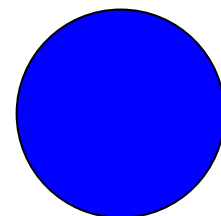


# Length Sensing and Control of AdLIGO

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ISC session, LSC at LSU  
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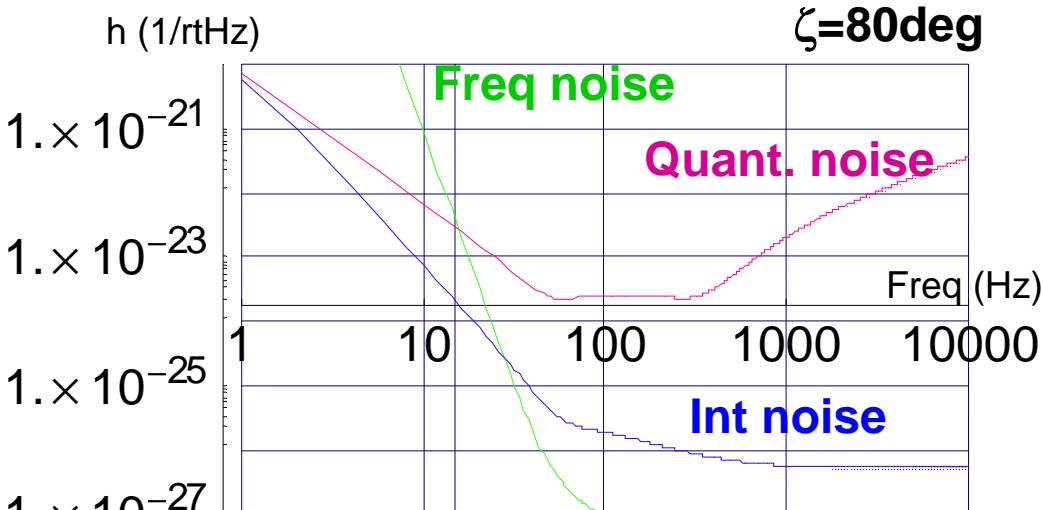
K. Somiya

# Contents

- **Brief Review of LSC (1 page each)**
  - DC readout in RSE
  - DDM with HF/LF control scheme
  - Constraints from MC, PRC, and Asymmetry
  - Simulation software
- **Development of a calculation tool**
- **I'll show 4 candidates; let's pick one**
  - Possibility of “flexible detuning”
  - Comparison

# ***Brief Review of LSC***

# DC readout in RSE



Readout quadrature is determined by a ratio of contrast defect due to loss imbalance and offset light. (~30ppm)

The better one for binaries ( $\zeta \sim 90\text{deg}$ ) requires more offset light.

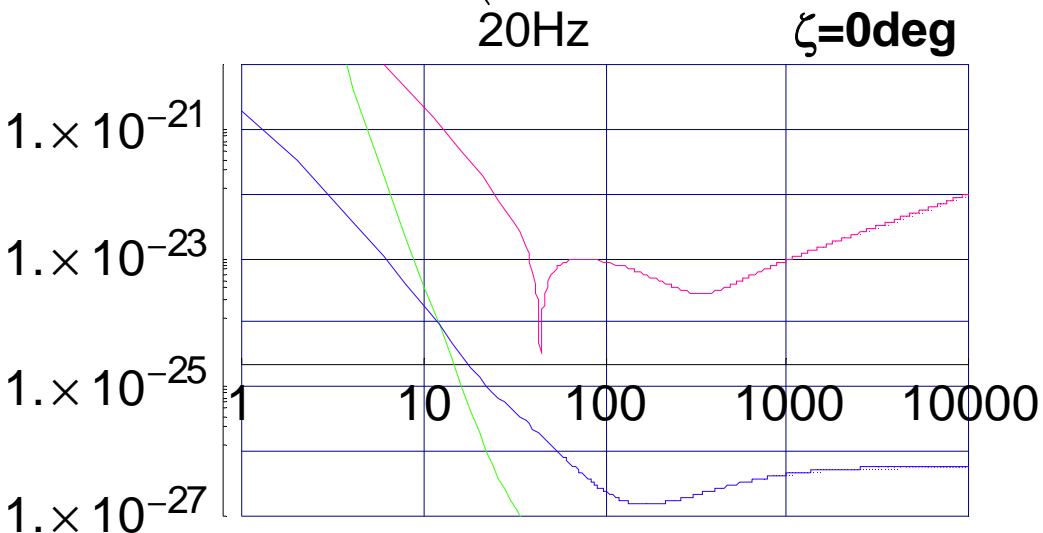
→ Laser noise becomes big.



Upper limit will be  $\sim 80\text{deg}$ . Also PD can afford  $< 100\text{mW}$  light.

**We choose 78 deg.**

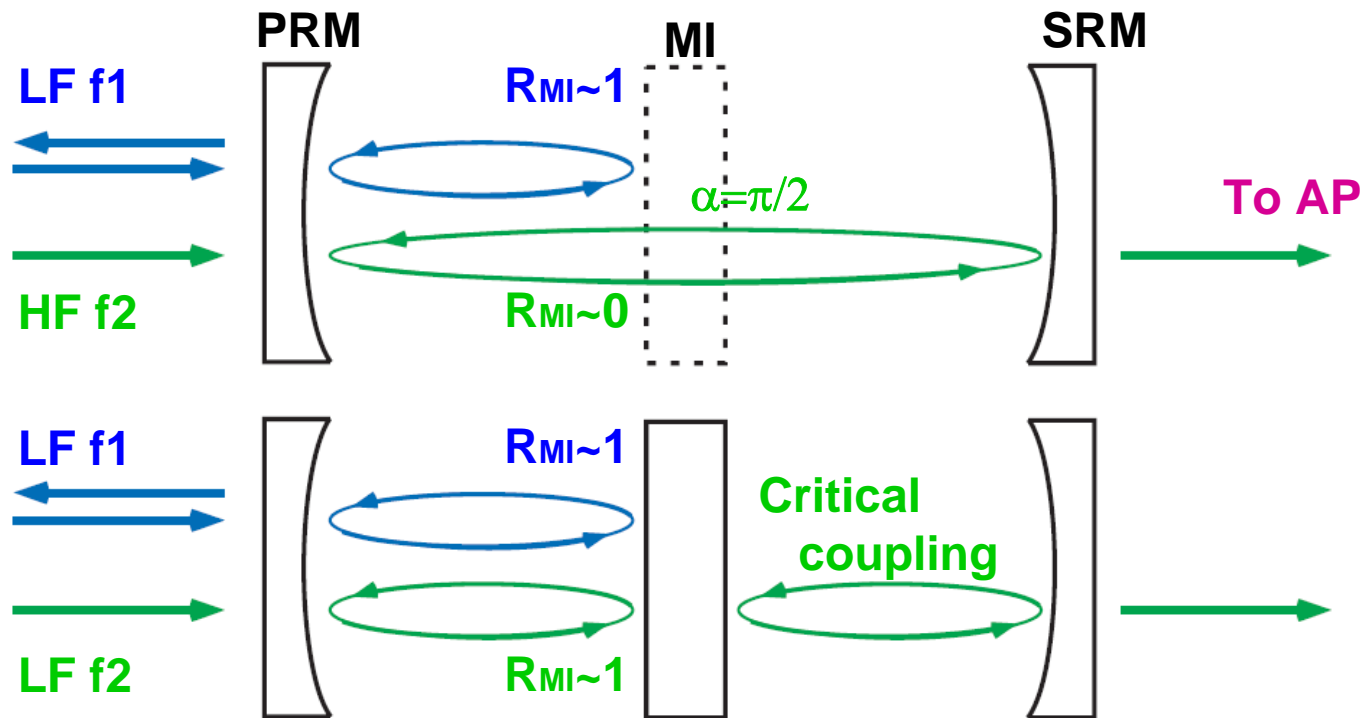
( $\sim 5.6\text{e-}12\text{m}$  offset)



# Double demodulation with HF/LF control

L- : AP-DC readout, L+ : SP-RF readout  
slp(l+), slm(l-), sls(l<sub>s</sub>) → Double demodulation

There are 2 ways of choosing 2 RF-SB frequencies.



9MHz-180MHz is HF, and 27-45MHz is LF control scheme.

# Constraints from MC and Asymmetry

- AdLIGO uses same vacuum chambers as LIGO
- FSR of MC is fixed to  $\sim 9\text{MHz}$
- Asymmetry can be extended but only up to 75cm

## HF scheme

9-180MHz ( $\Delta l=40\text{cm}$ ) requires too-high DDM freq.  
Due to  $\Delta l < 75\text{cm}$ , the lowest possible  $f_2$  is 108MHz.

## LF scheme

Required asymmetry is  $\sim 4\text{cm}$ .  
Use of common multiple of 9MHz helps to avoid harmonics problem.

Here we pick up 9-108MHz and 27-45MHz scheme.

# Simulation software

Now we must calculate noise spectra to evaluate control schemes.

Which freq-domain software should we use?

- FINESSE : High utility, RF- and DC-readout is available  
Radiation-pressure is not included (no optical spring)
- MIT code : Radiation pressure and squeezing effects are included  
RF-control is not included
- Analytical work : Most things can be calculated by Mathematica  
It won't cover everything
- Optickle : RF-control and Radiation pressure effect are included  
Squeezing is not available yet

We use both FINESSE and my Mathematica code, and combine them on Matlab.

