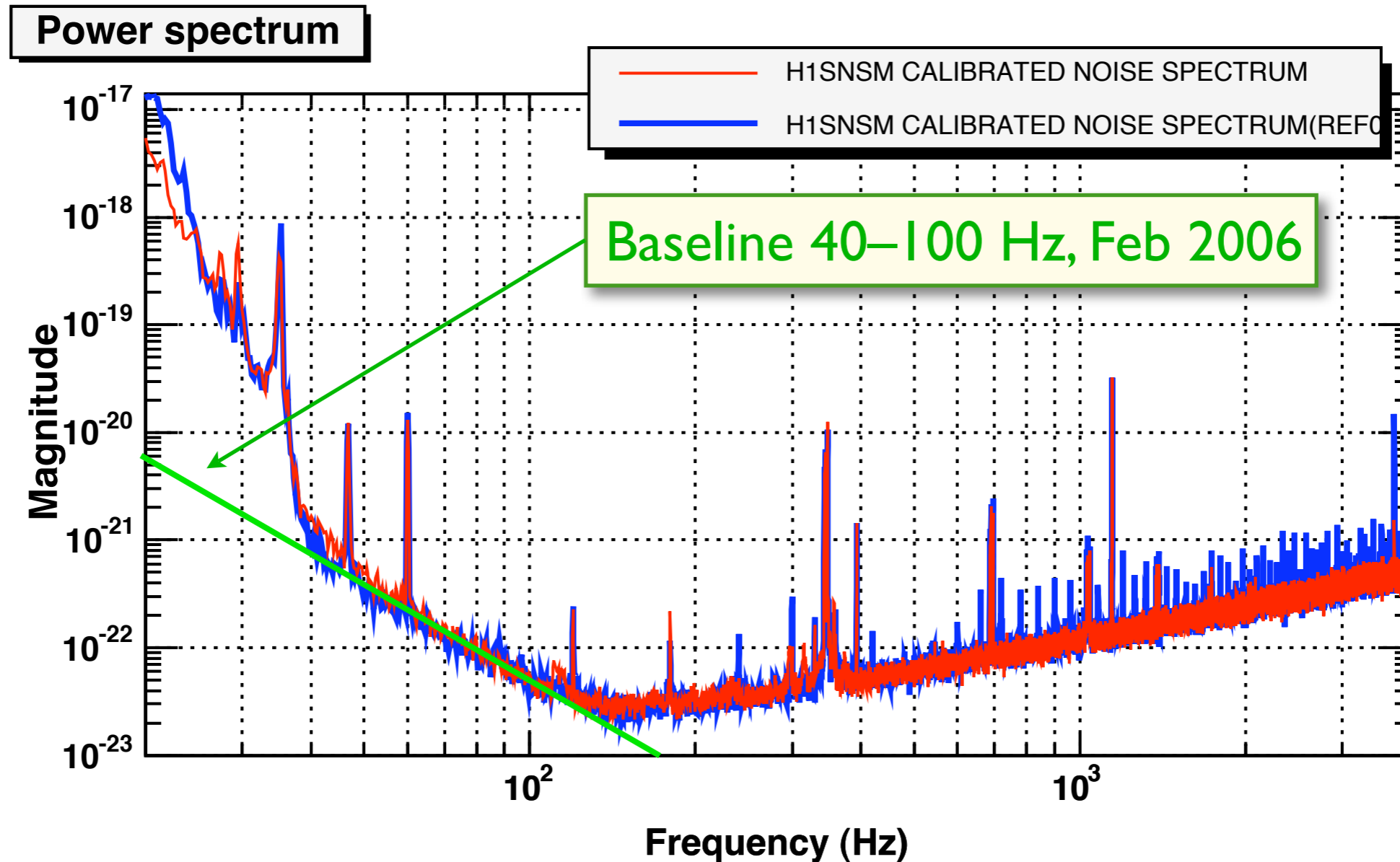

Suspension Thermal Noise in Initial LIGO

Steve Penn, Gregg Harry, Andri Gretarsson

LSC Meeting - LSU - August 2006

LIGO DCC LIGO-G060477-00-Z

The Problem

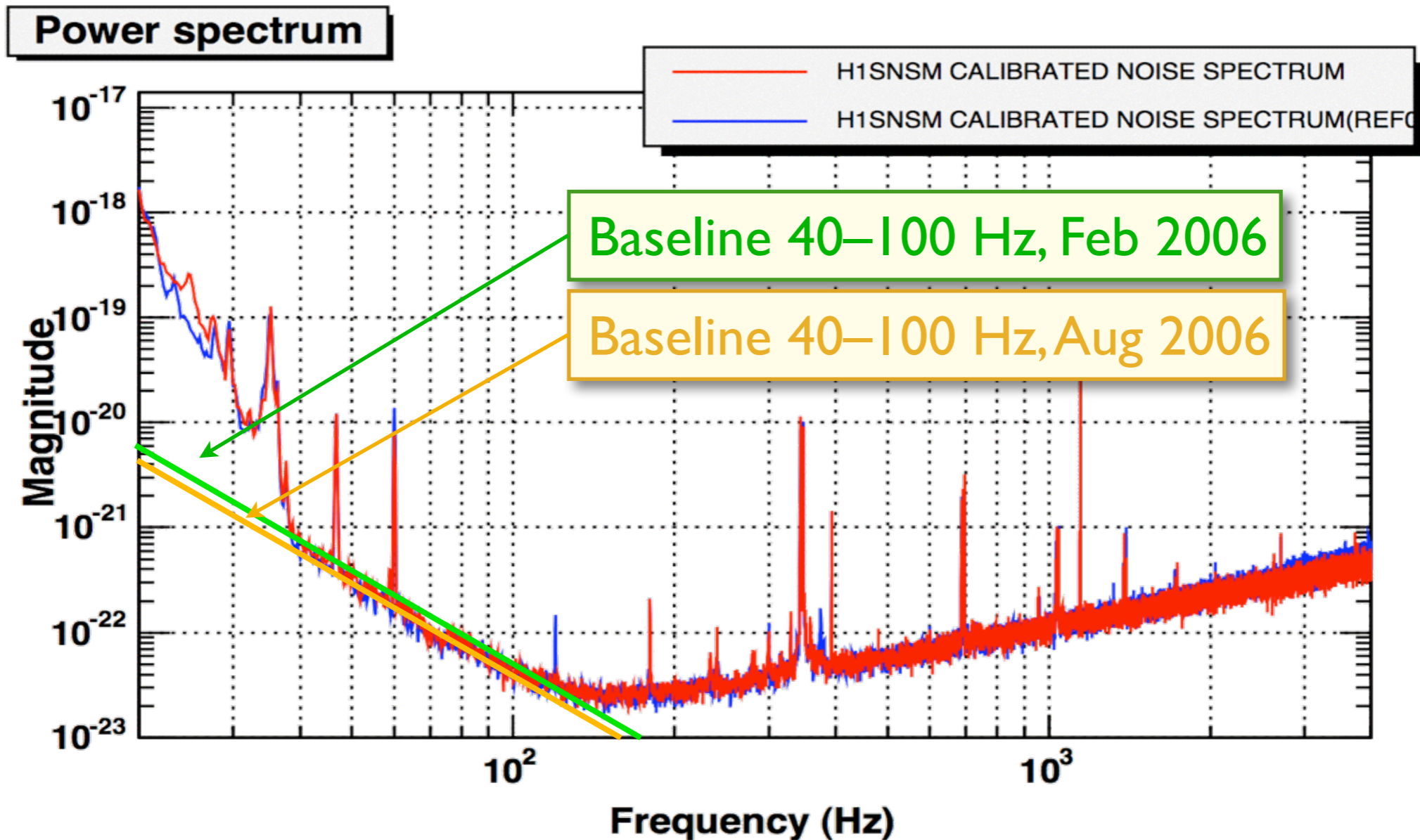


*T0=13/02/2006 12:22:47

Avg=15

- Noise between 40 Hz and 150 Hz has slope near 5/2
- Level is high, but not impossibly high, to be suspension thermal noise
- Very similar level in all three interferometers

