4	1 20.07	3/16 5533.49	5537.51 210.02
10	STA 6	1 46.68	3/16 617.61	17489.86 17478.89
10	END 4	1 16.69	5/16 365.60	17521.33 17517.51
11	STA 5	1 149.67	6/16 2779.46	20041.71 19847.48
11	END 5	1 299.34	3/16 5558.91	5569.03 151.78
12	STA 5	1 311.19	4/16 599.98	20066.28 20054.90
12	END 5	1 248.95	5/16 479.98	17948.66 17940.51
13	STA 6	1 39.26	3/16 11.99	4544.02 4543.84
13	END 1	1 0.05	3/16 0.02	275.31 275.31
14	STA 6	1 37.86	3/16 82.69	8876.14 8875.67
14	END 6	1 37.86	3/16 82.69	274.40 258.89
15	STA 6	1 52.09	5/16 304.72	17164.33 17161.54
15	END 6	1 86.82	3/16 507.86	18744.22 18737.14
16	STA 5	1 463.01	5/16 670.76	17937.95 17919.42
16	END 5	1 578.76	4/16 838.46	18196.77 18168.22

B6 & B7 MANIFOLD SUPPORT  
\*\*\* ( B-7 BOUNDING CASE )

-- PAGE NO. 29

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

---

\*\*\*\*\* END OF TABULATED WELD DESIGN \*\*\*\*\*

159. FINISH

\*\*\*\*\* END OF STAAD-III \*\*\*\*\*

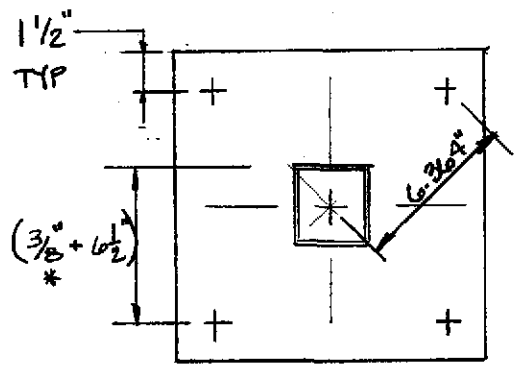
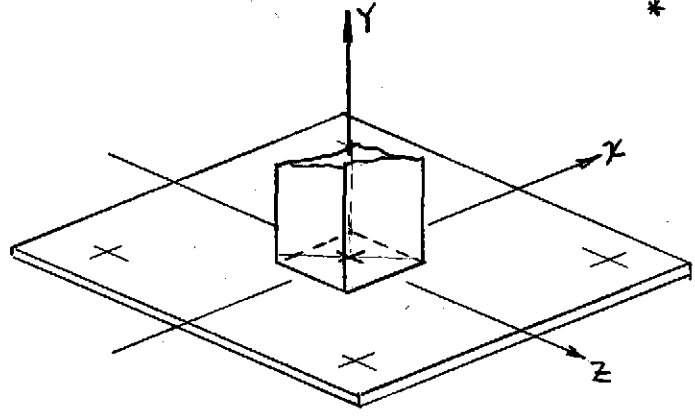
\*\*\*\* DATE= SEP 25,1996 TIME= 16:11: 7 \*\*\*\*

\*\*\*\*\*  
\* For questions on STAAD-III, contact: \*  
\* Research Engineers, Inc at \*  
\* Ph: (714) 974-2500 Fax: (714) 921-2543 \*  
\*\*\*\*\*

DESIGN ANCHORAGE

TRY PL 12"x12"

JT's B f 11



\* DIMENSION considers weld at T.S. to PL.

WORST CASE SUPPORT REACTIONS @ JT 11 LOADCASE 6

$F_x = 1660 \text{ lbs}$	$M_x = 41626 \text{ in-lbs}$
$F_y = 25646 \text{ lbs (TENSION)}$	$M_y = 1691 \text{ in-lbs}$
$F_z = 667 \text{ lbs}$	$M_z = 26848 \text{ in-lbs}$

BOLTS

TENSION

$$T = \frac{25646 \text{ lbs}}{4 \text{ BOLTS}} + \frac{41626 \text{ in-lbs} + 26848 \text{ in-lbs}}{2 (6.875 \text{ in})}$$

$$= 11391 \text{ lbs/BOLT}$$

\* include 3/8" fillet all around weld

SHEAR

$$V = \frac{1660 \text{ lbs} + 667 \text{ lbs}}{4 \text{ BOLTS}} + \frac{1691 \text{ in-lbs}}{4 \text{ BOLTS} (6.3125 \text{ in})}$$

$$= 648 \text{ lbs/BOLT}$$

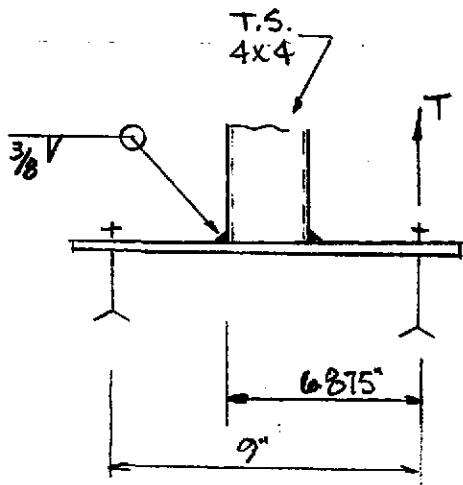
TRY 1"  $\phi$  HILTI HVA @ 12 3/8" EMBT TAIL = 12120 lbs VAIL = 7630 lbs

$$\left(\frac{11391}{12120}\right)^{5/3} + \left(\frac{648}{7630}\right)^{5/3} = 0.92 < 1.0 \therefore \text{O.K.}$$

STO BOLT OK

**USE 1"  $\phi$  HILTI HVA @ 12 3/8" EMBT**

DETERMINE PLATE THICKNESS



$$F_y = 36000 \text{ #/in}^2$$

$$F_b = .75 F_y = 27000 \text{ #/in}^2$$

$$f_b = \frac{M}{S} \Rightarrow S = \frac{M}{f_b}$$

$$T = 11391$$

$$S_{req} = \frac{M}{f_b} = \frac{T(6.875 \text{ in})}{27000 \text{ #/in}^2}$$

$$= \frac{(11391 \text{ lbs})(6.875 \text{ in})}{27000 \text{ #/in}^2}$$

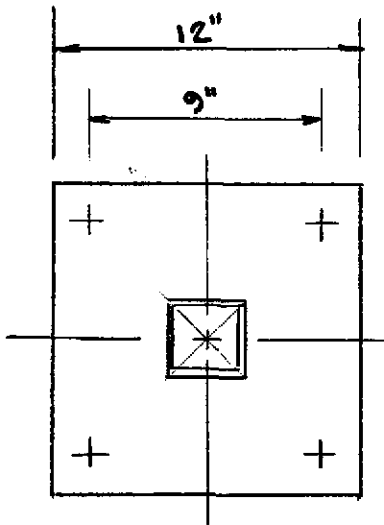
$$S_{reqd} = 2.90 \text{ in}^3$$

$$S = bd^2/6 \Rightarrow d = \sqrt{\frac{6S}{b}}$$

$$= \sqrt{\frac{6(2.90 \text{ in}^3)}{12 \text{ in}}}$$

$$d = THKS = 1.20 \text{ in}$$

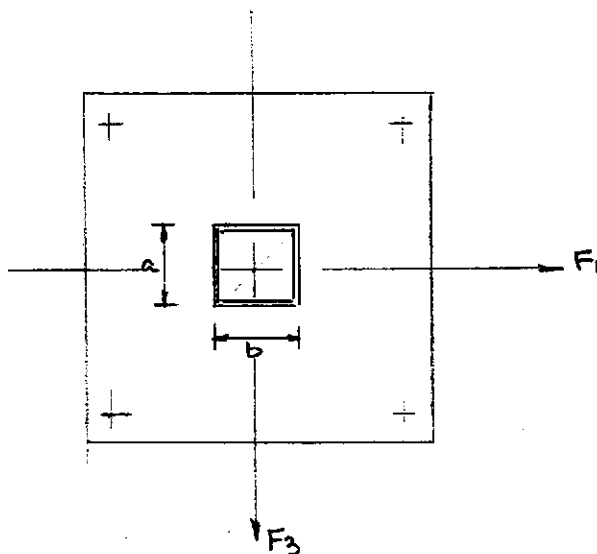
USE PL 1 3/8" THK.



Filename: B-6 & B-7

ALL AROUND RECTANGULAR OR SQUARE FILLET WELD

Between part Jts. 11 & 8 and BASEPLTS



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
1660.00	25646.00	667.00	41626.00	1691.00	26848.00

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)	SKEWED ANGLE (90° > α < 120°)
4.000	4.000	21000	90.000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
16.000	21.333	21.333	85.333	2.000	2.000

EFFECTIVE THROAT CORRECTION FACTOR

Mf  
1.00

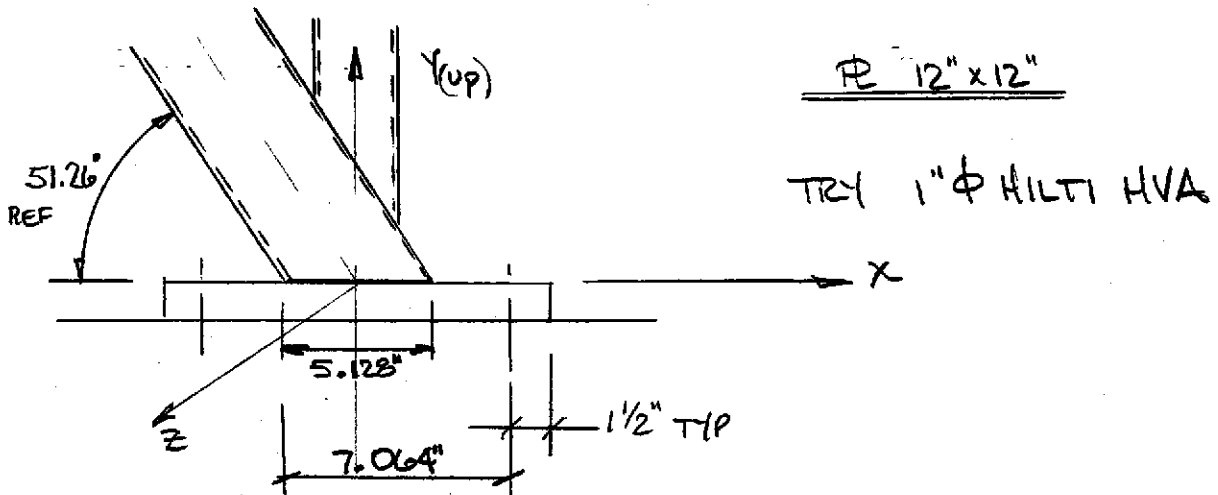
MAXIMUM WELD LOAD (f) - #/INCH

f=  
4815

REQUIRED FILLET WELD SIZE (INCHES)

w=  
0.324

DESIGN ANCHORAGE AT JTS 13 + 15



- FOR JTS 13 + 15 W/OREST LOADING OCCURS AT JT 15 L.C. #5

$F_x = 18472 \text{ lbs}$

$M_x = 35490 \text{ in-lbs}$

$F_y = 27634 \text{ lbs (TENSION)}$

$M_y = 9658 \text{ in-lbs}$

$F_z = 438 \text{ lbs}$

$M_z = 27418 \text{ in-lbs}$

TENSION

$$T = \frac{27634 \text{ lbs}}{4 \text{ BOLTS}} + \frac{35490 \text{ in-lbs}}{2 \text{ BOLTS (6.5in)}} + \frac{27418 \text{ in-lbs}}{2 \text{ BOLTS (7.064in)}}$$

$= 11579 \text{ lbs/BOLT}$

SHEAR

$$V = \frac{18472 \text{ lbs} + 438 \text{ lbs}}{4 \text{ BOLTS}} + \frac{9658 \text{ in-lbs}}{4 \text{ BOLTS (6.364in)}}$$

$= 5107 \text{ lbs/BOLT}$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



TRY 1"  $\phi$  HILTI @ 12<sup>3</sup>/<sub>8</sub>" EMBT

T<sub>ALL</sub> = 12120 lbs

V<sub>ALL</sub> = 7630 lbs

$$\left(\frac{11579 \text{ lbs}}{12120 \text{ lbs}}\right)^{5/3} + \left(\frac{5107 \text{ lbs}}{7630 \text{ lbs}}\right)^{5/3} = .93 + .51 = 1.44$$

1.44 > 1.0 ∴ N.G.

TRY 1"  $\phi$  HILTI HVA - HAS SUPER SAE 4140

T<sub>ALL</sub> = 16450 lbs.

V<sub>ALL</sub> = 13760 lbs.

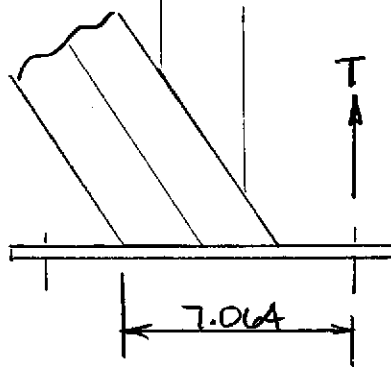
$$\left(\frac{11579 \text{ lbs}}{16450 \text{ lbs}}\right)^{5/3} + \left(\frac{5107 \text{ lbs}}{13760 \text{ lbs}}\right)^{5/3} = .56 + .19 = .75$$

.75 < 1.0 ∴ O.K.

USE 1"  $\phi$  HILTI HVA - HAS SUPER  
 SAE-4140  
 @ 12<sup>3</sup>/<sub>8</sub>" EMBT

BASEPLATE

PL 12" x 12"



T = 11579 lbs.

F<sub>y</sub> = 36000 psi    F<sub>b</sub> = .75 F<sub>y</sub> = 27000 psi<sup>2</sup>

f<sub>b</sub> = M/s ∴ s = M/f<sub>b</sub>

S<sub>REQ'D</sub> = M/f<sub>b</sub> = T(7.064 in) / 27000 psi<sup>2</sup>

S<sub>REQ'D</sub> = 3.029 in<sup>3</sup>

S = bd<sup>2</sup>/6

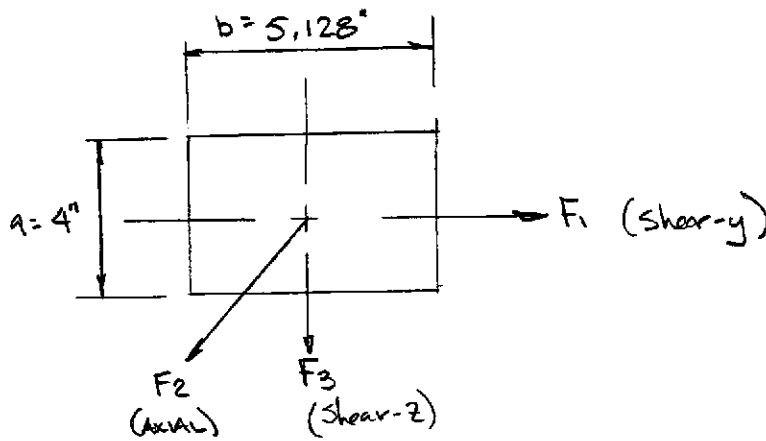
d =  $\sqrt{\frac{6S}{b}}$  =  $\sqrt{\frac{6(3.029)}{12 \text{ in}}}$  = 1.23 in

USE PL 12" x 12" x 1<sup>3</sup>/<sub>8</sub>"



ALL AROUND RECTANGULAR OR SQUARE FILLET WELD

Between part MEM 15 & 16 and BASEPLTS



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
1294.00	33551.00	17.43	1634.00	367.00	27583.00

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)	SKEWED ANGLE (90° > α < 120°)
4.000	5.128	21000	90.000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
18.256	25.845	29.277	126.758	2.000	2.564

EFFECTIVE THROAT CORRECTION FACTOR

Mf  
1.00

MAXIMUM WELD LOAD (f) - #/INCH

f=  
2844

REQUIRED FILLET WELD SIZE (INCHES)

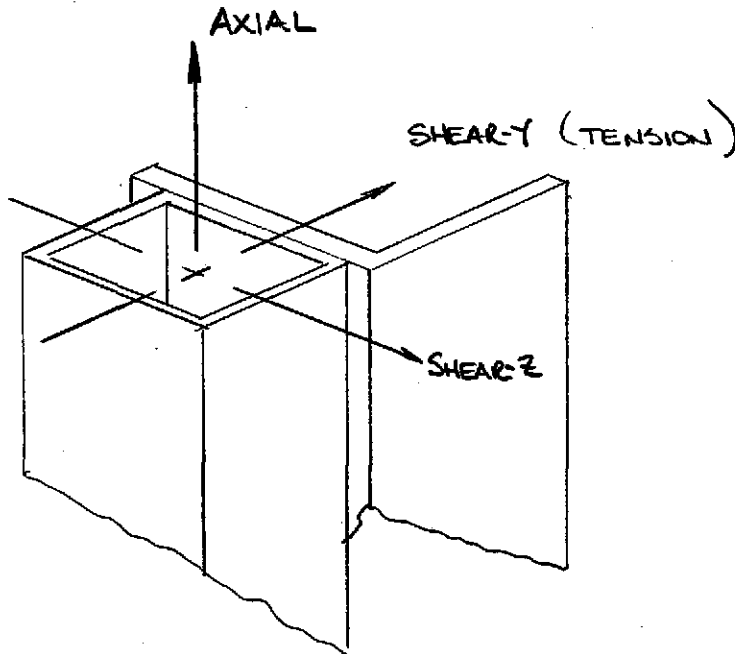
w=  
0.192

USE 1/4" fillet 3 sides + 1 side penetration fill



# DESIGN THRU BOLT CONNECTION

MEMBER 9 JOINT 6  
 MEMBER 11 JOINT 9  
 MEMBER 13 JOINT 12  
 MEMBER 14 JOINT 14



Worst loading occurs @ MEMBER 11 JT 9.

ENVELOPE  
OF  
LOADS

$$\left. \begin{aligned} \text{AXIAL} &= 496. \text{ lbs} \\ \text{SHEAR-Y} &= 16677. \text{ lbs.} \\ \text{SHEAR-Z} &= 939. \text{ lbs.} \end{aligned} \right\}$$

## SHEAR

$$V = \frac{496. \text{ lbs} + 939. \text{ lbs}}{3 \text{ BOLTS}} = 478. \text{ lbs/BOLT}$$

## TENSION

$$T = \frac{16677. \text{ lbs}}{3 \text{ BOLTS}} = 5559. \text{ lbs/BOLT}$$

TRY 5/8"  $\phi$  A325 BOLTS T<sub>ALL</sub> = 13500. V<sub>ALL</sub> = 5220 lbs.

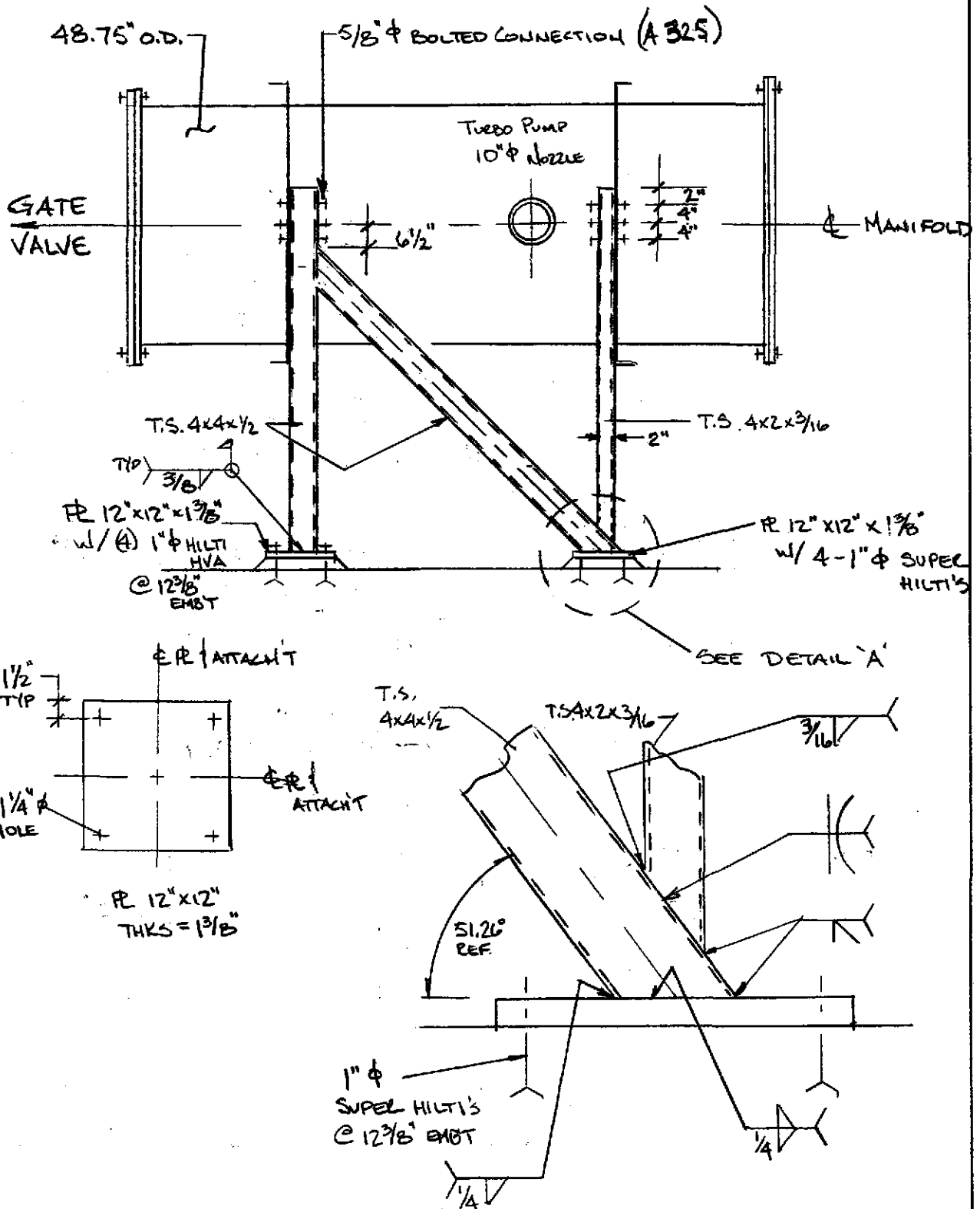
$$\frac{5559(1.2)}{13500} + \frac{478}{5220} = .59 < 1.0 \therefore \text{OK.}$$

**USE 5/8"  $\phi$  A325 BOLTS**



# B6 & B7 SUPPORT DETAIL

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



PROCESS SYSTEMS INTERNATIONAL, INC.  
WESTBOROUGH, MA

ENGINEERING  
CALCULATIONS

NO: V049-1-098

PAGE 1 OF 17

REV.	DEO #	DATE	BY:	CHECK
0	139	4-22-96	AGR	RDC

TITLE:  
MAIN TURBO CART  
FRAME EXTENSION

By: ART ROUSSOPOULOS DEPT.: 749

PROJECT: LIGO

PROJECT NO: V59049

PURPOSE: VERIFY THE STRUCTURAL ADEQUACY OF THE  
FRAME EXTENSION

METHOD: CLASSICAL STRESS ANALYSIS

ASSUMPTIONS: SEE CALCS

INPUTS: EDWARDS DWG D-4507  
PSI DWG V049-4-012

REFERENCES: BLODGETT "DESIGN OF WELDED STRUCTURES" - 1982  
AISC - SCM - 9TH ED.  
ROARK, "FORMULAS OF STRESS + STRAIN, 5TH ED.  
MACHINE DESIGN - THEORY + PRACTICE - 1975

CALCULATIONS: (SEE ATTACHED)

CONCLUSIONS: THE SUBJECT FRAME CART IS STRUCTURALLY ADEQUATE  
PER THE DESIGN SKETCHES

NOTES:

# TABLE OF CONTENTS

	<u>PAGE</u>
1.0 - DESIGN SKETCH	3
• SHEET 1	3
• SHEET 2	4
2.0 - DESIGN CRITERIA	5
3.0 - ALLOWABLE STRESSES	5
4.0 - DESIGN	5
4.1 • MODEL	5
4.2 • OPERATIONAL STRESSES	6
4.2.1 - STRESS ON C4X7.25 - A SIDE	6
4.2.2 - VERTICAL C4X7.25 LEG	9
4.2.3 - STRESS ON C4X7.25 - B SIDE	11
4.3 • EXCURSION STRESSES	12
4.4 • CONNECTION DETAILS	13
4.4.1 - ANCHOR BOLT SIZING	13
4.4.2 - PUMP FRAME TO EXTENSION FRAME EXTENSION	13
4.4.2.1 • LOADS	14
4.4.2.2 • BOLTING	15
4.4.2.3 • BOLT PRELOAD	15
4.4.2.4 • BOLT TORQUE	16
4.4.2.5 • SPECIAL WASHER DESIGN	17

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

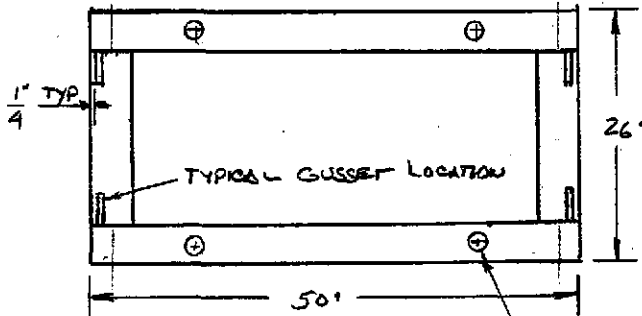


1.0 -

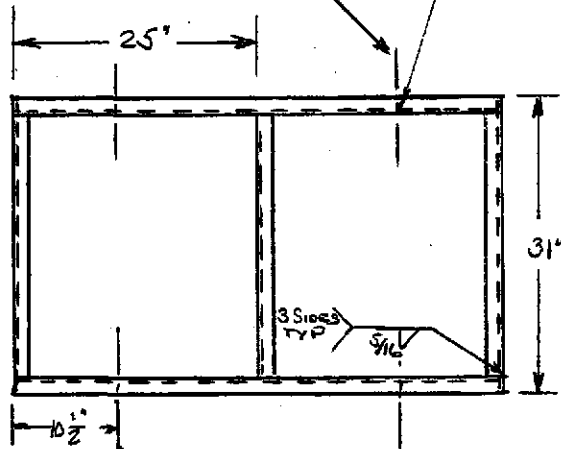
# DESIGN SKETCH

SK-V049-1-098, REV 0 = SHEET 1 OF 2

- ALL MEMBERS ARE C 4 x 7.25
- MATERIAL: A36



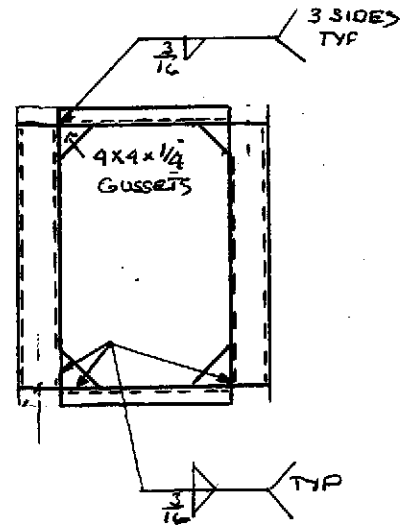
SEE SHEET #2  
FOR CONNECTION DETAILS



3/16" DRILL  
(FOUR LOCATIONS BOTTOM SIDE)

- SPECIFY: HILTI HFA 3/4 FOR  
6 5/8" EMBEDMENT DEPTH

15/8" DRILL (FOUR LOCATIONS TOP SIDE)

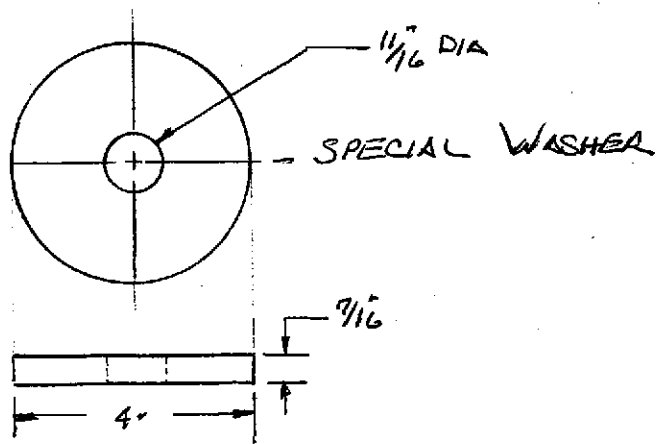
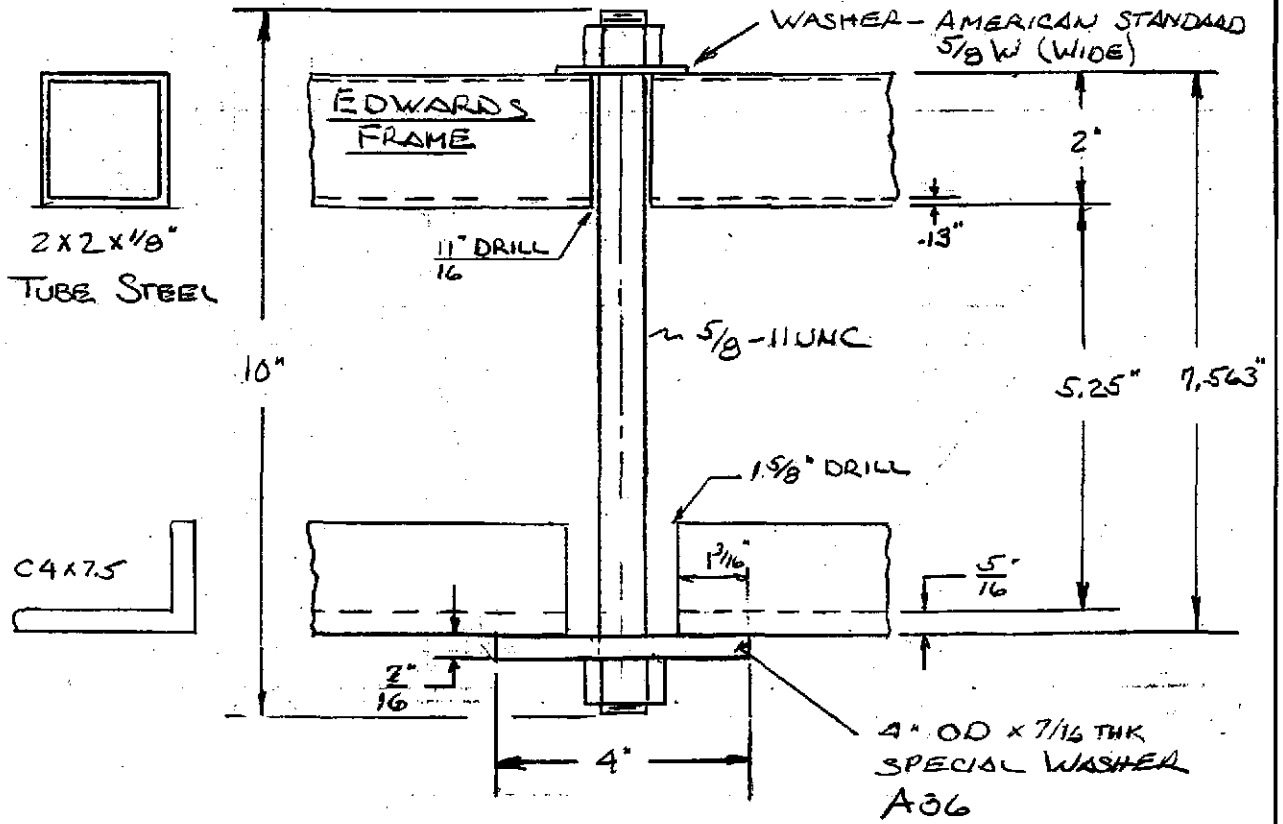


22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



# DESIGN SKETCH

SK-V049-1-098, REV 0 SHEET 2 OF 2



## CONNECTION DETAILS

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



2. - DESIGN CRITERIA

- OPERATIONAL LOAD AT Q OF TURBO PUMP

$$F = PA = 15 \frac{\#}{IN^2} \times \frac{\pi (10)^2}{4} IN^2 = 1178 \#$$

WHERE  $P_{ATM} = 15 \#/IN^2$

10" = PUMP I.D.

- EXCURSION LOAD

EXCURSION LOAD SHALL BE BASED ON AN ACCIDENT CONDITION OF STALLED TORQUE GENERATING A MOMENT LOAD OF 5200# AT ANCHOR BOLT LOCATIONS IN THE DIRECTION OF ROTATION

- DESIGN TEMP = 100°F

3. - ALLOWABLE STRESSES

- OPERATIONAL LOAD:

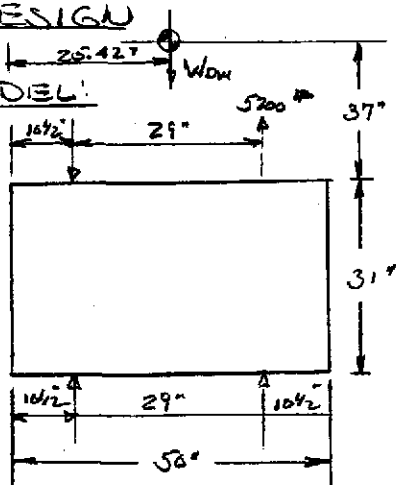
$$- T_{ALLOW} = .6 S_y = .6 (36,000) = 21,600 \text{ PSI}$$

- EXCURSION LOAD

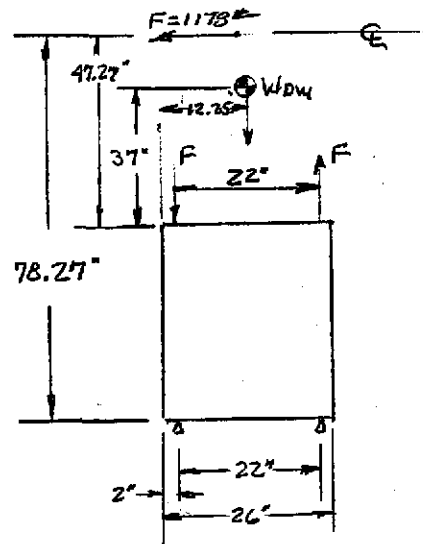
$$- T_{ALLOW} = .9 S_y = .9 (36,000) = 32,400 \text{ PSI}$$

4. - DESIGN

4.1 MODEL:



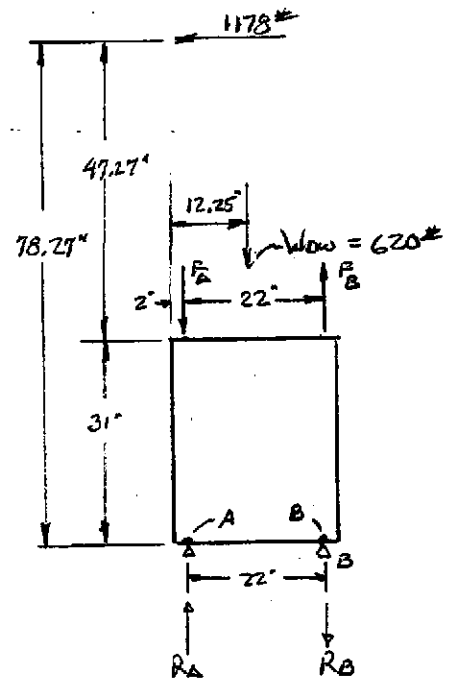
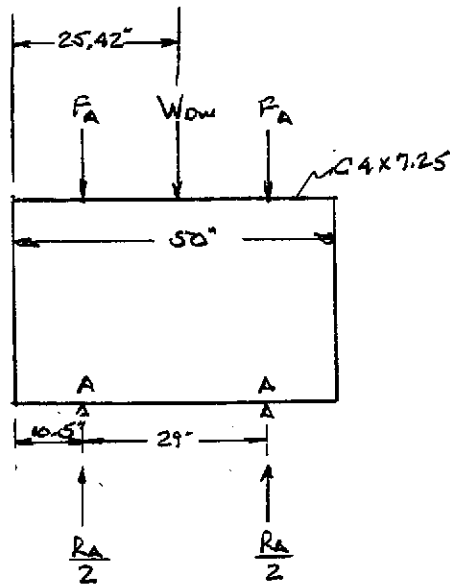
EXCURSION CONDITION



OPERATING CONDITION



## 4.2 OPERATIONAL STRESSES



### • REACTION LOADS $R_A, R_B$

$$\sum M_A = 0 = -78.27(1178) + 10.25(620) + 22 R_B = 0$$

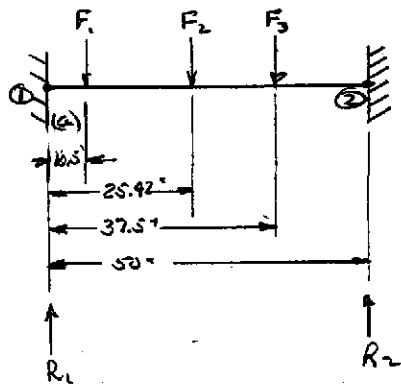
$$R_B = \frac{78.27(1178) - 10.25(620)}{22} = 3902 \#$$

$$\sum M_B = 0 = -78.27(1178) - 11.75(620) + 22 R_A = 0$$

$$R_A = \frac{78.27(1178) + 11.75(620)}{22} = 4522 \#$$

$$\therefore F_A = \frac{R_A}{2} = \frac{4522}{2} = 2261 \#$$

### 4.2.1 • STRESS ON C4 x 7.25 BEAM 50" LONG - A SIDE



REF. BLODGETT, CASE 4AB, P. 8.1-11

$$R_1 = \frac{Fb^2(3a+b)}{L^3} ; R_2 = \frac{Fa^2(a+3b)}{L^3}$$

$$M_1 = \frac{F_1 ab^2}{L^2} ; M_2 = \frac{F_2 a^2 b}{L^2} ; M_3 = \frac{2F_3 ab^2}{L^3}$$

C4 x 7.25

$$S_x = 2.29 \text{ in}^3, r_x = .450", r_y = 1.47"$$

$$A = 2.13 \text{ in}^2$$



4.2.1 CONT

- LOAD  $F_1 = F_A = 2261 \#$

$$R_1 = \frac{2261(50-10.5)^2(3 \times 10.5 + 39.5)}{50^3} = 2004 \#$$

$$R_2 = 2261 - 2004 = 257 \#$$

$$M_1 = 2261(10.5)(39.5)^2 / (50)^2 = 14,816 \text{ IN-}\#$$

$$M_2 = 2261(10.5)^2(39.5) / (50)^2 = 3,939 \text{ IN-}\#$$

$$M_{a_1} = 2(2261)(10.5)^2(39.5)^2 / (50)^3 = 6223 \text{ IN-}\#$$

$$\tau_{a_1} = 6223 / 2.29 = 2,717 \#/\text{IN}^2$$

- LOAD  $F_2 = W_{OW} = 620 \#$

$$R_1 = 620(24.58)^2(3 \times 25.42 + 24.58) / (50)^3 = 302 \#$$

$$R_2 = 620 - 302 = 318 \#$$

$$M_1 = 620(25.42)(24.58)^2 / (50)^2 = 3,809 \text{ IN-}\#$$

$$M_2 = 620(25.42)^2(24.58) / (50)^2 = 3,939 \text{ IN-}\#$$

$$M_{a_2} = 2(620)(25.42)^2(24.58)^2 / (50)^3 = 3,873 \text{ IN-}\#$$

$$\tau_{a_2} = 3,873 / 2.29 = 1,691 \#/\text{IN}^2$$

- LOAD  $F_3 = F_A = 2261 \#$

$$R_1 = 2261(12.5)^2(3 \times 37.5 + 12.5) / (50)^3 = 353 \#$$

$$R_2 = 2261 - 353 = 1908 \#$$

$$M_1 = 2261(37.5)(12.5)^2 / (50)^2 = 5,299 \text{ IN-}\#$$

$$M_2 = 2261(37.5)^2(12.5) / (50)^2 = 15,898 \text{ IN-}\#$$

$$M_{a_3} = 2(2261)(37.5)^2(12.5)^2 / (50)^3 = 7,949 \text{ IN-}\#$$

$$\tau_{a_3} = 7,949 / 2.29 = 3,471 \text{ PSI}$$



4.2.1 CONT.

SUMMATION OF MOMENTS BY SUPERPOSITION

- AT ①

$$\Sigma M_1 = 14,816 + 3809 + 5299 = 23,924 \text{ IN-}\#$$

$$T_1 = 23,924 / 2.29 = 10,447 \text{ PSI} < .6 S_y \therefore \text{OK}$$

- AT ②

$$\Sigma M_2 = 3939 + 3939 + 15898 = 23,776 \text{ IN-}\#$$

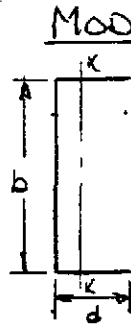
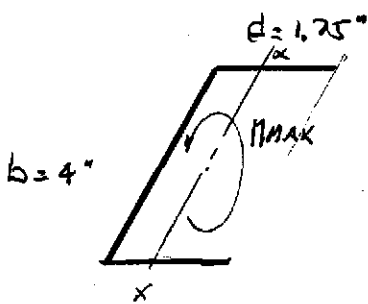
$$T_2 = 23,776 / 2.29 = 10,383 \text{ PSI} < .6 S_y \therefore \text{OK}$$

- AT ③

$$\Sigma M_3 = 6223 + 3873 + 7949 = 18,045 \text{ IN-}\#$$

$$T_3 = 18,045 / 2.29 = 7,880 \text{ PSI} < .6 S_y \therefore \text{OK}$$

CHECK WELD FOR WOLFE CASE END CONDITION



MODEL: REF: BUDGETT, TABLE 5, P. 7.4-7

$$S_w = \frac{2bd + d^2}{3}$$

$$S_w = \frac{2(4)(1.75) + (1.75)^2}{3}$$

$$S_w = 5.69 \text{ IN}^2$$

$$F_{max} = \frac{23924}{5.69} = 4205 \#/\text{IN}$$

- ALLOWABLE WELD TROD STRESS:

$$.3 S_T = .3 (70,000) = 21,000 \text{ PSI}$$

$$\bullet \text{ ALLOWABLE WELD LOAD IS: } .707 (21,000) = 14,847 \text{ PSI}$$

\therefore REQUIRED WELD SIZE IS:

$$W = \frac{4205}{14847} = .283 < 5/16 (.3125) \therefore \text{OK}$$

4.2.1 CONT

4.2.2 • CHECK VERTICAL C4X7.25 LEG - FOR BUCKLING

LR'S

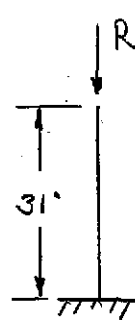
AT ①  $R_{TOT} = 2004 + 302 + 353 = 2659 \#$

AT ②  $R_{TOT} = 257 + 318 + 1908 = 2483 \#$

$R = 2659 \#$  - WORSE CASE

MODEL:

REF. AISC, E2-1, 2, P.5-42



$K = .7$  (BOTH ENDS FIXED)

$$\frac{KL}{r} = \frac{(.7)(31)}{1.47} = 14.8$$

$$C_c = \sqrt{\frac{2\pi^2 E}{F_y}} = \sqrt{\frac{2\pi^2(29 \times 10^6)}{(36,000)}} = 126$$

$\frac{KL}{r} < C_c \therefore$

$$F_a = \frac{\left[1 - \frac{(KL/r)^2}{2C_c^2}\right] F_y}{\frac{5}{3} + \frac{3(KL/r)}{8C_c} - \frac{(KL/r)^3}{8C_c^3}}$$

$$F_a = \frac{\left[1 - \frac{14.8^2}{2(126)^2}\right] 36000}{\frac{5}{3} + \frac{3(14.8)}{8(126)} - \frac{(14.8)^3}{8(126)^3}} = 29901 \# > 2659 \# \therefore \text{OK}$$

- COMPRESSIVE STRESS:

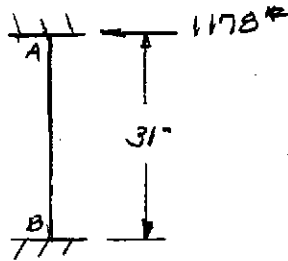
$$\sigma = \frac{2659}{2.13} = 1248 \#/\text{IN}^2 \therefore \text{OK}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



• CHECK FOR LATERAL LOAD

← 1178 #



REF: ROARK, 5TH. ED.,  
CASE 5d, P. 106

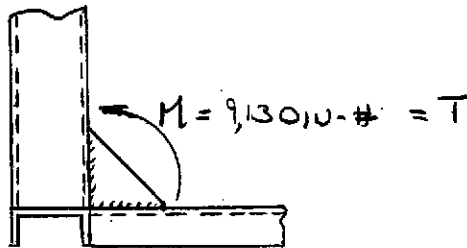
$$M_A = M_B$$

$$\therefore M_{A,B} = 1178(31) = \frac{36518 \text{ IN-#}}{4}$$

$$M_{A \text{ OR } B} = 9,130 \text{ IN-# PER VERTICAL SUPPORT}$$

$$\therefore \tau_{MAX} = \frac{9,130}{2.29} = 3,987 \text{ PSI} < 1.6 S_y \therefore \text{OK}$$

DESIGN GUSSET FOR CORNER WELD CONNECTION

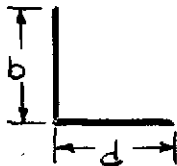


MODEL:

REF: BLOGGETT, TABLE 5, P. 7.4-7

$$b = 4"$$

$$d = 4"$$



$$J = \frac{(b+d)^3 - 6b^2d^2}{12(b+d)}$$

$$J = \frac{(4+4)^3 - 6(4)^2(4)^2}{12(4+4)} = 26.7 \text{ IN}^3$$

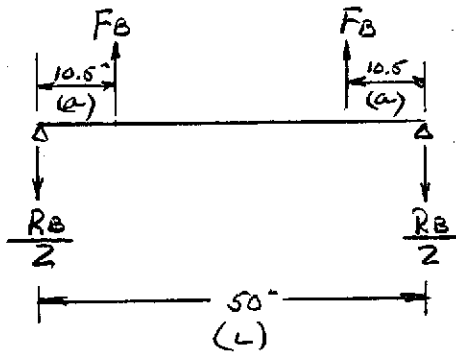
$$f = \frac{Tc}{J_w} = \frac{9130(4)}{26.7} = 1368 \text{ #/IN}$$

REQUIRED WELD SIZE:

$$w = \frac{1368}{14847} = .0921" < " \therefore \text{OK}$$



4.2.3 - STRESS ON C4X7.25 BEAM 50" LONG - B SIDE



REF: BLODGETT, CASE 3AC, P. 8.1-C

$$R_1, R_2 = F$$

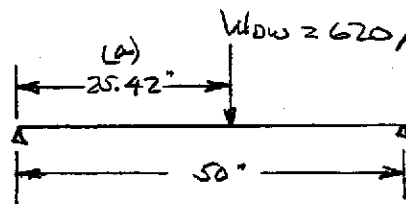
$$M_{MAX} = F_B a$$

$$a = 10.5"$$

$$M_{MAX_1} = 10.5 F_B = 10.5 (1951) = 20,486 \text{ IN-}\#$$

$$\text{WHEREAS: } F_B = \frac{R_B}{2} = \frac{3902}{2} = 1,951 \#$$

$$\tau_{MAX_1} = 20486 / 2.29 = 8,946 \text{ PSI}$$



REF: BLODGETT, CASE 4AB

$$M_{MAX} = M_2 = \frac{F a^2 b}{L^2}$$

$$M_{MAX_2} = \frac{(310)(25.42)^2 (24.58)}{50^2} = 1,969 \text{ IN-}\#$$

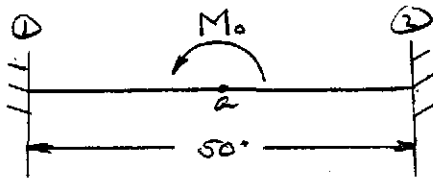
$$\tau_{MAX_2} = 1969 / 2.29 = 859 \text{ PSI}$$

ACTUAL MAX STRESS ON B SIDE

$$\tau_{MAX \text{ ACTUAL}} = 8946 - 859 = 8,087 \text{ PSI} < 1.6 S_y \therefore \text{OK}$$

MAX MOMENT GENERATED ON WELD END CONNECTION IS LESS THAN THE ONE EVALUATED FOR "A" SIDE  $\therefore$  "B" SIDE WELD IS OK

### 4.3 EXCURSION STRESSES



$$M_0 = FL = 6200 \# \times 29" = 150,800 \text{ IN-}\#$$

REF: BLODGETT, CASE 4E, P. 8.1-14

$$M_1 = \frac{M_0 b}{L^2} (L - 3a) \quad ; \quad M_2 = -\frac{M_0 a}{L^2} (2L - 3a)$$

$$\textcircled{1} - M_1 = \frac{(150,800)(25)(50 - 3 \times 25)}{(50)^2} = 37,700 \text{ IN-}\#$$

$$\textcircled{2} - M_2 = -\frac{(150,800)(25)(2 \times 50 - 3 \times 25)}{(50)^2} = -37,700 \text{ IN-}\#$$

$$\tau_{\text{MAX}} = \frac{37,700}{2.29} = 16,463 \text{ PSI} < .9S_y \quad \therefore \text{OK}$$

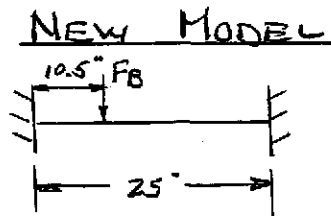
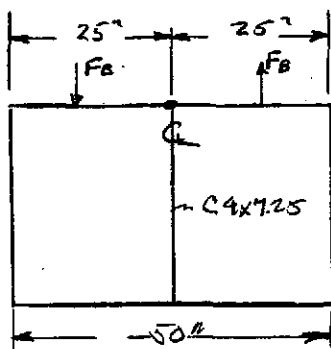
AT CENTER

$$M_{\text{MAX}} = M_0 = 150,800 \text{ IN-}\#$$

$$\tau_{\text{MAX}} = \frac{150,800}{2.29} = 65,851 \text{ PSI} > .9S_y = 33,400 \text{ PSI} \quad \therefore \text{N.G.}$$

SOLUTION:

PROVIDE VERTICAL C4x7.25 SUPPORT AT C  
TO REDUCE MAX MOMENT



REF: BLODGETT,  
CASE 4AB, P. 8.1-11



4.3 CONT.

$$M_{MAX} = \frac{F_a b^2}{L^2} = \frac{5200(10.5)(14.5)^2}{(25)^2} = 18,367 \text{ in}\cdot\#$$

$$f_{MAX} = \frac{18,367}{2.29} = 8,021 \text{ PSI} < .9S_y \therefore \text{OK}$$

#### 4.4 - CONNECTION DESIGNS

##### 4.4.1 - ANCHOR BOLT SIZING

• LOADS:

MAX TENSILE OPERATING LOAD:  $F_B = 1951 \#$   
 EXCURSION:  $5200 \# / \text{BOLT}$

TOTAL TENSILE LOAD  $= 5200 + 1951 = 7151 \#$

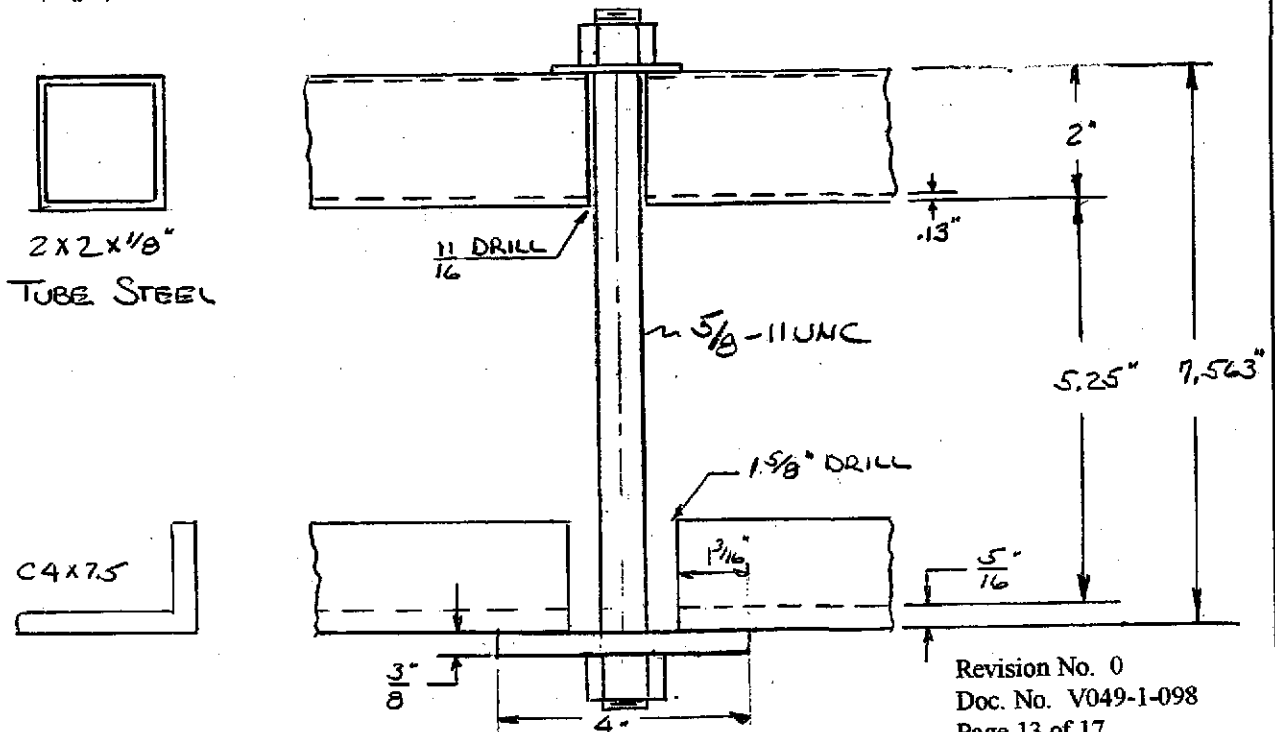
LATERAL SHEAR LOAD  $= \frac{1178}{4} = 295 \# / \text{BOLT}$

SPECIFY HILTI - HFA 3/4 - 6 5/8" EMBEDMENT DEPTH

HVA ALLOWABLE BOND STRENGTH AND STEEL STRENGTH FOR HFA INSERTS - REF: HILTI PRODUCT TECH GUIDE, P. 87

- BOND STRENGTH (4000PSI) =  $7260 \# > 7150 \# \therefore \text{OK}$
- SHEAR STRENGTH =  $7315 \# > 295 \# \therefore \text{OK}$

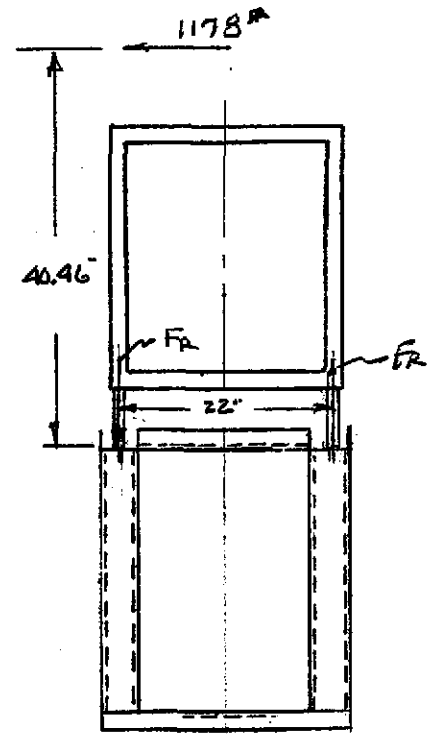
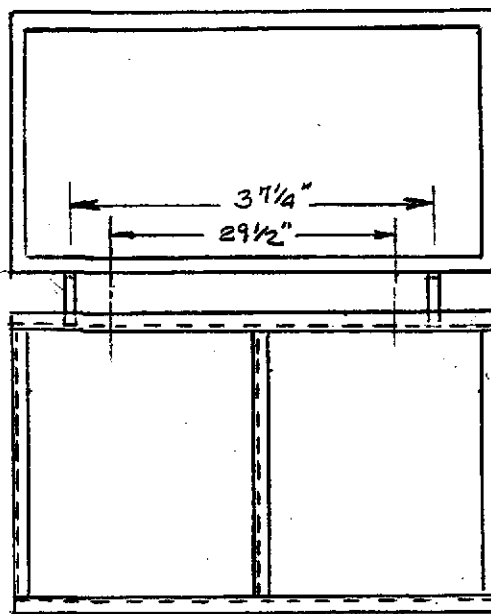
##### 4.4.2 - PUMP FRAME TO EXTENSION FRAME CONNECTION



4.4.2 CONT

4.4.2.1 • LOADS

- OPERATIONAL



$$FR = \frac{40.46(1178)}{22} = 2166 \#$$

$$\text{LOAD PER BOLT} = 2166 / 2 = 1083 \# - \text{TENSILE}$$

$$\text{SHEAR / SUP LOAD} = 1178 / 4 = 295 \#$$

- EXCURSION

$$\text{LOAD PER BOLT} = 5200 \#$$

$$\text{TOTAL LOAD - WORSE CASE} = 5200 + 1083 = 6283 \# - \text{TENSILE}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS





4.4.2 - CONT

4.4.2.2 • BOLTING - SPECIFY A36

ALLOWABLE LOADS:

- OPERATIONAL: REF: AISC, TABLE 1-A, P. 4-3.

5/8-11UNC TENSION - 5900# > 1083# ∴ OK  
 SHEAR - 3000# > 295# ∴ OK

- EXCURSION:

$S_y = 36,000 \text{ PSI}$

$.9S_y = .9(36000) = 32,400 \text{ PSI}$

$\tau = \frac{F}{A} = \frac{6283}{.202} = 31,104 \text{ PSI} < 32,400 \text{ PSI} \therefore \text{OK}$

WHEREAS:  $A = .202 \text{ IN}^2$  - ROOT AREA

4.4.2.3 • BOLT PRELOAD

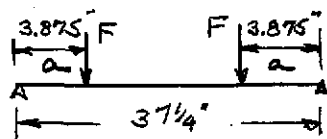
- BOLT PRELOAD SHALL BE BASED ON OPERATIONAL BOLT LOAD PLUS 10%

DESIGN PRELOAD =  $1.1(1083) = 1191 \# \rightarrow 1200 \#$

- CHECK EDWARDS FRAME FOR STRUCTURAL ADEQUACY:

$2 \times 2 \times 1/8" \quad S = \frac{bh^2}{6} = \frac{2(2)^2 - 1.75(1.75)^2}{6} = .515 \text{ IN}^3$

MODEL: REF: BUDGETT, CASE 3AC, P. 8.1-6



$M_{MAX} = Fa = 1200(3.875) = 4650 \text{ IN-#}$

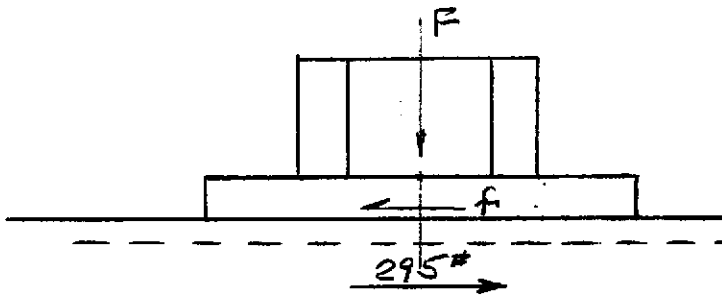
$\tau_{MAX} = \frac{4650}{.515} = 9,029 \text{ PSI} < .6S_y \therefore \text{OK}$

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



4.4.2 CONT

• CHECK FOR SLIP



WASHER - AMERICAN  
STANDARD TYPE B  
5/8 - W (WIDE)

.666" ID  
2.25" OD  
.160" THK

$F = 1200 \#$   
 $\mu = .2$  (ASSUME)

$f = \mu F = .2(1200) = 240 \# < 295 \#$  ACTUAL SHEAR  
 $\therefore$  N.G.

CRITERIA FOR PRELOAD  
SHALL BE BASED ON OPERATIONAL  
SHEAR LOAD PLUS 10%

NEW DESIGN PRELOAD

$(295)(1.1) = 324.5 \rightarrow 325$

$F = \frac{f}{\mu} = \frac{325}{.2} = 1625 \#$  PRELOAD

- CHECK EDWARDS 2X2X1/8" FRAME

$T = \frac{(1625)(3.875)}{.515} = 12,227 \text{ PSI} < .6S_y \therefore$  OK

4.4.2.4 - BOLT TORQUE REF: MACHINE DESIGN, THEORY + PRACTICE, 1975  
P. 816

$T = \mu D F$

$T = .2(.625)(1625) = 2031.25 \text{ IN-#} / 12 = 17 \text{ FT-#}$

SPECIFY 20FT-# FOR BOLT TORQUE

- CHECK FRAME

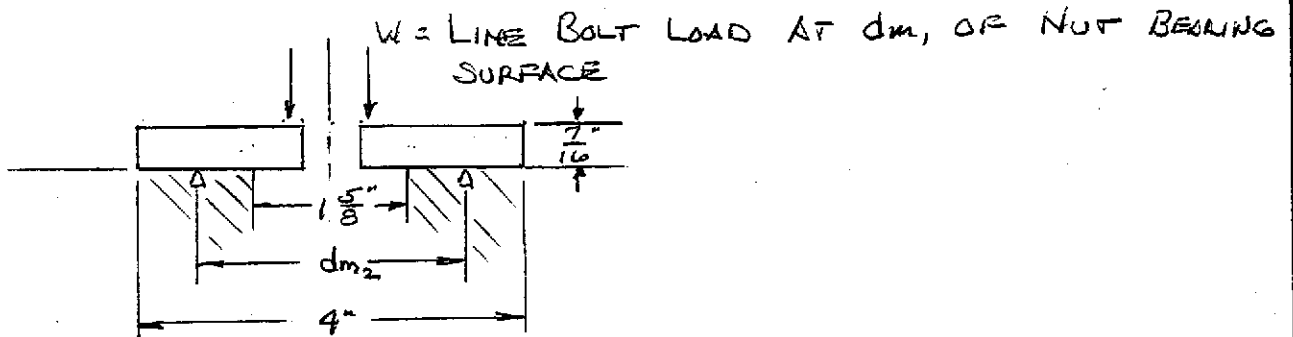
$F = \frac{20 \times 12}{.2(.625)} = 1920 \#$

$T = \frac{1920(3.875)}{.515} = 14,447 \text{ PSI}$   
 $< .6S_y = 21,600 \text{ PSI} \therefore$  OK

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



#### 4.4.2.5 SPECIAL WASHER DESIGN

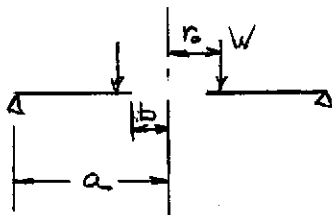


REACTION LOAD IS ASSUMED TO OCCUR AT THE MEAN DIAMETER OF CONTACT SURFACE:

$$\therefore d_{m1} = \frac{1.06 - .6875}{2} = .8738"$$

$$d_{m2} = \frac{4 + 1.625}{2} = 2.8125"$$

MODEL: REF: ROARK, CASE 1a, P. 334



$$r_0 = \frac{d_{m1}}{2} = \frac{.8738}{2} = .4369"$$

$$a = \frac{d_{m2}}{2} = \frac{2.8125}{2} = 1.406"$$

$$b = \frac{.6875}{2} = .3438"$$

$$M_{MAX} = M_{tb} = K_{Mtb} W a$$

$$b/a = .3438/1.406 = .2445 ; K_{Mtb} = .5423$$

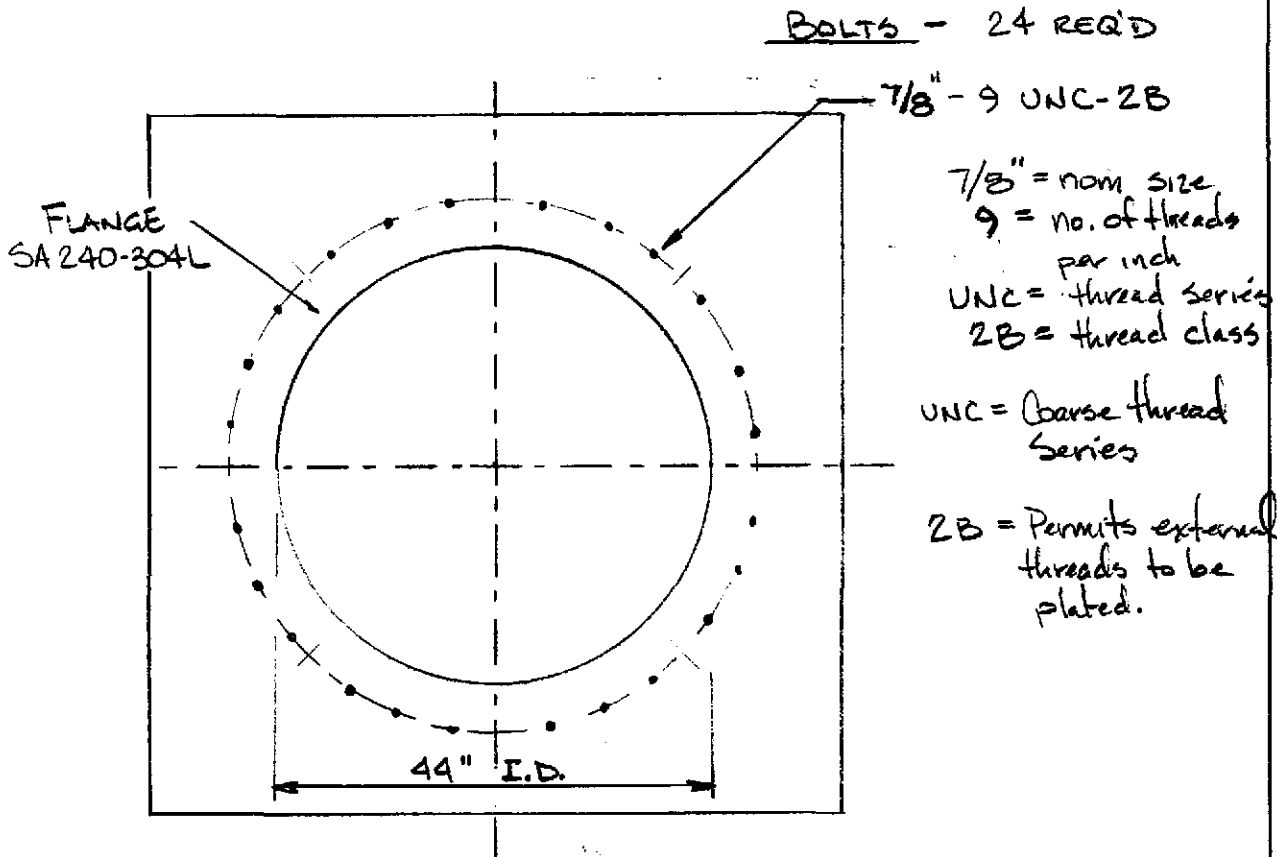
$$W = \frac{W}{\pi d_m} = \frac{1920}{\pi (.8738)} = 699 \text{ #/IN}$$

$$\therefore M_{MAX} = .5423 (699) (1.406) = 533$$

$$\sigma = \frac{6M}{t^2} = \frac{6(533)}{(.4375)^2} = 16,708 \text{ PSI} < 65 \text{ Sy} \quad \therefore \text{OK}$$

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-063 PAGE 1 OF 6
REV.	DEO #	DATE	BY:	CHECK	TITLE:  Flange Bolting Analysis of flange bolting for Gate Valves 112 CM & 122 CM	
0	0136	3/4/96	WDB	RDC		
					BY: W.Bilynsky	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<b>PURPOSE:</b> Evaluate the gate valves threaded fastening details. Bolts and their mating threaded (tapped) flange section are potential areas of failure due to thread stripping between differing materials.						
<b>METHOD:</b> Hand calculations utilizing standard formulas for Stress Areas and Length of Engagement of Screw Threads as specified in MACHINERY's HANDBOOK						
<b>ASSUMPTIONS:</b>						
<b>INPUTS:</b> 1. PSI Calc No. V049-1-042 2. GNB Drawings 103098						
<b>REFERENCES:</b> 1. Machinery's Handbook. Oberg & Jones 19th Ed. 1973. 2. Standard Handbook for Mechanical Engineers. Baumeister & Marks 7th Ed. 3. Specification for 112 and 122 CM Gate Valves PSI - V049-2-005 rev. 3 4. Doc. No. V049-1-066 LIGO Vacuum Equipment Structural Design Criteria						
<b>CALCULATIONS:</b>  ( See Attached )						
<b>CONCLUSIONS:</b> The requirements for proper and adequate bolting as specified in the Machinery's Handbook are satisfactorily met.						
<b>NOTES:</b>						

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



BOLTS - 24 REQ'D

7/8" - 9 UNC-2B

7/8" = NOM. SIZE  
 9 = no. of threads per inch  
 UNC = thread series  
 2B = thread class  
  
 UNC = Coarse thread series  
  
 2B = Permits external threads to be plated.

7/8" BOLT - Ref. Standard Handbook for Mechanical Engineers 7<sup>th</sup> ed. Section B-12

REF. TABLE 1 Pg. B-14

Major Diam,  $D_{max}$  = 0.8750 in. (SCREW BASIC DIAMETERS)  
 Pitch Diam,  $E_{max}$  = 0.8028 in.  
 $E_{min}$  = 0.7946 in.  
 Basic minor diam,  $K$  = 0.7387 in. (EXTERNAL THREADS)  
 Minor Diam,  $K_{n max}$  = 0.778 in. (INTERNAL THREADS)  
 Minor Diam,  $K_{n min}$  = 0.7547 in. (INTERNAL THREADS)  
 Minor Diam tolerances Class 2B = 0.0134 in. (INTERNAL THREADS)

Areas of section { Basic Min. Minor Diam = 0.4193 in<sup>2</sup>  
 Stress Area = 0.4612 in<sup>2</sup>

FORCE ON BOLTS

Ref. PSI Calc No. V049-1-042 Force<sub>TENS</sub> = 25.37 K on 44"  $\phi$  flange  
 Ref. SPECIFICATION FOR 112 AND 122 CM GATE VALVES  
 PSI - V049-2-005 REV. 3 = 21.0 K  
 SECTION 4.1.14

TOTAL TENSILE FORCE = 46.37 KIPS

$$\text{TENSILE FORCE PER BOLT} = F_{\text{Tens.}} = \frac{46370 \text{ lbs}}{24 \text{ BOLTS}}$$

$$F_{\text{Tens.}} = 1932.1 \text{ lbs/BOLT}$$

The critical areas of stress of mating screw threads are:

- 1) The effective cross-sectional area, or tensile stress area, of the external thread.
- 2) The shear area of the external thread, which depends principally on the minor diameter of the tapped hole.
- 3) The shear area of the internal thread, which depends principally on the major diameter of the external thread.

To prevent stripping of the external thread, the minimum length of engagement required is:

$$L_{e \text{ min.}} = \frac{2 \times A_t}{\pi K_n \text{ max} \left[ \frac{1}{2} + 0.57735 n (E_{s \text{ min.}} - K_n \text{ max.}) \right]}$$

where:  $n = \text{no. of threads per inch} = 9$

$$K_n \text{ max} = \text{max. minor diameter of internal threads} \\ = .778 \text{ in}$$

$$E_{s \text{ min.}} = \text{min. pitch diameter of external thread} \\ = .7946 \text{ in}$$

$$A_t = \text{tensile stress area} = .4612 \text{ in}^2 \\ = .7854 \left( D - \frac{0.9743}{n} \right)^2$$

$$L_{e \text{ min.}} = \frac{(2)(.4612)}{\pi (.778 \text{ in}) \left[ \frac{1}{2} + .57735(9) [.7946 - .778] \right]} \\ = .643 \text{ in.}$$

REF. MACHINERY'S HANDBOOK  
Pg. 1141

## STRIPPING OF INTERNAL THREAD.

IF THE INTERNAL THREAD (I.E. TAPPED FLANGE) IS MADE OF MATERIAL OF LOWER STRENGTH THAN THE EXTERNAL THREAD (I.E. BOLT), STRIPPING OF THE INTERNAL THREAD MAY TAKE PLACE BEFORE THE SCREW/BOLT BREAKS (DESIRED FAILURE MODE).

RELATIVE STRENGTH OF THE EXTERNAL AND INTERNAL THREADS IS;

$$J = \frac{A_s \times \text{Tensile strength of external thread mat'l}}{A_n \times \text{Tensile strength of internal thread mat'l}}$$

IF  $J \leq 1.0$  the length of engagement  $L_{\min}$  is adequate

IF  $J > 1.0$  the length of engagement to prevent stripping of the internal threads is multiplied by  $J$   
OR  $Q = J L_{\min}$

$$A_s = \pi n L_e K_n \max \left[ \frac{1}{2n} + 0.57735 (E_{s \min} - K_n \max) \right]$$

ref. table 4  
Machinery  
Handbook

$$n = \text{number of threads} = 9$$

$$L_e = .643 \text{ in}$$

$$K_n \max = .778 \text{ in} = \text{max minor dia. internal threds.}$$

$$E_{s \min} = .7946 \text{ in} = \text{min pitch dia. external threds.}$$

$$\begin{aligned} A_s &= \pi (9) (.643 \text{ in}) (.778 \text{ in}) \left[ \frac{1}{2(9)} + 0.57735 (.7946 \text{ in} - .778 \text{ in}) \right] \\ &= .9214 \text{ in}^2 \end{aligned}$$

$$A_n = \pi n L_e D_{s \min} \left[ \frac{1}{2n} + 0.57735 (D_{s \min} - E_n \max) \right]$$

$$D_{s \min} = .8592 \text{ in} = \text{min major dia. of external thred.}$$

$$E_n \max = .8110 \text{ in} = \text{max pitch dia. of internal thred.}$$

$$\begin{aligned} A_n &= \pi (9) (.643 \text{ in}) (.8592 \text{ in}) \left[ \frac{1}{2(9)} + 0.57735 (.8592 \text{ in} - .8110 \text{ in}) \right] \\ &= 1.303 \text{ in}^2 \end{aligned}$$

• tensile strength of valve flange

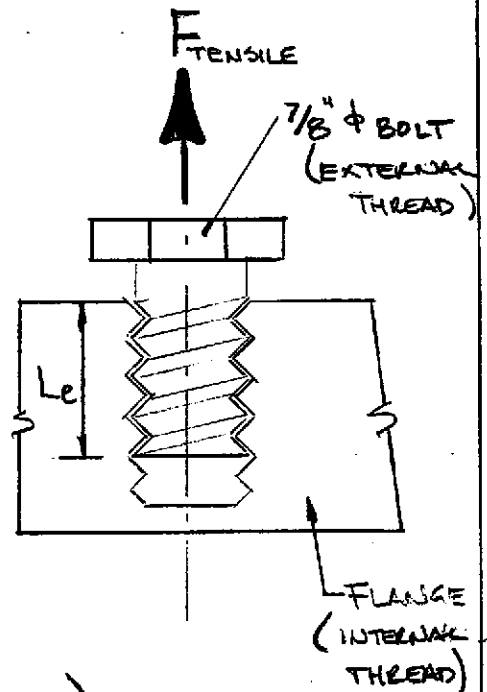
Material = SA240-304 L

$$S = 14.7 \text{ KSI}$$

• tensile strength of Bolts

material = SA-193-B7

$$S = 25.0 \text{ KSI}$$



$$J = \frac{A_s \times \text{Tensile strength (BOLT)}}{A_n \times \text{Tensile strength (Flange)}}$$

$$= \frac{.9214 \text{ in}^2 \times 25.0}{1.303 \text{ in}^2 \times 14.7}$$

$$J = 1.202 \text{ in} \quad \therefore L_e = .643 \text{ in} \text{ inadequate}$$

required engagement length

$$Q = J L_e$$

$$= (1.202 \text{ in})(.643 \text{ in})$$

$$= .773 \text{ in}$$

$$.773 \text{ in} < 1.42 \text{ in (actual depth)}$$

$\therefore$  Engagement length adequate

Stripping of internal thread is unlikely. Bolts + Flange are adequately sized.