# ***Calculation of control-loop noise*** ***~ development of tool***

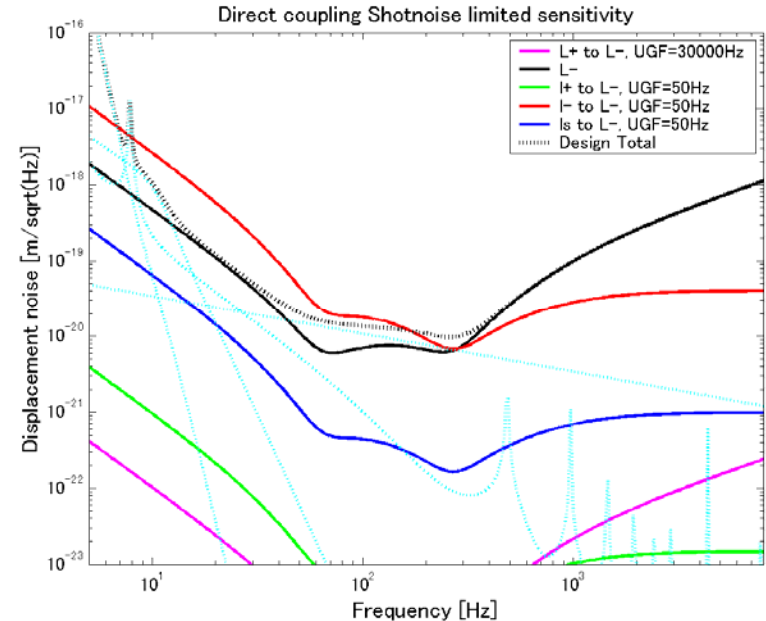


# What we used to do

## Length-sensing matrix (by FINESSE)

	L+	L-	slp	slm	sls
L+ port	1				
L- port		1		1e-3	
slp port			1		
slm port				1	
sls port					1

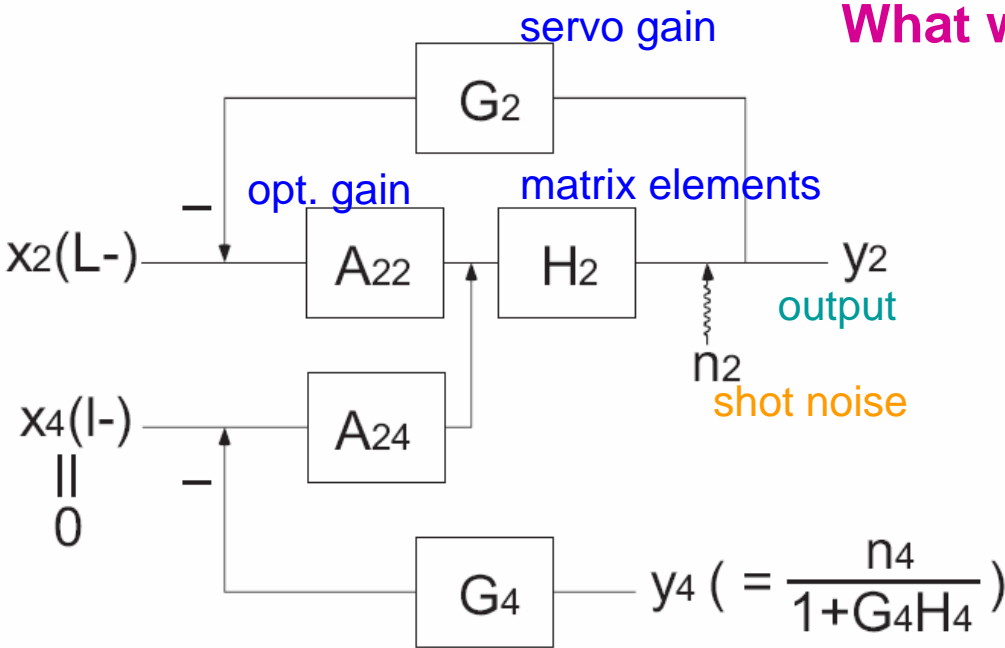
L- noise is calculated by BENCH.



- 1<sup>st</sup> order and 2<sup>nd</sup> order contributions were considered
- Degeneracy of signals did not appear in sensitivity
- Flat frequency response was assumed
- Improvement by factor of ~30 by feed-forward was assumed

**Degeneracy causes reduction of gain; should be included.**

# Block diagram expression

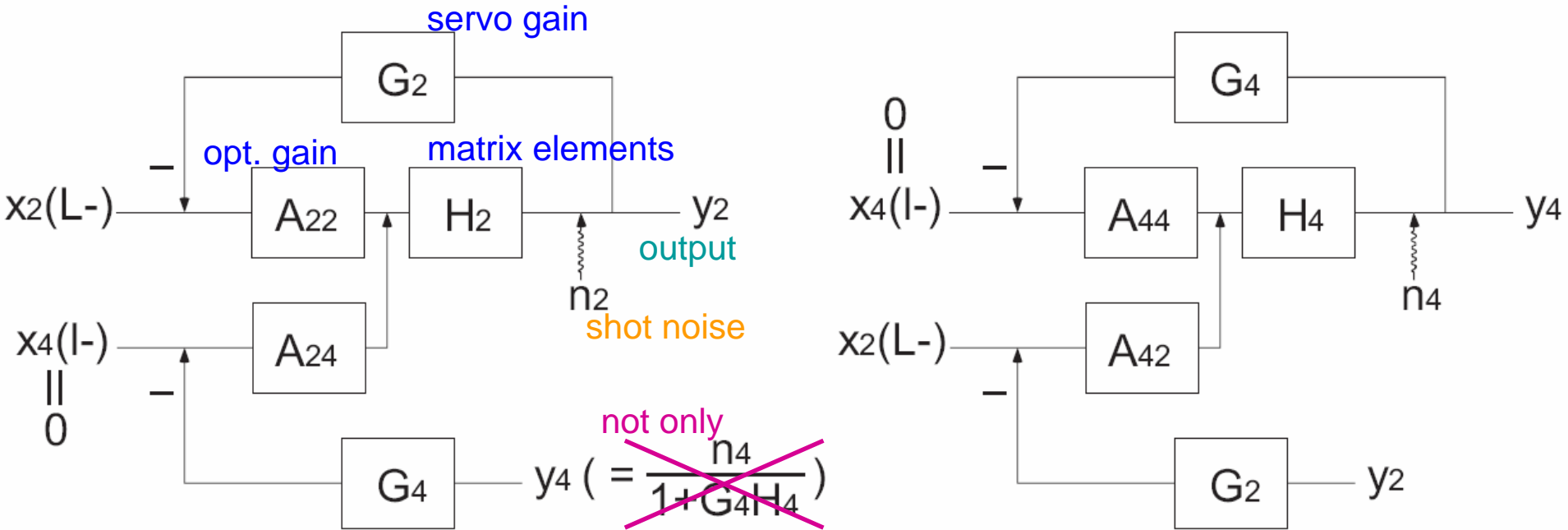


What we did can be described like this.

- Shot-noise-limited sensitivity ( $x_4=0$ )
- $n_4$  appears on  $y_2$  when  $GH > 1$
- Degeneracy does not appear

There must be a better way to express the system.

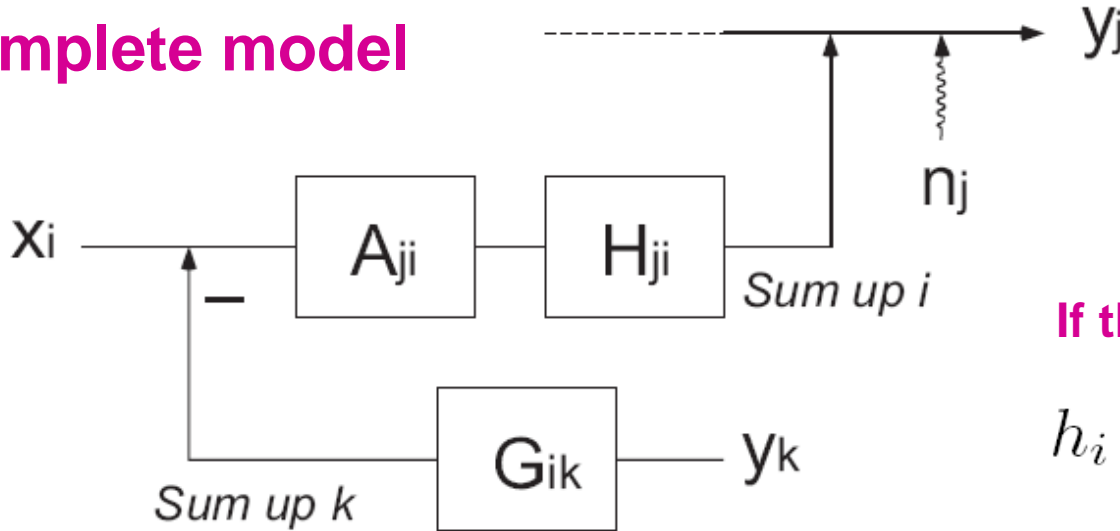
# Block diagram expression



- $y_4$  is not only  $n_4$ , even though  $x_4$  is zero
- Because  $y_4$  may include  $x_2$  (signal)
- The mixture of  $x_2$  will cause the gain reduction

# Block diagram expression

## Complete model



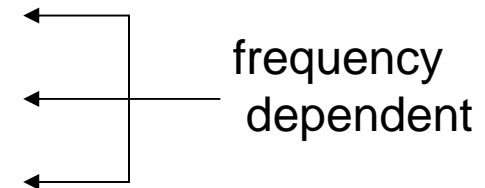
If the gains are high,

$$h_i = \sum_j (A^{-1})_{ij} n_j / H_j$$

Noise is big if  $\det[A] \sim 0$ ,  
which means degeneracy.

Now we combine tools.

