

Mechanical losses associated with the technique of silicate bonding fused silica to fused silica

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GEO 600 - Specifications —

main suspension systems.

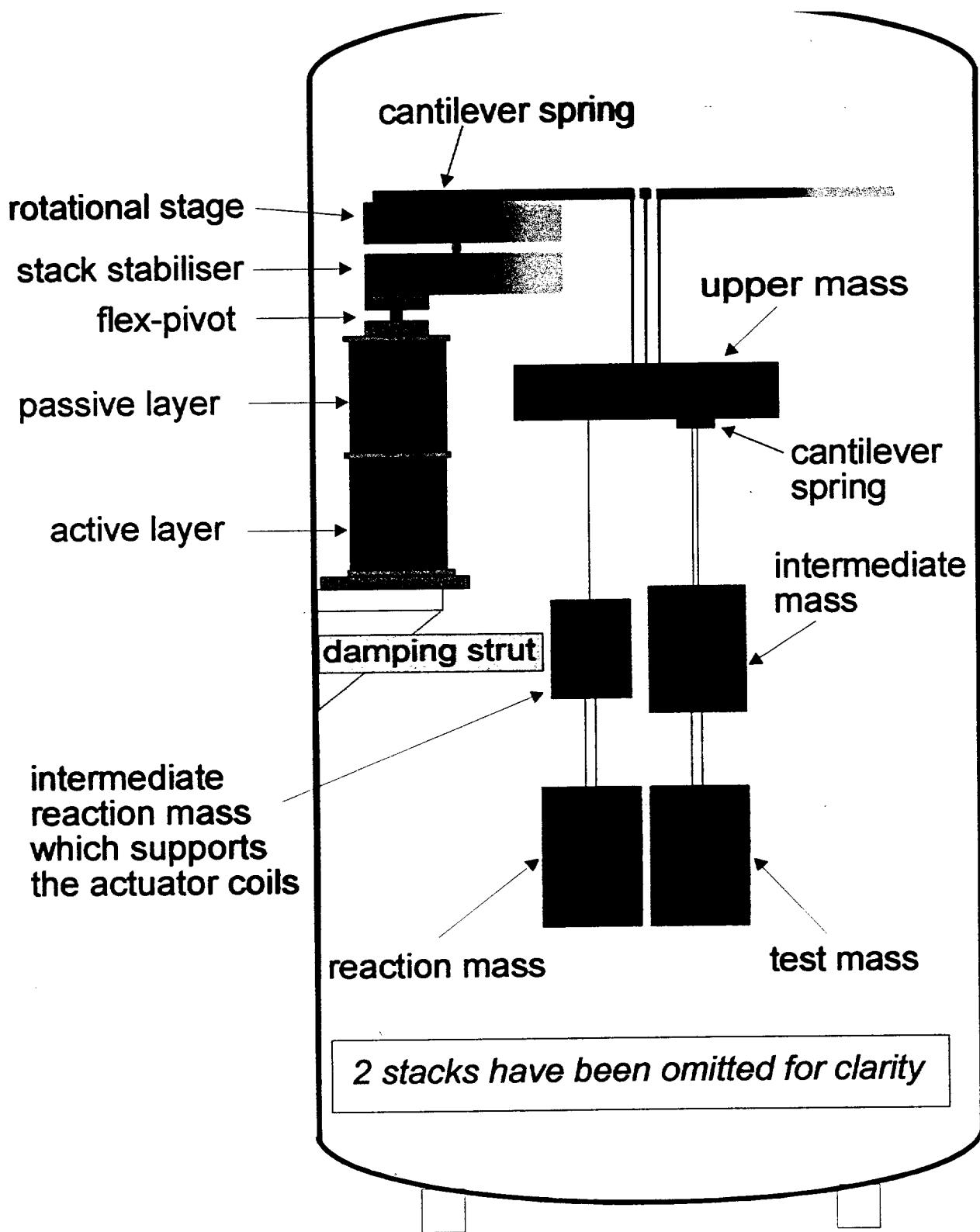
- Seismic Isolation Factors $\boxed{\text{@ } 50\text{Hz}}$

Vertical: $\sim 3 \times 10^6$ [assuming 0.1% cross-coupling factor]

Horizontal: $\sim 6 \times 10^9$

- Q pendulum $> 2 \times 10^7$

$\text{Q}_{\text{internal, test masses}} \sim 5 \times 10^6$



Schematic of test mass suspension
(view perpendicular to optic axis)

Fused silica developments at Glasgow

- Working towards construction of all-fused silica pendulums: 14kg silica masses on fused silica fibres

Measurements show:

- Material Q of suspension fibres:

$$Q_{\text{mat}} \sim 10^6$$

- Pendulum Q of 100g all fused silica (welded) pendulum:

$$Q_{\text{pend}} \sim 9 \times 10^7$$

(for 1.9kg mass: $Q_{\text{pend}} \sim 1.4 \times 10^7$: with Univ. Perugia, VIRGO)

- Violin Q of fused silica fibres:

$$Q_{\text{violin}} \sim 4 \times 10^6$$

All good enough for GEO 600 requirements - ($7 \times 10^{-20} \text{ m}/\sqrt{\text{Hz}}$ @ 60Hz)