# Average Thread Stress (SCREW)

$$\sigma_{AVER} = \frac{2 F_{TENSILE}}{\pi K L_e}$$

$$= \frac{2 (1932.1 \text{ lbs})}{\pi (0.7387 \text{ in})(0.643 \text{ in})}$$

$$\sigma_{AVER} = 2589.6 \text{ #/in}^2 / \text{BOLT}$$

Allow Stress = .6  $S_m$  ref. ASME SECTION VIII DIV. II  
AD-132.2

$$\sigma_{ALL} = .6 (14700 \text{ psi}) \quad (\text{FOR: SA 240-304 L})$$

$$\sigma_{ALLOW} = 8820 \text{ #/in}^2$$

$$\sigma_{ALL} > \sigma_{AVER} \quad F.S. = 3.4$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-068 PAGE 1 OF 5
REV.	DEO #	DATE	BY:	CHECK	TITLE:	
0	0141	4/19/96	RDC	WDB	Study of Required Bellows Deflections for Installation Fitup	
					BY: R. D. Ciatto	DEPT.: 744
PROJECT: LIGO Vacuum Equipment					PROJECT NO: V59049	
<p><b>PURPOSE:</b> Determine the maximum deformations required of the bellows to facilitate installation of equipment considering component construction tolerances.</p>						
<p><b>METHOD:</b> Hand calculation methods are used to determine the geometric configurations that bellows must assume to connect adjacent components.</p>						
<p><b>ASSUMPTIONS:</b> See calculations attached.</p>						
<p><b>INPUTS:</b> LIGO project drawings and sketches.</p>						
<p><b>REFERENCES:</b> Specification V049-2-017, Bellows Expansion Joints for LIGO Vacuum Equipment</p>						
<p><b>CALCULATIONS:</b> (SEE ATTACHED)</p>						
<p><b>CONCLUSIONS:</b> The required bellows axial and bending deflections have been determined.  Axial deflection.....+/- 2 in.  Bending rotation.....+/- .5°.</p>						
<p><b>NOTES:</b> The above deformations will be included in Specification V049-2-017. Shear deformation of bellows is not required.</p>						

1

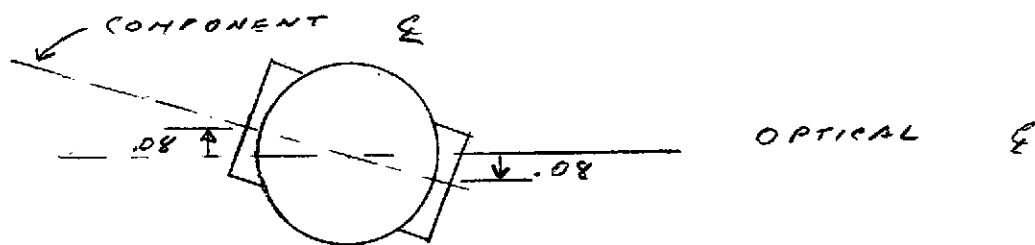
MAXIMUM DEVIATIONS REQUIRED AT  
ENDS OF BELLOWS

GIVEN:

1. EQUIPMENT TOLERANCES ARE AS SHOWN ON DWGS
2. EQUIPMENT  $\phi$  WILL BE INSTALLED TO WITHIN  $\pm 2\text{mm}$  ( $\pm .08\text{ IN}$ ) OF THE OPTICAL  $\phi$

ASSUME:

1. EACH MAJOR COMPONENT (BSC, ILM, LOR PUMA, ETC) MAY BE INSTALLED AT AN ANGLE TO THE OPTICAL  $\phi$  THAT IS LIMITED BY NO. 2 ABOVE

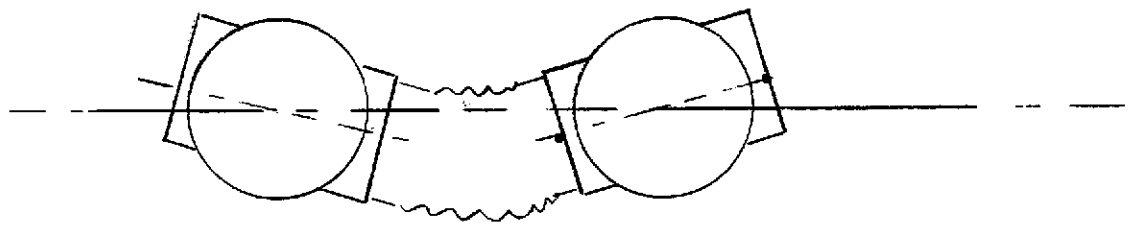


2. THE MISALIGNMENT SHOWN ABOVE CAN OCCUR IN THE HORIZONTAL PLANE AND THE VERTICAL PLANE SIMULTANEOUSLY

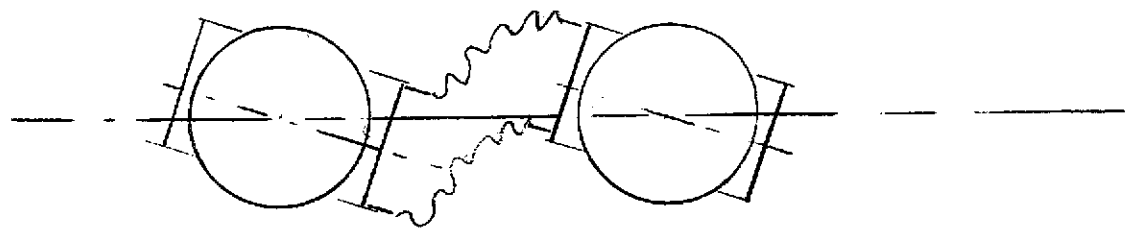
3. ASSUME THAT FLANGE PARALLELISM AND PERPENDICULARITY REQUIREMENTS FOR BSC (DWC V049-4-001) HOLD FOR ALL COMPONENTS.

4. MISALIGNMENT OF 2 ADJACENT COMPONENTS CAN OCCUR SUCH THAT AN ADAPTER WILL BE BENT IN EITHER SINGLE OR DOUBLE CURVATURE.

SINGLE CURVATURE



DOUBLE CURVATURE



CLEARLY, DOUBLE CURVATURE IMPOSES GREATER STRAIN ON THE ADAPTER BELLOW THAN SINGLE CURVATURE.

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

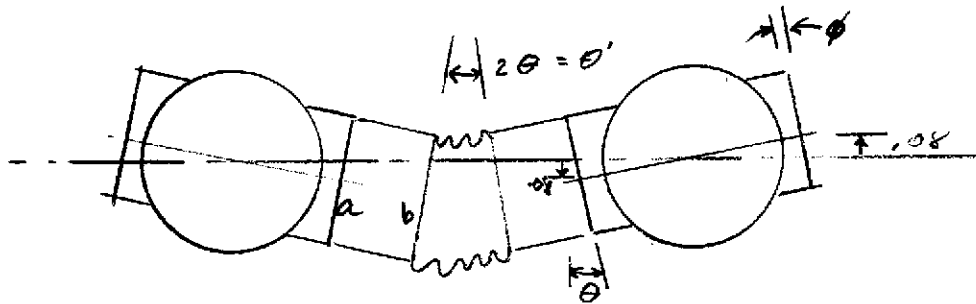


22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-143 200 SHEETS



HOWEVER, IT SHOULD BE POSSIBLE TO CONTROL INSTALLATION ALIGNMENT SO THAT ADAPTERS BETWEEN ADJACENT COMPONENTS ARE BENT IN SINGLE CURVATURES. EACH COMPONENT CAN BE SET IN ITS FINAL POSITION AFTER THE NEXT COMPONENT AND BELLOWS/RODATER ARE INSTALLED FOR ROUGH ALIGNMENT, I.E. CONCRETE ANCHORS ARE NOT INSTALLED.

THE MAXIMUM ROTATION AT THE BELLOWS IS A FUNCTION OF THE REGULAR MISALIGNMENT OF ADJACENT COMPONENTS AT INSTALLATION AND THE MISALIGNMENT OF FLANGES THAT ARE OUT OF PARALLEL AND NOT PERPENDICULAR TO THE OPTICAL  $\hat{z}$ . ROTATION FOR SINGLE CURVATURE IS INDEPENDENT OF ADAPTER LENGTH



ASSUME THAT ENDS OF ADAPTER SPOOLS,  $a$  &  $b$  ARE PARALLEL

$\theta$  IS LIKELY TO BE MAXIMUM FOR THE CORNER STATION DISCS. THE DISTANCE FROM THE BSC  $\hat{z}$  TO THE FACE OF THE COIN FLANGE IS  $113.75 / 2 = 56.9$  IN (DWG V049-4-001).

$$\theta = \frac{.08}{56.9} + \phi$$

$$= 1.407(10)^{-3} \text{ RAD} + \phi$$

$\phi$  IS THE ANGULAR MISALIGNMENT RESULTING FROM TOLERANCES ON PARALLELISM AND PERPENDICULARITY. THIS ANGLE IS MAXIMUM WHEN THE FLANGE FACE IS OUT OF PERPENDICULARITY.

$$\phi = \frac{.03}{r} \quad \text{WHERE } .03 \text{ IS TOLERANCE ON PERPENDICULARITY SEE DWG 1049-4-001}$$

$$r = \frac{\text{FLANGE MAX RADIUS}}{2} = \frac{69.25}{2} = 34.125$$

$$\phi = \frac{.03}{34.125} = .879 (10)^{-3} \text{ RAD}$$

$$\theta = (1.407 + .879)(10)^{-3} = 2.286 (10)^{-3} \text{ RAD}$$

THE MAX CHANGE IN ROTATION BETWEEN THE ENDS OF A BELLOW IS  $\theta' = 2\theta$

$$\theta' = 2(2.286)(10)^{-3} = .0046 \text{ RAD}$$

SINCE ROTATION CAN OCCUR IN BOTH THE VERTICAL & HORIZONTAL PLANES

$$\theta_{MAX} = [2(\theta')^2]^{\frac{1}{2}} = .0065 = 0.37^\circ \text{ SAY } 0.50^\circ$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-143 200 SHEETS



### LONGITUDINAL COMPRESSION OR EXTENSION

ASSUME THAT COMPONENT INSTALLATION CAN BE WITHIN  $\pm .25$  IN IN AXIAL DIRECTION OF OPTICAL BEAM. HENCE, FOR 2 ADJACENT COMPONENTS, THE MAX BELLOWS FLONGATION OR COMPRESSION DURING INSTALLATION IS

$$\delta = \pm .50 \text{ IN}$$

IT IS REASONABLE TO ASSUME THAT THE  $\pm 2"$  OF MOTION REQUIRED BY THE SPEC (4412, VOYS-2-017) IS ENOUGH TO ALLOW FOR  $\delta$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

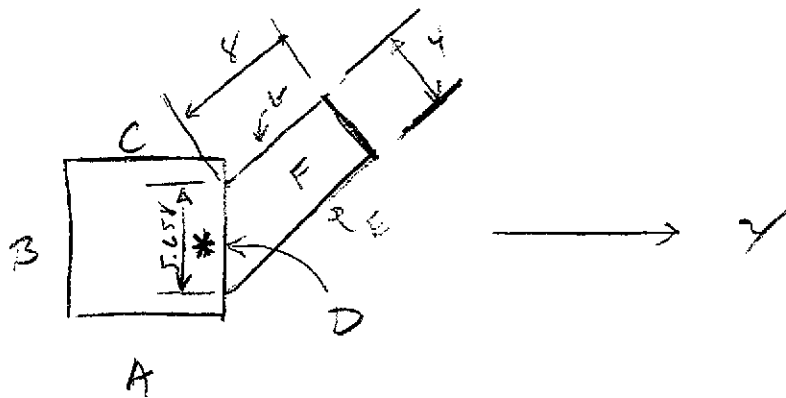
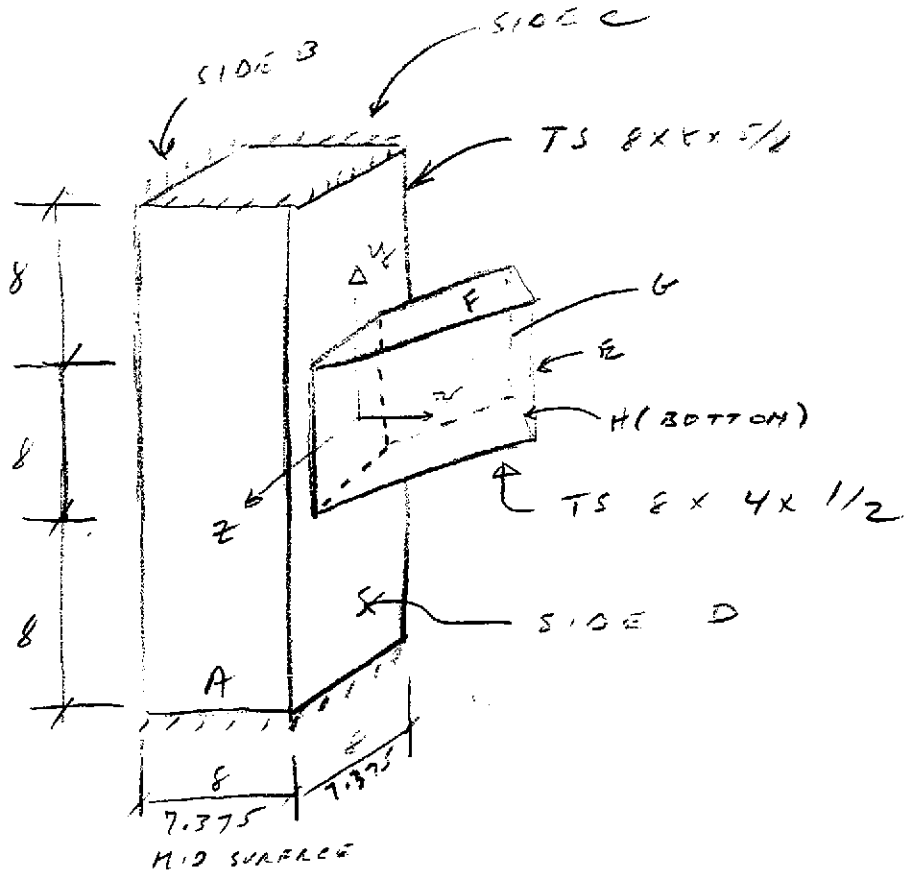


PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-079 PAGE 1 OF 7
REV.	DEO #	DATE	BY:	CHECK	TITLE:	
0	0.131	4/19/96	RSC	WDB	Analysis of BSC Support Leg to Cross Beam Connection	
					BY: R. D. Ciatto	DEPT.: 744
PROJECT: LIGO Vacuum Equipment					PROJECT NO: V59049	
<p><u>PURPOSE:</u> Analyze welded tube steel connection at junction of support leg and cross member to confirm structural integrity of the side of the support leg which is required to resist a high bending moment at the end of the cross member.</p>						
<p><u>METHOD:</u> A local finite element model of the connection was created to analyze the support leg stresses. The IMAGES program was used.</p>						
<p><u>ASSUMPTIONS:</u> See calculations attached.</p>						
<p><u>INPUTS:</u> Forces and moments at end of cross member from Doc. No. V049-1-024</p>						
<p><u>REFERENCES:</u> 1. LIGO project drawings V049-4-001 and V049-4-023  2. Calculation V049-1-024, Design of Support Legs and Base Plates  3. IMAGES-3D, Version 3.0, R. L. Cloud and Associates  4. V049-1-066, LIGO VACUUM EQUIP. STRUCT. DESIGN CRITERIA</p>						
<p><u>CALCULATIONS:</u> (SEE ATTACHED)</p>						
<p><u>CONCLUSIONS:</u> The cross member was changed from a 7x4 tube steel member to an 8x4 in tube steel member to reduce the bending stress applied to the support leg. Stresses in the 8x8 tube steel leg member are within AISC code limits.</p>						
<p><u>NOTES:</u> Load case 1 includes the 3 forces, load case 2 includes the 3 moments and load case 3 is the combined forces and moments. The IMAGES file is SUPPCONN.*</p>						



# RE MODEL

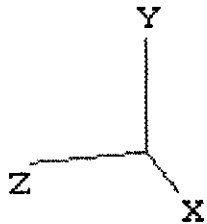
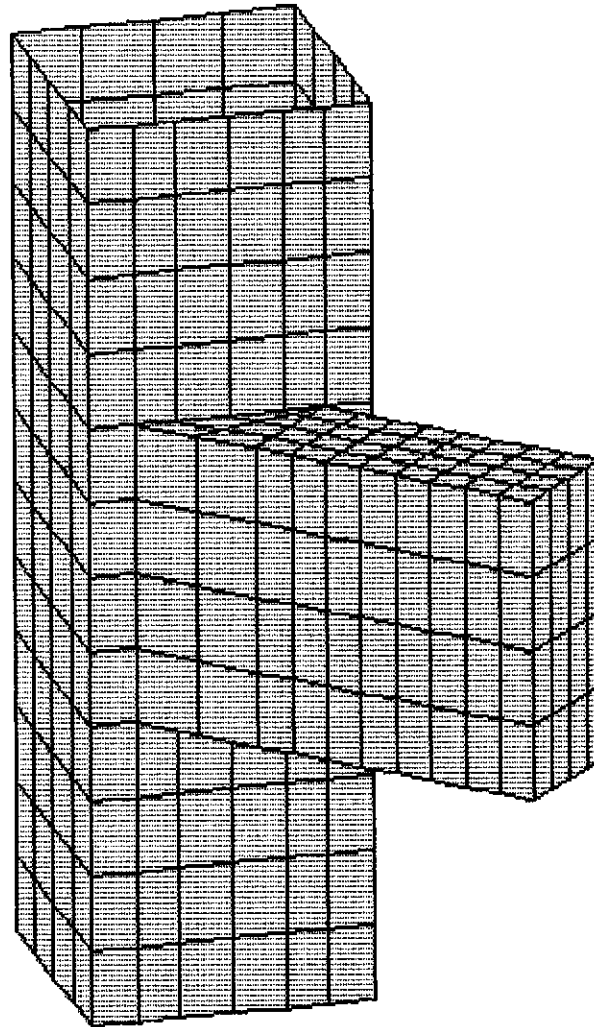
22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-143 200 SHEETS



\* MID SURFACE LENGTH  
 $\frac{4-15}{.707} = 11.950$

REV 0  
 Doc No V049-1-079  
 P. 2 007

IMAGES-3D  
Ver. 3.0  
Geometry Plot



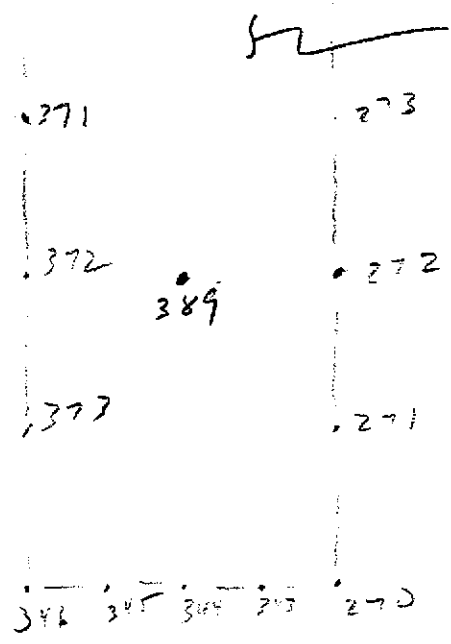
BSC Support Connection  
Hidden Line Removal

4/ 1/96  
12:42:54

Rev 0  
Doc. No. V048-1-073  
P. 3 of 7

TWO VIEW OF CROSS MEMBER MODEL

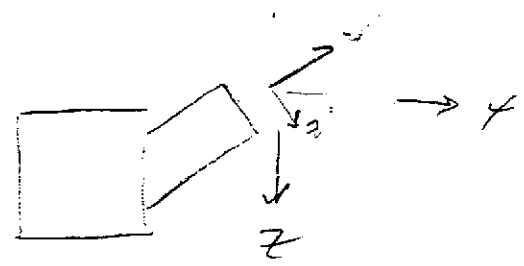
310 308 307 274



STIFF PLATE  
ELEMENTS AT END  
OF MODEL TRANSFER  
FORCES & MOMENT  
FROM NODE 389 TO  
PERIMETER NODES.  
SEE PLOT ON  
P. 3

FORCES AT NODE 389


FROM CALL V049-1-024, THE MAX  
CROSS MEMBER STRESSES ARE IN ELEMENT  
B-9. THE GLOBAL LOADS FROM THE  
FRAME MODEL ARE AT 45° TO THE  
GLOBAL AXIS OF THE FE PLATE MODEL.  
NODE 5 HAS THE LARGER LOADS. LET  
THE FRAME MODEL GLOBAL AXES BE  
THE PRIME AXES, X', Y', Z'.

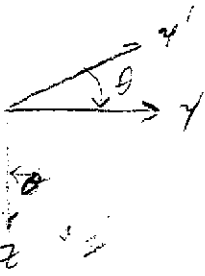


- $F_{X'} = 2235 \text{ LB}$
- $F_{Y'} = 9287$
- $F_{Z'} = 15 \text{ SAY } = 0$
- $M_{X'} = 4593 \text{ IN LB}$
- $M_{Y'} = 713$
- $M_{Z'} = 404300$

REV 0  
Doc. No V049-1-079  
P. 4 OF 7

22-141 50 SHEETS  
22-142 100 SHEETS  
22-143 200 SHEETS





$$F_y = F_x' \sin \theta + F_z' \cos \theta$$

$$F_x = -F_x' \cos \theta + F_z' \sin \theta$$

$$F_y = -10$$

$$F_y = 8235(.707) + 0$$

$$= 5822$$

$$F_x = 9287$$

$$F_x = -8235(.707) + 0$$

$$= -5822$$

$$M_y = 4993(.707) + 404300(.707)$$

$$= 289270$$

$$M_z = M_z' = 713$$

$$M_x = -4993(.707) + 404300(.707)$$

$$= 282310$$

THESE FORCES ARE APPLIED TO NODE 389 WHICH IS AT THE CENTER OF A STIFF ( $E = 90 \times 10^6$  PSI), THICK (3 IN) PLATE AT THE END OF THE 8 X 4 STUD IN THE MODEL.

REV D  
 Doc. No. V048-1-079  
 P. 5 OF 7

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



STRESS IN SIDE D OF 8x8 5/8 TS  
COLUMN.

THE LOCAL STRESS INTENSITY IS SHOWN  
IN THE STRESS CONTOUR PLOT ON THE  
FOLLOWING SHEET. THE MAX SE IS  
LOCATED AT THE CORNER OF THE  
JUNCTION WITH THE 8x4x1/2 TS CROSS  
MEMBER,

$$SE = 34,200 \text{ PSI}$$

$$< .75 F_y^*$$

$$= .75(46)$$

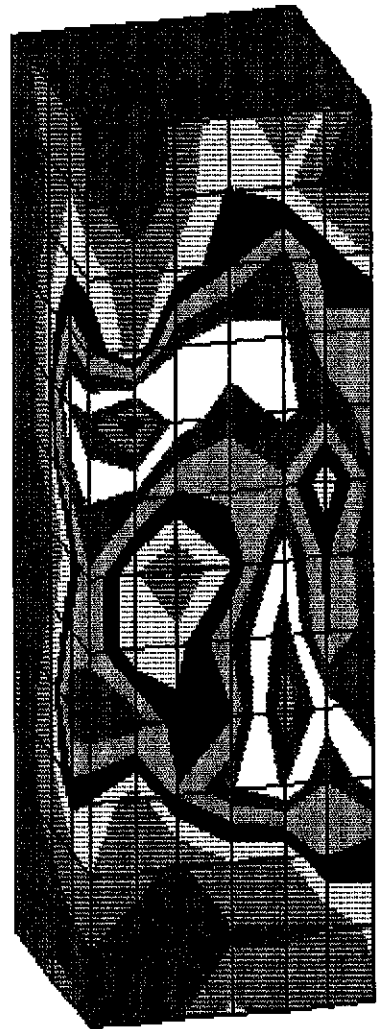
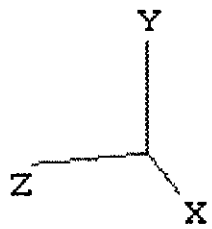
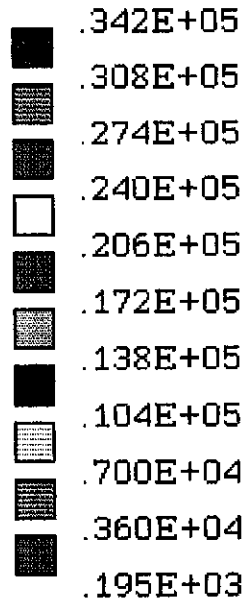
$$= 34.5 \text{ KSI}$$

$$* F_y = 46 \text{ KSI FOR A500 GR B}$$

THE SE IS MUCH LESS (10 TO 24 KSI)  
FOR OTHER LOCATIONS AT THE  
UNBOLTED CONNECTION WHICH WILL  
BE A FULL PEN. WELD.

REV D  
Doc. No. V249-1-079  
P. 6 OF 7

**IMAGES-3D**  
**Version 3.0**



Load Case  
3

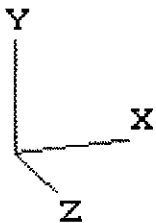
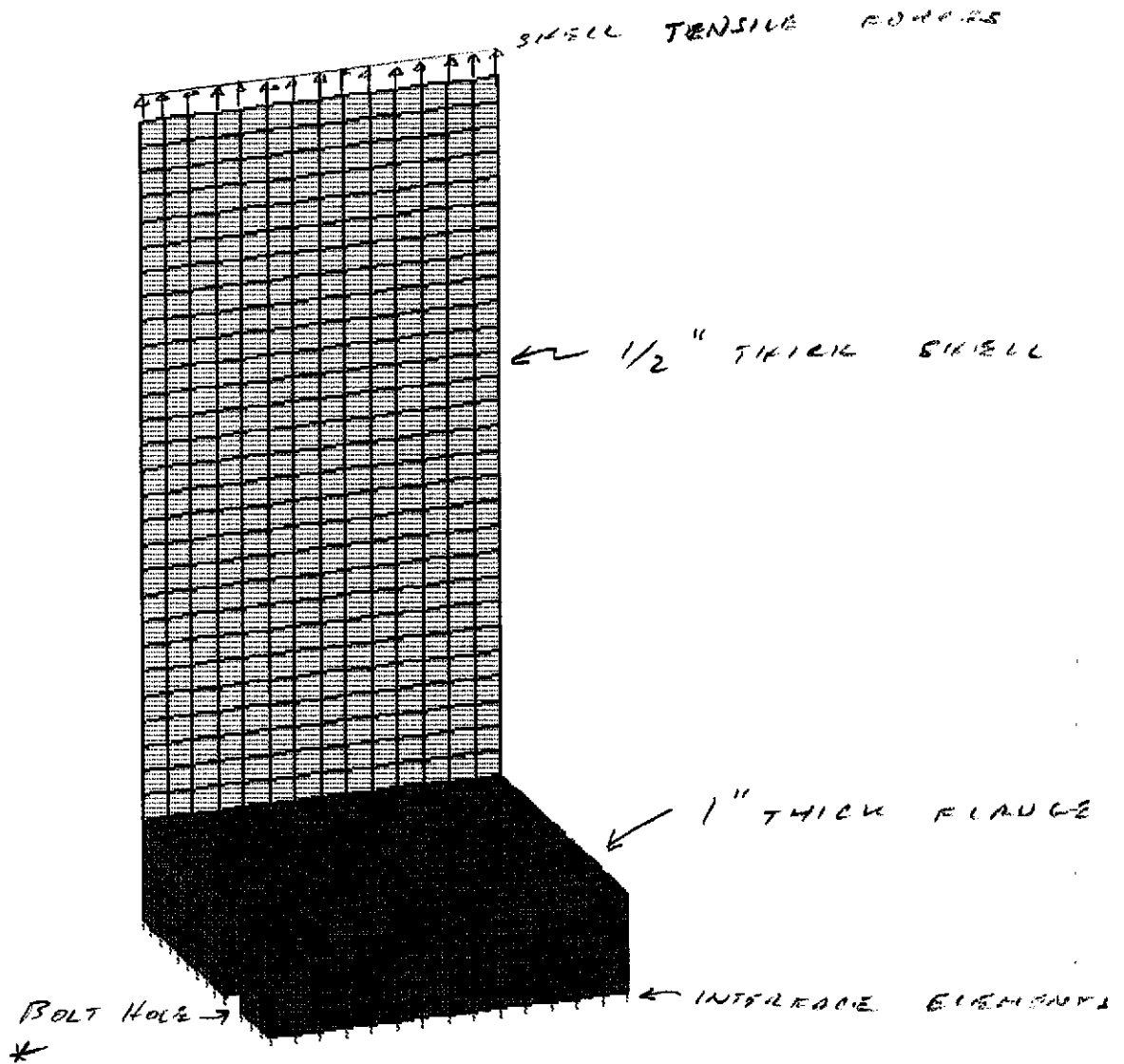
Stress Contour Plot  
Surf: Top  
Stress Intensity

4/ 1/96  
12:48:49

*REV 0*  
*Doc. No. 1019-1-079*  
*P. 7 of 7*

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-080 PAGE 1 OF 10
REV.	DEO #	DATE	BY:	CHECK	TITLE: Analysis of Bolted Flange for Initial Out of Flatness	
0	0141	4/27/96	RBC	AGR		
					BY: R. D. Ciatto	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<b>PURPOSE:</b> To determine if Viton O-rings in the bolted flanges will seal if flange flatness is at maximum tolerance considering the stiffening effects of the attached shell.						
<b>METHOD:</b> A 3D IMAGES finite element model of a segment of the bolted flange was created. The flange out of flatness was analyzed using gap elements, with the gap equal to the flatness tolerance at the flange mating surface. A nonlinear analysis of this model was performed. Loads included the bolt preload, which is 10 kips, and the maximum tensile load in the shell.						
<b>ASSUMPTIONS:</b> The maximum gap occurs at the bolt centerline. The amplitude of the gap is the same as the flatness tolerance for the 60 in flange.						
<b>INPUTS:</b> Drawing V049-4-019 for the flatness tolerance Calculation V049-1-016 for the initial 3D finite element model Calculations V049-1-018 and -042 for Viton properties and shell forces, respectively.						
<b>REFERENCES:</b> See Inputs						
<b>CALCULATIONS:</b> (SEE ATTACHED)						
<b>CONCLUSIONS:</b> Even though the bolt clamping force must resist the shell stiffness, the bolt will bring the flanges together and the seal will be maintained. When the maximum gap occurs between bolts, the clamping force cannot close the gap but the seal is maintained even with the maximum tolerance.						
<b>NOTES:</b> The computer file is FLANGED.*						

IMAGES-3D  
Ver. 3.0  
Geometry Plot



Bolted Flange - 48.25 in, 24 bolts  
Hidden Line Removal

4/3/96  
15:6:5

\* BOLT FORCE NOT SHOWN

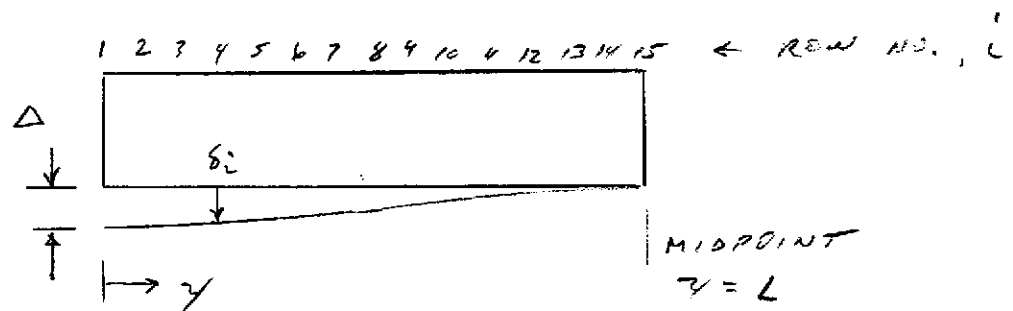
REV 0  
Doc. No. V049-1-060  
P. 2 OF 10



THERE ARE 15 ROWS OF NONLINEAR FOUNDATION ELEMENTS. THE NON LINEAR SPRING CONSTANTS CAN BE VARIED FROM ROW TO ROW TO SIMULATE A GAP THAT CAN RESULT FROM THE FLATNESS TOLERANCE

IT IS ASSUMED THAT FLANGE FACES ARE IN CONTACT AT THE MIDPOINT BETWEEN BOLTS AND THAT THE GAP IS MAXIMUM AT THE BOLTS. THEN BOLTUP CAN BE USED TO CLOSE THE GAP.

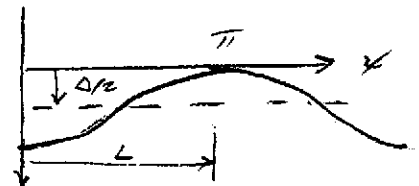
1/2 BOLT



$$\Delta = .010 \text{ IN (FLATNESS TOLERANCE - DWG V049-4-019)}$$

ASSUME THAT GAP VARIES AS A SINE FUNCTION

$$\delta = \frac{\Delta}{2} + \frac{\Delta}{2} \cos \frac{y}{L} \pi$$



$$\delta_i = \frac{\Delta}{2} + \frac{\Delta}{2} \cos \left( \frac{(i-1)L}{14} \pi \right)$$

$$= \frac{\Delta}{2} \left( 1 + \cos \left( \frac{(i-1)}{14} \pi \right) \right)$$

$$= .005 \left( 1 + \cos \left( \frac{(i-1)}{14} \pi \right) \right)$$

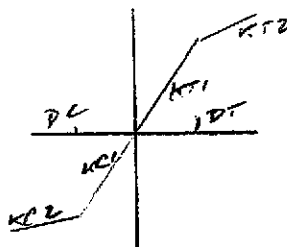
REV D  
Doc. No. V049-1-009  
P. 3 OF 10

22-141 50 STREETS  
22-142 100 STREETS  
22-143 200 STREETS



Row	i	Theta (i-1)*Pi/15	A cos Theta	B A+1	delta .005*B
1	0	0	1	2	0.0100
2	1	0.2094393	0.978148	1.978148	0.0099
3	2	0.4188787	0.913546	1.913546	0.0096
4	3	0.628318	0.809017	1.809017	0.0090
5	4	0.8377573	0.669131	1.669131	0.0083
6	5	1.0471967	0.500001	1.500001	0.0075
7	6	1.256636	0.309018	1.309018	0.0065
8	7	1.4660753	0.10453	1.10453	0.0055
9	8	1.6755147	-0.10453	0.895473	0.0045
10	9	1.884954	-0.30902	0.690985	0.0035
11	10	2.0943933	-0.5	0.500002	0.0025
12	11	2.3038327	-0.66913	0.330871	0.0017
13	12	2.513272	-0.80902	0.190984	0.0010
14	13	2.7227113	-0.91354	0.086455	0.0004
15	14	2.9321507	-0.97815	0.021853	0.0001

IMAGES NON LINEAR SPRING CONSTANTS



$KT1 = 0$   
 $KC1 = 0$  (EXCEPT ROW 15,  $KC1 = 1 \times 10^8$ )  
 $KT2 = 0$   
 $KC2 = 1 \times 10^8$   
 $DT = 1$   
 $DC = \delta$  FROM ABOVE FOR EACH ROW OR NON LIN SPRINGS

FOR ROWS 1 TO 14 SPRING CONSTANT NUMBERS ARE 2 TO 15, RESPECTIVELY FOR ROW 15, THE SPRING CONSTANT NUMBER IS 1, FOR THAT ROW

$KT1 = 0$   
 $KC1 = 1 \times 10^8$   
 $KT2 = 0$   
 $KC2 = 1 \times 10^8$   
 $DT = 1$   
 $DC = 1$

REV 0  
 Doc. No. V047-1-080  
 P. 4 OF 10

ADDED MASS / ELEMENT TO REPRESENT SHELL

USE MAX SHELL THICKNESS

$$t = .5 \text{ IN}$$

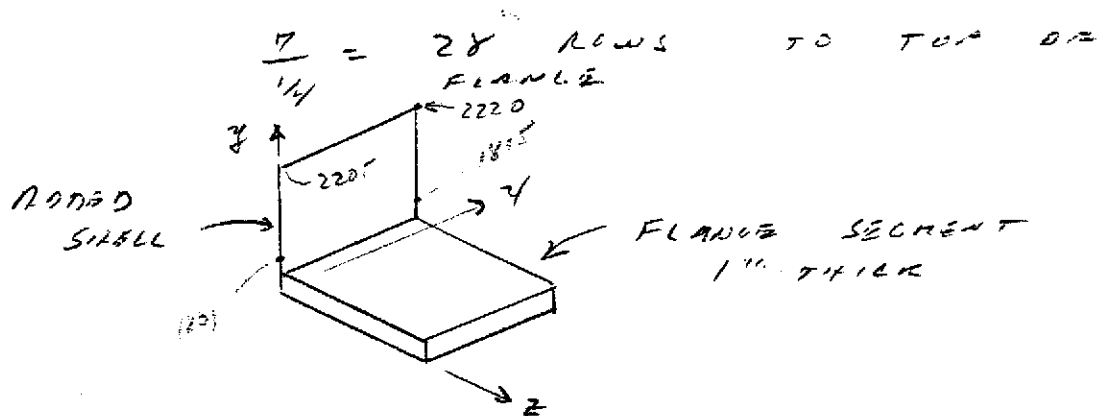
SHELL WILL BE IN X-Y PLANE ( $z=0$ )  
ADD ENOUGH PLATE ELEMENTS TO GIVE A  
LONG SHELL LENGTH. FOR THE 30 IN DIA  
FLANGE,

$$L = 2.5 \sqrt{RE}$$

$$= 2.5 (15(.5))^{.5}$$

$$= 6.8 \text{ IN SAY } 7 \text{ IN}$$

FOR 1/4 IN WIDE ELEMENTS ADD



SEE CALC DIR, P. 5 FOR SPRING STIFFNESS  
OF VITON O-RING

$$R_s = 709 \text{ LB/IN}$$

REV 0  
Doc. No V049-1-080  
P. 5 OF 10

INNER VITON O-RING IS REPRESENTED BY THE LINEAR SPRINGS

FIRST: NODE 1576 TO NODE 1, INCR = 15

DOF = 1  
SPRING CONSTANT = 1



LAST: NODE 1786 TO NODE 211

OUTER O-RING IS REPRESENTED BY SIMILAR ELEMENTS  
SEE CALC 016, P. 18

MAXIMUM AXIAL FORCE IN SHELL (F<sub>y</sub>)  
OCCURS IN 30" TUBE (SEE CALC 042)

F<sub>y</sub> = 93.1 @ NODES 2207 TO 2219  
(INCR = 1)

F<sub>y</sub> = 46.6 @ NODES 2206 & 2220

REF PD 18 & 19 CALC V049-1-042

BOLT FORCE

EACH BOLT IS PRELOADED TO 10K, FOR THE HALF MODEL, THE NODAL FORCES FOR PRELOAD ARE GIVEN IN CALC 042, P. 20

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS





TIRE DISPLACEMENT CONTOUR PLOT ON THE FOLLOWING SHEET SHOWS THAT THE BOLT CLAMPING FORCE IS BRINGING THE TWO FLANGES TOGETHER WHEN THEY HAVE A HILK SPOT THAT IS MIDWAY BETWEEN TWO BOLTS.

HOWEVER, THE MAXIMUM TENSILE FORCE IN THE SKEW TENDS TO OPEN THE GAP SLIGHTLY. THE MAXIMUM GAP OPENING IS AT THE INNER O-RING,

$$\Delta_y = .00136 \text{ REF: P. 8}$$

THIS IS AT THE MID-POINT BETWEEN FLANGES AND THE OUT OF FLATNESS DOES NOT ADD TO THE GAP. FOR 2 FLANGES

$$\Delta_y = 2(.00136) = .00272 \text{ IN}$$

$\ll .058 \text{ IN}$  WHICH IS THE MIN O-RING COMPRESSION

AT THE BOLT  $e$ , THE MAXIMUM OPENING IS .000953 WHICH ADDS TO THE INITIAL GAP CAUSED BY OUT OF FLATNESS.

$$\Delta_y = .000953 + .010 = .0110 \text{ IN}$$

REF: P. 8

FOR 2 FLANGES

$$\Delta_y = 2(.0110) = .022$$

$\ll .058 \text{ MIN O-RING COMPRESSION}$

OK

$$\text{RATIO} = \frac{.058}{.022} = 2.6$$

REV 0  
 DOC. N. 1049-1-083  
 P. 7 OF 10

IMAGES-3D  
Version 3.0

DISPLACEMENT CONTOUR AT  
INNER O-RING



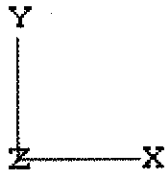
Q Bolt

M.I.D PLANE



$\Delta_y = .000953 \text{ IN}$

$\Delta_y = .00136 \text{ IN}$



REV D  
Doc No. 1049-1-060  
A. S. 10

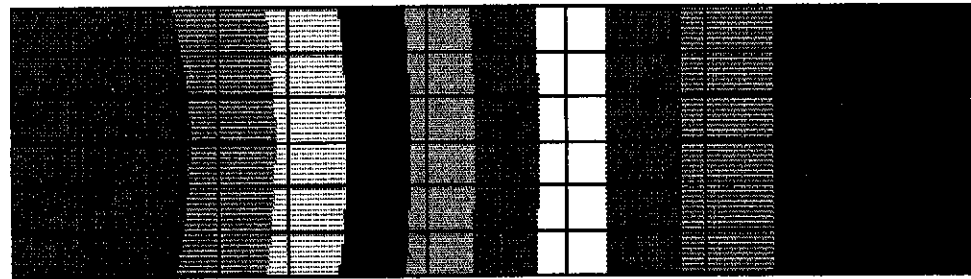
Load Case  
1

Displacement Contour Plot  
DY

4/ 3/96  
14:22:37

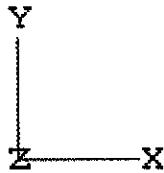
IMAGES-3D  
Version 3.0

DISPLACEMENT CONTOURS AT  
OUTER O-RING



$\Delta y = -.00157$  IN

$\Delta y = .153(10)^{-4}$  IN



REV 0  
DOC. NO. V019-1-050  
1.9 02 10

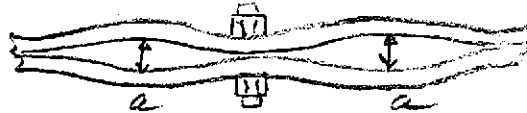
Load Case  
1

Displacement Contour Plot  
DY

4/ 3/96  
14:25:53

QUESTION:

WHAT HAPPENS WHEN THE MAXIMUM  
OUT OF FLATNESS OCCURS AT THE  
MIDPOINT BETWEEN TWO FLANGES?  
BOLT TIGHTENING WILL NOT CLOSE  
THE GAP.



THE OPENING INCREASES DUE TO  
TENSILE FORCE IN THE SHELL. THE  
MAX DEFLECTION AT THE INNER  
O-RING IS

$$\Delta = .00372 \quad \text{CALL V049-1-042} \\ \text{P. 25}$$

TOTAL DEFLECTION FOR 2 FLANGES

$$a = 2(.010 + .00372) \\ = .0274 \\ < .058$$

RATIO  $\frac{.058}{.0274} = 2.1$

REV 0  
Doc. No. V049-1-050  
P. 10 OF 10



PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-084 PAGE 1 OF 37
REV.	DEO #	DATE	BY:	CHECK	TITLE: Expansion Joint Tie Rod "Lug" Design	
0	0024	4/12/96	AGR	RDC		
1	0293	6/7/96	WDB	RDC		
2		11/26/96	WDB	RDC		
					BY: W. Bilynsky	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<b>PURPOSE:</b> The purpose of this calculation is to provide a single lug design for all expansion joint/tube sizes up to and including 72 ¼ in. I.D.						
<b>METHOD:</b> COMPRESS 5.53R computer pressure vessel software						
<b>ASSUMPTIONS</b> See Calculation						
<b>INPUTS:</b> "Design Loads" from Doc. No. V049-1-048 "Structural Design Criteria" Doc. No. V049-1-066 Doc. No. V049-1-032 Component Interface Loads						
<b>REFERENCES:</b> 1. Doc. No. V049-1-048 2. COMPRESS - Computer Aided Vessel Design program - version 5.53 3. Doc. No. V049-1-066, LIGO Vacuum Equipment Structural Design Criteria						
<b>CALCULATIONS:</b> (SEE ATTACHED)						
<b>CONCLUSIONS:</b> A single lug design as shown in design sketch utilizing 4 lugs per expansion joint is adequate for 60.5 in to and 72 ¼ in I.D. and 3 lugs per expansion joint for smaller diameters.						
<b>NOTES:</b> This lug design requires a reinforcing pad/washer as shown in the design sketch						

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE 2 OF 37
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug" Design		

**TABLE OF CONTENTS**

Revision History	3
1.0 Design Sketch	4
2.0 Compress Input	6
3.0 Lug To Shell Stress Summary	8
4.0 Compress 5.53R Output	
Spool BE-5	9
Spool BE-3	13
Spool A-13	18
Spool A-2	23
Spool A-1	28
Spool B-2	33
Appendix 'A'	A-1 to A-30
Revised Stress Summary	
Appendix 'B'	B-1 to B-3
Lug Detail For Test Condition	
Appendix 'C'	C-1 to C-3
Reinforcing Washer As An Option To A Welded Pad	

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE 3 OF 37
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug" Design		

### REVISION HISTORY

Rev. 0            Original Issue  
                         April 12, 1996

Rev. 1            Issue Date  
                         June 7, 1996

- Added Appendices 'A', 'B', and 'C'.

Rev. 2            Issue Date  
                         November 26, 1996

- Corrected Max Bolt Forces for the rod compression. (Appendix 'B')
- Added analysis of BE-1 for 1/4" thick shell with repad at each lug.

1.0-

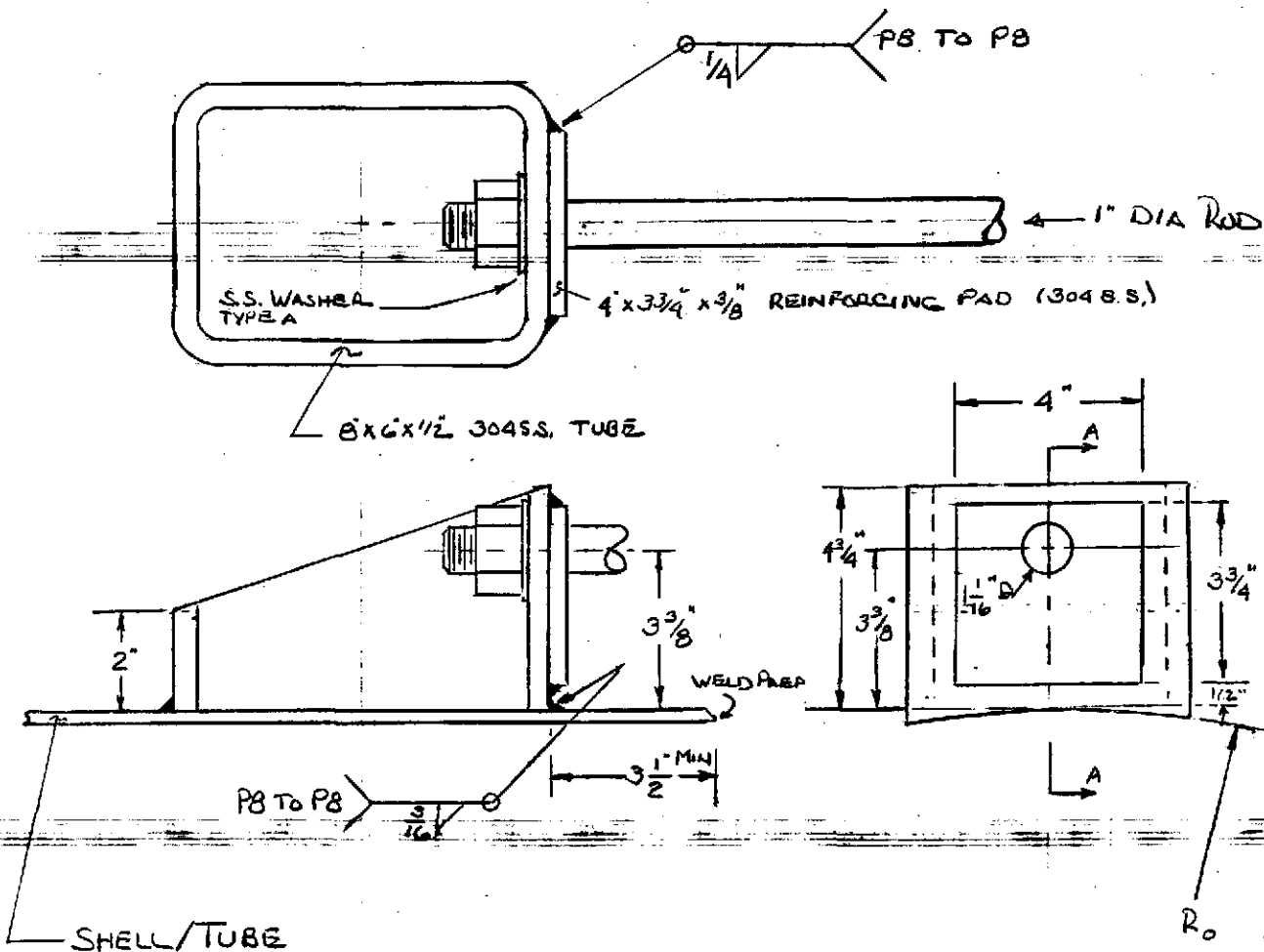
DESIGN SKETCH

SHEET 1 OF 2

SK-V049-1-084 REV0

- LUG TO SHELL ATTACHMENT FOR EXPANSION JOINT TIE ROD CONNECTIONS UP TO AND INCLUDING 72 1/4" ID TUBE SIZE FOR SPOOL BE-3 SEE SHEET 2 FOR MODIFIED DESIGN

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



WHERE:  
 $R_o$  = OUTSIDE RADIUS  
 OF TUBE  
 TYPICAL FRONT +  
 REAR

NOTE:  
 THIS DESIGN IS BASED ON  
 USING FOUR (4) LUGS SPACED  
 AT 90°

LOG WELD STRESS FOR 72" Ø TUBE  
 $F = 16,075 \text{ lb}$

$$A_w = [2(6) + 2(4)] \left(\frac{3}{16}\right) (1.707) = 3.71 \text{ in}^2$$

$$f_v = \frac{F}{A_w} = \frac{16,075}{3.71} = 4.3 \text{ ksi OK}$$

SHEAR STRESS DUE TO BENDING

$$M = \frac{4507 \text{ LB-FT} \times 12 \text{ IN}}{\text{FT}} = 54,084 \text{ IN-LB}$$
$$= 54 \text{ IN-K}$$

$$I = \left[ 2 \left( \frac{16}{12} \right)^3 + 2(6)(4)^2 \right] \left( \frac{3}{16} \right) (1.707)$$
$$= [682 + 192] \left( \frac{3}{16} \right) (1.707)$$
$$= 116$$

$$s_v = \frac{54(4)}{116} = 1.86 \text{ ksi}$$

TOTAL

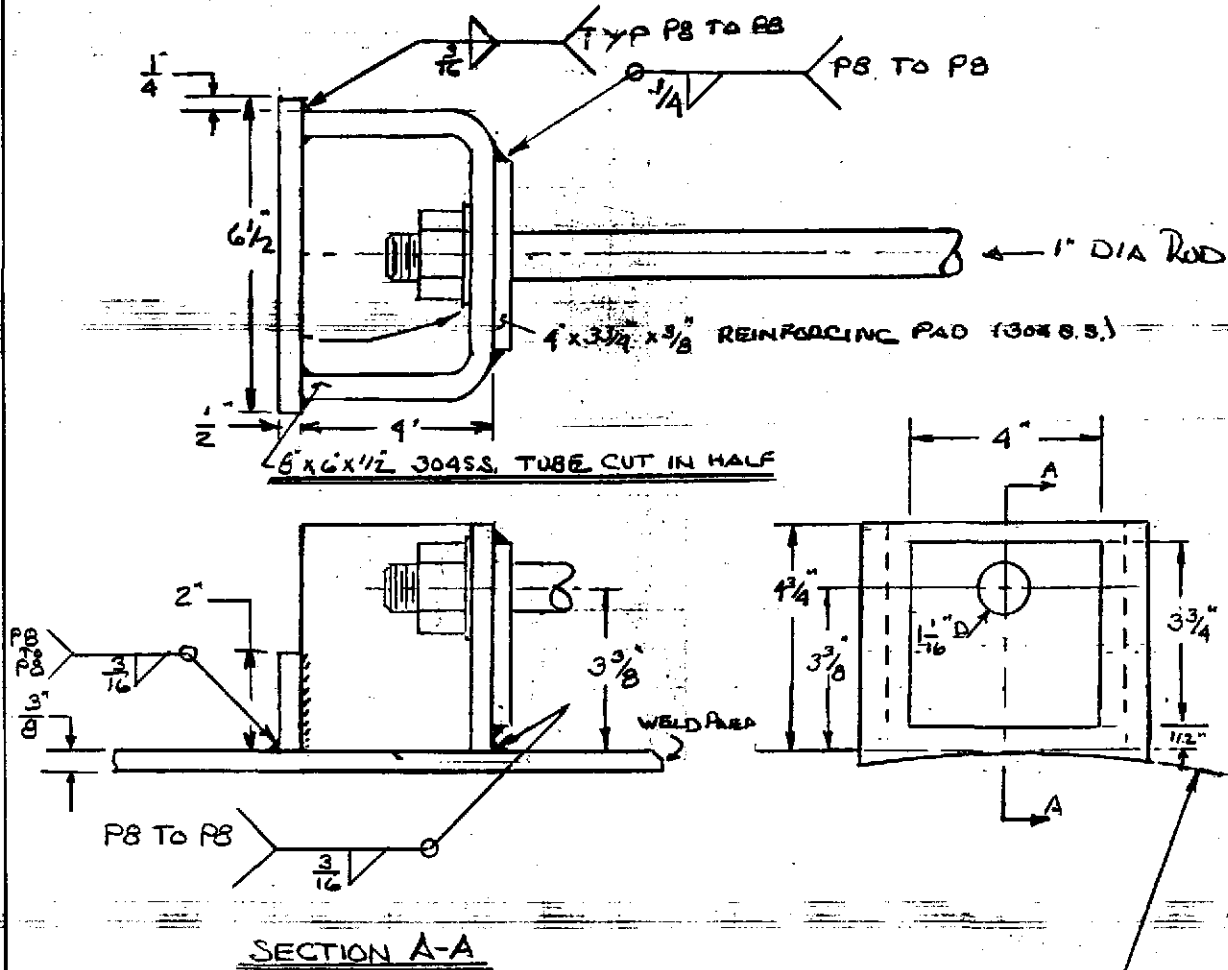
$$f_v = 1.86 + 4.3 = 6.2 \text{ ksi OK}$$

DESIGN SKETCH

SHEET 2 OF 2

SK-V049-1-084 REV0

MODIFIED DESIGN FOR SPOOL BE-3 WITH 3/8" THK WALL



SECTION A-A

WHERE:  
 $R_o$  = OUTSIDE RADIUS OF TUBE  
 TYPICAL FRONT + REAR

NOTE: THIS DESIGN IS BASED ON USING FOUR (4) LUGS SPACED AT 90°

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



## 2.0 - COMPRESS INPUT FOR SPOOL A-13 (TYPICAL)

### • SHELL/TUBE

- MATERIAL: SA 304L HIGH
- EXTERNAL/INTERNAL PRESSURE = 0 PSI
- TEMP =
- ID = 60.5" (SPOOL A-13)
- LENGTH = 23" (SPOOL A-13)
- THK'S = 3/16"

### • LUG

- MATERIAL: SA 240 304
- LUG ALLOWABLE STRESS = 16,200 PSI
- WP = 2" - HEIGHT OF LUG-BACKSIDE
- WB = 4.75" - HEIGHT OF LUG-TIE ROD SIDE
- T = .5" - THK'S OF LUG-BACKSIDE
- TB = .75" - THK'S OF LUG-TIE ROD SIDE (INCLUDES 1/4" THK PAD)
- L = 6" - LUG WIDTH / CIRC. LENGTH
- h = 8 - 2 x 1/2" THK = 7" - GUSSET HEIGHT / LUG SIDES
- TG = .5" - GUSSET THK'S / SIDE THK
- NUMBER OF LUGS - 4
- ANGULAR POSITION 1ST LUG = 0° (NOTE FOR DRAFT VESSEL LAYOUT INFO ONLY)
- FILLET WELD SIZE - 3/16" - LUG TO VESSEL WELD
- FORCE BEARING WIDTH = 2" - DIAMETER OR 1" ROD WASHER

### • DESIGN LOAD INPUT FROM DOC. NO. V049-1-048 FOR SPOOL BE-3; ID = 60.5"

$$\text{LOAD PER ROD} = 6,400\# \quad (\text{REVISED SEE APPENDIX A})$$

$$\text{DISTANCE FROM SHELL TO ROD} = 3\ 3/8"$$

- d = 3.375" - DISTANCE TO LOAD
- VL = 6400# - LONGITUDINAL SHEAR LOAD
- ML = 1800 FT-# - LONGITUDINAL MOMENT LOAD

$$\text{WHERE: } ML = 6400\# \times 3.38\text{m} / 12\text{"/FT} = 1800\text{ FT-}\#$$

- DESIGN FACTOR = 3 ; STRESS CONCENTRATION = 0
- NO PAD

$$\text{- MIN DISTANCE OF LUG TO WELD} = \sqrt{Dt} = \sqrt{(60.5)(.1875)} = 3.37"$$

$$\text{TO DATUM: } 4 + 3.37 = 7.37\text{"} \text{ MIN} \rightarrow 7\ 1/2"$$



• DESIGN LOADS FOR OTHER TUBE SIZES

- SHALL BE BASED ON A DESIGN AXIAL SPAING RATE OR 7500 #/IN FOR 2" TRAVEL  
REF: DOC. NO. V049-1-048 (EX. JT. FOR SPALL BE-3)

1. CIRCUMFERENTIAL LOADING IS:

$$- \frac{7500 \text{ #/IN}}{\pi D \text{ IN}} = \frac{7500}{\pi(60.5)} = \frac{39.5 \text{ #/IN}}{\text{IN}}$$

- FOR 2" TRAVEL:

$$\text{LOAD} = 39.5 \times 2 = 79 \text{ #/IN OF CIRCUMFERENCE}$$

- SPECIFY 100 #/IN OF CIRCUMFERENCE FOR DESIGN

2. THE DESIGN ATTACHMENT INPUT LOADS, BASED ON LOADING ONLY 3 ROAS, FOR THE FOLLOWING SIZE ARE:

- 72.25" ID:

$$\bullet V_L = \pi(72.25)(100)/3 = 7566 \text{ #}$$

$$\bullet M_L = (7566)(3.375/12) = 2128 \text{ FT-#}$$

- 48.25" ID:

$$\bullet V_L = \pi(48.25)(100)/3 = 5053 \text{ #}$$

$$\bullet M_L = (5053)(3.375/12) = 1,421 \text{ FT-#}$$

- 44.625" ID:

$$\bullet V_L = \pi(44.625)(100)/3 = 4673 \text{ #}$$

$$\bullet M_L = (4673)(3.375/12) = 1,314 \text{ FT-#}$$

- 30.5" ID:

$$\bullet V_L = \pi(30.5)(100)/3 = 3194 \text{ #}$$

$$\bullet M_L = (3194)(3.375/12) = 898 \text{ #}$$





22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



### 3.0 - LUG TO SHELL STRESS SUMMARY

- 8" X 6" X 1/2" 304 S.S. TUBE ; ALLOWABLE AT 1000°F = 18,800 PSI
- SHELL - SA 304L HIGH ; ALLOWABLE AT 1000°F = 16,700 PSI
- PRIMARY MEMBRANE ALLOWABLE STRESS:  
 $1.5S = 1.5(16,700) = 25,050 \text{ PSI}$
- PRIMARY MEMBRANE PLUS SECONDARY ALLOWABLE STRESS:  
 $3S = 3(16,700) = 50,100 \text{ PSI}$

SPOOL PIECE	ID	THK'S	LOADS		PRIMARY MEMBRANE	PRIMARY + SECONDARY
			VL[#]	ML[FT-#]		
BE 5 & BEL	72.25"	1/4" (1)	7566	2128	-9,537	-29,777
BE-3 & BE-3A	60.5	3/8"	6400	1800	-6,062	-24,261
* A-13	60.5	3/16"	6400	1800	-12,905	-37,235
* A-2	48.25	3/16"	5053	1421	-9583	-26,071
* A-1	44.625	3/16"	4673	1314	-8672	-22614
B-2	30.5	1/4"	3194	898	-4966	-12259

\* STRESS SUMMARY FOR 1/4 THK IN LIEU OF 3/16"

A-13	60.5	1/4"	6400	1800	-7903	-23871
A-2	48.25	1/4"	5053	1421	-6030	-16274
A-1	44.625	1/4"	4673	1314	-5482	-14739

NOTE: THE FINAL DESIGN FOR SPOOL PIECES A-1, A-2 + A-13 HAS INCORPORATED A 1/4" WALL THICKNESS

(1) Now  $t = 3/8"$  FOR BE-5  
 SEE Pg. A-9 (REV.1)

**BELLOWS BE-5**

**ASME Section VIII Division 1, 1995 Edition, A95 Addenda**

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0                      Outer = 0                      in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
Category B joints - Spot UW-11(b) type 1

Estimated weight: new = 1033.1    corr = 1033.1    lb  
capacity: new = 1102.711    corr = 1102.711    US ga

OD = 72.25    length Lc = 63    t = 0.25    in (new)

**MAP: (New & at 0 deg F)                      Appendix 1-1(a)**

$$\begin{aligned} P &= S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0 \\ &= 98.50798 \text{ psi} \end{aligned}$$

**MAWP: (Corroded & at 0 deg F)                      Appendix 1-1(a)**

$$\begin{aligned} P &= S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0 \\ &= 98.50798 \text{ psi} \end{aligned}$$

### BE-5 Lug (No Pad)

Lug material specification	= A 240 304
Lug allowable stress	= 18800 psi
Top plate width	wp = 2 in
Base plate width	wb = 4.75 in
Top plate thickness	t = 0.5 in
Base plate thickness	tb = 0.875 in
Lug length circ. direction	L = 6 in
Gusset height	h = 7 in
Gusset thickness	tg = 0.5 in
Number of lugs	= 4
Angular position, first lug	= 0 degrees
Fillet weld size	tw = 0.1875 in
Force bearing width	Fb = 2 in
Distance to load	d = 3.375 in

#### Lug top plate required thickness, Bednar pg 153

$$\begin{aligned}ta &= 0.75*(VL*d*L)/(Sa*wp^2*h) \\ &= 0.75*(7566*3.375*6)/(18800*2^2*7) \\ &= 0.25 \text{ in}\end{aligned}$$

#### Lug gusset required thickness

$$\begin{aligned}Sc &= 18000/(1 + (1/18000)*(h/(0.289*tg))^2) \\ &= 18000/(1 + (1/18000)*(7/(0.289*0.5))^2) \\ &= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}tg &= VL*(3*d - wb)/(Sc*wb^2*SIN(Alpha)^2) \\ &= 7566*(3*3.375 - 4.75)/(15923.95*4.75^2*SIN(68.552)^2) \\ &= 0.1307 \text{ in}\end{aligned}$$

#### Lug base plate required thickness

From Escoe table 4-8

$$fc = VL/(Fb*L) = 630.5 \text{ psi}$$

$$\begin{aligned}Mx &= Cx*fc*Gs^2 \\ &= 0.0923*630.5*5^2 = 1454.879\end{aligned}$$

$$\begin{aligned}My &= Cy*fc*wb^2 \\ &= -.126*630.5*4.75^2 = -1792.433\end{aligned}$$

$$\begin{aligned}tb &= \text{Sqr}(6*Mmax / Sa) \\ &= \text{Sqr}(6*1792.433 / 18800) \\ &= 0.7563 \text{ in}\end{aligned}$$

#### Check lug attachment stresses

Radial load	Pr = 0 lbf
Circumferential moment	Mc = 0 lbf-ft
Circumferential shear	Vc = 0 lbf
Longitudinal moment	ML = 2128 lbf-ft
Longitudinal shear	VL = 7566 lbf

**BE-5 Lug (No Pad)**

Internal pressure  $P = 0$  psi

**Stresses at the lug edge per WRC bulletin 107 ( psi)**

Mean radius  $R_m = 36$  in

$R_m/t = 144$

$C_1 = 3, C_2 = 4.1875$  in

Stress concentration factor  $K_n$  (tension) = 1

Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -29777 psi

Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -9537 psi

Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.

**BE-5 Lug (No Pad)**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	Dl
3C*	12.092	0.116								
4C*	20.080	0.106								
1C	0.0826	0.094								
2C-1	0.0493	0.094								
3A*	5.5740	0.093								
1A	0.0798	0.097								
3B*	14.704	0.104	-9537	-9537	9537	9537				
1B-1	0.0287	0.097	-20240	20240	20240	-20240				
pressure stress*										
Total circ stress			-29777	10703	29777	-10703				
Primary membrane circ stress*			-9537	-9537	9537	9537				
3C*	13.227	0.106								
4C*	19.332	0.116								
1C-1	0.0731	0.108								
2C	0.0440	0.108								
4A*	10.076	0.093								
2A	0.0378	0.109								
4B*	5.6219	0.104	-4517	-4517	4517	4517				
2B-1	0.0356	0.108	-22539	22539	22539	-22539				
pressure stress*										
Total long stress			-27056	18022	27056	-18022				
Primary membrane long stress*			-4517	-4517	4517	4517				
torsion moment Mt										
Circ shear from Vc										
Long shear from VL							-1807	1807	-1807	1807
Total Shear stress							-1807	-1807	1807	1807
Combined stress			-29777	18022	29777	-18022	3614	3614	3614	3614

TABLE OF CONTENTS

SPOOL BE-3 . . . . .	1
8X6 LUG - WITH NO PAD . . . . .	2
Total Pages In This Report . . . . .	4

SPOOL BE-3

ASME Section VIII Division 1, 1992 Edition, A94 Addenda

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0 Outer= 0 in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
Category B joints - Spot UW-11(b) type 1

Estimated weight: new = 478.4 corr = 478.4 lb  
capacity: new = 286.231 corr = 286.231 US ga

ID = 60.5 length Lc= 23 t = 0.375 in (new)

MAP: (New & at 0 deg F) UG-27(c) (1)

$$P = S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s$$
$$= 16700 \cdot 0.85 \cdot 0.375 / (30.25 + 0.6 \cdot 0.375) - 0$$
$$= 174.6719 \text{ psi}$$

MAWP: (Corroded & at 100 deg F) UG-27(c) (1)

$$P = S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s$$
$$= 16700 \cdot 0.85 \cdot 0.375 / (30.25 + 0.6 \cdot 0.375) - 0$$
$$= 174.6719 \text{ psi}$$

## BX6 LUG - WITH NO PAD

Lug material specification = A 240 304  
Lug allowable stress = 18800 psi  
Top plate width wp = 2 in  
Base plate width wb = 4.75 in  
Top plate thickness t = 0.5 in  
Base plate thickness tb = 0.75 in  
Lug length circ. direction L = 6 in  
Gusset height h = 3.25 in  
Gusset thickness tg = 0.5 in  
Number of lugs = 4  
Angular position, first lug = 0 degrees  
Fillet weld size tw = 0.1875 in  
Force bearing width Fb = 2 in  
Distance to load d = 3.375 in

### Lug top plate required thickness. Bednar pg 153

$$\begin{aligned}ta &= 0.75 \cdot (VL \cdot d \cdot L) / (Sa \cdot wp^2 \cdot h) \\ &= 0.75 \cdot (6400 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 3.25) \\ &= 0.3977 \text{ in}\end{aligned}$$

### Lug gusset required thickness

$$\begin{aligned}Sc &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot tg))^2) \\ &= 18000 / (1 + (1/18000) \cdot (3.25 / (0.289 \cdot 0.5))^2) \\ &= 17507.97 \text{ psi}\end{aligned}$$

$$\begin{aligned}tg &= VL \cdot (3 \cdot d - wb) / (Sc \cdot wb^2 \cdot \sin(\alpha)^2) \\ &= 6400 \cdot (3 \cdot 3.375 - 4.75) / (17507.97 \cdot 4.75^2 \cdot \sin(49.764)^2) \\ &= 0.1494 \text{ in}\end{aligned}$$

### Lug base plate required thickness

From Escoe table 4-8

$$fc = VL / (Fb \cdot L) = 533.3333 \text{ psi}$$

$$\begin{aligned}Mx &= Cx \cdot fc \cdot Gs^2 \\ &= 0.0923 \cdot 533.3333 \cdot 5^2 = 1230.667\end{aligned}$$

$$\begin{aligned}My &= Cy \cdot fc \cdot wb^2 \\ &= -.126 \cdot 533.3333 \cdot 4.75^2 = -1516.2\end{aligned}$$

$$\begin{aligned}tb &= \text{Sqr}(6 \cdot M_{\max} / Sa) \\ &= \text{Sqr}(6 \cdot 1516.2 / 18800) \\ &= 0.6956 \text{ in}\end{aligned}$$

### Check lug attachment stresses

Radial load Pr = 0 lbf  
Circumferential moment Mc = 0 lbf-ft  
Circumferential shear Vc = 0 lbf



8X6 LUG - WITH NO PAD

Longitudinal moment            ML = 1800 lbf-ft  
Longitudinal shear            VL = 6400 lbf  
Internal pressure              P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius  $R_m = 30.4375$  in  
 $R_m/t = 81.16666$

$C_1 = 3, C_2 = 2.25$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -24621 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -6062 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.

8X6 LUG - WITH NO PAD

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	D
3C*	11.520	0.085								
4C*	13.244	0.092								
1C	0.1040	0.093								
2C-1	0.0696	0.093								
3A*	2.8538	0.09								
1A	0.0879	0.099								
3B*	8.6001	0.081	-6062	-6062	6062	6062				
1B-1	0.0421	0.083	-15275	15275	15275	-15275				
pressure stress*										
Total circ stress			-21337	9213	21337	-9213				
Primary membrane circ stress*			-6062	-6062	6062	6062				
3C*	10.947	0.092								
4C*	13.484	0.085								
1C-1	0.1104	0.087								
2C	0.0740	0.087								
4A*	4.4600	0.09								
2A	0.0475	0.095								
4B*	2.6643	0.081	-1663	-1663	1663	1663				
2B-1	0.0642	0.085	-22958	22958	22958	-22958				
pressure stress*										
Total long stress			-24621	21295	24621	-21295				
Primary membrane long stress*			-1663	-1663	1663	1663				
torsion moment Mt										
Circ shear from Vc							-1896	-1896	1896	18
Long shear from VL										
Total Shear stress							-1896	-1896	1896	18
Combined stress			-24621	21295	24621	-21295	3792	3792	3792	38

TABLE OF CONTENTS

SPOOL A-13 . . . . .	1
8X6 LUG - WITH NO PAD . . . . .	2
Total Pages In This Report . . . . .	4

SPOOL A-13

ASME Section VIII Division 1, 1992 Edition, A94 Addenda

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0                      Outer = 0                      in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
                  Category B joints - Spot UW-11(b) type 1

Estimated weight:                      new = 238.4                      corr = 238.4                      lb  
                  capacity:                      new = 286.231                      corr = 286.231                      US ga

ID = 60.5                      length Lc = 23                      t = 0.1875                      in (new)

MAP:                      (New & at 0 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (30.25 + 0.6 \cdot 0.1875) - 0 \\ &= 87.65953 \text{ psi} \end{aligned}$$

MAWP:                      (Corroded & at 100 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (30.25 + 0.6 \cdot 0.1875) - 0 \\ &= 87.65953 \text{ psi} \end{aligned}$$

### 8X6 LUG - WITH NO PAD

Lug material specification = A 240 304  
Lug allowable stress = 18800 psi  
Top plate width wp = 2 in  
Base plate width wb = 4.75 in  
Top plate thickness t = 0.5 in  
Base plate thickness tb = 0.75 in  
Lug length circ. direction L = 6 in  
Gusset height h = 7 in  
Gusset thickness tg = 0.5 in  
Number of lugs = 4  
Angular position, first lug = 0 degrees  
Fillet weld size tw = 0.1875 in  
Force bearing width Fb = 2 in  
Distance to load d = 3.375 in

#### Lug top plate required thickness, Bednar pg 153

$$\begin{aligned}ta &= 0.75 \cdot (VL \cdot d \cdot L) / (Sa \cdot wp^2 \cdot h) \\ &= 0.75 \cdot (6400 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 7) \\ &= 0.25 \text{ in}\end{aligned}$$

#### Lug gusset required thickness

$$\begin{aligned}Sc &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot tg))^2) \\ &= 18000 / (1 + (1/18000) \cdot (7 / (0.289 \cdot 0.5))^2) \\ &= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}tg &= VL \cdot (3 \cdot d - wb) / (Sc \cdot wb^2 \cdot \text{SIN}(\text{Alpha})^2) \\ &= 6400 \cdot (3 \cdot 3.375 - 4.75) / (15923.95 \cdot 4.75^2 \cdot \text{SIN}(68.552)^2) \\ &= 0.1105 \text{ in}\end{aligned}$$

#### Lug base plate required thickness

From Escoe table 4-8

$$fc = VL / (Fb \cdot L) = 533.3333 \text{ psi}$$

$$\begin{aligned}Mx &= Cx \cdot fc \cdot Gs^2 \\ &= 0.0923 \cdot 533.3333 \cdot 5^2 = 1230.667\end{aligned}$$

$$\begin{aligned}My &= Cy \cdot fc \cdot wb^2 \\ &= -.126 \cdot 533.3333 \cdot 4.75^2 = -1516.2\end{aligned}$$

$$\begin{aligned}tb &= \text{Sqr}(6 \cdot M_{\text{max}} / Sa) \\ &= \text{Sqr}(6 \cdot 1516.2 / 18800) \\ &= 0.6956 \text{ in}\end{aligned}$$

#### Check lug attachment stresses

Radial load Pr = 0 lbf  
Circumferential moment Mc = 0 lbf-ft  
Circumferential shear Vc = 0 lbf

8X6 LUG - WITH NO PAD

Longitudinal moment            ML = 1800 lbf-ft  
Longitudinal shear            VL = 6400 lbf  
Internal pressure              P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius Rm = 30.34375 in  
Rm/t = 161.8333

C1 = 3, C2 = 4.125 in

Stress concentration factor Kn (tension) = 1  
Stress concentration factor Kb (bending) = 1

Local circ. pressure stress =  $P \cdot Rm/t = 0$  psi

~~Local long. pressure stress =  $P \cdot Rm/2t = 0$  psi~~

Maximum combined stress = -37235 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -12905 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.

**8X6 LUG - WITH NO PAD**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	D
3C*	10.354	0.136								
4C*	20.589	0.124								
1C	0.0707	0.111								
2C-1	0.0366	0.111								
3A*	6.3028	0.11								
1A	0.0729	0.114								
3B*	14.701	0.122	-12905	-12905	12905	12905				
1B-1	0.0226	0.113	-24330	24330	24330	-24330				
pressure stress*										
Total circ stress			-37235	11425	37235	-11425				
Primary membrane circ stress*			-12905	-12905	12905	12905				
3C*	11.749	0.124								
4C*	19.629	0.136								
1C-1	0.0613	0.126								
2C	0.0391	0.126								
4A*	12.653	0.11								
2A	0.0328	0.127								
4B*	5.9259	0.122	-6520	-6520	6520	6520				
2B-1	0.0273	0.125	-26506	26506	26506	-26506				
pressure stress*										
Total long stress			-33026	19986	33026	-19986				
Primary membrane long stress*			-6520	-6520	6520	6520				
torsion moment Mt										
Circ shear from Vc							-2069	-2069	2069	20
Long shear from VL										
Total Shear stress							-2069	-2069	2069	20
Combined stress			-37235	19986	37235	-19986	4138	4138	4138	40

TABLE OF CONTENTS

SPOOL A-2 . . . . .	1
8X6 LUG - WITH NO PAD . . . . .	2
Total Pages In This Report . . . . .	4



SPOOL A-2

ASME Section VIII Division 1, 1992 Edition, A94 Addenda

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0                      Outer= 0                      in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
Category B joints - Spot UW-11(b) type 1

Estimated weight:                      new = 224.5                      corr = 224.5                      lb  
capacity:                      new = 214.744                      corr = 214.744                      US ga

ID = 48.25      length Lc= 27.13                      t = 0.1875      in (new)

MAP:                      (New & at 0 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (24.125 + 0.6 \cdot 0.1875) - 0 \\ &= 109.8118 \text{ psi} \end{aligned}$$

MAWP:                      (Corroded & at 100 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (24.125 + 0.6 \cdot 0.1875) - 0 \\ &= 109.8118 \text{ psi} \end{aligned}$$

## 8X6 LUG - WITH NO PAD

Lug material specification = A 240 304  
Lug allowable stress = 18800 psi  
Top plate width wp = 2 in  
Base plate width wb = 4.75 in  
Top plate thickness t = 0.5 in  
Base plate thickness tb = 0.625 in  
Lug length circ. direction L = 6 in  
Gusset height h = 7 in  
Gusset thickness tg = 0.5 in  
Number of lugs = 4  
Angular position, first lug = 0 degrees  
Fillet weld size tw = 0.1875 in  
Force bearing width Fb = 2 in  
Distance to load d = 3.375 in

### Lug top plate required thickness, Bednar pg 153

$$\begin{aligned}ta &= 0.75 \cdot (VL \cdot d \cdot L) / (Sa \cdot wp^2 \cdot h) \\ &= 0.75 \cdot (5053 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 7) \\ &= 0.25 \text{ in}\end{aligned}$$

### Lug gusset required thickness

$$\begin{aligned}Sc &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot tg))^2) \\ &= 18000 / (1 + (1/18000) \cdot (7 / (0.289 \cdot 0.5))^2) \\ &= 15923.95 \text{ psi} \\ tg &= VL \cdot (3 \cdot d - wb) / (Sc \cdot wb^2 \cdot \text{SIN}(\text{Alpha})^2) \\ &= 5053 \cdot (3 \cdot 3.375 - 4.75) / (15923.95 \cdot 4.75^2 \cdot \text{SIN}(68.552)^2) \\ &= 0.0873 \text{ in}\end{aligned}$$

### Lug base plate required thickness

From Escoe table 4-8

$$\begin{aligned}fc &= VL / (Fb \cdot L) = 421.0833 \text{ psi} \\ Mx &= Cx \cdot fc \cdot Gs^2 \\ &= 0.0923 \cdot 421.0833 \cdot 5^2 = 971.6498 \\ My &= Cy \cdot fc \cdot wb^2 \\ &= -.126 \cdot 421.0833 \cdot 4.75^2 = -1197.087 \\ tb &= \text{Sqr}(6 \cdot Mmax / Sa) \\ &= \text{Sqr}(6 \cdot 1197.087 / 18800) \\ &= 0.6181 \text{ in}\end{aligned}$$

### Check lug attachment stresses

Radial load Pr = 0 lbf  
Circumferential moment Mc = 0 lbf-ft  
Circumferential shear Vc = 0 lbf

8X6 LUG - WITH NO PAD

Longitudinal moment            ML = 1421 lbf-ft  
Longitudinal shear            VL = 5053 lbf  
Internal pressure              P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius  $R_m = 24.21875$  in  
 $R_m/t = 129.1667$

$C_1 = 3$ ,  $C_2 = 4.0625$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -26071 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -9583 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.