- $A_{ij}$  (sensing matrix at DC) : FINESSE
- $H_{ij}$  (transfer function) : Mathematica
- $x_j$  and  $n_j$  (signal and noise) : Mathematica
- $G_{ij}$  (servo gain) : Matlab



# Frequency dependence

$H_{ij}(f)$	$L_+$	$L_-$	$\ell_+$	$\ell_-$	$\ell_s$
$L_+$	cavity pole	flat	flat	flat	flat
$L_-$	2 peaks	2 peaks	2 peaks*	2 peaks*	2 peaks*
$\ell_+$	flat	flat	flat	flat	flat
$\ell_-$	flat	flat	flat	flat	flat
$\ell_s$	flat	flat	flat	flat	flat

$G_{ij}(f)$	$L_+$	$L_-$	$\ell_+$	$\ell_-$	$\ell_s$
$L_+$	$1/f$ ; 30k	–	–**	–	–**
$L_-$	–	$1/f$ ; 200	–	Feed-forward	–
$\ell_+$	–	–	$1/f$ ; 50	–	–
$\ell_-$	–	–	–	$1/f$ ; 50	–
$\ell_s$	–	–	–	–	$1/f$ ; 50

**Unity-gain frequency**

- Only limited numbers of elements are calculated
  - ~ We need Optickle to complete all the elements
- TF from slm to L- shows 2 peaks like L- response
  - ~ It would be same for slp or sls to L-
- Feed-forward can be included
- Coupling from L+ to slp and sls via laser freq is not included

# ***Downselection of control scheme***

***~ Let's see the first two candidates***

# 9-108MHz scheme

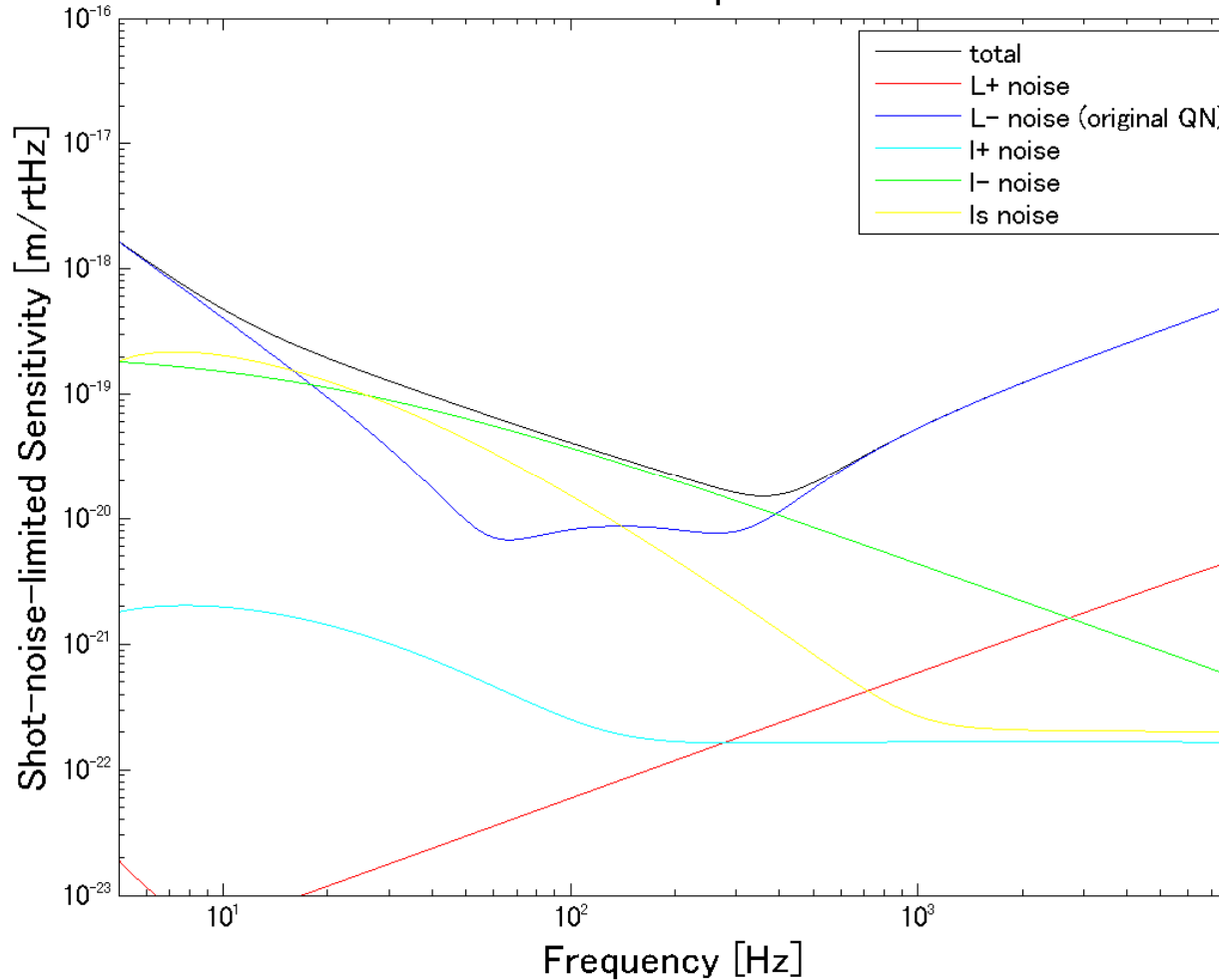
$A_{ij}$

$i \backslash j$	L+	L-	Slp	Slm	SlS	H	det/sh
SP f1	1	2.6e-3	1.1e-3	3.3e-6	2.1e-7	8.5e20	--
AP DDM	3.7e-4	1	1.1e-6	1.3e-3	1.7e-6	8.5e19	0
SP DDM	-9.1e-3	-6.2e-5	1	-0.042	0.341	1.3e17	213%
AP DDM	4.4e-3	7.2e-3	-0.310	1	-0.438	-9.2e15	69%
PO DDM	-8.6e-3	1.3e-5	0.542	-0.110	1	9.4e14	<1%

- $A[24]$  is determined by finesse of arm cavities.
- $A[43]$  and  $A[45]$  is big due to large asymmetry for f1 (75cm, 9MHz).
- SP detector noise could be reduced by a use of SSB for f2.
- AP detector noise is large also due to big asymmetry for f1.

# 9-108MHz scheme

Control-loop noise



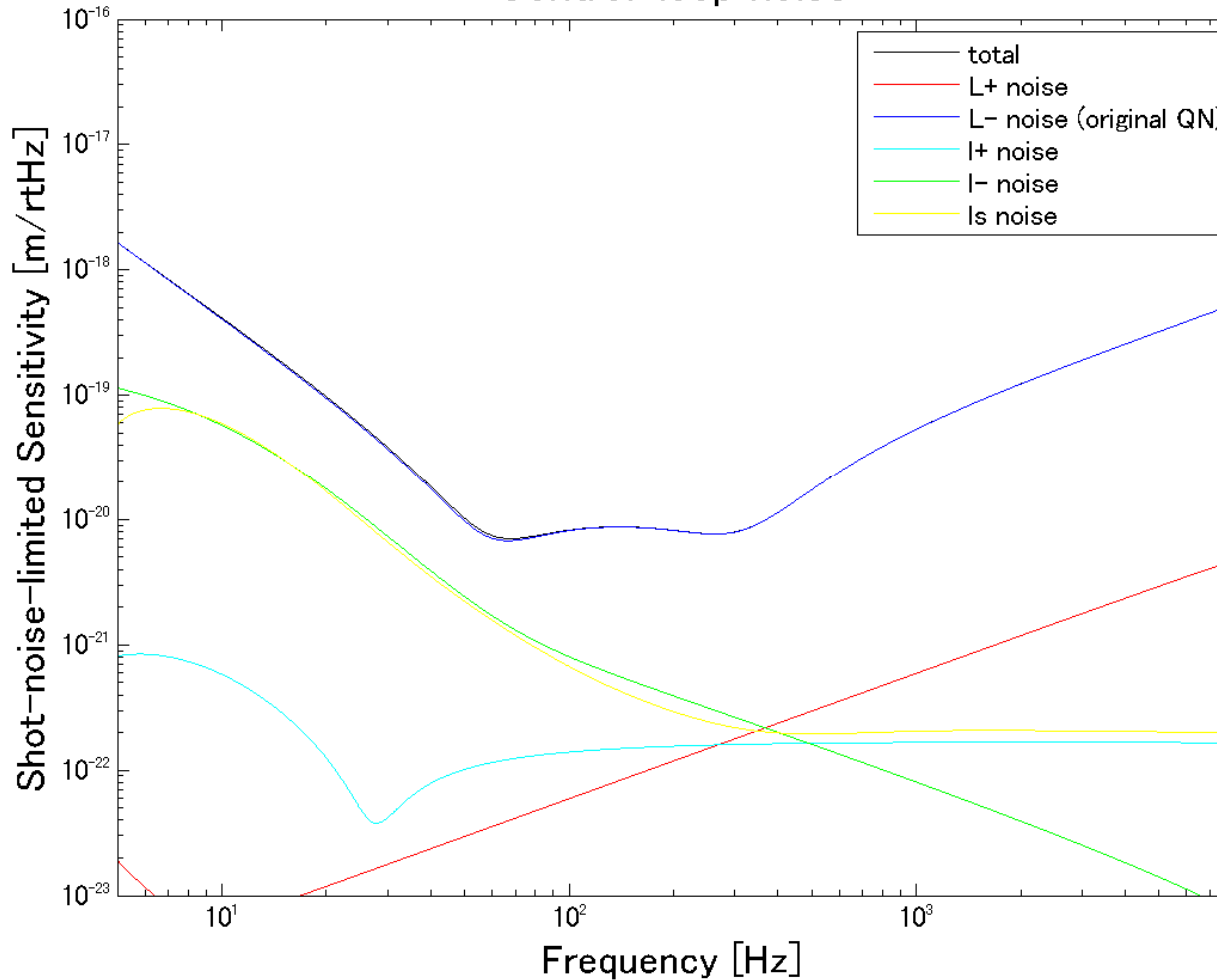
Sensitivity is limited by l- noise and ls noise.  
Let's try feed-forward.