need to continue work on scaling these to larger pendulums

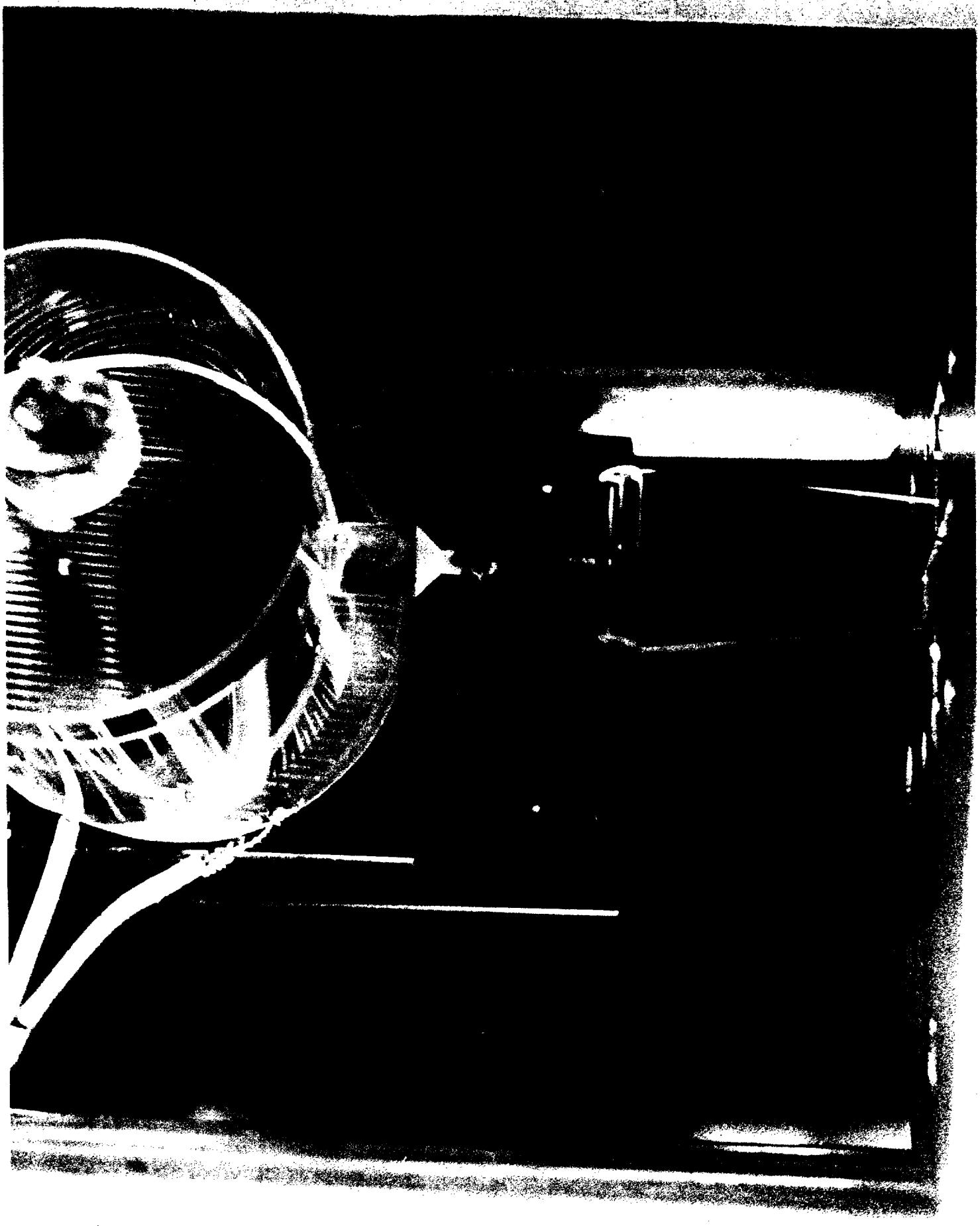
Need a method of jointing fused silica fibres to fused silica test mass which is:

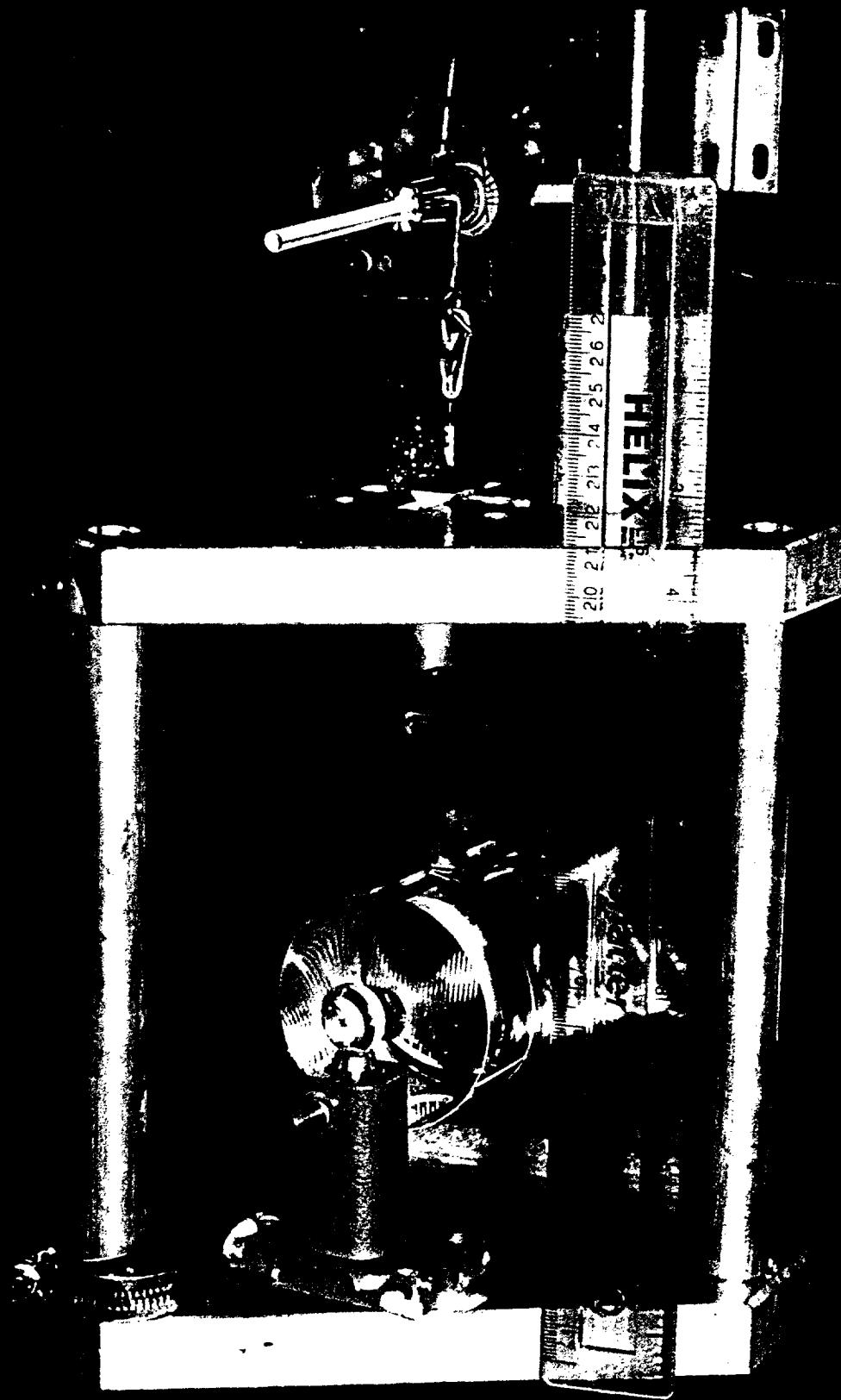
- mechanically strong
- of very low mechanical loss

→ investigate technique of Silicate Bonding

Developed by Jason Gwo at Stanford University for use in Gravity Probe B experiment.

GEO collaborating with GALILEO project on evaluation of this technique for use in Advanced gravitational wave detectors.