**BX6 LUG - WITH NO PAD**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	D
3C*	7.1556	0.168								
4C*	15.373	0.154								
1C	0.0648	0.138								
2C-1	0.0308	0.138								
3A*	4.9415	0.137								
1A	0.0672	0.143								
3B*	10.889	0.152	-9583	-9583	9583	9583				
1B-1	0.0195	0.142	-16488	16488	16488	-16488				
pressure stress*										
Total circ stress			-26071	6905	26071	-6905				
Primary membrane circ stress*			-9583	-9583	9583	9583				
3C*	7.9455	0.154								
4C*	14.630	0.168								
1C-1	0.0520	0.157								
2C	0.0357	0.157								
4A*	10.505	0.137								
2A	0.0289	0.16								
4B*	4.6023	0.152	-4863	-4863	4863	4863				
2B-1	0.0220	0.158	-16744	16744	16744	-16744				
pressure stress*										
Total long stress			-21607	11881	21607	-11881				
Primary membrane long stress*			-4863	-4863	4863	4863				
torsion moment Mt										
Circ shear from Vc							-1658	-1658	1658	18
Long shear from VL										
Total Shear stress							-1658	-1658	1658	18
Combined stress			-26071	11881	26071	-11881	3316	3316	3316	38

TABLE OF CONTENTS

SPOOL A-1 . . . . . 1  
8X6 LUG - WITH NO PAD . . . . . 2  
Total Pages In This Report . . . . . 4

SPOOL A-1

ASME Section VIII Division 1, 1992 Edition, A94 Addenda

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0                      Outer = 0                      in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
                  Category B joints - Spot UW-11(b) type 1

Estimated weight:            new = 229.7            corr = 229.7            lb  
                  capacity:            new = 203.121        corr = 203.121        US ga

ID = 44.625    length Lc = 30            t = 0.1875    in (new)

MAP:            (New & at 0 deg F)                      UG-27(c)(1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (22.3125 + 0.6 \cdot 0.1875) - 0 \\ &= 118.6873 \text{ psi} \end{aligned}$$

MAWP:            (Corroded & at 100 deg F)                      UG-27(c)(1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.1875 / (22.3125 + 0.6 \cdot 0.1875) - 0 \\ &= 118.6873 \text{ psi} \end{aligned}$$

## 8X6 LUG - WITH NO PAD

Lug material specification = A 240 304  
Lug allowable stress = 18800 psi  
Top plate width wp = 2 in  
Base plate width wb = 4.75 in  
Top plate thickness t = 0.5 in  
Base plate thickness tb = 0.625 in  
Lug length circ. direction L = 6 in  
Gusset height h = 7 in  
Gusset thickness tg = 0.5 in  
Number of lugs = 4  
Angular position, first lug = 0 degrees  
Fillet weld size tw = 0.1875 in  
Force bearing width Fb = 2 in  
Distance to load d = 3.375 in

### Lug top plate required thickness. Bednar pg 153

$$\begin{aligned}ta &= 0.75 * (VL * d * L) / (Sa * wp^2 * h) \\ &= 0.75 * (4673 * 3.375 * 6) / (18800 * 2^2 * 7) \\ &= 0.25 \text{ in}\end{aligned}$$

### Lug gusset required thickness

$$\begin{aligned}Sc &= 18000 / (1 + (1/18000) * (h / (0.289 * tg))^2) \\ &= 18000 / (1 + (1/18000) * (7 / (0.289 * 0.5))^2) \\ &= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}tg &= VL * (3 * d - wb) / (Sc * wb^2 * SIN(Alpha)^2) \\ &= 4673 * (3 * 3.375 - 4.75) / (15923.95 * 4.75^2 * SIN(68.552)^2) \\ &= 0.0807 \text{ in}\end{aligned}$$

### Lug base plate required thickness

From Escoe table 4-8

$$fc = VL / (Fb * L) = 389.4167 \text{ psi}$$

$$\begin{aligned}Mx &= Cx * fc * Gs^2 \\ &= 0.0923 * 389.4167 * 5^2 = 898.5789\end{aligned}$$

$$\begin{aligned}My &= Cy * fc * wb^2 \\ &= -.126 * 389.4167 * 4.75^2 = -1107.063\end{aligned}$$

$$\begin{aligned}tb &= Sqr(6 * Mmax / Sa) \\ &= Sqr(6 * 1107.063 / 18800) \\ &= 0.5944 \text{ in}\end{aligned}$$

### Check lug attachment stresses

Radial load Pr = 0 lbf  
Circumferential moment Mc = 0 lbf-ft  
Circumferential shear Vc = 0 lbf

8X6 LUG - WITH NO PAD

Longitudinal moment            ML = 1314 lbf-ft  
Longitudinal shear            VL = 4673 lbf  
Internal pressure              P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius  $R_m = 22.40625$  in  
 $R_m/t = 119.5$

$C_1 = 3$ ,  $C_2 = 4.0625$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -22614 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -8672 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.



8X6 LUG - WITH NO PAD

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	D
3C*	6.2968	0.182								
4C*	13.925	0.167								
1C	0.0603	0.149								
2C-1	0.0271	0.149								
3A*	4.6292	0.148								
1A	0.0651	0.155								
3B*	9.8548	0.164	-8672	-8672	8672	8672				
1B-1	0.0179	0.154	-13942	13942	13942	-13942				
pressure stress*										
Total circ stress			-22614	5270	22614	-5270				
Primary membrane circ stress*			-8672	-8672	8672	8672				
3C*	7.1198	0.167								
4C*	13.186	0.182								
1C-1	0.0491	0.169								
2C	0.0352	0.169								
4A*	10.031	0.148								
2A	0.0277	0.174								
4B*	4.2361	0.164	-4428	-4428	4428	4428				
2B-1	0.0209	0.172	-14636	14636	14636	-14636				
pressure stress*										
Total long stress			-19064	10208	19064	-10208				
Primary membrane long stress*			-4428	-4428	4428	4428				
torsion moment Mt										
Circ shear from Vc							-1534	-1534	1534	15
Long shear from VL										
Total Shear stress							-1534	-1534	1534	15
Combined stress			-22614	10208	22614	-10208	3068	3068	3068	30

NOTE: LAST COLUMN IS "DL" WITH VALUES IDENTICAL TO "Du"

TABLE OF CONTENTS

SPOOL B-2 . . . . .	1
8X6 LUG - WITH NO PAD . . . . .	2
Total Pages In This Report . . . . .	4

SPOOL B-2

ASME Section VIII Division 1, 1992 Edition, A94 Addenda

Component: Cylinder  
Material specification: SA 240 304L HIGH

Corrosion allowance: Inner C = 0                      Outer= 0                      in

\* PWHT is performed

Radiography:    Category A joints - Spot UW-11(b) type 1  
                  Category B joints - Spot UW-11(b) type 1

Estimated weight:            new = 546.3            corr = 546.3            lb  
                  capacity:            new = 246.702        corr = 246.702        US ga

ID = 30.5            length Lc= 78            t = 0.25            in (new)

MAP:            (New & at 0 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.25 / (15.25 + 0.6 \cdot 0.25) - 0 \\ &= 230.4383 \text{ psi} \end{aligned}$$

MAWP:            (Corroded & at 100 deg F)                      UG-27(c) (1)

$$\begin{aligned} P &= S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s \\ &= 16700 \cdot 0.85 \cdot 0.25 / (15.25 + 0.6 \cdot 0.25) - 0 \\ &= 230.4383 \text{ psi} \end{aligned}$$

## 8X6 LUG - WITH NO PAD

Lug material specification = A 240 304  
Lug allowable stress = 18800 psi  
Top plate width wp = 2 in  
Base plate width wb = 4.75 in  
Top plate thickness t = 0.5 in  
Base plate thickness tb = 0.625 in  
Lug length circ. direction L = 6 in  
Gusset height h = 7 in  
Gusset thickness tg = 0.5 in  
Number of lugs = 4  
Angular position, first lug = 0 degrees  
Fillet weld size tw = 0.1875 in  
Force bearing width Fb = 2 in  
Distance to load d = 3.375 in

### Lug top plate required thickness, Bednar pg 153

$$\begin{aligned}t_a &= 0.75 \cdot (V_L \cdot d \cdot L) / (S_a \cdot w_p^2 \cdot h) \\&= 0.75 \cdot (3200 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 7) \\&= 0.25 \text{ in}\end{aligned}$$

### Lug gusset required thickness

$$\begin{aligned}S_c &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot t_g))^2) \\&= 18000 / (1 + (1/18000) \cdot (7 / (0.289 \cdot 0.5))^2) \\&= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}t_g &= V_L \cdot (3 \cdot d - w_b) / (S_c \cdot w_b^2 \cdot \sin(\text{Alpha})^2) \\&= 3200 \cdot (3 \cdot 3.375 - 4.75) / (15923.95 \cdot 4.75^2 \cdot \sin(68.552)^2) \\&= 0.0553 \text{ in}\end{aligned}$$

### Lug base plate required thickness

From Escoe table 4-8

$$f_c = V_L / (F_b \cdot L) = 266.6667 \text{ psi}$$

$$\begin{aligned}M_x &= C_x \cdot f_c \cdot G_s^2 \\&= 0.0923 \cdot 266.6667 \cdot 5^2 = 615.3333\end{aligned}$$

$$\begin{aligned}M_y &= C_y \cdot f_c \cdot w_b^2 \\&= -.126 \cdot 266.6667 \cdot 4.75^2 = -758.1\end{aligned}$$

$$\begin{aligned}t_b &= \text{Sqr}(6 \cdot M_{\text{max}} / S_a) \\&= \text{Sqr}(6 \cdot 758.1 / 18800) \\&= 0.4919 \text{ in}\end{aligned}$$

### Check lug attachment stresses

Radial load Pr = 0 lbf  
Circumferential moment Mc = 0 lbf-ft  
Circumferential shear Vc = 0 lbf

8X6 LUG - WITH NO PAD

Longitudinal moment            ML = 900 lbf-ft  
Longitudinal shear            VL = 3200 lbf  
Internal pressure              P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius  $R_m = 15.375$  in  
 $R_m/t = 61.5$

$C_1 = 3, C_2 = 4.0625$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -8055 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 50100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -3214 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 25050$  psi

The maximum primary membrane stress is within allowable limits.

8X6 LUG - WITH NO PAD

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	D
3C*	2.9982	0.265								
4C*	6.9678	0.243								
1C	0.0648	0.218								
2C-1	0.0231	0.218								
3A*	2.3063	0.216								
1A	0.0633	0.235								
3B*	4.8286	0.239	-3214	-3214	3214	3214				
1B-1	0.0164	0.231	-4792	4792	4792	-4792				
pressure stress*										
Total circ stress			-8006	1578	8006	-1578				
Primary membrane circ stress*			-3214	-3214	3214	3214				
3C*	3.3975	0.243								
4C*	6.5477	0.265								
1C-1	0.0403	0.247								
2C	0.0321	0.247								
4A*	5.4408	0.216								
2A	0.0254	0.263								
4B*	2.2933	0.239	-1831	-1831	1831	1831				
2B-1	0.0237	0.257	-6224	6224	6224	-6224				
pressure stress*										
Total long stress			-8055	4393	8055	-4393				
Primary membrane long stress*			-1831	-1831	1831	1831				
torsion moment Mt										
Circ shear from Vc										
Long shear from VL							-788	-788	788	8
Total Shear stress							-788	-788	788	8
Combined stress			-8055	4393	8055	-4393	1576	1576	1576	18

NOTE: LAST COLUMN IS "DL" WITH VALUES IDENTICAL TO "Du"

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE A-1 OF A-30
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug Design"		

## APPENDIX - A

### Revised Stress Summary

Revision 0 of Doc No. V049-1-084 provided the design for the LIGO Expansion Joint Tie Rod "Lugs". The original design used 6400. lbs per rod for the "Lugs" on spool pieces BE-3 & BE-3A. The design loads for all other vacuum tubes with expansion joints used an axial spring rate of 7500. #/in.

All vacuum tubes are to undergo vacuum testing to check against leakage. Although the design loads are valid for operating conditions, the vacuum test will produce forces equivalent to those generated in Doc. No. V049-1-032 *Component Interface Loads*. Revision 1 uses these interface loads to evaluate stresses in vacuum tubes having tie rod lugs for expansion joints.

Revision 1 includes appendices to the original calculation. The force per lug from the component interface loads is factored against the loads used in Rev. 0. This ratio is applied to the tabulated stresses in Rev. 0 additionally, the local circumferential and longitudinal stresses at the lug are calculated and added to the membrane stresses. The resulting primary and primary plus secondary membrane stresses are compared against allowable stress limits at 400° F ("Bakeout" conditions).

Previous revisions inexplicably omitted spool BE-1, Revision 2 of Doc No. V049-1-084 evaluates BE-1. BE-1 has a shell thickness of 1/4 in. to alleviate the overstress condition due to the lugs *interaction with the thin shell*, repads are required at the lugs.

The results indicate that all vacuum tubes are within allowable Primary Membrane Stress limits at 400 F. All vacuum tubes require a minimum shell thickness of 0.250 inches. The exception is Beam Tube Manifolds: BE-3, BE-3A and BE-5 require a minimum shell thickness of 0.375 in. and Beam Tube Manifold BE-1 requires repads at the lugs (see pg A-16).

Note: To economize on material costs, vacuum tube BE-5 may be 0.250 in thick with the bellows section (60 inch length) at 0.375 in.

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE A-2 OF A-30
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug Design"		

### CORRECTED PRIMARY MEMBRANE STRESSES

SPOOL PIECE	I. D. Ø	Shell Thickness	Primary Stress (psi)	Stress Correction Factor Force/Rod ÷ Force/Rod	Local Stress		Corrected Primary Stress (psi)	Allowable Primary Stress (psi)	Stress Result
					Circ.σ	Long.σ			
BE-5	72.25 in.	3/8 in.	9588.	See page A-29	1431.	715.	11734.	22050. @ 400.° F	√
* BE-1	72.25 in.	1/4in.	9820.	See page A-20	2140.	1070.	13030.	22050. @ 400.° F	√
BE-3 & BE-3A	60.5 in.	3/8 in.	6062.	11365. ÷ 6400. = 1.776	1193.	597.	12555.	22050. @ 400.° F	√
A-13	60.5 in.	1/4in.	12905.	11365. ÷ 6400. = 2.362	1793.	897.	16725.	22050. @ 400.° F	√
A-2	48.25 in.	1/4in.	9583.	9813. ÷ 5053. = 1.942	1433.	717.	13861.	22050. @ 400.° F	√
A-1	44.63 in.	1/4in.	5482.	8467. ÷ 4673. = 1.812	1327.	663.	11923.	22050. @ 400.° F	√
B-2	30.5 in.	1/4in.	4966.	4128. ÷ 3194. = 1.292	911.	456.	7785.	22050. @ 400.° F	√

\* BE-1 with 3/8 in. repads at lugs

### CORRECTED PRIMARY + SECONDARY MEMBRANE STRESSES

SPOOL PIECE	I. D. Ø	Shell Thickness	Primary + Secondary σ	Stress Correction Factor (Force/Rod + Force/Rod)	Local Stress		Corrected Stress Primary + Secondary	Allowable Stress Primary + Secondary	Stress Result
					Circ.σ	Long.σ			
BE-5	72.25 in.	3/8 in.	31316.	See page A-29	1431.	715.	33462.	44100. @ 400.° F	√
* BE-1	72.25 in.	1/4in.	25126.	See page A-20	2140.	1070.	28336.	44100. @ 400.° F	√
BE-3 & BE-3A	60.5 in.	3/8 in.	24261.	11365. ÷ 6400. = 1.776	1193.	597.	44872.	44100. @ 400.° F	2% over
A-13	60.5 in.	1/4in.	23871.	11365. ÷ 6400. = 2.362	1793.	897.	45080.	44100. @ 400.° F	2% over
A-2	48.25 in.	1/4in.	16274.	9813. ÷ 5053. = 1.942	1433.	717.	33755.	44100. @ 400.° F	√
A-1	44.63 in.	1/4in.	14739.	8467. ÷ 4673. = 1.812	1327.	663.	28696.	44100. @ 400.° F	√
B-2	30.5 in.	1/4in.	12259.	4128. ÷ 3194. = 1.292	911.	456.	17211.	44100. @ 400.° F	√

\* BE-1 with 3/8 in. repads at lugs



COMPONENT INTERFACE LOADS REF DOC No. V049-1-032

44.625"  $\phi$  TUBE

$$F = 25.4 \text{ K}$$

$$3 \text{ LUGS} \Rightarrow 25.4 \text{ K} / 3 = 8.467 \text{ K/LUG}$$

48.25"  $\phi$  TUBE

$$F = 29.44 \text{ K}$$

$$3 \text{ LUGS} \Rightarrow 29.44 \text{ K} / 3 = 9.8133 \text{ K/LUG}$$

60.5"  $\phi$  TUBE

$$F = 45.46 \text{ K}$$

$$4 \text{ LUGS} \Rightarrow 45.46 \text{ K} / 4 = 11.365 \text{ K/LUG}$$

72.25"  $\phi$  TUBE

$$F = 64.1 \text{ K}$$

$$4 \text{ LUGS} \Rightarrow 64.1 \text{ K} / 4 = 16.025 \text{ K/LUG}$$

30.5"  $\phi$  TUBE

$$F = \left( 14.7 \frac{\text{lbs}}{\text{in}^2} \right) \frac{\left( 30.5" + 2.25" \right)^2 \pi}{4} = 12383. \text{ lbs.}$$

$$3 \text{ LUGS} \Rightarrow 12383 \text{ lbs} / 3 \text{ LUGS} = 4128 \text{ lbs/LUG.}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



B-2

30.5"  $\phi$  TUBE 1/4" SHELL

Primary Membrane Stress

$$\begin{aligned}\sigma_M &= 4966 \text{ psi} \left( \frac{4128 \text{ lbs.}}{3194 \text{ lbs}} \right) \\ &= 6418 \text{ psi}\end{aligned}$$

Primary + Secondary Stress

$$\sigma_{M+PS} = 12259 \text{ psi} \left( \frac{4128 \text{ lbs.}}{3194 \text{ lbs}} \right) = 15844 \text{ psi}$$

• Local Circ. Stress (@ Wg)

$$\sigma_c = \frac{(14.7 \text{ #/in}^2)(15.5 \text{ in})}{.25 \text{ in}} = 911 \text{ psi}$$

• Local Long Stress (@ Wg)

$$\sigma_L = \frac{(14.7 \text{ #/in}^2)(15.5 \text{ in})}{2 (.25 \text{ in})} = 456 \text{ psi}$$

Max Primary Membrane Stress

$$\sigma_M = 6418 \text{ psi} + 911 \text{ psi} + 456 \text{ psi} = 7785 \text{ psi}$$

$$\begin{aligned}7785 \text{ psi} &< 22050 \text{ psi @ } 400^\circ\text{F} \\ &< 25050 \text{ psi @ } 100^\circ\text{F}\end{aligned}$$

Max Primary + Secondary Membrane Stress

$$\sigma_{M+PS} = 15844 \text{ psi} + 911 \text{ psi} + 456 \text{ psi} = 17211 \text{ psi}$$

$$\begin{aligned}17211 \text{ psi} &< 44100 \text{ psi @ } 400^\circ\text{F} \\ &< 50100 \text{ psi @ } 100^\circ\text{F}\end{aligned}$$



44.625"  $\phi$  TUBE w/ 1/4" SHELL

A-1

- Primary Membrane Stress

$$\sigma_M = 5482 \text{ psi} \left( \frac{8467 \text{ lbs}}{4673 \text{ lbs}} \right) = 9933 \text{ psi}$$

- Primary + Secondary Membrane Stress

$$\sigma_{M_{PS}} = 14739 \text{ psi} \left( \frac{8467 \text{ lbs}}{4673 \text{ lbs}} \right) = 26706 \text{ psi}$$

- Local Circ. Stress (@ Lug)

$$\sigma_c = \frac{(14.7 \text{ */in}^2)(22.5625 \text{ in})}{.25 \text{ in}} = 1327 \text{ psi}$$

- Local Long. Stress (@ Lug)

$$\sigma_L = \frac{(14.7 \text{ */in}^2)(22.5625 \text{ in})}{2(.25 \text{ in})} = 663 \text{ psi}$$

Max Primary Membrane Stress

$$\sigma_M = 9933 \text{ psi} + 1327 \text{ psi} + 663 \text{ psi} = 11923 \text{ psi}$$

$$11923 \text{ psi} < 22050 \text{ psi} \\ < 25050 \text{ psi}$$

Max Primary + Secondary Membrane Stress

$$\sigma_{M_{PS}} = 26706 \text{ psi} + 1327 \text{ psi} + 663 \text{ psi} = 28696 \text{ psi}$$

$$28696 \text{ psi} < 44100 \text{ psi} \\ < 50100 \text{ psi}$$



48.25"  $\phi$  TUBE w/ 1/4" SHELL

A-2

- Primary Membrane Stress

$$\bar{\sigma}_M = 6030 \text{ psi} \left( \frac{9813.3 \text{ lbs}}{5053 \text{ lbs}} \right) = 11711 \text{ psi}$$

- Primary + Secondary Membrane Stress

$$\bar{\sigma}_{M+S} = 16274 \text{ psi} \left( \frac{9813.3 \text{ lbs}}{5053 \text{ lbs}} \right) = 31605 \text{ psi}$$

- Local Circ. Stress (@ Lug)

$$\sigma_c = \frac{(14.7 \text{ psi/in}^2)(24.375 \text{ in})}{.25 \text{ in}} = 1433.25 \text{ psi} \approx 1433 \text{ psi}$$

- Local Long. Stress (@ Lug)

$$\sigma_L = \frac{(14.7 \text{ psi/in}^2)(24.375 \text{ in})}{2(.25 \text{ in})} = 716.6 \text{ psi} \approx 717 \text{ psi}$$

### Max Primary Membrane Stress

$$\bar{\sigma}_M = 11711 \text{ psi} + 1433 \text{ psi} + 717 \text{ psi} = 13861 \text{ psi}$$

$$13861 \text{ psi} < 22050 \text{ psi @ } 400^\circ\text{F}$$
$$< 25050 \text{ psi @ } 100^\circ\text{F}$$

### Max Primary + Secondary Membrane Stress

$$\bar{\sigma}_{M+S} = 31605 \text{ psi} + 1433 \text{ psi} + 717 \text{ psi} = 33755 \text{ psi}$$

$$33755 \text{ psi} < 44100 \text{ psi @ } 400^\circ\text{F}$$
$$< 50100 \text{ psi @ } 100^\circ\text{F}$$



60.5"  $\phi$  TUBE WITH 1/4" SHELL

A-13

- Primary Membrane Stress

$$\sigma_M = 7903 \text{ psi} \left( \frac{11365 \text{ lbs}}{6400 \text{ lbs}} \right) = 14035 \text{ psi}$$

- Primary + Secondary Membrane Stress

$$\sigma_{M_{P+S}} = 23871 \text{ psi} \left( \frac{11365 \text{ lbs}}{6400 \text{ lbs}} \right) = 42390 \text{ psi}$$

- Local circumferential stress (@ Lug)

$$\sigma_c = \frac{(14.7 \text{ in}^2)(30.50 \text{ in})}{.25 \text{ in}} = 1793.4 \approx 1793 \text{ psi}$$

- Local longitudinal stress (@ Lug)

$$\sigma_L = \frac{(14.7 \text{ in}^2)(30.50 \text{ in})}{2(.25 \text{ in})} = 896.7 \text{ psi} \approx 897 \text{ psi}$$

Max Primary Membrane Stress

$$\sigma_M = 14035 \text{ psi} + 1793 \text{ psi} + 897 \text{ psi} = 16725 \text{ psi}$$

$$16725 \text{ psi} < 22050 \text{ psi @ } 400^\circ\text{F} \\ < 25050 \text{ psi @ } 100^\circ\text{F}$$

Max Primary + Secondary Membrane Stress

$$\sigma_{M_{P+S}} = 42390 \text{ psi} + 1793 \text{ psi} + 897 \text{ psi} = 45080 \text{ psi}$$

$$45080 \text{ psi} > 44100 \text{ psi @ } 400^\circ\text{F} \quad (2\%) \\ < 50100 \text{ psi @ } 100^\circ\text{F}$$



60.5"  $\phi$  TUBE WITH  $\frac{3}{8}$ " SHELL

BE-3 & BE-3A

Primary Membrane Stress

$$\sigma_M = 6062 \text{ psi} \left( \frac{11365 \text{ lbs}}{6400 \text{ lbs}} \right)$$

$$\sigma_M = 10765 \text{ psi}$$

Primary + Secondary Membrane Stress

$$\sigma_{M+PS} = 24261 \text{ psi} \left( \frac{11365 \text{ lbs}}{6400 \text{ lbs}} \right)$$

$$\sigma_{M+PS} = 43082 \text{ psi}$$

$$\sigma_L = \frac{(4.7 \text{ in}^2)(30.4375 \text{ in})}{2(.375 \text{ in})} = 596.6 \text{ psi} \approx 597 \text{ psi}$$

$$\sigma_C = \frac{(4.7 \text{ in}^2)(30.4375 \text{ in})}{.375 \text{ in}} = 1193.15 \text{ psi} \approx 1193 \text{ psi}$$

Max Primary Membrane Stress

$$\sigma_M = 10765 \text{ psi} + 597 \text{ psi} + 1193 \text{ psi} = 12555 \text{ psi}$$

$$12555 \text{ psi} < 22050 \text{ psi @ } 400^\circ\text{F}$$
$$< 25050 \text{ psi @ } 100^\circ\text{F}$$

Max Primary + Secondary Stress

$$\sigma_{M+PS} = 43082 \text{ psi} + 597 + 1193 = 44872 \text{ psi}$$

$$44872 \text{ psi} > 44100 \text{ psi @ } 400^\circ\text{F} \quad (2\%)$$
$$< 50100 \text{ psi @ } 100^\circ\text{F}$$



72.25"  $\phi$  TUBE w/ 1/4" SHELL

BE-1

$$\begin{aligned} \text{I.D.} &= 72.25'' \\ t &= .25'' \end{aligned}$$

$$P = 16025 \text{ lbs.} \quad (\text{Pg A-3})$$

LOCAL CIRCUM. STRESS (@ LUG)

$$\sigma_c = \frac{(14.7 \text{ * / in}^2)(36 \text{ }^3\text{/B in})}{.25 \text{ in}} = \cancel{2138.75} \approx 2140 \text{ psi}$$

Local Long. stress

$$\sigma_l = \frac{(14.7 \text{ * / in}^2)(36 \text{ }^3\text{/B in})}{2(.25 \text{ in})} = 1070 \text{ psi}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



**BELLOWS BE-1 W/NO REPADS**

**ASME Section VIII Division 1, 1995 Edition, A95 Addenda**

Component: Cylinder  
Material specification: SA 240 304L HIGH  
External design pressure:  $P_e = 14.7$  psi @ 400 deg F  
Corrosion allowance: Inner C = 0 Outer = 0 in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
Category B joints - Spot UW-11(b) type 1

Estimated weight: new = 983.9 corr = 983.9 lb  
capacity: new = 1050.201 corr = 1050.201 US ga

OD = 72.25 length  $L_c = 60$  t = 0.25 in (new)

**MAP: (New & at 400 deg F) Appendix 1-1(a)**

$$P = S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s$$
$$= 14700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0$$
$$= 86.71062 \text{ psi}$$

**MAWP: (Corroded & at 400 deg F) Appendix 1-1(a)**

$$P = S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s$$
$$= 14700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0$$
$$= 86.71062 \text{ psi}$$

**External Pressure: (Corroded & at 400 deg F) UG-28**

$$L/D_o = 75.95833/72.25 = 1.0513 \quad D_o/t = 72.25/0.24489 = 295.0304$$

From table G: A = 0.000249  
From table HA-3: B = 3287

$$P_a = 4 \cdot B / (3 \cdot D_o/t)$$
$$= 4 \cdot 3287 / (3 \cdot 72.25/0.24489)$$
$$= 14.855 \text{ psi}$$

**Design thickness for external pressure  $P_a = 14.855$  psi:**

$$= t + \text{Corrosion}$$
$$= 0.24489 + 0$$
$$= 0.24489 \text{ in}$$

**Maximum Allowable External Pressure: (Corroded @ 400 deg F)**

$$L/D_o = 75.95833/72.25 = 1.0513 \quad D_o/t = 72.25/0.25 = 289$$

From table G: A = 0.000258  
From table HA-3: B = 3407

$$P_a = 4 \cdot B / (3 \cdot D_o/t)$$



**BELLOWS BE-1 W/NO REPADS**

=  $4 \cdot 3407 / (3 \cdot 72.25 / 0.25)$   
= 15.7186 psi

### BE-1 Lug (Without Pad)

Lug material specification	= A 240 304
Lug allowable stress	= 18800 psi
Top plate width	wp = 2 in
Base plate width	wb = 4.75 in
Top plate thickness	t = 0.5 in
Base plate thickness	tb = 1.125 in
Lug length circ. direction	L = 6 in
Gusset height	h = 7 in
Gusset thickness	tg = 0.5 in
Number of lugs	= 4
Angular position, first lug	= 0 degrees
Fillet weld size	tw = 0.1875 in
Force bearing width	Fb = 2 in
Distance to load	d = 3.375 in

#### Lug top plate required thickness. Bednar pg 153

$$\begin{aligned}t_a &= 0.75 \cdot (VL \cdot d \cdot L) / (S_a \cdot w_p^2 \cdot h) \\&= 0.75 \cdot (16025 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 7) \\&= 0.4623 \text{ in}\end{aligned}$$

#### Lug gusset required thickness

$$\begin{aligned}S_c &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot t_g))^2) \\&= 18000 / (1 + (1/18000) \cdot (7 / (0.289 \cdot 0.5))^2) \\&= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}t_g &= VL \cdot (3 \cdot d - w_b) / (S_c \cdot w_b^2 \cdot \sin(\alpha)^2) \\&= 16025 \cdot (3 \cdot 3.375 - 4.75) / (15923.95 \cdot 4.75^2 \cdot \sin(68.552)^2) \\&= 0.2767 \text{ in}\end{aligned}$$

#### Lug base plate required thickness

From Escoe table 4-8

$$f_c = VL / (F_b \cdot L) = 1335.417 \text{ psi}$$

$$\begin{aligned}M_x &= C_x \cdot f_c \cdot G_s^2 \\&= 0.0923 \cdot 1335.417 \cdot 5^2 = 3081.474\end{aligned}$$

$$\begin{aligned}M_y &= C_y \cdot f_c \cdot w_b^2 \\&= -.126 \cdot 1335.417 \cdot 4.75^2 = -3796.423\end{aligned}$$

$$\begin{aligned}t_b &= \text{Sqr}(6 \cdot M_{\max} / S_a) \\&= \text{Sqr}(6 \cdot 3796.423 / 18800) \\&= 1.1007 \text{ in}\end{aligned}$$

#### Check lug attachment stresses

Radial load	Pr = 0 lbf
Circumferential moment	Mc = 0 lbf-ft
Circumferential shear	Vc = 0 lbf
Longitudinal moment	ML = 4507 lbf-ft
Longitudinal shear	VL = 16025 lbf

**BE-1 Lug (Without Pad)**

Internal pressure  $P = 0$  psi

**Stresses at the lug edge per WRC bulletin 107 (psi)**

Mean radius  $R_m = 36$  in  
 $R_m/t = 144$

$C_1 = 3$ ,  $C_2 = 4.3125$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -61030 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 44100$  psi

**WARNING! The maximum combined stress is excessive.**

Maximum primary membrane stress = -19543 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 22050$  psi

The maximum primary membrane stress is within allowable limits.

**BE-1 Lug (Without Pad)**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	Dl
3C*	11.760	0.119								
4C*	19.928	0.108								
1C	0.0817	0.095								
2C-1	0.0484	0.095								
3A*	5.5914	0.094								
1A	0.0795	0.098								
3B*	14.567	0.106	-19543	-19543	19543	19543				
1B-1	0.0282	0.098	-41487	41487	41487	-41487				
pressure stress*										
Total circ stress			-61030	21944	61030	-21944				
Primary membrane circ stress*			-19543	-19543	19543	19543				
3C*	12.996	0.108								
4C*	19.113	0.119								
1C-1	0.0720	0.11								
2C	0.0436	0.11								
4A*	10.157	0.094								
2A	0.0375	0.11								
4B*	15.5915	0.106	-9432	-9432	9432	9432				
2B-1	0.0349	0.11	-45885	45885	45885	-45885				
pressure stress*										
Total long stress			-55317	36453	55317	-36453				
Primary membrane long stress*			-9432	-9432	9432	9432				
torsion moment Mt										
Circ shear from Vc										
Long shear from VL							-3716	-3716	3716	3716
Total Shear stress							-3716	-3716	3716	3716
Combined stress			-61030	36453	61030	-36453	7432	7432	7432	7432

**BELLOWS BE-1 W/REPADS**

**ASME Section VIII Division 1, 1995 Edition, A95 Addenda**

Component: Cylinder  
Material specification: SA 240 304L HIGH  
External design pressure:  $P_e = 14.7$  psi @ 400 deg F  
Corrosion allowance: Inner C = 0 Outer = 0 in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
Category B joints - Spot UW-11(b) type 1

Estimated weight: new = 983.9 corr = 983.9 lb  
Capacity: new = 1050.201 corr = 1050.201 US ga

OD = 72.25 length  $L_c = 60$  t = 0.25 in (new)

**MAP: (New & at 400 deg F) Appendix 1-1(a)**

$$P = S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s$$
$$= 14700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0$$
$$= 86.71062 \text{ psi}$$

**MAWP: (Corroded & at 400 deg F) Appendix 1-1(a)**

$$P = S \cdot E \cdot t / (R_o - 0.4 \cdot t) - P_s$$
$$= 14700 \cdot 0.85 \cdot 0.25 / (36.125 - 0.4 \cdot 0.25) - 0$$
$$= 86.71062 \text{ psi}$$

**External Pressure: (Corroded & at 400 deg F) UG-28**

$$L/Do = 75.95833/72.25 = 1.0513 \quad Do/t = 72.25/0.24489 = 295.0304$$

From table G: A = 0.000249  
From table HA-3: B = 3287

$$P_a = 4 \cdot B / (3 \cdot Do/t)$$
$$= 4 \cdot 3287 / (3 \cdot 72.25 / 0.24489)$$
$$= 14.855 \text{ psi}$$

**Design thickness for external pressure  $P_a = 14.855$  psi:**

$$= t + \text{Corrosion}$$
$$= 0.24489 + 0$$
$$= 0.24489 \text{ in}$$

**Maximum Allowable External Pressure: (Corroded @ 400 deg F)**

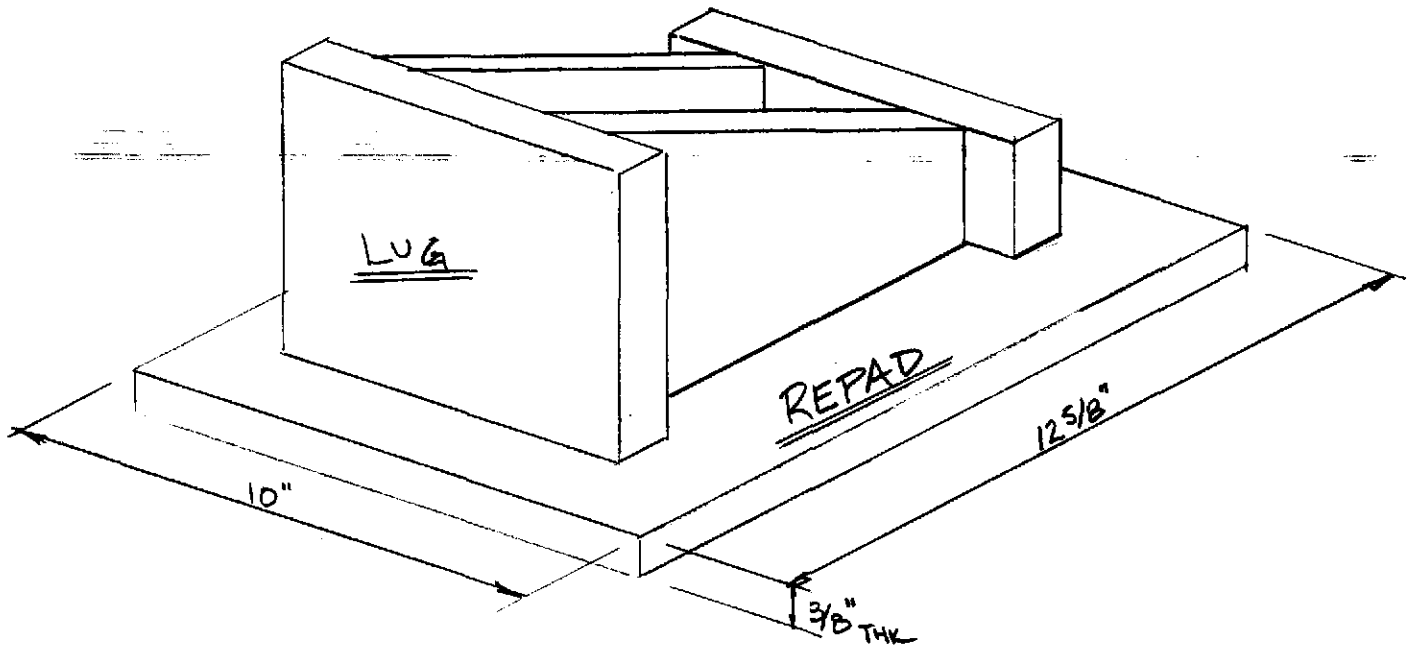
$$L/Do = 75.95833/72.25 = 1.0513 \quad Do/t = 72.25/0.25 = 289$$

From table G: A = 0.000258  
From table HA-3: B = 3407

$$P_a = 4 \cdot B / (3 \cdot Do/t)$$

**BELLOWS BE-1 W/REPADS**

=  $4 \cdot 3407 / (3 \cdot 72.25 / 0.25)$   
= 15.7186 psi



REPAD  $\frac{3}{8}$ " THK X  $12\frac{5}{8}$ " LONG X 10" WIDE

NOTE:

PAD TO SHELL WELD IS  $\frac{3}{16}$ " fillet (all-around)  
LUG TO REPAD WELD IS  $\frac{1}{4}$ " fillet (all-around)

### BE-1 Lug (With Pad)

Lug material specification	= A 240 304
Lug allowable stress	= 18800 psi
Top plate width	wp = 2 in
Base plate width	wb = 4.75 in
Top plate thickness	t = 0.5 in
Base plate thickness	tb = 1.125 in *
Lug length circ. direction	L = 6 in
Gusset height	h = 7 in
Gusset thickness	tg = 0.5 in
Number of lugs	= 4
Angular position, first lug	= 0 degrees
Fillet weld size	tw = 0.1875 in
Force bearing width	Fb = 2 in
Distance to load	d = 3.375 in

ACTUAL THKS 1/2" but WASHER PL IS 1" THK  
∴ TOTAL THKS = 1 1/2" > 1.125"  
CONSERVATIVE

### Lug top plate required thickness, Bednar pg 153

$$\begin{aligned}t_a &= 0.75 \cdot (V_L \cdot d \cdot L) / (S_a \cdot w_p^2 \cdot h) \\&= 0.75 \cdot (16025 \cdot 3.375 \cdot 6) / (18800 \cdot 2^2 \cdot 7) \\&= 0.4623 \text{ in}\end{aligned}$$

### Lug gusset required thickness

$$\begin{aligned}S_c &= 18000 / (1 + (1/18000) \cdot (h / (0.289 \cdot t_g))^2) \\&= 18000 / (1 + (1/18000) \cdot (7 / (0.289 \cdot 0.5))^2) \\&= 15923.95 \text{ psi}\end{aligned}$$

$$\begin{aligned}t_g &= V_L \cdot (3 \cdot d - w_b) / (S_c \cdot w_b^2 \cdot \sin(\alpha)^2) \\&= 16025 \cdot (3 \cdot 3.375 - 4.75) / (15923.95 \cdot 4.75^2 \cdot \sin(68.552)^2) \\&= 0.2767 \text{ in}\end{aligned}$$

### Lug base plate required thickness

From Escoe table 4-8

$$f_c = V_L / (F_b \cdot L) = 1335.417 \text{ psi}$$

$$\begin{aligned}M_x &= C_x \cdot f_c \cdot G_s^2 \\&= 0.0923 \cdot 1335.417 \cdot 5^2 = 3081.474\end{aligned}$$

$$\begin{aligned}M_y &= C_y \cdot f_c \cdot w_b^2 \\&= -.126 \cdot 1335.417 \cdot 4.75^2 = -3796.423\end{aligned}$$

$$\begin{aligned}t_b &= \sqrt{6 \cdot M_{\max} / S_a} \\&= \sqrt{6 \cdot 3796.423 / 18800} \\&= 1.1007 \text{ in}\end{aligned}$$

### Check lug attachment stresses

Radial load	Pr = 0 lbf
Circumferential moment	Mc = 0 lbf-ft
Circumferential shear	Vc = 0 lbf
Longitudinal moment	ML = 4507 lbf-ft
Longitudinal shear	VL = 16025 lbf

**BE-1 Lug (With Pad)**

Internal pressure  $P = 0$  psi

**Stresses at the lug edge per WRC bulletin 107 ( psi)**

Mean radius  $R_m = 36$  in

$R_m/t = 57.6$

$C_1 = 3$ ,  $C_2 = 4.3125$  in

Stress concentration factor  $K_n$  (tension) = 1

Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -12922 psi

Allowable combined stress =  $\pm 3 \cdot S = \pm 44100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -3546 psi

Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 22050$  psi

The maximum primary membrane stress is within allowable limits.



**BE-1 Lug (With Pad)**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	Dl
3C*	7.3557	0.119								
4C*	9.5108	0.108								
1C	0.1138	0.095								
2C-1	0.0794	0.095								
3A*	1.9292	0.094								
1A	0.0925	0.102								
3B*	6.5090	0.106	-3546	-3546	3546	3546				
1B-1	0.0410	0.102	-9272	9272	9272	-9272				
pressure stress*										
Total circ stress			-12818	5726	12818	-5726				
Primary membrane circ stress*			-3546	-3546	3546	3546				
3C*	7.8410	0.108								
4C*	9.2595	0.119								
1C-1	0.1038	0.11								
2C	0.0684	0.11								
4A*	2.8344	0.094								
2A	0.0468	0.116								
4B*	1.9932	0.106	-1341	-1341	1341	1341				
2B-1	0.0575	0.115	-11581	11581	11581	-11581				
pressure stress*										
Total long stress			-12922	10240	12922	-10240				
Primary membrane long stress*			-1341	-1341	1341	1341				
torsion moment Mt										
Circ shear from Vc							-1486	-1486	1486	1486
Long shear from VL										
Total Shear stress							-1486	-1486	1486	1486
Combined stress			-12922	10240	12922	-10240	2972	2972	2972	2972

**BE-1 Lug (With Pad)**

**Stresses at the pad edge per WRC bulletin 107 ( psi)**

Mean radius  $R_m = 36$  in  
 $R_m/t = 144$

$C_1 = 5$ ,  $C_2 = 6.3125$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -25126 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 44100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -9820 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 22050$  psi

The maximum primary membrane stress is within allowable limits.

**BE-1 Lug (With Pad)**

From Fig.	Value read	beta	Au	Al	Bu	Bl	Cu	Cl	Du	Dl
3C*	6.8370	0.177								
4C*	16.042	0.165								
1C	0.0600	0.151								
2C-1	0.0238	0.151								
3A*	5.2855	0.15								
1A	0.0626	0.157								
3B*	10.997	0.162	-9820	-9820	9820	9820				
1B-1	0.0162	0.153	-15306	15306	15306	-15306				
pressure stress*										
Total circ stress			-25126	5486	25126	-5486				
Primary membrane circ stress*			-9820	-9820	9820	9820				
3C*	7.5546	0.165								
4C*	15.323	0.177								
1C-1	0.0470	0.167								
2C	0.0353	0.167								
4A*	12.228	0.15								
2A	0.0267	0.172								
4B*	4.7200	0.162	-4972	-4972	4972	4972				
2B-1	0.0194	0.168	-16694	16694	16694	-16694				
pressure stress*										
Total long stress			-21666	11722	21666	-11722				
Primary membrane long stress*			-4972	-4972	4972	4972				
torsion moment Mt										
Circ shear from Vc										
Long shear from VL							-2539	-2539	2539	2539
Total Shear stress							-2539	-2539	2539	2539
Combined stress			-25126	11722	25126	-11722	5078	5078	5078	5078

72.25"  $\phi$  TUBE W/ 3/8" SHELL

BE-5

PRIMARY MEMBRANE STRESS

$$\sigma_M = 9588 \text{ psi}$$

PRIMARY + SECONDARY MEMBRANE STRESS

$$\sigma_{M+S} = 31316 \text{ psi}$$

Local circ. stress (@ Lug)

$$\sigma_c = \frac{(14.7 \text{ in}^2)(36.5 \text{ in})}{.375 \text{ in}} = 1430.8 \text{ psi} \approx 1431 \text{ psi}$$

Local long. stress (@ Lug)

$$\sigma_L = \frac{(14.7 \text{ in}^2)(36.5 \text{ in})}{2(.375 \text{ in})} = 715 \text{ psi}$$

Max Primary Membrane Stress

$$\sigma_M = 9588 \text{ psi} + 1431 \text{ psi} + 715 \text{ psi} = 11734 \text{ psi}$$

$$\sigma_M = 11734 \text{ psi} < 22050 \text{ psi @ } 400^\circ\text{F}$$
$$< 25050 \text{ psi @ } 100^\circ\text{F}$$

Max Primary + Secondary Membrane Stress

$$\sigma_{M+S} = 31316 \text{ psi} + 1431 \text{ psi} + 715 \text{ psi}$$
$$= 33462 \text{ psi} < 44100 \text{ psi @ } 400^\circ\text{F}$$
$$< 50100 \text{ psi @ } 100^\circ\text{F}$$

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



Pressure Summary

Pressure summary for pressure chamber 1

Identifier	P	T	MAWP	MAP	Pe	UG-99	UCS-66		Corrosion
	design (psi)	design (deg F)	(psi)	(psi)	external (psi)	Ratio	MDMT (deg F)	Exemption or Stress Reduction	Allowance (in)
Bellows Spool BE-5	0.0	400.0	128.9	146.4	33.5	1.136		Not applicable	0.000

Vessel MAWP hot & corroded is 128.9 psi @ 400 degrees F.

Vessel MAP new & cold is 146.44 psi @ 0 degrees F.

Vessel allowable external pressure is 33.54 psi @ 400 degrees F.

Hydrotest pressure calculation based on MAWP

$$= 1.5 * (\text{MAWP} + \text{Operating Liquid Head}) * 1.136 = 219.7 \text{ psi}$$

Vessel hydrotest pressure is 219.7 psi.

Note: vessel MAP rating not valid unless hydrotest pressure based on MAP.

Weight Summary

Component	Weight (lbs) Contributed by Vessel Elements											
	Metal	Metal	Trays	Packed	Insul	Lining	Piping	Ladder	Rings	Oper	Test	Nozzle
	New	Corr	& sup	Beds				& plat	& Misc	Liquid	Liquid	& flg
Bellows spool b	1563	1563	0	0	0	0	0	0	0	0	9326	0
	1563	1563	0	0	0	0	0	0	0	0	9326	0

Vessel operating weight, corroded: 1,563 lbs  
 Vessel empty weight, corroded: 1,563 lbs  
 Vessel empty weight, new: 1,563 lbs  
 Vessel test weight, new: 10,889 lbs

Vessel center of gravity location (from right weld seam)

Vessel lift weight, new: 1,563 lbs  
 Center of gravity to seam: 31.5 in

Thickness Summary

Component Identifier	ID (in)	Length (in)	Nom t (in)	Req t (in)	Joint E	Governing Load Status	Deflect (in)
Bellows spool be-5	72.25	63.00	0.3750	0.2503	0.85	external	

Nom t - vessel wall thickness

Req t - required vessel wall thickness due to governing loading

E - longitudinal seam joint efficiency

Load:

internal - circ stress due to internal pressure governs

external - external pressure governs

wind - combined long stress due to STATUS + wind governs

seismic - combined long stress due to STATUS + seismic governs

Bellows Spool BE-5ASME Section VIII Division 1, 1995 Edition, A95 Addenda

Component: Cylinder  
 Material specification: SA 240 304L HIGH  
 External design pressure:  $P_e = 14.7$  psi @ 400 deg F  
 Corrosion allowance: Inner C = 0 Outer = 0 in

\* PWHT is performed

Radiography: Category A joints - Spot UW-11(b) type 1  
 Category B joints - Spot UW-11(b) type 1

Estimated weight: new = 1563.2 corr = 1563.2 lb  
 capacity: new = 1118.134 corr = 1118.134 US ga

ID = 72.25 length  $L_c = 63$  t = 0.375 in (new)

MAP: (New & at 0 deg F) UG-27(c)(1)

$$P = S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s$$

$$= 16700 \cdot 0.85 \cdot 0.375 / (36.125 + 0.6 \cdot 0.375) - 0$$

$$= 146.4409 \text{ psi}$$

MAWP: (Corroded & at 400 deg F) UG-27(c)(1)

$$P = S \cdot E \cdot t / (R + 0.6 \cdot t) - P_s$$

$$= 14700 \cdot 0.85 \cdot 0.375 / (36.125 + 0.6 \cdot 0.375) - 0$$

$$= 128.903 \text{ psi}$$

External Pressure: (Corroded & at 400 deg F) UG-28

$$L/Do = 79.04167/73 = 1.0828 \quad Do/t = 73/0.25037 = 291.5685$$

From table G: A = 0.000247  
 From table HA-3: B = 3260.4

$$P_a = 4 \cdot B / (3 \cdot Do/t)$$

$$= 4 \cdot 3260.4 / (3 \cdot 73/0.25037)$$

$$= 14.9097 \text{ psi}$$

Design thickness for external pressure  $P_a = 14.9097$  psi:

$$= t + \text{Corrosion}$$

$$= 0.25037 + 0$$

$$= 0.25037 \text{ in}$$

Maximum Allowable External Pressure: (Corroded @ 400 deg F)

$$L/Do = 79.04167/73 = 1.0828 \quad Do/t = 73/0.375 = 194.6667$$

From table G: A = 0.000457  
 From table HA-3: B = 4896.7



Bellows Spool BE-5

$$\begin{aligned} Pa &= 4*B/(3*Do/t) \\ &= 4*4896.7/(3*73/0.375) \\ &= 33.539 \text{ psi} \end{aligned}$$

8x6 LUG - WITH NO PAD

Lug material specification	= A 240 304
Lug allowable stress	= 18800 psi
Top plate width	wp = 2 in
Base plate width	wb = 4.75 in
Top plate thickness	t = 0.5 in
Base plate thickness	tb = 1.125 in
Lug length circ. direction	L = 6 in
Gusset height	h = 7 in
Gusset thickness	tg = 0.5 in
Number of lugs	= 4
Angular position, first lug	= 0 degrees
Fillet weld size	tw = 0.25 in
Force bearing width	Fb = 2 in
Distance to load	d = 3.375 in

Lug top plate required thickness, Bednar pg 153

$$\begin{aligned} ta &= 0.75*(VL*d*L)/(Sa*wp^2*h) \\ &= 0.75*(16025*3.375*6)/(18800*2^2*7) \\ &= 0.4623 \text{ in} \end{aligned}$$

Lug gusset required thickness

$$\begin{aligned} Sc &= 18000/(1 + (1/18000)*(h/(0.289*tg))^2) \\ &= 18000/(1 + (1/18000)*(7/(0.289*0.5))^2) \\ &= 15923.95 \text{ psi} \end{aligned}$$

$$\begin{aligned} tg &= VL*(3*d - wb)/(Sc*wb^2*SIN(Alpha)^2) \\ &= 16025*(3*3.375 - 4.75)/(15923.95*4.75^2*SIN(68.552)^2) \\ &= 0.2767 \text{ in} \end{aligned}$$

Lug base plate required thickness

From Escoe table 4-8

$$fc = VL/(Fb*L) = 1335.417 \text{ psi}$$

$$\begin{aligned} Mx &= Cx*fc*Gs^2 \\ &= 0.0923*1335.417*5^2 = 3081.474 \end{aligned}$$

$$\begin{aligned} My &= Cy*fc*wb^2 \\ &= -.126*1335.417*4.75^2 = -3796.423 \end{aligned}$$

$$\begin{aligned} tb &= \text{Sqr}(6*Mmax / Sa) \\ &= \text{Sqr}(6*3796.423 / 18800) \\ &= 1.1007 \text{ in} \end{aligned}$$

Check lug attachment stresses

Radial load	Pr = 0 lbf
Circumferential moment	Mc = 0 lbf-ft
Circumferential shear	Vc = 0 lbf

8x6 LUG - WITH NO PAD

Longitudinal moment      ML = 4507 lbf-ft  
Longitudinal shear      VL = 16025 lbf  
Internal pressure        P = 0 psi

Stresses at the lug edge per WRC bulletin 107 ( psi)

Mean radius  $R_m = 36.3125$  in  
 $R_m/t = 96.83334$

$C_1 = 3$ ,  $C_2 = 4.3125$  in

Stress concentration factor  $K_n$  (tension) = 1  
Stress concentration factor  $K_b$  (bending) = 1

Local circ. pressure stress =  $P \cdot R_m/t = 0$  psi

Local long. pressure stress =  $P \cdot R_m/2t = 0$  psi

Maximum combined stress = -31316 psi  
Allowable combined stress =  $\pm 3 \cdot S = \pm 44100$  psi

The maximum combined stress is within allowable limits.

Maximum primary membrane stress = -9588 psi  
Allowable primary membrane stress =  $\pm 1.5 \cdot S = \pm 22050$  psi

The maximum primary membrane stress is within allowable limits.

8x6 LUG - WITH NO PAD

From Fig.	Value read	beta	Au	A1	Bu	B1	Cu	C1	Du	D1
3C*	10.196	0.118								
4C*	14.666	0.107								
1C	0.0937	0.094								
2C-1	0.0598	0.094								
3A*	3.6058	0.093								
1A	0.0843	0.098								
3B*	10.778	0.105	-9588	-9588	9588	9588				
1B-1	0.0339	0.099	-21728	21728	21728	-21728				
pressure stress*										
Total circ stress			-31316	12140	31316	-12140				
Primary membrane circ stress*			-9588	-9588	9588	9588				
3C*	11.128	0.107								
4C*	14.149	0.118								
1C-1	0.0812	0.109								
2C	0.0513	0.109								
4A*	5.8491	0.093								
2A	0.0409	0.112								
4B*	3.7668	0.105	-4010	-4010	4010	4010				
2B-1	0.0427	0.112	-24320	24320	24320	-24320				
pressure stress*										
Total long stress			-28330	20310	28330	-20310				
Primary membrane long stress*			-4010	-4010	4010	4010				
torsion moment Mt										
Circ shear from Vc										
Long shear from VL							-2477	-2477	2477	2477
Total Shear stress							-2477	-2477	2477	2477
Combined stress			-31316	20310	31316	-20310	4954	4954	4954	4954

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE B-1 OF 3
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug Design"		

## APPENDIX - B

### Lug Detail For Test Condition

Revision 0 of Doc No. V049-1-084 provided the design for the LIGO Expansion Joint Tie Rod "Lugs". The original design used 6400. lbs per rod for the "Lugs" on spool pieces BE-3 and BE-3A. The design loads for all other vacuum tubes with expansion joints used an axial spring rate of 7500. #/in.

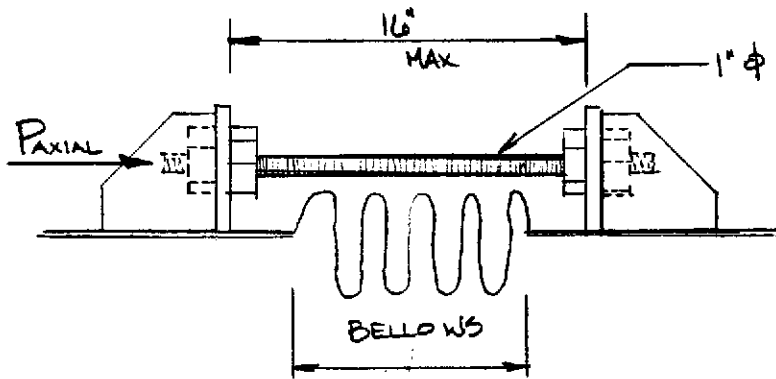
All vacuum tubes are to undergo vacuum testing to check against leakage. Although the design loads are valid for operating conditions, the vacuum test will produce compressive forces at the expansion joint rods which may produce minor bending. Revision 1 uses these compressive forces to evaluate the tie rods.

The evaluation indicated a 15% overstress in the tie rods due to the applied compressive load. Revision 1, Appendix 'B' provided a tie rod/lug detail to be used during vacuum/pressure testing of the vacuum tubes.. Though a margin exists between local bending and member yielding, tie rods were to be sleeved during testing conditions to ensure against potential bending.

Revision 2, Appendix 'B' uses the maximum axial forces indicated in appendix 'A'. The evaluation denotes that for tube sizes of 48-1/2"Ø and smaller, the 1"Ø (A-36) rods were acceptable. However, for 60-1/2"Ø and 72-1/4"Ø tubes, 1-1/4"Ø (A-36) rods are required.

# COMPRESSION IN LUG BOLTS

(TEST CONDITION)



1"  $\phi$  A-36 THREADED ROD  
DOUBLE NUTS @ ENDS.

ROD MAT'L

A-36

$F_y = 36000 \text{ psi}$

ASSUME: DOUBLE NUTS ACT AS A RIGID ANCHOR AT EACH END.

$$KL/r = .5 (16 \text{ in}) / r$$

$$1" \phi \text{ rod} \Rightarrow \text{root dia.} = 0.865 \text{ in} \quad (\text{AISC pg 4-147})$$

$$r = 0.865 / 4 = 0.21625$$

$$KL/r = 0.5 (16 \text{ in}) / 0.21625 = 36.994 \approx 37$$

$$F_A = 19420 \text{ psi}$$

(AISC pg 3-16)

For Tubes up to 48 1/4" I.D.  $P_{\text{MAX}} = 9813 \text{ lbs}$

(REF. Pg A-3)

$$f_A = \frac{P}{A} = \frac{9813 \text{ lbs}}{\text{AREA ROD}}$$

$$A = \text{MIN ROOT AREA (pg. 4-147)} \\ = 0.551 \text{ in}^2$$

$$= \frac{12300 \text{ lbs}}{0.551 \text{ in}}$$

$$f_A = 17800. \text{ psi}$$

$f_A < F_A \therefore \text{O.K. for } 48 \frac{1}{4} \phi \text{ (I.D.)}$   
 $\frac{1}{2} \text{ smaller tube sizes.}$



FOR 60.5"  $\phi$   $\approx$  72.25"  $\phi$  TUBES

$$P_{MAX} = 16.025K \quad (\text{REF. Pg A-3})$$

$$f_a = \frac{16025 \text{ lbs}}{.551 \text{ in}^2} \approx 29000 \text{ #/in}^2$$

$$f_a > F_a$$

$$29000 \text{ psi} > 19420 \text{ psi} \quad \therefore \text{N.G.}$$

TRY 1/4"  $\phi$  THREADED ROD (A-36)

$$A_{min} = .890 \text{ in}^2$$

$$f_a = \frac{16025 \text{ lbs}}{.890 \text{ in}^2} \approx 18000 \text{ psi}$$

$$D_{min} = 1.095 \text{ in}$$

$$I = \frac{\pi R^4}{4} = \frac{\pi (1.095 \text{ in}/2)^4}{4}$$
$$= .07057 \text{ in}^4$$

$$r = \left( \frac{I}{A} \right)^{1/2} = \left( \frac{.07057 \text{ in}^4}{.890 \text{ in}^2} \right)^{1/2} = .2816 \text{ in}$$

$$\frac{KL}{r} = \frac{.5(16 \text{ in})}{.2816 \text{ in}} = 28.4$$

$$F_a = 20 \text{ ksi} > f_a \quad \therefore \text{O.K.}$$



PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-084
		Rev. No. 2
		PAGE C-1 OF 3
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Expansion Joint Tie Rod "Lug Design"		

## APPENDIX - C

### Reinforcing Washer Plate as an Option to Welded Pad

Revision 0 of Doc No. V049-1-084 provided the design for the LIGO Expansion Joint Tie Rod "Lugs". The original design required a welded 4" x 3 3/4" x 3/8" thick reinforcing pad. To minimize welding and ensure design integrity the option of using a thicker washer was evaluated.

The evaluation indicated that a washer plate 3" x 5" x 1" thick could be used in lieu of the welded pad. Revision 1, Appendix 'C' provides a washer design and detail which may be used for the expansion joint tie-rod "Lugs".





WASHER PLATE (BEARING PLATE) FOR LOG

MTL: A588,  $F_y = 50 \text{ KSI MIN}$

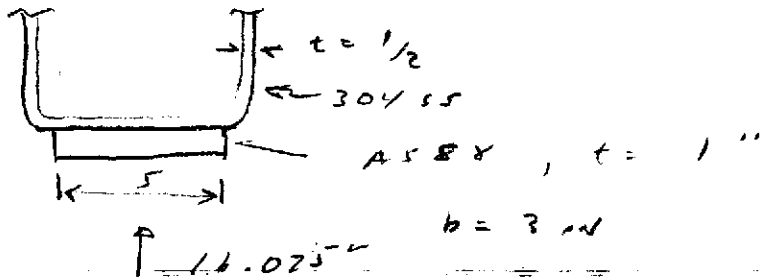
$$t = .5$$

Risk DWG V049-4-124

$$L = 5 \text{ IN}$$

THE MAX FORCE DURING BEARING CHECK IS

$$P = 16.025 \text{ K} \quad (P. A-2)$$



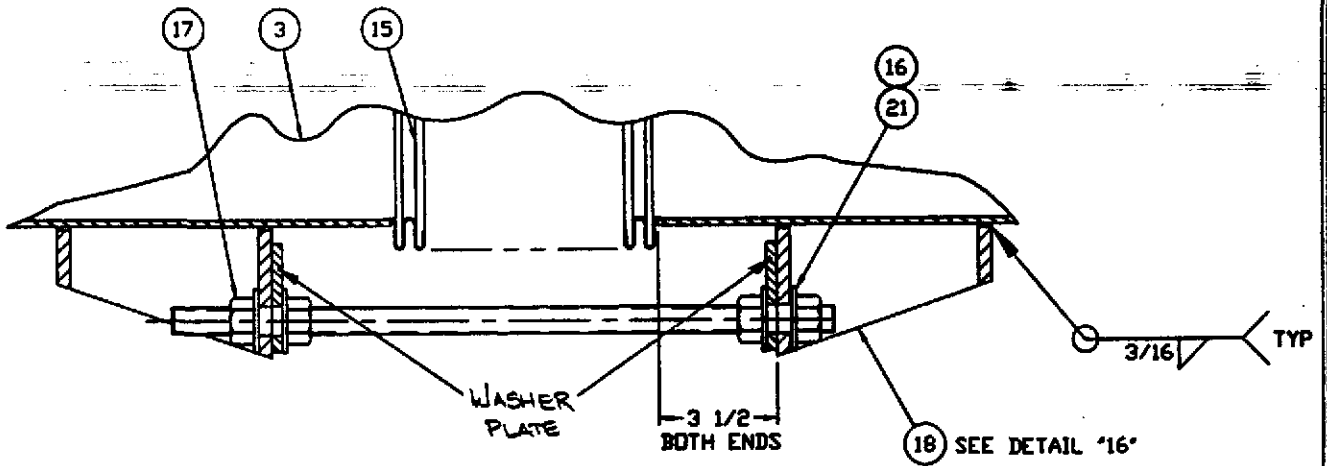
NEGLECT BENDING RESISTANCE OF 304 SS TUBE, ASSUME A588 PLATE TAKES ALL BENDING FOR LINE CHECK

$$M = \frac{16.025 (5)}{4} = 20.0 \text{ IN-K}$$

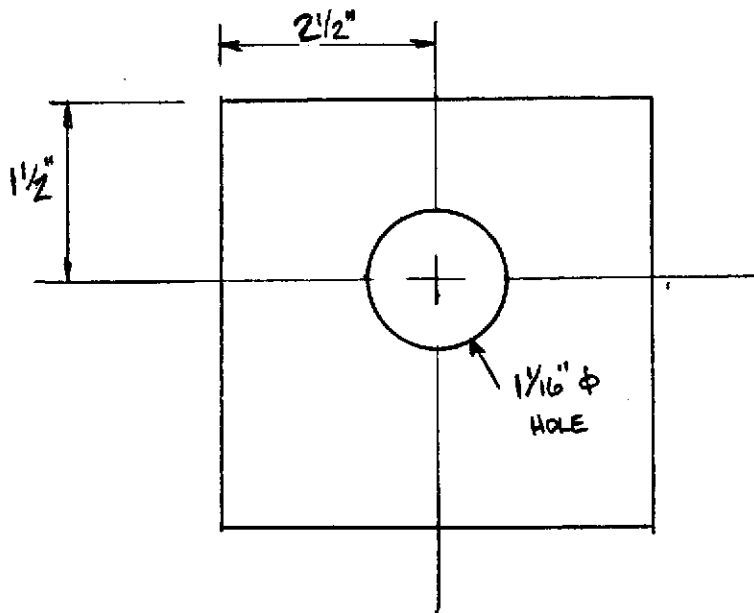
$$f_b = \frac{M}{bt^2} = \frac{6 (20.0)}{3 (1)^2} = 40 \text{ KSI}$$

$< F_y$  OK FOR TEST CONDITION, NEGLECT SHEAR ACTION FOR RECTANGULAR SECTION

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



TYPICAL  
EXPANSION JOINT & TIE-ROD ASSY.  
QTY: 3



WASHER  
PL 3" x 5" x 1" THK

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-108 PAGE 1 OF 34
REV.	DEO #	DATE	BY:	CHECK	TITLE:  <b>Stiffener Rings at Axial Restraints of Tubular Components</b>	
0	0293	9/30/96	RPC	WDB		
					BY: R. D. Ciatto	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<b>PURPOSE:</b> Determine size and thickness of stiffener rings at axial restraints of tubular components including mode cleaner tubes (30.5 in), adapters B-6 and B-7 (48.25 in), beam tube manifolds (72.25 in), and outer shells of 80k pumps (80 in).						
<b>METHOD:</b> Local finite element models of shells at the stiffener rings were generated at axial restraints. The shell models extended at least a long shell distance from the stiffener ring. Axial forces resulting from closed valves or unbalanced forces due to different size bellows were applied to the ring at the junction of the axial restraint diagonal member.						
<b>ASSUMPTIONS:</b> The axial restraint at the 80k pump is assumed to be enveloped by the beam tube manifold which is almost the same diameter (72.25 in vs. 80 in) but which has a significantly higher axial force (38.13 k vs. 27.57 k).						
<b>INPUTS:</b> LIGO project drawings of spools and adapters. Calc. No. V049-1-066, Structural Design Criteria Calc. No. V049-1-083 for axial force on 80k pump (27.57 k). Calc. No. V049-1-095 for axial force on 48.25 in tube (32.17 k). Calc. No. V049-1-089 for axial force on beam tube manifold (38.13 k).						
<b>REFERENCES:</b> ASME Boiler & Pressure Vessel Code, Sect. VIII, Div. 2, Pressure Vessels IMAGES-3D, R. L. Cloud & Assoc.						
<b>CALCULATIONS:</b> (SEE ATTACHED)						
<b>CONCLUSIONS:</b> Stiffener rings at axial restraints must be thicker than those at other locations in order to transfer the large axial loads between the shell and the support. The thicker rings, which are 3x3x3/8 and 4x3x1/2 angles, result in ring stress and shell stresses that meet Section VIII, Div. 2.						
<b>NOTES:</b> IMAGES computer files are: MDCLEAN.*, BMTUBEMN.*, ADAPB6.*, & 80KRING.*						

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-108
		Rev. No. 0
		Page 2 of 34
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Stiffener Rings at Axial Restraints of Tubular Components		

**TABLE OF CONTENTS**

Summary of Results	3
Mode Cleaner Tubes	4
Beam Tube Manifolds	13
Adapters B6 & B7	24
Ring Analysis of 80k Stiffener for Reservoir Supp. Load 29	

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-108
		Rev. No. 0
		Page 3 of 34
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: Stiffener Rings at Axial Restraints of Tubular Components		

### SUMMARY OF RESULTS

The required angle stiffeners at the axial restraints are as follows:

Mode cleaner tubes:	L3x3x3/8
Beam tube manifold:	L4x3x1/2
Adapters B6 & B7:	L3x3x3/8
80k pump:	L4x3x1/2

304ss will be used for all stiffeners which will be rolled the "hard" way. For the 4x3 angles, the 4 in dimension will be in the radial direction.

The finite element models consist of plate elements. Surface stresses in the ring stiffeners are categorized as primary bending stresses and the stress intensities are compared to 1.5 S<sub>m</sub> in accordance with Section VIII, Div. 2 of the ASME code.

The analysis of the beam tube manifold envelopes the 80k pump shell which has a slightly larger diameter (80 in compared to 72.25 in) but which also has a significantly smaller axial load (27.57 k compared to 38.13k). Stiffeners for the 80k pumps also support the reservoir which is hung internally by 2 spring hangers. An analysis of the beam tube manifold was performed to simulate the spring hanger load in addition to the axial restraint load to which the 80k pump stiffener is subjected. It was found that the stress in the stiffener is low for the hanger load.

Also, an independent analysis of the stiffener at the 80k pump is included in this calculation for a 4x3x1/4 in thick angle that supports the internal reservoir. In this analysis the ring is subjected to the spring hanger loads; the axial restraint force was not included since this model represents the ring that is not located at the axial restraint. Beam elements were used to represent the 4x3x1/4 in angle. The results showed that stresses are acceptable for the vertical hanger loads but it also showed that 2x2x1/4 stiffeners are not acceptable for supporting the reservoir.

MODE CLEANER TUBE

FILES: MD CLEAN.\*

$$ID = 30.5$$

$$t = .25$$

$$r = \frac{ID}{2} + \frac{t}{2} = 15.375 \text{ M.A. RADIUS}$$

LONG. SHELL DISTANCE

$$L = 2.5 \sqrt{rt}$$

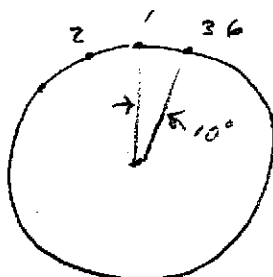
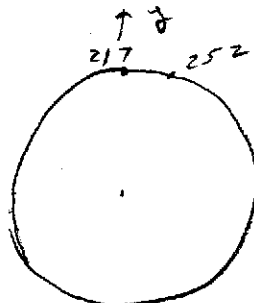
$$= 2.5 \sqrt{15.375 (.25)} = 4.90 \text{ IN}$$

FOR  $10^\circ$  SPLICING, ELEMENT ARC IS

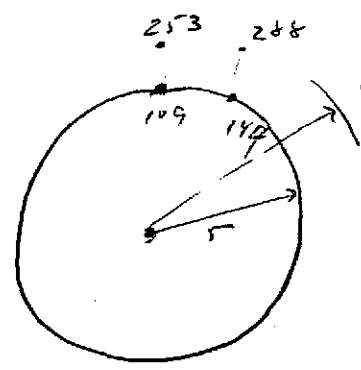
$$S = r\theta$$

$$\theta = 10^\circ = \frac{10\pi}{180} = .175 \text{ RAD}$$

$$S = 15.375 (.175) = 2.69$$

SPACE RINGS AT 3 IN. USE 18 IN LENGTH  $\Rightarrow$  6 SECTIONS (7 RINGS)1ST PATTERN  $\uparrow$  8 $\rightarrow$  7LAST PATTERN  $\uparrow$  8 $\rightarrow$  7

STIFFENER IS ON 4<sup>TH</sup> PATTERN

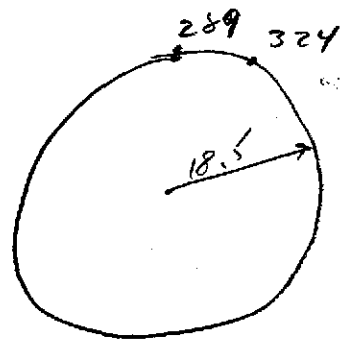


$$r' = 15.375 + 3 + .125$$

$$= 18.5 \text{ IN}$$

STIFFER IS  $L 3 \times 3 \times 1/4$

NODES AT END OF STIFFENER



LOADS IN Z DIR AT FOLLOWING NODES

- 117, 118, 119, 135, 136, 137  
 261, 262, 263, 279, 280, 281

MAY AXIAL REACTION FROM UNBALANCED FORCE IS 33,780<sup>\*</sup> LB. THIS WILL BE APPLIED TO THE 12 NODES LISTED ABOVE

\*REF: CALL 087

$$F_{Z1} = \frac{33780}{12} = 2815$$

PRESS = -14.7 EL 1 TO 216

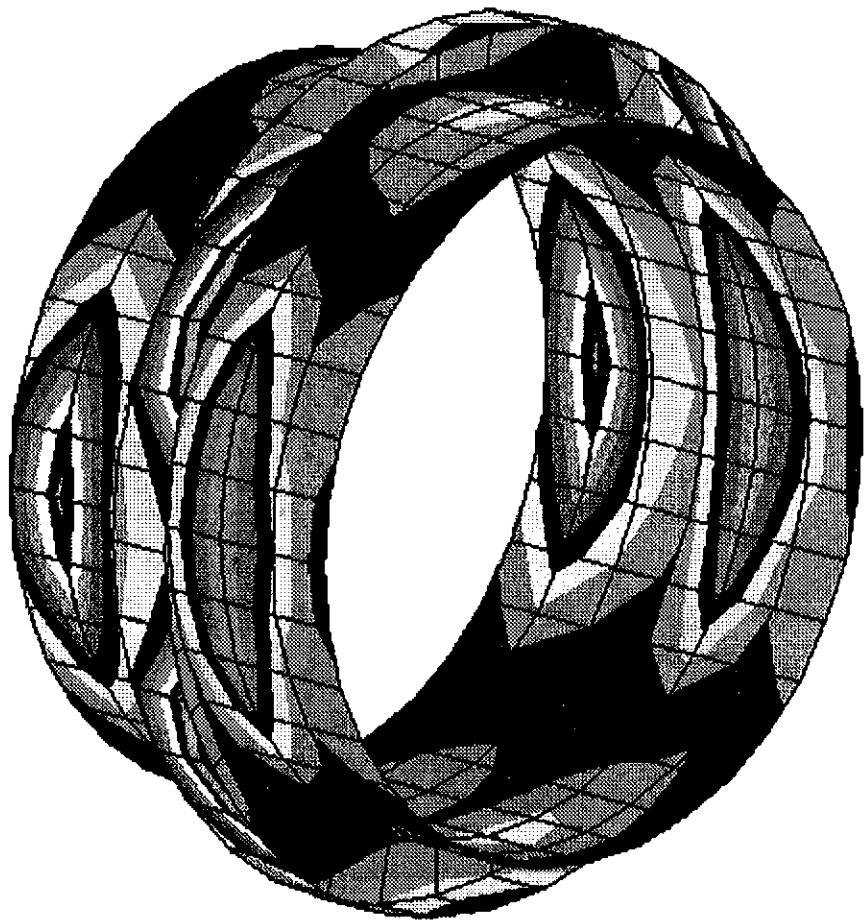
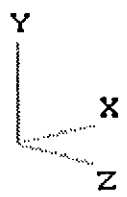
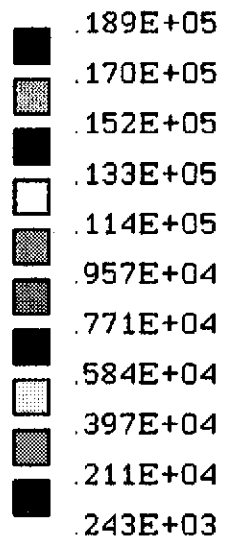
NO BND CAP FORCE DUE TO BELLOWS

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



3 x 3 x 1/2 ROLLER STIFF RIGID  
SHELL THICKNESS = 1/4 IN  
I.D. = 30.5 IN

IMAGES-3D  
Version 3.0



Load Case  
3

MODE CLEARANCE TUBE  
Stress Contour Plot  
Surf: Bottom  
Stress Intensity

9/20/96  
9: 2:54



LOAD CASE 1: EXTERNAL PRESSURE = 14.7 PSI  
 LOAD CASE 2: AXIAL RESTRAINT FORCE  
 LOAD CASE 3: CASE 1 + CASE 2

NOTE: UNBAL FORCE IS CONSERVATIVE. USING DIMENSIONS OF HUSPAN BELLONS, FORCE IS ACTUALLY

$$F_R = 37.6K < 33.8K$$

SEE FOLLOWING SHEET

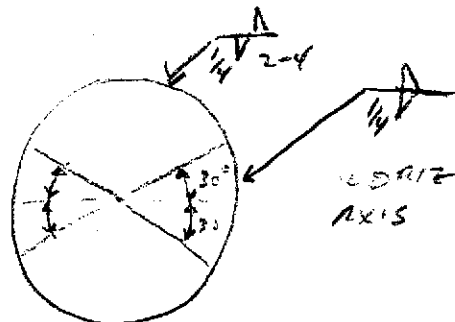
STRESS EVALUATION AT STIFFENER

$$\text{MAX } S_I = 18.9 \text{ KSI FROM PLOT}$$

ALTHOUGH THIS IS A LOCAL STRESS IT WILL BE COMPARED TO 1.5  $S_M$  FOR PRIMARY BENDING PER SECT. VIII, DIV. 2.