With Feed-forward  
(1% accuracy is needed)

# 9-108MHz scheme

Control-loop noise



UGF=20Hz  
FF:1-pole LPF

Now we have a good sensitivity curve.  
But we need 1% accuracy for feed-forward gain.

# 27-45MHz scheme

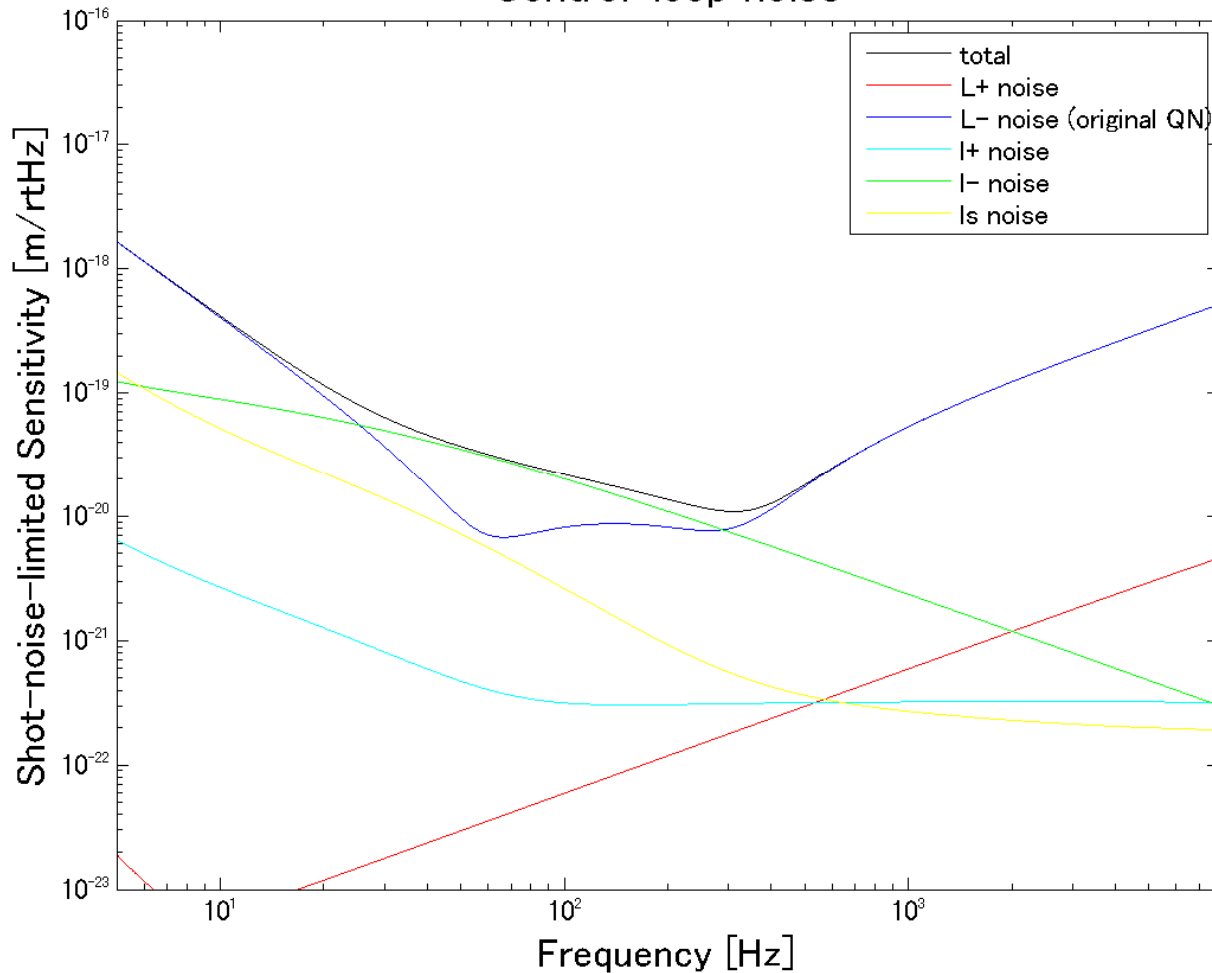
$A_{ij}$

$i \backslash j$	L+	L-	Slp	Slm	Sls	H	det/sh
SP f1	1	2.5e-3	1.1e-3	2.1e-6	9.4e-7	9.0e20	--
AP DDM	3.7e-4	1	1.1e-6	1.3e-3	1.7e-6	8.5e19	0
SP DDM	7.8e-4	1.3e-3	1	0.784	0.880	-5.9e16	165%
AP DDM	6.8e-5	1.4e-3	0.083	1	0.094	-1.0e16	3%
PO DDM	1.6e-3	2.7e-3	0.318	1.589	1	-1.0e15	1%

- Optical gains (H) are similar to those of 9-108MHz scheme.
- $A_{43}$  and  $A_{45}$  is small due to small asymmetry for f1 (4cm, 27MHz).
- SP detector noise could be reduced by a use of SSB for f2.
- AP detector noise is small also due to small asymmetry for f1.

# 27-45MHz scheme

Control-loop noise

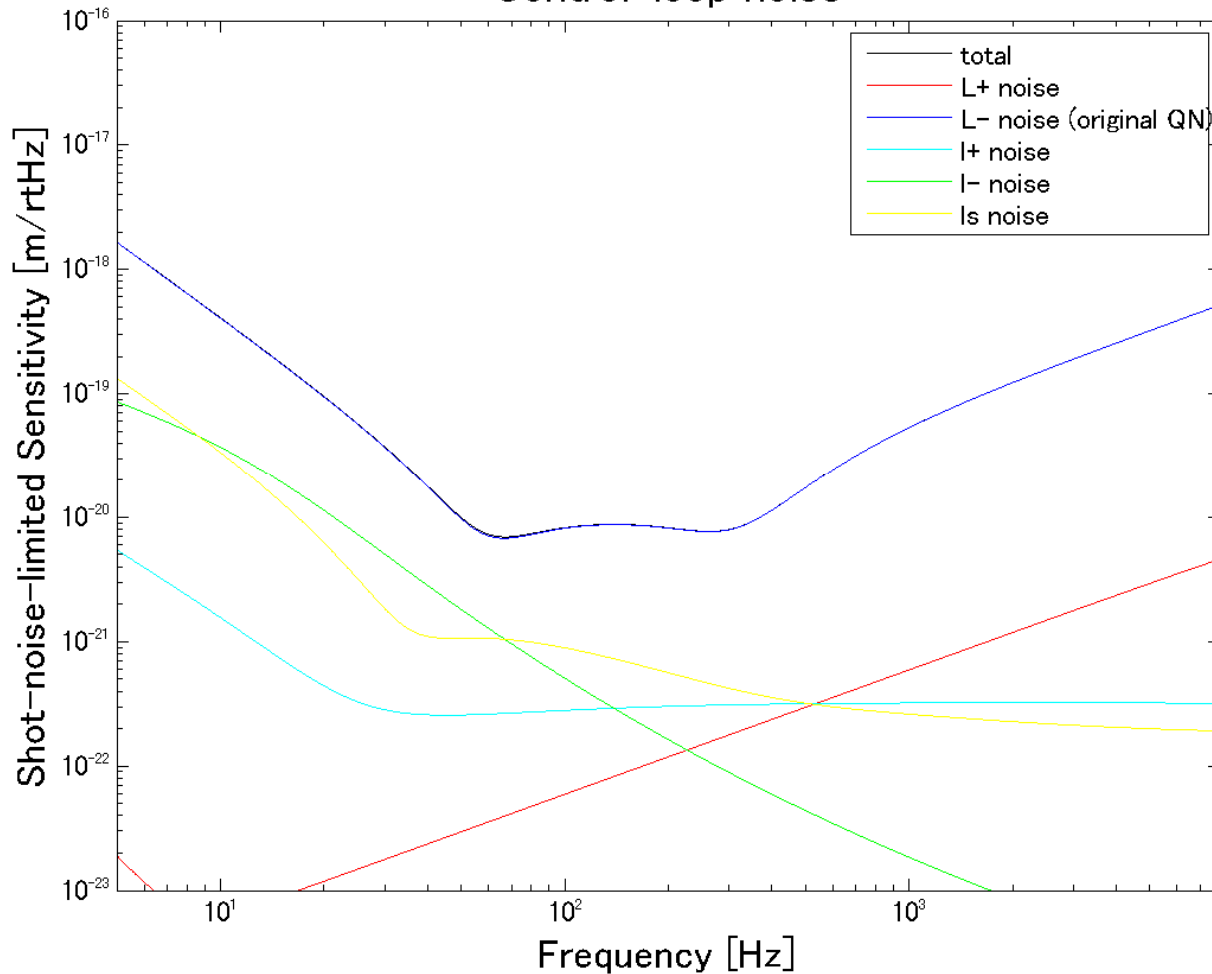


Sensitivity is limited by l- noise.  
Let's try feed-forward.