RESULTS

Measured Q values for fundamental longitudinal modes of:

(a) CONTROL MASS

$$(1.47 \pm 0.02) \times 10^6$$

(b) MASS + KOH BONDED ATTACHMENT

$$(1.40 \pm 0.02) \times 10^6$$

Recall: At resonant angular frequency ω_0 :

$$\phi(\omega_0) = \frac{1}{Q}$$

Then Assuming all additional loss in measurement

(b) is due to KOH bond we can write:

$$\begin{aligned} \phi(\omega_0) &= \frac{1}{Q_{\text{KOH bonded mass}}} - \frac{1}{Q_{\text{control mass}}} \\ \text{loss due to bond} & \end{aligned}$$

$$= (3 \pm 1) \times 10^{-8}$$

$$R \leq 4 \times 10^{-8} \quad (\text{cf } 3 \times 10^{-3})$$

→ Suggests no significant loss introduced by placing bond under stress

(nb: wire breakaway conditions different in (a) and (b) above)

CONCLUSIONS

Scale results to find expected loss resulting from area of KOH bond needed to support a kg GEO 600 test mass on fused silica fibres.

Bond area = $\times 5$ smaller than used here

$$\Rightarrow \text{Expect loss} : \frac{4 \times 10^{-3}}{5} = 8 \times 10^{-9}$$

Test mass = $\times 32$ larger than used here

$$\Rightarrow \text{Expect loss} : \frac{8 \times 10^{-9}}{32} = \underline{\underline{2.5 \times 10^{-10}}}$$

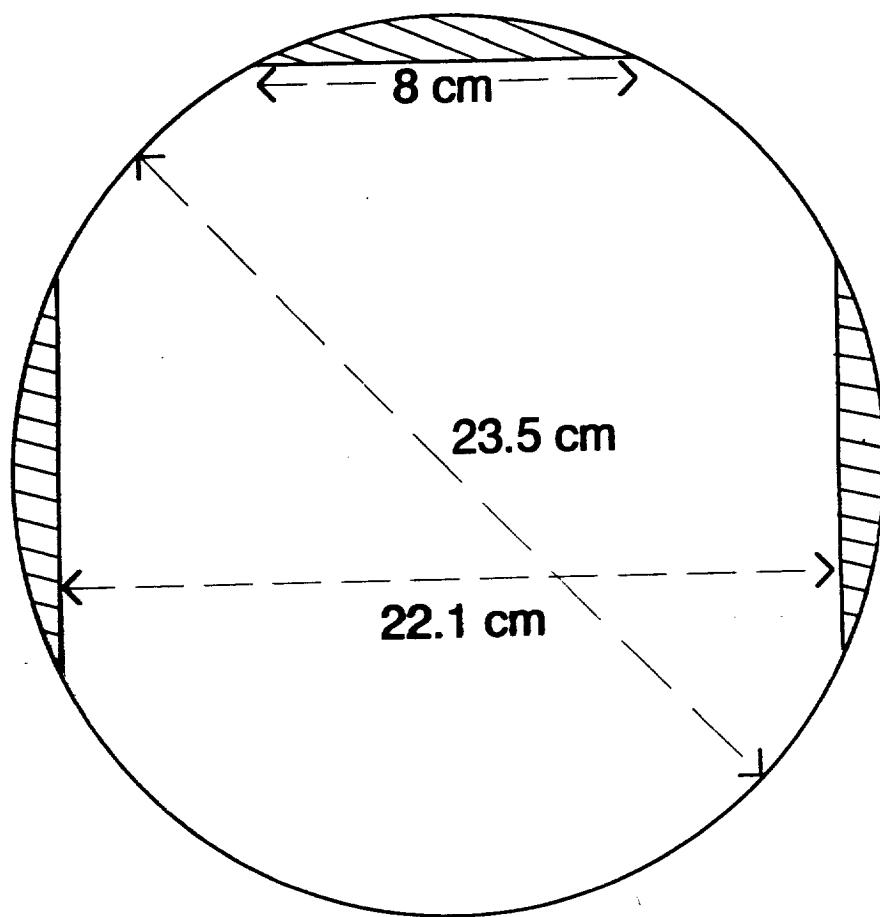
i.e.: Negligible & internal loss of fused silica test mass

\Rightarrow KOH bonding looks like an excellent method of producing low loss fused silica / fused silica joints.

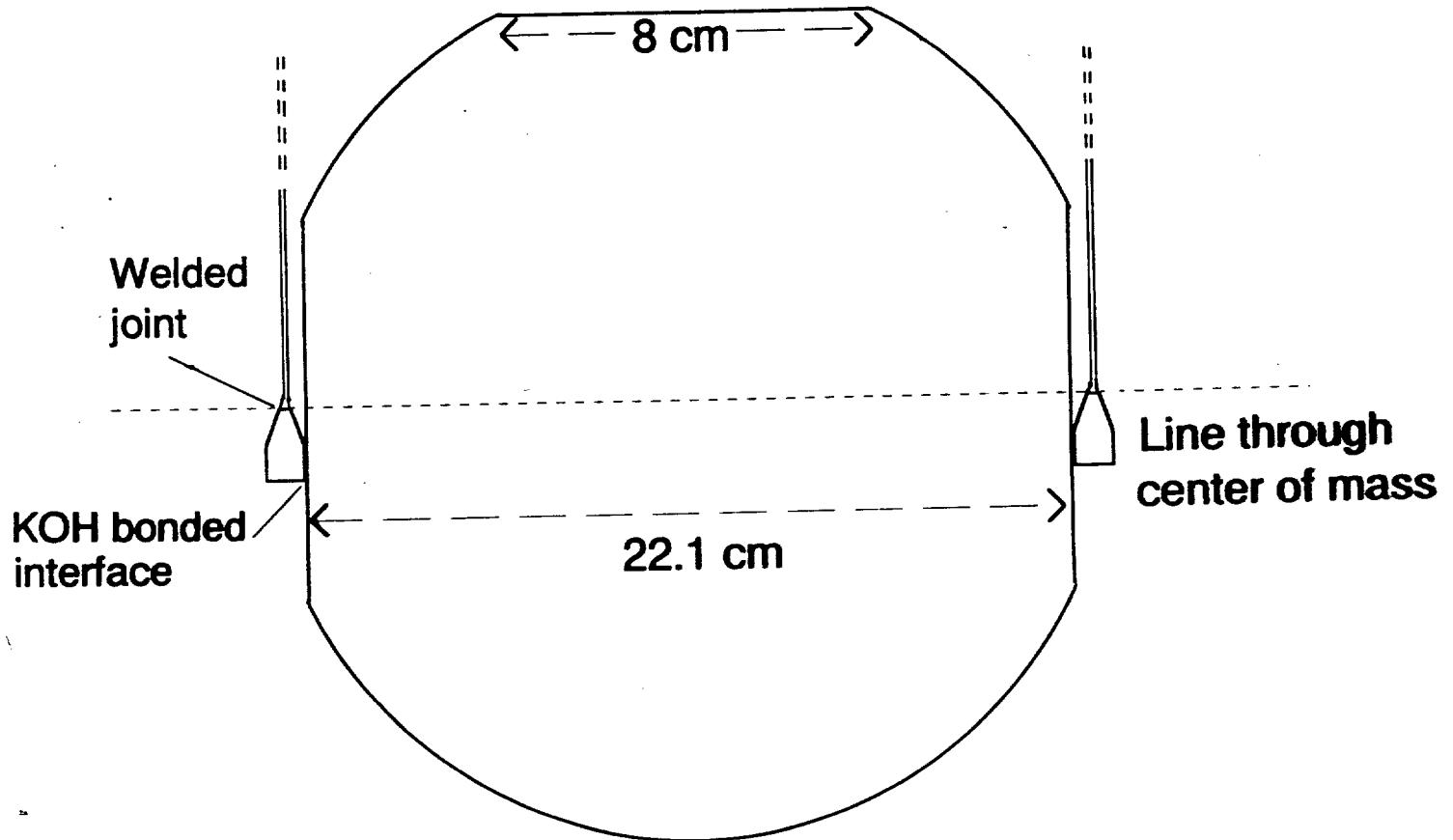
+ has potential to joint a number of ultra low loss materials i.e. sapphire and silicon (see J. Gwo, R. Route, Stanford)