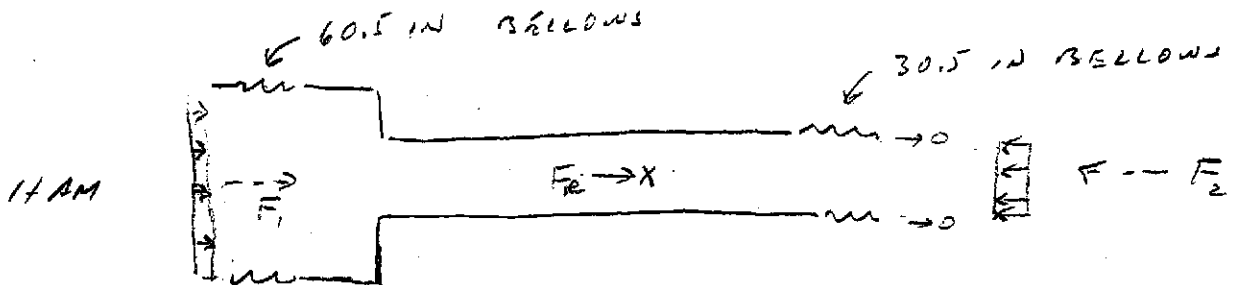
$$\begin{aligned} \Rightarrow P_b &= 18.9 \\ &< 1.5 S_M = 1.5(18.7) \text{ KSI @ } 400^\circ\text{F} \\ &= 28.0 \text{ KSI FOR 304 SS } \checkmark \end{aligned}$$

STIFFENER TO SHELL WELD AT AXIAL REST.



REF CALC OIS P. 13 FOR SHELL WELD

MODE CLEANER TUBE UNBALANCED FORCE



$F_R$  = AXIAL REACTION

$$F_R = F_2 - F_1$$

$$F_1 = 60" \text{ BELLONS} = -45.46 \text{ K}$$

$$F_2 = 30.5" \text{ BELLONS} \\ = P \pi r^2$$

$$r = \frac{D_M}{2}$$

$$D_M = 31.803 \text{ (HYSPAN CALC - 7/9/96)}$$

$$F_2 = \pi \left( \frac{31.803}{2} \right)^2 \times -14.7 \\ = -11.68 \text{ K}$$

$$F_R = -11.68 - (-45.46) \\ = 33.78 \text{ K (34.36 K USED)}$$

BUT  $F_1 = -14.7 \pi \left( \frac{D_M}{2} \right)^2$

$$D_M = 61.928 \text{ (HYSPAN CALC - 7/9/96)}$$

$$F_1 = -14.7 \pi \left( \frac{61.928}{2} \right)^2 = -44277 \text{ LB}$$

$$\Rightarrow F_R = -11.68 - (-44.28) = 32.597 \text{ K}$$

$\therefore$  ACTUAL UNBALANCED FORCE IS 32.6 K

MODE CLEANER TUBE CONT.

TRY REDUCING ANGLE THICKNESS TO 3/16"  
(USE 3x3x3/8 ANGLE SPACER)

PLOT ON THE FOLLOWING SHEET  
SHOWS THAT THE MAX  $SE = 27.2$  KSI

$$P_s = 27.2 \text{ KSI}$$

$$< 1.5 S_M = 28.0 \text{ KSI @ } 400^\circ\text{F}$$

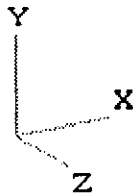
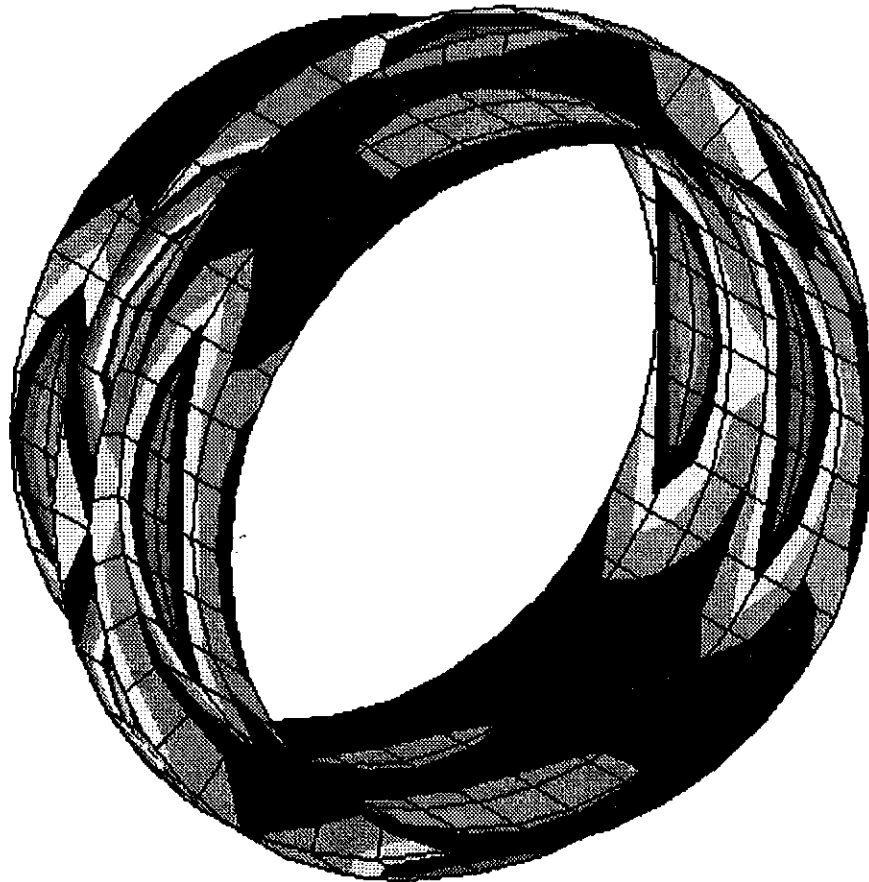
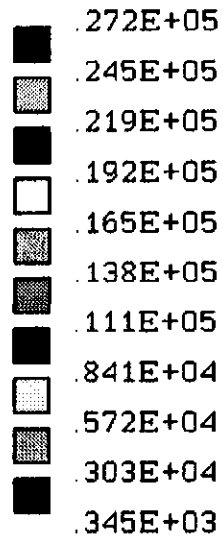
FOR 304 SS

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



3 1/2 x 3/8 ANGLE STIFFENER  
SHELL THICKNESS = 1/4 IN  
I.D. = 30.5 IN

IMAGES-3D  
Version 3.0



MODE CLEANER TUBE

Load Case  
3

Stress Contour Plot  
Surf: Bottom  
Stress Intensity

9/30/96  
9: 3:49

MODE CLEANER TUBE CONT.

TRY ADJUSTED REDUCTION OF THE  
STIFFENER THICKNESS TO  $1/4$ "

THE FOLLOWING PLOT SHOWS THAT  
THE STRESS IN THE STIFFENER IS  
TOO HIGH.  $SE = 49.1$  KSI

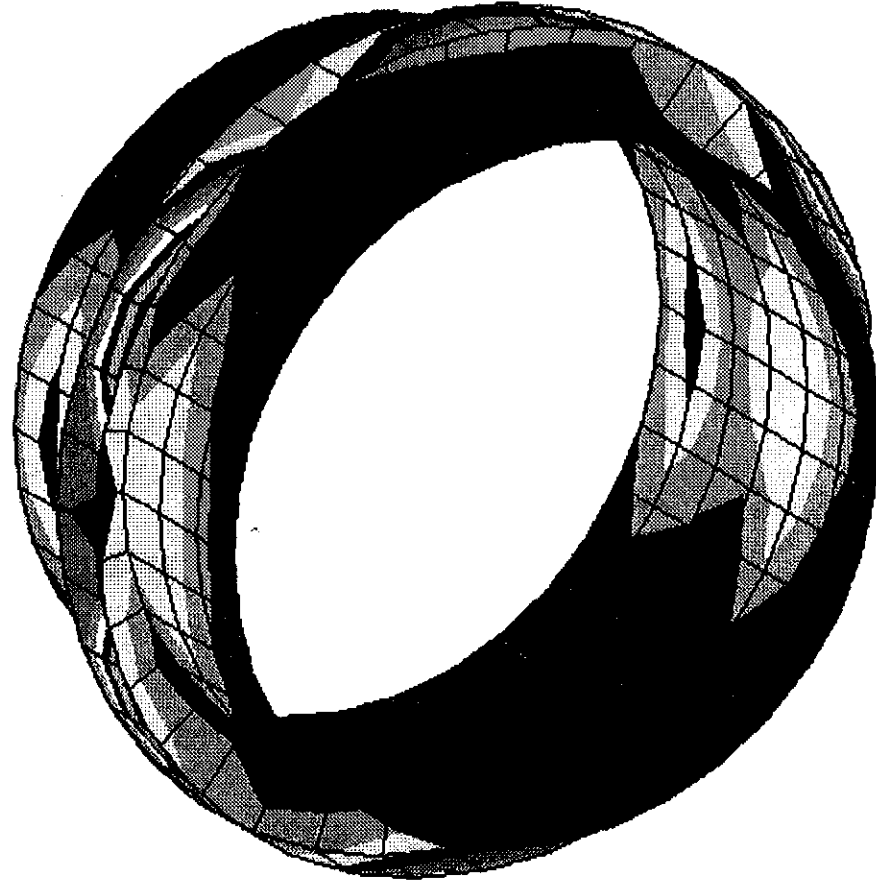
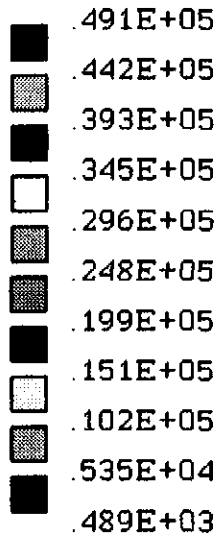
∴ USE  $L 3 \times 3 \times 3/8$  FOR STIFFENER  
RING AT AXIAL RESTRAINT OF  
MODE CLEANER TUBE

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



3 x 3 x 1/4 IN ANGLE STIFFENER  
SWELL THICKNESS = 1/4 IN  
ID = 30.5 IN

IMAGES-3D  
Version 3.0



MODE CLEANER TUBE

Load Case  
3

Stress Contour Plot  
Surf: Bottom  
Stress Intensity

9/30/96  
14:14:46

IMAGES MODEL FOR BEAM TUBE MANIFOLD

ID = 72.25, SHELL THICKNESS, t = .25

MID RADIUS = r =  $\frac{72.25}{2} + .125$

= 36.25 IN

SPACE NODES AT 10°

LONG SIDE LENGTH

L = 2.5  $\sqrt{r t}$

= 2.5  $\sqrt{36.25(.25)}$

= 7.53

ELEMENT ARC LENGTH

S = r  $\theta$

$\theta = 10^\circ = \frac{10}{180} \pi = .175 \text{ RAD}$

S = 36.25 (.175) = 6.34

IF ARC IS 5°, S = 36.25 x  $\frac{5}{180} \pi = 3.16 \text{ IN}$

SPACE RINGS AT 3 IN ALONG AXIS  
USE 18 IN LENGTH  $\Rightarrow \frac{360}{5} = 72 \text{ NODES/RING}$

$\Rightarrow \frac{72 \text{ NODES}}{\text{RING}} \times \left(\frac{18}{3} + 1\right) = 504 \text{ NODES}$

+ 144 NODES FOR STIFFENER

FILES: BMTUBE.MN.\*

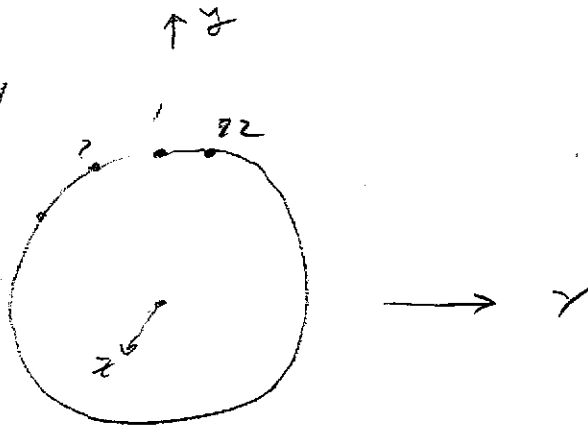
22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



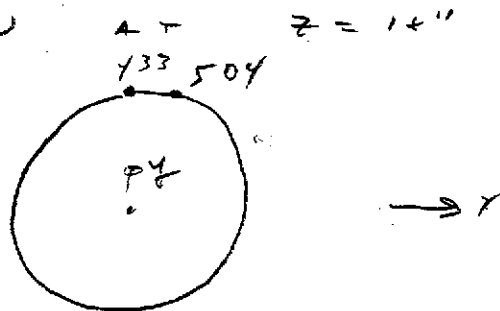
SHELL ELEMENTS - PLATE 1

STIFFENER ELEMENT - PLATE 2

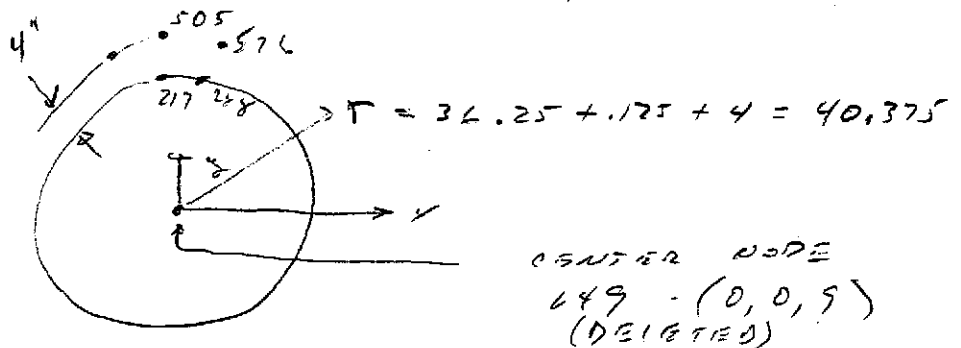
1ST PATTERN



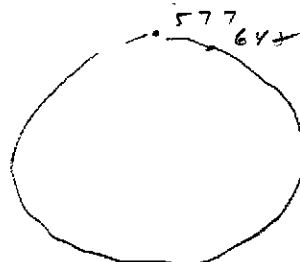
LAST PATTERN



STIFFENER IS ON 4TH PATTERN  
z = 9



NOSES AT END OF STIFFENER



22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS





RESTRAINTS

NODES 1 TO 72 RESTRAINED IN Z-DIRECTION

NODES 1 & 36 RESTRAINED IN X-DIR

NODES 18 & 54 " " Y-

THESE PREVENT TORSION & TRANSLATION

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



LOADS

MAX AXIAL FORCE IS 38,130 LB\* OR

$$F_z = \frac{38130}{2} = 19065 \text{ LB EA SIDE}$$

DIVIDE OVER 8 NODES ON EA SIDE

$$F_{z_i} = \frac{19065}{8} = 2383 \text{ LB / NODE}$$

THESE NODES ARE 233, 234, 235, 236

269, 270, 271, 272

521, 522, 523, 524

557, 558, 559, 560

PRESSURE

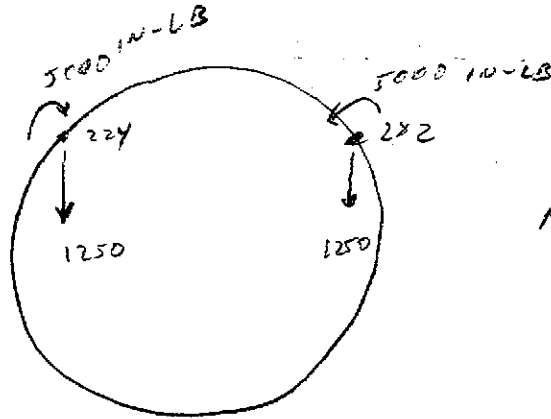
-14.7, EL 1 TO 432

END CAP FORCE ON CASE RING

F = 0 DUE TO BELLOWS

\* REF CALL V049-1-089, p.8A

WT LOAD FROM RESERVOIR HANGERS ON 80 K \*\*



$$M_E = 1750 \times 4$$

$$= 5000 \text{ IN-LB}$$

LOAD CASE 4 - ABOVE LOADS

LOAD CASE 5 - ABOVE COMBINED WITH  
VACUUM PRESS & UNBAL  
AXIAL FORCE (LC 3)

LOAD CASE 1 - EXTERNAL PRESSURE = 14.7 PSI

" " 2 - AXIAL RESTRAINT LOAD

" " 3 - CASE 1 + CASE 2

\* REF CALL V049-1-070, P. 5  
WT = 5000 LB

$$= \frac{5000}{4} = 1250 \text{ LB PER HANGER}$$

\*\* THIS ANALYSIS IS PERFORMED ON MODEL  
OF BEAM TUBE MANIPLED SINCE  
DIAMETERS ARE ALMOST THE SAME.

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



LOAD CASE 1 UNBAL AXIAL FORCE

$$F_z = 38130 \text{ LB}$$

LOAD CASE 2 VAC PRESS = -14.7 PSI

LOAD CASE 3 : 1 & 2 COMBINED

LOAD CASE 4 : HANGER FORCE  
REPRESENTING WT OF 80K PUMP  
INCLUDES MOMENT DUE TO OFFSET  
OR ROD SUPPORT BRACKET

$$F_y = -1250 \text{ LB}$$

$$M_z = \pm 5000 \text{ IN-LB} \\ (4 \text{ IN OFFSET})$$

LOAD CASE 5 : ALL LOADS

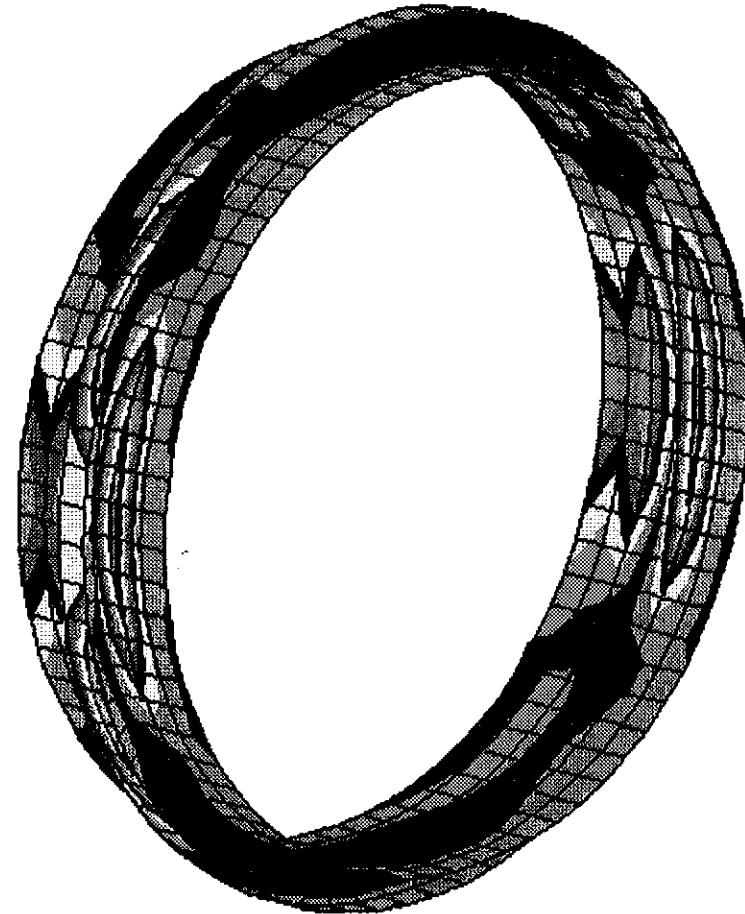
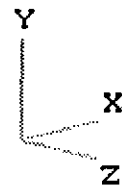
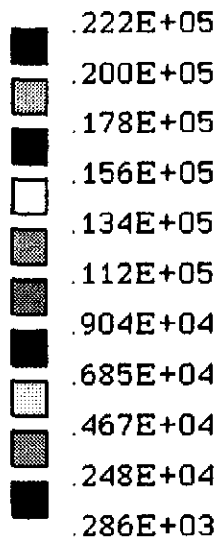
3 COMBINED WITH 4

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



4 x 3 x 1/2 ANGLE STEEL  
 SHELL THICKNESS = 1/4  
 ID = 70.25  
 4 IN LGB IS IN RADIAL DIRECTION

IMAGES-3D  
 Version 3.0



Load Case  
 3

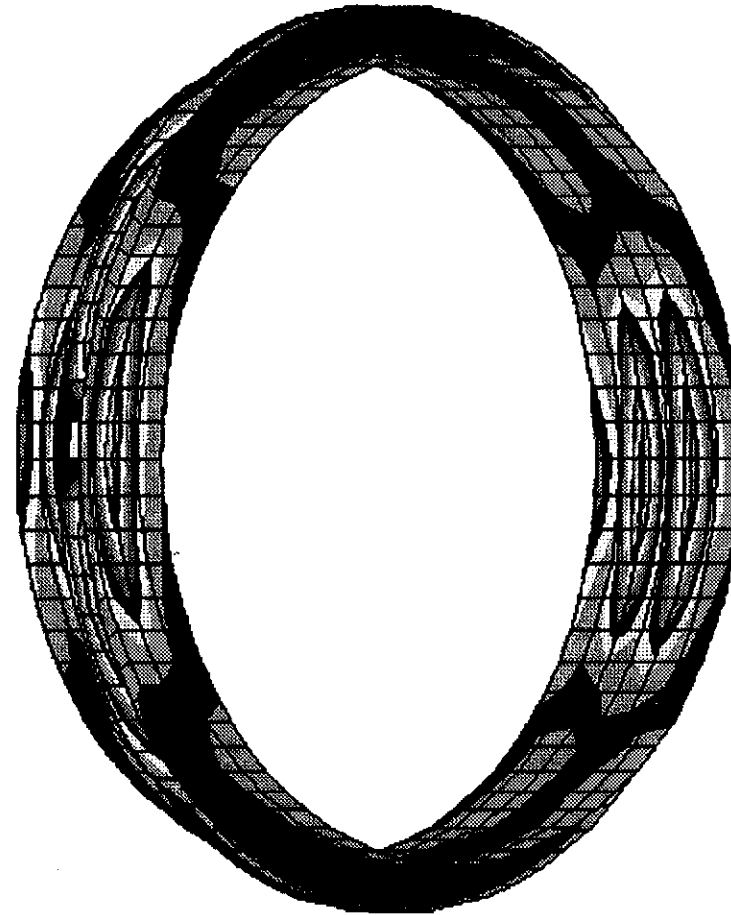
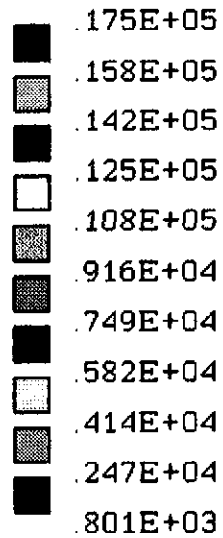
Stress Contour Plot  
 Surf: Bottom  
 Stress Intensity

9/20/96  
 11:17:35

COMBINED UNBALANCED AXIAL FORCE  
 & VACUUM PRESSURE

44 34 1/2 ANGLE STIFFENER  
 SHELL THICKNESS = 1/4  
 ID = 72.25

IMAGES-3D  
 Version 3.0



\* 4" LEG IS  
 IN RADIAL  
 DIRECTION

BEAM TUBE MANIFOLD

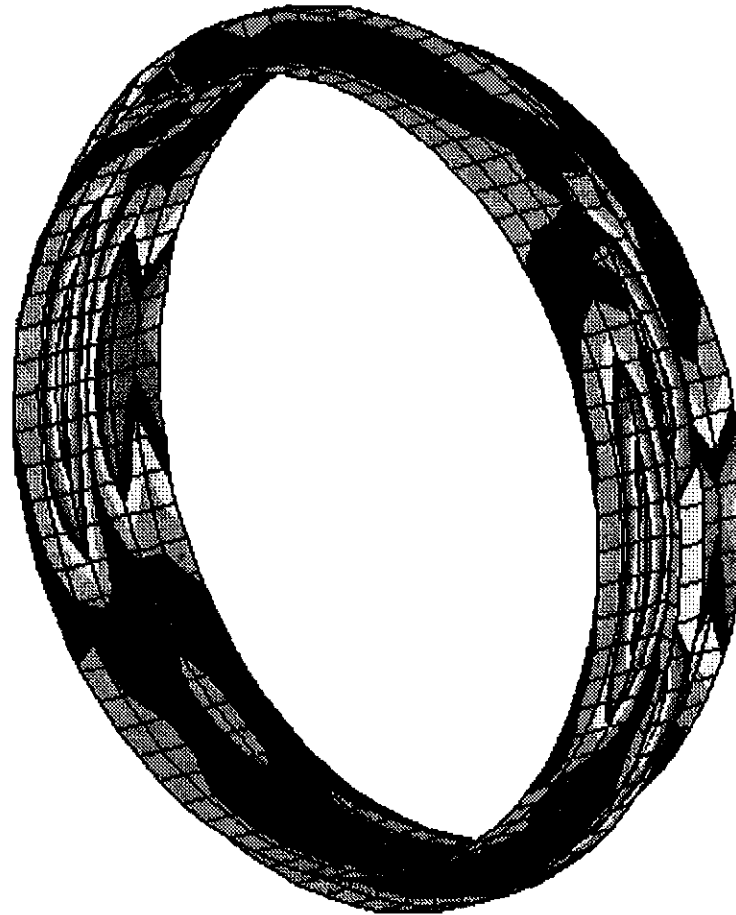
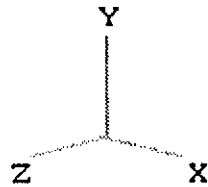
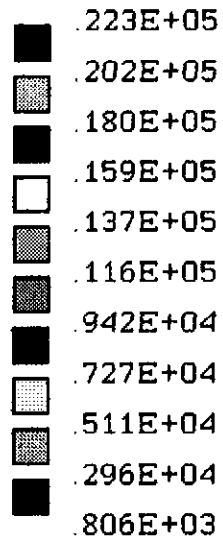
Load Case  
 3

Stress Contour Plot  
 Surf: Top  
 Stress Intensity

9/16/96  
 11: 6: 9

SAME CONFIGURATION

IMAGES-3D  
Version 3.0



BEAM TUBE MANIFOLD

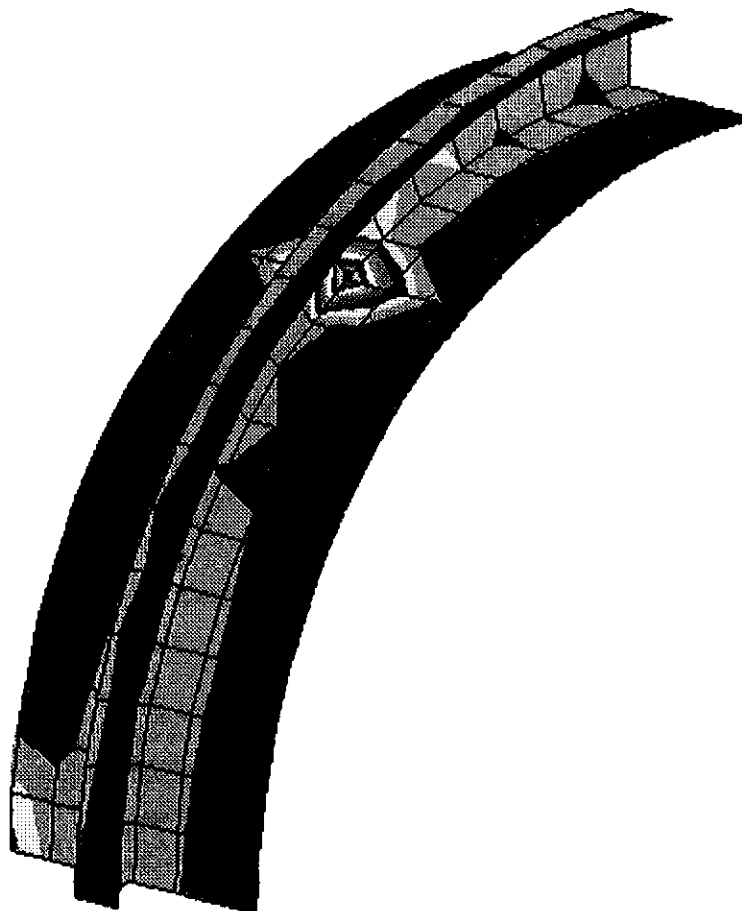
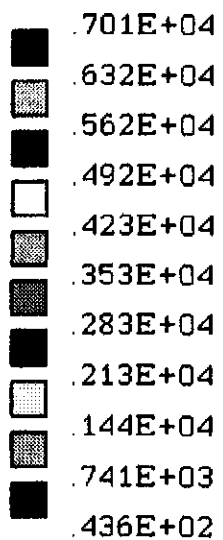
Load Case  
5

Stress Contour Plot  
Surf: Bottom  
Stress Intensity

9/20/96  
11:27:35

↖ LOAD CASE 3 COMBINED WITH  
HANGER LOAD FROM 50 K PUMP RESERVOIR

IMAGES-3D  
Version 3.0



Load Case  
4

BEAM TUBE MANIFOLD

Stress Contour Plot

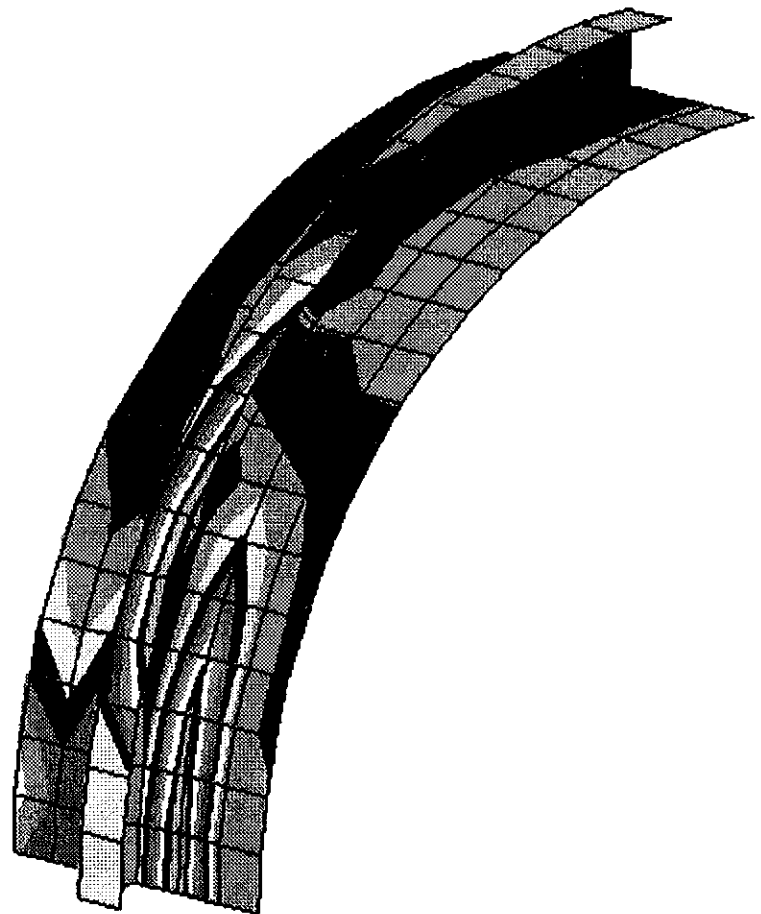
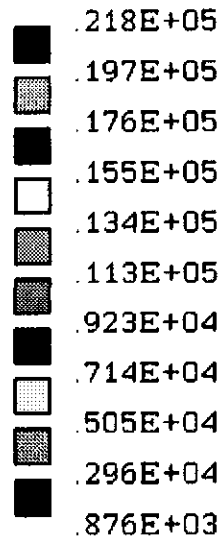
Surf: Middle

Stress Intensity

9/20/96  
10:58:38

↑ 1250 LB HANGER FORCE FROM 60K PUMP  
+ 5000 IN-LB MOMENT AT SAME LOCATION

IMAGES-3D  
Version 3.0



BEAM TUBE MANIFOLD

Stress Contour Plot  
Surf: Bottom      Stress Intensity

Load Case  
5

9/20/96  
11: 8: 5



BEAM TUBE MANIPULO 1/2 80 K PUMP  
STRESS EVALUATION

MAX STRESS INTENSITY IS 22,300 PSI

=>  $P_H = 22.3 \text{ KSI}$

$< 1.5 S_H = 28.0 \text{ KSI @ } 400^\circ\text{F}$

50 SHEETS  
100 SHEETS  
200 SHEETS  
22-141  
22-142  
22-144



ADAPTERS B6 & B7

$$ID = 48.25$$
$$t = .25$$

$$M.O \text{ RADIUS } r = \frac{48.25 + .25}{2}$$
$$= 24.25 \text{ IN}$$

LONG SHELL DIST

$$L = 2.5 \sqrt{r t}$$
$$= 2.5 (24.25 (.25))^{\frac{1}{2}}$$
$$= 6.16 \text{ IN}$$

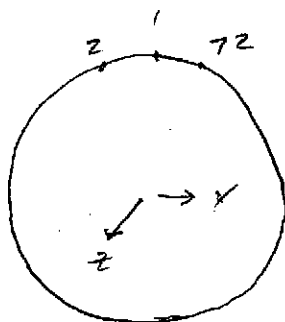
SPACE NODES AT 5°

$$S = r \theta$$
$$\theta = 5^\circ \times \frac{\pi}{180} = .0873 \text{ RAD}$$
$$S = 24.25 (.0873) = 2.116 \text{ IN}$$

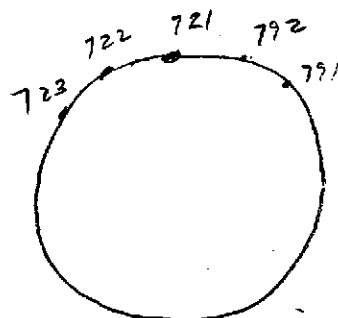
USE 20 IN FOR MODEL LENGTH, SPACE RINGS AT 2 IN. STIFFENER IS AT MID LENGTH, Z = 10 IN

$$72 \text{ NODES PER RING} \Rightarrow 11 \times 72 + 2 \times 72 = 936 \text{ NODES}$$

1ST RING



LAST RING

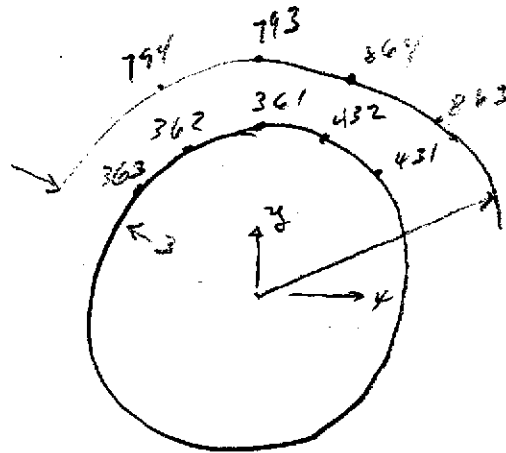


22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



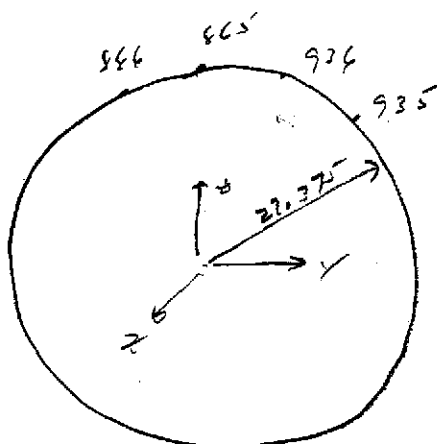
BL 937 CONT

STIFFENER IS ON 6TH RING (L 3x3 x 3/4)



$$r = 24.25 + .125 + 3 = 27.375$$

NODES AT END OF STIFFENER



RESTRAINTS

AT  $z = 0$ , AXIAL RESTRAINT - Z

NODES 1, 36 - X DIR RESTRAINED

NODES 18, 54 - Y DIR RESTRAINED

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



B-6 & B-7 CONT

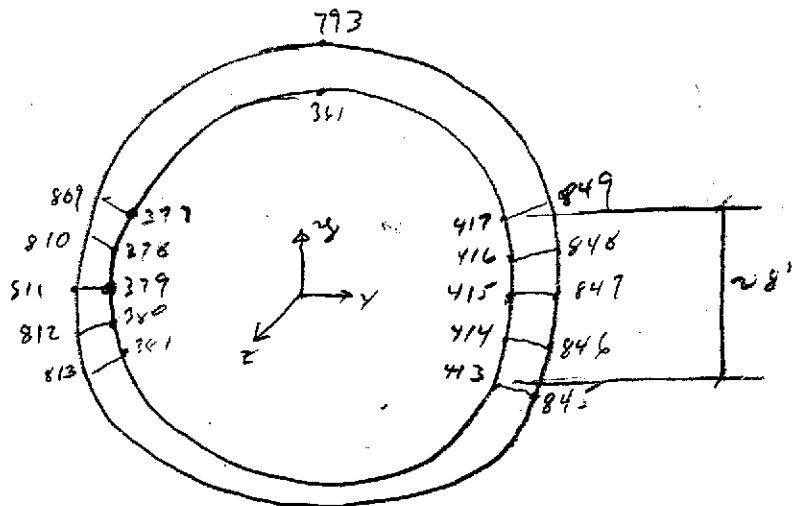
LOADS

PRESSURE -14.7 EL 1 TO 120

AXIAL FORCES

F<sub>z</sub> = 32170 LB REF CALC V049-1-095 P.7

DIVIDE LOAD OVER 10 NODES ON EA SIDE AT STIFF RING



F<sub>zL</sub> =  $\frac{32170}{20}$  = 1608.5 LB

PLOTS ON FOLLOWING SHEETS SHOW

P<sub>b</sub> = 23.8 KSI

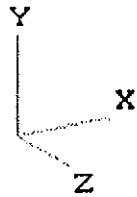
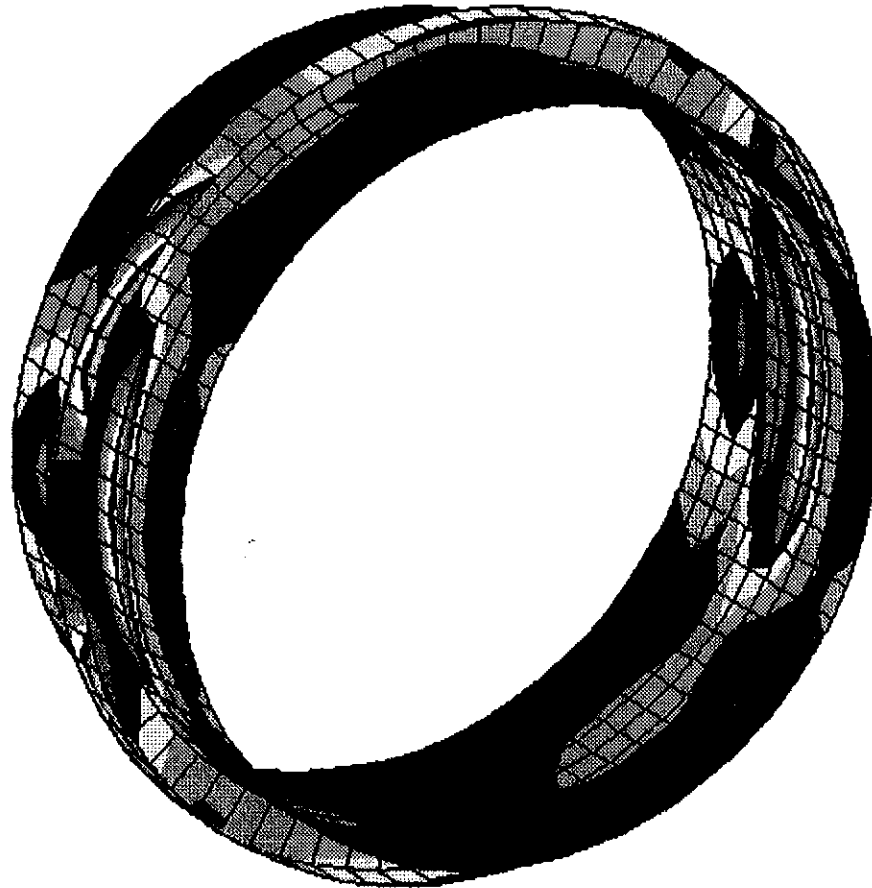
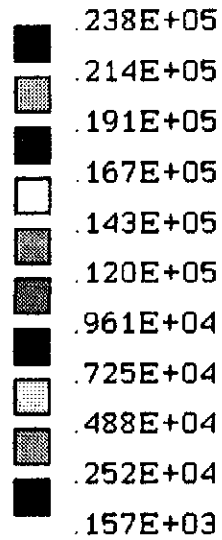
< 1.5 S<sub>m</sub> = 28 KSI @ 400°F FOR 304 SS

OR



3 x 3 x 3/8 ANGLE STIFFENED  
 SHELL THICKNESS = 1/4"  
 I D = 48.25 IN

IMAGES-3D  
 Version 3.0



Load Case  
 3 \*

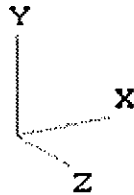
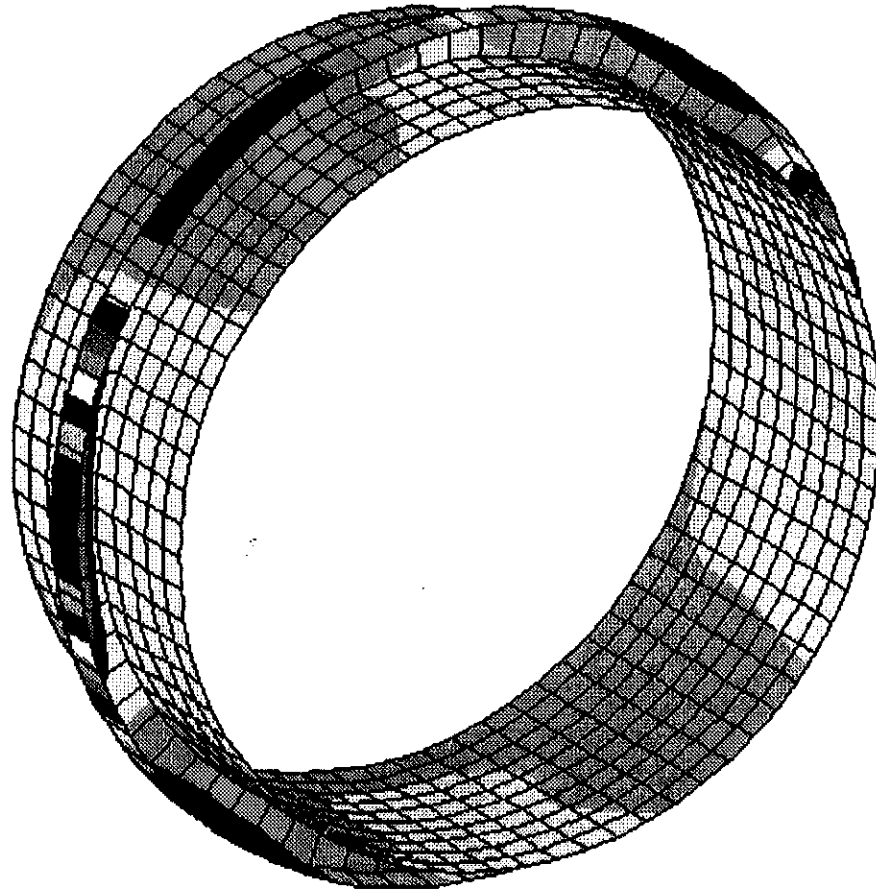
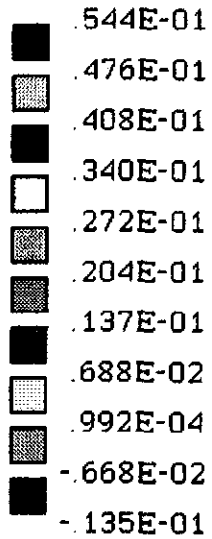
APPARATUS B-6 & B-7  
 Stress Contour Plot  
 Surf: Bottom  
 Stress Intensity

9/30/96  
 11:58:45

\* AXIAL FORCE + PRESSURE

3 x 3 x 3/8 ANGLE STIFFENER  
SHELL THICKNESS = 1/4"  
ID = 48.75 IN

IMAGES-3D  
Version 3.0



ADONIS B-6 & B-7

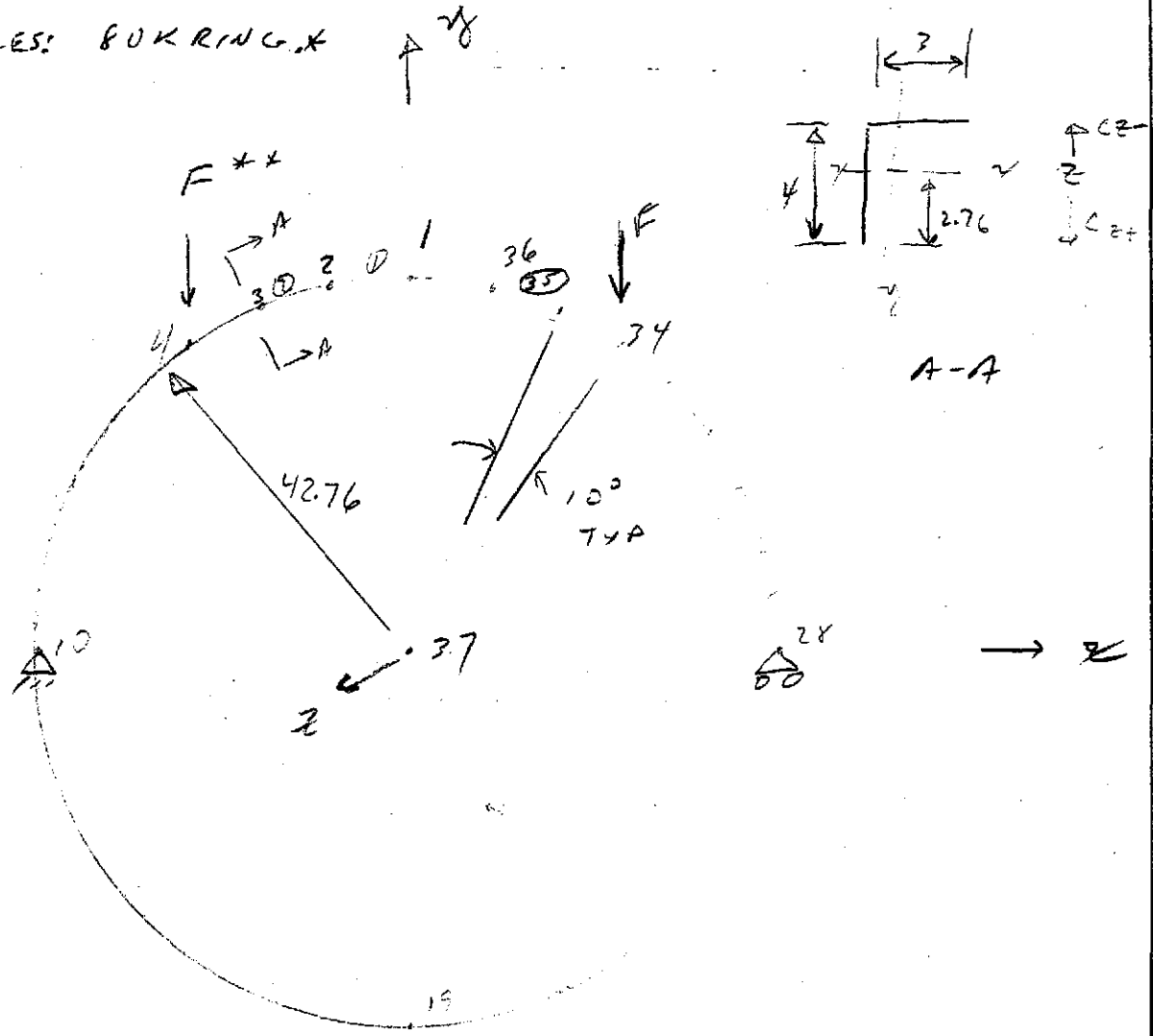
Displacement Contour Plot  
DZ

Load Case  
3

9/30/96  
12:10:12

80K STIFFENER RING \*  
FILES: 80K RING.X

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



SMALL OD = 80 IN

STIFFENER: L 4x3x 1/4

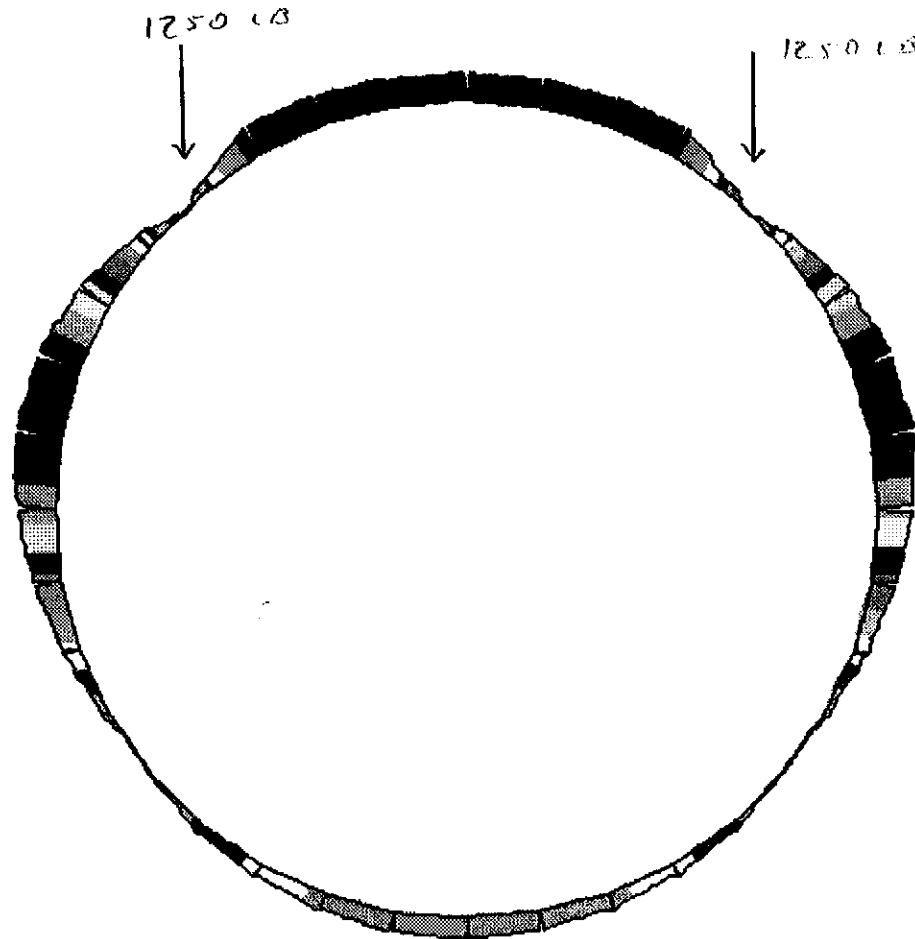
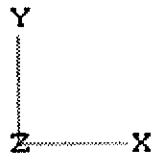
\* THIS ANALYSIS PERTAINS TO RING THAT SUPPORTS RESERVOIR BUT NOT EXTERNAL AXIAL RESTRAINT.

Revision No. 0  
Doc. No. V049-1-108  
Page 29 of 34

\*\* F = 1250 LB DEAD WT ONLY - LOAD CASE 1  
F = 1500 LB SHIPPING FORCE - LOAD CASE 2

L 4x3x1/4 STIFFENER - 304 SS

IMAGES-3D  
Version 3.0



Load Case \*  
1

80K PUMP STIFFENER RING  
Stress Diagram  
Minimum Normal

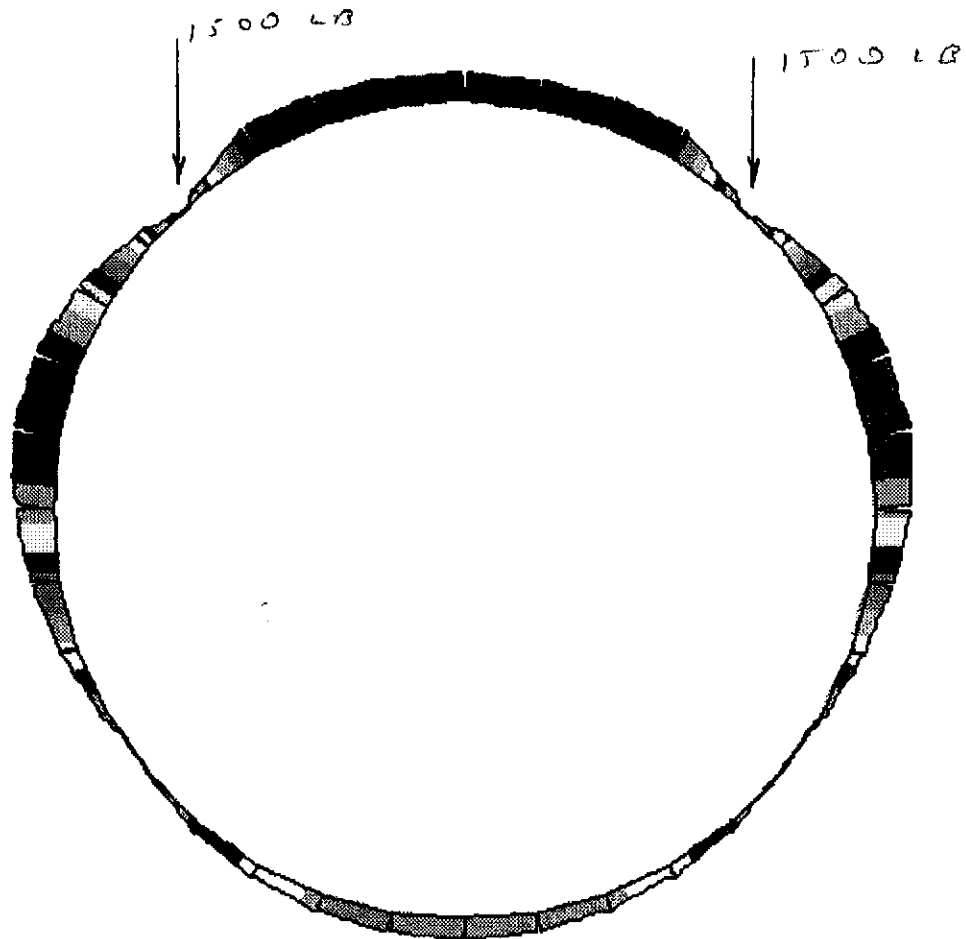
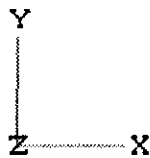
9/ 9/96  
13:38:47

\* VERTICAL - WT ONLY  
RESERVOIR FILLED



L 4 X 3 X 1/4 STIRRER RING - 304 SS

IMAGES-3D  
Version 3.0



Load Case \*  
2

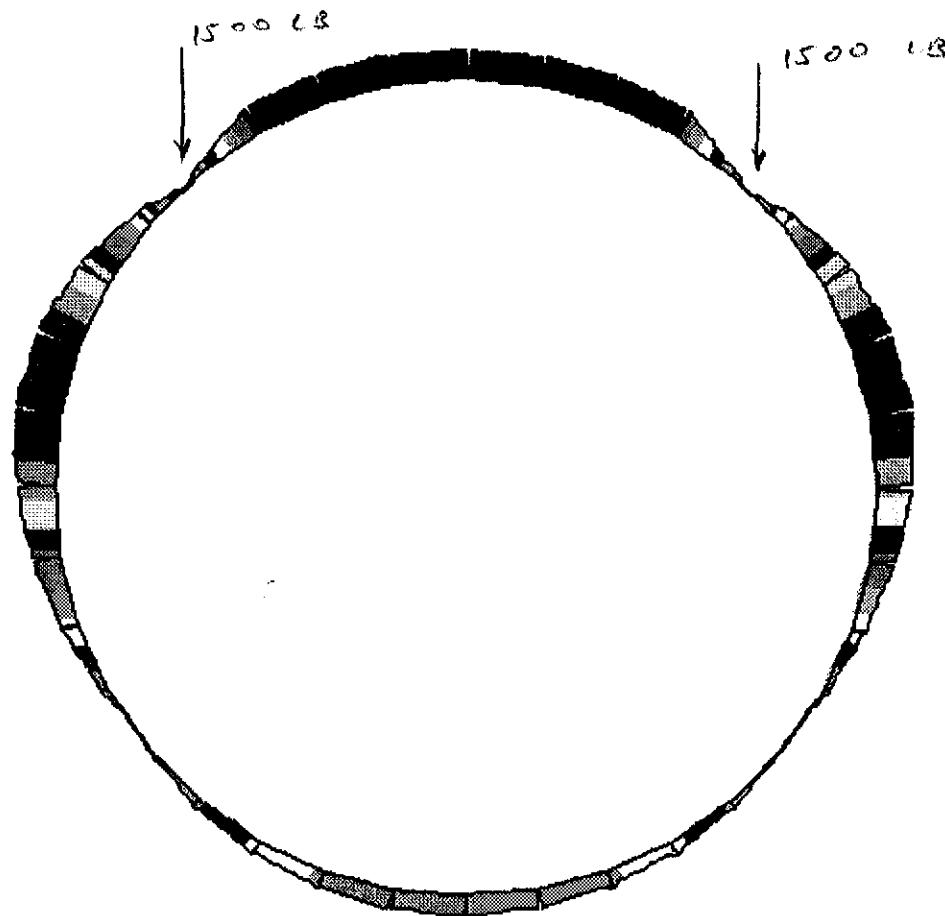
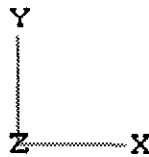
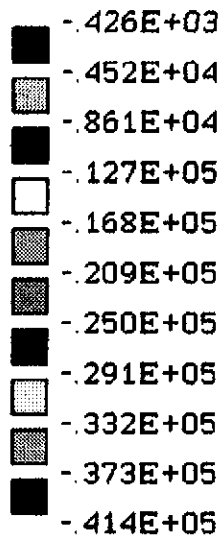
80K PUMP STIRRER RING  
Stress Diagram  
Minimum Normal

9/ 9/96  
13:43:51

\* VERTICAL WT + SHIPPING LOAD  
RESERVOIR EMPTY

L 2x2x 1/4 STAINLESS STEEL - 304 SS

IMAGES-3D  
Version 3.0



Load Case  
1 \*

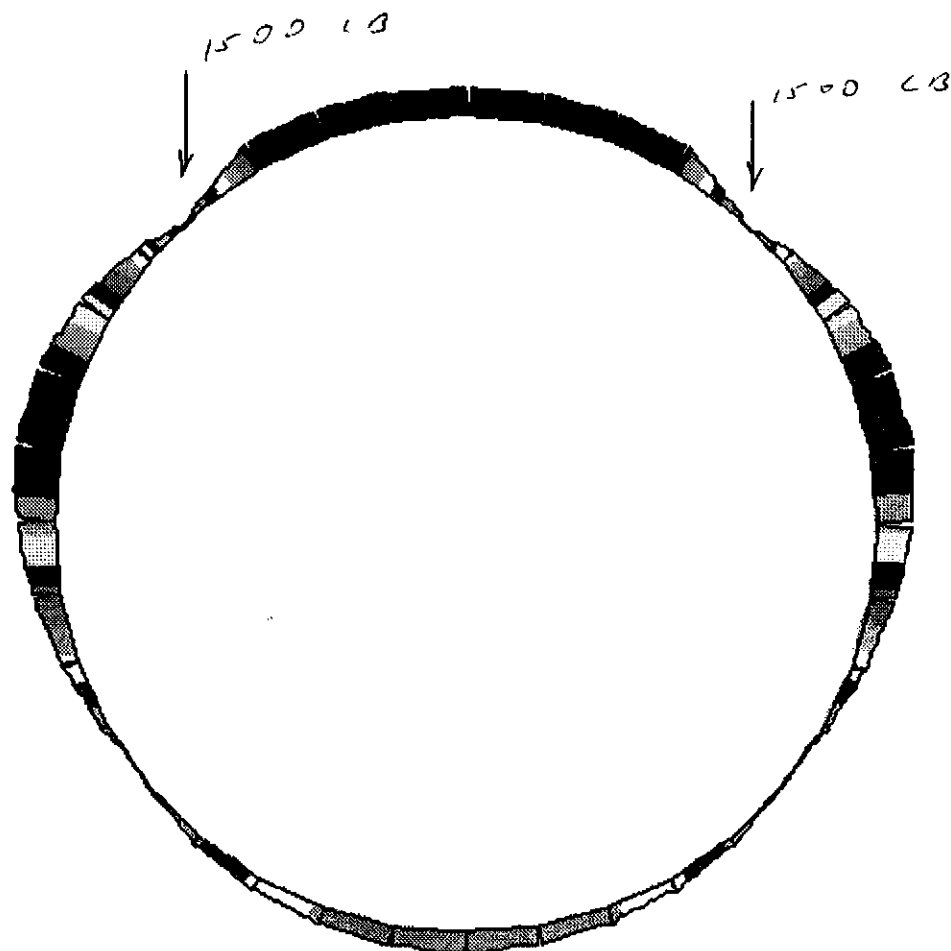
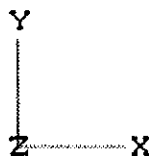
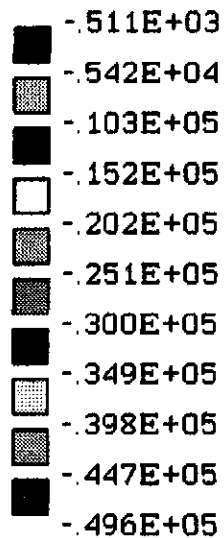
Stress Diagram  
Minimum Normal

9/ 9/96  
14: 5: 1

\* VERT LOAD - WT ONLY  
RESERVOIR FILLED

L 2x2 x 1/4 STAINLESS - 204 SA

IMAGES-3D  
Version 3.0



Load Case \*  
2

Stress Diagram  
Minimum Normal

9/ 9/96  
14: 1:53

\* VERT WT + SHIPBOARD LOAD  
RESERVOIR EMPTY

80K STIFFENER RING (L 4x3 x 1/4)

STRESS EVAL

MAXIMUM STRESS RESULTING FROM  
BENDING OF RING DURING SHIPPING  
IS 12,700 psi

$$P_M = 12.7 \text{ ksi}$$

$$L 1.5 S_M = 28.0 \text{ ksi}$$

*M*

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-112 PAGE 1 OF 107
REV.	DEO #	DATE	BY:	CHECK	TITLE:  <b>BSC Portable Clean Room</b>	
0	349	10.8.96	WDB	RDC		
					BY: W. Bilynsky	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<p><b>PURPOSE:</b></p> <p>Design mobile (portable) Clean Room for the Beam Splitter Chamber (BSC). The frame design must be able to withstand the installed weight of the air circulators and various pumps and must also be fairly lightweight to allow unconstrained mobility. Additionally, the BSC clean room frame will have adjustable (telescoping) legs for fitup and alignment and will also be easily assembled and disassembled as needed.</p>						
<p><b>METHOD:</b></p> <p>Support frame is designed to AISC standards using classical hand calculations and STAAD-III computer program (release 21).</p>						
<p><b>ASSUMPTIONS:</b></p> <p>See calculation</p>						
<p><b>INPUTS:</b></p> <ol style="list-style-type: none"> <li>Design load = 10.0 lbs/ft<sup>2</sup></li> <li>Non-standard AISC Structural Members (see calculation)</li> </ol>						
<p><b>REFERENCES:</b></p> <ol style="list-style-type: none"> <li>STAAD-III , Research Engineers, Release 21</li> <li>AISC - ASD 9th edition</li> <li>Doc. No. V049-1-066 LIGO Vacuum Equipment Structural Design Criteria</li> <li>Aluminum Construction Manual, Section 3, Engineering data for aluminum structures.</li> </ol>						
<p><b>CALCULATIONS:</b></p>						
<p><b>CONCLUSIONS:</b></p> <p>The requirements of the AISC Codes and Standards and the Ligo Vacuum Equipment Structural Design Criteria are met.</p>						
<p><b>NOTES:</b> STAAD-III Computer File: BSCLNRM3.*</p>						

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-112
		Rev. No. 0
		Page 2 of 107
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: BSC ( Beam Splitter Chamber ) Portable Cleanroom		

### TABLE OF CONTENTS

Revision History	3
BSC Cleanroom Design/Analysis	
Member Properties	4
Loading Condition	5
STAAD Input Model	6
STAAD Computer Generated Plot	8
STAAD Output File	11
Moment (Bolted) Connection Design	104
Lifting Lug	106
Design Details	
Weld Calculation	
Attachment 'A'	
Detail Design Sketches	A1 - A5
Attachment 'B'	
Final Design Drawing	B1 - B2



MEMBER PROPERTIES

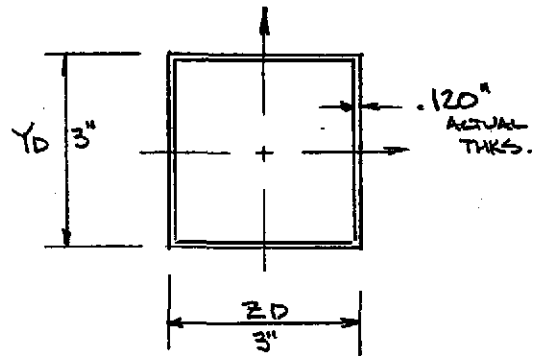
AISC TABLE (CARBON STEEL)

- TUBE STEEL 6" x 3" x 3/16"  
TABLE ST TUB 60303
- TUBE STEEL 3" x 2" x 3/16"  
TABLE ST TUB 30203
- TUBE STEEL 3 1/2" x 3 1/2" x 3/16"  
TABLE ST TUB 35353
- TUBE STEEL 2" x 2" x 3/16"  
TABLE ST TUB 20203

PRISMATIC PROPERTIES (ALUMINUM STRUCTURAL MEMBERS)

- ALUMINUM COLUMN TUBE LEGS 3" x 3" x 1/8"

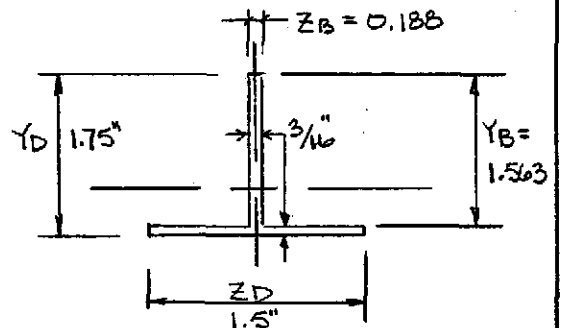
$A_x = 1.382 \text{ in}^2$   
 $I_y = 1.914 \text{ in}^4$   
 $I_z = 1.914 \text{ in}^4$   
 $Y_D = 3.0 \text{ in}$   
 $Z_D = 3.0 \text{ in}$



REF. ALUMINUM CONSTRUCTION MANUAL  
SECTION 3  
Engineering data for aluminum structures  
THE ALUMINUM ASSOCIATION

- ALUMINUM TEES

$Y_D = 1.75 \text{ in}$   
 $Z_D = 1.50 \text{ in}$   
 $Y_B = 1.563 \text{ in}$   
 $Z_B = 0.188 \text{ in}$





LOADING CONDITION

PER PANEL

$$2'-0" \times 3'-0" = 6 \text{ FT}^2$$

SAY: 50 lbs / PANEL (AIR CIRCULATORS & PUMPS)

$$\therefore \frac{50 \text{ lbs / PANEL}}{6 \text{ FT}^2} = 8.33 \text{ lbs / FT}^2$$

ADD ADDITIONAL MISC DEAD WGT  $\approx$  10.0 lbs / FT<sup>2</sup>  
TOTAL

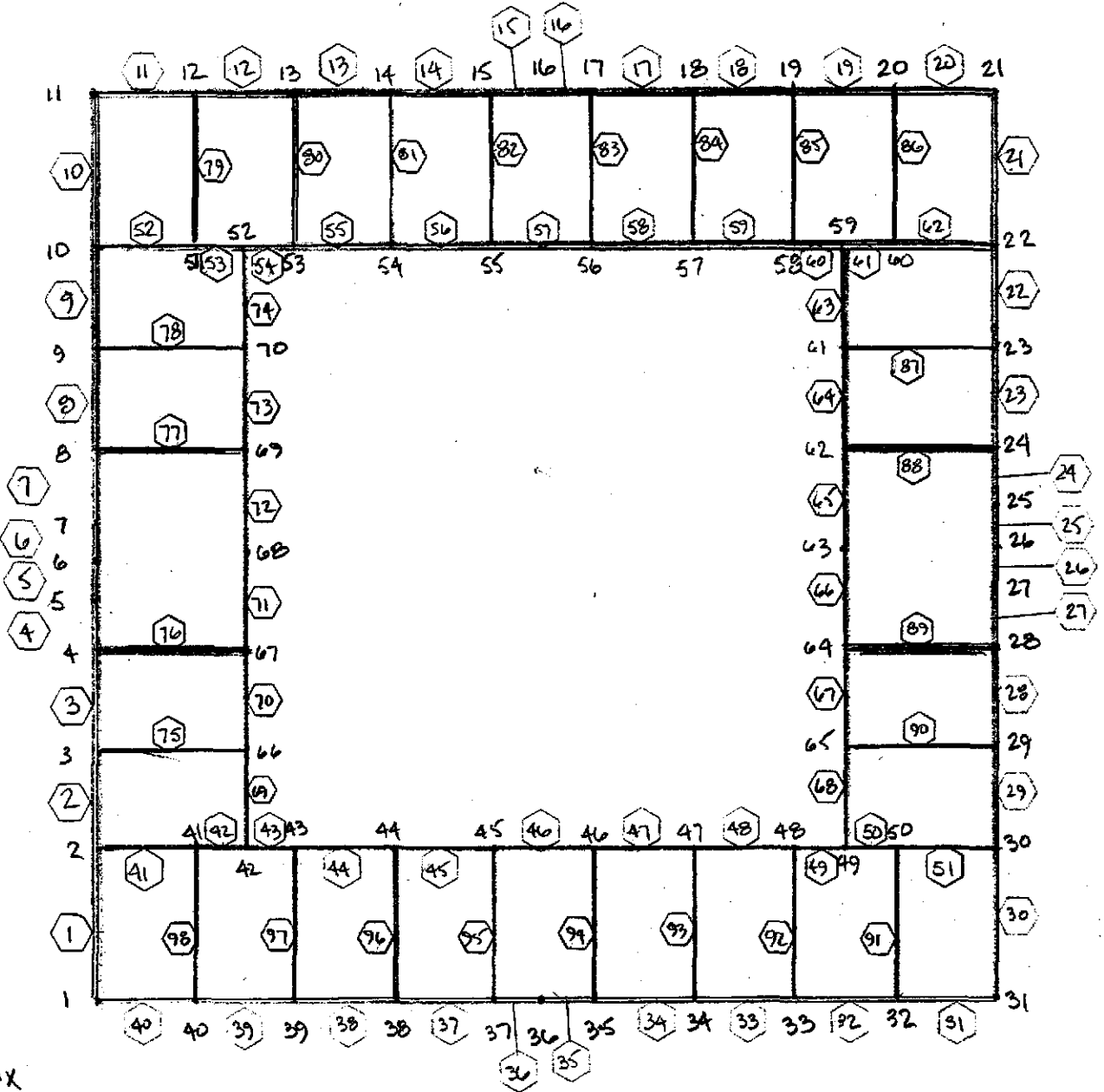
$$10 \frac{\text{lbs}}{\text{FT}^2} = 0.0694 \frac{\text{lbs}}{\text{IN}^2} \approx 0.10 \frac{\text{lbs}}{\text{IN}^2}$$

DESIGN FOR 0.10 lbs / in<sup>2</sup> + SELF WEIGHT

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS

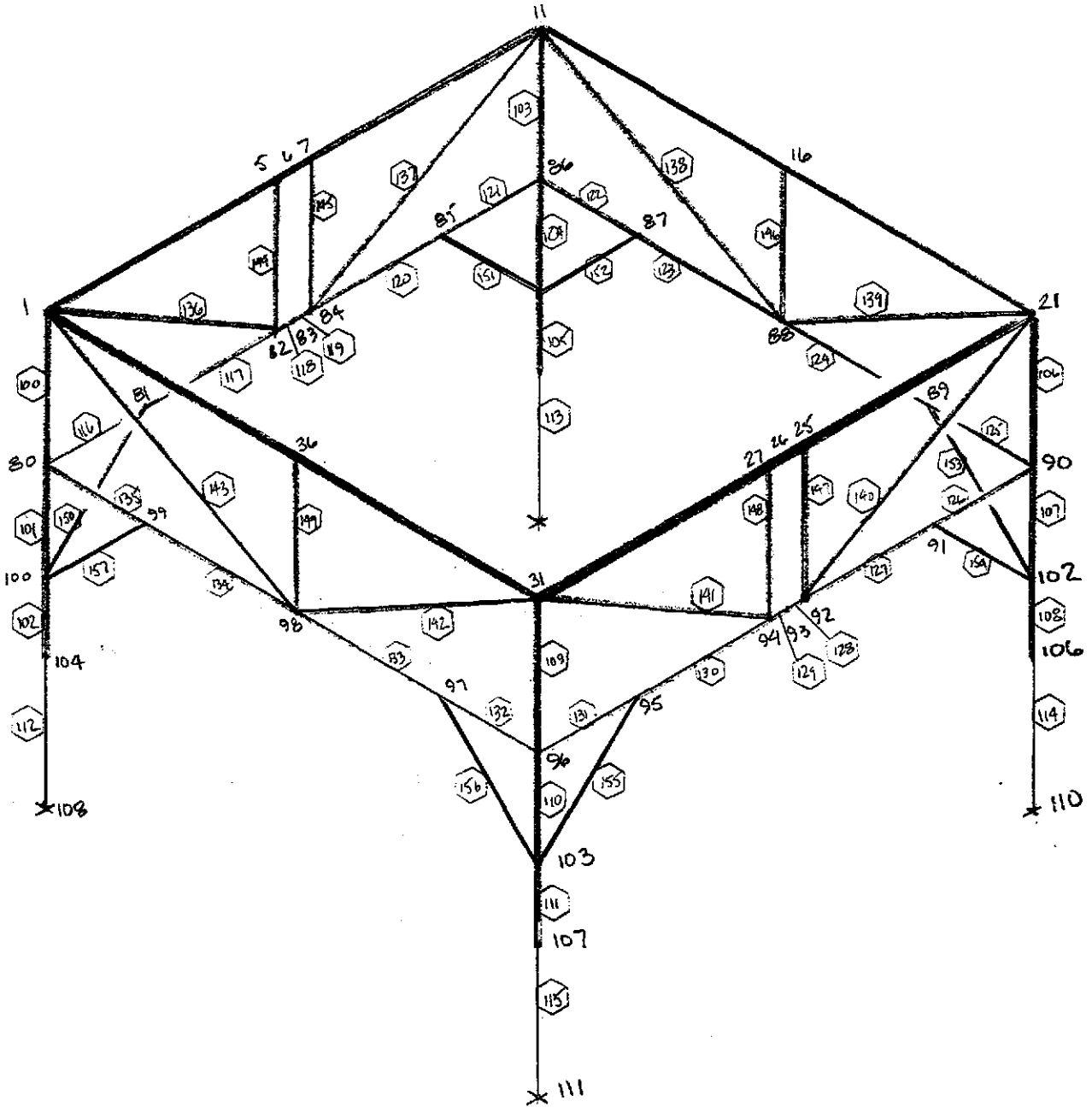



50 SHEETS  
 22-141 22-142 100 SHEETS  
 22-144 200 SHEETS



ALUMINUM 75 78 TO 87  
 90 TO 98

BSCLNRM3

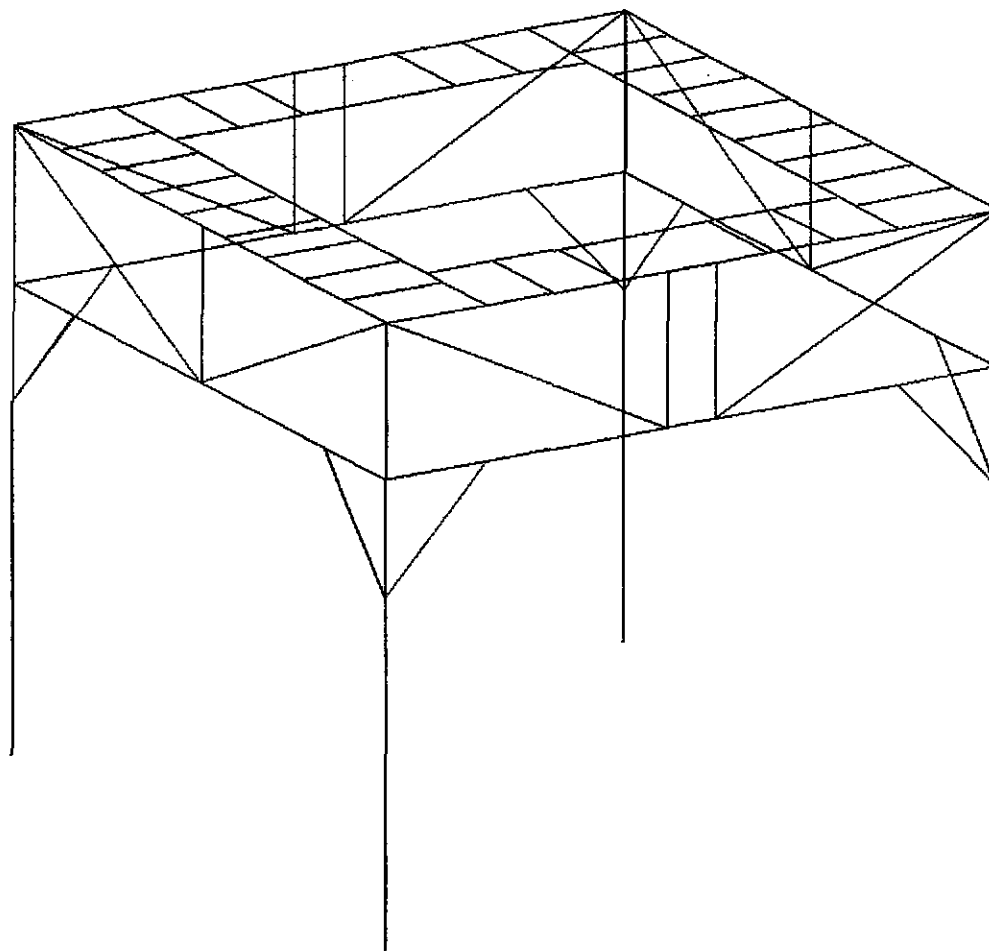


REV	BY	DATE	CHECKED	DATE					PAGE
									Revision No. 0 Doc. No. V049-1-112 Page 7 of 107