With Feed-forward  
(10% accuracy is ok)

# 27-45MHz scheme

Control-loop noise

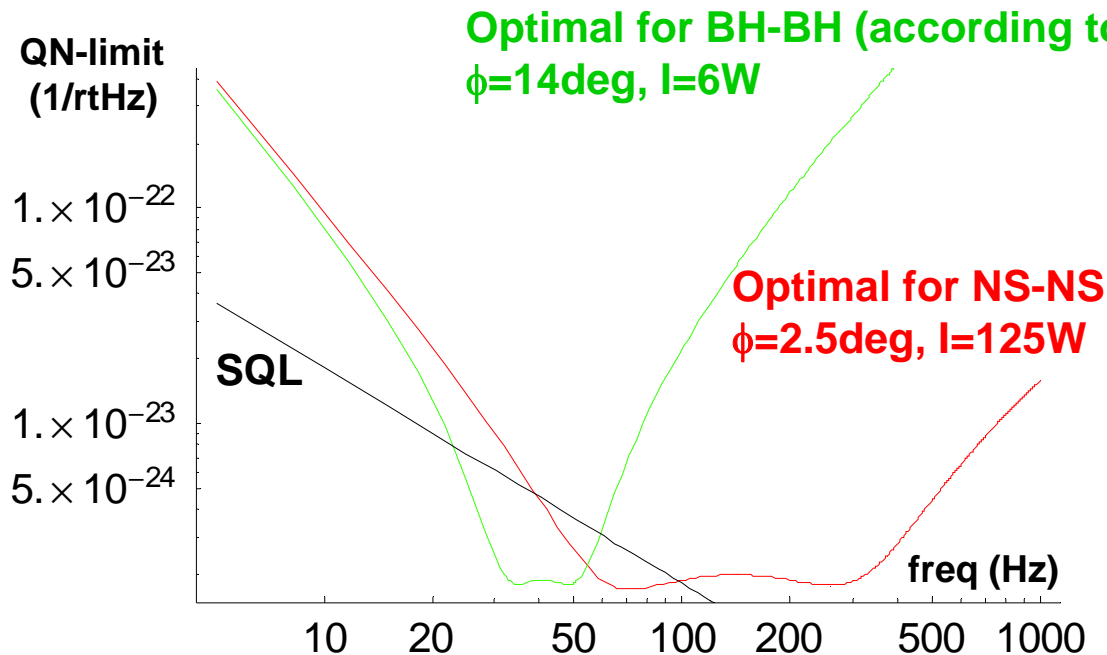


UGF=20Hz  
FF:1-pole LPF

27-45MHz scheme looks better than 9-108MHz scheme.  
Are there any other conditions that we should meet?

# Flexible detuning

- Detune phase is determined by f2-SB freq that resonates in SRC.
- So, it is fixed, so far to the optimal one for NS-NS binaries.
- But we may want to change it to the optimal for BH-BH.
- Or we may use lower power at the beginning; optimal phase changes.

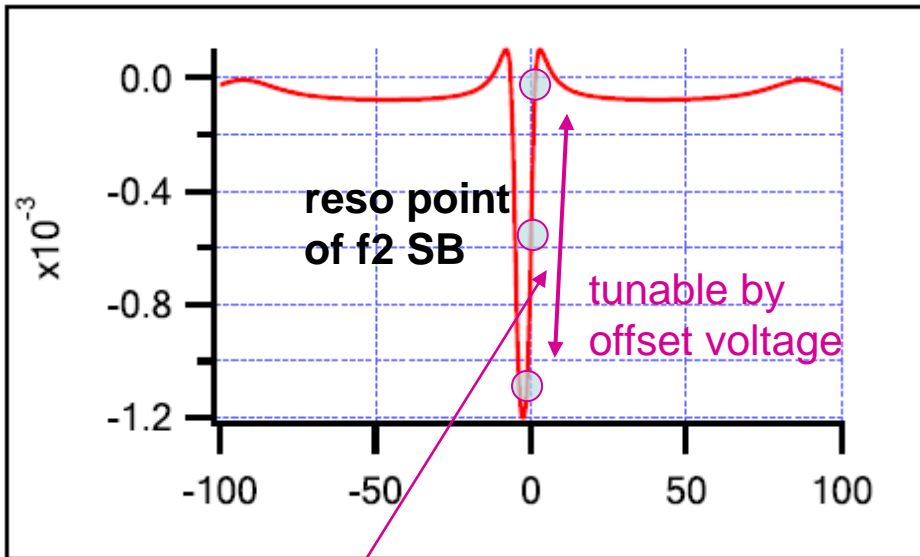


Can we shift detuning by

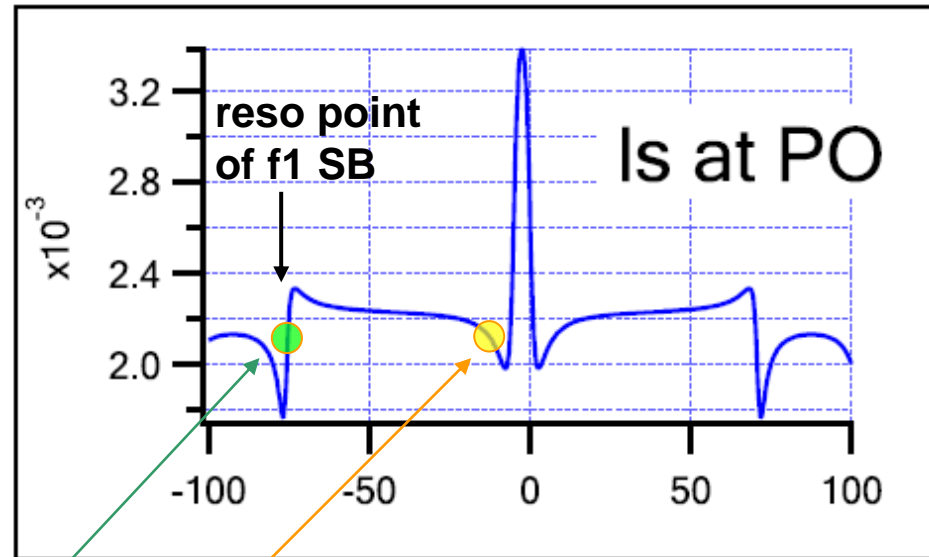
- adding offset to  $I_s$  signal,
- or
- changing SB freq within MC bandwidth?

# Dynamic range of clean Is signal

Error signal of Is (HF scheme)



(LF scheme)

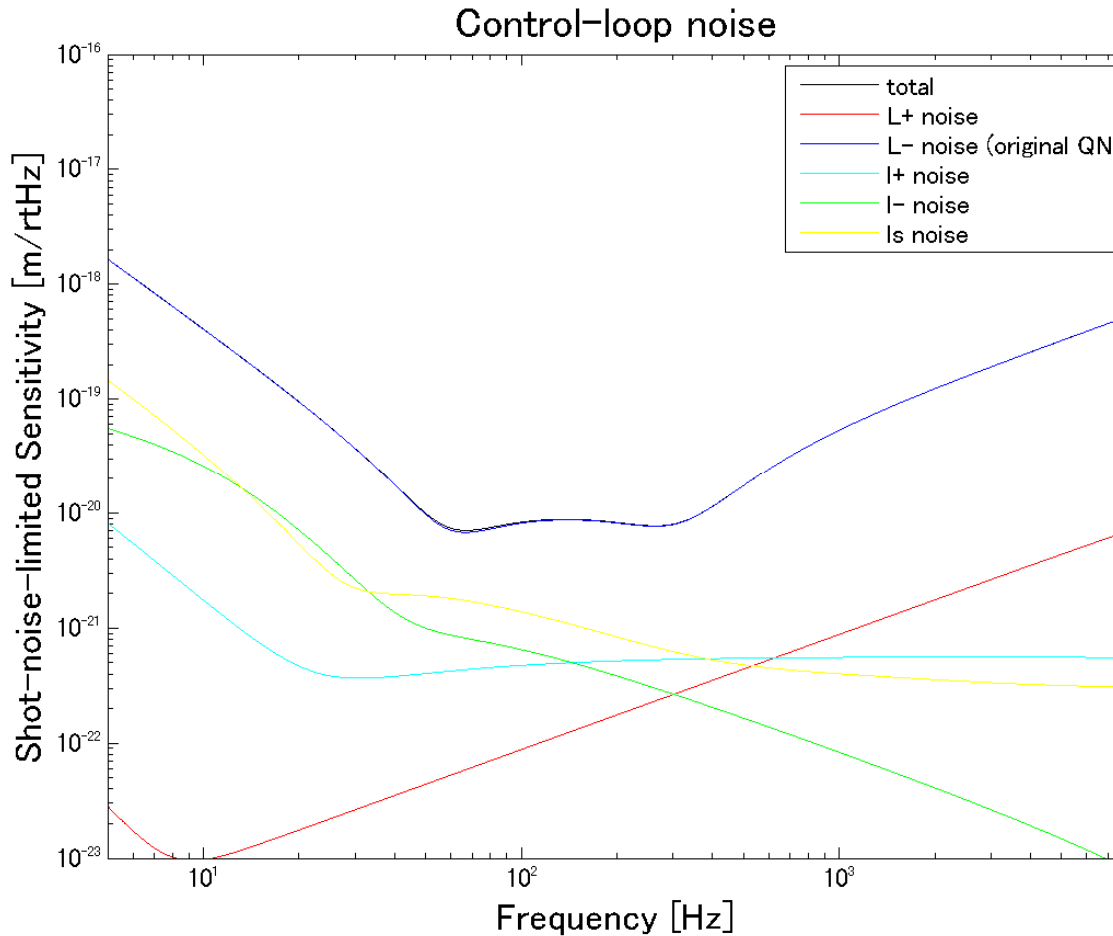


- Tunable range is  $\sim \pm 2$  deg, regardless of HF or LF.
- Maybe we can lock to somewhere like here (non-resonant point).
- We have another operation point where f1 SB resonates in the SRC. (HF scheme doesn't have this feature due to a large asymmetry.)