The Problem



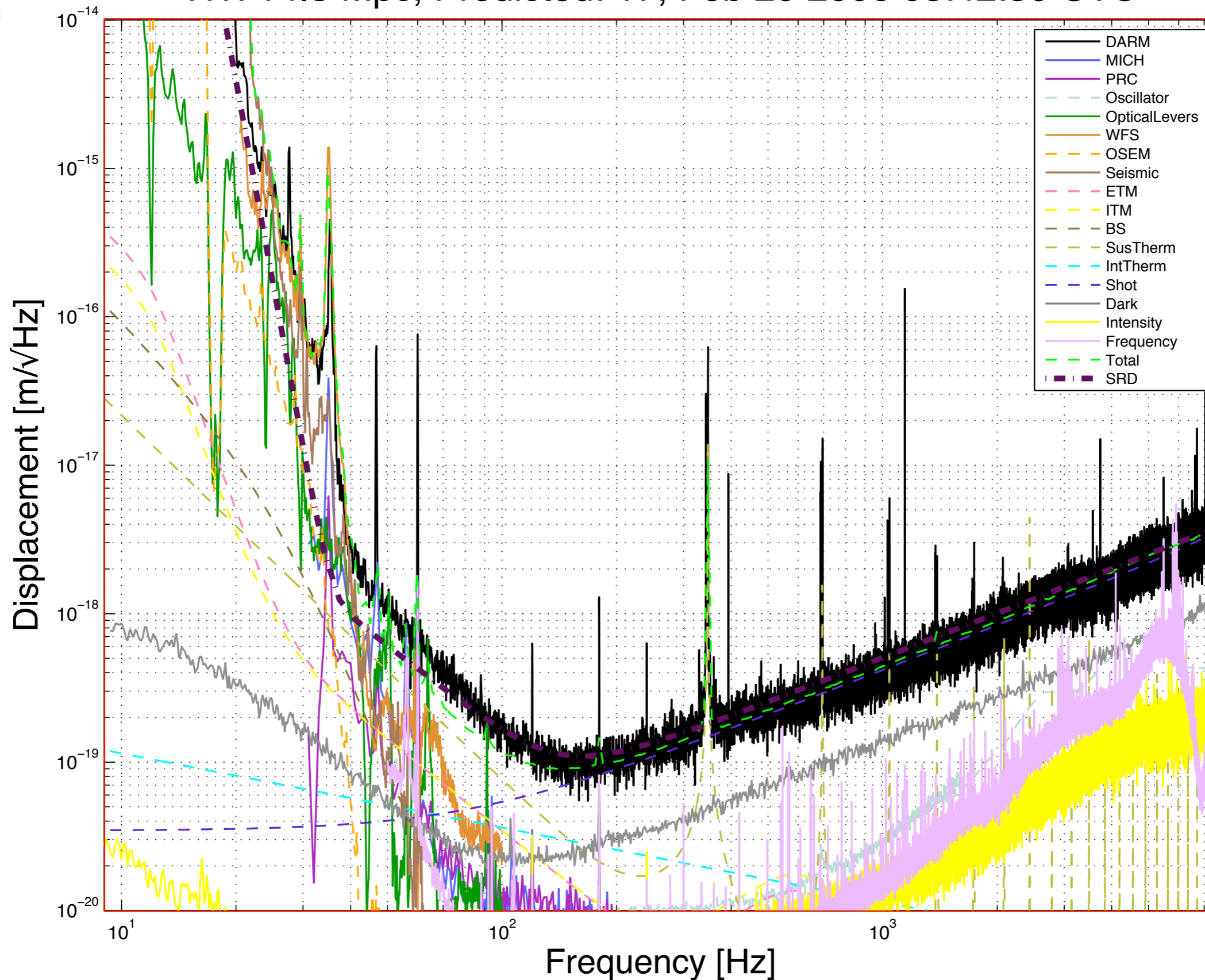
*T0=15/08/2006 06:38:47

Avg=15

- Noise between 40 Hz and 150 Hz has slope near 5/2
- Level is high, but not impossibly high, to be suspension thermal noise
- Very similar level in all three interferometers