HN/ELEN

STRUCTURE DATA

TYPE = SPACE  
NJ = 102  
NM = 156  
NE = 0  
NS = 4  
NL = 1  
XMAX= 223.0  
YMAX= 192.0  
ZMAX= 223.0



J=102,H=156

UNIT INC POU

USER ID:PROCESS SYSTEMS INTERNATIONAL

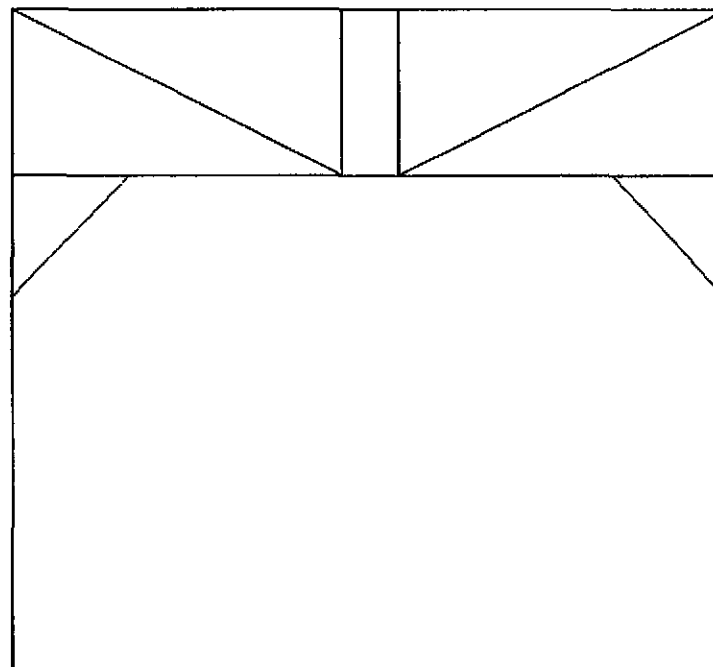
STAAD POST - PLOT (REV: 21.0 )  
IN  
TITLE: BSC PORTABLE CLEANROOM

DATE: OCT 7, 1996

NH/ELEH

STRUCTURE DATA

TYPE = SPACE  
NJ = 102  
NH = 156  
NE = 0  
NS = 4  
NL = 1  
XMAX= 223.0  
YMAX= 192.0  
ZMAX= 223.0



J=102,N=156

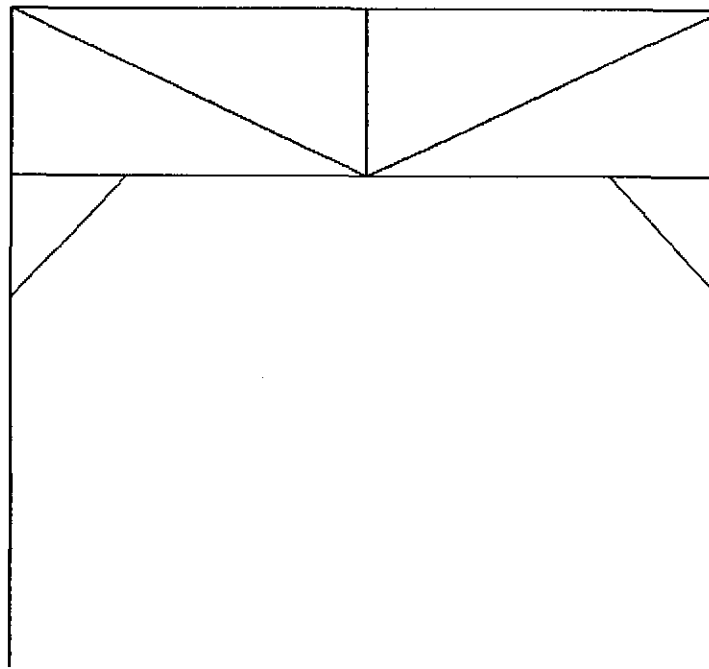
UNIT INC POU

ST A A D P O S T - P L O T (REV: 21.0 )  
USER ID:PROCESS SYSTEMS INTERNATIONAL IN  
TITLE: B5C PORTABLE CLEANROOM

DATE: OCT 7, 1996

STRUCTURE DATA

TYPE = SPACE  
 NJ = 102  
 NH = 156  
 NE = 0  
 NS = 4  
 NL = 1  
 XMAX= 223.0  
 YMAX= 192.0  
 ZMAX= 223.0



J=102,N=156

UNIT INC POU

```

*****
*
*           S T A A D - III           *
*           Revision 21.0             *
*           Proprietary Program of    *
*           Research Engineers, Inc.   *
*           Date=   SEP 25, 1996      *
*           Time=   8:38:27           *
*
*           USER ID: PROCESS SYSTEMS INTERNATIONAL IN *
*****

```

1. STAAD SPACE BSC PORTABLE CLEANROOM
2. INPUT WIDTH 72
3. UNIT INCHES POUND
4. JOINT COORDINATES
5. 1 0. 0.; 2 36. 0. 0.; 3 60. 0. 0.; 4 84. 0. 0.; 5 102.333 0. 0.
6. 6 111.5 0. 0.; 7 120.667 0. 0.; 8 139. 0. 0.; 9 163. 0. 0.
7. 10 187. 0. 0.; 11 223. 0. 0.; 12 223. 0. 26.5; 13 223. 0. 50.5
8. 14 223. 0. 74.5; 15 223. 0. 98.5; 16 223. 0. 111.5; 17 223. 0. 124.5
9. 18 223. 0. 148.5; 19 223. 0. 172.5; 20 223. 0. 196.5; 21 223. 0. 223.
10. 22 187. 0. 223.; 23 163. 0. 223.; 24 139. 0. 223.; 25 120.667 0. 223.
11. 26 111.5 0. 223.; 27 102.333 0. 223.; 28 84. 0. 223.; 29 60. 0. 223.
12. 30 36. 0. 223.; 31 0. 0. 223.; 32 0. 0. 196.5; 33 0. 0. 172.5
13. 34 0. 0. 148.5; 35 0. 0. 124.5; 36 0. 0. 111.5; 37 0. 0. 98.5
14. 38 0. 0. 74.5; 39 0. 0. 50.5; 40 0. 0. 26.5; 41 36. 0. 26.5
15. 42 36. 0. 36.; 43 36. 0. 50.5; 44 36. 0. 74.5; 45 36. 0. 98.5
16. 46 36. 0. 124.5; 47 36. 0. 148.5; 48 36. 0. 172.5; 49 36. 0. 187.
17. 50 36. 0. 196.5; 51 187. 0. 26.5; 52 187. 0. 36.; 53 187. 0. 50.5
18. 54 187. 0. 74.5; 55 187. 0. 98.5; 56 187. 0. 124.5; 57 187. 0. 148.5
19. 58 187. 0. 172.5; 59 187. 0. 187.; 60 187. 0. 196.5; 61 163. 0. 187.
20. 62 139. 0. 187.; 63 111.5 0. 187.; 64 84. 0. 187.; 65 60. 0. 187.
21. 66 60. 0. 36.; 67 84. 0. 36.; 68 111.5 0. 36.; 69 139. 0. 36.
22. 70 163. 0. 36.; 80 0. -48. 0.; 81 36. -48. 0.; 82 102.333 -48. 0.
23. 83 111.5 -48. 0.; 84 120.667 -48. 0.; 85 187. -48. 0.; 86 223. -48. 0.
24. 87 223. -48. 36.; 88 223. -48. 111.5; 89 223. -48. 187.
25. 90 223. -48. 223.; 91 187. -48. 223.; 92 120.667 -48. 223.
26. 93 111.5 -48. 223.; 94 102.333 -48. 223.; 95 36. -48. 223.
27. 96 0. -48. 223.; 97 0. -48. 187.; 98 0. -48. 111.5; 99 0. -48. 36.
28. 100 0. -84. 0.; 101 223. -84. 0.; 102 223. -84. 223.; 103 0. -84. 223.
29. 104 0. -90. 0.; 105 223. -90. 0.; 106 223. -90. 223.; 107 0. -90. 223.
30. 108 0. -192. 0.; 109 223. -192. 0.; 110 223. -192. 223.
31. 111 0. -192. 223.
32. MEMBER INCIDENCES
33. 1 1 2; 2 2 3; 3 3 4; 4 4 5; 5 5 6; 6 6 7; 7 7 8; 8 8 9; 9 9 10; 10 10 11
34. 11 11 12; 12 12 13; 13 13 14; 14 14 15; 15 15 16; 16 16 17; 17 17 18
35. 18 18 19; 19 19 20; 20 20 21; 21 21 22; 22 22 23; 23 23 24; 24 24 25
36. 25 25 26; 26 26 27; 27 27 28; 28 28 29; 29 29 30; 30 30 31; 31 31 32
37. 32 32 33; 33 33 34; 34 34 35; 35 35 36; 36 36 37; 37 37 38; 38 38 39
38. 39 39 40; 40 40 1; 41 2 41; 42 41 42; 43 42 43; 44 43 44; 45 44 45
39. 46 45 46; 47 46 47; 48 47 48; 49 48 49; 50 49 50; 51 50 30; 52 10 51
40. 53 51 52; 54 52 53; 55 53 54; 56 54 55; 57 55 56; 58 56 57; 59 57 58
41. 60 58 59; 61 59 60; 62 60 22; 63 59 61; 64 61 62; 65 62 63; 66 63 64

42. 67 64 65; 68 65 49; 69 42 66; 70 66 67; 71 67 68; 72 68 69; 73 69 70
43. 74 70 52; 75 3 66; 76 4 67; 77 8 69; 78 9 70; 79 12 51; 80 13 53
44. 81 14 54; 82 15 55; 83 17 56; 84 18 57; 85 19 58; 86 20 60; 87 23 61
45. 88 24 62; 89 28 64; 90 29 65; 91 32 50; 92 33 48; 93 34 47; 94 35 46
46. 95 37 45; 96 38 44; 97 39 43; 98 40 41; 100 1 80; 101 80 100
47. 102 100 104; 103 11 86; 104 86 101; 105 101 105; 106 21 90; 107 90 102
48. 108 102 106; 109 31 96; 110 96 103; 111 103 107; 112 104 108
49. 113 105 109; 114 106 110; 115 107 111; 116 80 81; 117 81 82; 118 82 83
50. 119 83 84; 120 84 85; 121 85 86; 122 86 87; 123 87 88; 124 88 89
51. 125 89 90; 126 90 91; 127 91 92; 128 92 93; 129 93 94; 130 94 95
52. 131 95 96; 132 96 97; 133 97 98; 134 98 99; 135 99 80; 136 1 82
53. 137 11 84; 138 11 88; 139 21 88; 140 21 92; 141 31 94; 142 31 98
54. 143 1 98; 144 5 82; 145 7 84; 146 16 88; 147 25 92; 148 27 94; 149 36 98
55. 150 100 81; 151 101 85; 152 101 87; 153 102 89; 154 102 91; 155 103 95
56. 156 103 97; 157 100 99
57. MEMBER PROPERTY AMER
58. 1 TO 62 TABLE ST TUB60303
59. 63 TO 74 TABLE ST TUB30203
60. 75 78 TO 87 90 TO 98 PRI YD 1.75 ZD 1.5 YB 1.563 ZB 0.188
61. \*\*\* ALUM. TEES @ 180 DEG.
62. 100 TO 111 TABLE ST TUB35353
63. \*\*\* COLUMN TUBE STEEL LEGS
64. 112 TO 115 PRI AX 1.382 IY 1.914 IZ 1.914 YD 3. ZD 3.
65. \*\*\* ALUMINUM COLUMN TUBE LEGS (3" X 3" X 1/8")
66. 76 77 88 89 116 TO 157 TABLE ST TUB20203
67. MEMBER RELEASE
68. 75 78 TO 87 90 TO 98 START MX MY MZ
69. 75 78 TO 87 90 TO 98 END MX MY MZ
70. CONSTANTS
71. E STEEL MEMB 1 TO 74 76 77 88 89 100 TO 111 116 TO 157
72. E ALUMINUM MEMB 75 78 TO 87 90 TO 98 112 TO 115
73. POISSON STEEL MEMB 1 TO 74 76 77 88 89 100 TO 111 116 TO 157
74. POISSON ALUMINUM MEMB 75 78 TO 87 90 TO 98 112 TO 115
75. DENSITY STEEL MEMB 1 TO 74 76 77 88 89 100 TO 111 116 TO 157
76. DENSITY ALUMINUM MEMB 75 78 TO 87 90 TO 98 112 TO 115
77. BETA 180. MEMB 75 78 TO 87 90 TO 98
78. SUPPORTS
79. 108 FIXED BUT FX FZ MX MZ
80. 109 FIXED BUT FX FZ MX MZ
81. 110 FIXED BUT FX FZ MX MZ
82. 111 FIXED BUT FX FZ MX MZ
83. LOAD 1 AREA LOAD
84. SELFWEIGHT Y -1.
85. AREA LOAD
86. 1 TO 98 ALOAD -0.1
87. PERFORM ANALYSIS



P R O B L E M   S T A T I S T I C S

---

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS = 102/ 156/ 4  
 ORIGINAL/FINAL BAND-WIDTH = 88/ 13  
 TOTAL PRIMARY LOAD CASES = 1, TOTAL DEGREES OF FREEDOM = 604  
 SIZE OF STIFFNESS MATRIX = 50736 DOUBLE PREC. WORDS  
 REQD/AVAIL. DISK SPACE = 12.49/ 952.0 MB, EXMEM = 14.83 MB

++ PROCESSING ELEMENT STIFFNESS MATRIX. 8:38:30  
 ++ PROCESSING GLOBAL STIFFNESS MATRIX. 8:38:31  
 ++ PROCESSING TRIANGULAR FACTORIZATION. 8:38:31

\*\*\*WARNING - IMPROPER LOAD WILL CAUSE INSTABILITY AT JOINT 57 \*  
 DIRECTION = FZ PROBABLE CAUSE MODELING PROBLEM 0.727E-11

++ CALCULATING JOINT DISPLACEMENTS. 8:38:32  
 ++ CALCULATING MEMBER FORCES. 8:38:33

88. PRINT MATERIAL PROPERTIES ALL

\* PROGRAM RECOVERED FROM INSTABILITY

## MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
1	29000000.0	11153846.0	0.28299999	0.00000000
2	29000000.0	11153846.0	0.28299999	0.00000000
3	29000000.0	11153846.0	0.28299999	0.00000000
4	29000000.0	11153846.0	0.28299999	0.00000000
5	29000000.0	11153846.0	0.28299999	0.00000000
6	29000000.0	11153846.0	0.28299999	0.00000000
7	29000000.0	11153846.0	0.28299999	0.00000000
8	29000000.0	11153846.0	0.28299999	0.00000000
9	29000000.0	11153846.0	0.28299999	0.00000000
10	29000000.0	11153846.0	0.28299999	0.00000000
11	29000000.0	11153846.0	0.28299999	0.00000000
12	29000000.0	11153846.0	0.28299999	0.00000000
13	29000000.0	11153846.0	0.28299999	0.00000000
14	29000000.0	11153846.0	0.28299999	0.00000000
15	29000000.0	11153846.0	0.28299999	0.00000000
16	29000000.0	11153846.0	0.28299999	0.00000000
17	29000000.0	11153846.0	0.28299999	0.00000000
18	29000000.0	11153846.0	0.28299999	0.00000000
19	29000000.0	11153846.0	0.28299999	0.00000000
20	29000000.0	11153846.0	0.28299999	0.00000000
21	29000000.0	11153846.0	0.28299999	0.00000000
22	29000000.0	11153846.0	0.28299999	0.00000000
23	29000000.0	11153846.0	0.28299999	0.00000000
24	29000000.0	11153846.0	0.28299999	0.00000000
25	29000000.0	11153846.0	0.28299999	0.00000000
26	29000000.0	11153846.0	0.28299999	0.00000000
27	29000000.0	11153846.0	0.28299999	0.00000000
28	29000000.0	11153846.0	0.28299999	0.00000000
29	29000000.0	11153846.0	0.28299999	0.00000000
30	29000000.0	11153846.0	0.28299999	0.00000000
31	29000000.0	11153846.0	0.28299999	0.00000000
32	29000000.0	11153846.0	0.28299999	0.00000000
33	29000000.0	11153846.0	0.28299999	0.00000000
34	29000000.0	11153846.0	0.28299999	0.00000000
35	29000000.0	11153846.0	0.28299999	0.00000000
36	29000000.0	11153846.0	0.28299999	0.00000000
37	29000000.0	11153846.0	0.28299999	0.00000000
38	29000000.0	11153846.0	0.28299999	0.00000000
39	29000000.0	11153846.0	0.28299999	0.00000000
40	29000000.0	11153846.0	0.28299999	0.00000000
41	29000000.0	11153846.0	0.28299999	0.00000000
42	29000000.0	11153846.0	0.28299999	0.00000000
43	29000000.0	11153846.0	0.28299999	0.00000000
44	29000000.0	11153846.0	0.28299999	0.00000000
45	29000000.0	11153846.0	0.28299999	0.00000000
46	29000000.0	11153846.0	0.28299999	0.00000000

## MATERIAL PROPERTIES.

ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
47	29000000.0	11153846.0	0.28299999	0.00000000
48	29000000.0	11153846.0	0.28299999	0.00000000
49	29000000.0	11153846.0	0.28299999	0.00000000
50	29000000.0	11153846.0	0.28299999	0.00000000
51	29000000.0	11153846.0	0.28299999	0.00000000
52	29000000.0	11153846.0	0.28299999	0.00000000
53	29000000.0	11153846.0	0.28299999	0.00000000
54	29000000.0	11153846.0	0.28299999	0.00000000
55	29000000.0	11153846.0	0.28299999	0.00000000
56	29000000.0	11153846.0	0.28299999	0.00000000
57	29000000.0	11153846.0	0.28299999	0.00000000
58	29000000.0	11153846.0	0.28299999	0.00000000
59	29000000.0	11153846.0	0.28299999	0.00000000
60	29000000.0	11153846.0	0.28299999	0.00000000
61	29000000.0	11153846.0	0.28299999	0.00000000
62	29000000.0	11153846.0	0.28299999	0.00000000
63	29000000.0	11153846.0	0.28299999	0.00000000
64	29000000.0	11153846.0	0.28299999	0.00000000
65	29000000.0	11153846.0	0.28299999	0.00000000
66	29000000.0	11153846.0	0.28299999	0.00000000
67	29000000.0	11153846.0	0.28299999	0.00000000
68	29000000.0	11153846.0	0.28299999	0.00000000
69	29000000.0	11153846.0	0.28299999	0.00000000
70	29000000.0	11153846.0	0.28299999	0.00000000
71	29000000.0	11153846.0	0.28299999	0.00000000
72	29000000.0	11153846.0	0.28299999	0.00000000
73	29000000.0	11153846.0	0.28299999	0.00000000
74	29000000.0	11153846.0	0.28299999	0.00000000
75	9999999.0	3999999.8	0.09548600	0.00000000
76	29000000.0	11153846.0	0.28299999	0.00000000
77	29000000.0	11153846.0	0.28299999	0.00000000
78	9999999.0	3999999.8	0.09548600	0.00000000
79	9999999.0	3999999.8	0.09548600	0.00000000
80	9999999.0	3999999.8	0.09548600	0.00000000
81	9999999.0	3999999.8	0.09548600	0.00000000
82	9999999.0	3999999.8	0.09548600	0.00000000
83	9999999.0	3999999.8	0.09548600	0.00000000
84	9999999.0	3999999.8	0.09548600	0.00000000
85	9999999.0	3999999.8	0.09548600	0.00000000
86	9999999.0	3999999.8	0.09548600	0.00000000
87	9999999.0	3999999.8	0.09548600	0.00000000
88	29000000.0	11153846.0	0.28299999	0.00000000
89	29000000.0	11153846.0	0.28299999	0.00000000
90	9999999.0	3999999.8	0.09548600	0.00000000
91	9999999.0	3999999.8	0.09548600	0.00000000
92	9999999.0	3999999.8	0.09548600	0.00000000

## MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
93	9999999.0	3999999.8	0.09548600	0.00000000
94	9999999.0	3999999.8	0.09548600	0.00000000
95	9999999.0	3999999.8	0.09548600	0.00000000
96	9999999.0	3999999.8	0.09548600	0.00000000
97	9999999.0	3999999.8	0.09548600	0.00000000
98	9999999.0	3999999.8	0.09548600	0.00000000
100	29000000.0	11153846.0	0.28299999	0.00000000
101	29000000.0	11153846.0	0.28299999	0.00000000
102	29000000.0	11153846.0	0.28299999	0.00000000
103	29000000.0	11153846.0	0.28299999	0.00000000
104	29000000.0	11153846.0	0.28299999	0.00000000
105	29000000.0	11153846.0	0.28299999	0.00000000
106	29000000.0	11153846.0	0.28299999	0.00000000
107	29000000.0	11153846.0	0.28299999	0.00000000
108	29000000.0	11153846.0	0.28299999	0.00000000
109	29000000.0	11153846.0	0.28299999	0.00000000
110	29000000.0	11153846.0	0.28299999	0.00000000
111	29000000.0	11153846.0	0.28299999	0.00000000
112	9999999.0	3999999.8	0.09548600	0.00000000
113	9999999.0	3999999.8	0.09548600	0.00000000
114	9999999.0	3999999.8	0.09548600	0.00000000
115	9999999.0	3999999.8	0.09548600	0.00000000
116	29000000.0	11153846.0	0.28299999	0.00000000
117	29000000.0	11153846.0	0.28299999	0.00000000
118	29000000.0	11153846.0	0.28299999	0.00000000
119	29000000.0	11153846.0	0.28299999	0.00000000
120	29000000.0	11153846.0	0.28299999	0.00000000
121	29000000.0	11153846.0	0.28299999	0.00000000
122	29000000.0	11153846.0	0.28299999	0.00000000
123	29000000.0	11153846.0	0.28299999	0.00000000
124	29000000.0	11153846.0	0.28299999	0.00000000
125	29000000.0	11153846.0	0.28299999	0.00000000
126	29000000.0	11153846.0	0.28299999	0.00000000
127	29000000.0	11153846.0	0.28299999	0.00000000
128	29000000.0	11153846.0	0.28299999	0.00000000
129	29000000.0	11153846.0	0.28299999	0.00000000
130	29000000.0	11153846.0	0.28299999	0.00000000
131	29000000.0	11153846.0	0.28299999	0.00000000
132	29000000.0	11153846.0	0.28299999	0.00000000
133	29000000.0	11153846.0	0.28299999	0.00000000
134	29000000.0	11153846.0	0.28299999	0.00000000
135	29000000.0	11153846.0	0.28299999	0.00000000
136	29000000.0	11153846.0	0.28299999	0.00000000
137	29000000.0	11153846.0	0.28299999	0.00000000
138	29000000.0	11153846.0	0.28299999	0.00000000
139	29000000.0	11153846.0	0.28299999	0.00000000

## MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
140	29000000.0	11153846.0	0.28299999	0.00000000
141	29000000.0	11153846.0	0.28299999	0.00000000
142	29000000.0	11153846.0	0.28299999	0.00000000
143	29000000.0	11153846.0	0.28299999	0.00000000
144	29000000.0	11153846.0	0.28299999	0.00000000
145	29000000.0	11153846.0	0.28299999	0.00000000
146	29000000.0	11153846.0	0.28299999	0.00000000
147	29000000.0	11153846.0	0.28299999	0.00000000
148	29000000.0	11153846.0	0.28299999	0.00000000
149	29000000.0	11153846.0	0.28299999	0.00000000
150	29000000.0	11153846.0	0.28299999	0.00000000
151	29000000.0	11153846.0	0.28299999	0.00000000
152	29000000.0	11153846.0	0.28299999	0.00000000
153	29000000.0	11153846.0	0.28299999	0.00000000
154	29000000.0	11153846.0	0.28299999	0.00000000
155	29000000.0	11153846.0	0.28299999	0.00000000
156	29000000.0	11153846.0	0.28299999	0.00000000
157	29000000.0	11153846.0	0.28299999	0.00000000

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

89. PRINT MEMBER INFORMATION ALL

## MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
1	1	2	36.000	0.00	
2	2	3	24.000	0.00	
3	3	4	24.000	0.00	
4	4	5	18.333	0.00	
5	5	6	9.167	0.00	
6	6	7	9.167	0.00	
7	7	8	18.333	0.00	
8	8	9	24.000	0.00	
9	9	10	24.000	0.00	
10	10	11	36.000	0.00	
11	11	12	26.500	0.00	
12	12	13	24.000	0.00	
13	13	14	24.000	0.00	
14	14	15	24.000	0.00	
15	15	16	13.000	0.00	
16	16	17	13.000	0.00	
17	17	18	24.000	0.00	
18	18	19	24.000	0.00	
19	19	20	24.000	0.00	
20	20	21	26.500	0.00	
21	21	22	36.000	0.00	
22	22	23	24.000	0.00	
23	23	24	24.000	0.00	
24	24	25	18.333	0.00	
25	25	26	9.167	0.00	
26	26	27	9.167	0.00	
27	27	28	18.333	0.00	
28	28	29	24.000	0.00	
29	29	30	24.000	0.00	
30	30	31	36.000	0.00	
31	31	32	26.500	0.00	
32	32	33	24.000	0.00	
33	33	34	24.000	0.00	
34	34	35	24.000	0.00	
35	35	36	13.000	0.00	
36	36	37	13.000	0.00	
37	37	38	24.000	0.00	
38	38	39	24.000	0.00	
39	39	40	24.000	0.00	
40	40	1	26.500	0.00	
41	2	41	26.500	0.00	
42	41	42	9.500	0.00	
43	42	43	14.500	0.00	
44	43	44	24.000	0.00	
45	44	45	24.000	0.00	
46	45	46	26.000	0.00	

## MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
47	46	47	24.000	0.00	
48	47	48	24.000	0.00	
49	48	49	14.500	0.00	
50	49	50	9.500	0.00	
51	50	30	26.500	0.00	
52	10	51	26.500	0.00	
53	51	52	9.500	0.00	
54	52	53	14.500	0.00	
55	53	54	24.000	0.00	
56	54	55	24.000	0.00	
57	55	56	26.000	0.00	
58	56	57	24.000	0.00	
59	57	58	24.000	0.00	
60	58	59	14.500	0.00	
61	59	60	9.500	0.00	
62	60	22	26.500	0.00	
63	59	61	24.000	0.00	
64	61	62	24.000	0.00	
65	62	63	27.500	0.00	
66	63	64	27.500	0.00	
67	64	65	24.000	0.00	
68	65	49	24.000	0.00	
69	42	66	24.000	0.00	
70	66	67	24.000	0.00	
71	67	68	27.500	0.00	
72	68	69	27.500	0.00	
73	69	70	24.000	0.00	
74	70	52	24.000	0.00	
75	3	66	36.000	180.00	000111000111
76	4	67	36.000	0.00	
77	8	69	36.000	0.00	
78	9	70	36.000	180.00	000111000111
79	12	51	36.000	180.00	000111000111
80	13	53	36.000	180.00	000111000111
81	14	54	36.000	180.00	000111000111
82	15	55	36.000	180.00	000111000111
83	17	56	36.000	180.00	000111000111
84	18	57	36.000	180.00	000111000111
85	19	58	36.000	180.00	000111000111
86	20	60	36.000	180.00	000111000111
87	23	61	36.000	180.00	000111000111
88	24	62	36.000	0.00	
89	28	64	36.000	0.00	
90	29	65	36.000	180.00	000111000111
91	32	50	36.000	180.00	000111000111
92	33	48	36.000	180.00	000111000111

## MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
93	34	47	36.000	180.00	000111000111
94	35	46	36.000	180.00	000111000111
95	37	45	36.000	180.00	000111000111
96	38	44	36.000	180.00	000111000111
97	39	43	36.000	180.00	000111000111
98	40	41	36.000	180.00	000111000111
100	1	80	48.000	0.00	
101	80	100	36.000	0.00	
102	100	104	6.000	0.00	
103	11	86	48.000	0.00	
104	86	101	36.000	0.00	
105	101	105	6.000	0.00	
106	21	90	48.000	0.00	
107	90	102	36.000	0.00	
108	102	106	6.000	0.00	
109	31	96	48.000	0.00	
110	96	103	36.000	0.00	
111	103	107	6.000	0.00	
112	104	108	102.000	0.00	
113	105	109	102.000	0.00	
114	106	110	102.000	0.00	
115	107	111	102.000	0.00	
116	80	81	36.000	0.00	
117	81	82	66.333	0.00	
118	82	83	9.167	0.00	
119	83	84	9.167	0.00	
120	84	85	66.333	0.00	
121	85	86	36.000	0.00	
122	86	87	36.000	0.00	
123	87	88	75.500	0.00	
124	88	89	75.500	0.00	
125	89	90	36.000	0.00	
126	90	91	36.000	0.00	
127	91	92	66.333	0.00	
128	92	93	9.167	0.00	
129	93	94	9.167	0.00	
130	94	95	66.333	0.00	
131	95	96	36.000	0.00	
132	96	97	36.000	0.00	
133	97	98	75.500	0.00	
134	98	99	75.500	0.00	
135	99	80	36.000	0.00	
136	1	82	113.031	0.00	
137	11	84	113.031	0.00	
138	11	88	121.393	0.00	
139	21	88	121.393	0.00	



MEMBER INFORMATION  
-----

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
140	21	92	113.031	0.00	
141	31	94	113.031	0.00	
142	31	98	121.393	0.00	
143	1	98	121.393	0.00	
144	5	82	48.000	0.00	
145	7	84	48.000	0.00	
146	16	88	48.000	0.00	
147	25	92	48.000	0.00	
148	27	94	48.000	0.00	
149	36	98	48.000	0.00	
150	100	81	50.912	0.00	
151	101	85	50.912	0.00	
152	101	87	50.912	0.00	
153	102	89	50.912	0.00	
154	102	91	50.912	0.00	
155	103	95	50.912	0.00	
156	103	97	50.912	0.00	
157	100	99	50.912	0.00	

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

90. PRINT JOINT COORDINATES ALL

## JOINT COORDINATES

-----  
COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
1	0.000	0.000	0.000
2	36.000	0.000	0.000
3	60.000	0.000	0.000
4	84.000	0.000	0.000
5	102.333	0.000	0.000
6	111.500	0.000	0.000
7	120.667	0.000	0.000
8	139.000	0.000	0.000
9	163.000	0.000	0.000
10	187.000	0.000	0.000
11	223.000	0.000	0.000
12	223.000	0.000	26.500
13	223.000	0.000	50.500
14	223.000	0.000	74.500
15	223.000	0.000	98.500
16	223.000	0.000	111.500
17	223.000	0.000	124.500
18	223.000	0.000	148.500
19	223.000	0.000	172.500
20	223.000	0.000	196.500
21	223.000	0.000	223.000
22	187.000	0.000	223.000
23	163.000	0.000	223.000
24	139.000	0.000	223.000
25	120.667	0.000	223.000
26	111.500	0.000	223.000
27	102.333	0.000	223.000
28	84.000	0.000	223.000
29	60.000	0.000	223.000
30	36.000	0.000	223.000
31	0.000	0.000	223.000
32	0.000	0.000	196.500
33	0.000	0.000	172.500
34	0.000	0.000	148.500
35	0.000	0.000	124.500
36	0.000	0.000	111.500
37	0.000	0.000	98.500
38	0.000	0.000	74.500
39	0.000	0.000	50.500
40	0.000	0.000	26.500
41	36.000	0.000	26.500
42	36.000	0.000	36.000
43	36.000	0.000	50.500
44	36.000	0.000	74.500
45	36.000	0.000	98.500
46	36.000	0.000	124.500
47	36.000	0.000	148.500

## JOINT COORDINATES

-----  
COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
48	36.000	0.000	172.500
49	36.000	0.000	187.000
50	36.000	0.000	196.500
51	187.000	0.000	26.500
52	187.000	0.000	36.000
53	187.000	0.000	50.500
54	187.000	0.000	74.500
55	187.000	0.000	98.500
56	187.000	0.000	124.500
57	187.000	0.000	148.500
58	187.000	0.000	172.500
59	187.000	0.000	187.000
60	187.000	0.000	196.500
61	163.000	0.000	187.000
62	139.000	0.000	187.000
63	111.500	0.000	187.000
64	84.000	0.000	187.000
65	60.000	0.000	187.000
66	60.000	0.000	36.000
67	84.000	0.000	36.000
68	111.500	0.000	36.000
69	139.000	0.000	36.000
70	163.000	0.000	36.000
80	0.000	-48.000	0.000
81	36.000	-48.000	0.000
82	102.333	-48.000	0.000
83	111.500	-48.000	0.000
84	120.667	-48.000	0.000
85	187.000	-48.000	0.000
86	223.000	-48.000	0.000
87	223.000	-48.000	36.000
88	223.000	-48.000	111.500
89	223.000	-48.000	187.000
90	223.000	-48.000	223.000
91	187.000	-48.000	223.000
92	120.667	-48.000	223.000
93	111.500	-48.000	223.000
94	102.333	-48.000	223.000
95	36.000	-48.000	223.000
96	0.000	-48.000	223.000
97	0.000	-48.000	187.000
98	0.000	-48.000	111.500
99	0.000	-48.000	36.000
100	0.000	-84.000	0.000
101	223.000	-84.000	0.000
102	223.000	-84.000	223.000
103	0.000	-84.000	223.000

## JOINT COORDINATES

-----  
COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
104	0.000	-90.000	0.000
105	223.000	-90.000	0.000
106	223.000	-90.000	223.000
107	0.000	-90.000	223.000
108	0.000	-192.000	0.000
109	223.000	-192.000	0.000
110	223.000	-192.000	223.000
111	0.000	-192.000	223.000

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

## 91. PRINT SUPPORT INFORMATION ALL

SUPPORT INFORMATION (1=FIXED, 0=RELEASED)

-----  
UNITS FOR SPRING CONSTANTS ARE POUN INCH DEGREES

JOINT	FORCE-X/ KFX	FORCE-Y/ KFY	FORCE-Z/ KFZ	MOM-X/ KMX	MOM-Y/ KMY	MOM-Z/ KMZ
108	0	1	0	0	1	0
	0.0	0.0	0.0	0.0	0.0	0.0
109	0	1	0	0	1	0
	0.0	0.0	0.0	0.0	0.0	0.0
110	0	1	0	0	1	0
	0.0	0.0	0.0	0.0	0.0	0.0
111	0	1	0	0	1	0
	0.0	0.0	0.0	0.0	0.0	0.0

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

## 92. PRINT ANALYSIS RESULTS

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
1	1	0.00012	-0.01037	0.00086	0.00046	0.00003	-0.00042
2	1	-0.00021	-0.02588	0.00005	0.00214	-0.00001	-0.00026
3	1	-0.00043	-0.02750	0.00094	0.00222	-0.00005	0.00009
4	1	-0.00065	-0.02306	0.00218	0.00231	-0.00004	0.00022
5	1	-0.00082	-0.01947	0.00281	0.00219	-0.00002	0.00011
6	1	-0.00091	-0.01897	0.00289	0.00219	0.00000	0.00000
7	1	-0.00099	-0.01947	0.00281	0.00219	0.00002	-0.00011
8	1	-0.00116	-0.02306	0.00218	0.00231	0.00004	-0.00022
9	1	-0.00138	-0.02750	0.00095	0.00222	0.00005	-0.00009
10	1	-0.00160	-0.02588	0.00005	0.00214	0.00001	0.00026
11	1	-0.00193	-0.01037	0.00087	0.00046	-0.00003	0.00042
12	1	-0.00138	-0.02009	0.00067	0.00025	0.00003	0.00039
13	1	-0.00073	-0.02355	0.00048	0.00004	0.00002	0.00037
14	1	-0.00049	-0.02238	0.00030	-0.00011	0.00000	0.00034
15	1	-0.00049	-0.01928	0.00011	-0.00010	0.00000	0.00032
16	1	-0.00050	-0.01841	0.00001	0.00000	0.00000	0.00030
17	1	-0.00049	-0.01928	-0.00009	0.00010	0.00000	0.00032
18	1	-0.00050	-0.02238	-0.00027	0.00011	0.00000	0.00034
19	1	-0.00073	-0.02355	-0.00045	-0.00004	-0.00002	0.00037
20	1	-0.00139	-0.02009	-0.00064	-0.00025	-0.00003	0.00039
21	1	-0.00194	-0.01037	-0.00084	-0.00046	0.00003	0.00042
22	1	-0.00161	-0.02588	-0.00003	-0.00214	-0.00001	0.00026
23	1	-0.00139	-0.02750	-0.00092	-0.00222	-0.00005	-0.00009
24	1	-0.00117	-0.02306	-0.00216	-0.00231	-0.00004	-0.00022
25	1	-0.00100	-0.01947	-0.00279	-0.00219	-0.00002	-0.00011
26	1	-0.00091	-0.01897	-0.00287	-0.00219	0.00000	0.00000
27	1	-0.00083	-0.01947	-0.00279	-0.00219	0.00002	0.00011
28	1	-0.00066	-0.02306	-0.00216	-0.00231	0.00004	0.00022
29	1	-0.00044	-0.02750	-0.00093	-0.00222	0.00005	0.00009
30	1	-0.00022	-0.02588	-0.00003	-0.00214	0.00001	-0.00026
31	1	0.00011	-0.01037	-0.00085	-0.00046	-0.00003	-0.00042
32	1	-0.00043	-0.02009	-0.00064	-0.00025	0.00003	-0.00039
33	1	-0.00109	-0.02355	-0.00046	-0.00004	0.00002	-0.00037
34	1	-0.00132	-0.02238	-0.00028	0.00011	0.00000	-0.00034
35	1	-0.00133	-0.01928	-0.00009	0.00010	0.00000	-0.00032
36	1	-0.00131	-0.01841	0.00001	0.00000	0.00000	-0.00030
37	1	-0.00133	-0.01928	0.00011	-0.00010	0.00000	-0.00032
38	1	-0.00132	-0.02238	0.00029	-0.00011	0.00000	-0.00034
39	1	-0.00108	-0.02355	0.00048	0.00004	-0.00002	-0.00037
40	1	-0.00043	-0.02009	0.00066	0.00025	-0.00003	-0.00039
41	1	-0.00060	-0.08498	0.00004	0.00220	-0.00002	-0.00040
42	1	-0.00086	-0.10553	0.00003	0.00209	-0.00002	-0.00045
43	1	-0.00111	-0.13418	0.00003	0.00183	-0.00001	-0.00045
44	1	-0.00131	-0.17101	0.00002	0.00120	0.00000	-0.00045
45	1	-0.00134	-0.19096	0.00001	0.00044	0.00000	-0.00045
46	1	-0.00134	-0.19096	0.00000	-0.00044	0.00000	-0.00045
47	1	-0.00132	-0.17101	0.00000	-0.00120	0.00000	-0.00045
48	1	-0.00112	-0.13418	-0.00001	-0.00183	0.00001	-0.00045

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
49	1	-0.00087	-0.10553	-0.00002	-0.00209	0.00002	-0.00045
50	1	-0.00060	-0.08498	-0.00002	-0.00220	0.00002	-0.00040
51	1	-0.00121	-0.08498	0.00004	0.00220	0.00002	0.00040
52	1	-0.00095	-0.10553	0.00004	0.00209	0.00002	0.00045
53	1	-0.00070	-0.13418	0.00003	0.00183	0.00001	0.00045
54	1	-0.00050	-0.17101	0.00003	0.00120	0.00000	0.00045
55	1	-0.00047	-0.19096	0.00002	0.00044	0.00000	0.00045
56	1	-0.00047	-0.19096	0.00001	-0.00044	0.00000	0.00045
57	1	-0.00050	-0.17101	0.00000	-0.00120	0.00000	0.00045
58	1	-0.00070	-0.13418	-0.00001	-0.00183	-0.00001	0.00045
59	1	-0.00095	-0.10553	-0.00001	-0.00209	-0.00002	0.00045
60	1	-0.00122	-0.08498	-0.00002	-0.00220	-0.00002	0.00040
61	1	-0.00094	-0.11778	-0.00096	-0.00248	-0.00005	0.00047
62	1	-0.00092	-0.12606	-0.00215	-0.00288	-0.00002	0.00023
63	1	-0.00091	-0.12939	-0.00249	-0.00288	0.00000	0.00000
64	1	-0.00090	-0.12606	-0.00215	-0.00288	0.00002	-0.00023
65	1	-0.00088	-0.11778	-0.00096	-0.00248	0.00005	-0.00047
66	1	-0.00088	-0.11778	0.00098	0.00248	-0.00005	-0.00047
67	1	-0.00089	-0.12606	0.00217	0.00288	-0.00002	-0.00023
68	1	-0.00091	-0.12939	0.00251	0.00288	0.00000	0.00000
69	1	-0.00092	-0.12606	0.00217	0.00288	0.00002	0.00023
70	1	-0.00093	-0.11778	0.00098	0.00248	0.00005	0.00047
80	1	-0.00145	-0.00963	-0.00040	-0.00004	0.00021	0.00002
81	1	-0.00131	-0.01220	-0.01865	0.00016	0.00074	-0.00013
82	1	-0.00112	-0.01906	-0.06606	0.00097	0.00026	0.00006
83	1	-0.00091	-0.01881	-0.06724	0.00097	0.00000	0.00000
84	1	-0.00069	-0.01906	-0.06606	0.00097	-0.00026	-0.00006
85	1	-0.00050	-0.01220	-0.01864	0.00016	-0.00074	0.00013
86	1	-0.00036	-0.00963	-0.00040	-0.00004	-0.00021	-0.00002
87	1	-0.00326	-0.01171	-0.00024	0.00011	0.00002	0.00003
88	1	0.00463	-0.01784	0.00001	0.00000	0.00000	0.00005
89	1	-0.00326	-0.01171	0.00027	-0.00011	-0.00002	0.00003
90	1	-0.00037	-0.00963	0.00043	0.00004	0.00021	-0.00002
91	1	-0.00050	-0.01220	0.01867	-0.00016	0.00074	0.00013
92	1	-0.00070	-0.01906	0.06608	-0.00097	0.00026	-0.00006
93	1	-0.00091	-0.01881	0.06726	-0.00097	0.00000	0.00000
94	1	-0.00112	-0.01906	0.06608	-0.00097	-0.00026	0.00006
95	1	-0.00132	-0.01220	0.01866	-0.00016	-0.00074	-0.00013
96	1	-0.00146	-0.00963	0.00042	0.00004	-0.00021	0.00002
97	1	0.00144	-0.01171	0.00027	-0.00011	0.00002	-0.00003
98	1	-0.00644	-0.01784	0.00001	0.00000	0.00000	-0.00005
99	1	0.00145	-0.01171	-0.00025	0.00011	-0.00002	-0.00003
100	1	-0.00438	-0.00905	-0.00283	0.00011	0.00023	-0.00012
101	1	0.00257	-0.00905	-0.00282	0.00011	-0.00023	0.00012
102	1	0.00256	-0.00905	0.00285	-0.00011	0.00023	0.00012
103	1	-0.00438	-0.00905	0.00284	-0.00011	-0.00023	-0.00012
104	1	-0.00511	-0.00895	-0.00347	0.00011	0.00023	-0.00012
105	1	0.00330	-0.00895	-0.00346	0.00011	-0.00023	0.00012

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
106	1	0.00329	-0.00895	0.00349	-0.00011	0.00023	0.00012
107	1	-0.00512	-0.00895	0.00348	-0.00011	-0.00023	-0.00012
108	1	-0.01760	0.00000	-0.01435	0.00011	0.00000	-0.00012
109	1	0.01579	0.00000	-0.01434	0.00011	0.00000	0.00012
110	1	0.01578	0.00000	0.01437	-0.00011	0.00000	0.00012
111	1	-0.01761	0.00000	0.01437	-0.00011	0.00000	-0.00012

SUPPORT REACTIONS -UNIT POUN INCH      STRUCTURE TYPE = SPACE

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
108	1	0.00	1219.11	0.00	0.00	-88.55	0.00
109	1	0.00	1219.10	0.00	0.00	88.57	0.00
110	1	0.00	1219.10	0.00	0.00	-88.55	0.00
111	1	0.00	1219.10	0.00	0.00	88.57	0.00



## MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	1	1	833.35	333.56	16.82	-6178.02	-167.52	3696.44
		2	-833.35	-253.87	-16.82	6178.02	-438.09	6877.31
2	1	2	837.10	-115.98	-14.75	-491.53	416.62	-7571.42
		3	-837.10	137.30	14.75	491.53	-62.60	4532.09
3	1	3	837.10	-181.49	-9.24	-491.53	62.60	-4532.09
		4	-837.10	202.82	9.24	491.53	159.10	-79.54
4	1	4	842.06	-280.02	-14.98	878.28	-59.44	-86.68
		5	-842.06	296.31	14.98	-878.28	334.06	-5196.25
5	1	5	832.85	8.15	0.00	-0.01	-257.39	4952.47
		6	-832.85	-0.01	0.00	0.01	257.38	-4915.09
6	1	6	832.85	0.00	0.00	0.00	-257.39	4915.10
		7	-832.85	8.15	0.00	0.00	257.39	-4952.46
7	1	7	842.06	296.31	14.98	-878.29	-334.06	5196.24
		8	-842.06	-280.02	-14.98	878.29	59.44	86.66
8	1	8	837.10	202.82	9.24	491.53	-159.10	79.55
		9	-837.10	-181.49	-9.24	-491.53	-62.60	4532.11
9	1	9	837.10	137.30	14.75	491.53	62.60	-4532.11
		10	-837.10	-115.97	-14.75	-491.53	-416.61	7571.40
10	1	10	833.36	-253.87	-16.82	6178.02	438.09	-6877.31
		11	-833.36	333.56	16.82	-6178.02	167.52	-3696.44
11	1	11	698.75	65.53	29.22	140.26	-701.48	-2445.48
		12	-698.75	-41.98	-29.22	-140.26	-72.80	3869.94
12	1	12	698.75	-4.46	1.87	140.26	72.79	-3869.95
		13	-698.75	25.79	-1.87	-140.26	-117.65	3507.04
13	1	13	698.75	-69.97	-2.79	140.26	117.65	-3507.04
		14	-698.75	91.30	2.79	-140.26	-50.69	1571.80
14	1	14	698.75	-135.49	-1.74	140.26	50.69	-1571.81
		15	-698.75	156.81	1.74	-140.26	-8.87	-1935.79
15	1	15	698.75	-202.80	-3.57	140.26	8.87	1935.74
		16	-698.75	214.36	3.57	-140.26	37.57	-4647.30

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
16	1	16	698.75	214.36	3.57	-140.26	-37.57	4647.30
		17	-698.75	-202.80	-3.57	140.26	-8.87	-1935.75
17	1	17	698.75	156.81	1.74	-140.26	8.87	1935.80
		18	-698.75	-135.49	-1.74	140.26	-50.69	1571.81
18	1	18	698.75	91.30	2.79	-140.26	50.69	-1571.80
		19	-698.75	-69.97	-2.79	140.26	-117.65	3507.03
19	1	19	698.75	25.78	-1.87	-140.26	117.65	-3507.03
		20	-698.75	-4.46	1.87	140.26	-72.79	3869.96
20	1	20	698.75	-41.98	-29.22	-140.26	72.79	-3869.93
		21	-698.75	65.53	29.22	140.26	701.48	2445.48
21	1	21	833.35	333.56	16.82	-6178.02	-167.52	3696.44
		22	-833.35	-253.87	-16.82	6178.02	-438.09	6877.32
22	1	22	837.10	-115.98	-14.75	-491.53	416.62	-7571.46
		23	-837.10	137.31	14.75	491.53	-62.60	4532.05
23	1	23	837.10	-181.49	-9.24	-491.53	62.60	-4532.09
		24	-837.10	202.82	9.24	491.53	159.09	-79.55
24	1	24	842.06	-280.02	-14.98	878.28	-59.44	-86.64
		25	-842.06	296.31	14.98	-878.28	334.06	-5196.21
25	1	25	832.85	8.14	0.00	0.00	-257.39	4952.43
		26	-832.85	0.00	0.00	0.00	257.39	-4915.13
26	1	26	832.85	0.00	0.00	0.00	-257.39	4915.14
		27	-832.85	8.14	0.00	0.00	257.39	-4952.43
27	1	27	842.06	296.31	14.98	-878.28	-334.06	5196.22
		28	-842.06	-280.02	-14.98	878.28	59.44	86.66
28	1	28	837.10	202.82	9.24	491.53	-159.10	79.57
		29	-837.10	-181.49	-9.24	-491.53	-62.60	4532.12
29	1	29	837.10	137.30	14.75	491.53	62.60	-4532.12
		30	-837.10	-115.97	-14.75	-491.53	-416.61	7571.40
30	1	30	833.35	-253.87	-16.82	6178.02	438.09	-6877.30
		31	-833.35	333.56	16.82	-6178.02	167.52	-3696.42
31	1	31	698.75	65.53	29.22	140.26	-701.48	-2445.48
		32	-698.75	-41.98	-29.22	-140.26	-72.79	3869.93

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
32	1	32	698.75	-4.46	1.87	140.26	72.80	-3869.94
		33	-698.75	25.78	-1.87	-140.26	-117.65	3507.05
33	1	33	698.75	-69.97	-2.79	140.26	117.65	-3507.05
		34	-698.75	91.30	2.79	-140.26	-50.69	1571.79
34	1	34	698.75	-135.49	-1.74	140.26	50.69	-1571.80
		35	-698.75	156.81	1.74	-140.26	-8.87	-1935.78
35	1	35	698.75	-202.80	-3.57	140.26	8.87	1935.78
		36	-698.75	214.35	3.57	-140.26	37.57	-4647.28
36	1	36	698.75	214.35	3.57	-140.26	-37.57	4647.27
		37	-698.75	-202.80	-3.57	140.26	-8.87	-1935.78
37	1	37	698.75	156.81	1.74	-140.26	8.87	1935.78
		38	-698.75	-135.49	-1.74	140.26	-50.69	1571.79
38	1	38	698.75	91.30	2.79	-140.26	50.69	-1571.80
		39	-698.75	-69.97	-2.79	140.26	-117.65	3507.04
39	1	39	698.75	25.78	-1.87	-140.26	117.65	-3507.04
		40	-698.75	-4.46	1.87	140.26	-72.79	3869.95
40	1	40	698.75	-41.98	-29.22	-140.26	72.79	-3869.95
		1	-698.75	65.53	29.22	140.26	701.48	2445.47
41	1	2	31.57	369.84	3.75	694.11	21.48	5686.48
		41	-31.57	-314.50	-3.75	-694.11	-120.74	3381.02
42	1	41	31.57	268.08	-23.60	694.11	120.74	-3380.96
		42	-31.57	-259.63	23.60	-694.11	103.49	5887.55
43	1	42	31.80	201.46	5.44	0.00	-142.29	-6286.47
		43	-31.80	-188.57	-5.44	0.00	63.39	9114.08
44	1	43	31.80	144.38	0.78	0.00	-63.39	-9114.13
		44	-31.80	-123.05	-0.78	0.00	44.62	12323.27
45	1	44	31.80	78.86	1.83	0.00	-44.62	-12323.29
		45	-31.80	-57.54	-1.83	0.00	0.70	13960.17
46	1	45	31.80	11.55	0.00	0.00	-0.70	-13960.21
		46	-31.80	11.55	0.00	0.00	0.70	13960.14
47	1	46	31.80	-57.54	-1.83	0.00	-0.70	-13960.16
		47	-31.80	78.87	1.83	0.00	44.62	12323.28

MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
48	1	47	31.80	-123.05	-0.78	0.00	-44.62	-12323.26
		48	-31.80	144.38	0.78	0.00	63.39	9114.14
49	1	48	31.80	-188.59	-5.44	0.00	-63.39	-9114.19
		49	-31.80	201.47	5.44	0.00	142.29	6286.36
50	1	49	31.57	-259.63	23.60	-694.11	-103.49	-5887.60
		50	-31.57	268.08	-23.60	694.11	-120.74	3380.98
51	1	50	31.57	-314.50	-3.75	-694.11	120.74	-3381.07
		30	-31.57	369.85	3.75	694.11	-21.48	-5686.53
52	1	10	31.57	369.84	-3.75	-694.11	-21.48	5686.48
		51	-31.57	-314.50	3.75	694.11	120.74	3381.03
53	1	51	31.57	268.08	23.60	-694.11	-120.74	-3380.95
		52	-31.57	-259.63	-23.60	694.11	-103.49	5887.57
54	1	52	31.80	201.45	-5.44	0.00	142.29	-6286.47
		53	-31.80	-188.57	5.44	0.00	-63.39	9114.02
55	1	53	31.80	144.38	-0.78	0.00	63.39	-9114.13
		54	-31.80	-123.05	0.78	0.00	-44.62	12323.28
56	1	54	31.80	78.86	-1.83	0.00	44.62	-12323.33
		55	-31.80	-57.53	1.83	0.00	-0.70	13960.13
57	1	55	31.80	11.55	0.00	0.00	0.70	-13960.18
		56	-31.80	11.55	0.00	0.00	-0.70	13960.17
58	1	56	31.80	-57.54	1.83	0.00	0.70	-13960.19
		57	-31.80	78.87	-1.83	0.00	-44.62	12323.26
59	1	57	31.80	-123.06	0.78	0.00	44.62	-12323.33
		58	-31.80	144.38	-0.78	0.00	-63.39	9114.09
60	1	58	31.80	-188.57	5.44	0.00	63.39	-9114.10
		59	-31.80	201.46	-5.44	0.00	-142.29	6286.45
61	1	59	31.57	-259.61	-23.60	694.11	103.49	-5887.42
		60	-31.57	268.06	23.60	-694.11	120.74	3381.12
62	1	60	31.57	-314.49	3.75	694.11	-120.74	-3380.99
		22	-31.57	369.84	-3.75	-694.11	21.48	-5686.46
63	1	59	29.04	58.16	-0.23	-398.96	38.80	694.10
		61	-29.04	-47.03	0.23	398.96	-33.31	568.18

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
64	1	61	29.04	2.84	-5.74	-398.96	33.31	-568.20
		62	-29.04	8.30	5.74	398.96	104.51	502.64
65	1	62	24.09	12.76	0.00	0.00	-25.70	-336.44
		63	-24.09	0.00	0.00	0.00	25.70	511.94
66	1	63	24.09	0.00	0.00	0.00	-25.70	-511.94
		64	-24.09	12.76	0.00	0.00	25.70	336.44
67	1	64	29.04	8.30	5.74	398.96	-104.51	-502.67
		65	-29.04	2.84	-5.74	-398.96	-33.31	568.18
68	1	65	29.04	-47.03	0.23	398.96	33.31	-568.18
		49	-29.04	58.16	-0.23	-398.96	-38.80	-694.10
69	1	42	29.04	58.17	-0.23	-398.96	38.80	694.11
		66	-29.04	-47.03	0.23	398.96	-33.31	568.18
70	1	66	29.04	2.84	-5.74	-398.96	33.31	-568.19
		67	-29.04	8.30	5.74	398.96	104.51	502.66
71	1	67	24.09	12.76	0.00	0.00	-25.70	-336.44
		68	-24.09	0.00	0.00	0.00	25.70	511.94
72	1	68	24.09	0.00	0.00	0.00	-25.70	-511.94
		69	-24.09	12.76	0.00	0.00	25.70	336.44
73	1	69	29.04	8.30	5.74	398.96	-104.51	-502.66
		70	-29.04	2.84	-5.74	-398.96	-33.31	568.19
74	1	70	29.05	-47.03	0.23	398.96	33.31	-568.21
		52	-29.05	58.17	-0.23	-398.96	-38.80	-694.13
75	1	3	-5.51	-44.19	0.00	0.00	0.00	0.00
		66	5.51	-44.19	0.00	0.00	0.00	0.00
76	1	4	5.74	77.20	4.96	166.22	-99.66	1369.81
		67	-5.74	-21.06	-4.96	-166.22	-78.81	398.96
77	1	8	5.74	77.20	-4.96	-166.22	99.66	1369.81
		69	-5.74	-21.06	4.96	166.22	78.80	398.96
78	1	9	-5.51	-44.19	0.00	0.00	0.00	0.00
		70	5.51	-44.19	0.00	0.00	0.00	0.00
79	1	12	27.35	-46.44	0.00	0.00	0.00	0.00
		51	-27.35	-46.44	0.00	0.00	0.00	0.00

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
80	1	13	4.66	-44.19	0.00	0.00	0.00	0.00
		53	-4.66	-44.19	0.00	0.00	0.00	0.00
81	1	14	-1.05	-44.19	0.00	0.00	0.00	0.00
		54	1.05	-44.19	0.00	0.00	0.00	0.00
82	1	15	1.83	-45.99	0.00	0.00	0.00	0.00
		55	-1.83	-45.99	0.00	0.00	0.00	0.00
83	1	17	1.83	-45.99	0.00	0.00	0.00	0.00
		56	-1.83	-45.99	0.00	0.00	0.00	0.00
84	1	18	-1.05	-44.19	0.00	0.00	0.00	0.00
		57	1.05	-44.19	0.00	0.00	0.00	0.00
85	1	19	4.66	-44.19	0.00	0.00	0.00	0.00
		58	-4.66	-44.19	0.00	0.00	0.00	0.00
86	1	20	27.35	-46.44	0.00	0.00	0.00	0.00
		60	-27.35	-46.44	0.00	0.00	0.00	0.00
87	1	23	-5.51	-44.19	0.00	0.00	0.00	0.00
		61	5.51	-44.19	0.00	0.00	0.00	0.00
88	1	24	5.74	77.20	4.96	166.22	-99.66	1369.81
		62	-5.74	-21.06	-4.96	-166.22	-78.81	398.95
89	1	28	5.74	77.20	-4.96	-166.22	99.66	1369.81
		64	-5.74	-21.06	4.96	166.22	78.80	398.96
90	1	29	-5.51	-44.19	0.00	0.00	0.00	0.00
		65	5.51	-44.19	0.00	0.00	0.00	0.00
91	1	32	27.35	-46.44	0.00	0.00	0.00	0.00
		50	-27.35	-46.44	0.00	0.00	0.00	0.00
92	1	33	4.66	-44.19	0.00	0.00	0.00	0.00
		48	-4.66	-44.19	0.00	0.00	0.00	0.00
93	1	34	-1.05	-44.19	0.00	0.00	0.00	0.00
		47	1.05	-44.19	0.00	0.00	0.00	0.00
94	1	35	1.83	-45.99	0.00	0.00	0.00	0.00
		46	-1.83	-45.99	0.00	0.00	0.00	0.00
95	1	37	1.83	-45.99	0.00	0.00	0.00	0.00
		45	-1.83	-45.99	0.00	0.00	0.00	0.00

MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
96	1	38	-1.05	-44.19	0.00	0.00	0.00	0.00
		44	1.05	-44.19	0.00	0.00	0.00	0.00
97	1	39	4.66	-44.19	0.00	0.00	0.00	0.00
		43	-4.66	-44.19	0.00	0.00	0.00	0.00
98	1	40	27.35	-46.44	0.00	0.00	0.00	0.00
		41	-27.35	-46.44	0.00	0.00	0.00	0.00
100	1	1	1051.92	-103.63	-114.03	296.99	4034.92	-3644.49
		80	-1084.39	103.63	114.03	-296.99	1438.36	-1329.64
101	1	80	1105.33	34.06	36.38	59.00	-1163.49	1118.54
		100	-1129.68	-34.06	-36.38	-59.00	-146.28	107.75
102	1	100	1201.58	0.00	0.00	-88.55	0.00	0.00
		104	-1205.64	0.00	0.00	88.55	0.00	0.00
103	1	11	1051.92	103.63	-114.03	-296.98	4034.92	3644.49
		86	-1084.39	-103.63	114.03	296.98	1438.36	1329.64
104	1	86	1105.33	-34.06	36.38	-58.99	-1163.49	-1118.54
		101	-1129.68	34.06	-36.38	58.99	-146.28	-107.75
105	1	101	1201.62	0.00	0.00	88.57	0.00	0.00
		105	-1205.68	0.00	0.00	-88.57	0.00	0.00
106	1	21	1051.92	103.63	114.03	296.99	-4034.92	3644.49
		90	-1084.39	-103.63	-114.03	-296.99	-1438.36	1329.64
107	1	90	1105.33	-34.06	-36.38	59.00	1163.49	-1118.54
		102	-1129.68	34.06	36.38	-59.00	146.28	-107.75
108	1	102	1201.60	0.00	0.00	-88.55	0.00	0.00
		106	-1205.66	0.00	0.00	88.55	0.00	0.00
109	1	31	1051.92	-103.63	114.03	-296.98	-4034.92	-3644.49
		96	-1084.39	103.63	-114.03	296.98	-1438.36	-1329.64
110	1	96	1105.33	34.06	-36.38	-58.99	1163.49	1118.54
		103	-1129.68	-34.06	36.38	58.99	146.28	107.75
111	1	103	1201.60	0.00	0.00	88.57	0.00	0.00
		107	-1205.66	0.00	0.00	-88.57	0.00	0.00
112	1	104	1205.65	0.00	0.00	-88.55	0.00	0.00
		108	-1219.11	0.00	0.00	88.55	0.00	0.00

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
113	1	105	1205.64	0.00	0.00	88.57	0.00	0.00
		109	-1219.10	0.00	0.00	-88.57	0.00	0.00
114	1	106	1205.64	0.00	0.00	-88.55	0.00	0.00
		110	-1219.10	0.00	0.00	88.55	0.00	0.00
115	1	107	1205.64	0.00	0.00	88.57	0.00	0.00
		111	-1219.10	0.00	0.00	-88.57	0.00	0.00
116	1	80	-140.16	10.20	6.19	-75.08	-410.74	189.96
		81	140.16	2.74	-6.19	75.08	187.97	-55.65
117	1	81	-107.65	15.67	11.91	-162.07	-247.88	200.91
		82	107.65	8.17	-11.91	162.07	-542.02	47.87
118	1	82	-856.94	3.30	0.00	0.00	571.34	132.09
		83	856.94	0.00	0.00	0.00	-571.37	-116.98
119	1	83	-856.94	0.00	0.00	0.00	571.37	116.99
		84	856.94	3.29	0.00	0.00	-571.34	-132.08
120	1	84	-107.65	8.17	-11.91	162.07	542.02	-47.87
		85	107.65	15.67	11.91	-162.07	247.89	-200.91
121	1	85	-140.16	2.74	-6.19	75.08	-187.97	55.65
		86	140.16	10.20	6.19	-75.08	410.74	-189.96
122	1	86	-156.60	10.75	2.47	-21.14	-172.75	199.78
		87	156.60	2.19	-2.47	21.14	83.95	-45.76
123	1	87	-125.93	14.71	4.02	-2.31	-146.35	184.53
		88	125.93	12.43	-4.02	2.31	-157.06	-98.44
124	1	88	-125.94	12.43	-4.02	2.31	157.06	98.44
		89	125.94	14.71	4.02	-2.31	146.36	-184.53
125	1	89	-156.60	2.19	-2.47	21.14	-83.95	45.76
		90	156.60	10.75	2.47	-21.14	172.75	-199.78
126	1	90	-140.16	10.20	6.19	-75.08	-410.74	189.96
		91	140.16	2.74	-6.19	75.08	187.97	-55.65
127	1	91	-107.65	15.67	11.91	-162.07	-247.88	200.91
		92	107.65	8.17	-11.91	162.07	-542.02	47.87
128	1	92	-856.94	3.29	0.00	0.00	571.36	132.08
		93	856.94	0.00	0.00	0.00	-571.34	-116.99



## MEMBER END FORCES      STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
129	1	93	-856.94	0.00	0.00	0.00	571.33	116.99
		94	856.94	3.29	0.00	0.00	-571.38	-132.08
130	1	94	-107.65	8.17	-11.91	162.07	542.02	-47.87
		95	107.65	15.67	11.91	-162.07	247.89	-200.91
131	1	95	-140.16	2.74	-6.19	75.08	-187.97	55.65
		96	140.16	10.20	6.19	-75.08	410.74	-189.96
132	1	96	-156.60	10.75	2.47	-21.14	-172.75	199.78
		97	156.60	2.19	-2.47	21.14	83.95	-45.76
133	1	97	-125.94	14.71	4.02	-2.31	-146.35	184.53
		98	125.94	12.43	-4.02	2.31	-157.06	-98.44
134	1	98	-125.93	12.43	-4.02	2.31	157.06	98.44
		99	125.93	14.71	4.02	-2.31	146.36	-184.53
135	1	99	-156.60	2.19	-2.47	21.14	-83.95	45.76
		80	156.60	10.75	2.47	-21.14	172.75	-199.78
136	1	1	-845.44	16.31	3.07	-42.47	-249.99	143.26
		82	828.19	20.47	-3.07	42.47	-97.16	-378.21
137	1	11	-845.45	16.31	-3.07	42.47	249.99	143.26
		84	828.19	20.47	3.07	-42.47	97.16	-378.21
138	1	11	-665.67	17.22	-0.45	39.14	48.07	157.76
		88	648.42	22.85	0.45	-39.14	6.11	-499.31
139	1	21	-665.67	17.22	0.45	-39.14	-48.07	157.76
		88	648.42	22.85	-0.45	39.14	-6.11	-499.31
140	1	21	-845.44	16.31	3.07	-42.47	-249.99	143.26
		92	828.19	20.47	-3.07	42.47	-97.16	-378.21
141	1	31	-845.44	16.31	-3.07	42.47	249.99	143.26
		94	828.19	20.47	3.07	-42.47	97.16	-378.21
142	1	31	-665.68	17.22	-0.45	39.14	48.07	157.76
		98	648.42	22.85	0.45	-39.14	6.11	-499.31
143	1	1	-665.68	17.22	0.45	-39.14	-48.07	157.76
		98	648.42	22.85	-0.45	39.14	-6.11	-499.31
144	1	5	304.46	9.21	-14.98	76.67	878.28	243.78
		82	-321.71	-9.21	14.98	-76.67	-159.26	198.26

## MEMBER END FORCES      STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
145	1	7	304.45	-9.21	-14.98	-76.67	878.28	-243.78
		84	-321.70	9.21	14.98	76.67	-159.26	-198.26
146	1	16	428.70	7.14	0.00	0.00	0.00	280.51
		88	-445.96	-7.14	0.00	0.00	0.00	62.44
147	1	25	304.46	-9.21	14.98	76.67	-878.28	-243.78
		92	-321.71	9.21	-14.98	-76.67	159.26	-198.26
148	1	27	304.45	9.21	14.98	-76.67	-878.28	243.78
		94	-321.70	-9.21	-14.98	76.67	159.26	198.26
149	1	36	428.70	-7.14	0.00	0.00	0.00	-280.51
		98	-445.95	7.14	0.00	0.00	0.00	-62.44
150	1	100	48.94	2.97	5.72	-103.88	-272.07	-33.05
		81	-36.01	9.97	-5.72	103.88	-19.14	-145.26
151	1	101	48.94	2.97	-5.72	103.88	272.08	-33.05
		85	-36.01	9.97	5.72	-103.88	19.14	-145.26
152	1	101	46.57	3.21	1.55	-30.81	-136.46	-27.34
		87	-33.63	9.73	-1.55	30.81	57.44	-138.77
153	1	102	46.57	3.21	-1.55	30.82	136.46	-27.34
		89	-33.63	9.73	1.55	-30.82	-57.44	-138.77
154	1	102	48.95	2.97	5.72	-103.88	-272.07	-33.05
		91	-36.01	9.97	-5.72	103.88	-19.14	-145.26
155	1	103	48.94	2.97	-5.72	103.88	272.08	-33.05
		95	-36.01	9.97	5.72	-103.88	19.14	-145.26
156	1	103	46.57	3.21	1.55	-30.81	-136.46	-27.34
		97	-33.63	9.73	-1.55	30.81	57.44	-138.77
157	1	100	46.57	3.21	-1.55	30.82	136.46	-27.34
		99	-33.63	9.73	1.55	-30.82	-57.44	-138.77

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

93. PRINT MEMBER STRESSES ALL

## MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
1	1	.0	265.4 C	52.3	775.5	1093.2	148.2	22.4
		1.00	265.4 C	136.9	1442.8	1845.1	112.8	22.4
2	1	.0	266.6 C	130.2	1588.4	1985.2	51.5	19.7
		1.00	266.6 C	19.6	950.8	1236.9	61.0	19.7
3	1	.0	266.6 C	19.6	950.8	1236.9	80.7	12.3
		1.00	266.6 C	49.7	16.7	333.0	90.1	12.3
4	1	.0	268.2 C	18.6	18.2	304.9	124.5	20.0
		1.00	268.2 C	104.4	1090.1	1462.7	131.7	20.0
5	1	.0	265.2 C	80.4	1039.0	1384.7	3.6	0.0
		1.00	265.2 C	80.4	1031.1	1376.8	0.0	0.0
6	1	.0	265.2 C	80.4	1031.1	1376.8	0.0	0.0
		1.00	265.2 C	80.4	1039.0	1384.6	3.6	0.0
7	1	.0	268.2 C	104.4	1090.1	1462.7	131.7	20.0
		1.00	268.2 C	18.6	18.2	304.9	124.5	20.0
8	1	.0	266.6 C	49.7	16.7	333.0	90.1	12.3
		1.00	266.6 C	19.6	950.8	1236.9	80.7	12.3
9	1	.0	266.6 C	19.6	950.8	1236.9	61.0	19.7
		1.00	266.6 C	130.2	1588.4	1985.2	51.5	19.7
10	1	.0	265.4 C	136.9	1442.8	1845.1	112.8	22.4
		1.00	265.4 C	52.4	775.5	1093.2	148.2	22.4
11	1	.0	222.5 C	219.2	513.0	954.8	29.1	39.0
		1.00	222.5 C	22.7	811.9	1057.2	18.7	39.0
12	1	.0	222.5 C	22.7	811.9	1057.2	2.0	2.5
		1.00	222.5 C	36.8	735.7	995.0	11.5	2.5
13	1	.0	222.5 C	36.8	735.7	995.0	31.1	3.7
		1.00	222.5 C	15.8	329.7	568.1	40.6	3.7
14	1	.0	222.5 C	15.8	329.7	568.1	60.2	2.3
		1.00	222.5 C	2.8	406.1	631.4	69.7	2.3
15	1	.0	222.5 C	2.8	406.1	631.4	90.1	4.8
		1.00	222.5 C	11.7	975.0	1209.2	95.3	4.8
16	1	.0	222.5 C	11.7	975.0	1209.2	95.3	4.8
		1.00	222.5 C	2.8	406.1	631.4	90.1	4.8
17	1	.0	222.5 C	2.8	406.1	631.4	69.7	2.3
		1.00	222.5 C	15.8	329.8	568.1	60.2	2.3

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
18	1	.0	222.5 C	15.8	329.7	568.1	40.6	3.7
		1.00	222.5 C	36.8	735.7	995.0	31.1	3.7
19	1	.0	222.5 C	36.8	735.7	995.0	11.5	2.5
		1.00	222.5 C	22.7	811.9	1057.2	2.0	2.5
20	1	.0	222.5 C	22.7	811.9	1057.2	18.7	39.0
		1.00	222.5 C	219.2	513.0	954.8	29.1	39.0
21	1	.0	265.4 C	52.3	775.5	1093.2	148.2	22.4
		1.00	265.4 C	136.9	1442.8	1845.1	112.8	22.4
22	1	.0	266.6 C	130.2	1588.4	1985.2	51.5	19.7
		1.00	266.6 C	19.6	950.8	1236.9	61.0	19.7
23	1	.0	266.6 C	19.6	950.8	1236.9	80.7	12.3
		1.00	266.6 C	49.7	16.7	333.0	90.1	12.3
24	1	.0	268.2 C	18.6	18.2	304.9	124.5	20.0
		1.00	268.2 C	104.4	1090.1	1462.7	131.7	20.0
25	1	.0	265.2 C	80.4	1039.0	1384.6	3.6	0.0
		1.00	265.2 C	80.4	1031.1	1376.8	0.0	0.0
26	1	.0	265.2 C	80.4	1031.1	1376.8	0.0	0.0
		1.00	265.2 C	80.4	1039.0	1384.6	3.6	0.0
27	1	.0	268.2 C	104.4	1090.1	1462.7	131.7	20.0
		1.00	268.2 C	18.6	18.2	304.9	124.5	20.0
28	1	.0	266.6 C	49.7	16.7	333.0	90.1	12.3
		1.00	266.6 C	19.6	950.8	1236.9	80.7	12.3
29	1	.0	266.6 C	19.6	950.8	1236.9	61.0	19.7
		1.00	266.6 C	130.2	1588.4	1985.2	51.5	19.7
30	1	.0	265.4 C	136.9	1442.8	1845.1	112.8	22.4
		1.00	265.4 C	52.4	775.5	1093.2	148.2	22.4
31	1	.0	222.5 C	219.2	513.0	954.8	29.1	39.0
		1.00	222.5 C	22.7	811.9	1057.2	18.7	39.0
32	1	.0	222.5 C	22.7	811.9	1057.2	2.0	2.5
		1.00	222.5 C	36.8	735.7	995.0	11.5	2.5
33	1	.0	222.5 C	36.8	735.7	995.0	31.1	3.7
		1.00	222.5 C	15.8	329.7	568.1	40.6	3.7
34	1	.0	222.5 C	15.8	329.7	568.1	60.2	2.3
		1.00	222.5 C	2.8	406.1	631.4	69.7	2.3

## MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
35	1	.0	222.5 C	2.8	406.1	631.4	90.1	4.8
		1.00	222.5 C	11.7	975.0	1209.2	95.3	4.8
36	1	.0	222.5 C	11.7	975.0	1209.2	95.3	4.8
		1.00	222.5 C	2.8	406.1	631.4	90.1	4.8
37	1	.0	222.5 C	2.8	406.1	631.4	69.7	2.3
		1.00	222.5 C	15.8	329.7	568.1	60.2	2.3
38	1	.0	222.5 C	15.8	329.7	568.1	40.6	3.7
		1.00	222.5 C	36.8	735.7	995.0	31.1	3.7
39	1	.0	222.5 C	36.8	735.7	995.0	11.5	2.5
		1.00	222.5 C	22.7	811.9	1057.2	2.0	2.5
40	1	.0	222.5 C	22.7	811.9	1057.2	18.7	39.0
		1.00	222.5 C	219.2	513.0	954.8	29.1	39.0
41	1	.0	10.1 C	6.7	1193.0	1209.7	164.4	5.0
		1.00	10.1 C	37.7	709.3	757.1	139.8	5.0
42	1	.0	10.1 C	37.7	709.3	757.1	119.1	31.5
		1.00	10.1 C	32.3	1235.2	1277.5	115.4	31.5
43	1	.0	10.1 C	44.5	1318.8	1373.4	89.5	7.3
		1.00	10.1 C	19.8	1912.0	1942.0	83.8	7.3
44	1	.0	10.1 C	19.8	1912.1	1942.0	64.2	1.0
		1.00	10.1 C	13.9	2585.3	2609.4	54.7	1.0
45	1	.0	10.1 C	13.9	2585.3	2609.4	35.1	2.4
		1.00	10.1 C	0.2	2928.7	2939.1	25.6	2.4
46	1	.0	10.1 C	0.2	2928.7	2939.1	5.1	0.0
		1.00	10.1 C	0.2	2928.7	2939.0	5.1	0.0
47	1	.0	10.1 C	0.2	2928.7	2939.1	25.6	2.4
		1.00	10.1 C	13.9	2585.3	2609.4	35.1	2.4
48	1	.0	10.1 C	13.9	2585.3	2609.4	54.7	1.0
		1.00	10.1 C	19.8	1912.1	1942.0	64.2	1.0
49	1	.0	10.1 C	19.8	1912.1	1942.0	83.8	7.3
		1.00	10.1 C	44.5	1318.8	1373.4	89.5	7.3
50	1	.0	10.1 C	32.3	1235.2	1277.6	115.4	31.5
		1.00	10.1 C	37.7	709.3	757.1	119.1	31.5
51	1	.0	10.1 C	37.7	709.3	757.1	139.8	5.0
		1.00	10.1 C	6.7	1193.0	1209.7	164.4	5.0