View of prototype GEO 600 test mass showing front face

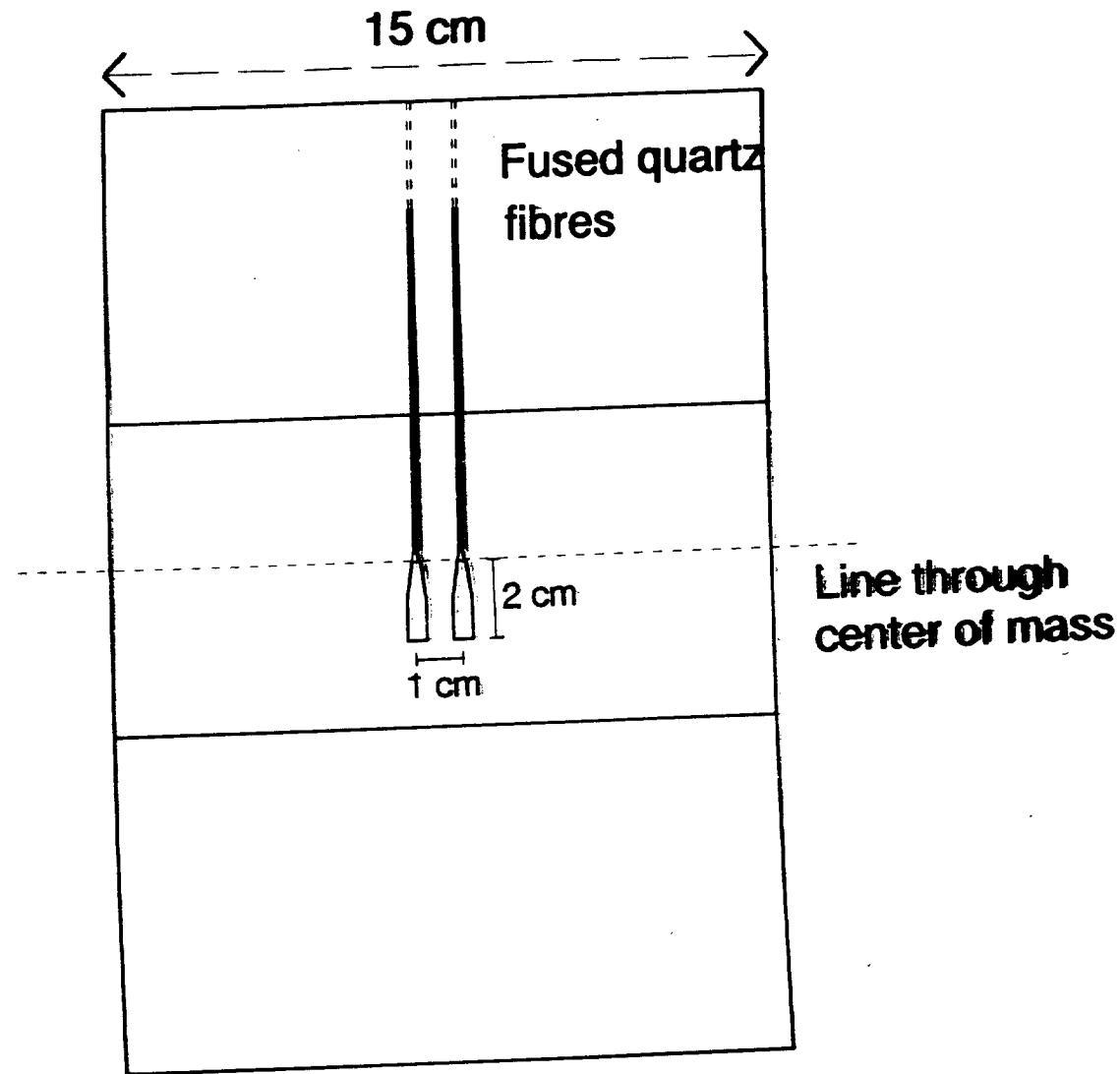
Shaded areas removed



**View of prototype GEO 600 test mass showing front face
and silicate bonded attachments**