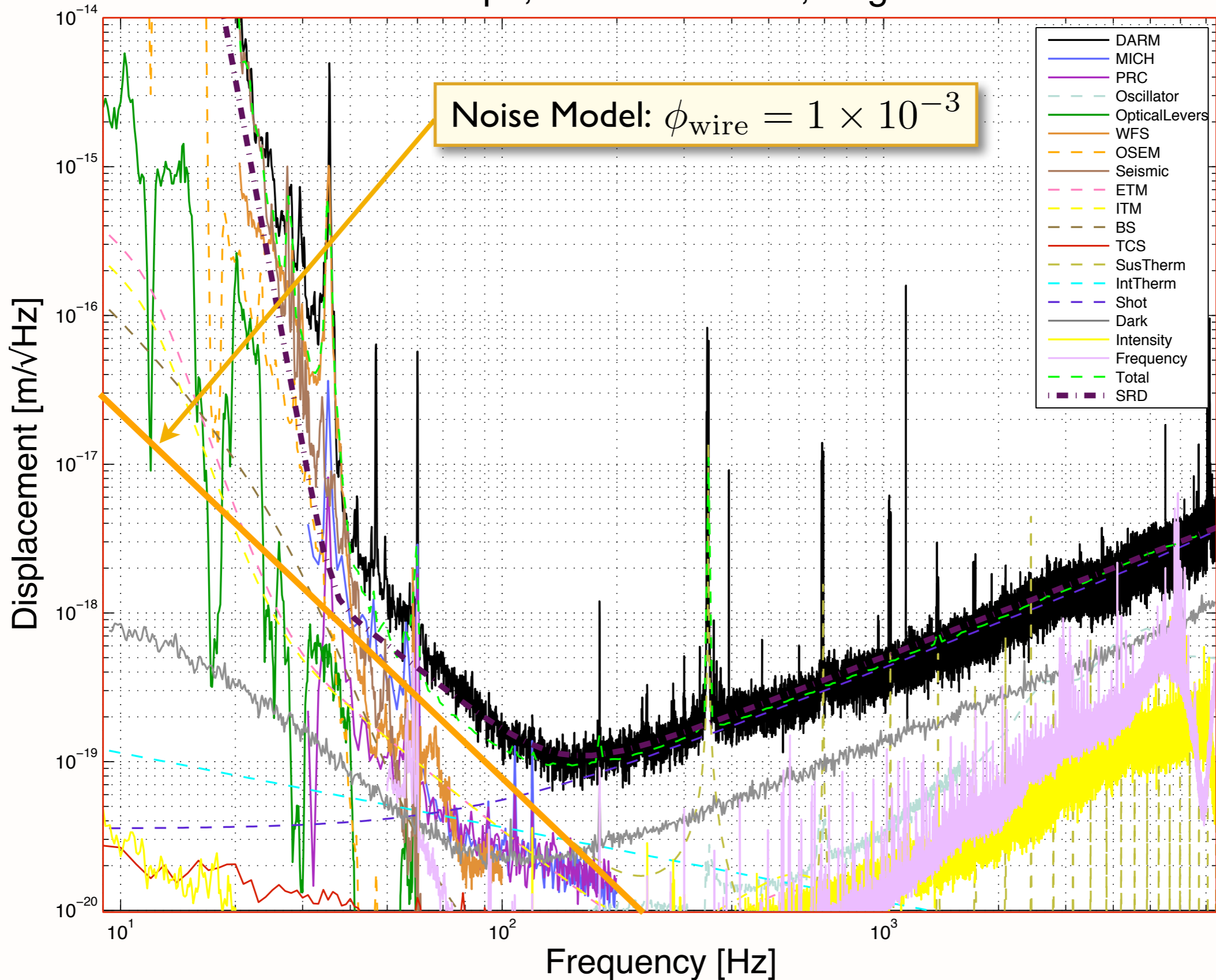
The Problem

H1: 14.5 