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
52	1	.0	10.1 C	6.7	1193.0	1209.7	164.4	5.0
		1.00	10.1 C	37.7	709.3	757.1	139.8	5.0
53	1	.0	10.1 C	37.7	709.3	757.1	119.1	31.5
		1.00	10.1 C	32.3	1235.2	1277.6	115.4	31.5
54	1	.0	10.1 C	44.5	1318.8	1373.4	89.5	7.3
		1.00	10.1 C	19.8	1912.0	1942.0	83.8	7.3
55	1	.0	10.1 C	19.8	1912.1	1942.0	64.2	1.0
		1.00	10.1 C	13.9	2585.3	2609.4	54.7	1.0
56	1	.0	10.1 C	13.9	2585.3	2609.4	35.0	2.4
		1.00	10.1 C	0.2	2928.7	2939.0	25.6	2.4
57	1	.0	10.1 C	0.2	2928.7	2939.1	5.1	0.0
		1.00	10.1 C	0.2	2928.7	2939.1	5.1	0.0
58	1	.0	10.1 C	0.2	2928.7	2939.1	25.6	2.4
		1.00	10.1 C	13.9	2585.3	2609.4	35.1	2.4
59	1	.0	10.1 C	13.9	2585.3	2609.4	54.7	1.0
		1.00	10.1 C	19.8	1912.0	1942.0	64.2	1.0
60	1	.0	10.1 C	19.8	1912.0	1942.0	83.8	7.3
		1.00	10.1 C	44.5	1318.8	1373.4	89.5	7.3
61	1	.0	10.1 C	32.3	1235.1	1277.5	115.4	31.5
		1.00	10.1 C	37.7	709.3	757.1	119.1	31.5
62	1	.0	10.1 C	37.7	709.3	757.1	139.8	5.0
		1.00	10.1 C	6.7	1193.0	1209.7	164.4	5.0
63	1	.0	17.7 C	38.8	548.0	604.5	51.7	0.5
		1.00	17.7 C	33.3	448.6	499.6	41.8	0.5
64	1	.0	17.7 C	33.3	448.6	499.6	2.5	11.5
		1.00	17.7 C	104.5	396.8	519.0	7.4	11.5
65	1	.0	14.7 C	25.7	265.6	306.0	11.3	0.0
		1.00	14.7 C	25.7	404.2	444.6	0.0	0.0
66	1	.0	14.7 C	25.7	404.2	444.6	0.0	0.0
		1.00	14.7 C	25.7	265.6	306.0	11.3	0.0
67	1	.0	17.7 C	104.5	396.8	519.1	7.4	11.5
		1.00	17.7 C	33.3	448.6	499.6	2.5	11.5
68	1	.0	17.7 C	33.3	448.6	499.6	41.8	0.5
		1.00	17.7 C	38.8	548.0	604.5	51.7	0.5

## MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
69	1	.0	17.7 C	38.8	548.0	604.5	51.7	0.5
		1.00	17.7 C	33.3	448.6	499.6	41.8	0.5
70	1	.0	17.7 C	33.3	448.6	499.6	2.5	11.5
		1.00	17.7 C	104.5	396.8	519.1	7.4	11.5
71	1	.0	14.7 C	25.7	265.6	306.0	11.3	0.0
		1.00	14.7 C	25.7	404.2	444.6	0.0	0.0
72	1	.0	14.7 C	25.7	404.2	444.6	0.0	0.0
		1.00	14.7 C	25.7	265.6	306.0	11.3	0.0
73	1	.0	17.7 C	104.5	396.8	519.1	7.4	11.5
		1.00	17.7 C	33.3	448.6	499.6	2.5	11.5
74	1	.0	17.7 C	33.3	448.6	499.6	41.8	0.5
		1.00	17.7 C	38.8	548.0	604.5	51.7	0.5
75	1	.0	9.6 T	0.0	0.0	9.6	134.3	0.0
		1.00	9.6 T	0.0	0.0	9.6	134.3	0.0
76	1	.0	4.5 C	142.4	1956.9	2103.8	102.9	6.6
		1.00	4.5 C	112.6	569.9	687.0	28.1	6.6
77	1	.0	4.5 C	142.4	1956.9	2103.8	102.9	6.6
		1.00	4.5 C	112.6	569.9	687.0	28.1	6.6
78	1	.0	9.6 T	0.0	0.0	9.6	134.3	0.0
		1.00	9.6 T	0.0	0.0	9.6	134.3	0.0
79	1	.0	47.6 C	0.0	0.0	47.6	141.1	0.0
		1.00	47.6 C	0.0	0.0	47.6	141.1	0.0
80	1	.0	8.1 C	0.0	0.0	8.1	134.3	0.0
		1.00	8.1 C	0.0	0.0	8.1	134.3	0.0
81	1	.0	1.8 T	0.0	0.0	1.8	134.3	0.0
		1.00	1.8 T	0.0	0.0	1.8	134.3	0.0
82	1	.0	3.2 C	0.0	0.0	3.2	139.8	0.0
		1.00	3.2 C	0.0	0.0	3.2	139.8	0.0
83	1	.0	3.2 C	0.0	0.0	3.2	139.8	0.0
		1.00	3.2 C	0.0	0.0	3.2	139.8	0.0
84	1	.0	1.8 T	0.0	0.0	1.8	134.3	0.0
		1.00	1.8 T	0.0	0.0	1.8	134.3	0.0
85	1	.0	8.1 C	0.0	0.0	8.1	134.3	0.0
		1.00	8.1 C	0.0	0.0	8.1	134.3	0.0

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
86	1	.0	47.6 C	0.0	0.0	47.6	141.1	0.0
		1.00	47.6 C	0.0	0.0	47.6	141.1	0.0
87	1	.0	9.6 T	0.0	0.0	9.6	134.3	0.0
		1.00	9.6 T	0.0	0.0	9.6	134.3	0.0
88	1	.0	4.5 C	142.4	1956.9	2103.8	102.9	6.6
		1.00	4.5 C	112.6	569.9	687.0	28.1	6.6
89	1	.0	4.5 C	142.4	1956.9	2103.8	102.9	6.6
		1.00	4.5 C	112.6	569.9	687.0	28.1	6.6
90	1	.0	9.6 T	0.0	0.0	9.6	134.3	0.0
		1.00	9.6 T	0.0	0.0	9.6	134.3	0.0
91	1	.0	47.6 C	0.0	0.0	47.6	141.1	0.0
		1.00	47.6 C	0.0	0.0	47.6	141.1	0.0
92	1	.0	8.1 C	0.0	0.0	8.1	134.3	0.0
		1.00	8.1 C	0.0	0.0	8.1	134.3	0.0
93	1	.0	1.8 T	0.0	0.0	1.8	134.3	0.0
		1.00	1.8 T	0.0	0.0	1.8	134.3	0.0
94	1	.0	3.2 C	0.0	0.0	3.2	139.8	0.0
		1.00	3.2 C	0.0	0.0	3.2	139.8	0.0
95	1	.0	3.2 C	0.0	0.0	3.2	139.8	0.0
		1.00	3.2 C	0.0	0.0	3.2	139.8	0.0
96	1	.0	1.8 T	0.0	0.0	1.8	134.3	0.0
		1.00	1.8 T	0.0	0.0	1.8	134.3	0.0
97	1	.0	8.1 C	0.0	0.0	8.1	134.3	0.0
		1.00	8.1 C	0.0	0.0	8.1	134.3	0.0
98	1	.0	47.6 C	0.0	0.0	47.6	141.1	0.0
		1.00	47.6 C	0.0	0.0	47.6	141.1	0.0
100	1	.0	440.1 C	1642.1	1483.2	3565.5	79.0	86.9
		1.00	453.7 C	585.4	541.1	1580.2	79.0	86.9
101	1	.0	462.5 C	473.5	455.2	1391.2	26.0	27.7
		1.00	472.7 C	59.5	43.9	576.1	26.0	27.7
102	1	.0	502.8 C	0.0	0.0	502.8	0.0	0.0
		1.00	504.5 C	0.0	0.0	504.5	0.0	0.0
103	1	.0	440.1 C	1642.1	1483.2	3565.5	79.0	86.9
		1.00	453.7 C	585.4	541.1	1580.2	79.0	86.9



## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
104	1	.0 1.00	462.5 C 472.7 C	473.5 59.5	455.2 43.9	1391.2 576.1	26.0 26.0	27.7 27.7
105	1	.0 1.00	502.8 C 504.5 C	0.0 0.0	0.0 0.0	502.8 504.5	0.0 0.0	0.0 0.0
106	1	.0 1.00	440.1 C 453.7 C	1642.1 585.4	1483.2 541.1	3565.5 1580.2	79.0 79.0	86.9 86.9
107	1	.0 1.00	462.5 C 472.7 C	473.5 59.5	455.2 43.9	1391.2 576.1	26.0 26.0	27.7 27.7
108	1	.0 1.00	502.8 C 504.5 C	0.0 0.0	0.0 0.0	502.8 504.5	0.0 0.0	0.0 0.0
109	1	.0 1.00	440.1 C 453.7 C	1642.1 585.4	1483.2 541.1	3565.5 1580.2	79.0 79.0	86.9 86.9
110	1	.0 1.00	462.5 C 472.7 C	473.5 59.5	455.2 43.9	1391.2 576.1	26.0 26.0	27.7 27.7
111	1	.0 1.00	502.8 C 504.5 C	0.0 0.0	0.0 0.0	502.8 504.5	0.0 0.0	0.0 0.0
112	1	.0 1.00	872.4 C 882.1 C	0.0 0.0	0.0 0.0	872.4 882.1	0.0 0.0	0.0 0.0
113	1	.0 1.00	872.4 C 882.1 C	0.0 0.0	0.0 0.0	872.4 882.1	0.0 0.0	0.0 0.0
114	1	.0 1.00	872.4 C 882.1 C	0.0 0.0	0.0 0.0	872.4 882.1	0.0 0.0	0.0 0.0
115	1	.0 1.00	872.4 C 882.1 C	0.0 0.0	0.0 0.0	872.4 882.1	0.0 0.0	0.0 0.0
116	1	.0 1.00	110.4 T 110.4 T	586.8 268.5	271.4 79.5	968.5 458.4	13.6 3.7	8.3 8.3
117	1	.0 1.00	84.8 T 84.8 T	354.1 774.3	287.0 68.4	725.9 927.5	20.9 10.9	15.9 15.9
118	1	.0 1.00	674.8 T 674.8 T	816.2 816.2	188.7 167.1	1679.6 1658.1	4.4 0.0	0.0 0.0
119	1	.0 1.00	674.8 T 674.8 T	816.2 816.2	167.1 188.7	1658.1 1679.6	0.0 4.4	0.0 0.0
120	1	.0 1.00	84.8 T 84.8 T	774.3 354.1	68.4 287.0	927.5 725.9	10.9 20.9	15.9 15.9

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
121	1	.0	110.4 T	268.5	79.5	458.4	3.7	8.3
		1.00	110.4 T	586.8	271.4	968.5	13.6	8.3
122	1	.0	123.3 T	246.8	285.4	655.5	14.3	3.3
		1.00	123.3 T	119.9	65.4	308.6	2.9	3.3
123	1	.0	99.2 T	209.1	263.6	571.9	19.6	5.4
		1.00	99.2 T	224.4	140.6	464.2	16.6	5.4
124	1	.0	99.2 T	224.4	140.6	464.2	16.6	5.4
		1.00	99.2 T	209.1	263.6	571.9	19.6	5.4
125	1	.0	123.3 T	119.9	65.4	308.6	2.9	3.3
		1.00	123.3 T	246.8	285.4	655.5	14.3	3.3
126	1	.0	110.4 T	586.8	271.4	968.5	13.6	8.3
		1.00	110.4 T	268.5	79.5	458.4	3.7	8.3
127	1	.0	84.8 T	354.1	287.0	725.9	20.9	15.9
		1.00	84.8 T	774.3	68.4	927.5	10.9	15.9
128	1	.0	674.8 T	816.2	188.7	1679.7	4.4	0.0
		1.00	674.8 T	816.2	167.1	1658.1	0.0	0.0
129	1	.0	674.8 T	816.2	167.1	1658.1	0.0	0.0
		1.00	674.8 T	816.3	188.7	1679.7	4.4	0.0
130	1	.0	84.8 T	774.3	68.4	927.5	10.9	15.9
		1.00	84.8 T	354.1	287.0	725.9	20.9	15.9
131	1	.0	110.4 T	268.5	79.5	458.4	3.7	8.3
		1.00	110.4 T	586.8	271.4	968.5	13.6	8.3
132	1	.0	123.3 T	246.8	285.4	655.5	14.3	3.3
		1.00	123.3 T	119.9	65.4	308.6	2.9	3.3
133	1	.0	99.2 T	209.1	263.6	571.9	19.6	5.4
		1.00	99.2 T	224.4	140.6	464.2	16.6	5.4
134	1	.0	99.2 T	224.4	140.6	464.2	16.6	5.4
		1.00	99.2 T	209.1	263.6	571.9	19.6	5.4
135	1	.0	123.3 T	119.9	65.4	308.6	2.9	3.3
		1.00	123.3 T	246.8	285.4	655.5	14.3	3.3
136	1	.0	665.7 T	357.1	204.7	1227.5	21.7	4.1
		1.00	652.1 T	138.8	540.3	1331.2	27.3	4.1
137	1	.0	665.7 T	357.1	204.7	1227.5	21.7	4.1
		1.00	652.1 T	138.8	540.3	1331.2	27.3	4.1

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
138	1	.0	524.2 T	68.7	225.4	818.2	23.0	0.6
		1.00	510.6 T	8.7	713.3	1232.6	30.5	0.6
139	1	.0	524.2 T	68.7	225.4	818.2	23.0	0.6
		1.00	510.6 T	8.7	713.3	1232.6	30.5	0.6
140	1	.0	665.7 T	357.1	204.7	1227.5	21.7	4.1
		1.00	652.1 T	138.8	540.3	1331.2	27.3	4.1
141	1	.0	665.7 T	357.1	204.7	1227.5	21.7	4.1
		1.00	652.1 T	138.8	540.3	1331.2	27.3	4.1
142	1	.0	524.2 T	68.7	225.4	818.2	23.0	0.6
		1.00	510.6 T	8.7	713.3	1232.6	30.5	0.6
143	1	.0	524.2 T	68.7	225.4	818.2	23.0	0.6
		1.00	510.6 T	8.7	713.3	1232.6	30.5	0.6
144	1	.0	239.7 C	1254.7	348.3	1842.7	12.3	20.0
		1.00	253.3 C	227.5	283.2	764.1	12.3	20.0
145	1	.0	239.7 C	1254.7	348.3	1842.7	12.3	20.0
		1.00	253.3 C	227.5	283.2	764.1	12.3	20.0
146	1	.0	337.6 C	0.0	400.7	738.3	9.5	0.0
		1.00	351.1 C	0.0	89.2	440.3	9.5	0.0
147	1	.0	239.7 C	1254.7	348.3	1842.7	12.3	20.0
		1.00	253.3 C	227.5	283.2	764.1	12.3	20.0
148	1	.0	239.7 C	1254.7	348.3	1842.7	12.3	20.0
		1.00	253.3 C	227.5	283.2	764.1	12.3	20.0
149	1	.0	337.6 C	0.0	400.7	738.3	9.5	0.0
		1.00	351.1 C	0.0	89.2	440.3	9.5	0.0
150	1	.0	38.5 C	388.7	47.2	474.4	4.0	7.6
		1.00	28.4 C	27.3	207.5	263.2	13.3	7.6
151	1	.0	38.5 C	388.7	47.2	474.4	4.0	7.6
		1.00	28.4 C	27.3	207.5	263.2	13.3	7.6
152	1	.0	36.7 C	194.9	39.1	270.7	4.3	2.1
		1.00	26.5 C	82.1	198.2	306.8	13.0	2.1
153	1	.0	36.7 C	194.9	39.1	270.7	4.3	2.1
		1.00	26.5 C	82.1	198.2	306.8	13.0	2.1
154	1	.0	38.5 C	388.7	47.2	474.4	4.0	7.6
		1.00	28.4 C	27.3	207.5	263.2	13.3	7.6

## MEMBER STRESSES

-----  
ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
155	1	.0	38.5 C	388.7	47.2	474.4	4.0	7.6
		1.00	28.4 C	27.3	207.5	263.2	13.3	7.6
156	1	.0	36.7 C	194.9	39.1	270.7	4.3	2.1
		1.00	26.5 C	82.1	198.2	306.8	13.0	2.1
157	1	.0	36.7 C	194.9	39.1	270.7	4.3	2.1
		1.00	26.5 C	82.1	198.2	306.8	13.0	2.1

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

94. PARAMETER  
 95. CODE AISC  
 96. FYLD 36000. MEMB 1 TO 74 76 77 88 89 100 TO 111 116 TO 135 144 TO 157  
 97. FYLD 21999.994 MEMB 75 78 TO 87 90 TO 98 112 TO 115  
 98. WMIN 0.188 ALL  
 99. DFF 0.063 ALL  
 100. LY 223. MEMB 1 TO 62  
 101. LZ 223. MEMB 1 TO 62  
 102. CB 1. ALL  
 103. MAIN 0. ALL  
 104. TRACK 1. ALL  
 105. RATIO 1. ALL  
 106. WELD 1. ALL  
 107. LOAD LIST ALL  
 108. CHECK CODE ALL

STAAD-III CODE CHECKING - (AISC)  
 \*\*\*\*\*

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
1	ST TUB 60303	PASS 833.35 C	AISC- H1-3 -438.09	0.131 6877.31	1 36.00
MEM= 1, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
2	ST TUB 60303	PASS 837.10 C	AISC- H1-3 416.62	0.138 -7571.42	1 0.00
MEM= 2, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
3	ST TUB 60303	PASS 837.10 C	AISC- H1-3 62.60	0.103 -4532.09	1 0.00
MEM= 3, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
4	ST TUB 60303	PASS 842.06 C	AISC- H1-3 334.06	0.114 -5196.25	1 18.33
MEM= 4, UNIT KIP-INCH, L= 18.3 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
5	ST TUB 60303	PASS 832.85 C	AISC- H1-3 -257.39	0.110 4952.47	1 0.00
MEM= 5, UNIT KIP-INCH, L= 9.2 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
6	ST TUB 60303	PASS 832.85 C	AISC- H1-3 257.39	0.110 -4952.46	1 9.17
MEM= 6, UNIT KIP-INCH, L= 9.2 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
7	ST TUB 60303	PASS 842.06 C	AISC- H1-3 -334.06	0.114 5196.24	1 0.00
MEM= 7, UNIT KIP-INCH, L= 18.3 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
8	ST TUB 60303	PASS 837.10 C	AISC- H1-3 -62.60	0.103 4532.11	1 24.00
MEM= 8, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
9	ST TUB 60303	PASS 837.10 C	AISC- H1-3 -416.61	0.138 7571.40	1 24.00
MEM= 9, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
10	ST TUB 60303	PASS 833.36 C	AISC- H1-3 438.09	0.131 -6877.31	1 0.00
MEM= 10, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
11	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -72.80	0.087 3869.94	1 26.50
MEM= 11, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
12	ST TUB 60303	PASS 698.75 C	AISC- H1-3 72.79	0.087 -3869.95	1 0.00
MEM= 12, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
13	ST TUB 60303	PASS 698.75 C	AISC- H1-3 117.65	0.084 -3507.04	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 13, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
14	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -8.87	0.067 -1935.79	1 24.00
MEM= 14, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
15	ST TUB 60303	PASS 698.75 C	AISC- H1-3 37.57	0.094 -4647.30	1 13.00
MEM= 15, UNIT KIP-INCH, L= 13.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
16	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -37.57	0.094 4647.30	1 0.00
MEM= 16, UNIT KIP-INCH, L= 13.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
17	ST TUB 60303	PASS 698.75 C	AISC- H1-3 8.87	0.067 1935.80	1 0.00
MEM= 17, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
18	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -117.65	0.084 3507.03	1 24.00
MEM= 18, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
19	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -72.79	0.087 3869.96	1 24.00
MEM= 19, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
20	ST TUB 60303	PASS 698.75 C	AISC- H1-3 72.79	0.087 -3869.93	1 0.00
MEM= 20, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
21	ST TUB 60303	PASS 833.35 C	AISC- H1-3 -438.09	0.131 6877.32	1 36.00
MEM= 21, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
22	ST TUB 60303	PASS 837.10 C	AISC- H1-3 416.62	0.138 -7571.46	1 0.00
MEM= 22, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
23	ST TUB 60303	PASS 837.10 C	AISC- H1-3 62.60	0.103 -4532.09	1 0.00
MEM= 23, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
24	ST TUB 60303	PASS 842.06 C	AISC- H1-3 334.06	0.114 -5196.21	1 18.33
MEM= 24, UNIT KIP-INCH, L= 18.3 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
25	ST TUB 60303	PASS 832.85 C	AISC- H1-3 -257.39	0.110 4952.43	1 0.00
MEM= 25, UNIT KIP-INCH, L= 9.2 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
26	ST TUB 60303	PASS 832.85 C	AISC- H1-3 257.39	0.110 -4952.43	1 9.17



ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 26, UNIT KIP-INCH, L= 9.2 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
27	ST TUB 60303	PASS 842.06 C	AISC- H1-3 -334.06	0.114 5196.22	1 0.00
MEM= 27, UNIT KIP-INCH, L= 18.3 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
28	ST TUB 60303	PASS 837.10 C	AISC- H1-3 -62.60	0.103 4532.12	1 24.00
MEM= 28, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
29	ST TUB 60303	PASS 837.10 C	AISC- H1-3 -416.61	0.138 7571.40	1 24.00
MEM= 29, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
30	ST TUB 60303	PASS 833.35 C	AISC- H1-3 438.09	0.131 -6877.30	1 0.00
MEM= 30, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
31	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -72.79	0.087 3869.93	1 26.50
MEM= 31, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
32	ST TUB 60303	PASS 698.75 C	AISC- H1-3 72.80	0.087 -3869.94	1 0.00
MEM= 32, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
33	ST TUB 60303	PASS 698.75 C	AISC- H1-3 117.65	0.084 -3507.05	1 0.00
MEM= 33, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
34	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -8.87	0.067 -1935.78	1 24.00
MEM= 34, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
35	ST TUB 60303	PASS 698.75 C	AISC- H1-3 37.57	0.094 -4647.28	1 13.00
MEM= 35, UNIT KIP-INCH, L= 13.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
36	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -37.57	0.094 4647.27	1 0.00
MEM= 36, UNIT KIP-INCH, L= 13.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
37	ST TUB 60303	PASS 698.75 C	AISC- H1-3 8.87	0.067 1935.78	1 0.00
MEM= 37, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
38	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -117.65	0.084 3507.04	1 24.00
MEM= 38, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
39	ST TUB 60303	PASS 698.75 C	AISC- H1-3 -72.79	0.087 3869.95	1 24.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 39, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
40	ST TUB 60303	PASS 698.75 C	AISC- H1-3 72.79	0.087 -3869.95	1 0.00
MEM= 40, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
41	ST TUB 60303	PASS 31.57 C	AISC- H1-3 21.48	0.058 5686.48	1 0.00
MEM= 41, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
42	ST TUB 60303	PASS 31.57 C	AISC- H1-3 103.49	0.061 5887.55	1 9.50
MEM= 42, UNIT KIP-INCH, L= 9.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
43	ST TUB 60303	PASS 31.80 C	AISC- H1-3 63.39	0.092 9114.08	1 14.50
MEM= 43, UNIT KIP-INCH, L= 14.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
44	ST TUB 60303	PASS 31.80 C	AISC- H1-3 44.62	0.123 12323.27	1 24.00
MEM= 44, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
45	ST TUB 60303	PASS 31.80 C	AISC- H1-3 0.70	0.138 13960.17	1 24.00
MEM= 45, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
46	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -0.70	0.138 -13960.21	1 0.00
MEM= 46, UNIT KIP-INCH, L= 26.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
47	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -0.70	0.138 -13960.16	1 0.00
MEM= 47, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
48	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -44.62	0.123 -12323.26	1 0.00
MEM= 48, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
49	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -63.39	0.092 -9114.19	1 0.00
MEM= 49, UNIT KIP-INCH, L= 14.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
50	ST TUB 60303	PASS 31.57 C	AISC- H1-3 -103.49	0.061 -5887.60	1 0.00
MEM= 50, UNIT KIP-INCH, L= 9.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
51	ST TUB 60303	PASS 31.57 C	AISC- H1-3 -21.48	0.058 -5686.53	1 26.50
MEM= 51, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
52	ST TUB 60303	PASS 31.57 C	AISC- H1-3 -21.48	0.058 5686.48	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 52, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
53	ST TUB 60303	PASS 31.57 C	AISC- H1-3 -103.49	0.061 5887.57	1 9.50
MEM= 53, UNIT KIP-INCH, L= 9.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
54	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -63.39	0.092 9114.02	1 14.50
MEM= 54, UNIT KIP-INCH, L= 14.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
55	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -44.62	0.123 12323.28	1 24.00
MEM= 55, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
56	ST TUB 60303	PASS 31.80 C	AISC- H1-3 -0.70	0.138 13960.13	1 24.00
MEM= 56, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
57	ST TUB 60303	PASS 31.80 C	AISC- H1-3 0.70	0.138 -13960.18	1 0.00
MEM= 57, UNIT KIP-INCH, L= 26.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
58	ST TUB 60303	PASS 31.80 C	AISC- H1-3 0.70	0.138 -13960.19	1 0.00
MEM= 58, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
59	ST TUB 60303	PASS 31.80 C	AISC- H1-3 44.62	0.123 -12323.33	1 0.00
MEM= 59, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
60	ST TUB 60303	PASS 31.80 C	AISC- H1-3 63.39	0.092 -9114.10	1 0.00
MEM= 60, UNIT KIP-INCH, L= 14.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
61	ST TUB 60303	PASS 31.57 C	AISC- H1-3 103.49	0.061 -5887.42	1 0.00
MEM= 61, UNIT KIP-INCH, L= 9.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
62	ST TUB 60303	PASS 31.57 C	AISC- H1-3 21.48	0.058 -5686.46	1 26.50
MEM= 62, UNIT KIP-INCH, L= 26.5 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 180.4 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 4.59 FT= 21.60 FV= 14.40					
63	ST TUB 30203	PASS 29.04 C	AISC- H1-3 38.80	0.028 694.10	1 0.00
MEM= 63, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
64	ST TUB 30203	PASS 29.04 C	AISC- H1-3 104.51	0.024 502.64	1 24.00
MEM= 64, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
65	ST TUB 30203	PASS 24.09 C	AISC- H1-3 25.70	0.021 511.94	1 27.50

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 65, UNIT KIP-INCH, L= 27.5 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 35.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.56 FT= 21.60 FV= 14.40					
66	ST TUB 30203	PASS 24.09 C	AISC- H1-3 -25.70	0.021 -511.94	1 0.00
MEM= 66, UNIT KIP-INCH, L= 27.5 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 35.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.56 FT= 21.60 FV= 14.40					
67	ST TUB 30203	PASS 29.04 C	AISC- H1-3 -104.51	0.024 -502.67	1 0.00
MEM= 67, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
68	ST TUB 30203	PASS 29.04 C	AISC- H1-3 -38.80	0.028 -694.10	1 24.00
MEM= 68, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
69	ST TUB 30203	PASS 29.04 C	AISC- H1-3 38.80	0.028 694.11	1 0.00
MEM= 69, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
70	ST TUB 30203	PASS 29.04 C	AISC- H1-3 104.51	0.024 502.66	1 24.00
MEM= 70, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
71	ST TUB 30203	PASS 24.09 C	AISC- H1-3 25.70	0.021 511.94	1 27.50
MEM= 71, UNIT KIP-INCH, L= 27.5 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 35.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.56 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
72	ST TUB 30203	PASS 24.09 C	AISC- H1-3 -25.70	0.021 -511.94	1 0.00
MEM= 72, UNIT KIP-INCH, L= 27.5 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 35.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.56 FT= 21.60 FV= 14.40					
73	ST TUB 30203	PASS 29.04 C	AISC- H1-3 -104.51	0.024 -502.66	1 0.00
MEM= 73, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
74	ST TUB 30203	PASS 29.05 C	AISC- H1-3 -38.80	0.028 -694.13	1 24.00
MEM= 74, UNIT KIP-INCH, L= 24.0 AX= 1.64 SZ= 1.3 SY= 1.0 KL/R-Y= 30.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.89 FT= 21.60 FV= 14.40					
75	PRI SMAT	PASS 5.51 T	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 75, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
76	ST TUB 20203	PASS 5.74 C	AISC- H1-3 -99.66	0.097 1369.81	1 0.00
MEM= 76, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
77	ST TUB 20203	PASS 5.74 C	AISC- H1-3 99.66	0.097 1369.81	1 0.00
MEM= 77, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
78	PRI SMAT	PASS 5.51 T	SHEAR -Y 0.00	0.015 0.00	1 0.00



ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
-----					
MEM=	78, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
79	PRI SMAT	PASS	SHEAR -Y	0.016	1
		27.35 C	0.00	0.00	0.00
-----					
MEM=	79, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
80	PRI SMAT	PASS	SHEAR -Y	0.015	1
		4.66 C	0.00	0.00	0.00
-----					
MEM=	80, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
81	PRI SMAT	PASS	SHEAR -Y	0.015	1
		1.05 T	0.00	0.00	0.00
-----					
MEM=	81, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
82	PRI SMAT	PASS	SHEAR -Y	0.016	1
		1.83 C	0.00	0.00	0.00
-----					
MEM=	82, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
83	PRI SMAT	PASS	SHEAR -Y	0.016	1
		1.83 C	0.00	0.00	0.00
-----					
MEM=	83, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80
84	PRI SMAT	PASS	SHEAR -Y	0.015	1
		1.05 T	0.00	0.00	0.00
-----					
MEM=	84, UNIT KIP-INCH,	L= 36.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	118.0	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.70	FT= 13.20 FV= 8.80

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
85	PRI SMAT	PASS 4.66 C	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 85, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
86	PRI SMAT	PASS 27.35 C	SHEAR -Y 0.00	0.016 0.00	1 0.00
MEM= 86, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
87	PRI SMAT	PASS 5.51 T	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 87, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
88	ST TUB 20203	PASS 5.74 C	AISC- H1-3 -99.66	0.097 1369.81	1 0.00
MEM= 88, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
89	ST TUB 20203	PASS 5.74 C	AISC- H1-3 99.66	0.097 1369.81	1 0.00
MEM= 89, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
90	PRI SMAT	PASS 5.51 T	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 90, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
91	PRI SMAT	PASS 27.35 C	SHEAR -Y 0.00	0.016 0.00	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 91, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
92	PRI SMAT	PASS 4.66 C	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 92, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
93	PRI SMAT	PASS 1.05 T	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 93, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
94	PRI SMAT	PASS 1.83 C	SHEAR -Y 0.00	0.016 0.00	1 0.00
MEM= 94, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
95	PRI SMAT	PASS 1.83 C	SHEAR -Y 0.00	0.016 0.00	1 0.00
MEM= 95, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
96	PRI SMAT	PASS 1.05 T	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 96, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
97	PRI SMAT	PASS 4.66 C	SHEAR -Y 0.00	0.015 0.00	1 0.00
MEM= 97, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
98	PRI SMAT	PASS 27.35 C	SHEAR -Y 0.00	0.016 0.00	1 0.00
MEM= 98, UNIT KIP-INCH, L= 36.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 118.0 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.70 FT= 13.20 FV= 8.80					
100	ST TUB 35353	PASS 1051.92 C	AISC- H1-3 4034.92	0.167 -3644.49	1 0.00
MEM= 100, UNIT KIP-INCH, L= 48.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 35.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.51 FT= 21.60 FV= 14.40					
101	ST TUB 35353	PASS 1105.33 C	AISC- H1-3 -1163.49	0.066 1118.54	1 0.00
MEM= 101, UNIT KIP-INCH, L= 36.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 26.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 20.16 FT= 21.60 FV= 14.40					
102	ST TUB 35353	PASS 1201.58 C	AISC- H1-3 0.00	0.023 0.00	1 0.00
MEM= 102, UNIT KIP-INCH, L= 6.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 4.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.41 FT= 21.60 FV= 14.40					
103	ST TUB 35353	PASS 1051.92 C	AISC- H1-3 4034.92	0.167 3644.49	1 0.00
MEM= 103, UNIT KIP-INCH, L= 48.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 35.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.51 FT= 21.60 FV= 14.40					
104	ST TUB 35353	PASS 1105.33 C	AISC- H1-3 -1163.49	0.066 -1118.54	1 0.00
MEM= 104, UNIT KIP-INCH, L= 36.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 26.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 20.16 FT= 21.60 FV= 14.40					
105	ST TUB 35353	PASS 1201.62 C	AISC- H1-3 0.00	0.023 0.00	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 105, UNIT KIP-INCH, L= 6.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 4.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.41 FT= 21.60 FV= 14.40					
106	ST TUB 35353	PASS 1051.92 C	AISC- H1-3 -4034.92	0.167 3644.49	1 0.00
MEM= 106, UNIT KIP-INCH, L= 48.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 35.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.51 FT= 21.60 FV= 14.40					
107	ST TUB 35353	PASS 1105.33 C	AISC- H1-3 1163.49	0.066 -1118.54	1 0.00
MEM= 107, UNIT KIP-INCH, L= 36.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 26.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 20.16 FT= 21.60 FV= 14.40					
108	ST TUB 35353	PASS 1201.60 C	AISC- H1-3 0.00	0.023 0.00	1 0.00
MEM= 108, UNIT KIP-INCH, L= 6.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 4.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.41 FT= 21.60 FV= 14.40					
109	ST TUB 35353	PASS 1051.92 C	AISC- H1-3 -4034.92	0.167 -3644.49	1 0.00
MEM= 109, UNIT KIP-INCH, L= 48.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 35.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 19.51 FT= 21.60 FV= 14.40					
110	ST TUB 35353	PASS 1105.33 C	AISC- H1-3 1163.49	0.066 1118.54	1 0.00
MEM= 110, UNIT KIP-INCH, L= 36.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 26.8 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 20.16 FT= 21.60 FV= 14.40					
111	ST TUB 35353	PASS 1201.60 C	AISC- H1-3 0.00	0.023 0.00	1 0.00
MEM= 111, UNIT KIP-INCH, L= 6.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 4.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.41 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
112	PRI SMAT	PASS 1219.11 C	AISC- H1-3 0.00	0.132 0.00	1 102.00
MEM= 112, UNIT KIP-INCH, L= 102.0 AX= 1.38 SZ= 1.3 SY= 1.3 KL/R-Y= 86.7 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 6.68 FT= 13.20 FV= 8.80					
113	PRI SMAT	PASS 1219.10 C	AISC- H1-3 0.00	0.132 0.00	1 102.00
MEM= 113, UNIT KIP-INCH, L= 102.0 AX= 1.38 SZ= 1.3 SY= 1.3 KL/R-Y= 86.7 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 6.68 FT= 13.20 FV= 8.80					
114	PRI SMAT	PASS 1219.10 C	AISC- H1-3 0.00	0.132 0.00	1 102.00
MEM= 114, UNIT KIP-INCH, L= 102.0 AX= 1.38 SZ= 1.3 SY= 1.3 KL/R-Y= 86.7 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 6.68 FT= 13.20 FV= 8.80					
115	PRI SMAT	PASS 1219.10 C	AISC- H1-3 0.00	0.132 0.00	1 102.00
MEM= 115, UNIT KIP-INCH, L= 102.0 AX= 1.38 SZ= 1.3 SY= 1.3 KL/R-Y= 86.7 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 6.68 FT= 13.20 FV= 8.80					
116	ST TUB 20203	PASS 140.16 T	AISC- H2-1 -410.74	0.045 189.96	1 0.00
MEM= 116, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
117	ST TUB 20203	PASS 107.65 T	AISC- H2-1 -542.02	0.043 47.87	1 66.33
MEM= 117, UNIT KIP-INCH, L= 66.3 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 89.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 14.28 FT= 21.60 FV= 14.40					
118	ST TUB 20203	PASS 856.94 T	AISC- H2-1 571.34	0.078 132.09	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 118, UNIT KIP-INCH, L= 9.2 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 12.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.03 FT= 21.60 FV= 14.40					
119	ST TUB 20203	PASS 856.94 T	AISC- H2-1 -571.34	0.078 -132.08	1 9.17
MEM= 119, UNIT KIP-INCH, L= 9.2 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 12.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.03 FT= 21.60 FV= 14.40					
120	ST TUB 20203	PASS 107.65 T	AISC- H2-1 542.02	0.043 -47.87	1 0.00
MEM= 120, UNIT KIP-INCH, L= 66.3 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 89.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 14.28 FT= 21.60 FV= 14.40					
121	ST TUB 20203	PASS 140.16 T	AISC- H2-1 410.74	0.045 -189.96	1 36.00
MEM= 121, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
122	ST TUB 20203	PASS 156.60 T	AISC- H2-1 -172.75	0.030 199.78	1 0.00
MEM= 122, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
123	ST TUB 20203	PASS 125.93 T	AISC- H2-1 -146.35	0.026 184.53	1 0.00
MEM= 123, UNIT KIP-INCH, L= 75.5 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 101.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 12.76 FT= 21.60 FV= 14.40					
124	ST TUB 20203	PASS 125.94 T	AISC- H2-1 146.36	0.026 -184.53	1 75.50
MEM= 124, UNIT KIP-INCH, L= 75.5 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 101.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 12.76 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
125	ST TUB 20203	PASS 156.60 T	AISC- H2-1 172.75	0.030 -199.78	1 36.00
MEM= 125, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
126	ST TUB 20203	PASS 140.16 T	AISC- H2-1 -410.74	0.045 189.96	1 0.00
MEM= 126, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
127	ST TUB 20203	PASS 107.65 T	AISC- H2-1 -542.02	0.043 47.87	1 66.33
MEM= 127, UNIT KIP-INCH, L= 66.3 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 89.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 14.28 FT= 21.60 FV= 14.40					
128	ST TUB 20203	PASS 856.94 T	AISC- H2-1 571.36	0.078 132.08	1 0.00
MEM= 128, UNIT KIP-INCH, L= 9.2 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 12.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.03 FT= 21.60 FV= 14.40					
129	ST TUB 20203	PASS 856.94 T	AISC- H2-1 -571.38	0.078 -132.08	1 9.17
MEM= 129, UNIT KIP-INCH, L= 9.2 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 12.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 21.03 FT= 21.60 FV= 14.40					
130	ST TUB 20203	PASS 107.65 T	AISC- H2-1 542.02	0.043 -47.87	1 0.00
MEM= 130, UNIT KIP-INCH, L= 66.3 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 89.3 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 14.28 FT= 21.60 FV= 14.40					
131	ST TUB 20203	PASS 140.16 T	AISC- H2-1 410.74	0.045 -189.96	1 36.00



ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 131, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
132	ST TUB 20203	PASS 156.60 T	AISC- H2-1 -172.75	0.030 199.78	1 0.00
MEM= 132, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
133	ST TUB 20203	PASS 125.94 T	AISC- H2-1 -146.35	0.026 184.53	1 0.00
MEM= 133, UNIT KIP-INCH, L= 75.5 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 101.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 12.76 FT= 21.60 FV= 14.40					
134	ST TUB 20203	PASS 125.93 T	AISC- H2-1 146.36	0.026 -184.53	1 75.50
MEM= 134, UNIT KIP-INCH, L= 75.5 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 101.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 12.76 FT= 21.60 FV= 14.40					
135	ST TUB 20203	PASS 156.60 T	AISC- H2-1 172.75	0.030 -199.78	1 36.00
MEM= 135, UNIT KIP-INCH, L= 36.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 48.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 18.48 FT= 21.60 FV= 14.40					
136	ST TUB 20203	PASS 828.19 T	AISC- H2-1 -97.16	0.062 -378.21	1 113.03
MEM= 136, UNIT KIP-INCH, L= 113.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 152.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 6.44 FT= 21.60 FV= 14.40					
137	ST TUB 20203	PASS 828.19 T	AISC- H2-1 97.16	0.062 -378.21	1 113.03
MEM= 137, UNIT KIP-INCH, L= 113.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 152.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 6.44 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
138	ST TUB 20203	PASS 648.42 T	AISC- H2-1 6.11	0.057 -499.31	1 121.39
MEM= 138, UNIT KIP-INCH, L= 121.4 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 163.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 5.59 FT= 21.60 FV= 14.40					
139	ST TUB 20203	PASS 648.42 T	AISC- H2-1 -6.11	0.057 -499.31	1 121.39
MEM= 139, UNIT KIP-INCH, L= 121.4 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 163.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 5.59 FT= 21.60 FV= 14.40					
140	ST TUB 20203	PASS 828.19 T	AISC- H2-1 -97.16	0.062 -378.21	1 113.03
MEM= 140, UNIT KIP-INCH, L= 113.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 152.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 6.44 FT= 21.60 FV= 14.40					
141	ST TUB 20203	PASS 828.19 T	AISC- H2-1 97.16	0.062 -378.21	1 113.03
MEM= 141, UNIT KIP-INCH, L= 113.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 152.2 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 6.44 FT= 21.60 FV= 14.40					
142	ST TUB 20203	PASS 648.42 T	AISC- H2-1 6.11	0.057 -499.31	1 121.39
MEM= 142, UNIT KIP-INCH, L= 121.4 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 163.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 5.59 FT= 21.60 FV= 14.40					
143	ST TUB 20203	PASS 648.42 T	AISC- H2-1 -6.11	0.057 -499.31	1 121.39
MEM= 143, UNIT KIP-INCH, L= 121.4 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 163.5 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 5.59 FT= 21.60 FV= 14.40					
144	ST TUB 20203	PASS 304.46 C	AISC- H1-3 878.28	0.088 243.78	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 144, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
145	ST TUB 20203	PASS 304.45 C	AISC- H1-3 878.28	0.088 -243.78	1 0.00
MEM= 145, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
146	ST TUB 20203	PASS 428.70 C	AISC- H1-3 0.00	0.038 280.51	1 0.00
MEM= 146, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
147	ST TUB 20203	PASS 304.46 C	AISC- H1-3 -878.28	0.088 -243.78	1 0.00
MEM= 147, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
148	ST TUB 20203	PASS 304.45 C	AISC- H1-3 -878.28	0.088 243.78	1 0.00
MEM= 148, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
149	ST TUB 20203	PASS 428.70 C	AISC- H1-3 0.00	0.038 -280.51	1 0.00
MEM= 149, UNIT KIP-INCH, L= 48.0 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 64.7 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.97 FT= 21.60 FV= 14.40					
150	ST TUB 20203	PASS 48.94 C	AISC- H1-3 -272.07	0.023 -33.05	1 0.00
MEM= 150, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
151	ST TUB 20203	PASS 48.94 C	AISC- H1-3 272.08	0.023 -33.05	1 0.00
MEM= 151, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
152	ST TUB 20203	PASS 33.63 C	AISC- H1-3 57.44	0.015 -138.77	1 50.91
MEM= 152, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
153	ST TUB 20203	PASS 33.63 C	AISC- H1-3 -57.44	0.015 -138.77	1 50.91
MEM= 153, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
154	ST TUB 20203	PASS 48.95 C	AISC- H1-3 -272.07	0.023 -33.05	1 0.00
MEM= 154, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
155	ST TUB 20203	PASS 48.94 C	AISC- H1-3 272.08	0.023 -33.05	1 0.00
MEM= 155, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
156	ST TUB 20203	PASS 33.63 C	AISC- H1-3 57.44	0.015 -138.77	1 50.91
MEM= 156, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 36.00 ALLOWABLE STRESSES: FCZ= 21.60 FTZ= 21.60 FCY= 21.60 FTY= 21.60 FA= 16.57 FT= 21.60 FV= 14.40					
157	ST TUB 20203	PASS 33.63 C	AISC- H1-3 -57.44	0.015 -138.77	1 50.91

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
--------	-------	---------------	----------------------	--------------	----------------------

MEM=	157, UNIT KIP-INCH,	L=	50.9	AX=	1.27	SZ=	0.7	SY=	0.7
KL/R-Y=	68.6	CB=	1.00	YLD=	36.00	ALLOWABLE STRESSES:	FCZ=	21.60	
FTZ=	21.60	FCY=	21.60	FTY=	21.60	FA=	16.57	FT=	21.60
		FV=	14.40						

109. SELECT WELD ALL

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
1	STA 1	1 818.55	3/16 505.62	1349.72 946.61
1	END 1	1 818.55	3/16 482.00	1844.27 1580.81

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

2	STA 1	1 69.10	3/16 66.73	1702.58 1699.87
2	END 1	1 69.10	3/16 73.05	1074.35 1069.63

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

3	STA 1	1 67.46	3/16 86.14	1075.21 1069.63
3	END 1	1 67.46	3/16 92.46	323.50 302.58

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

4	STA 1	1 120.10	3/16 140.80	335.63 280.00
4	END 1	1 120.10	3/16 145.62	1272.20 1258.12

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

5	STA 1	1 0.00	3/16 2.42	1192.58 1192.58
5	END 1	1 0.00	3/16 0.00	1185.93 1185.93

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

6	STA	1	3/16	1185.93
	1	0.00	0.00	1185.93
6	END	1	3/16	1192.58
	1	0.00	2.41	1192.58

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

7	STA	1	3/16	1272.20
	1	120.10	145.63	1258.11
7	END	1	3/16	335.63
	1	120.10	140.80	280.00

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

8	STA	1	3/16	323.50
	1	67.47	92.46	302.58
8	END	1	3/16	1075.22
	1	67.47	86.14	1069.64

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

9	STA	1	3/16	1074.35
	1	69.10	73.05	1069.64
9	END	1	3/16	1702.58
	1	69.10	66.73	1699.86

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

10	STA	1	3/16	1844.27
	1	818.55	482.00	1580.81

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
10	END 1	1 818.55	3/16 505.62	1349.72 946.61
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
				CH= 3.00
				CV= 1.50
-----				
11	STA 1	1 27.13	3/16 28.65	820.89 819.94
11	END 1	1 27.13	3/16 21.67	914.17 913.51
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
				CH= 3.00
				CV= 1.50
-----				
12	STA 1	1 19.02	3/16 10.56	913.77 913.51
12	END 1	1 19.02	3/16 16.88	860.77 860.39
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
				CH= 3.00
				CV= 1.50
-----				
13	STA 1	1 19.30	3/16 29.97	861.13 860.39
13	END 1	1 19.30	3/16 36.29	501.03 499.34
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
				CH= 3.00
				CV= 1.50
-----				
14	STA 1	1 18.99	3/16 49.38	502.14 499.34
14	END 1	1 18.99	3/16 55.70	556.55 553.43
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
				CH= 3.00
				CV= 1.50



STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

15	STA 1	1 19.53	3/16 69.33	558.09 553.42
----	----------	------------	---------------	------------------

15	END 1	1 19.53	3/16 72.75	1045.48 1042.77
----	----------	------------	---------------	--------------------

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

16	STA 1	1 19.53	3/16 72.75	1045.48 1042.77
----	----------	------------	---------------	--------------------

16	END 1	1 19.53	3/16 69.33	558.09 553.42
----	----------	------------	---------------	------------------

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

17	STA 1	1 18.99	3/16 55.70	556.55 553.43
----	----------	------------	---------------	------------------

17	END 1	1 18.99	3/16 49.38	502.14 499.34
----	----------	------------	---------------	------------------

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

18	STA 1	1 19.30	3/16 36.29	501.03 499.34
----	----------	------------	---------------	------------------

18	END 1	1 19.30	3/16 29.97	861.13 860.39
----	----------	------------	---------------	------------------

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

19	STA 1	1 19.02	3/16 16.87	860.76 860.39
----	----------	------------	---------------	------------------

19	END 1	1 19.02	3/16 10.56	913.78 913.52
----	----------	------------	---------------	------------------

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

20	STA 1	1 27.13	3/16 21.67	914.17 913.51
20	END 1	1 27.13	3/16 28.65	820.89 819.94

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

21	STA 1	1 818.55	3/16 505.62	1349.72 946.61
21	END 1	1 818.55	3/16 482.00	1844.27 1580.82

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

22	STA 1	1 69.10	3/16 66.73	1702.59 1699.87
22	END 1	1 69.10	3/16 73.05	1074.34 1069.63

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

23	STA 1	1 67.46	3/16 86.14	1075.22 1069.63
23	END 1	1 67.46	3/16 92.46	323.50 302.58

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

24	STA 1	1 120.10	3/16 140.80	335.63 280.00
----	----------	-------------	----------------	------------------

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
24	END 1	1 120.10	3/16 145.62	1272.19 1258.11
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
25	STA 1	1 0.00	3/16 2.41	1192.57 1192.57
25	END 1	1 0.00	3/16 0.00	1185.94 1185.94
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
26	STA 1	1 0.00	3/16 0.00	1185.94 1185.94
26	END 1	1 0.00	3/16 2.41	1192.57 1192.57
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
27	STA 1	1 120.10	3/16 145.62	1272.19 1258.11
27	END 1	1 120.10	3/16 140.80	335.63 280.00
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
28	STA 1	1 67.46	3/16 92.46	323.51 302.58
28	END 1	1 67.46	3/16 86.14	1075.22 1069.64
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

29	STA	1	3/16	1074.35
	1	69.10	73.05	1069.64
29	END	1	3/16	1702.57
	1	69.10	66.73	1699.86

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

30	STA	1	3/16	1844.27
	1	818.55	482.00	1580.81
30	END	1	3/16	1349.72
	1	818.55	505.62	946.61

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

31	STA	1	3/16	820.89
	1	27.13	28.65	819.94
31	END	1	3/16	914.17
	1	27.13	21.67	913.51

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

32	STA	1	3/16	913.77
	1	19.02	10.56	913.51
32	END	1	3/16	860.77
	1	19.02	16.87	860.39

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

33	STA	1	3/16	861.13
	1	19.30	29.97	860.39
33	END	1	3/16	501.03
	1	19.30	36.29	499.34

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
38	END 1	1 19.30	3/16 29.97	861.13 860.39
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
39	STA 1	1 19.02	3/16 16.87	860.77 860.39
39	END 1	1 19.02	3/16 10.56	913.78 913.52
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
40	STA 1	1 27.13	3/16 21.67	914.18 913.52
40	END 1	1 27.13	3/16 28.65	820.89 819.94
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
41	STA 1	1 92.52	3/16 155.29	1041.54 1025.74
41	END 1	1 92.52	3/16 138.89	662.45 641.09
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
42	STA 1	1 98.40	3/16 125.13	660.55 641.08
42	END 1	1 98.40	3/16 122.63	1093.67 1082.31
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

43	STA 1	1 1.61	3/16 59.69	1164.69 1163.16
43	END 1	1 1.61	3/16 55.87	1646.75 1645.80

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

44	STA 1	1 0.23	3/16 42.78	1646.37 1645.81
44	END 1	1 0.23	3/16 36.46	2211.86 2211.56

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

45	STA 1	1 0.54	3/16 23.37	2211.68 2211.56
45	END 1	1 0.54	3/16 17.05	2491.47 2491.41

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

46	STA 1	1 0.00	3/16 3.42	2491.42 2491.41
46	END 1	1 0.00	3/16 3.42	2491.41 2491.40

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

47	STA 1	1 0.54	3/16 17.05	2491.47 2491.41
47	END 1	1 0.54	3/16 23.37	2211.68 2211.56

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
48	STA 1	1 0.23	3/16 36.46	2211.86 2211.56
48	END 1	1 0.23	3/16 42.78	1646.37 1645.81
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
49	STA 1	1 1.61	3/16 55.88	1646.77 1645.82
49	END 1	1 1.61	3/16 59.69	1164.67 1163.14
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
50	STA 1	1 98.40	3/16 122.63	1093.68 1082.32
50	END 1	1 98.40	3/16 125.13	660.55 641.08
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
51	STA 1	1 92.51	3/16 138.89	662.46 641.10
51	END 1	1 92.51	3/16 155.29	1041.55 1025.75
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
52	STA 1	1 92.52	3/16 155.29	1041.55 1025.74

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
52	END 1	1 92.52	3/16 138.89	662.45 641.09
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
53	STA 1	1 98.40	3/16 125.13	660.55 641.08
53	END 1	1 98.40	3/16 122.63	1093.68 1082.32
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
54	STA 1	1 1.61	3/16 59.69	1164.69 1163.16
54	END 1	1 1.61	3/16 55.87	1646.74 1645.79
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
55	STA 1	1 0.23	3/16 42.78	1646.37 1645.81
55	END 1	1 0.23	3/16 36.46	2211.86 2211.56
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
56	STA 1	1 0.54	3/16 23.37	2211.69 2211.57
56	END 1	1 0.54	3/16 17.05	2491.46 2491.40
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				



STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

57	STA 1	1 0.00	3/16 3.42	2491.41 2491.41
57	END 1	1 0.00	3/16 3.42	2491.41 2491.41

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

58	STA 1	1 0.54	3/16 17.05	2491.47 2491.41
58	END 1	1 0.54	3/16 23.37	2211.68 2211.56

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

59	STA 1	1 0.23	3/16 36.46	2211.87 2211.57
59	END 1	1 0.23	3/16 42.78	1646.36 1645.80

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

60	STA 1	1 1.61	3/16 55.87	1646.76 1645.81
60	END 1	1 1.61	3/16 59.69	1164.68 1163.15

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

61	STA 1	1 98.40	3/16 122.63	1093.65 1082.29
61	END 1	1 98.40	3/16 125.13	660.57 641.11

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
62	STA 1	1 92.52	3/16 138.89	662.45 641.08
62	END 1	1 92.52	3/16 155.29	1041.54 1025.74
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH= 3.00 CV= 1.50
-----				
63	STA 1	1 153.32	3/16 133.15	498.29 455.03
63	END 1	1 153.32	3/16 127.21	425.89 376.41
-----				
AX=	10.00 SZ=	9.00 SY=	7.33 JW=	20.83 CH= 1.50 CV= 1.00
-----				
64	STA 1	1 156.26	3/16 103.65	420.54 376.43
64	END 1	1 156.26	3/16 106.56	432.87 389.36
-----				
AX=	10.00 SZ=	9.00 SY=	7.33 JW=	20.83 CH= 1.50 CV= 1.00
-----				
65	STA 1	1 0.00	3/16 6.81	231.01 230.91
65	END 1	1 0.00	3/16 0.00	334.91 334.91
-----				
AX=	10.00 SZ=	9.00 SY=	7.33 JW=	20.83 CH= 1.50 CV= 1.00
-----				
66	STA 1	1 0.00	3/16 0.00	334.91 334.91

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
66	END 1	1 0.00	3/16 6.81	231.01 230.91
-----				
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83
		CH= 1.50	CV= 1.00	
67	STA 1	1 156.26	3/16 106.56	432.88 389.37
67	END 1	1 156.26	3/16 103.65	420.53 376.41
-----				
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83
		CH= 1.50	CV= 1.00	
68	STA 1	1 153.32	3/16 127.21	425.88 376.41
68	END 1	1 153.32	3/16 133.15	498.29 455.03
-----				
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83
		CH= 1.50	CV= 1.00	
69	STA 1	1 153.32	3/16 133.15	498.29 455.04
69	END 1	1 153.32	3/16 127.21	425.89 376.42
-----				
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83
		CH= 1.50	CV= 1.00	
70	STA 1	1 156.26	3/16 103.65	420.54 376.42
70	END 1	1 156.26	3/16 106.56	432.88 389.37
-----				
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83
		CH= 1.50	CV= 1.00	

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS		
71	STA 1	1 0.00	3/16 6.81	231.01 230.91		
71	END 1	1 0.00	3/16 0.00	334.91 334.91		
-----						
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83	CH= 1.50	CV= 1.00
72	STA 1	1 0.00	3/16 0.00	334.91 334.91		
72	END 1	1 0.00	3/16 6.81	231.01 230.91		
-----						
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83	CH= 1.50	CV= 1.00
73	STA 1	1 156.26	3/16 106.56	432.88 389.37		
73	END 1	1 156.26	3/16 103.65	420.54 376.42		
-----						
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83	CH= 1.50	CV= 1.00
74	STA 1	1 153.32	3/16 127.21	425.90 376.43		
74	END 1	1 153.32	3/16 133.16	498.30 455.05		
-----						
AX=	10.00	SZ= 9.00	SY= 7.33	JW= 20.83	CH= 1.50	CV= 1.00
76	STA 1	1 86.41	3/16 134.58	1481.95 1473.30		
76	END 1	1 86.41	3/16 97.15	498.83 481.59		

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

77	STA 1	1 86.41	3/16 134.58	1481.95 1473.30
77	END 1	1 86.41	3/16 97.15	498.83 481.59

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

88	STA 1	1 86.41	3/16 134.58	1481.95 1473.29
88	END 1	1 86.41	3/16 97.15	498.83 481.59

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

89	STA 1	1 86.41	3/16 134.58	1481.95 1473.30
89	END 1	1 86.41	3/16 97.15	498.83 481.59

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

100	STA 1	1 91.93	3/16 87.97	2911.08 2908.30
100	END 1	1 91.93	3/16 87.97	1323.07 1316.94

-----  
 AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
 -----

101	STA 1	1 23.49	3/16 22.61	1166.69 1166.23
-----	----------	------------	---------------	--------------------

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
101	END 1	1 23.49	3/16 22.61	514.34 513.30
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
		CH= 1.75	CV= 1.75	
-----				
102	STA 1	1 14.46	3/16 14.46	458.20 457.75
102	END 1	1 14.46	3/16 14.46	459.75 459.29
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
		CH= 1.75	CV= 1.75	
-----				
103	STA 1	1 91.93	3/16 87.96	2911.08 2908.30
103	END 1	1 91.93	3/16 87.96	1323.07 1316.94
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
		CH= 1.75	CV= 1.75	
-----				
104	STA 1	1 23.49	3/16 22.61	1166.69 1166.23
104	END 1	1 23.49	3/16 22.61	514.34 513.30
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
		CH= 1.75	CV= 1.75	
-----				
105	STA 1	1 14.46	3/16 14.46	458.22 457.76
105	END 1	1 14.46	3/16 14.46	459.76 459.31
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
		CH= 1.75	CV= 1.75	

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
106	STA 1	1 91.93	3/16 87.97	2911.08 2908.30
106	END 1	1 91.93	3/16 87.97	1323.07 1316.94

AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75

107	STA 1	1 23.49	3/16 22.61	1166.69 1166.23
107	END 1	1 23.49	3/16 22.61	514.34 513.30

AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75

108	STA 1	1 14.46	3/16 14.46	458.21 457.75
108	END 1	1 14.46	3/16 14.46	459.75 459.30

AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75

109	STA 1	1 91.93	3/16 87.96	2911.08 2908.30
109	END 1	1 91.93	3/16 87.96	1323.07 1316.94

AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75

110	STA 1	1 23.49	3/16 22.61	1166.69 1166.23
110	END 1	1 23.49	3/16 22.61	514.34 513.30

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
				CH= 1.75
				CV= 1.75
-----				
111	STA	1	3/16	458.21
	1	14.46	14.46	457.76
111	END	1	3/16	459.76
	1	14.46	14.46	459.30
-----				
AX=	14.00	SZ= 16.33	SY= 16.33	JW= 57.17
				CH= 1.75
				CV= 1.75
-----				
116	STA	1	3/16	696.81
	1	41.67	44.34	694.14
116	END	1	3/16	341.89
	1	41.67	39.37	337.05
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
-----				
117	STA	1	3/16	535.97
	1	88.97	91.48	520.56
117	END	1	3/16	673.19
	1	88.97	86.48	661.66
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
-----				
118	STA	1	3/16	1274.72
	1	0.00	2.20	1274.72
118	END	1	3/16	1259.64
	1	0.00	0.00	1259.64
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
-----				
119	STA	1	3/16	1259.64
	1	0.00	0.00	1259.64



STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
119	END 1	1 0.00	3/16 2.20	1274.71 1274.71
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
120	STA 1	1 88.97	3/16 86.48	673.19 661.66
120	END 1	1 88.97	3/16 91.48	535.98 520.56
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
121	STA 1	1 41.67	3/16 39.37	341.89 337.05
121	END 1	1 41.67	3/16 44.34	696.81 694.15
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
122	STA 1	1 12.21	3/16 17.73	477.42 476.93
122	END 1	1 12.21	3/16 12.03	234.73 234.10
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00
123	STA 1	1 3.83	3/16 10.96	415.00 414.84
123	END 1	1 3.83	3/16 9.44	339.61 339.45
-----				
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67
				CH= 1.00
				CV= 1.00

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS		
124	STA 1	1 3.83	3/16 9.44	339.61 339.46		
124	END 1	1 3.83	3/16 10.96	415.01 414.84		
-----						
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67	CH= 1.00	CV= 1.00
125	STA 1	1 12.21	3/16 12.03	234.73 234.11		
125	END 1	1 12.21	3/16 17.73	477.42 476.93		
-----						
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67	CH= 1.00	CV= 1.00
126	STA 1	1 41.67	3/16 44.34	696.81 694.15		
126	END 1	1 41.67	3/16 39.37	341.89 337.05		
-----						
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67	CH= 1.00	CV= 1.00
127	STA 1	1 88.97	3/16 91.48	535.97 520.56		
127	END 1	1 88.97	3/16 86.48	673.19 661.66		
-----						
AX=	8.00	SZ= 5.33	SY= 5.33	JW= 10.67	CH= 1.00	CV= 1.00
128	STA 1	1 0.00	3/16 2.20	1274.74 1274.74		
128	END 1	1 0.00	3/16 0.00	1259.62 1259.62		

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
129	STA 1	1 0.00	3/16 0.00	1259.61 1259.61
129	END 1	1 0.00	3/16 2.20	1274.75 1274.75
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
130	STA 1	1 88.97	3/16 86.48	673.19 661.66
130	END 1	1 88.97	3/16 91.48	535.98 520.56
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
131	STA 1	1 41.67	3/16 39.37	341.89 337.05
131	END 1	1 41.67	3/16 44.34	696.81 694.15
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
132	STA 1	1 12.21	3/16 17.73	477.42 476.93
132	END 1	1 12.21	3/16 12.03	234.73 234.10
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
133	STA 1	1 3.83	3/16 10.96	415.00 414.84

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
133	END 1	1 3.83	3/16 9.44	339.61 339.45
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
134	STA 1	1 3.83	3/16 9.44	339.61 339.46
134	END 1	1 3.83	3/16 10.96	415.01 414.84
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
135	STA 1	1 12.21	3/16 12.03	234.73 234.11
135	END 1	1 12.21	3/16 17.73	477.42 476.93
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
136	STA 1	1 23.28	3/16 32.11	957.71 956.89
136	END 1	1 23.28	3/16 34.88	1028.36 1027.50
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
137	STA 1	1 23.28	3/16 32.11	957.71 956.89
137	END 1	1 23.28	3/16 34.88	1028.36 1027.50
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

138	STA	1	3/16	650.66
	1	19.87	31.05	649.61

138	END	1	3/16	938.56
	1	19.87	34.80	937.70

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

139	STA	1	3/16	650.66
	1	19.87	31.05	649.61

139	END	1	3/16	938.56
	1	19.87	34.80	937.71

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

140	STA	1	3/16	957.71
	1	23.28	32.11	956.89

140	END	1	3/16	1028.36
	1	23.28	34.88	1027.50

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

141	STA	1	3/16	957.71
	1	23.28	32.11	956.89

141	END	1	3/16	1028.36
	1	23.28	34.88	1027.50

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

142	STA	1	3/16	650.66
	1	19.87	31.05	649.61

142	END	1	3/16	938.56
	1	19.87	34.80	937.71

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

143	STA 1	1 19.87	3/16 31.05	650.66 649.61
143	END 1	1 19.87	3/16 34.80	938.56 937.71

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

144	STA 1	1 48.32	3/16 44.48	1326.66 1325.04
144	END 1	1 48.32	3/16 44.48	575.75 571.99

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

145	STA 1	1 48.32	3/16 44.48	1326.66 1325.04
145	END 1	1 48.32	3/16 44.48	575.75 571.99

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

146	STA 1	1 0.00	3/16 4.76	566.33 566.31
146	END 1	1 0.00	3/16 4.76	359.78 359.75

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

147	STA 1	1 48.32	3/16 44.48	1326.67 1325.04
-----	----------	------------	---------------	--------------------

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

147	END 1	1 48.32	3/16 44.48	575.75 571.99
-----	----------	------------	---------------	------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

148	STA 1	1 48.32	3/16 44.48	1326.66 1325.04
-----	----------	------------	---------------	--------------------

148	END 1	1 48.32	3/16 44.48	575.75 571.99
-----	----------	------------	---------------	------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

149	STA 1	1 0.00	3/16 4.76	566.33 566.31
-----	----------	-----------	--------------	------------------

149	END 1	1 0.00	3/16 4.76	359.78 359.74
-----	----------	-----------	--------------	------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

150	STA 1	1 55.75	3/16 53.92	346.54 337.75
-----	----------	------------	---------------	------------------

150	END 1	1 55.75	3/16 58.59	205.03 188.41
-----	----------	------------	---------------	------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

151	STA 1	1 55.75	3/16 53.92	346.55 337.76
-----	----------	------------	---------------	------------------

151	END 1	1 55.75	3/16 58.59	205.03 188.41
-----	----------	------------	---------------	------------------

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

152	STA	1	3/16	196.32
	1	16.44	17.55	194.85
152	END	1	3/16	220.34
	1	16.44	21.90	218.63

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

153	STA	1	3/16	196.33
	1	16.44	17.55	194.85
153	END	1	3/16	220.34
	1	16.44	21.90	218.63

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

154	STA	1	3/16	346.54
	1	55.75	53.92	337.75
154	END	1	3/16	205.03
	1	55.75	58.59	188.41

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

155	STA	1	3/16	346.55
	1	55.75	53.92	337.76
155	END	1	3/16	205.03
	1	55.75	58.59	188.41

AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00

156	STA	1	3/16	196.33
	1	16.44	17.55	194.85
156	END	1	3/16	220.34
	1	16.44	21.90	218.63



STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH=
				1.00 CV=
				1.00
-----				
157	STA	1	3/16	196.33
	1	16.44	17.55	194.85
157	END	1	3/16	220.34
	1	16.44	21.90	218.64
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH=
				1.00 CV=
				1.00
-----				

\*\*\*\*\* END OF TABULATED WELD DESIGN \*\*\*\*\*

110. STEEL TAKE OFF

STEEL TAKE-OFF

PROFILE	LENGTH (INCH)	WEIGHT (POUN)
ST TUB 60303	1338.00	1188.974
ST TUB 30203	302.00	140.164
ST TUB 20203	2668.99	959.262
ST TUB 35353	360.00	243.493
TOTAL =		2531.89

TOTAL VOLUME OF PRISMATIC SECTIONS = 329.78 CUBIC INCH

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

111. FINISH

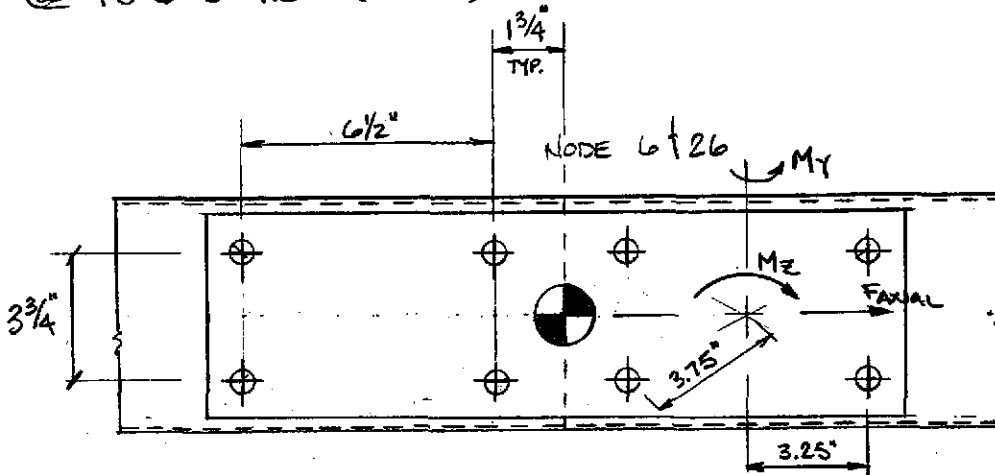
\*\*\*\*\* END OF STAAD-III \*\*\*\*\*

\*\*\*\* DATE= SEP 25,1996 TIME= 8:38:38 \*\*\*\*

\*\*\*\*\*  
 \* For questions on STAAD-III, contact: \*  
 \* Research Engineers, Inc at \*  
 \* Ph: (714) 974-2500 Fax: (714) 921-2543 \*  
 \*\*\*\*\*

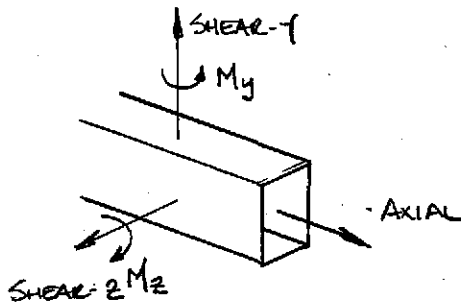
THRU BOLTED  
MOMENT CONNECTION

@ TS 6x3x3/16 (2 PCS)



MEMBER 5 JT 6 (BSCLNRM 3)

AXIAL	833 lbs.	TORSION	0.
SHEAR-Y	0.	MOM-Y	258 in-lbs.
SHEAR-Z	0.	MOM-Z	4915 in-lbs.



BOLTS 1/2" φ HEX HEAD (A-307)  
 $A_k = .126 \text{ in}^2$      $A_{TENS.} = .142 \text{ in}^2$   
 $F_v = 0.17 F_u$   
 $F_u = 58 \text{ KSI} \therefore F_v = .17(58 \text{ KSI})$   
 $= 9.86 \text{ KSI}$   
 $V_{ALL} = 9.86 \text{ KSI} (.126 \text{ in}^2)$   
 $= 1.242 \text{ K} \approx 1242 \text{ LBS/BOLT}$   
 (SINGLE SHEAR)  
 $F_t = .33 F_u = 19.14 \text{ KSI}$   
 $T_{ALL} = 19.14 \text{ KSI} (.142 \text{ in}^2) = 2718 \text{ LBS/BOLT}$

CONSERVATIVELY; (ASSUMING SINGLE SHEAR)

SHEAR FORCE PER BOLT

$$V = \frac{\text{AXIAL}}{4 \text{ BOLTS}} + \frac{M_z}{4 \text{ BOLTS} (3.75 \text{ in})} = \frac{833 \text{ lbs}}{4 \text{ BOLTS}} + \frac{4915 \text{ lbs-in}}{4 \text{ BOLTS} (3.75 \text{ in})} = 536 \text{ lbs/BOLT (DOUBLE SHEAR)}$$

TENSION FORCE PER BOLT

$$T = \frac{M_y}{2 \text{ BOLTS} (3.25 \text{ in})} = \frac{258 \text{ in-lbs}}{2 \text{ BOLTS} (3.25 \text{ in})} = 40 \text{ lbs/BOLT}$$

= 268 lbs/bolt (SINGLE SHEAR)

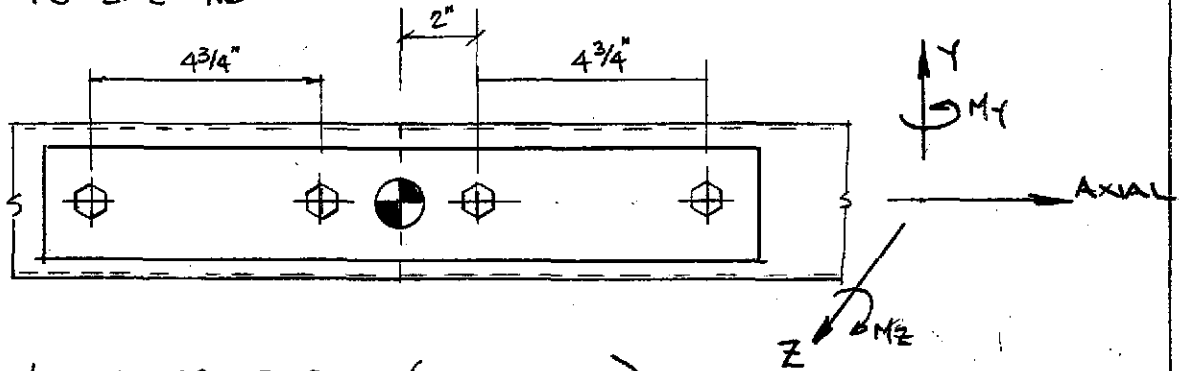
USE: 1/2" φ A-307  
HEX HEAD



THRU-BOLTED  
MOMENT CONNECTIONS (CON'T)

AT JTS 93 & 83

@ TS 2x2x3/16



MEMBER 128 JT 93 (BSCLNRM3)

AXIAL = 857 lbs

TORSION = 0.

SHEAR-Y = 0.

$M_y = 571$  in-lbs,

SHEAR-Z = 0.

$M_z = 117$  in-lbs.

BOLTS 3/8"

$A_k = .068$  in<sup>2</sup>

$A_{TENSILE} = .078$  in<sup>2</sup>

$F_v = 0.17 F_u = .17(58 \text{ KSI}) = 9.86 \text{ KSI}$

$V_{all} = 9.86 \text{ KSI} (.068 \text{ in}^2) = 670 \text{ lbs/BOLT (SINGLE SHEAR)}$

$F_t = .33 F_u = .33(58 \text{ KSI}) = 19.14 \text{ KSI}$

$T_{all} = 19.14 \text{ KSI} (.078 \text{ in}^2) = 1493 \text{ lbs/BOLT}$

CONSERVATIVELY;

SHEAR FORCE PER BOLT

$$V = \frac{857 \text{ lbs}}{2 \text{ BOLTS}} + \frac{117 \text{ in-lbs}}{2 \text{ BOLTS (2in)}} = 457.75 \text{ lbs/BOLT}$$

TENSION FORCE PER BOLT

$$T = \frac{571 \text{ in-lbs}}{2 \text{ BOLTS (2in)}} = 142.75 \text{ #/BOLT}$$

Revision No. 0  
Doc. No. V049-1-112  
Page 105 of 107

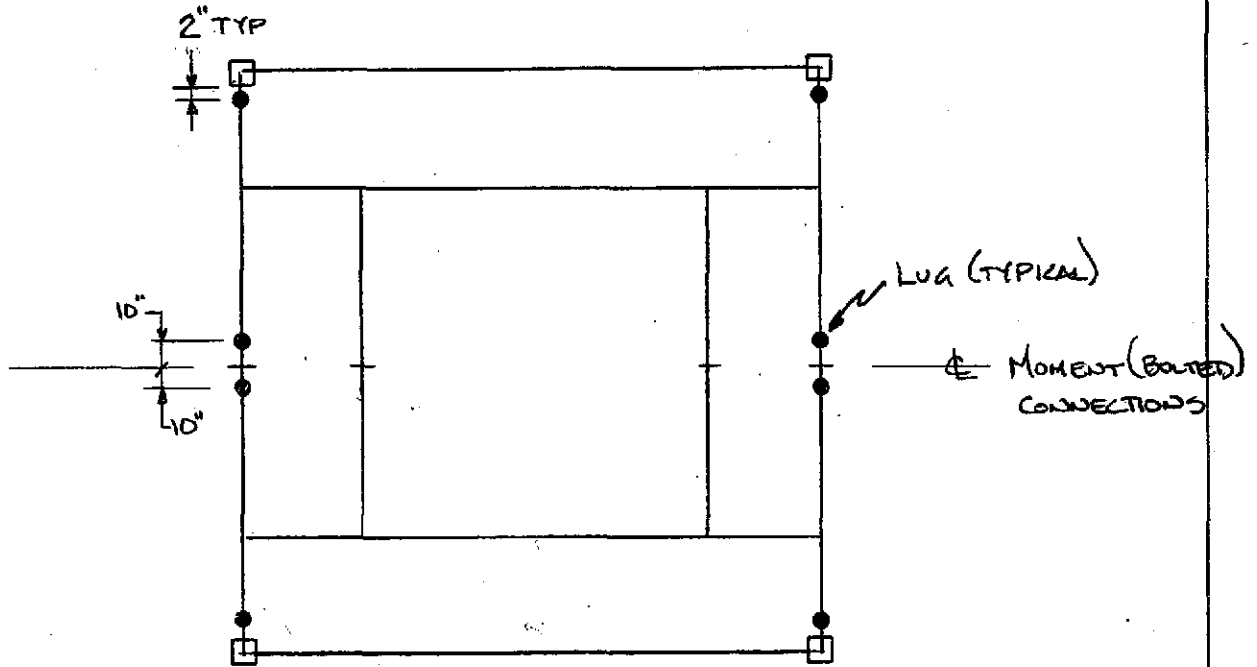
THE ABOVE SHEAR & TENSION ASSUMES SINGLE SHEAR  
ACTUAL SHEAR IS DOUBLE (I.E. HALF), THEREFORE QUITE  
CONSERVATIVE, ADDITIONALLY ONLY TWO BOLTS ARE ASSUMED  
TO TAKE ALL THE SHEAR & TENSION WHEN IN FACT THERE ARE 4 BOLTS.

USE: 3/8" A-307 BOLTS



LIFTING LUG

LOCATION OF LIFTING LUGS



ASSUME WEIGHT OF STRUCTURE + EQUIPMENT MOUNTED  
(AIR CIRCULATORS + PUMPS)

= 8000 lbs.