**Let's see loop-noise spectrum for each situation.**

# Slight detune-phase-shift by offset

27-45MHz with Feed-forward



$\phi=2.5\text{deg}$



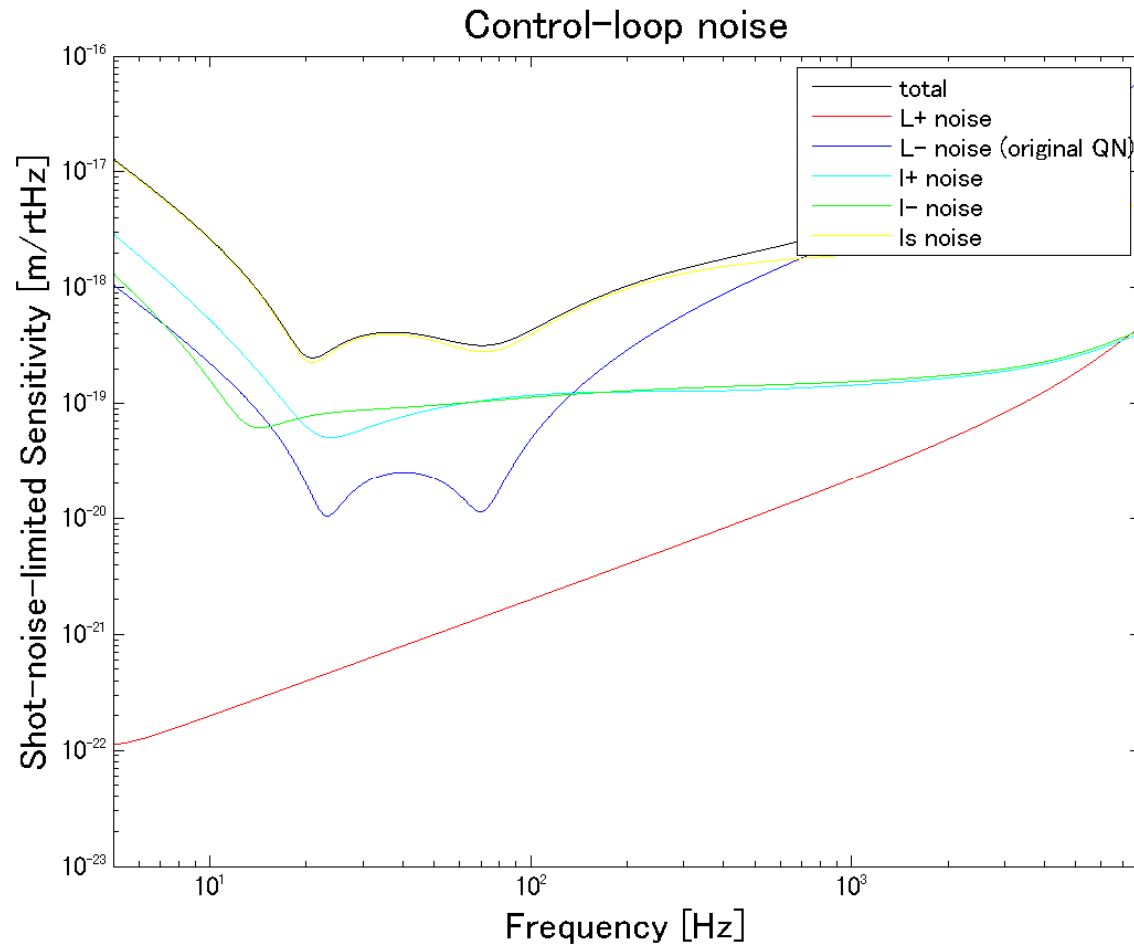
$\phi=3.5\text{deg}$

Freq-dependence  
Of  $\phi=2.5$  is used.

**Almost no change. Very good.**

# Operation at non-resonant point

w/o feed-forward



**Very bad.**

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# Operation with f1 being resonant

Relation between detune phase and RFSB frequency:

$$\frac{c}{2L_s} = \pi \times \frac{f_1}{n_1\pi - \phi_1} = \pi \times \frac{f_2}{n_2\pi - \phi_2} \quad \mathbf{n=integer}$$

Difficulty comes from the fact that f1 and f2 should be multiple of 9MHz.

If we set  $\phi_2$  to be 2.5 deg,

w/ telescope

27-45MHz >>  $\phi_1=35\text{deg}$  (Ls= 7m or 57m)

9-45MHz >>  $\phi_1=37\text{deg}$  (Ls=13m or 53m)

9-63MHz >>  $\phi_1=26\text{deg}$  (Ls=14m or 52m)

27-63MHz >>  $\phi_1=25\text{deg}$  (Ls=12m or 62m)

**What if f1 is higher than f2?**

# Can we choose $f_1/f_2$ for 2.5deg and 14deg?

If we set  $\phi_2$  to be 2.5 deg,

45-27MHz  $\gg \phi_1 = 4.1$ deg (Ls=17m or 50m)

→ 45-9MHz  $\gg \phi_1 = 12.5$ deg (Ls=16m or 50m)

63-9MHz  $\gg \phi_1 = 17.5$ deg (Ls=16m or 50m)

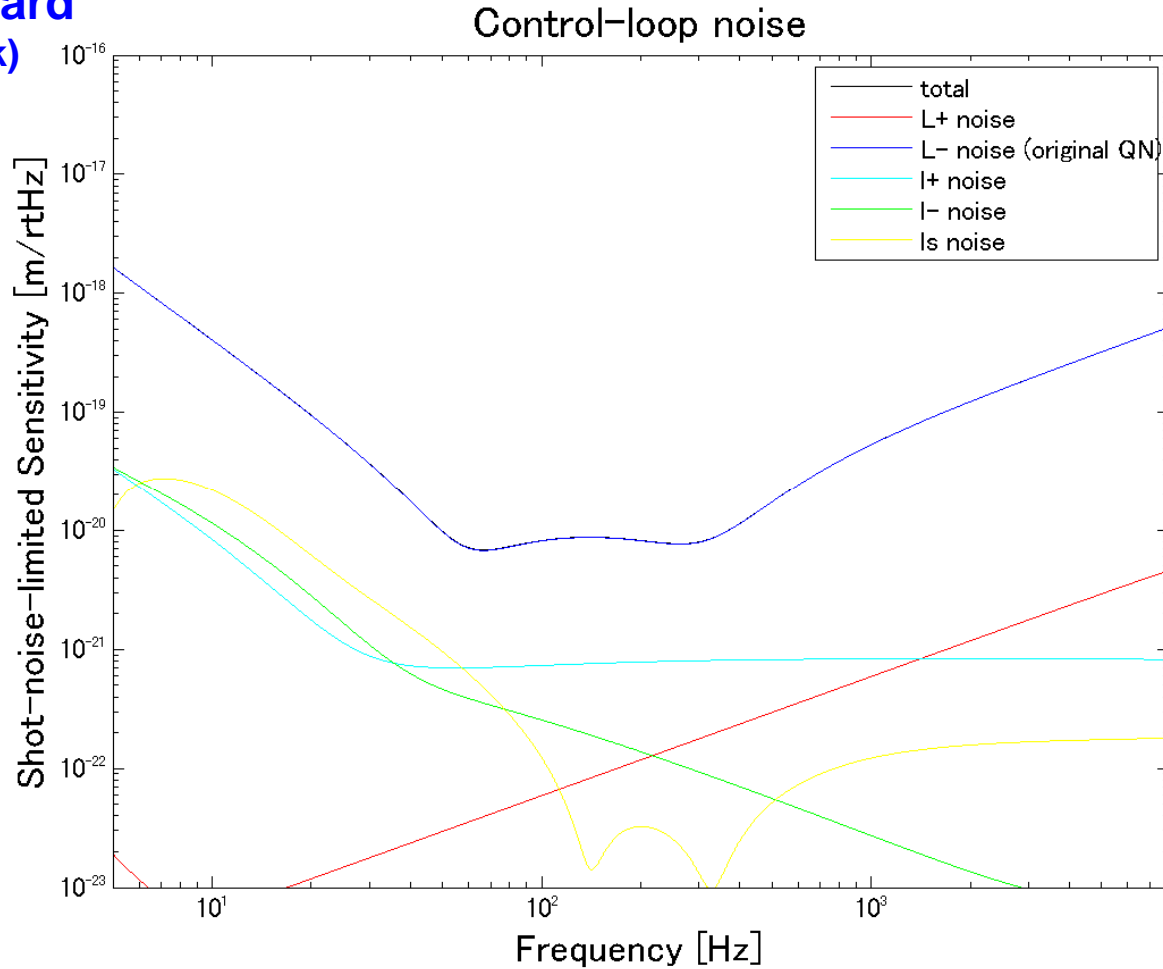
63-27MHz  $\gg \phi_1 = 5.8$ deg (Ls=17m or 50m)

**This one looks good.**

- Asymmetry is set not to be optimized to one of them but middle
- For BHBH, as input power is low, we can increase  $m$  (set to 0.8)
- Attenuators can be removed but other optics are all fixed