Mpc, Predicted: 17, Feb 20 2006 05:42:50 UTC



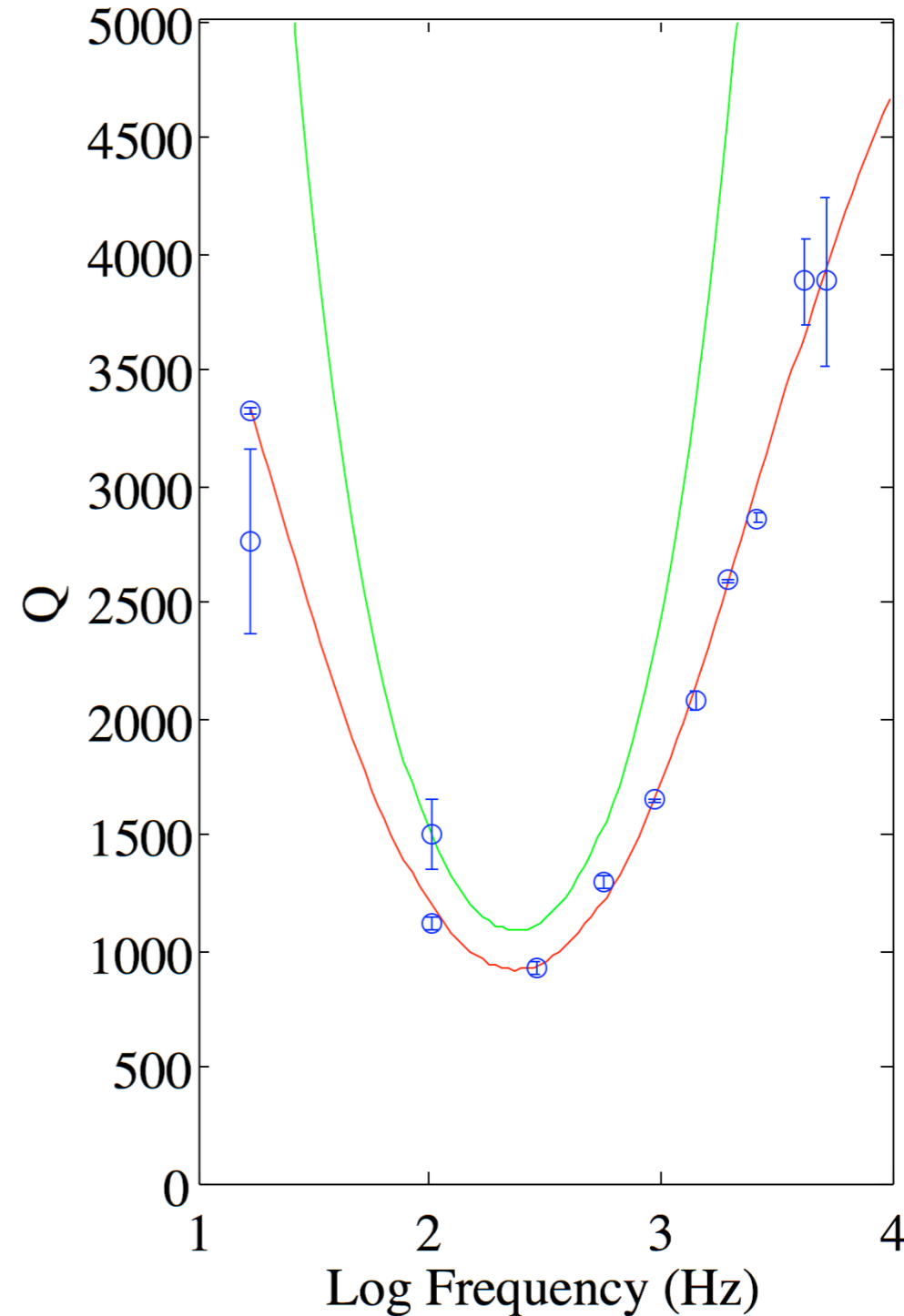