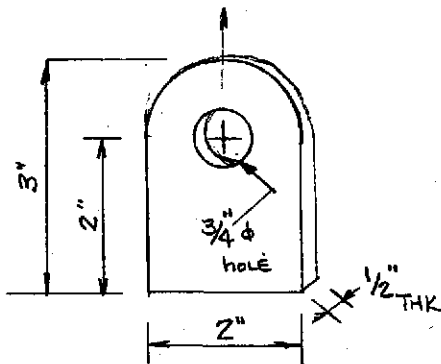
NOTE: CRANE IS A 5 TON CAPACITY CRANE

$$\frac{8000 \text{ lbs}}{8 \text{ LUGS}} = 1000 \text{ lbs/LUG}$$

$$\text{SHEAR} = \frac{P}{A} = \frac{1000 \text{ lbs}}{(\pi/8)(1/2)} = 3200 \text{ lb/in}^2$$

$$F_{\text{VALL}} = .4(36000 \text{ #/in}^2) = 14400 \text{ lb/in}^2$$

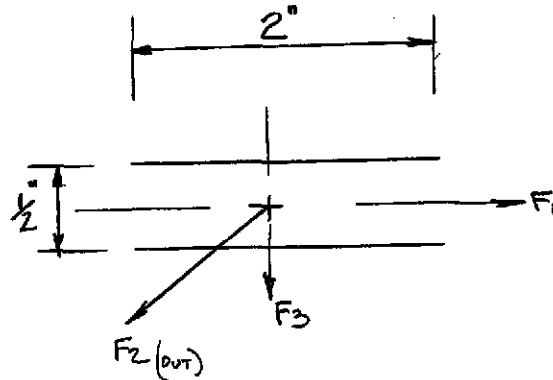
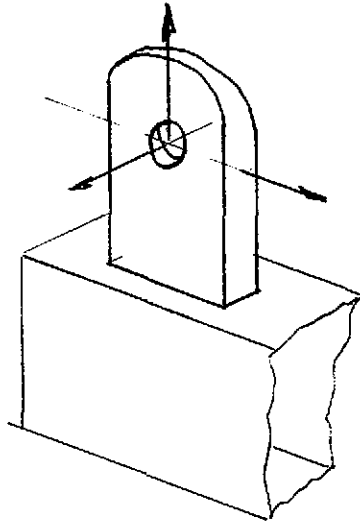
$$3200 \text{ #/in}^2 < 14400 \text{ #/in}^2$$



filename: BSC CLEAN RM

HORIZONTAL FILLET WELDS PARALLEL TO F1 AXIS

Between part LIFTING LUG AND TS 6X3



LOAD INPUT ( LBS., INCH-LBS. )

F1	F2	F3	M1	M2	M3
	1000.00				

GEOMETRIC DIMENSIONS

a	b	WELD STRESS (PSI)
0.500	3.000	21000

SECTION PROPERTIES

A	Sw1	Sw3	J	C1	C3
6.000	1.500	3.000	4.875	0.250	1.500

MAXIMUM WELD LOAD (f) - #/INCH

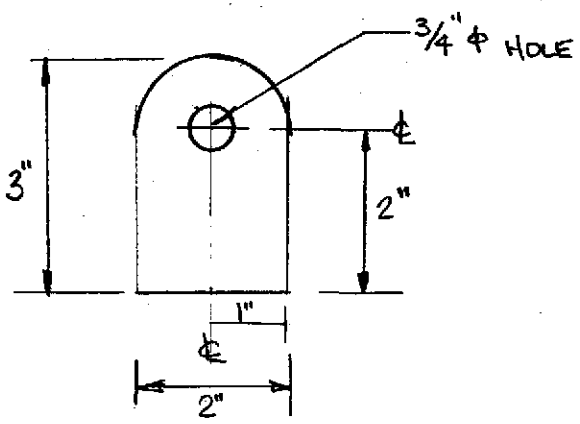
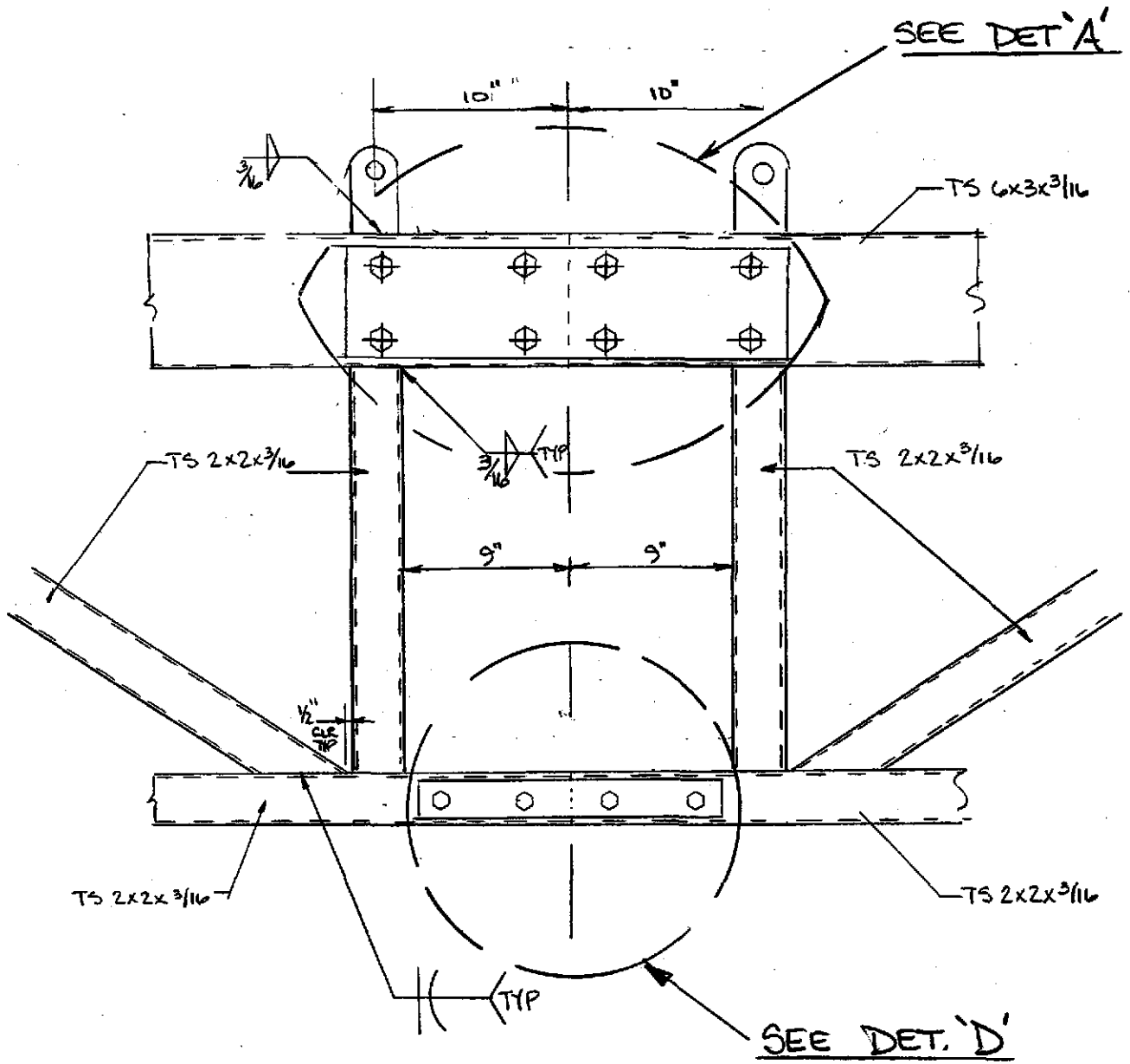
f
167

REQUIRED FILLET WELD SIZE (INCHES)

w
0.011

USE 3/16" FILLET 2" LONG (NEAR SIDE/FAR SIDE)

DETAIL DESIGN SKETCH

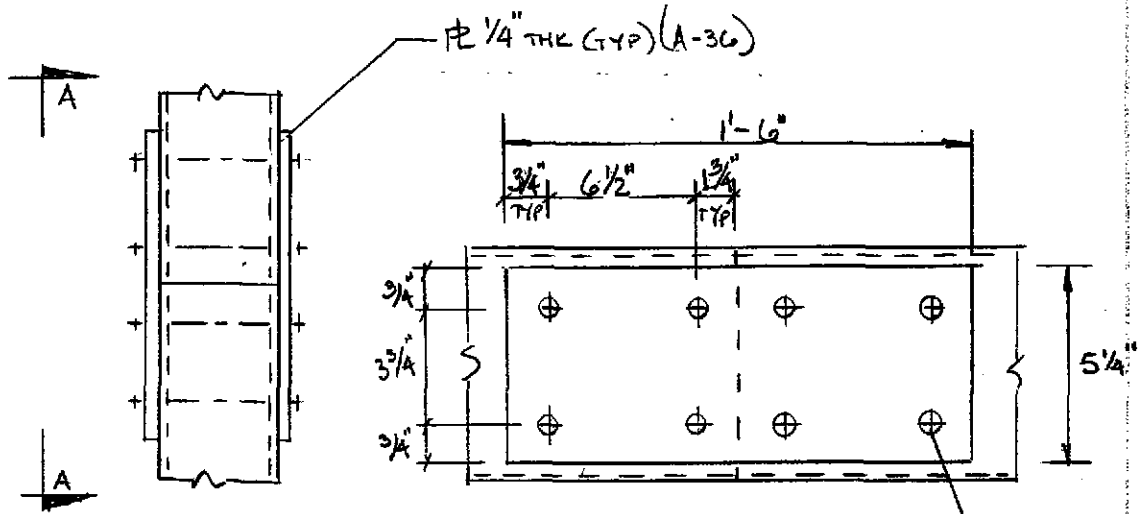


LIFTING LUG DETAIL

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



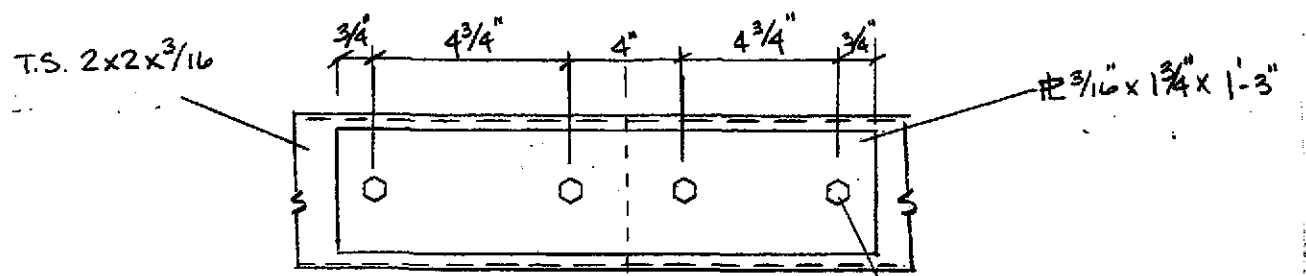
DETAIL DESIGN SKETCH



DET. 'A'  
(SPICE CONNECTION)  
DETAIL  
TYP 2 PLS.

DET. A  
SECTION A-A

1/2"  $\phi$  HEX HD  
- L=4 1/2"  
THRU BOLT  
W/ HEX NUTS  
& WASHER



DET. 'D'  
(TYP 2 PLS)

3/8"  $\phi$  HEX HD  
BOLT W/OUT WASHER  
(TYP)

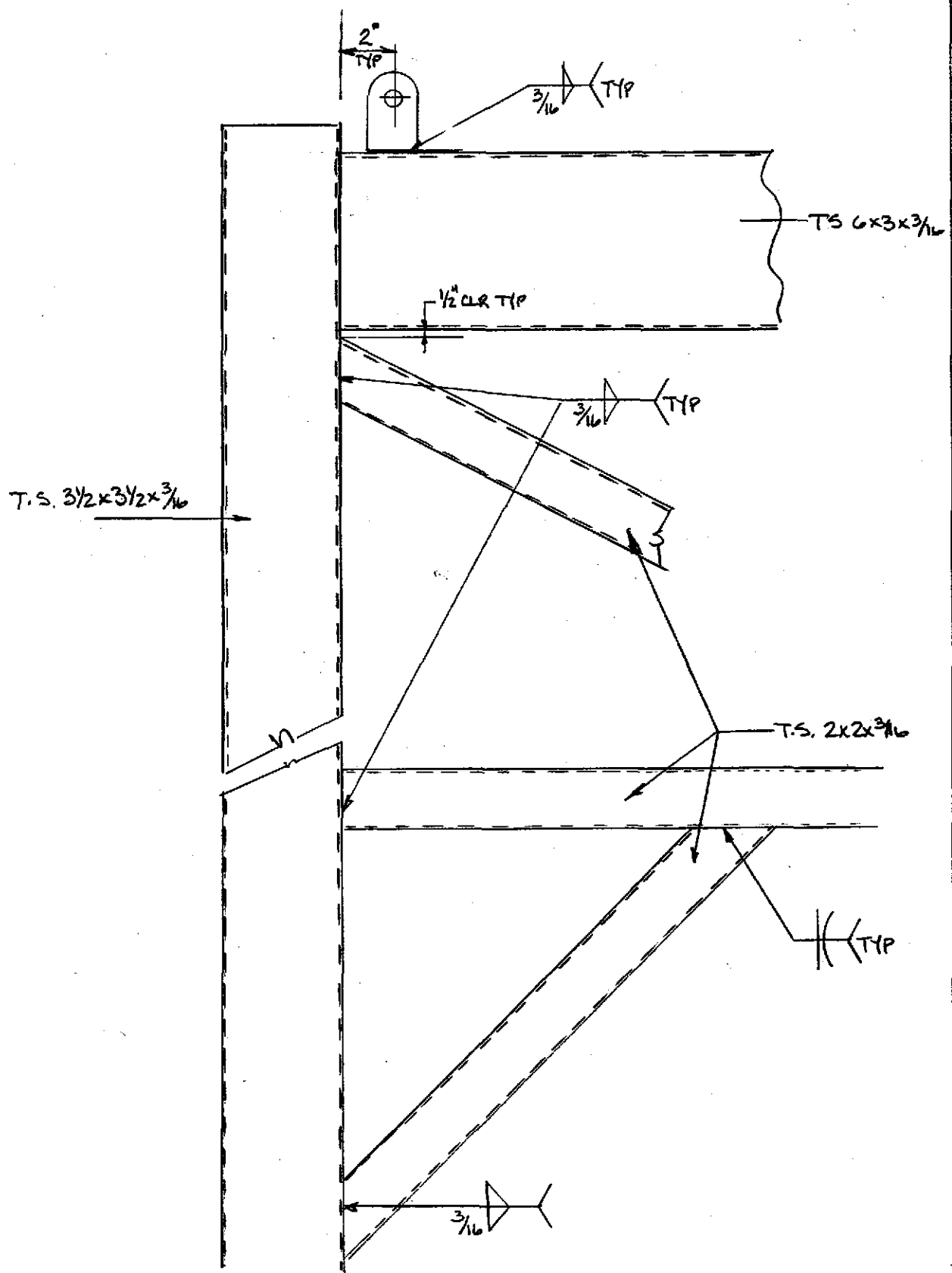
22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS





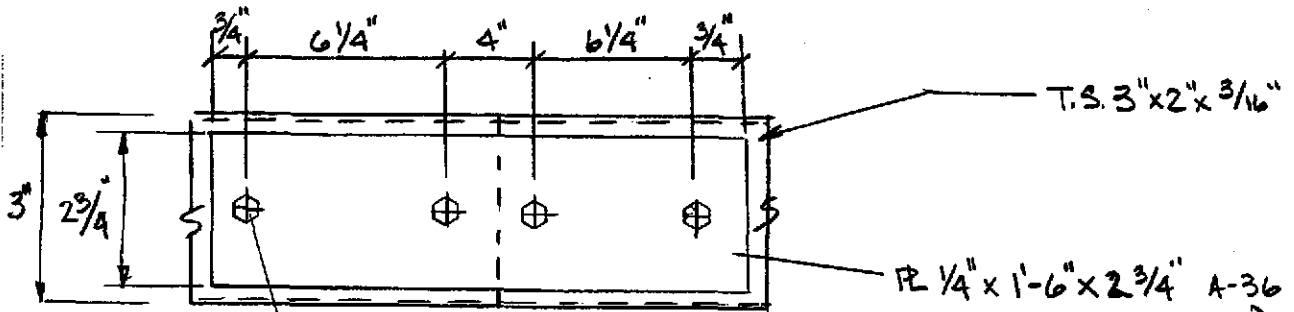
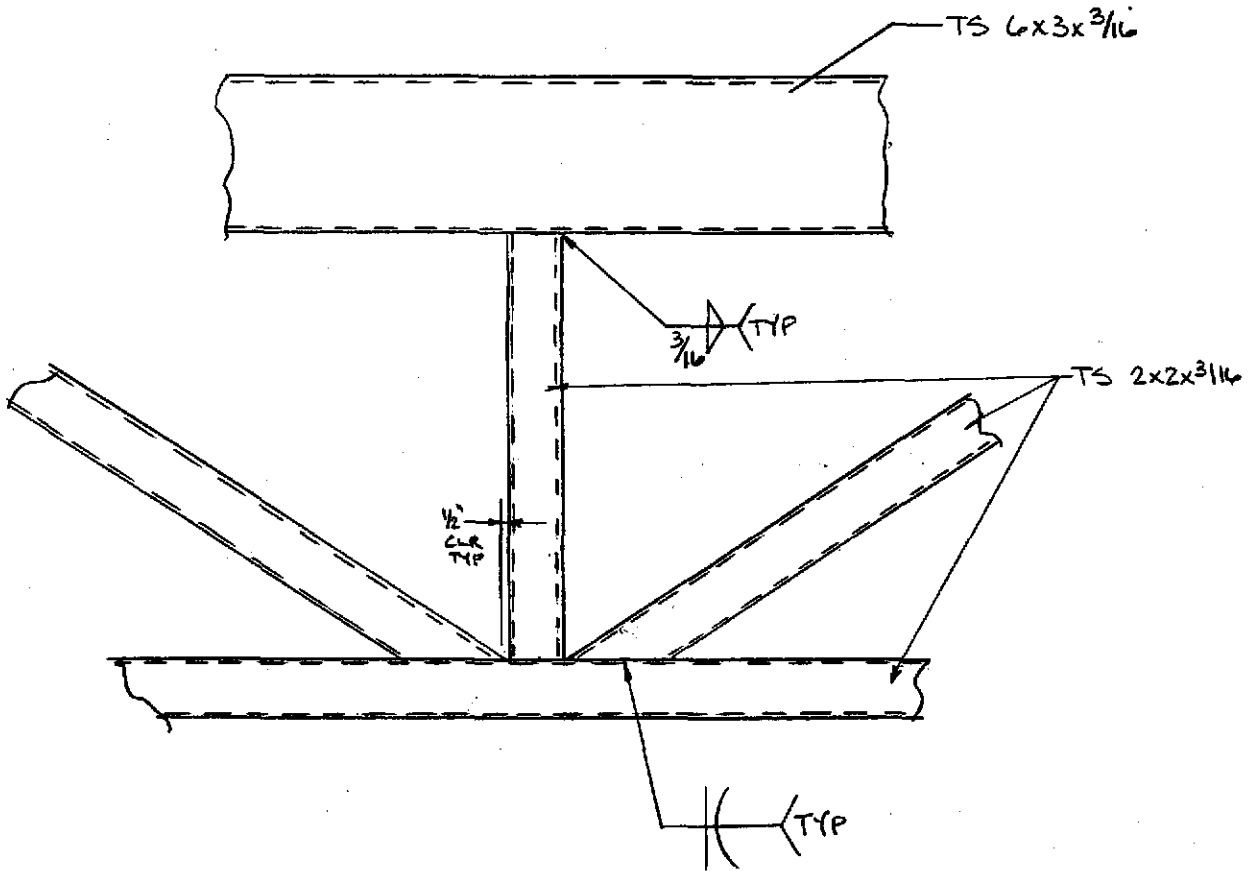
DETAIL DESIGN SKETCH

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



DETAIL DESIGN SKETCH

22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



MOMENT (BOLTED) CONNECTION  
 SPLICE DETAIL \*  
 (TYP 2 PLS)

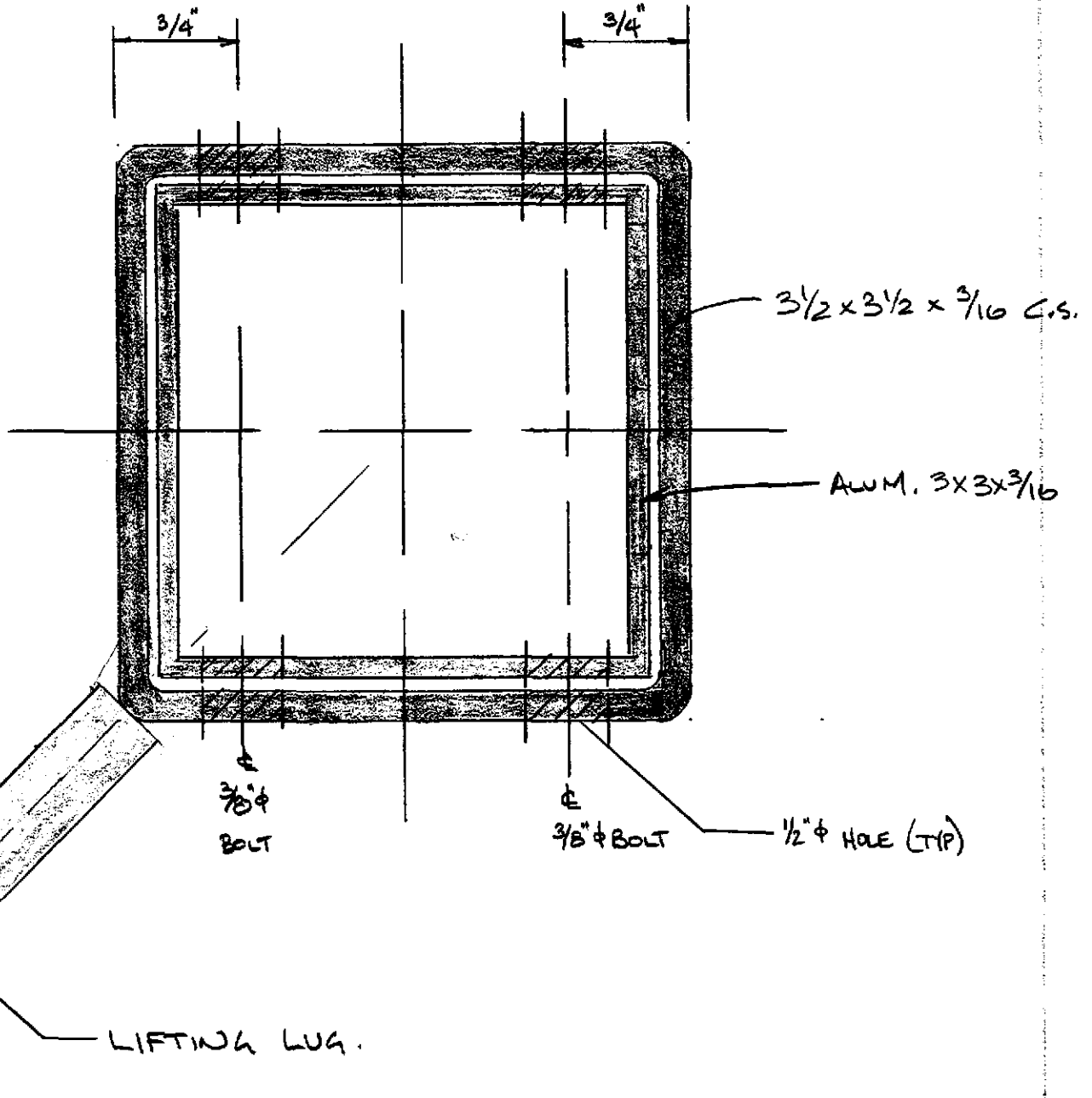
1/2" Hex HD  
 BOLT w/ NUT / WASHER

T.S. 3"x2"x3/16"  
 PL 1/4"x1'-6"x2 3/4" A-36  
 4 PLS REQ'D (TOTAL)

\* ONLY @ 3x2x3/16 T.S.

DETAIL DESK SKETCH

22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA					ENGINEERING CALCULATIONS	NO: V049-1-113 PAGE 1 OF 72
REV.	DEO #	DATE	BY:	CHECK	TITLE:  <b>HAM Portable Clean Room</b>	
0	349	10.7.96	WDB	RDC		
					BY: W. Bilynsky	DEPT.: 744
<b>PROJECT:</b> LIGO Vacuum Equipment					<b>PROJECT NO:</b> V59049	
<p><b>PURPOSE:</b></p> <p>Design mobile (portable) Clean Room for the Horizontal Access Module (HAM). The frame design must be able to withstand the installed weight of the air circulators and various pumps and must also be fairly lightweight to allow unconstrained mobility. Additionally, the HAM clean room frame will have adjustable (telescoping) legs for fitup and alignment.</p>						
<p><b>METHOD:</b></p> <p>Support frame is designed to AISC standards using classical hand calculations and STAAD-III computer program (release 21).</p>						
<p><b>ASSUMPTIONS:</b></p> <p>See calculation</p>						
<p><b>INPUTS:</b></p> <ol style="list-style-type: none"> <li>Design load = 10.0 lbs/ft<sup>2</sup></li> <li>Non-standard AISC Structural Members (see calculation)</li> </ol>						
<p><b>REFERENCES:</b></p> <ol style="list-style-type: none"> <li>STAAD-III , Research Engineers, Release 21</li> <li>AISC - ASD 9th edition</li> <li>Doc. No. V049-1-066 LIGO Vacuum Equipment Structural Design Criteria</li> <li>Aluminum Construction Manual, Section 3, Engineering data for aluminum structures.</li> </ol>						
<p><b>CALCULATIONS:</b></p>						
<p><b>CONCLUSIONS:</b></p> <p>The requirements of the AISC Codes and Standards and the Ligo Vacuum Equipment Structural Design Criteria are met.</p>						
<p><b>NOTES:</b> STAAD-III Computer File: HAMCLNRM.*</p>						

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-113
		Rev. No. 0
		Page 2 of 72
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: HAM (Horizontal Access Module) Portable Cleanroom		

TABLE OF CONTENTS

Revision History	3
Design Loading Condition	4
Member Properties	4
HAM Clean Room	
STAAD Model	5
STAAD Computer Generated Plots	7
STAAD Output File	8
Lifting Lugs	69
Detail Design Sketches	71
Final Design Drawing	72

PROCESS SYSTEMS INTERNATIONAL, INC. WESTBOROUGH, MA	ENGINEERING CALCULATIONS	NO: V049-1-113
		Rev. No. 0
		Page 3 of 72
PROJECT: LIGO VACUUM EQUIPMENT	PROJECT NO: V59049	
CALCULATION TITLE: HAM (Horizontal Access Module) Portable Cleanroom		

REVISION HISTORY

Rev. 0            Original Issue  
   October 7, 1996

## DESIGN LOADING CONDITION

2'-0" x 4'-0" PANELS WILL PROVIDE SUPPORT FOR PUMPS, AIR CIRCULATORS, DUCT WORK LIGHTING ETC.

ASSUME 50#/PANEL

$$2'-0" \times 4'-0" = 8 \text{ FT}^2$$

$$\frac{50 \text{ lbs}}{8 \text{ FT}^2} = 6.25 \text{ lbs/FT}^2 = 0.043 \frac{\text{lbs}}{\text{IN}^2}$$

ASSUME ADDITIONAL WEIGHT OF LIVE LOADS FROM MAINTENANCE OPERATORS.  $\therefore$  USE  $0.10 \frac{\text{lb}}{\text{IN}^2}$   
 $\rightarrow$  DESIGN LOAD = 10 psf

MEMBER PROPERTIES - ALL MEMBERS ARE STANDARD AISC STEEL SECTIONS THE EXCEPTIONS ARE THE RETRACTABLE LEGS AND THE TEE SECTIONS WHICH MAKE UP THE PANEL SECTIONS THESE ARE ALUMINUM AND REQUIRE PRISMATIC PROPERTIES FOR PROPER MODELING.

• ALUMINUM LEGS 3" x 3" x 1/8" REF. ALUMINUM CONSTRUCTION MANUAL

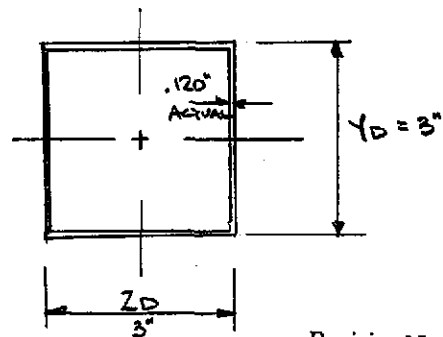
$$A_x = 1.382 \text{ in}^2$$

$$I_y = 1.914 \text{ in}^4$$

$$I_z = 1.914 \text{ in}^4$$

$$Y_D = 3.0 \text{ in}$$

$$Z_D = 3.0 \text{ in}$$



Revision No. 0  
 Doc. No. V049-1-113  
 Page 4 of 72

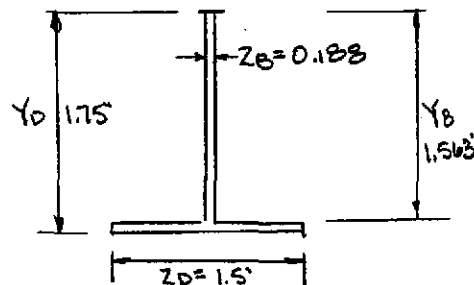
• ALUMINUM TEE

$$Y_D = 1.75 \text{ in}$$

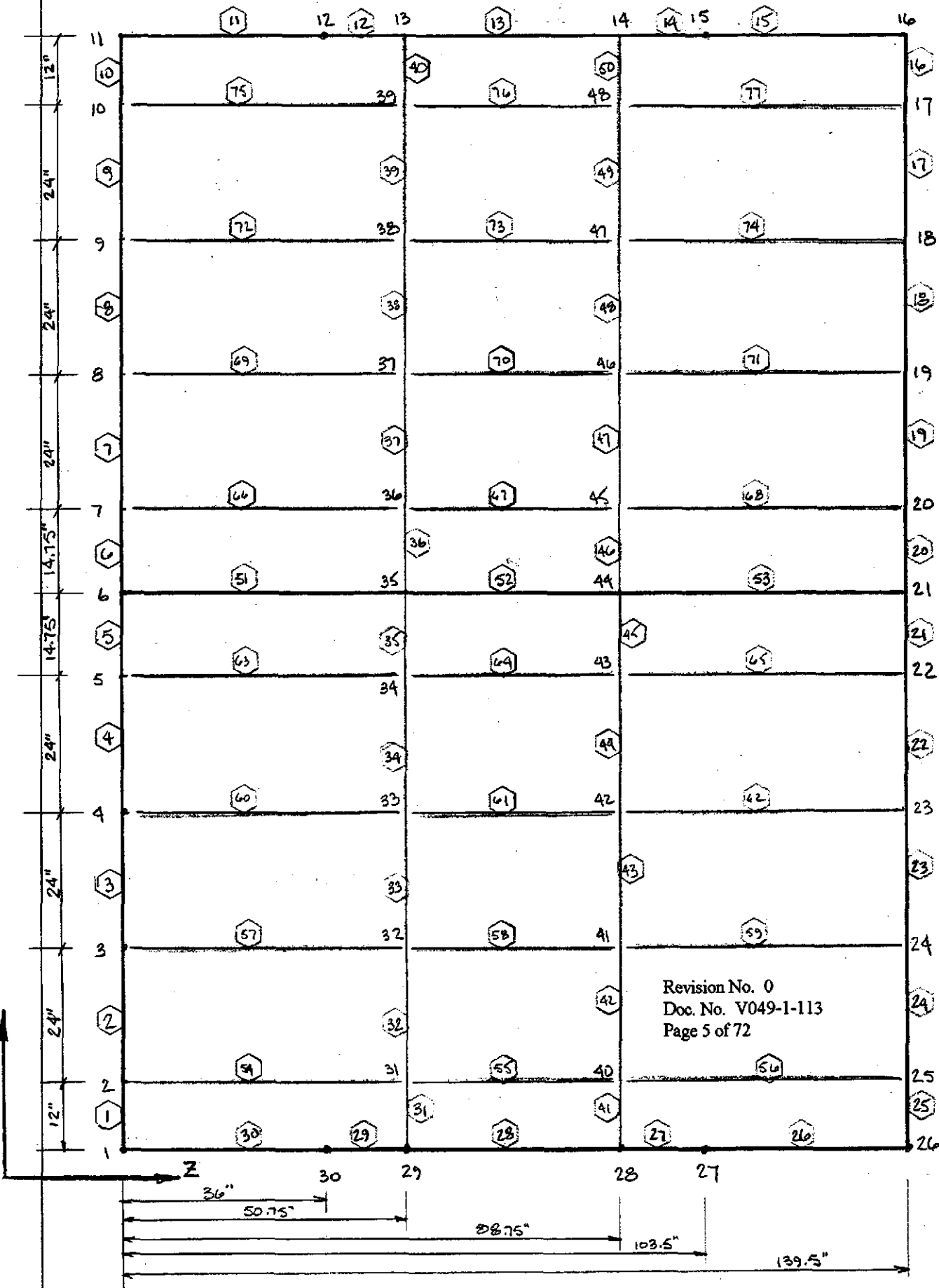
$$Z_D = 1.50 \text{ in}$$

$$Y_B = 1.563 \text{ in}$$

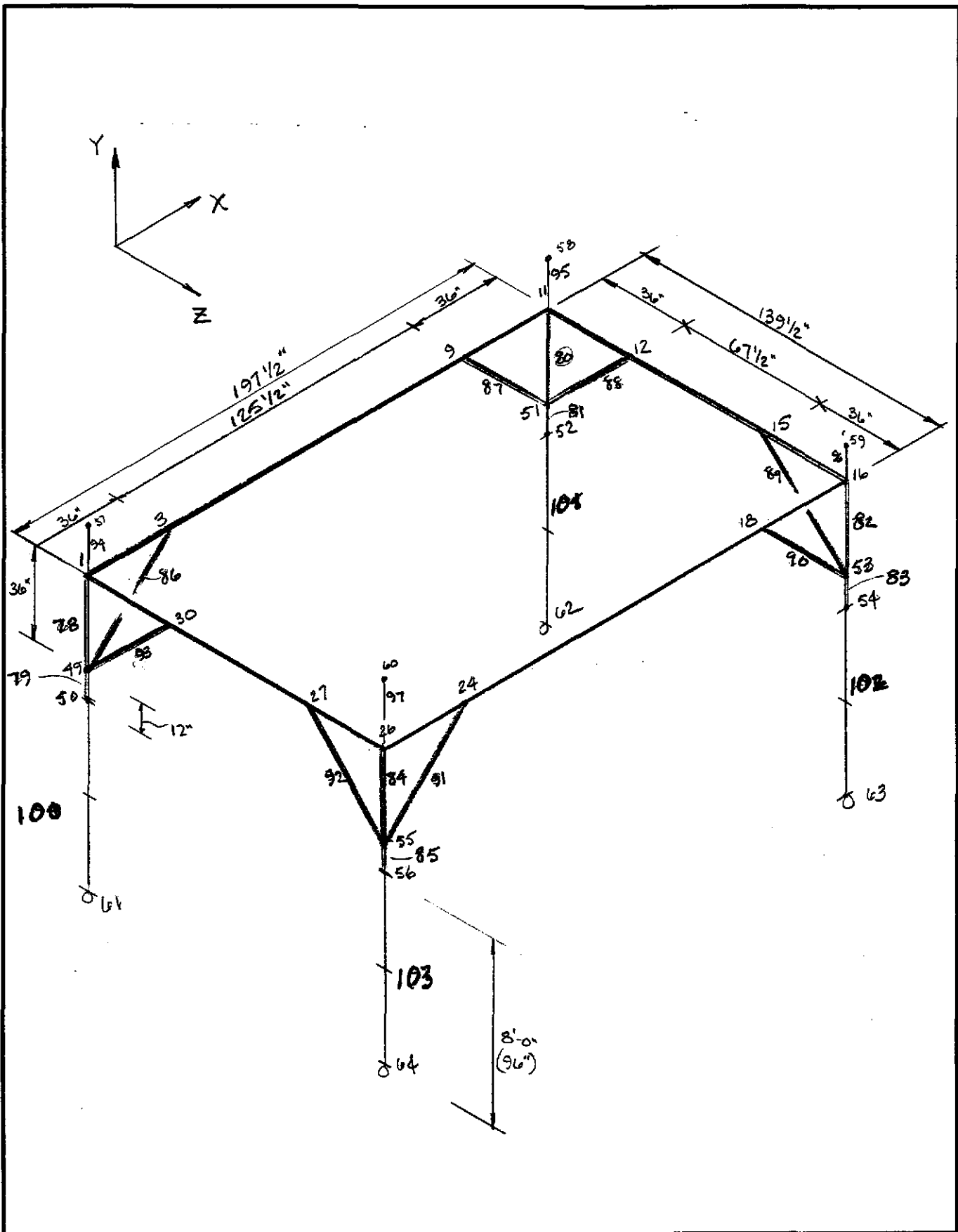
$$Z_B = 0.188 \text{ in}$$



22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



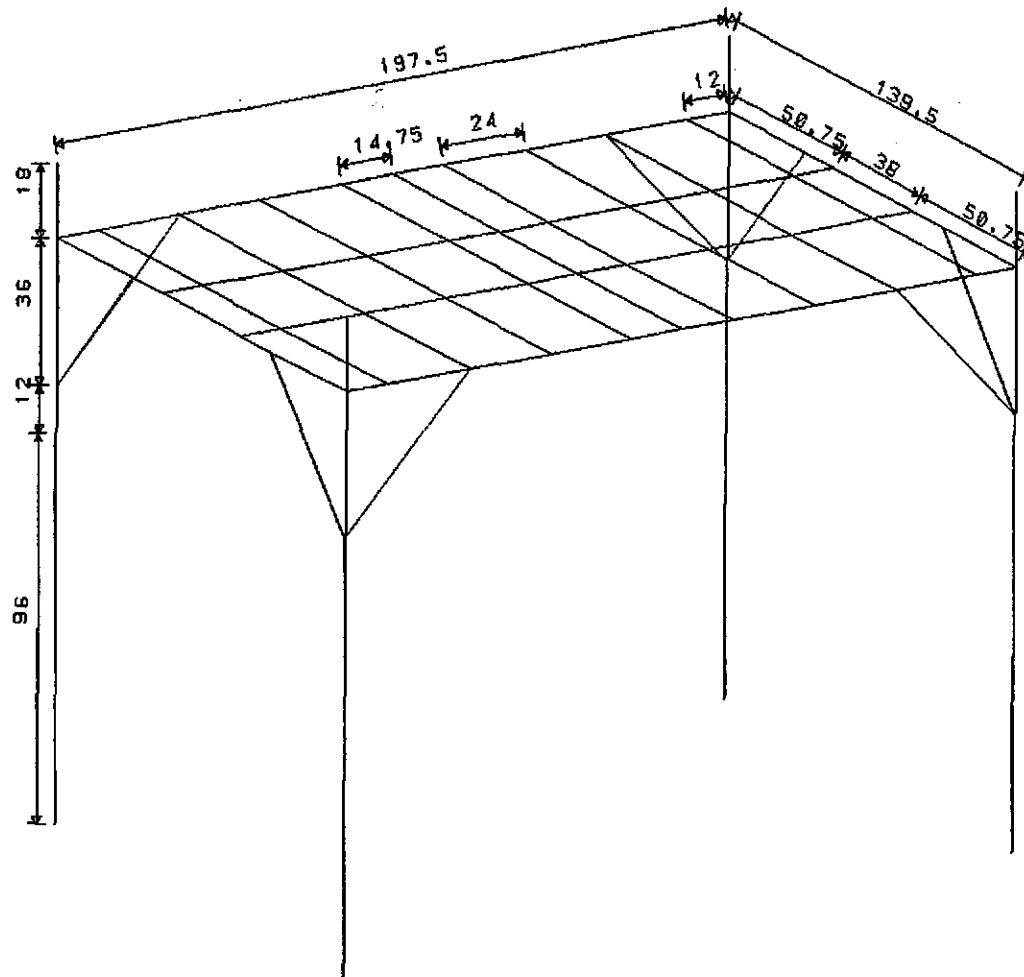




					PSI .A	Revision No. 0 Doc. No. V049-1-113 Page 6 of 72	PAGE	
							OF	
REV	BY	DATE	CHECKED	DATE				

STRUCTURE DATA

TYPE = SPACE  
 NJ = 64  
 NM = 101  
 NE = 0  
 NS = 4  
 NL = 1  
 XMAX= 197.5  
 YMAX= 162.0  
 ZMAX= 139.5



J=64, N=101

UNIT INC POU

USER ID:PROCESS SYSTEMS INTERNATIONAL IN  
 STAAD POST - PLOT (REV: 21.0 )  
 TITLE: HAM PORTABLE CLEANROOM

DATE: OCT 7, 1996

```

*****
*                               *
*          S T A A D - III      *
*          Revision 21.0        *
*          Proprietary Program of *
*          Research Engineers, Inc. *
*          Date=   OCT  4, 1996  *
*          Time=   15:53:41      *
*                               *
*          USER ID: PROCESS SYSTEMS INTERNATIONAL IN *
*****

```

1. STAAD SPACE HAM PORTABLE CLEANROOM
2. INPUT WIDTH 72
3. UNIT INCHES POUND
4. JOINT COORDINATES
5. 1 0. 0. 0.; 2 12. 0. 0.; 3 36. 0. 0.; 4 60. 0. 0.; 5 84. 0. 0.
6. 6 98.75 0. 0.; 7 113.5 0. 0.; 8 137.5 0. 0.; 9 161.5 0. 0.
7. 10 185.5 0. 0.; 11 197.5 0. 0.; 12 197.5 0. 36.; 13 197.5 0. 50.75
8. 14 197.5 0. 88.75; 15 197.5 0. 103.5; 16 197.5 0. 139.5
9. 17 185.5 0. 139.5; 18 161.5 0. 139.5; 19 137.5 0. 139.5
10. 20 113.5 0. 139.5; 21 98.75 0. 139.5; 22 84. 0. 139.5; 23 60. 0. 139.5
11. 24 36. 0. 139.5; 25 12. 0. 139.5; 26 0. 0. 139.5; 27 0. 0. 103.5
12. 28 0. 0. 88.75; 29 0. 0. 50.75; 30 0. 0. 36.; 31 12. 0. 50.75
13. 32 36. 0. 50.75; 33 60. 0. 50.75; 34 84. 0. 50.75; 35 98.75 0. 50.75
14. 36 113.5 0. 50.75; 37 137.5 0. 50.75; 38 161.5 0. 50.75
15. 39 185.5 0. 50.75; 40 12. 0. 88.75; 41 36. 0. 88.75; 42 60. 0. 88.75
16. 43 84. 0. 88.75; 44 98.75 0. 88.75; 45 113.5 0. 88.75; 46 137.5 0. 88.75
17. 47 161.5 0. 88.75; 48 185.5 0. 88.75; 49 0. -36. 0.; 50 0. -48. 0.
18. 51 197.5 -36. 0.; 52 197.5 -48. 0.; 53 197.5 -36. 139.5
19. 54 197.5 -48. 139.5; 55 0. -36. 139.5; 56 0. -48. 139.5; 57 0. 18. 0.
20. 58 197.5 18. 0.; 59 197.5 18. 139.5; 60 0. 18. 139.5; 61 0. -144. 0.
21. 62 197.5 -144. 0.; 63 197.5 -144. 139.5; 64 0. -144. 139.5
22. MEMBER INCIDENCES
23. 1 1 2; 2 2 3; 3 3 4; 4 4 5; 5 5 6; 6 6 7; 7 7 8; 8 8 9; 9 9 10; 10 10 11
24. 11 11 12; 12 12 13; 13 13 14; 14 14 15; 15 15 16; 16 16 17; 17 17 18
25. 18 18 19; 19 19 20; 20 20 21; 21 21 22; 22 22 23; 23 23 24; 24 24 25
26. 25 25 26; 26 26 27; 27 27 28; 28 28 29; 29 29 30; 30 30 1; 31 29 31
27. 32 31 32; 33 32 33; 34 33 34; 35 34 35; 36 35 36; 37 36 37; 38 37 38
28. 39 38 39; 40 39 13; 41 28 40; 42 40 41; 43 41 42; 44 42 43; 45 43 44
29. 46 44 45; 47 45 46; 48 46 47; 49 47 48; 50 48 14; 51 6 35; 52 35 44
30. 53 44 21; 54 2 31; 55 31 40; 56 40 25; 57 3 32; 58 32 41; 59 41 24
31. 60 4 33; 61 33 42; 62 42 23; 63 5 34; 64 34 43; 65 43 22; 66 7 36
32. 67 36 45; 68 45 20; 69 8 37; 70 37 46; 71 46 19; 72 9 38; 73 38 47
33. 74 47 18; 75 10 39; 76 39 48; 77 48 17; 78 1 49; 79 49 50; 80 11 51
34. 81 51 52; 82 16 53; 83 53 54; 84 26 55; 85 55 56; 86 3 49; 87 9 51
35. 88 12 51; 89 15 53; 90 18 53; 91 24 55; 92 27 55; 93 30 49; 94 1 57
36. 95 11 58; 96 16 59; 97 26 60; 100 50 61; 101 52 62; 102 54 63; 103 56 64
37. MEMBER PROPERTY AMER
38. 1 TO 30 TABLE ST TUB60303
39. 31 TO 53 TABLE ST TUB40203
40. 54 TO 77 PRI YD 1.75 ZD 1.5 YB 1.563 ZB 0.188
41. \*\*\* ALUMINUM TEES

42. 78 TO 85 94 TO 97 TABLE ST TUB35353  
 43. 86 TO 93 TABLE ST TUB20203  
 44. 100 TO 103 PRI AX 1.382 IY 1.914 IZ 1.914 YD 3. ZD 3.  
 45. \*\*\* ALUMINUM TUBE (3" X 3" X 1/8")  
 46. CONSTANTS  
 47. E STEEL MEMB 1 TO 53 78 TO 97  
 48. E ALUMINUM MEMB 54 TO 77 100 TO 103  
 49. POISSON STEEL MEMB 1 TO 53 78 TO 97  
 50. POISSON ALUMINUM MEMB 54 TO 77 100 TO 103  
 51. DENSITY STEEL MEMB 1 TO 53 78 TO 97  
 52. DENSITY ALUMINUM MEMB 54 TO 77 100 TO 103  
 53. BETA 180. MEMB 54 TO 77  
 54. SUPPORTS  
 55. 61 FIXED BUT FX MZ  
 56. 62 FIXED BUT FX FZ MX MZ  
 57. 63 FIXED BUT FX MZ  
 58. 64 FIXED BUT FX FZ  
 59. LOAD 1  
 60. SELFWEIGHT Y -1.  
 61. AREA LOAD  
 62. 1 TO 77 ALOAD -0.1  
 63. PERFORM ANALYSIS

P R O B L E M   S T A T I S T I C S

-----

NUMBER OF JOINTS/MEMBER+ELEMENTS/SUPPORTS = 64/ 101/ 4  
 ORIGINAL/FINAL BAND-WIDTH = 56/ 7  
 TOTAL PRIMARY LOAD CASES = 1, TOTAL DEGREES OF FREEDOM = 370  
 SIZE OF STIFFNESS MATRIX = 17760 DOUBLE PREC. WORDS  
 REQD/AVAIL. DISK SPACE = 12.24/ 943.7 MB, EXMEM = 14.83 MB

++ PROCESSING ELEMENT STIFFNESS MATRIX. 15:53:43  
 ++ PROCESSING GLOBAL STIFFNESS MATRIX. 15:53:43  
 ++ PROCESSING TRIANGULAR FACTORIZATION. 15:53:44

\*\*\*WARNING - IMPROPER LOAD WILL CAUSE INSTABILITY AT JOINT 63 \*  
 DIRECTION = FX PROBABLE CAUSE MODELING PROBLEM 0.622E-11  
 ++ CALCULATING JOINT DISPLACEMENTS. 15:53:44  
 ++ CALCULATING MEMBER FORCES. 15:53:44

64. PRINT MATERIAL PROPERTIES ALL

\* PROGRAM RECOVERED FROM INSTABILITY

## MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
1	29000000.0	11153846.0	0.28299999	0.00000000
2	29000000.0	11153846.0	0.28299999	0.00000000
3	29000000.0	11153846.0	0.28299999	0.00000000
4	29000000.0	11153846.0	0.28299999	0.00000000
5	29000000.0	11153846.0	0.28299999	0.00000000
6	29000000.0	11153846.0	0.28299999	0.00000000
7	29000000.0	11153846.0	0.28299999	0.00000000
8	29000000.0	11153846.0	0.28299999	0.00000000
9	29000000.0	11153846.0	0.28299999	0.00000000
10	29000000.0	11153846.0	0.28299999	0.00000000
11	29000000.0	11153846.0	0.28299999	0.00000000
12	29000000.0	11153846.0	0.28299999	0.00000000
13	29000000.0	11153846.0	0.28299999	0.00000000
14	29000000.0	11153846.0	0.28299999	0.00000000
15	29000000.0	11153846.0	0.28299999	0.00000000
16	29000000.0	11153846.0	0.28299999	0.00000000
17	29000000.0	11153846.0	0.28299999	0.00000000
18	29000000.0	11153846.0	0.28299999	0.00000000
19	29000000.0	11153846.0	0.28299999	0.00000000
20	29000000.0	11153846.0	0.28299999	0.00000000
21	29000000.0	11153846.0	0.28299999	0.00000000
22	29000000.0	11153846.0	0.28299999	0.00000000
23	29000000.0	11153846.0	0.28299999	0.00000000
24	29000000.0	11153846.0	0.28299999	0.00000000
25	29000000.0	11153846.0	0.28299999	0.00000000
26	29000000.0	11153846.0	0.28299999	0.00000000
27	29000000.0	11153846.0	0.28299999	0.00000000
28	29000000.0	11153846.0	0.28299999	0.00000000
29	29000000.0	11153846.0	0.28299999	0.00000000
30	29000000.0	11153846.0	0.28299999	0.00000000
31	29000000.0	11153846.0	0.28299999	0.00000000
32	29000000.0	11153846.0	0.28299999	0.00000000
33	29000000.0	11153846.0	0.28299999	0.00000000
34	29000000.0	11153846.0	0.28299999	0.00000000
35	29000000.0	11153846.0	0.28299999	0.00000000
36	29000000.0	11153846.0	0.28299999	0.00000000
37	29000000.0	11153846.0	0.28299999	0.00000000
38	29000000.0	11153846.0	0.28299999	0.00000000
39	29000000.0	11153846.0	0.28299999	0.00000000
40	29000000.0	11153846.0	0.28299999	0.00000000
41	29000000.0	11153846.0	0.28299999	0.00000000
42	29000000.0	11153846.0	0.28299999	0.00000000
43	29000000.0	11153846.0	0.28299999	0.00000000
44	29000000.0	11153846.0	0.28299999	0.00000000
45	29000000.0	11153846.0	0.28299999	0.00000000
46	29000000.0	11153846.0	0.28299999	0.00000000

## MATERIAL PROPERTIES.

-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
47	29000000.0	11153846.0	0.28299999	0.00000000
48	29000000.0	11153846.0	0.28299999	0.00000000
49	29000000.0	11153846.0	0.28299999	0.00000000
50	29000000.0	11153846.0	0.28299999	0.00000000
51	29000000.0	11153846.0	0.28299999	0.00000000
52	29000000.0	11153846.0	0.28299999	0.00000000
53	29000000.0	11153846.0	0.28299999	0.00000000
54	9999999.0	3999999.8	0.09548600	0.00000000
55	9999999.0	3999999.8	0.09548600	0.00000000
56	9999999.0	3999999.8	0.09548600	0.00000000
57	9999999.0	3999999.8	0.09548600	0.00000000
58	9999999.0	3999999.8	0.09548600	0.00000000
59	9999999.0	3999999.8	0.09548600	0.00000000
60	9999999.0	3999999.8	0.09548600	0.00000000
61	9999999.0	3999999.8	0.09548600	0.00000000
62	9999999.0	3999999.8	0.09548600	0.00000000
63	9999999.0	3999999.8	0.09548600	0.00000000
64	9999999.0	3999999.8	0.09548600	0.00000000
65	9999999.0	3999999.8	0.09548600	0.00000000
66	9999999.0	3999999.8	0.09548600	0.00000000
67	9999999.0	3999999.8	0.09548600	0.00000000
68	9999999.0	3999999.8	0.09548600	0.00000000
69	9999999.0	3999999.8	0.09548600	0.00000000
70	9999999.0	3999999.8	0.09548600	0.00000000
71	9999999.0	3999999.8	0.09548600	0.00000000
72	9999999.0	3999999.8	0.09548600	0.00000000
73	9999999.0	3999999.8	0.09548600	0.00000000
74	9999999.0	3999999.8	0.09548600	0.00000000
75	9999999.0	3999999.8	0.09548600	0.00000000
76	9999999.0	3999999.8	0.09548600	0.00000000
77	9999999.0	3999999.8	0.09548600	0.00000000
78	29000000.0	11153846.0	0.28299999	0.00000000
79	29000000.0	11153846.0	0.28299999	0.00000000
80	29000000.0	11153846.0	0.28299999	0.00000000
81	29000000.0	11153846.0	0.28299999	0.00000000
82	29000000.0	11153846.0	0.28299999	0.00000000
83	29000000.0	11153846.0	0.28299999	0.00000000
84	29000000.0	11153846.0	0.28299999	0.00000000
85	29000000.0	11153846.0	0.28299999	0.00000000
86	29000000.0	11153846.0	0.28299999	0.00000000
87	29000000.0	11153846.0	0.28299999	0.00000000
88	29000000.0	11153846.0	0.28299999	0.00000000
89	29000000.0	11153846.0	0.28299999	0.00000000
90	29000000.0	11153846.0	0.28299999	0.00000000
91	29000000.0	11153846.0	0.28299999	0.00000000
92	29000000.0	11153846.0	0.28299999	0.00000000

MATERIAL PROPERTIES:-----  
ALL UNITS ARE - POUN INCH

MEMBER	E	G	DEN	ALPHA
93	29000000.0	11153846.0	0.28299999	0.00000000
94	29000000.0	11153846.0	0.28299999	0.00000000
95	29000000.0	11153846.0	0.28299999	0.00000000
96	29000000.0	11153846.0	0.28299999	0.00000000
97	29000000.0	11153846.0	0.28299999	0.00000000
100	9999999.0	3999999.8	0.09548600	0.00000000
101	9999999.0	3999999.8	0.09548600	0.00000000
102	9999999.0	3999999.8	0.09548600	0.00000000
103	9999999.0	3999999.8	0.09548600	0.00000000

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

65. PRINT MEMBER INFORMATION ALL

MEMBER INFORMATION  
-----

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
1	1	2	12.000	0.00	
2	2	3	24.000	0.00	
3	3	4	24.000	0.00	
4	4	5	24.000	0.00	
5	5	6	14.750	0.00	
6	6	7	14.750	0.00	
7	7	8	24.000	0.00	
8	8	9	24.000	0.00	
9	9	10	24.000	0.00	
10	10	11	12.000	0.00	
11	11	12	36.000	0.00	
12	12	13	14.750	0.00	
13	13	14	38.000	0.00	
14	14	15	14.750	0.00	
15	15	16	36.000	0.00	
16	16	17	12.000	0.00	
17	17	18	24.000	0.00	
18	18	19	24.000	0.00	
19	19	20	24.000	0.00	
20	20	21	14.750	0.00	
21	21	22	14.750	0.00	
22	22	23	24.000	0.00	
23	23	24	24.000	0.00	
24	24	25	24.000	0.00	
25	25	26	12.000	0.00	
26	26	27	36.000	0.00	
27	27	28	14.750	0.00	
28	28	29	38.000	0.00	
29	29	30	14.750	0.00	
30	30	1	36.000	0.00	
31	29	31	12.000	0.00	
32	31	32	24.000	0.00	
33	32	33	24.000	0.00	
34	33	34	24.000	0.00	
35	34	35	14.750	0.00	
36	35	36	14.750	0.00	
37	36	37	24.000	0.00	
38	37	38	24.000	0.00	
39	38	39	24.000	0.00	
40	39	13	12.000	0.00	
41	28	40	12.000	0.00	
42	40	41	24.000	0.00	
43	41	42	24.000	0.00	
44	42	43	24.000	0.00	
45	43	44	14.750	0.00	
46	44	45	14.750	0.00	



## MEMBER INFORMATION

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
47	45	46	24.000	0.00	
48	46	47	24.000	0.00	
49	47	48	24.000	0.00	
50	48	14	12.000	0.00	
51	6	35	50.750	0.00	
52	35	44	38.000	0.00	
53	44	21	50.750	0.00	
54	2	31	50.750	180.00	
55	31	40	38.000	180.00	
56	40	25	50.750	180.00	
57	3	32	50.750	180.00	
58	32	41	38.000	180.00	
59	41	24	50.750	180.00	
60	4	33	50.750	180.00	
61	33	42	38.000	180.00	
62	42	23	50.750	180.00	
63	5	34	50.750	180.00	
64	34	43	38.000	180.00	
65	43	22	50.750	180.00	
66	7	36	50.750	180.00	
67	36	45	38.000	180.00	
68	45	20	50.750	180.00	
69	8	37	50.750	180.00	
70	37	46	38.000	180.00	
71	46	19	50.750	180.00	
72	9	38	50.750	180.00	
73	38	47	38.000	180.00	
74	47	18	50.750	180.00	
75	10	39	50.750	180.00	
76	39	48	38.000	180.00	
77	48	17	50.750	180.00	
78	1	49	36.000	0.00	
79	49	50	12.000	0.00	
80	11	51	36.000	0.00	
81	51	52	12.000	0.00	
82	16	53	36.000	0.00	
83	53	54	12.000	0.00	
84	26	55	36.000	0.00	
85	55	56	12.000	0.00	
86	3	49	50.912	0.00	
87	9	51	50.912	0.00	
88	12	51	50.912	0.00	
89	15	53	50.912	0.00	
90	18	53	50.912	0.00	
91	24	55	50.912	0.00	
92	27	55	50.912	0.00	

MEMBER INFORMATION  
-----

MEMBER	START JOINT	END JOINT	LENGTH (INCH)	BETA (DEG)	RELEASES
93	30	49	50.912	0.00	
94	1	57	18.000	0.00	
95	11	58	18.000	0.00	
96	16	59	18.000	0.00	
97	26	60	18.000	0.00	
100	50	61	96.000	0.00	
101	52	62	96.000	0.00	
102	54	63	96.000	0.00	
103	56	64	96.000	0.00	

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

66. PRINT JOINT COORDINATES ALL

## JOINT COORDINATES

-----  
COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
1	0.000	0.000	0.000
2	12.000	0.000	0.000
3	36.000	0.000	0.000
4	60.000	0.000	0.000
5	84.000	0.000	0.000
6	98.750	0.000	0.000
7	113.500	0.000	0.000
8	137.500	0.000	0.000
9	161.500	0.000	0.000
10	185.500	0.000	0.000
11	197.500	0.000	0.000
12	197.500	0.000	36.000
13	197.500	0.000	50.750
14	197.500	0.000	88.750
15	197.500	0.000	103.500
16	197.500	0.000	139.500
17	185.500	0.000	139.500
18	161.500	0.000	139.500
19	137.500	0.000	139.500
20	113.500	0.000	139.500
21	98.750	0.000	139.500
22	84.000	0.000	139.500
23	60.000	0.000	139.500
24	36.000	0.000	139.500
25	12.000	0.000	139.500
26	0.000	0.000	139.500
27	0.000	0.000	103.500
28	0.000	0.000	88.750
29	0.000	0.000	50.750
30	0.000	0.000	36.000
31	12.000	0.000	50.750
32	36.000	0.000	50.750
33	60.000	0.000	50.750
34	84.000	0.000	50.750
35	98.750	0.000	50.750
36	113.500	0.000	50.750
37	137.500	0.000	50.750
38	161.500	0.000	50.750
39	185.500	0.000	50.750
40	12.000	0.000	88.750
41	36.000	0.000	88.750
42	60.000	0.000	88.750
43	84.000	0.000	88.750
44	98.750	0.000	88.750
45	113.500	0.000	88.750
46	137.500	0.000	88.750
47	161.500	0.000	88.750

JOINT COORDINATES

-----  
 COORDINATES ARE INCH UNIT

JOINT	X	Y	Z
48	185.500	0.000	88.750
49	0.000	-36.000	0.000
50	0.000	-48.000	0.000
51	197.500	-36.000	0.000
52	197.500	-48.000	0.000
53	197.500	-36.000	139.500
54	197.500	-48.000	139.500
55	0.000	-36.000	139.500
56	0.000	-48.000	139.500
57	0.000	18.000	0.000
58	197.500	18.000	0.000
59	197.500	18.000	139.500
60	0.000	18.000	139.500
61	0.000	-144.000	0.000
62	197.500	-144.000	0.000
63	197.500	-144.000	139.500
64	0.000	-144.000	139.500

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

67. PRINT SUPPORT INFORMATION ALL

SUPPORT INFORMATION (1=FIXED, 0=RELEASED)

-----  
 UNITS FOR SPRING CONSTANTS ARE POUN INCH DEGREES

JOINT	FORCE-X/ KFX	FORCE-Y/ KFY	FORCE-Z/ KFZ	MOM-X/ KMX	MOM-Y/ KMY	MOM-Z/ KMZ
61	0	1	1	1	1	0
62	0.0	0.0	0.0	0.0	0.0	0.0
63	0	1	1	1	1	0
64	0	1	0	1	1	1
	0.0	0.0	0.0	0.0	0.0	0.0

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

68. PRINT ANALYSIS RESULTS

## JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
1	1	-0.91001	-0.00785	0.16347	0.00254	0.00162	-0.00505
2	1	-0.91002	-0.06838	0.14397	0.00276	0.00163	-0.00496
3	1	-0.91005	-0.18074	0.10441	0.00313	0.00168	-0.00425
4	1	-0.91005	-0.26800	0.06411	0.00352	0.00168	-0.00292
5	1	-0.91005	-0.31834	0.02388	0.00381	0.00167	-0.00120
6	1	-0.91005	-0.32740	-0.00074	0.00393	0.00167	0.00000
7	1	-0.91004	-0.31835	-0.02537	0.00382	0.00167	0.00120
8	1	-0.91004	-0.26802	-0.06564	0.00355	0.00168	0.00292
9	1	-0.91004	-0.18073	-0.10563	0.00317	0.00165	0.00425
10	1	-0.91007	-0.06830	-0.14533	0.00280	0.00164	0.00496
11	1	-0.91008	-0.00773	-0.16492	0.00257	0.00161	0.00505
12	1	-0.85187	-0.09178	-0.16496	0.00181	0.00165	0.00565
13	1	-0.82748	-0.11346	-0.16496	0.00107	0.00165	0.00599
14	1	-0.76520	-0.11301	-0.16495	-0.00109	0.00163	0.00598
15	1	-0.74135	-0.09120	-0.16495	-0.00181	0.00161	0.00565
16	1	-0.68262	-0.00784	-0.16497	-0.00256	0.00162	0.00501
17	1	-0.68261	-0.06793	-0.14546	-0.00278	0.00163	0.00492
18	1	-0.68258	-0.17940	-0.10589	-0.00315	0.00168	0.00421
19	1	-0.68258	-0.26584	-0.06559	-0.00355	0.00168	0.00289
20	1	-0.68258	-0.31553	-0.02535	-0.00384	0.00167	0.00118
21	1	-0.68258	-0.32432	-0.00073	-0.00396	0.00167	-0.00001
22	1	-0.68258	-0.31515	0.02390	-0.00384	0.00167	-0.00120
23	1	-0.68258	-0.26500	0.06417	-0.00356	0.00168	-0.00290
24	1	-0.68259	-0.17852	0.10414	-0.00317	0.00165	-0.00420
25	1	-0.68257	-0.06757	0.14383	-0.00278	0.00164	-0.00490
26	1	-0.68256	-0.00777	0.16342	-0.00255	0.00161	-0.00500
27	1	-0.74079	-0.09105	0.16346	-0.00179	0.00166	-0.00562
28	1	-0.76518	-0.11259	0.16346	-0.00106	0.00165	-0.00597
29	1	-0.82746	-0.11226	0.16345	0.00108	0.00163	-0.00600
30	1	-0.85131	-0.09063	0.16345	0.00179	0.00161	-0.00567
31	1	-0.82746	-0.18551	0.14388	0.00108	0.00164	-0.00610
32	1	-0.82746	-0.32463	0.10430	0.00116	0.00166	-0.00525
33	1	-0.82746	-0.43055	0.06413	0.00131	0.00168	-0.00345
34	1	-0.82746	-0.48743	0.02385	0.00154	0.00167	-0.00128
35	1	-0.82747	-0.49665	-0.00074	0.00171	0.00165	-0.00001
36	1	-0.82747	-0.48763	-0.02533	0.00153	0.00168	0.00127
37	1	-0.82747	-0.43107	-0.06562	0.00131	0.00168	0.00343
38	1	-0.82747	-0.32545	-0.10571	0.00115	0.00166	0.00524
39	1	-0.82748	-0.18659	-0.14531	0.00107	0.00164	0.00609
40	1	-0.76518	-0.18557	0.14382	-0.00107	0.00164	-0.00608
41	1	-0.76519	-0.32424	0.10423	-0.00117	0.00166	-0.00524
42	1	-0.76519	-0.42984	0.06414	-0.00134	0.00168	-0.00344
43	1	-0.76519	-0.48654	0.02386	-0.00158	0.00168	-0.00128
44	1	-0.76519	-0.49573	-0.00074	-0.00176	0.00165	-0.00001
45	1	-0.76520	-0.48672	-0.02532	-0.00158	0.00167	0.00126
46	1	-0.76520	-0.43027	-0.06561	-0.00135	0.00168	0.00343
47	1	-0.76520	-0.32480	-0.10578	-0.00118	0.00166	0.00524
48	1	-0.76520	-0.18609	-0.14538	-0.00109	0.00164	0.00609

JOINT DISPLACEMENT (INCH RADIANS)      STRUCTURE TYPE = SPACE  
 -----

JOINT	LOAD	X-TRANS	Y-TRANS	Z-TRANS	X-ROTAN	Y-ROTAN	Z-ROTAN
49	1	-1.08372	-0.00730	0.08003	0.00217	0.00147	-0.00476
50	1	-1.14087	-0.00712	0.05463	0.00207	0.00138	-0.00476
51	1	-0.73623	-0.00717	-0.24979	0.00230	0.00148	0.00475
52	1	-0.67919	-0.00699	-0.27735	0.00230	0.00139	0.00475
53	1	-0.51023	-0.00729	-0.08095	-0.00218	0.00147	0.00472
54	1	-0.45354	-0.00711	-0.05536	-0.00208	0.00138	0.00472
55	1	-0.85403	-0.00722	0.24747	-0.00224	0.00147	-0.00463
56	1	-0.90902	-0.00705	0.27414	-0.00220	0.00139	-0.00454
57	1	-0.81910	-0.00785	0.20918	0.00254	0.00162	-0.00505
58	1	-1.00105	-0.00773	-0.11860	0.00257	0.00161	0.00505
59	1	-0.77288	-0.00784	-0.21099	-0.00256	0.00162	0.00501
60	1	-0.59265	-0.00777	0.11745	-0.00255	0.00161	-0.00500
61	1	-1.59801	0.00000	0.00000	0.00000	0.00000	-0.00476
62	1	-0.22285	0.00000	-0.49783	0.00230	0.00000	0.00475
63	1	0.00000	0.00000	0.00000	0.00000	0.00000	0.00472
64	1	-1.12686	0.00000	0.37980	0.00000	0.00000	0.00000

SUPPORT REACTIONS -UNIT POUN INCH      STRUCTURE TYPE = SPACE  
-----

JOINT	LOAD	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM Z
61	1	0.00	1031.83	11.55	141.92	-568.89	0.00
62	1	0.00	1013.21	0.00	0.00	-572.50	0.00
63	1	0.00	1030.42	-11.55	-138.88	-568.63	0.00
64	1	0.00	1020.96	0.00	438.87	-571.42	904.84



MEMBER END FORCES -- STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
1	1	1	102.52	560.28	-3.74	-2444.31	-79.31	272.76
		2	-102.52	-549.61	3.74	2444.31	124.16	6386.57
2	1	2	102.21	499.50	-13.70	-2024.74	-124.48	-6387.16
		3	-102.21	-478.17	13.70	2024.74	453.24	18119.21
3	1	3	-3.48	336.83	-0.01	-2197.78	8.72	-19014.54
		4	3.48	-315.50	0.01	2197.78	-8.58	26842.41
4	1	4	-3.23	247.02	2.56	-1587.92	5.36	-26842.72
		5	3.23	-225.69	-2.56	1587.92	-66.84	32515.27
5	1	5	-3.15	169.88	-0.48	-1104.75	63.95	-32515.54
		6	3.15	-156.78	0.48	1104.75	-56.86	34924.72
6	1	6	-9.05	-156.29	0.90	1014.99	-89.82	-34929.59
		7	9.05	169.40	-0.90	-1014.99	76.56	32527.97
7	1	7	-9.01	-225.19	5.92	1497.59	-79.54	-32527.80
		8	9.01	246.52	-5.92	-1497.59	-62.47	26867.36
8	1	8	-8.80	-314.96	8.66	2105.97	59.35	-26867.34
		9	8.80	336.29	-8.66	-2105.97	-267.27	19052.19
9	1	9	99.05	-478.77	18.06	2059.69	-193.80	-18145.39
		10	-99.05	500.09	-18.06	-2059.69	-239.75	6399.06
10	1	10	97.55	-550.28	19.82	2479.28	238.76	-6398.76
		11	-97.55	560.95	-19.82	-2479.28	-476.60	-268.63
11	1	11	102.29	504.33	-18.95	-2209.24	178.92	-37.57
		12	-102.29	-450.74	18.95	2209.24	503.27	17228.99
12	1	12	0.62	379.49	9.05	-2998.41	2.33	-18078.96
		13	-0.62	-357.53	-9.05	2998.41	-135.86	23514.55
13	1	13	-10.68	18.18	2.34	13.47	37.00	-23524.60
		14	10.68	38.39	-2.34	-13.47	-125.86	23140.61
14	1	14	-10.92	-377.44	-2.94	3010.89	162.53	-23116.13
		15	10.92	399.40	2.94	-3010.89	-119.21	17386.94
15	1	15	43.47	-418.63	17.06	2335.76	-351.06	-16495.53
		16	-43.47	472.23	-17.06	-2335.76	-263.06	460.05

## MEMBER END FORCES    STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
16	1	16	103.37	557.67	-3.98	-2460.62	-75.32	223.87
		17	-103.37	-547.01	3.98	2460.62	123.08	6404.18
17	1	17	103.05	496.86	-13.83	-2040.56	-123.36	-6404.81
		18	-103.05	-475.53	13.83	2040.56	455.22	18073.40
18	1	18	-2.91	333.55	-0.02	-2217.74	10.23	-18968.12
		19	2.91	-312.22	0.02	2217.74	-9.83	26717.31
19	1	19	-2.92	243.70	2.53	-1606.22	6.63	-26717.39
		20	2.92	-222.37	-2.53	1606.22	-67.32	32310.16
20	1	20	-4.20	166.57	-0.54	-1121.46	64.47	-32309.82
		21	4.20	-153.46	0.54	1121.46	-56.54	34670.12
21	1	21	-8.26	-161.42	0.84	1079.86	-87.71	-34675.22
		22	8.26	174.53	-0.84	-1079.86	75.26	32197.91
22	1	22	-8.94	-230.38	5.89	1564.91	-78.21	-32197.92
		23	8.94	251.70	-5.89	-1564.91	-63.04	26413.06
23	1	23	-8.72	-320.27	8.65	2176.85	59.99	-26413.26
		24	8.72	341.60	-8.65	-2176.85	-267.68	18470.63
24	1	24	69.04	-450.78	17.78	2123.20	-190.78	-17537.01
		25	-69.04	472.10	-17.78	-2123.20	-235.91	6462.45
25	1	25	68.65	-522.30	19.76	2543.24	235.03	-6461.73
		26	-68.65	532.96	-19.76	-2543.24	-472.15	130.20
26	1	26	88.35	490.70	-18.37	-2318.73	168.25	-236.10
		27	-88.35	-437.11	18.37	2318.73	493.22	16936.65
27	1	27	1.31	381.85	8.94	-3127.83	5.28	-17799.41
		28	-1.31	-359.90	-8.94	3127.83	-137.06	23269.86
28	1	28	-10.57	20.48	2.44	-82.77	35.54	-23307.66
		29	10.57	36.08	-2.44	82.77	-128.19	23011.23
29	1	29	-10.65	-375.64	-2.93	2940.96	163.12	-23006.02
		30	10.65	397.59	2.93	-2940.96	-119.79	17303.43
30	1	30	42.98	-416.58	16.60	2279.34	-341.36	-16416.41
		1	-42.98	470.17	-16.60	-2279.34	-256.39	455.05
31	1	29	5.88	339.58	-0.22	-5.15	-35.04	3023.79
		31	-5.88	-332.72	0.22	5.15	37.69	1009.93

## MEMBER END FORCES -- STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
32	1	31	5.54	253.47	-0.23	-141.94	-38.02	-1009.34
		32	-5.54	-239.75	0.23	141.94	43.51	6928.03
33	1	32	5.72	136.34	1.91	-273.65	-48.06	-6927.47
		33	-5.72	-122.62	-1.91	273.65	2.14	10035.15
34	1	33	5.22	19.95	1.29	-393.74	-8.67	-10034.78
		34	-5.22	-6.23	-1.29	393.74	-22.22	10348.90
35	1	34	5.11	-76.95	5.60	-513.52	16.28	-10349.03
		35	-5.11	85.39	-5.60	513.52	-98.81	9151.67
36	1	35	7.09	85.57	5.67	515.17	-101.81	-9147.10
		36	-7.09	-77.14	-5.67	-515.17	18.22	10347.23
37	1	36	6.66	-6.03	1.82	395.75	-24.30	-10347.33
		37	-6.66	19.75	-1.82	-395.75	-19.38	10037.97
38	1	37	6.64	-122.46	0.99	276.37	12.99	-10038.14
		38	-6.64	136.18	-0.99	-276.37	-36.72	6934.47
39	1	38	6.74	-239.65	0.27	145.34	32.91	-6934.87
		39	-6.74	253.37	-0.27	-145.34	-39.46	1018.75
40	1	39	7.33	-332.49	-11.45	10.01	38.75	-1019.21
		13	-7.33	339.35	11.45	-10.01	98.68	-3011.76
41	1	28	6.20	339.42	-11.69	37.73	101.42	3045.02
		40	-6.20	-332.56	11.69	-37.73	38.78	986.78
42	1	40	6.60	253.38	0.26	172.32	-39.39	-986.26
		41	-6.60	-239.66	-0.26	-172.32	33.24	6902.70
43	1	41	6.26	136.23	0.99	299.75	-36.96	-6902.09
		42	-6.26	-122.51	-0.99	-299.75	13.26	10007.03
44	1	42	6.73	19.80	1.82	414.89	-19.57	-10006.65
		43	-6.73	-6.08	-1.82	-414.89	-24.08	10317.29
45	1	43	6.33	-77.09	5.59	531.72	18.06	-10317.12
		44	-6.33	85.52	-5.59	-531.72	-100.55	9117.79
46	1	44	4.95	85.98	5.52	-525.47	-98.06	-9123.12
		45	-4.95	-77.54	-5.52	525.47	16.58	10329.13
47	1	45	5.27	-5.63	1.29	-407.52	-22.50	-10329.25
		46	-5.27	19.35	-1.29	407.52	-8.36	10029.40

MEMBER END FORCES STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
48	1	46	5.41	-122.07	1.92	-289.99	1.84	-10029.66
		47	-5.41	135.79	-1.92	289.99	-47.85	6935.35
49	1	47	5.42	-239.23	-0.21	-160.37	43.29	-6935.86
		48	-5.42	252.95	0.21	160.37	-38.13	1029.60
50	1	48	5.63	-332.20	-0.09	-24.39	37.75	-1030.13
		14	-5.63	339.06	0.09	24.39	-36.72	-2997.38
51	1	6	-1.38	313.13	-5.38	4.91	146.68	2119.76
		35	1.38	-209.27	5.38	-4.91	126.21	11136.15
52	1	35	-1.45	38.30	-3.92	0.10	74.40	-10107.46
		44	1.45	39.47	3.92	-0.10	74.72	10085.21
53	1	44	-1.38	-211.00	-5.28	5.42	123.90	-11142.45
		21	1.38	314.87	5.28	-5.42	144.26	-2201.33
54	1	2	9.96	-50.14	0.02	0.57	-0.34	-419.57
		31	-9.96	-43.99	-0.02	-0.57	-0.48	263.51
55	1	31	9.98	-35.24	-0.01	-0.01	0.15	-126.71
		40	-9.98	-35.24	0.01	0.01	0.12	126.68
56	1	40	-1.96	-43.94	0.03	-0.59	-0.73	-261.27
		25	1.96	-50.20	-0.03	0.59	-0.86	420.04
57	1	3	12.44	-67.77	0.11	0.50	-2.95	-599.68
		32	-12.44	-56.82	-0.11	-0.50	-2.59	321.75
58	1	32	10.30	-46.60	0.10	-0.01	-1.96	-190.05
		41	-10.30	-46.69	-0.10	0.01	-1.90	191.77
59	1	41	9.56	-56.75	0.07	-0.51	-1.81	-319.19
		24	-9.56	-67.83	-0.07	0.51	-1.53	600.43
60	1	4	-2.56	-68.49	0.13	0.26	-3.22	-609.86
		33	2.56	-56.09	-0.13	-0.26	-3.23	295.28
61	1	33	-1.94	-46.58	0.17	-0.01	-3.30	-175.19
		42	1.94	-46.70	-0.17	0.01	-3.25	177.49
62	1	42	-2.77	-56.00	0.12	-0.27	-3.07	-292.63
		23	2.77	-68.58	-0.12	0.27	-3.05	611.95
63	1	5	3.04	-55.76	0.11	0.04	-2.88	-483.17
		34	-3.04	-45.35	-0.11	-0.04	-2.93	219.12