# 45-9MHz scheme for NS-NS

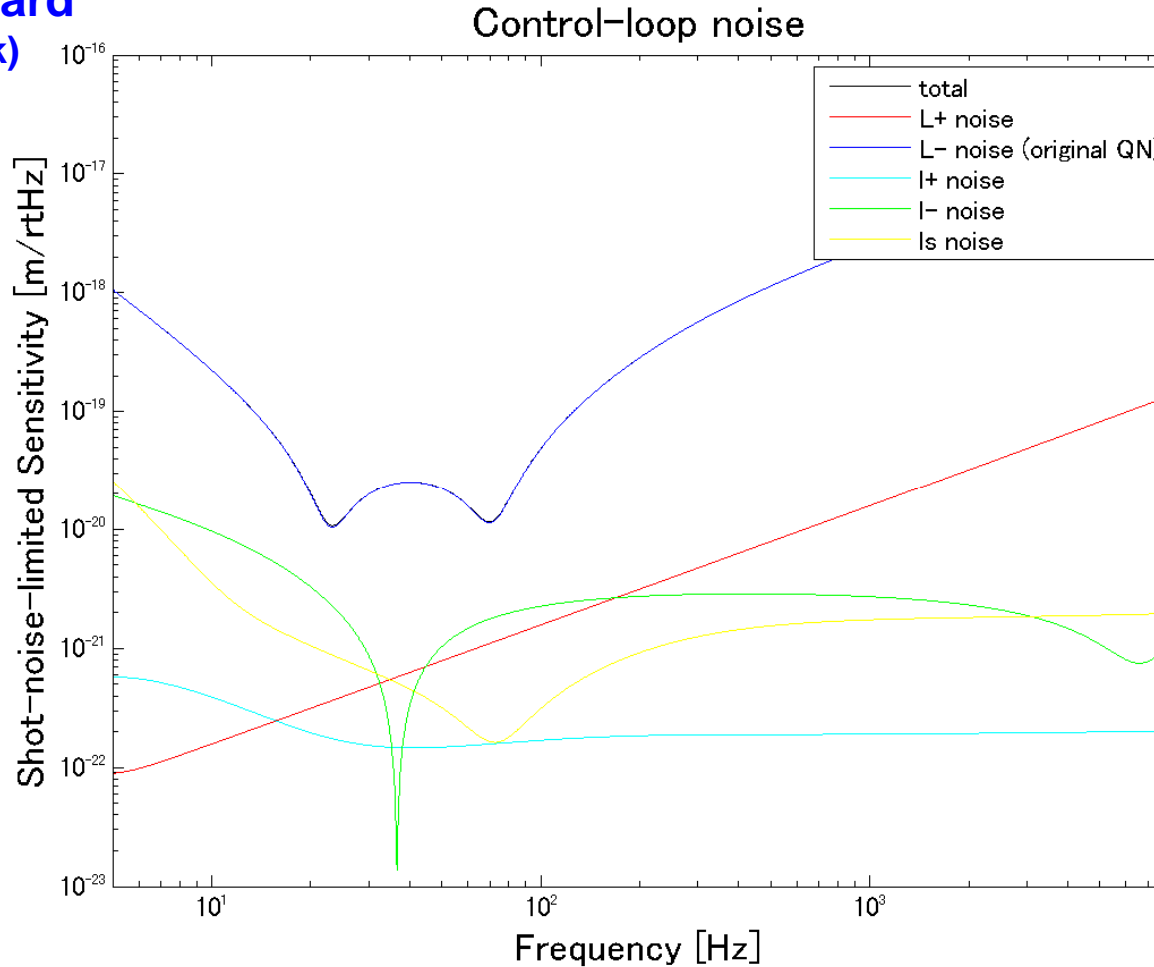
With Feed-forward  
(15% accuracy is ok)



**Very good.**

# 45-9MHz scheme for BH-BH

With Feed-forward  
(15% accuracy is ok)



**Very good.**

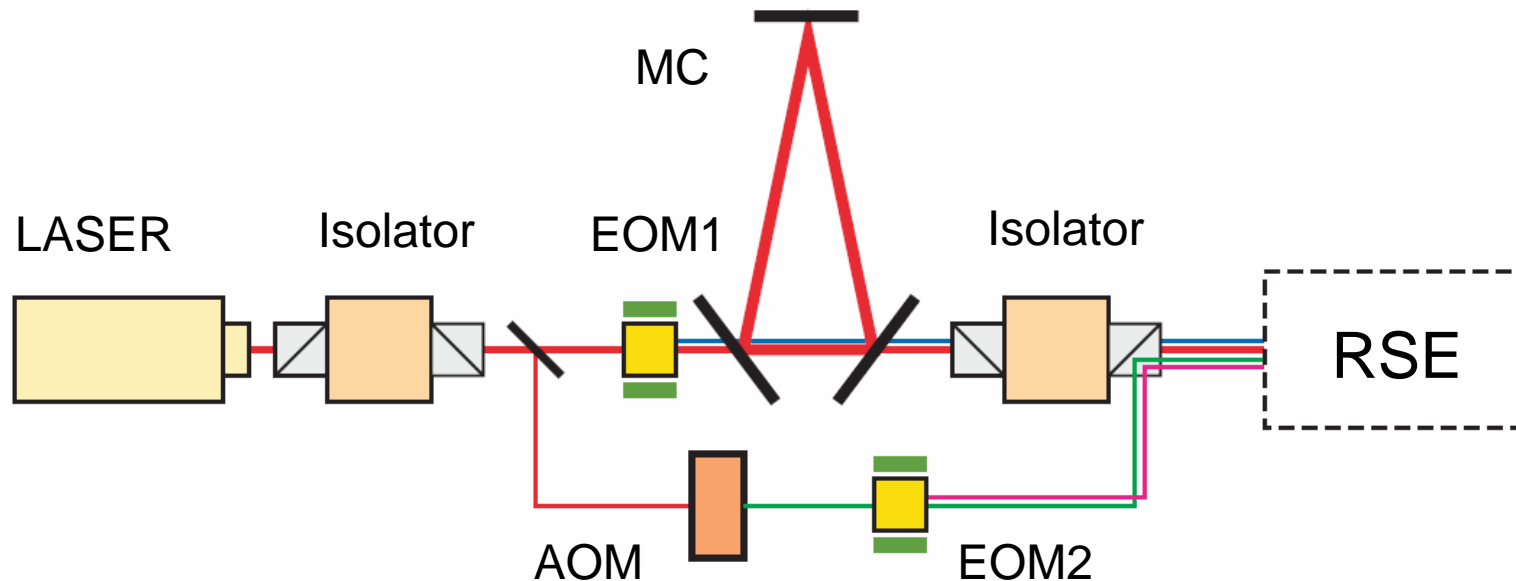
# Actually,...

*It'd be better if we can  
continuously change detuning.*

*Is it possible?*

**We need new scheme.**

# Control scheme with the other polarization

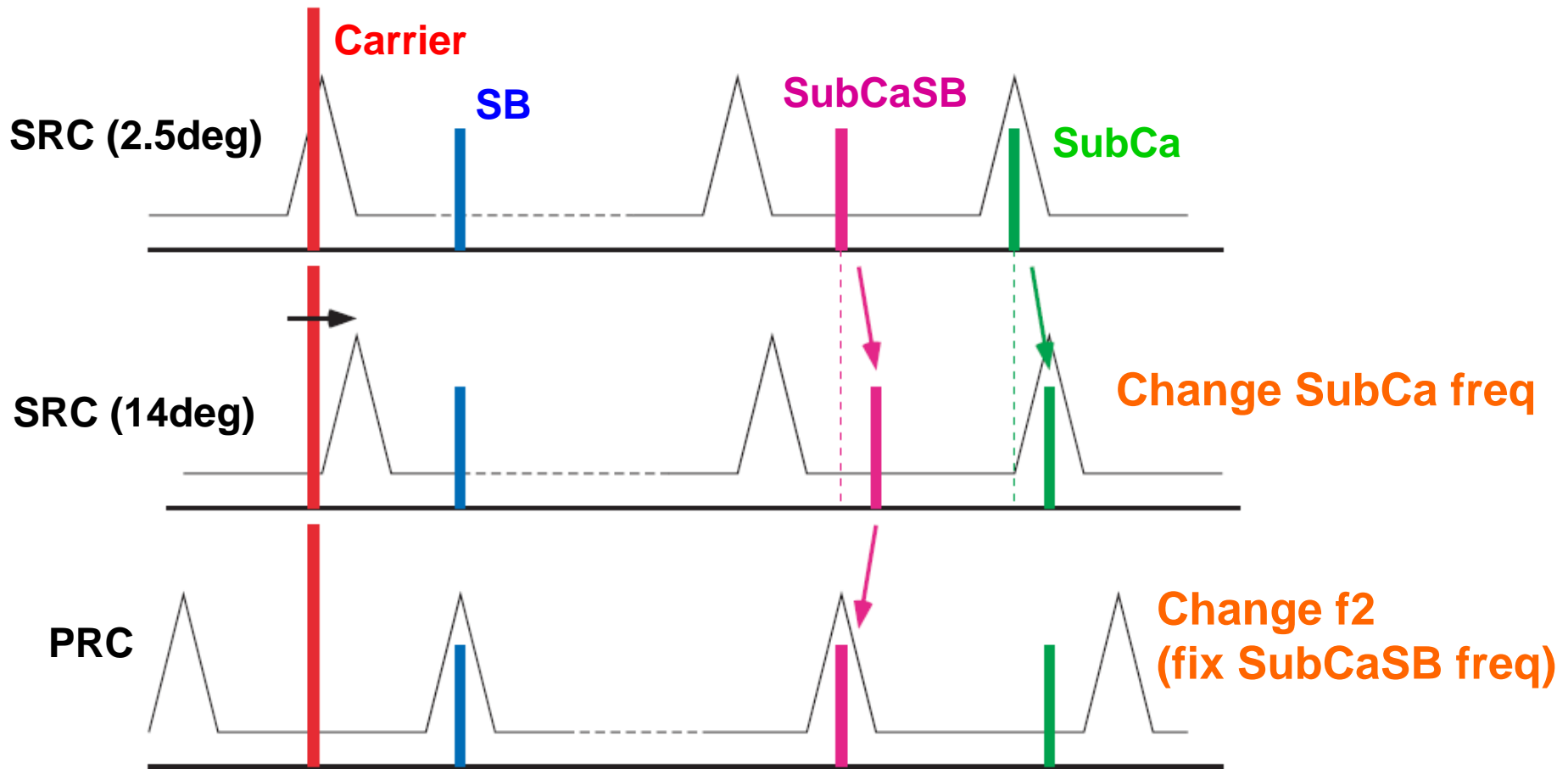


- Flexible detuning may be possible with light that doesn't transmit MC
- We'll have Faraday after MC → Let's inject light from Faraday

Carrier } → L+  
SB }  
Sub-Carrier } → I+, I-, Is  
Sub-Ca SB }

Single demodulation!  
No Mach-Zehnder!