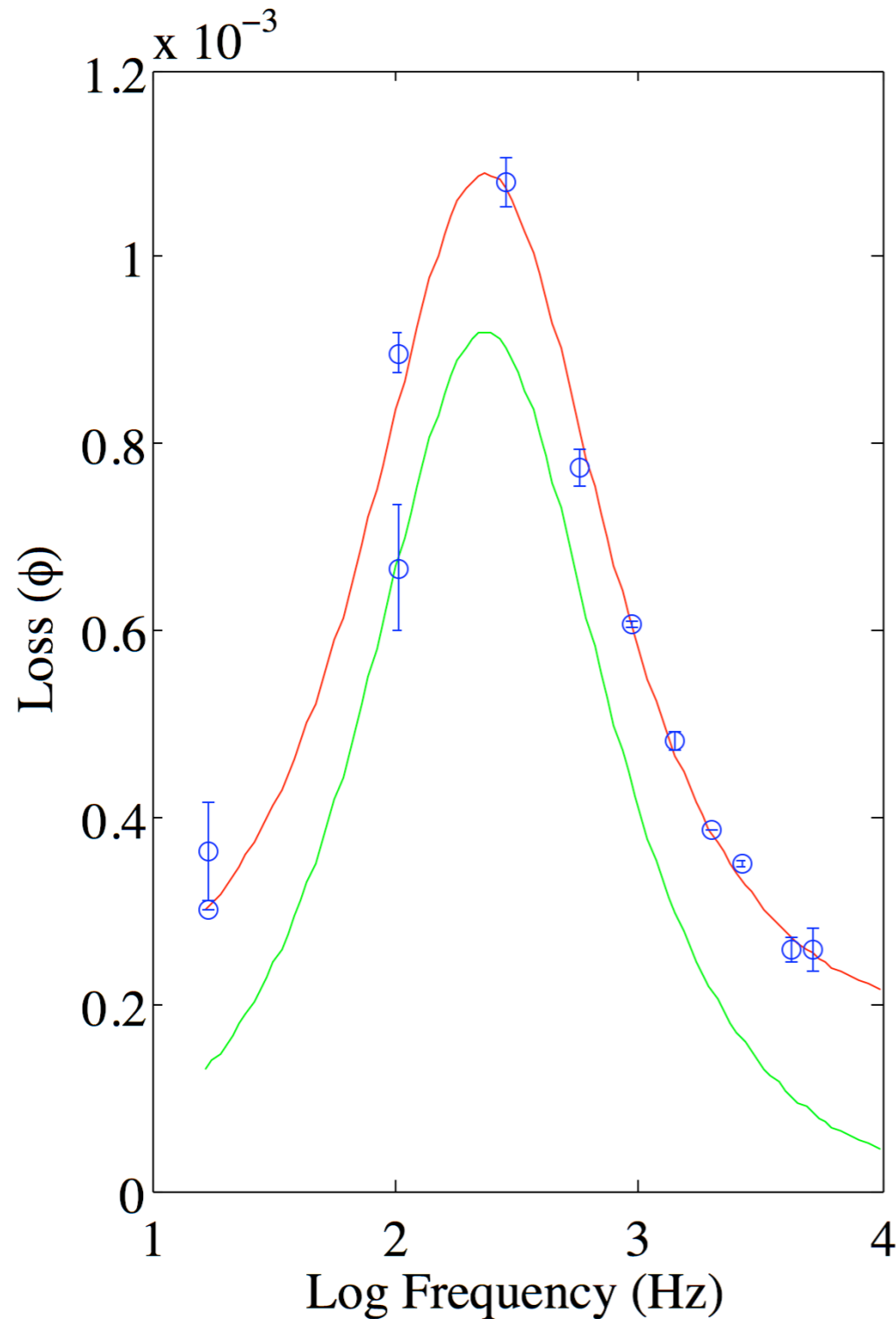
The Problem