## MEMBER END FORCES -- STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
64	1	34	-1.27	-37.81	0.16	0.00	-3.02	-99.34
		43	1.27	-37.90	-0.16	0.00	-3.05	100.94
65	1	43	-5.04	-45.29	0.12	-0.04	-2.97	-217.77
		22	5.04	-55.82	-0.12	0.04	-2.96	485.05
66	1	7	-5.02	-55.75	0.12	-0.03	-3.00	-482.58
		36	5.02	-45.36	-0.12	0.03	-3.02	219.00
67	1	36	-1.17	-37.83	0.16	0.00	-3.05	-99.57
		45	1.17	-37.88	-0.16	0.00	-3.03	100.56
68	1	45	3.06	-45.31	0.11	0.04	-2.89	-218.52
		20	-3.06	-55.80	-0.11	-0.04	-2.84	484.75
69	1	8	-2.74	-68.47	0.12	-0.26	-3.11	-608.39
		37	2.74	-56.11	-0.12	0.26	-3.13	294.87
70	1	37	-1.91	-46.61	0.17	0.00	-3.27	-175.50
		46	1.91	-46.68	-0.17	0.00	-3.32	176.77
71	1	46	-2.55	-56.04	0.13	0.27	-3.21	-294.30
		19	2.55	-68.54	-0.13	-0.27	-3.20	611.52
72	1	9	9.67	-67.74	0.07	-0.49	-1.60	-597.39
		38	-9.67	-56.84	-0.07	0.49	-1.88	320.94
73	1	38	10.38	-46.61	0.10	0.00	-1.93	-189.91
		47	-10.38	-46.67	-0.10	0.00	-1.99	191.13
74	1	47	12.52	-56.77	0.11	0.51	-2.57	-320.75
		18	-12.52	-67.81	-0.11	-0.51	-2.94	600.98
75	1	10	-1.74	-50.20	0.03	-0.56	-0.92	-419.58
		39	1.74	-43.94	-0.03	0.56	-0.79	260.69
76	1	39	9.99	-35.20	-0.01	0.00	0.08	-125.36
		48	-9.99	-35.28	0.01	0.00	0.11	126.82
77	1	48	9.86	-43.97	0.02	0.58	-0.47	-262.80
		17	-9.86	-50.17	-0.02	-0.58	-0.32	420.07
78	1	1	1042.63	-86.30	-39.23	-335.66	1989.25	-2552.52
		49	-1066.98	86.30	39.23	335.66	-576.81	-554.24
79	1	49	1011.06	-0.05	-11.55	-568.89	1105.66	-0.58
		50	-1019.18	0.05	11.55	568.89	-967.09	-0.57

## MEMBER END FORCES -- STRUCTURE TYPE = SPACE

ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
80	1	11	1077.46	79.88	-82.50	-297.62	2441.70	2477.90
		51	-1101.81	-79.88	82.50	297.62	528.34	397.85
81	1	51	992.40	-0.01	0.00	-572.50	-0.01	-0.10
		52	-1000.51	0.01	0.00	572.50	-0.02	-0.01
82	1	16	1042.09	86.44	39.50	-338.48	-2000.56	2559.78
		53	-1066.44	-86.44	-39.50	338.48	578.40	552.04
83	1	53	1009.63	-0.05	11.55	-568.63	-1108.71	-0.30
		54	-1017.74	0.05	-11.55	568.63	970.07	-0.36
84	1	26	1035.85	-50.45	68.44	-303.85	-2307.26	-2188.68
		55	-1060.20	50.45	-68.44	303.85	-156.74	372.46
85	1	55	1000.19	0.03	-0.01	-571.42	-438.80	-904.38
		56	-1008.30	-0.03	0.01	571.42	438.91	904.94
86	1	3	-126.90	-22.82	26.14	-217.66	-875.14	-894.81
		49	113.97	35.76	-26.14	217.66	-455.52	-596.36
87	1	9	-129.08	-23.44	-19.07	130.27	780.03	-906.36
		51	116.14	36.38	19.07	-130.27	190.88	-616.26
88	1	12	-122.20	-21.44	27.99	-200.51	-915.54	-849.95
		51	109.26	34.38	-27.99	200.51	-509.38	-571.19
89	1	15	-51.98	-24.79	-19.99	144.75	810.04	-891.37
		53	39.04	37.73	19.99	-144.75	207.80	-700.00
90	1	18	-127.75	-22.81	26.33	-219.02	-881.46	-894.11
		53	114.81	35.75	-26.33	219.02	-459.00	-596.63
91	1	24	-84.18	-25.71	-18.69	139.38	785.63	-933.01
		55	71.24	38.65	18.69	-139.38	166.07	-705.54
92	1	27	-100.68	-22.54	27.28	-219.49	-924.75	-862.68
		55	87.74	35.48	-27.28	219.49	-464.36	-614.47
93	1	30	-51.48	-24.64	-19.55	141.82	793.83	-886.98
		49	38.55	37.58	19.55	-141.82	201.50	-697.04
94	1	1	12.19	0.04	0.00	0.01	-0.02	0.43
		57	-0.01	-0.04	0.00	-0.01	0.01	0.45
95	1	11	12.17	-0.02	0.00	-0.01	0.02	-0.17
		58	0.00	0.02	0.00	0.01	0.03	-0.17

MEMBER END FORCES -- STRUCTURE TYPE = SPACE

-----  
ALL UNITS ARE -- POUN INCH

MEMBER	LOAD	JT	AXIAL	SHEAR-Y	SHEAR-Z	TORSION	MOM-Y	MOM-Z
96	1	16	12.18	0.01	0.00	0.00	-0.02	0.09
		59	0.00	-0.01	0.00	0.00	-0.01	0.10
97	1	26	12.18	0.00	0.00	-0.01	0.00	0.13
		60	-0.01	0.00	0.00	0.01	0.00	0.14
100	1	50	1019.17	0.00	-11.55	-568.89	967.05	0.00
		61	-1031.83	0.00	11.55	568.89	141.92	0.00
101	1	52	1000.55	0.00	0.00	-572.50	0.00	0.00
		62	-1013.21	0.00	0.00	572.50	0.00	0.00
102	1	54	1017.75	0.00	11.55	-568.63	-970.09	0.03
		63	-1030.42	0.00	-11.55	568.63	-138.88	0.00
103	1	56	1008.30	0.00	0.00	-571.42	-438.87	-904.85
		64	-1020.96	0.00	0.00	571.42	438.87	904.84

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

69. PRINT MEMBER STRESSES ALL

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
1	1	.0	32.6 C	24.8	57.2	114.7	249.0	5.0
		1.00	32.6 C	38.8	1339.8	1411.3	244.3	5.0
2	1	.0	32.6 C	38.9	1340.0	1411.4	222.0	18.3
		1.00	32.6 C	141.6	3801.2	3975.4	212.5	18.3
3	1	.0	1.1 T	2.7	3989.1	3992.9	149.7	0.0
		1.00	1.1 T	2.7	5631.3	5635.1	140.2	0.0
4	1	.0	1.0 T	1.7	5631.3	5634.0	109.8	3.4
		1.00	1.0 T	20.9	6821.4	6843.3	100.3	3.4
5	1	.0	1.0 T	20.0	6821.4	6842.4	75.5	0.6
		1.00	1.0 T	17.8	7326.9	7345.6	69.7	0.6
6	1	.0	2.9 T	28.1	7327.9	7358.8	69.5	1.2
		1.00	2.9 T	23.9	6824.1	6850.9	75.3	1.2
7	1	.0	2.9 T	24.9	6824.0	6851.7	100.1	7.9
		1.00	2.9 T	19.5	5636.5	5658.9	109.6	7.9
8	1	.0	2.8 T	18.5	5636.5	5657.9	140.0	11.6
		1.00	2.8 T	83.5	3997.0	4083.3	149.5	11.6
9	1	.0	31.5 C	60.6	3806.7	3898.8	212.8	24.1
		1.00	31.5 C	74.9	1342.5	1448.9	222.3	24.1
10	1	.0	31.1 C	74.6	1342.4	1448.1	244.6	26.4
		1.00	31.1 C	148.9	56.4	236.4	249.3	26.4
11	1	.0	32.6 C	55.9	7.9	96.4	224.1	25.3
		1.00	32.6 C	157.3	3614.5	3804.3	200.3	25.3
12	1	.0	0.2 C	0.7	3792.8	3793.7	168.7	12.1
		1.00	0.2 C	42.5	4933.1	4975.8	158.9	12.1
13	1	.0	3.4 T	11.6	4935.2	4950.2	8.1	3.1
		1.00	3.4 T	39.3	4854.7	4897.4	17.1	3.1
14	1	.0	3.5 T	50.8	4849.5	4903.8	167.8	3.9
		1.00	3.5 T	37.3	3647.6	3688.3	177.5	3.9
15	1	.0	13.8 C	109.7	3460.6	3584.1	186.1	22.7
		1.00	13.8 C	82.2	96.5	192.6	209.9	22.7
16	1	.0	32.9 C	23.5	47.0	103.4	247.9	5.3
		1.00	32.9 C	38.5	1343.5	1414.9	243.1	5.3
17	1	.0	32.8 C	38.6	1343.7	1415.0	220.8	18.4
		1.00	32.8 C	142.3	3791.6	3966.7	211.3	18.4



## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
18	1	.0	0.9 T	3.2	3979.3	3983.5	148.2	0.0
		1.00	0.9 T	3.1	5605.0	5609.0	138.8	0.0
19	1	.0	0.9 T	2.1	5605.0	5608.1	108.3	3.4
		1.00	0.9 T	21.0	6778.4	6800.3	98.8	3.4
20	1	.0	1.3 T	20.1	6778.3	6799.8	74.0	0.7
		1.00	1.3 T	17.7	7273.5	7292.5	68.2	0.7
21	1	.0	2.6 T	27.4	7274.5	7304.6	71.7	1.1
		1.00	2.6 T	23.5	6754.8	6781.0	77.6	1.1
22	1	.0	2.8 T	24.4	6754.8	6782.1	102.4	7.8
		1.00	2.8 T	19.7	5541.2	5563.7	111.9	7.8
23	1	.0	2.8 T	18.7	5541.2	5562.8	142.3	11.5
		1.00	2.8 T	83.6	3875.0	3961.4	151.8	11.5
24	1	.0	22.0 C	59.6	3679.1	3760.7	200.3	23.7
		1.00	22.0 C	73.7	1355.8	1451.5	209.8	23.7
25	1	.0	21.9 C	73.4	1355.6	1450.9	232.1	26.3
		1.00	21.9 C	147.5	27.3	196.7	236.9	26.3
26	1	.0	28.1 C	52.6	49.5	130.2	218.1	24.5
		1.00	28.1 C	154.1	3553.1	3735.4	194.3	24.5
27	1	.0	0.4 C	1.7	3734.1	3736.2	169.7	11.9
		1.00	0.4 C	42.8	4881.8	4925.0	160.0	11.9
28	1	.0	3.4 T	11.1	4889.7	4904.2	9.1	3.3
		1.00	3.4 T	40.1	4827.5	4871.0	16.0	3.3
29	1	.0	3.4 T	51.0	4826.4	4880.8	167.0	3.9
		1.00	3.4 T	37.4	3630.1	3670.9	176.7	3.9
30	1	.0	13.7 C	106.7	3444.0	3564.4	185.1	22.1
		1.00	13.7 C	80.1	95.5	189.3	209.0	22.1
31	1	.0	2.9 C	27.0	1550.7	1580.5	226.4	0.4
		1.00	2.9 C	29.0	517.9	549.8	221.8	0.4
32	1	.0	2.7 C	29.2	517.6	549.6	169.0	0.5
		1.00	2.7 C	33.5	3552.8	3589.0	159.8	0.5
33	1	.0	2.8 C	37.0	3552.5	3592.4	90.9	3.8
		1.00	2.8 C	1.6	5146.2	5150.7	81.7	3.8
34	1	.0	2.6 C	6.7	5146.0	5155.3	13.3	2.6
		1.00	2.6 C	17.1	5307.1	5326.8	4.2	2.6

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
35	1	.0	2.5 C	12.5	5307.2	5322.2	51.3	11.2
		1.00	2.5 C	76.0	4693.2	4771.7	56.9	11.2
36	1	.0	3.5 C	78.3	4690.8	4772.6	57.0	11.3
		1.00	3.5 C	14.0	5306.3	5323.8	51.4	11.3
37	1	.0	3.3 C	18.7	5306.3	5328.3	4.0	3.6
		1.00	3.3 C	14.9	5147.7	5165.9	13.2	3.6
38	1	.0	3.3 C	10.0	5147.8	5161.0	81.6	2.0
		1.00	3.3 C	28.2	3556.1	3587.7	90.8	2.0
39	1	.0	3.3 C	25.3	3556.3	3585.0	159.8	0.5
		1.00	3.3 C	30.4	522.4	556.1	168.9	0.5
40	1	.0	3.6 C	29.8	522.7	556.1	221.7	22.9
		1.00	3.6 C	75.9	1544.5	1624.0	226.2	22.9
41	1	.0	3.1 C	78.0	1561.6	1642.6	226.3	23.4
		1.00	3.1 C	29.8	506.0	538.9	221.7	23.4
42	1	.0	3.3 C	30.3	505.8	539.3	168.9	0.5
		1.00	3.3 C	25.6	3539.8	3568.7	159.8	0.5
43	1	.0	3.1 C	28.4	3539.5	3571.1	90.8	2.0
		1.00	3.1 C	10.2	5131.8	5145.1	81.7	2.0
44	1	.0	3.3 C	15.1	5131.6	5150.0	13.2	3.6
		1.00	3.3 C	18.5	5290.9	5312.8	4.1	3.6
45	1	.0	3.1 C	13.9	5290.8	5307.9	51.4	11.2
		1.00	3.1 C	77.3	4675.8	4756.3	57.0	11.2
46	1	.0	2.5 C	75.4	4678.5	4756.4	57.3	11.0
		1.00	2.5 C	12.8	5297.0	5312.2	51.7	11.0
47	1	.0	2.6 C	17.3	5297.1	5317.0	3.8	2.6
		1.00	2.6 C	6.4	5143.3	5152.3	12.9	2.6
48	1	.0	2.7 C	1.4	5143.4	5147.5	81.4	3.8
		1.00	2.7 C	36.8	3556.6	3596.1	90.5	3.8
49	1	.0	2.7 C	33.3	3556.8	3592.8	159.5	0.4
		1.00	2.7 C	29.3	528.0	560.0	168.6	0.4
50	1	.0	2.8 C	29.0	528.3	560.1	221.5	0.2
		1.00	2.8 C	28.2	1537.1	1568.2	226.0	0.2
51	1	.0	0.7 T	112.8	1087.1	1200.6	208.8	10.8
		1.00	0.7 T	97.1	5710.8	5808.6	139.5	10.8

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
52	1	.0	0.7 T	57.2	5183.3	5241.3	25.5	7.8
		1.00	0.7 T	57.5	5171.9	5230.1	26.3	7.8
53	1	.0	0.7 T	95.3	5714.1	5810.1	140.7	10.6
		1.00	0.7 T	111.0	1128.9	1240.5	209.9	10.6
54	1	.0	17.4 C	4.8	2974.5	2996.6	152.4	0.1
		1.00	17.4 C	6.8	1868.1	1892.2	133.7	0.1
55	1	.0	17.4 C	2.0	898.3	917.7	107.1	0.0
		1.00	17.4 C	1.7	898.1	917.2	107.1	0.0
56	1	.0	3.4 T	10.3	1852.2	1866.0	133.6	0.1
		1.00	3.4 T	12.1	2977.9	2993.3	152.6	0.1
57	1	.0	21.7 C	41.4	4251.4	4314.4	206.0	0.4
		1.00	21.7 C	36.3	2281.1	2339.0	172.7	0.4
58	1	.0	17.9 C	27.5	1347.4	1392.8	141.6	0.4
		1.00	17.9 C	26.7	1359.5	1404.1	141.9	0.4
59	1	.0	16.7 C	25.4	2262.9	2304.9	172.5	0.2
		1.00	16.7 C	21.5	4256.7	4294.8	206.2	0.2
60	1	.0	4.5 T	45.2	4323.6	4373.3	208.2	0.5
		1.00	4.5 T	45.4	2093.4	2143.2	170.5	0.5
61	1	.0	3.4 T	46.3	1242.0	1291.7	141.6	0.6
		1.00	3.4 T	45.5	1258.3	1307.2	142.0	0.6
62	1	.0	4.8 T	43.0	2074.6	2122.5	170.2	0.4
		1.00	4.8 T	42.7	4338.4	4385.9	208.5	0.4
63	1	.0	5.3 C	40.3	3425.4	3471.1	169.5	0.4
		1.00	5.3 C	41.0	1553.5	1599.8	137.9	0.4
64	1	.0	2.2 T	42.4	704.2	748.8	114.9	0.6
		1.00	2.2 T	42.7	715.6	760.6	115.2	0.6
65	1	.0	8.8 T	41.7	1543.9	1594.4	137.7	0.4
		1.00	8.8 T	41.5	3438.7	3488.9	169.7	0.4
66	1	.0	8.7 T	42.1	3421.2	3472.1	169.5	0.4
		1.00	8.7 T	42.4	1552.6	1603.8	137.9	0.4
67	1	.0	2.0 T	42.8	705.9	750.8	115.0	0.6
		1.00	2.0 T	42.5	712.9	757.4	115.1	0.6
68	1	.0	5.3 C	40.5	1549.2	1595.1	137.7	0.4
		1.00	5.3 C	39.8	3436.6	3481.8	169.6	0.4

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
69	1	.0	4.8 T	43.6	4313.1	4361.5	208.1	0.4
		1.00	4.8 T	43.9	2090.5	2139.1	170.6	0.4
70	1	.0	3.3 T	45.8	1244.2	1293.3	141.7	0.6
		1.00	3.3 T	46.6	1253.2	1303.1	141.9	0.6
71	1	.0	4.4 T	45.0	2086.4	2135.9	170.3	0.5
		1.00	4.4 T	44.9	4335.3	4384.6	208.3	0.5
72	1	.0	16.8 C	22.4	4235.2	4274.4	205.9	0.2
		1.00	16.8 C	26.3	2275.3	2318.4	172.8	0.2
73	1	.0	18.1 C	27.1	1346.4	1391.6	141.7	0.4
		1.00	18.1 C	28.0	1355.0	1401.1	141.9	0.4
74	1	.0	21.8 C	36.1	2274.0	2331.9	172.6	0.4
		1.00	21.8 C	41.2	4260.6	4323.6	206.1	0.4
75	1	.0	3.0 T	12.8	2974.6	2990.5	152.6	0.1
		1.00	3.0 T	11.2	1848.1	1862.3	133.5	0.1
76	1	.0	17.4 C	1.2	888.7	907.3	107.0	0.0
		1.00	17.4 C	1.5	899.1	918.0	107.2	0.0
77	1	.0	17.2 C	6.6	1863.1	1886.8	133.6	0.1
		1.00	17.2 C	4.5	2978.0	2999.8	152.5	0.1
78	1	.0	436.2 C	809.6	1038.8	2284.6	65.8	29.9
		1.00	446.4 C	234.7	225.6	906.7	65.8	29.9
79	1	.0	423.0 C	450.0	0.2	873.3	0.0	8.8
		1.00	426.4 C	393.6	0.2	820.2	0.0	8.8
80	1	.0	450.8 C	993.7	1008.4	2453.0	60.9	62.9
		1.00	461.0 C	215.0	161.9	837.9	60.9	62.9
81	1	.0	415.2 C	0.0	0.0	415.3	0.0	0.0
		1.00	418.6 C	0.0	0.0	418.6	0.0	0.0
82	1	.0	436.0 C	814.2	1041.8	2292.0	65.9	30.1
		1.00	446.2 C	235.4	224.7	906.3	65.9	30.1
83	1	.0	422.4 C	451.2	0.1	873.8	0.0	8.8
		1.00	425.8 C	394.8	0.1	820.8	0.0	8.8
84	1	.0	433.4 C	939.0	890.7	2263.2	38.4	52.1
		1.00	443.6 C	63.8	151.6	659.0	38.4	52.1
85	1	.0	418.5 C	178.6	368.1	965.1	0.0	0.0
		1.00	421.9 C	178.6	368.3	968.8	0.0	0.0

## MEMBER STRESSES

ALL UNITS ARE POUN/SQ INCH

MEMB	LD	SECT	AXIAL	BEND-Y	BEND-Z	COMBINED	SHEAR-Y	SHEAR-Z
86	1	.0	99.9 T	1250.2	1278.3	2628.4	30.4	34.8
		1.00	89.7 T	650.7	851.9	1592.4	47.7	34.8
87	1	.0	101.6 T	1114.3	1294.8	2510.8	31.3	25.4
		1.00	91.5 T	272.7	880.4	1244.5	48.5	25.4
88	1	.0	96.2 T	1307.9	1214.2	2618.3	28.6	37.3
		1.00	86.0 T	727.7	816.0	1629.7	45.8	37.3
89	1	.0	40.9 T	1157.2	1273.4	2471.5	33.1	26.7
		1.00	30.7 T	296.9	1000.0	1327.6	50.3	26.7
90	1	.0	100.6 T	1259.2	1277.3	2637.1	30.4	35.1
		1.00	90.4 T	655.7	852.3	1598.4	47.7	35.1
91	1	.0	66.3 T	1122.3	1332.9	2521.5	34.3	24.9
		1.00	56.1 T	237.2	1007.9	1301.2	51.5	24.9
92	1	.0	79.3 T	1321.1	1232.4	2632.7	30.1	36.4
		1.00	69.1 T	663.4	877.8	1610.3	47.3	36.4
93	1	.0	40.5 T	1134.0	1267.1	2441.7	32.9	26.1
		1.00	30.4 T	287.9	995.8	1314.0	50.1	26.1
94	1	.0	5.1 C	0.0	0.2	5.3	0.0	0.0
		1.00	0.0 C	0.0	0.2	0.2	0.0	0.0
95	1	.0	5.1 C	0.0	0.1	5.2	0.0	0.0
		1.00	0.0 C	0.0	0.1	0.1	0.0	0.0
96	1	.0	5.1 C	0.0	0.0	5.1	0.0	0.0
		1.00	0.0 C	0.0	0.0	0.0	0.0	0.0
97	1	.0	5.1 C	0.0	0.1	5.1	0.0	0.0
		1.00	0.0 C	0.0	0.1	0.1	0.0	0.0
100	1	.0	737.5 C	757.9	0.0	1495.3	0.0	8.4
		1.00	746.6 C	111.2	0.0	857.8	0.0	8.4
101	1	.0	724.0 C	0.0	0.0	724.0	0.0	0.0
		1.00	733.2 C	0.0	0.0	733.2	0.0	0.0
102	1	.0	736.4 C	760.3	0.0	1496.7	0.0	8.4
		1.00	745.6 C	108.8	0.0	854.4	0.0	8.4
103	1	.0	729.6 C	343.9	709.1	1782.7	0.0	0.0
		1.00	738.8 C	343.9	709.1	1791.8	0.0	0.0

\*\*\*\*\* END OF LATEST ANALYSIS RESULT \*\*\*\*\*

70. PARAMETER  
71. CODE AISC  
72. FYLD 42000. MEMB 1 TO 53 78 TO 97  
73. FYLD 21999.994 MEMB 54 TO 77 100 TO 103  
74. WMIN 0.188 ALL  
75. DFF 0.063 ALL  
76. LY 197.5 MEMB 1 TO 10 16 TO 25  
77. LZ 197.5 MEMB 1 TO 10 16 TO 25  
78. LY 139.5 MEMB 11 TO 15 26 TO 30 51 TO 53  
79. LZ 139.5 MEMB 11 TO 15 26 TO 30 51 TO 53  
80. UNL 96. MEMB 100 TO 103  
81. KY 1. MEMB 100 TO 103  
82. KZ 1. MEMB 100 TO 103  
83. CB 1. ALL  
84. MAIN 0. ALL  
85. TRACK 1. ALL  
86. RATIO 1. ALL  
87. WELD 1. ALL  
88. LOAD LIST ALL  
89. CHECK CODE ALL

STAAD-III CODE CHECKING - (AISC)  
 \*\*\*\*\*

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
1	ST TUB 60303	PASS 102.52 C	AISC- H1-3 124.16	0.060 6386.57	1 12.00
MEM= 1, UNIT KIP-INCH, L= 12.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
2	ST TUB 60303	PASS 102.21 C	AISC- H1-3 453.24	0.162 18119.21	1 24.00
MEM= 2, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
3	ST TUB 60303	PASS 3.48 T	AISC- H2-1 -8.58	0.224 26842.41	1 24.00
MEM= 3, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
4	ST TUB 60303	PASS 3.23 T	AISC- H2-1 -66.84	0.272 32515.27	1 24.00
MEM= 4, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
5	ST TUB 60303	PASS 3.15 T	AISC- H2-1 -56.86	0.291 34924.72	1 14.75
MEM= 5, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
6	ST TUB 60303	PASS 9.05 T	AISC- H2-1 -89.82	0.292 -34929.59	1 0.00
MEM= 6, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
7	ST TUB 60303	PASS 9.01 T	AISC- H2-1 -79.54	0.272 -32527.80	1 0.00
MEM= 7, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
8	ST TUB 60303	PASS 8.80 T	AISC- H2-1 59.35	0.225 -26867.34	1 0.00
MEM= 8, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
9	ST TUB 60303	PASS 99.05 C	AISC- H1-3 -193.80	0.159 -18145.39	1 0.00
MEM= 9, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
10	ST TUB 60303	PASS 97.55 C	AISC- H1-3 238.76	0.062 -6398.76	1 0.00
MEM= 10, UNIT KIP-INCH, L= 12.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
11	ST TUB 60303	PASS 102.29 C	AISC- H1-3 503.27	0.152 17228.99	1 36.00
MEM= 11, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
12	ST TUB 60303	PASS 0.62	AISC- H1-3 -135.86	0.197 23514.55	1 14.75
MEM= 12, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
13	ST TUB 60303	PASS 10.68 T	AISC- H2-1 37.00	0.196 -23524.60	1 0.00



ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 13, UNIT KIP-INCH, L= 38.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
14	ST TUB 60303	PASS 10.92 T	AISC- H2-1 162.53	0.195 -23116.13	1 0.00
MEM= 14, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
15	ST TUB 60303	PASS 43.47 C	AISC- H1-3 -351.06	0.143 -16495.53	1 0.00
MEM= 15, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
16	ST TUB 60303	PASS 103.37 C	AISC- H1-3 123.08	0.060 6404.18	1 12.00
MEM= 16, UNIT KIP-INCH, L= 12.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
17	ST TUB 60303	PASS 103.05 C	AISC- H1-3 455.22	0.162 18073.40	1 24.00
MEM= 17, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
18	ST TUB 60303	PASS 2.91 T	AISC- H2-1 -9.83	0.223 26717.31	1 24.00
MEM= 18, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
19	ST TUB 60303	PASS 2.92 T	AISC- H2-1 -67.32	0.270 32310.16	1 24.00
MEM= 19, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
20	ST TUB 60303	PASS 4.20 T	AISC- H2-1 -56.54	0.289 34670.12	1 14.75
MEM= 20, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
21	ST TUB 60303	PASS 8.26 T	AISC- H2-1 -87.71	0.290 -34675.22	1 0.00
MEM= 21, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
22	ST TUB 60303	PASS 8.94 T	AISC- H2-1 -78.21	0.269 -32197.92	1 0.00
MEM= 22, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
23	ST TUB 60303	PASS 8.72 T	AISC- H2-1 59.99	0.221 -26413.26	1 0.00
MEM= 23, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
24	ST TUB 60303	PASS 69.04 C	AISC- H1-3 -190.78	0.152 -17537.01	1 0.00
MEM= 24, UNIT KIP-INCH, L= 24.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
25	ST TUB 60303	PASS 68.65 C	AISC- H1-3 235.03	0.060 -6461.73	1 0.00
MEM= 25, UNIT KIP-INCH, L= 12.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 159.7 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 5.85 FT= 25.20 FV= 16.80					
26	ST TUB 60303	PASS 88.35 C	AISC- H1-3 493.22	0.150 16936.65	1 36.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 26, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
27	ST TUB 60303	PASS 1.31 C	AISC- H1-3 -137.06	0.195 23269.86	1 14.75
MEM= 27, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
28	ST TUB 60303	PASS 10.57 T	AISC- H2-1 35.54	0.195 -23307.66	1 0.00
MEM= 28, UNIT KIP-INCH, L= 38.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
29	ST TUB 60303	PASS 10.65 T	AISC- H2-1 163.12	0.194 -23006.02	1 0.00
MEM= 29, UNIT KIP-INCH, L= 14.8 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
30	ST TUB 60303	PASS 42.98 C	AISC- H1-3 -341.36	0.142 -16416.41	1 0.00
MEM= 30, UNIT KIP-INCH, L= 36.0 AX= 3.14 SZ= 4.8 SY= 3.2 KL/R-Y= 112.8 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 11.68 FT= 25.20 FV= 16.80					
31	ST TUB 40203	PASS 5.88 C	AISC- H1-3 -35.04	0.063 3023.79	1 0.00
MEM= 31, UNIT KIP-INCH, L= 12.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 15.0 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.29 FT= 25.20 FV= 16.80					
32	ST TUB 40203	PASS 5.54 C	AISC- H1-3 43.51	0.142 6928.03	1 24.00
MEM= 32, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
33	ST TUB 40203	PASS 5.72 C	AISC- H1-3 2.14	0.204 10035.15	1 24.00
MEM= 33, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
34	ST TUB 40203	PASS 5.22 C	AISC- H1-3 -22.22	0.211 10348.90	1 24.00
MEM= 34, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
35	ST TUB 40203	PASS 5.11 C	AISC- H1-3 16.28	0.211 -10349.03	1 0.00
MEM= 35, UNIT KIP-INCH, L= 14.8 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 18.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.04 FT= 25.20 FV= 16.80					
36	ST TUB 40203	PASS 7.09 C	AISC- H1-3 18.22	0.211 10347.23	1 14.75
MEM= 36, UNIT KIP-INCH, L= 14.8 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 18.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.04 FT= 25.20 FV= 16.80					
37	ST TUB 40203	PASS 6.66 C	AISC- H1-3 -24.30	0.211 -10347.33	1 0.00
MEM= 37, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
38	ST TUB 40203	PASS 6.64 C	AISC- H1-3 12.99	0.205 -10038.14	1 0.00
MEM= 38, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
39	ST TUB 40203	PASS 6.74 C	AISC- H1-3 32.91	0.142 -6934.87	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 39, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
40	ST TUB 40203	PASS 7.33 C	AISC- H1-3 98.68	0.064 -3011.76	1 12.00
MEM= 40, UNIT KIP-INCH, L= 12.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 15.0 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.29 FT= 25.20 FV= 16.80					
41	ST TUB 40203	PASS 6.20 C	AISC- H1-3 101.42	0.065 3045.02	1 0.00
MEM= 41, UNIT KIP-INCH, L= 12.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 15.0 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.29 FT= 25.20 FV= 16.80					
42	ST TUB 40203	PASS 6.60 C	AISC- H1-3 33.24	0.142 6902.70	1 24.00
MEM= 42, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
43	ST TUB 40203	PASS 6.26 C	AISC- H1-3 13.26	0.204 10007.03	1 24.00
MEM= 43, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
44	ST TUB 40203	PASS 6.73 C	AISC- H1-3 -24.08	0.211 10317.29	1 24.00
MEM= 44, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
45	ST TUB 40203	PASS 6.33 C	AISC- H1-3 18.06	0.211 -10317.12	1 0.00
MEM= 45, UNIT KIP-INCH, L= 14.8 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 18.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.04 FT= 25.20 FV= 16.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
46	ST TUB 40203	PASS 4.95 C	AISC- H1-3 16.58	0.211 10329.13	1 14.75
MEM= 46, UNIT KIP-INCH, L= 14.8 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 18.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.04 FT= 25.20 FV= 16.80					
47	ST TUB 40203	PASS 5.27 C	AISC- H1-3 -22.50	0.211 -10329.25	1 0.00
MEM= 47, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
48	ST TUB 40203	PASS 5.41 C	AISC- H1-3 1.84	0.204 -10029.66	1 0.00
MEM= 48, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
49	ST TUB 40203	PASS 5.42 C	AISC- H1-3 43.29	0.143 -6935.86	1 0.00
MEM= 49, UNIT KIP-INCH, L= 24.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 29.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 23.07 FT= 25.20 FV= 16.80					
50	ST TUB 40203	PASS 5.63 C	AISC- H1-3 -36.72	0.062 -2997.38	1 12.00
MEM= 50, UNIT KIP-INCH, L= 12.0 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 15.0 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.29 FT= 25.20 FV= 16.80					
51	ST TUB 40203	PASS 1.38 T	AISC- H2-1 126.21	0.231 11136.15	1 50.75
MEM= 51, UNIT KIP-INCH, L= 50.8 AX= 2.02 SZ= 2.0 SY= 1.3 KL/R-Y= 173.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 4.94 FT= 25.20 FV= 16.80					
52	ST TUB 40203	PASS 1.45 T	AISC- H2-1 74.40	0.208 -10107.46	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
--------	-------	---------------	----------------------	--------------	----------------------

MEM=	52, UNIT KIP-INCH, L= 38.0	AX= 2.02	SZ= 2.0	SY= 1.3	
KL/R-Y=	173.9	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES:	FCZ= 25.20
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 4.94	FT= 25.20 FV= 16.80

53	ST TUB 40203	PASS	AISC- H2-1	0.231	1
		1.38 T	123.90	-11142.45	0.00

MEM=	53, UNIT KIP-INCH, L= 50.8	AX= 2.02	SZ= 2.0	SY= 1.3	
KL/R-Y=	173.9	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES:	FCZ= 25.20
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 4.94	FT= 25.20 FV= 16.80

54	PRI SMAT	PASS	AISC- H1-3	0.235	1
		9.96 C	-0.34	-419.57	0.00

MEM=	54, UNIT KIP-INCH, L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1	
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES:	FCZ= 13.20
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80

55	PRI SMAT	PASS	AISC- H1-3	0.073	1
		9.98 C	0.15	-126.71	0.00

MEM=	55, UNIT KIP-INCH, L= 38.0	AX= 0.57	SZ= 0.1	SY= 0.1	
KL/R-Y=	124.6	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES:	FCZ= 13.20
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.32	FT= 13.20 FV= 8.80

56	PRI SMAT	PASS	AISC- H2-1	0.227	1
		1.96 T	-0.86	420.04	50.75

MEM=	56, UNIT KIP-INCH, L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1	
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES:	FCZ= 13.20
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80

57	PRI SMAT	PASS	AISC- H1-3	0.337	1
		12.44 C	-2.95	-599.68	0.00

MEM=	57, UNIT KIP-INCH, L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1	
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES:	FCZ= 13.20
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80

58	PRI SMAT	PASS	AISC- H1-3	0.110	1
		10.30 C	-1.90	191.77	38.00

MEM=	58, UNIT KIP-INCH, L= 38.0	AX= 0.57	SZ= 0.1	SY= 0.1	
KL/R-Y=	124.6	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES:	FCZ= 13.20
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.32	FT= 13.20 FV= 8.80

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
59	PRI SMAT	PASS 9.56 C	AISC- H1-3 -1.53	0.333 600.43	1 50.75
MEM= 59, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
60	PRI SMAT	PASS 2.56 T	AISC- H2-1 -3.22	0.331 -609.86	1 0.00
MEM= 60, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
61	PRI SMAT	PASS 1.94 T	AISC- H2-1 -3.25	0.099 177.49	1 38.00
MEM= 61, UNIT KIP-INCH, L= 38.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 124.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.32 FT= 13.20 FV= 8.80					
62	PRI SMAT	PASS 2.77 T	AISC- H2-1 -3.05	0.332 611.95	1 50.75
MEM= 62, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
63	PRI SMAT	PASS 3.04 C	AISC- H1-3 -2.88	0.265 -483.17	1 0.00
MEM= 63, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
64	PRI SMAT	PASS 1.27 T	AISC- H2-1 -3.05	0.057 100.94	1 38.00
MEM= 64, UNIT KIP-INCH, L= 38.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 124.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.32 FT= 13.20 FV= 8.80					
65	PRI SMAT	PASS 5.04 T	AISC- H2-1 -2.96	0.264 485.05	1 50.75



ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
--------	-------	---------------	----------------------	--------------	----------------------

-----					
MEM=	65, UNIT KIP-INCH,	L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80
66	PRI SMAT	PASS	AISC- H2-1	0.262	1
		5.02 T	-3.00	-482.58	0.00
-----					
MEM=	66, UNIT KIP-INCH,	L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80
67	PRI SMAT	PASS	AISC- H2-1	0.057	1
		1.17 T	-3.03	100.56	38.00
-----					
MEM=	67, UNIT KIP-INCH,	L= 38.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	124.6	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.32	FT= 13.20 FV= 8.80
68	PRI SMAT	PASS	AISC- H1-3	0.266	1
		3.06 C	-2.84	484.75	50.75
-----					
MEM=	68, UNIT KIP-INCH,	L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80
69	PRI SMAT	PASS	AISC- H2-1	0.330	1
		2.74 T	-3.11	-608.39	0.00
-----					
MEM=	69, UNIT KIP-INCH,	L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80
70	PRI SMAT	PASS	AISC- H2-1	0.098	1
		1.91 T	-3.32	176.77	38.00
-----					
MEM=	70, UNIT KIP-INCH,	L= 38.0	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	124.6	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 3.32	FT= 13.20 FV= 8.80
71	PRI SMAT	PASS	AISC- H2-1	0.332	1
		2.55 T	-3.20	611.52	50.75
-----					
MEM=	71, UNIT KIP-INCH,	L= 50.8	AX= 0.57	SZ= 0.1	SY= 0.1
KL/R-Y=	166.3	CB= 1.00	YLD= 22.00	ALLOWABLE STRESSES: FCZ= 13.20	
FTZ=	14.52	FCY= 13.20	FTY= 14.52	FA= 1.86	FT= 13.20 FV= 8.80
-----					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
72	PRI SMAT	PASS 9.67 C	AISC- H1-3 -1.60	0.332 -597.39	1 0.00
MEM= 72, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
73	PRI SMAT	PASS 10.38 C	AISC- H1-3 -1.99	0.110 191.13	1 38.00
MEM= 73, UNIT KIP-INCH, L= 38.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 124.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.32 FT= 13.20 FV= 8.80					
74	PRI SMAT	PASS 12.52 C	AISC- H1-3 -2.94	0.338 600.98	1 50.75
MEM= 74, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
75	PRI SMAT	PASS 1.74 T	AISC- H2-1 -0.92	0.226 -419.58	1 0.00
MEM= 75, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
76	PRI SMAT	PASS 9.99 C	AISC- H1-3 0.11	0.073 126.82	1 38.00
MEM= 76, UNIT KIP-INCH, L= 38.0 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 124.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 3.32 FT= 13.20 FV= 8.80					
77	PRI SMAT	PASS 9.86 C	AISC- H1-3 -0.32	0.235 420.07	1 50.75
MEM= 77, UNIT KIP-INCH, L= 50.8 AX= 0.57 SZ= 0.1 SY= 0.1 KL/R-Y= 166.3 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 1.86 FT= 13.20 FV= 8.80					
78	ST TUB 35353	PASS 1042.63 C	AISC- H1-3 1989.25	0.092 -2552.52	1 0.00

ALL UNITS ARE - POUN INCH. (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
-----					
MEM=	78, UNIT KIP-INCH,	L= 36.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	26.8	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 23.34	FT= 25.20 FV= 16.80
-----					
79	ST TUB 35353	PASS	AISC- H1-3	0.035	1
		1011.06 C	1105.66	-0.58	0.00
-----					
MEM=	79, UNIT KIP-INCH,	L= 12.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	8.9	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 24.70	FT= 25.20 FV= 16.80
-----					
80	ST TUB 35353	PASS	AISC- H1-3	0.099	1
		1077.46 C	2441.70	2477.90	0.00
-----					
MEM=	80, UNIT KIP-INCH,	L= 36.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	26.8	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 23.34	FT= 25.20 FV= 16.80
-----					
81	ST TUB 35353	PASS	AISC- H1-3	0.017	1
		1000.51 C	-0.02	-0.01	12.00
-----					
MEM=	81, UNIT KIP-INCH,	L= 12.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	8.9	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 24.70	FT= 25.20 FV= 16.80
-----					
82	ST TUB 35353	PASS	AISC- H1-3	0.092	1
		1042.09 C	-2000.56	2559.78	0.00
-----					
MEM=	82, UNIT KIP-INCH,	L= 36.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	26.8	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 23.34	FT= 25.20 FV= 16.80
-----					
83	ST TUB 35353	PASS	AISC- H1-3	0.035	1
		1009.63 C	-1108.71	-0.30	0.00
-----					
MEM=	83, UNIT KIP-INCH,	L= 12.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	8.9	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 24.70	FT= 25.20 FV= 16.80
-----					
84	ST TUB 35353	PASS	AISC- H1-3	0.091	1
		1035.85 C	-2307.26	-2188.68	0.00
-----					
MEM=	84, UNIT KIP-INCH,	L= 36.0	AX= 2.39	SZ= 2.5	SY= 2.5
KL/R-Y=	26.8	CB= 1.00	YLD= 42.00	ALLOWABLE STRESSES: FCZ= 25.20	
FTZ=	25.20	FCY= 25.20	FTY= 25.20	FA= 23.34	FT= 25.20 FV= 16.80
-----					

ALL UNITS ARE - POUN INCH. (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
85	ST TUB 35353	PASS 1008.30 C	AISC- H1-3 438.91	0.039 904.94	1 12.00
MEM= 85, UNIT KIP-INCH, L= 12.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 8.9 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.70 FT= 25.20 FV= 16.80					
86	ST TUB 20203	PASS 126.90 T	AISC- H2-1 -875.14	0.104 -894.81	1 0.00
MEM= 86, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
87	ST TUB 20203	PASS 129.08 T	AISC- H2-1 780.03	0.100 -906.36	1 0.00
MEM= 87, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
88	ST TUB 20203	PASS 122.20 T	AISC- H2-1 -915.54	0.104 -849.95	1 0.00
MEM= 88, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
89	ST TUB 20203	PASS 51.98 T	AISC- H2-1 810.04	0.098 -891.37	1 0.00
MEM= 89, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
90	ST TUB 20203	PASS 127.75 T	AISC- H2-1 -881.46	0.105 -894.11	1 0.00
MEM= 90, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
91	ST TUB 20203	PASS 84.18 T	AISC- H2-1 785.63	0.100 -933.01	1 0.00

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
MEM= 91, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
92	ST TUB 20203	PASS 100.68 T	AISC- H2-1 -924.75	0.104 -862.68	1 0.00
MEM= 92, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
93	ST TUB 20203	PASS 51.48 T	AISC- H2-1 793.83	0.097 -886.98	1 0.00
MEM= 93, UNIT KIP-INCH, L= 50.9 AX= 1.27 SZ= 0.7 SY= 0.7 KL/R-Y= 68.6 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 18.67 FT= 25.20 FV= 16.80					
94	ST TUB 35353	PASS 12.19 C	AISC- H1-3 -0.02	0.000 0.43	1 0.00
MEM= 94, UNIT KIP-INCH, L= 18.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 13.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.40 FT= 25.20 FV= 16.80					
95	ST TUB 35353	PASS 12.17 C	AISC- H1-3 0.02	0.000 -0.17	1 0.00
MEM= 95, UNIT KIP-INCH, L= 18.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 13.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.40 FT= 25.20 FV= 16.80					
96	ST TUB 35353	PASS 12.18 C	AISC- H1-3 -0.02	0.000 0.09	1 0.00
MEM= 96, UNIT KIP-INCH, L= 18.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 13.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.40 FT= 25.20 FV= 16.80					
97	ST TUB 35353	PASS 12.18 C	AISC- H1-3 0.00	0.000 0.13	1 0.00
MEM= 97, UNIT KIP-INCH, L= 18.0 AX= 2.39 SZ= 2.5 SY= 2.5 KL/R-Y= 13.4 CB= 1.00 YLD= 42.00 ALLOWABLE STRESSES: FCZ= 25.20 FTZ= 25.20 FCY= 25.20 FTY= 25.20 FA= 24.40 FT= 25.20 FV= 16.80					

ALL UNITS ARE - POUN INCH (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
--------	-------	---------------	----------------------	--------------	----------------------

100	PRI SMAT	PASS 1019.17 C	AISC- H1-3 967.05	0.159 0.00	1 0.00
-----	----------	-------------------	----------------------	---------------	-----------

MEM= 100, UNIT KIP-INCH, L= 96.0 AX= 1.38 SZ= 1.3 SY= 1.3  
 KL/R-Y= 81.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20  
 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 7.25 FT= 13.20 FV= 8.80

101	PRI SMAT	PASS 1013.21 C	AISC- H1-3 0.00	0.101 0.00	1 96.00
-----	----------	-------------------	--------------------	---------------	------------

MEM= 101, UNIT KIP-INCH, L= 96.0 AX= 1.38 SZ= 1.3 SY= 1.3  
 KL/R-Y= 81.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20  
 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 7.25 FT= 13.20 FV= 8.80

102	PRI SMAT	PASS 1017.75 C	AISC- H1-3 -970.09	0.159 0.03	1 0.00
-----	----------	-------------------	-----------------------	---------------	-----------

MEM= 102, UNIT KIP-INCH, L= 96.0 AX= 1.38 SZ= 1.3 SY= 1.3  
 KL/R-Y= 81.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20  
 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 7.25 FT= 13.20 FV= 8.80

103	PRI SMAT	PASS 1020.96 C	AISC- H1-3 438.87	0.182 904.84	1 96.00
-----	----------	-------------------	----------------------	-----------------	------------

MEM= 103, UNIT KIP-INCH, L= 96.0 AX= 1.38 SZ= 1.3 SY= 1.3  
 KL/R-Y= 81.6 CB= 1.00 YLD= 22.00 ALLOWABLE STRESSES: FCZ= 13.20  
 FTZ= 14.52 FCY= 13.20 FTY= 14.52 FA= 7.25 FT= 13.20 FV= 8.80

90. SELECT WELD ALL

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

1	STA 1	1 322.99	3/16 326.95	470.13 99.01
---	----------	-------------	----------------	-----------------

1	END 1	1 322.99	3/16 323.79	1281.67 1197.30
---	----------	-------------	----------------	--------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

2	STA 1	1 270.69	3/16 281.32	1259.43 1197.39
---	----------	-------------	----------------	--------------------

2	END 1	1 270.69	3/16 275.00	3388.63 3366.58
---	----------	-------------	----------------	--------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

3	STA 1	1 289.42	3/16 244.51	3404.75 3383.61
---	----------	-------------	----------------	--------------------

3	END 1	1 289.42	3/16 238.19	4789.88 4775.19
---	----------	-------------	----------------	--------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

4	STA 1	1 209.87	3/16 177.75	4782.27 4774.35
---	----------	-------------	----------------	--------------------

4	END 1	1 209.87	3/16 171.43	5804.75 5798.42
---	----------	-------------	----------------	--------------------

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

5	STA 1	1 145.62	3/16 123.08	5800.85 5797.72
---	----------	-------------	----------------	--------------------

5	END 1	1 145.62	3/16 119.19	6227.06 6224.21
---	----------	-------------	----------------	--------------------

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
6	STA	1	3/16	6237.66
	1	133.93	113.14	6235.20
6	END	1	3/16	5807.60
	1	133.93	117.02	5804.88
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
7	STA	1	3/16	5811.35
	1	198.97	165.33	5805.59
7	END	1	3/16	4802.15
	1	198.97	171.65	4794.96
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
8	STA	1	3/16	4807.86
	1	279.90	231.99	4794.10
8	END	1	3/16	3477.03
	1	279.90	238.31	3457.54
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
9	STA	1	3/16	3327.56
	1	276.59	277.47	3304.41
9	END	1	3/16	1290.21
	1	276.59	283.79	1227.85
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
10	STA	1	3/16	1312.52
	1	332.36	326.29	1227.10



STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
10	END 1	1 332.36	3/16 329.45	508.02 197.70
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
11	STA 1	1 296.54	3/16 294.90	426.26 82.43
11	END 1	1 296.54	3/16 279.02	3246.69 3221.06
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
12	STA 1	1 397.53	3/16 309.87	3254.09 3214.81
12	END 1	1 397.53	3/16 303.36	4244.61 4215.05
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
13	STA 1	1 2.47	3/16 6.27	4194.72 4194.71
13	END 1	1 2.47	3/16 12.26	4149.03 4149.01
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
14	STA 1	1 397.37	3/16 310.08	4184.52 4154.05
14	END 1	1 397.37	3/16 316.59	3165.56 3124.52
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
15	STA	1	3/16	3063.26
	1	312.64	277.83	3034.58
15	END	1	3/16	458.35
	1	312.64	293.71	161.47
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
16	STA	1	3/16	469.98
	1	325.21	327.25	89.56
16	END	1	3/16	1285.22
	1	325.21	324.09	1200.41
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
17	STA	1	3/16	1262.90
	1	272.81	281.57	1200.50
17	END	1	3/16	3381.48
	1	272.81	275.25	3359.19
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
18	STA	1	3/16	3397.02
	1	292.05	244.85	3375.57
18	END	1	3/16	4768.04
	1	292.05	238.53	4753.10
-----				
AX=	18.00	SZ= 30.00	SY= 21.00	JW= 121.50
		CH= 3.00	CV= 1.50	
-----				
19	STA	1	3/16	4760.38
	1	212.27	177.97	4752.31
19	END	1	3/16	5768.45
	1	212.27	171.65	5761.99

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
20	STA	1	3/16	5764.80
	1	147.84	123.19	5761.58
20	END	1	3/16	6182.10
	1	147.84	119.31	6179.18
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
21	STA	1	3/16	6191.99
	1	142.45	118.93	6189.21
21	END	1	3/16	5748.71
	1	142.45	122.81	5745.63
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
22	STA	1	3/16	5752.89
	1	207.82	171.30	5746.59
22	END	1	3/16	4722.23
	1	207.82	177.62	4714.31
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
23	STA	1	3/16	4728.38
	1	289.23	238.23	4713.51
23	END	1	3/16	3375.55
	1	289.23	244.55	3354.23
-----				
AX=	18.00 SZ=	30.00 SY=	21.00 JW=	121.50 CH=
				3.00 CV=
				1.50
-----				
24	STA	1	3/16	3210.96
	1	284.87	273.36	3186.60

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
24	END	1	3/16	1292.45
	1	284.87	279.68	1229.25

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

25	STA	1	3/16	1315.24
	1	340.77	322.21	1228.78
25	END	1	3/16	498.69
	1	340.77	325.37	163.40

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

26	STA	1	3/16	444.67
	1	310.79	298.07	110.88
26	END	1	3/16	3190.14
	1	310.79	282.19	3162.40

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

27	STA	1	3/16	3209.00
	1	414.54	319.09	3166.07
27	END	1	3/16	4204.24
	1	414.54	312.58	4172.06

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

28	STA	1	3/16	4155.78
	1	11.62	11.52	4155.74
28	END	1	3/16	4126.62
	1	11.62	16.14	4126.57

-----  
AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
-----

STAAD-III WELD DESIGN  
 \*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

29	STA	1	3/16	4163.90
	1	388.15	304.94	4134.54
29	END	1	3/16	3149.31
	1	388.15	311.45	3109.74

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

30	STA	1	3/16	3045.59
	1	305.08	273.51	3017.90
30	END	1	3/16	449.47
	1	305.08	289.39	158.75

-----  
 AX= 18.00 SZ= 30.00 SY= 21.00 JW= 121.50 CH= 3.00 CV= 1.50  
 -----

31	STA	1	3/16	1241.46
	1	1.62	151.69	1232.16
31	END	1	3/16	453.20
	1	1.62	148.64	428.13

-----  
 AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
 -----

32	STA	1	3/16	450.30
	1	42.16	133.68	427.92
32	END	1	3/16	2801.76
	1	42.16	127.58	2798.53

-----  
 AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
 -----

33	STA	1	3/16	2804.02
	1	81.93	101.14	2800.99
33	END	1	3/16	4019.78
	1	81.93	95.04	4017.82

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
				CH= 2.00
				CV= 1.00
-----				
34	STA	1	3/16	4023.46
	1	117.24	67.20	4021.19
34	END	1	3/16	4156.68
	1	117.24	61.10	4154.58
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
				CH= 2.00
				CV= 1.00
-----				
35	STA	1	3/16	4155.53
	1	154.64	110.28	4151.19
35	END	1	3/16	3724.36
	1	154.64	114.03	3719.40
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
				CH= 2.00
				CV= 1.00
-----				
36	STA	1	3/16	3725.16
	1	155.16	114.35	3720.17
36	END	1	3/16	4156.82
	1	155.16	110.61	4152.45
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
				CH= 2.00
				CV= 1.00
-----				
37	STA	1	3/16	4157.91
	1	118.07	61.31	4155.78
37	END	1	3/16	4031.52
	1	118.07	67.41	4029.22
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
				CH= 2.00
				CV= 1.00
-----				
38	STA	1	3/16	4027.60
	1	82.33	95.37	4025.63

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
38	END 1	1 82.33	3/16 101.47	2800.77 2797.72
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
		CH= 2.00	CV= 1.00	
-----				
39	STA 1	1 43.19	3/16 128.04	2799.01 2795.75
39	END 1	1 43.19	3/16 134.14	455.40 433.04
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
		CH= 2.00	CV= 1.00	
-----				
40	STA 1	1 8.06	3/16 149.26	458.15 433.08
40	END 1	1 8.06	3/16 152.30	1273.51 1264.34
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
		CH= 2.00	CV= 1.00	
-----				
41	STA 1	1 16.37	3/16 156.44	1288.36 1278.72
41	END 1	1 16.37	3/16 153.39	447.08 419.63
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
		CH= 2.00	CV= 1.00	
-----				
42	STA 1	1 51.17	3/16 138.14	445.04 419.95
42	END 1	1 51.17	3/16 132.04	2786.61 2783.01
-----				
AX=	12.00	SZ= 13.33	SY= 9.33	JW= 36.00
		CH= 2.00	CV= 1.00	

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

43	STA	1	3/16	2788.14
	1	89.25	104.95	2784.74

43	END	1	3/16	4015.38
	1	89.25	98.86	4013.17

-----  
AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
-----

44	STA	1	3/16	4019.35
	1	123.74	70.27	4016.83

44	END	1	3/16	4146.01
	1	123.74	64.17	4143.66

-----  
AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
-----

45	STA	1	3/16	4144.62
	1	160.03	113.04	4139.98

45	END	1	3/16	3712.68
	1	160.03	116.78	3707.39

-----  
AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
-----

46	STA	1	3/16	3712.67
	1	158.15	116.06	3707.48

46	END	1	3/16	4147.87
	1	158.15	112.31	4143.33

-----  
AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
-----

47	STA	1	3/16	4149.15
	1	121.32	62.88	4146.90

47	END	1	3/16	4021.30
	1	121.32	68.97	4018.88



STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	12.00 SZ=	13.33 SY=	9.33 JW=	36.00 CH= 2.00 CV= 1.00
-----				
48	STA	1	3/16	4017.43
	1	86.77	97.21	4015.32
48	END	1	3/16	2807.13
	1	86.77	103.31	2803.89
-----				
AX=	12.00 SZ=	13.33 SY=	9.33 JW=	36.00 CH= 2.00 CV= 1.00
-----				
49	STA	1	3/16	2804.91
	1	47.61	130.08	2801.49
49	END	1	3/16	459.28
	1	47.61	136.18	436.04
-----				
AX=	12.00 SZ=	13.33 SY=	9.33 JW=	36.00 CH= 2.00 CV= 1.00
-----				
50	STA	1	3/16	461.67
	1	7.26	151.26	436.13
50	END	1	3/16	1232.16
	1	7.26	154.31	1222.44
-----				
AX=	12.00 SZ=	13.33 SY=	9.33 JW=	36.00 CH= 2.00 CV= 1.00
-----				
51	STA	1	3/16	942.78
	1	3.85	139.90	932.34
51	END	1	3/16	4528.17
	1	3.85	93.74	4527.20
-----				
AX=	12.00 SZ=	13.33 SY=	9.33 JW=	36.00 CH= 2.00 CV= 1.00
-----				
52	STA	1	3/16	4086.18
	1	1.77	17.04	4086.15

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

52	END	1	3/16	4077.46
	1	1.77	17.56	4077.42

-----  
 AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
 -----

53	STA	1	3/16	4529.38
	1	3.95	94.58	4528.39

53	END	1	3/16	973.81
	1	3.95	140.74	963.58

-----  
 AX= 12.00 SZ= 13.33 SY= 9.33 JW= 36.00 CH= 2.00 CV= 1.00  
 -----

78	STA	1	3/16	1883.56
	1	69.75	87.68	1880.22

78	END	1	3/16	783.84
	1	69.75	87.68	775.79

-----  
 AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
 -----

79	STA	1	3/16	758.41
	1	97.28	92.90	746.39

79	END	1	3/16	716.96
	1	97.28	92.90	704.23

-----  
 AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
 -----

80	STA	1	3/16	2019.99
	1	80.02	79.02	2016.86

80	END	1	3/16	730.87
	1	80.02	79.02	722.17

-----  
 AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
 -----

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

81	STA	1	3/16	400.53
	1	93.47	93.47	378.09

81	END	1	3/16	403.43
	1	93.47	93.47	381.16

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

82	STA	1	3/16	1889.44
	1	70.31	88.19	1886.07

82	END	1	3/16	783.54
	1	70.31	88.19	775.38

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

83	STA	1	3/16	758.76
	1	97.24	92.86	746.75

83	END	1	3/16	717.30
	1	97.24	92.86	704.59

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

84	STA	1	3/16	1865.48
	1	75.68	68.83	1862.67

84	END	1	3/16	585.69
	1	75.68	68.83	576.69

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

85	STA	1	3/16	830.17
	1	93.30	93.30	819.61

85	END	1	3/16	833.43
	1	93.30	93.30	822.92

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
-----				
AX=	14.00 SZ=	16.33 SY=	16.33 JW=	57.17 CH= 1.75 CV= 1.75
-----				
86	STA	1	3/16	1862.98
	1	126.25	124.04	1854.55
86	END	1	3/16	1142.63
	1	126.25	132.67	1127.86
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
87	STA	1	3/16	1775.99
	1	77.85	80.76	1772.44
87	END	1	3/16	892.48
	1	77.85	89.38	884.57
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
88	STA	1	3/16	1854.32
	1	118.91	114.55	1846.95
88	END	1	3/16	1166.06
	1	118.91	123.18	1153.42
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
89	STA	1	3/16	1740.45
	1	85.70	88.90	1736.07
89	END	1	3/16	942.81
	1	85.70	97.53	933.83
-----				
AX=	8.00 SZ=	5.33 SY=	5.33 JW=	10.67 CH= 1.00 CV= 1.00
-----				
90	STA	1	3/16	1869.23
	1	127.06	124.72	1860.73

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
--------	----------------------	--------------------------	---------------------------	----------------------------

90	END	1	3/16	1147.05
	1	127.06	133.34	1132.17

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

91	STA	1	3/16	1778.79
	1	82.15	86.83	1774.76

91	END	1	3/16	927.69
	1	82.15	95.46	919.10

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

92	STA	1	3/16	1863.14
	1	127.94	124.78	1854.55

92	END	1	3/16	1152.25
	1	127.94	133.40	1137.32

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

93	STA	1	3/16	1719.41
	1	83.94	87.34	1715.14

93	END	1	3/16	932.99
	1	83.94	95.96	924.24

-----  
 AX= 8.00 SZ= 5.33 SY= 5.33 JW= 10.67 CH= 1.00 CV= 1.00  
 -----

94	STA	1	3/16	4.79
	1	0.00	0.02	4.79

94	END	1	3/16	0.16
	1	0.00	0.02	0.15

-----  
 AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
 -----

STAAD-III WELD DESIGN  
\*\*\*\*\*

ALL UNITS ARE - INCH POUN

MEMBER	LOCATION/ LOADING	WELD TYPE/ HOR STRESS	WELD SIZE/ VERT STRESS	COMB STRESS/ DIR STRESS
95	STA	1	3/16	4.70
	1	0.00	0.01	4.70
95	END	1	3/16	0.07
	1	0.00	0.01	0.06

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

96	STA	1	3/16	4.67
	1	0.00	0.00	4.67
96	END	1	3/16	0.04
	1	0.00	0.00	0.04

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

97	STA	1	3/16	4.68
	1	0.00	0.00	4.68
97	END	1	3/16	0.05
	1	0.00	0.00	0.05

-----  
AX= 14.00 SZ= 16.33 SY= 16.33 JW= 57.17 CH= 1.75 CV= 1.75  
-----

\*\*\*\*\* END OF TABULATED WELD DESIGN \*\*\*\*\*

91. STEEL TAKE OFF

STEEL TAKE-OFF

PROFILE	LENGTH (INCH)	WEIGHT (POUN)
ST TUB 60303	674.00	598.930
ST TUB 40203	534.50	305.552
ST TUB 35353	264.00	178.562
ST TUB 20203	407.29	146.385
TOTAL =		1229.43

TOTAL VOLUME OF PRISMATIC SECTIONS = 395.32 CUBIC INCH

\*\*\*\*\* END OF DATA FROM INTERNAL STORAGE \*\*\*\*\*

92. FINISH

\*\*\*\*\* END OF STAAD-III \*\*\*\*\*

\*\*\*\* DATE= OCT 4,1996 TIME= 15:53:49 \*\*\*\*

\*\*\*\*\*  
 \* For questions on STAAD-III, contact: \*  
 \* Research Engineers, Inc at \*  
 \* Ph: (714) 974-2500 Fax: (714) 921-2543 \*  
 \*\*\*\*\*

LIFTING LUGS

Total Weight = 1229.43 lbs = STEEL

395.32 in<sup>3</sup> ALUMINUM

$$(395.32 \text{ in}^3)(.098 \text{ */in}^3) = 38.74 \text{ lbs.}$$

TOTAL WEIGHT OF STRUCTURE

1229.43 lbs

38.74 lbs

1268.2 lbs.

WEIGHT OF PUMPS & AIR CIRCULATORS

SAY 50 lbs / PANEL x 12 PANELS = 600 lbs.

WEIGHT OF LIGHT FIXTURES

SAY 6 PANELS @ 20 lbs/PANEL = 120 lbs.

$$\begin{array}{r} \text{SUBTOTAL} = 1268. \text{ lbs} \\ 600 \text{ lbs} \\ \hline 120 \text{ lbs.} \\ \hline 1988 \text{ lbs.} \end{array}$$

SAY 2500 lbs TOTAL WEIGHT OF HAM CLNRROOM.

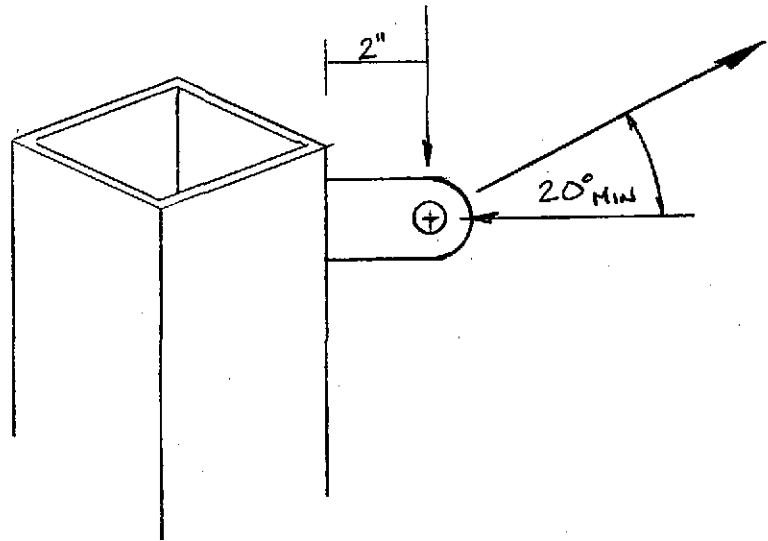
22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS





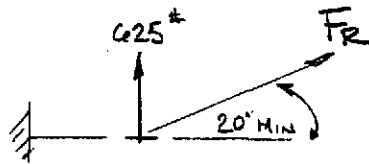
EVALUATE LUGS.

LUGS ARE USED FOR LIFTING HAM CLEARROOM  
 • SINGLE HOOK USED TO



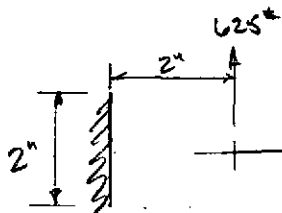
DEADWEIGHT OF HAM CLEARROOM  $\approx$  2500 lbs

$$\frac{2500 \text{ lbs}}{4 \text{ Lugs}} = 625 \text{ lbs/LUG}$$



RESULTANT FORCE = 1827 lbs.  
 w/ 20° MIN OFFSET

$\therefore$  WORST CONDITION PER LUG IS 1827 lbs RESULTANT FORCE



FORCES @ LUG WELD

TENSION = 1717 lbs +  $\frac{625 \text{ lbs} (2 \text{ in})}{2} = 2342 \text{ lbs.}$

SHEAR = 625 lbs

$$F_{weld} = \left[ (2342 \text{ lbs})^2 + (625 \text{ lbs})^2 \right]^{1/2} = 2424 \text{ lbs.}$$

Revision No. 0  
 Doc. No. V049-1-113  
 Page 70 of 72

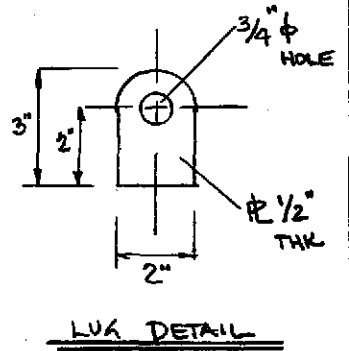
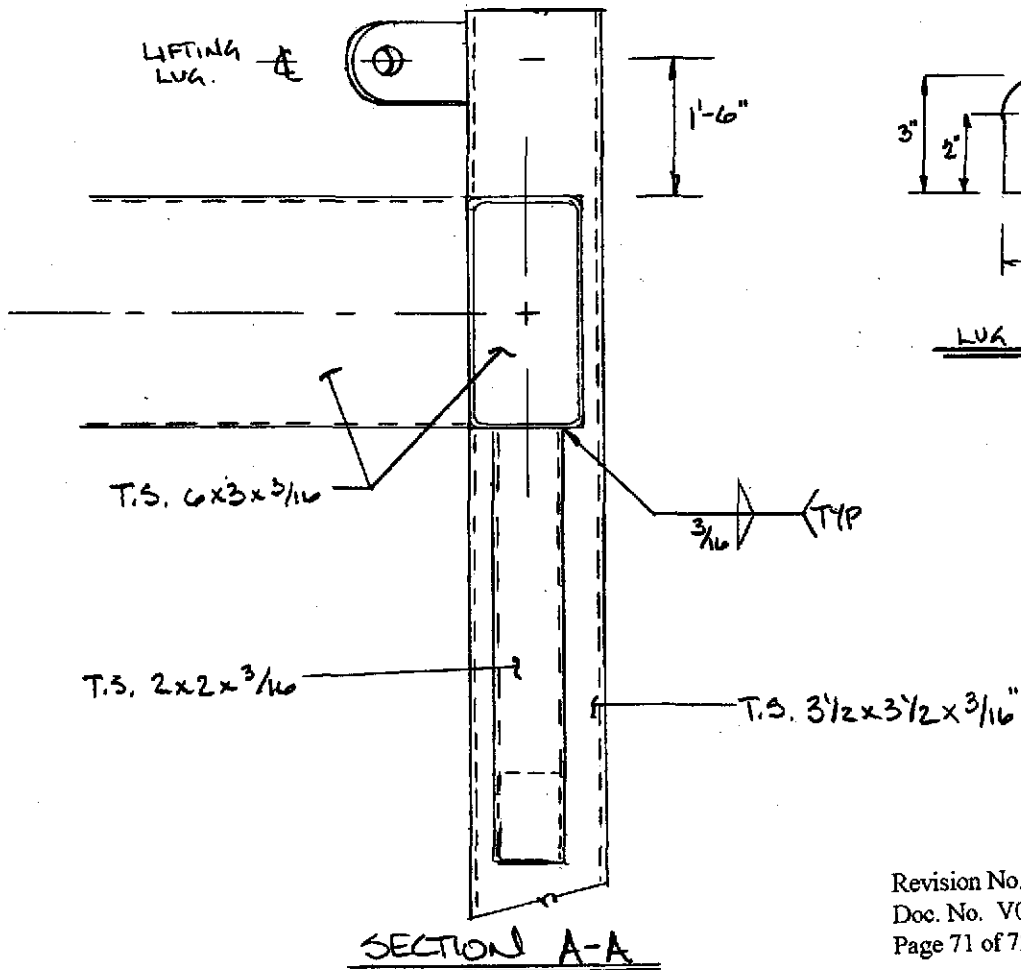
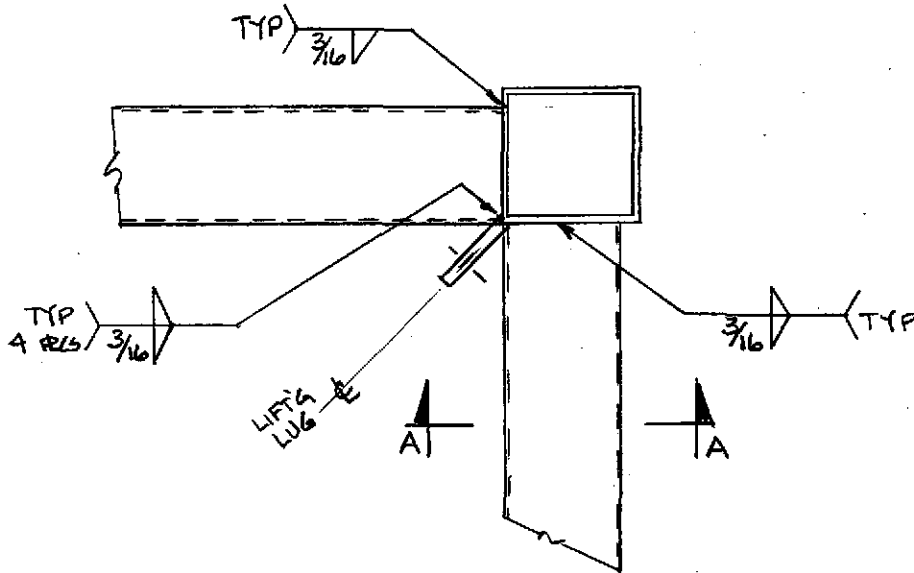
$$F_{allow} = \frac{3}{16} (2 \text{ in}) (2) (701) (18000 \text{ psi}) = 9545 \text{ lbs.} \therefore$$

2 sided  $\frac{3}{16}$  fillet weld is  
 ADEQUATE.

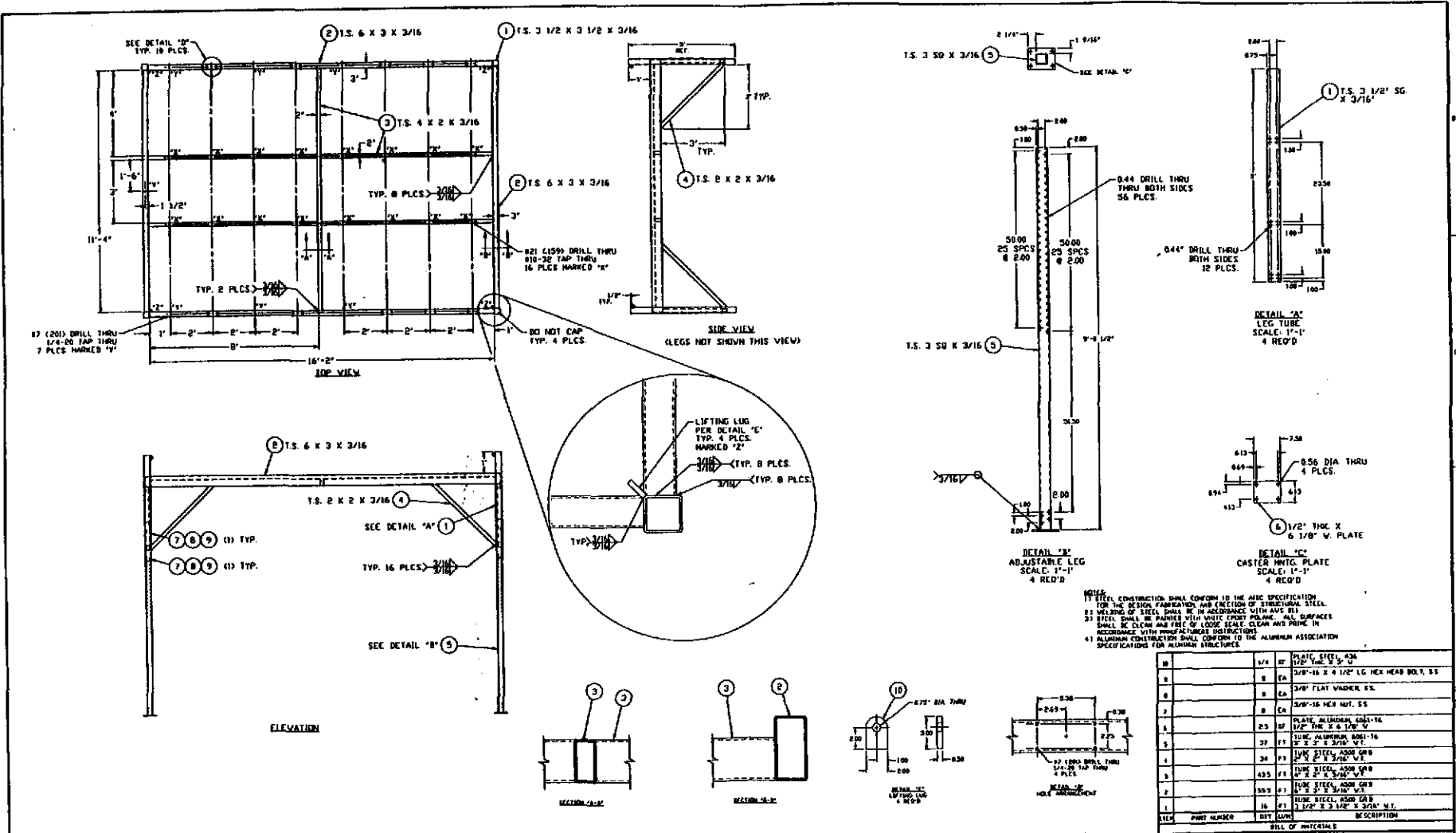
22-141 50 SHEETS  
 22-142 100 SHEETS  
 22-144 200 SHEETS



22-141 50 SHEETS  
22-142 100 SHEETS  
22-144 200 SHEETS



Revision No. 0  
Doc. No. V049-1-113  
Page 71 of 72



NOTES:  
 1) STEEL CONSTRUCTION SHALL CONFORM TO THE AISC SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL.  
 2) WELDING OF STEEL SHALL BE IN ACCORDANCE WITH AWS D11.  
 3) STEEL SHALL BE PAINTED WITH WHITE EPOXY PRIMER. ALL SURFACES SHALL BE CLEAN AND FREE OF LOOSE SCALE, CLEAN AND PRIME IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS.  
 4) ALUMINUM CONSTRUCTION SHALL CONFORM TO THE ALUMINUM ASSOCIATION SPECIFICATIONS FOR ALUMINUM STRUCTURES.

QTY	PART NUMBER	DESCRIPTION	ISSUE DESCRIPTION	CHG#	DATE	BY	REV
10	174	PLATE STEEL, 430					
8	8	3/8" X 4 1/2" LG. HEX HEAD BOLT, SS					
8	8	3/8" FLAT WASHER, SS					
2	8	3/8" X 16 HEX NUT, SS					
2	8	PLATE, ALUMINUM, 6061-T6					
1	25	1/2" THK. X 6 1/8" W.					
2	22	1/2" THK. ALUMINUM ANGLE, 6061-T6					
1	28	1/2" THK. STEEL, A304, 600					
1	28	1/2" THK. STEEL, A304, 600					
1	435	1/2" THK. STEEL, A304, 600					
2	557	1/2" THK. STEEL, A304, 600					
1	16	1/2" THK. STEEL, A304, 600					
1	16	1/2" THK. STEEL, A304, 600					
1	16	1/2" THK. STEEL, A304, 600					

**DESCRIPTIONS AND COMMENTS:**

DWG. NO.	DESCRIPTION	DWG. NO.	DESCRIPTION

**UNLESS OTHERWISE SPECIFIED**

WORKMANSHIP SHALL BE IN ACCORDANCE WITH THE FOLLOWING:

1. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

2. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

3. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

4. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

5. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

6. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

7. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

8. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

9. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

10. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

11. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

12. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

13. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

14. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

15. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

16. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

17. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

18. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

19. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

20. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

21. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

22. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

23. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

24. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

25. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

26. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

27. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

28. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

29. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

30. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

31. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

32. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

33. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

34. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

35. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

36. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

37. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

38. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

39. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

40. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

41. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

42. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

43. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

44. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

45. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

46. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

47. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

48. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

49. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

50. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

51. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

52. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

53. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

54. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

55. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

56. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

57. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

58. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

59. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

60. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

61. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

62. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

63. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

64. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

65. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

66. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

67. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

68. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

69. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

70. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

71. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

72. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

73. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

74. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

75. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

76. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

77. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

78. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

79. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

80. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

81. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

82. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

83. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

84. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

85. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

86. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

87. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

88. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

89. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

90. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

91. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

92. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

93. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

94. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

95. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

96. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

97. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

98. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

99. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

100. ALL DIMENSIONS SHALL BE TO UNLESS OTHERWISE SPECIFIED.

Revision No. 0  
 Doc. No. V049-1-113  
 Page 72 of 72