# Flexible detuning



SubCa should resonate in PR-SRC to probe  $I_s$  signal.  
SubCaSB should resonate in PRC to probe  $I_-$  signal.

# Sideband frequencies

## Carrier SB (PM)

It should better resonate in the PRC

$m=0.1$

It shouldn't resonate in the SRC

—————> 9MHz or 27MHz

## SubCa SB (SSB)

It should resonate in the PRC to probe I-

$m=1.15$

Asymmetry factor should be as low as possible

Modulation frequency should be as low as possible

—————> 216MHz (~ SubCa-108MHz)

## SubCa

1W

It should transmit Michelson part (HF scheme)

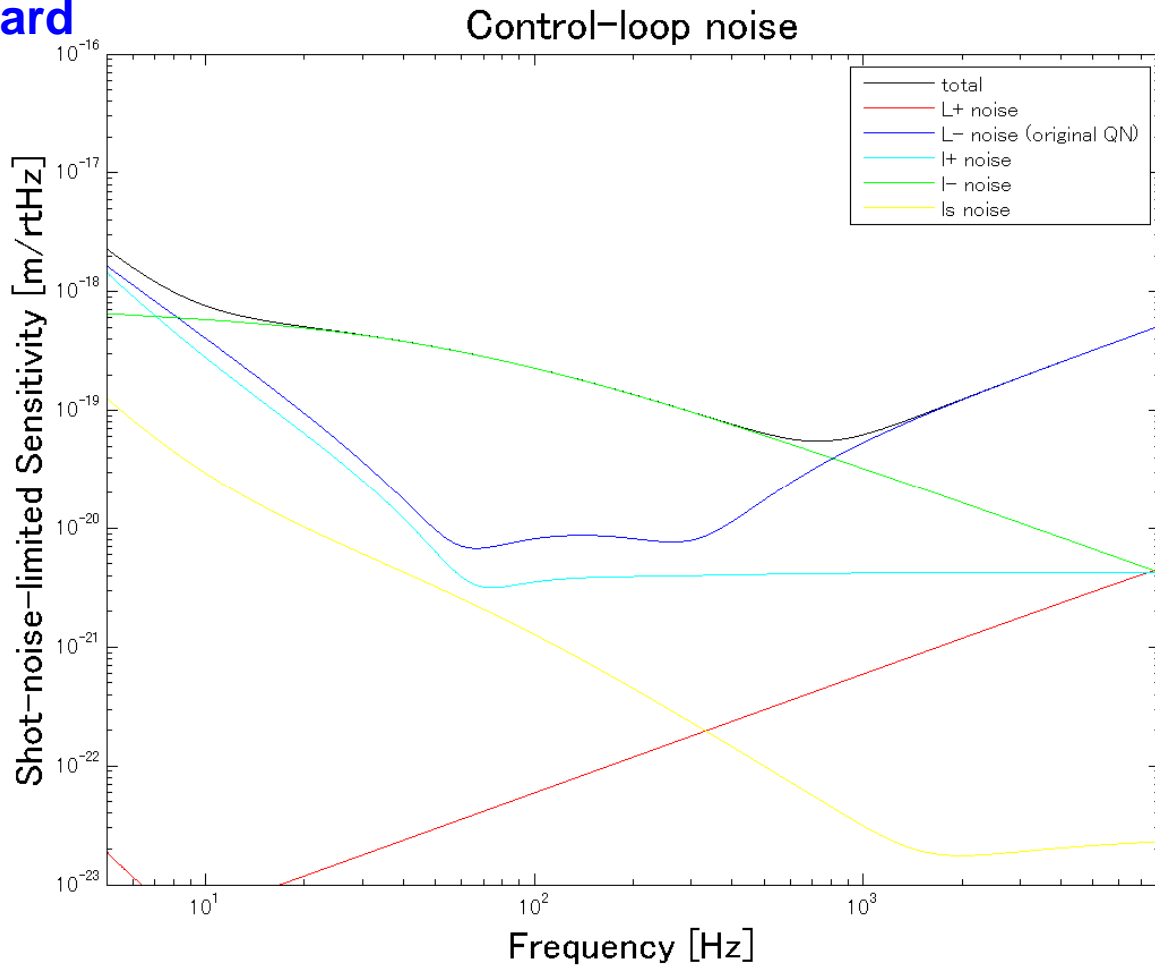
—————> ~324.3MHz

**Let's see the sensitivity curve.**



# Dual-polarization control scheme for NS-NS

w/o feed-forward

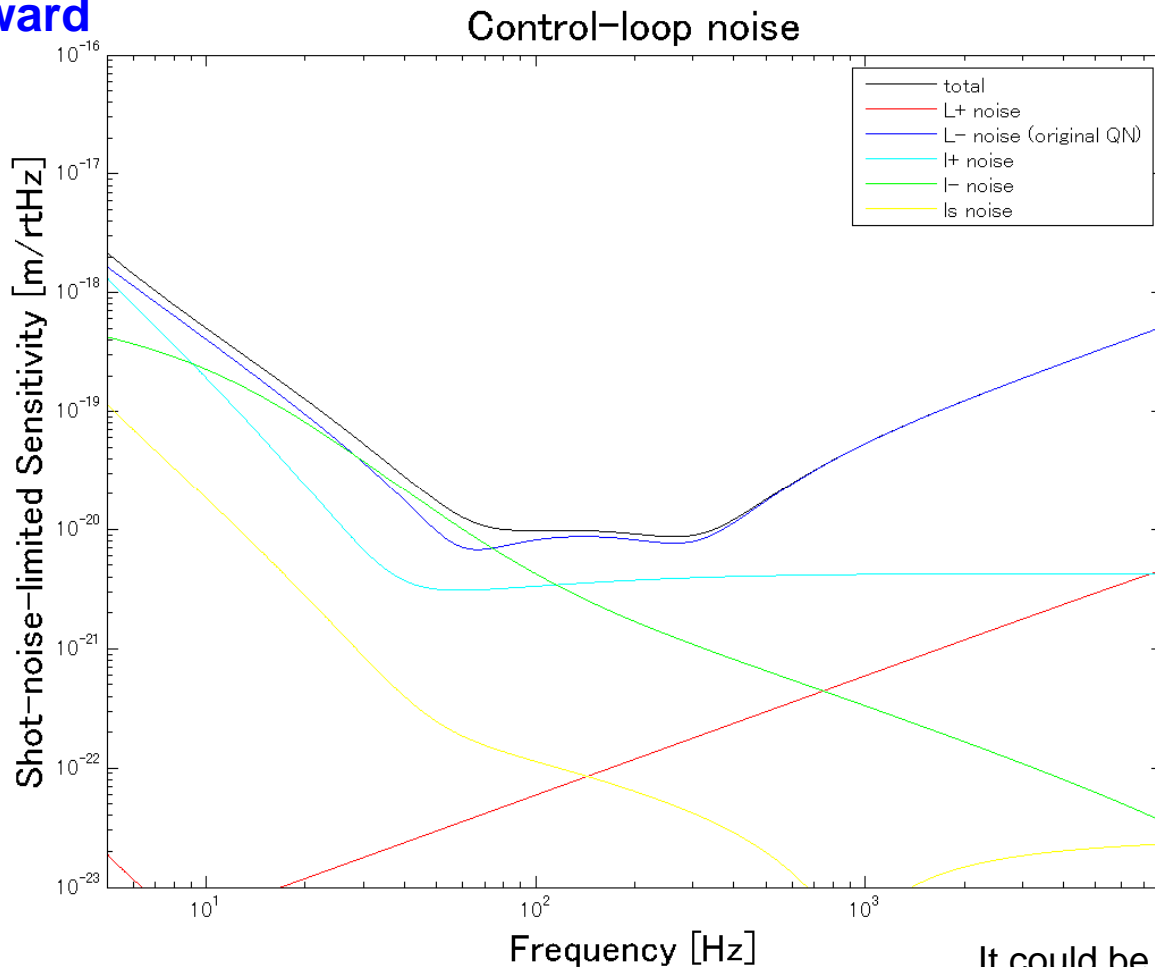


Quite bad.

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# Dual-polarization control scheme for NS-NS

with feed-forward



**Not good but close.**

# Let's make comparison

Now we have 4 candidates

1.  $f_1=27\text{MHz}$ ,  $f_2=45\text{MHz}$ , asymmetry=4cm (LF scheme)
2.  $f_1=9\text{MHz}$ ,  $f_2=108\text{MHz}$ , asymmetry=75cm (HF scheme)
3.  $f_1=45\text{MHz}$ ,  $f_2=9\text{MHz}$ , asymmetry=6.7cm (LF scheme)
4.  $f_1=27\text{MHz}$ , SubCa=324MHz,  $f_2=108\text{MHz}$ , asymmetry=75cm

# Let's make comparison

	27-45LF	9-108HF	45-9LF	dual-pol.
SB frequency	Low	High	Low	High
Loop noise	Good	Good	Good	Bad
Flexibility	1 for NS, the other is useless	Only for NS	1 for NS, the other for BH	It should be good
Misc.	--	Tested at the 40m	Harmonics ?	Many unknowns

- LF schemes look good
- Decision would depend on how we want flexibility
- How can we test LF scheme at the 40m?

# Summary

- We developed a tool to calculate control-loop noise
  - Now we can compare control schemes
  - We look at Low-freq scheme and it works well
  - Flexible detuning is attractive while quite hard to realize
  - Using the other polarization is one possibility
  - We'll be soon ready to pick one for AdLIGO, hopefully
- 
- We're waiting for Optickle to be ready (esp. for vacuum!)
  - Some parts in our calculation still needs modification
  - How to test at the 40m is a thing to be considered