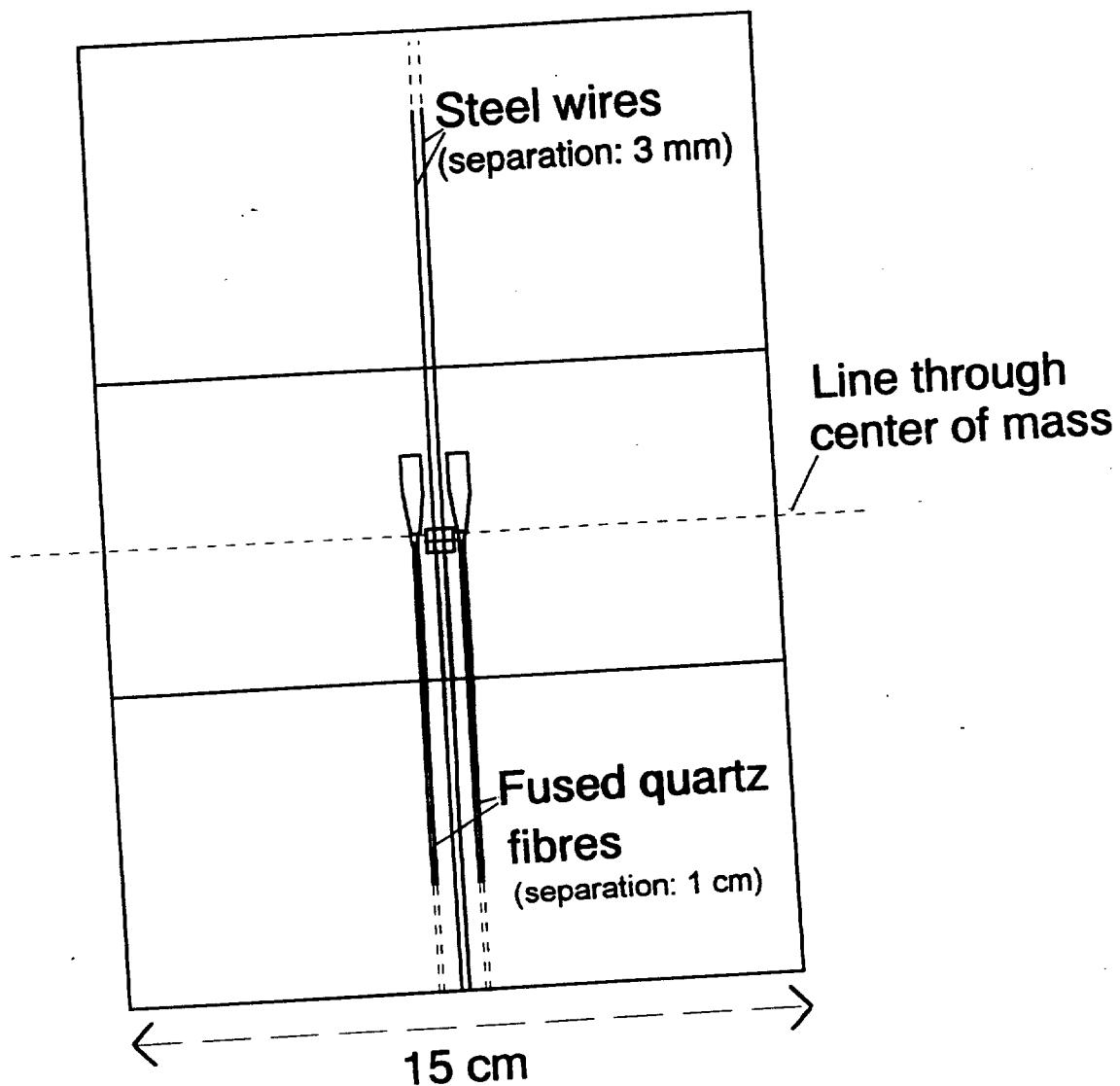


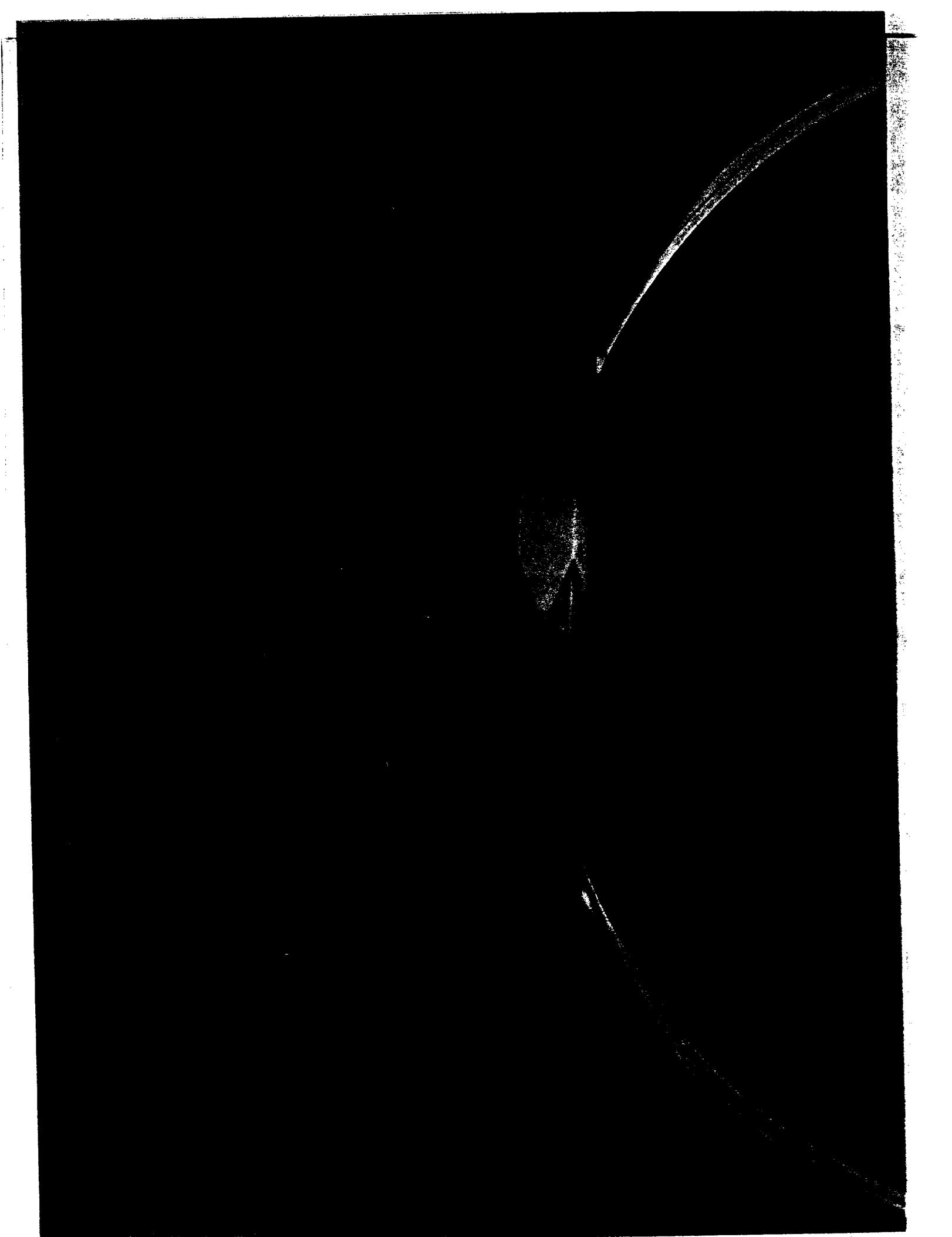
Side view of prototype GEO 600 test mass showing side view and silicate bonded attachments

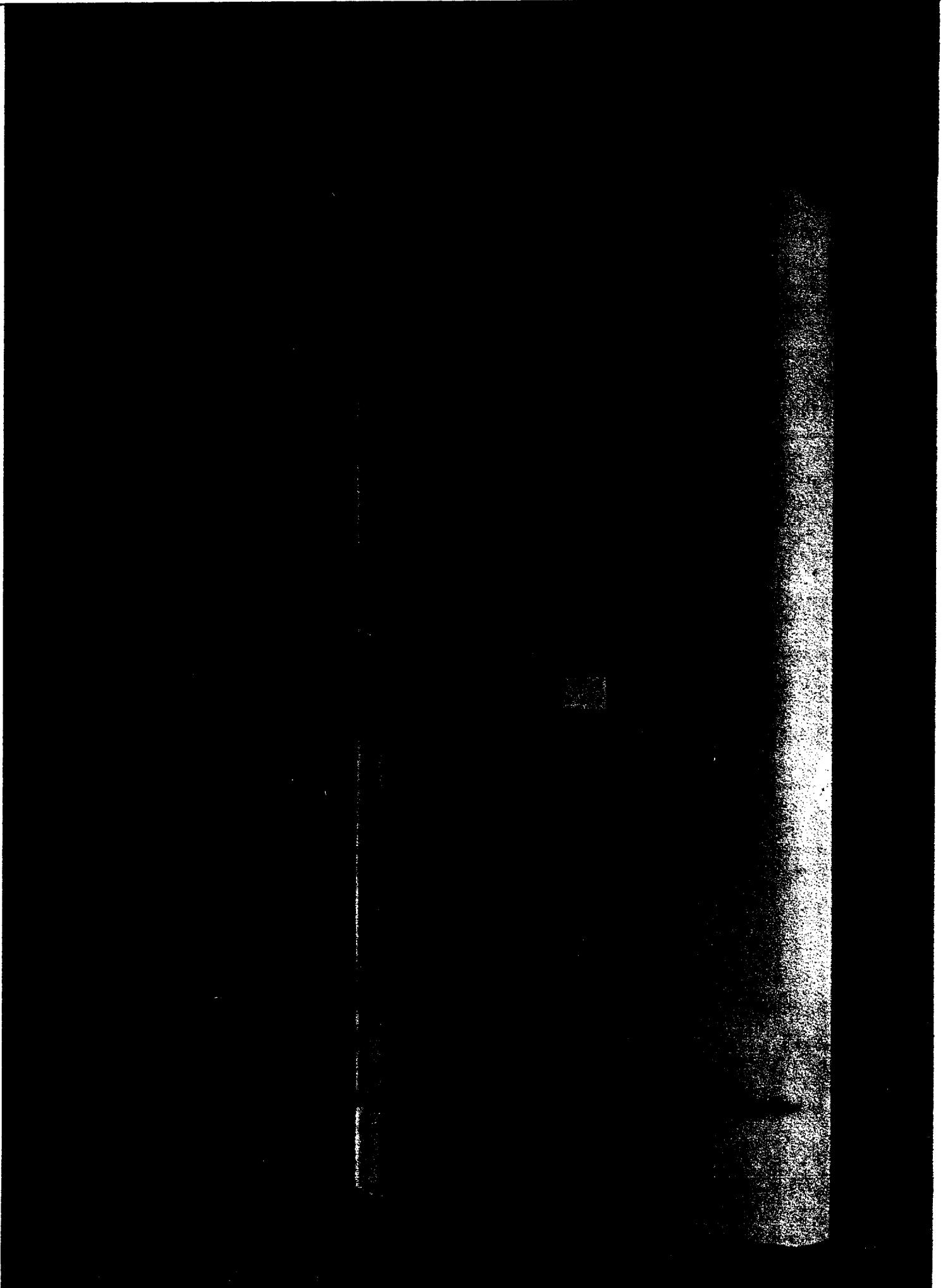


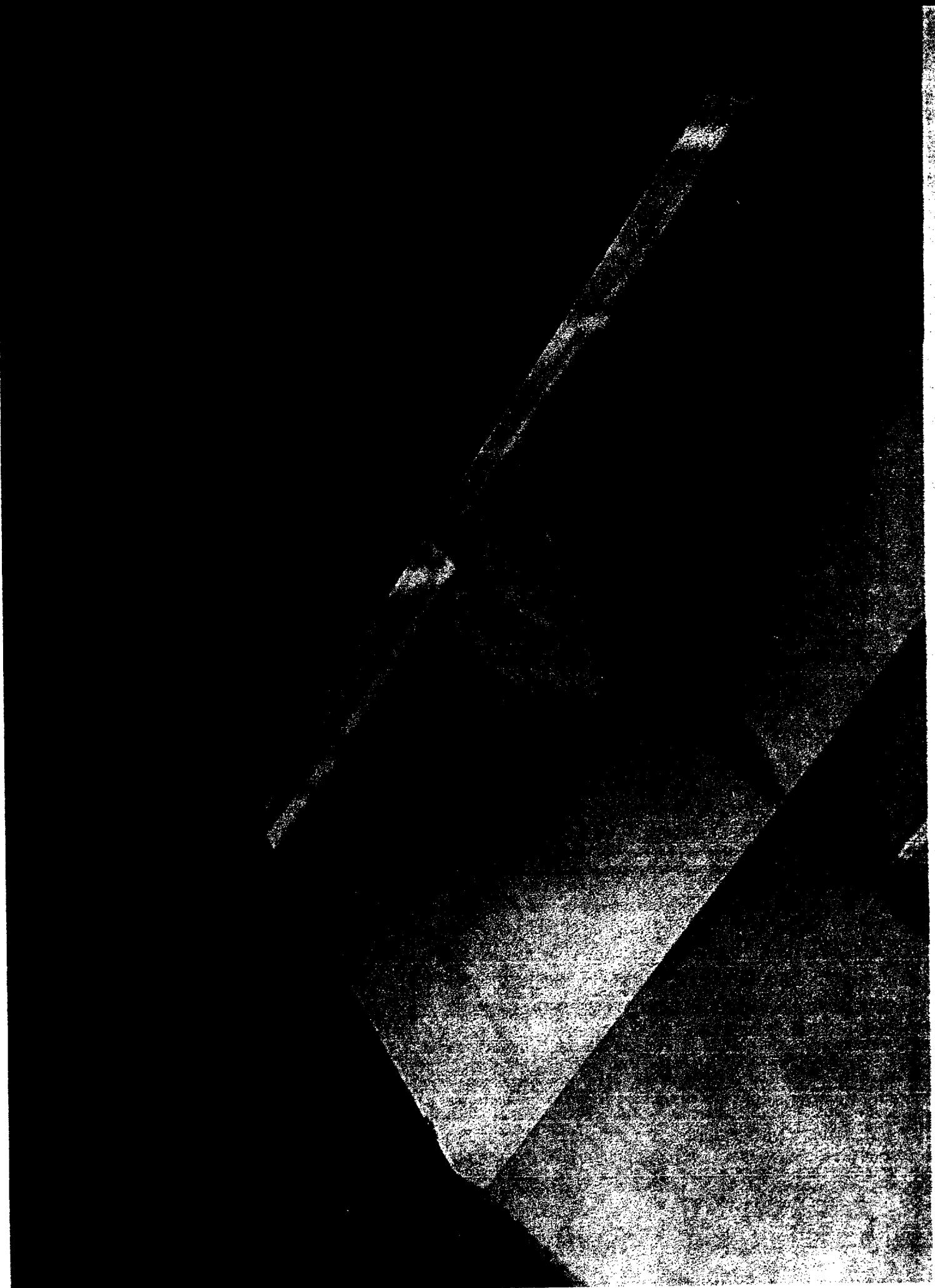
Side view of prototype GEO 600 test mass showing side view and silicate bonded attachments:

Intermediate mass



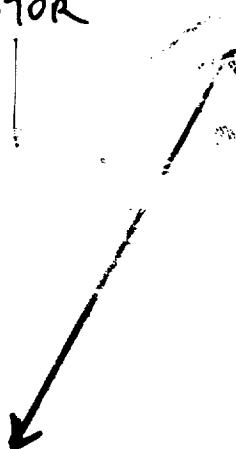






395mm

MOTOR



CANTILEVER
SPRING

CANTILEVER SPRING

— ROTATIONAL STAGE

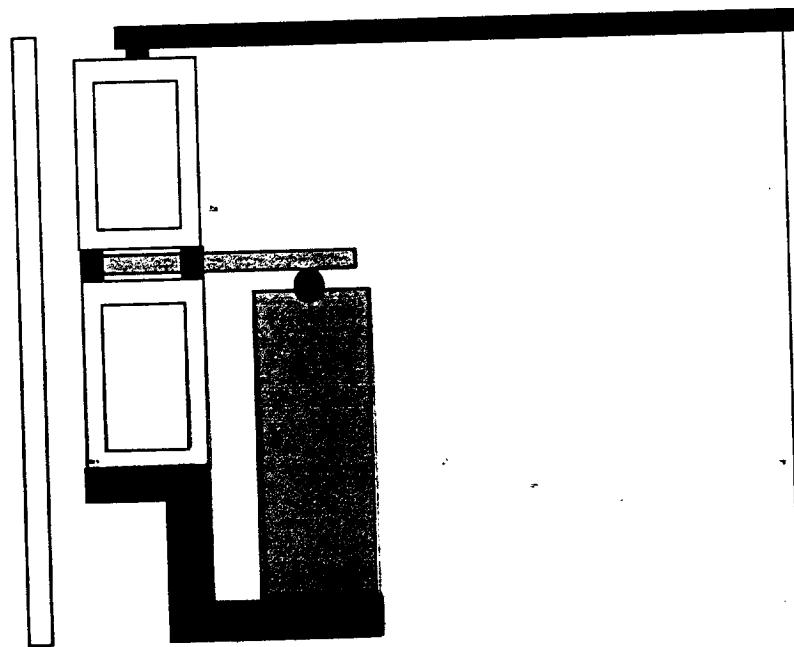
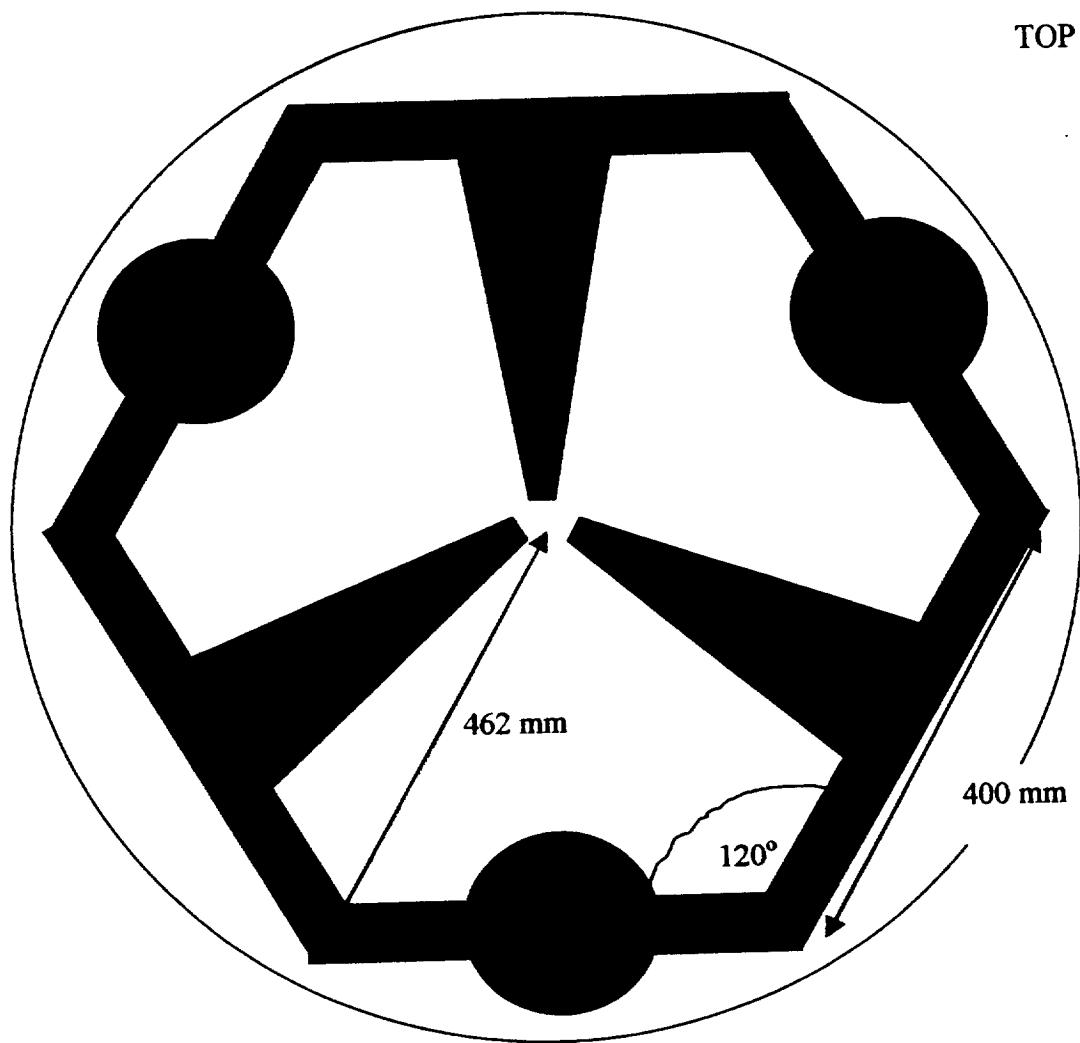
TANK
WALL



SUSPENSION
WIRE

— MOTOR

VIEWS of STACK STABILISER



OTHER ACTIVITIES

(M. PLISSI MAINLY)

- 1) MOTORISED & MANUAL ROTATION / TILT
CONTROL OF MAIN SUSPENSIONS
(TO WITHIN RANGE OF COIL-MAGNET ACTUATORS)
(\approx m rad)
- 2) INTERFACING WITH (TRIPLE) PENDULUM
(DOUBLE PENDULUM + EXTRA VERTICAL ISOLATION)

(2)

(UNCOUPLED)

RESONANCES

	ACTIVE*	PASSIVE
\leftarrow x, y	$\sim 45 \text{ Hz}$	$\sim 2 \text{ Hz}$
$\uparrow z$	$\sim 45 \text{ Hz}$	$\sim 12 \text{ Hz}$

* OPEN LOOP

AIMS OF ACTIVE STAGE.

- 1) SOME GAIN AT N SEISMIC PEAKS
($\sim 10 \text{ dB}$) ($0.1 \sim 0.3 \text{ Hz}$)
- 2) SOME GAIN (AT $\approx 12 \text{ Hz}$ ETZ.) TO
REDUCE TEST MASS VELOCITY AT
SYSTEM RESONANCES. ($\approx 1 \text{ Hz}$ TO 12 Hz)
- 3) GAIN AT $25 \sim 250 \text{ Hz}$ FOR IMPROVED
SENSITIVITY AT $50 \text{ Hz} \sim 100 \text{ Hz}$ (UP CONVERSION?)
- 4) INPUT FOR 1 Hz HORIZONTAL GEOPHONES
FOR IMPROVED ISOLATION AT $\sim 0.1 \rightarrow 0.5 \text{ Hz}$
($+10 \text{ dB}$)

GEO 600 MAIN SUSPENSION

K STRAN

12/3/98

①

ISOLATION STACKS

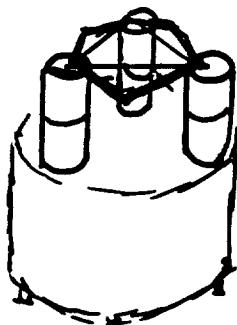
+ M. PLISSI + C. TORRIE

3 LEGS / TANK

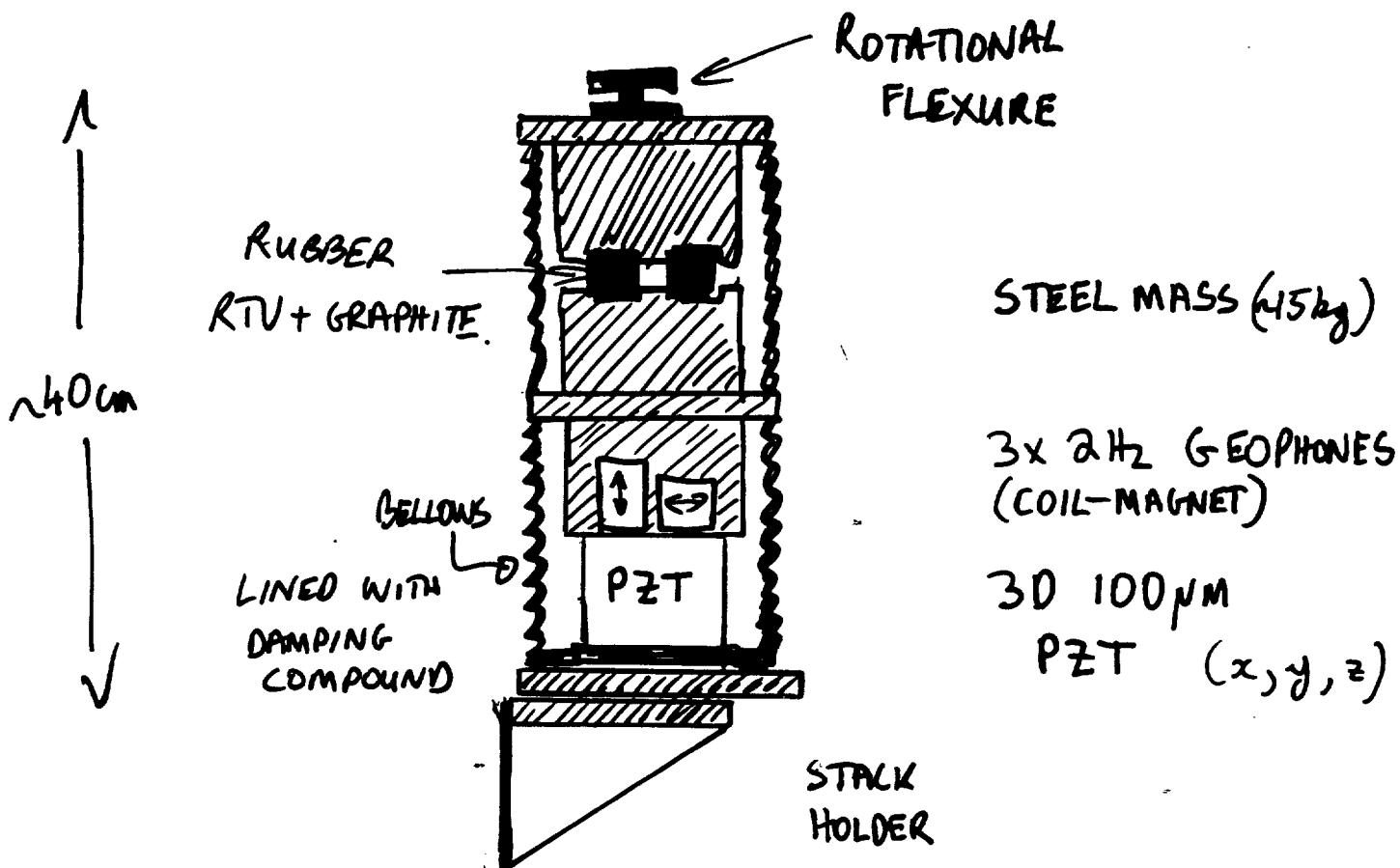
ACTIVE + PASSIVE

PZT
+
GEOPHONE

RTV
RUBBER
(+ DAMPING)



< 18 cm >



SKECH OF STACK LEG.

Note 1, Linda Turner, 04/20/98 05:16:34 PM
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