H1: UGF = 199 Hz 13.6 Mpc, Predicted: 16.4, Aug 12 2006 01:00:00 UTC

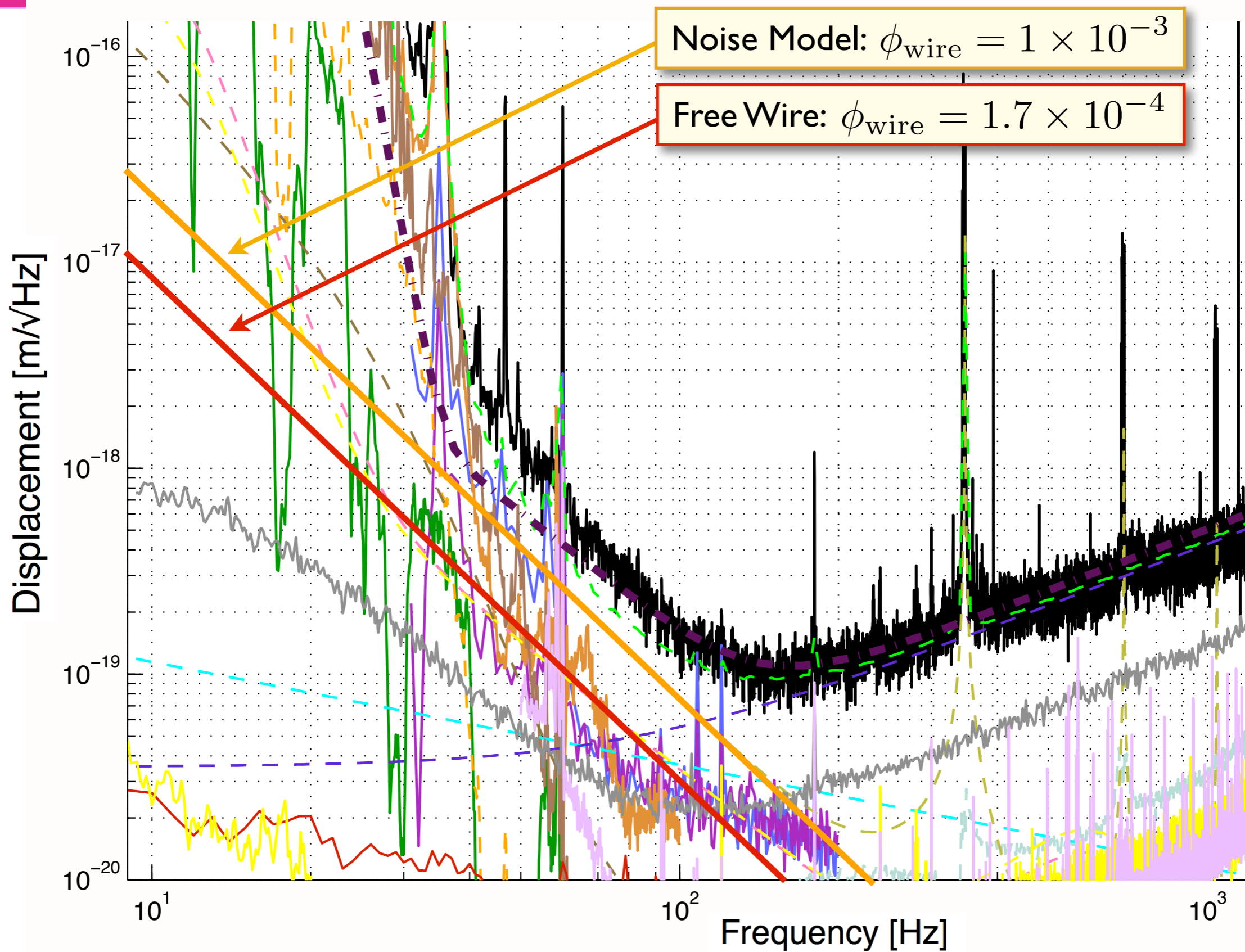


Mechanical Loss in Wires

$\phi_{\text{str}} = 1.70 \times 10^{-4}$ *Structural loss \approx half of assumed design value.*



The Problem

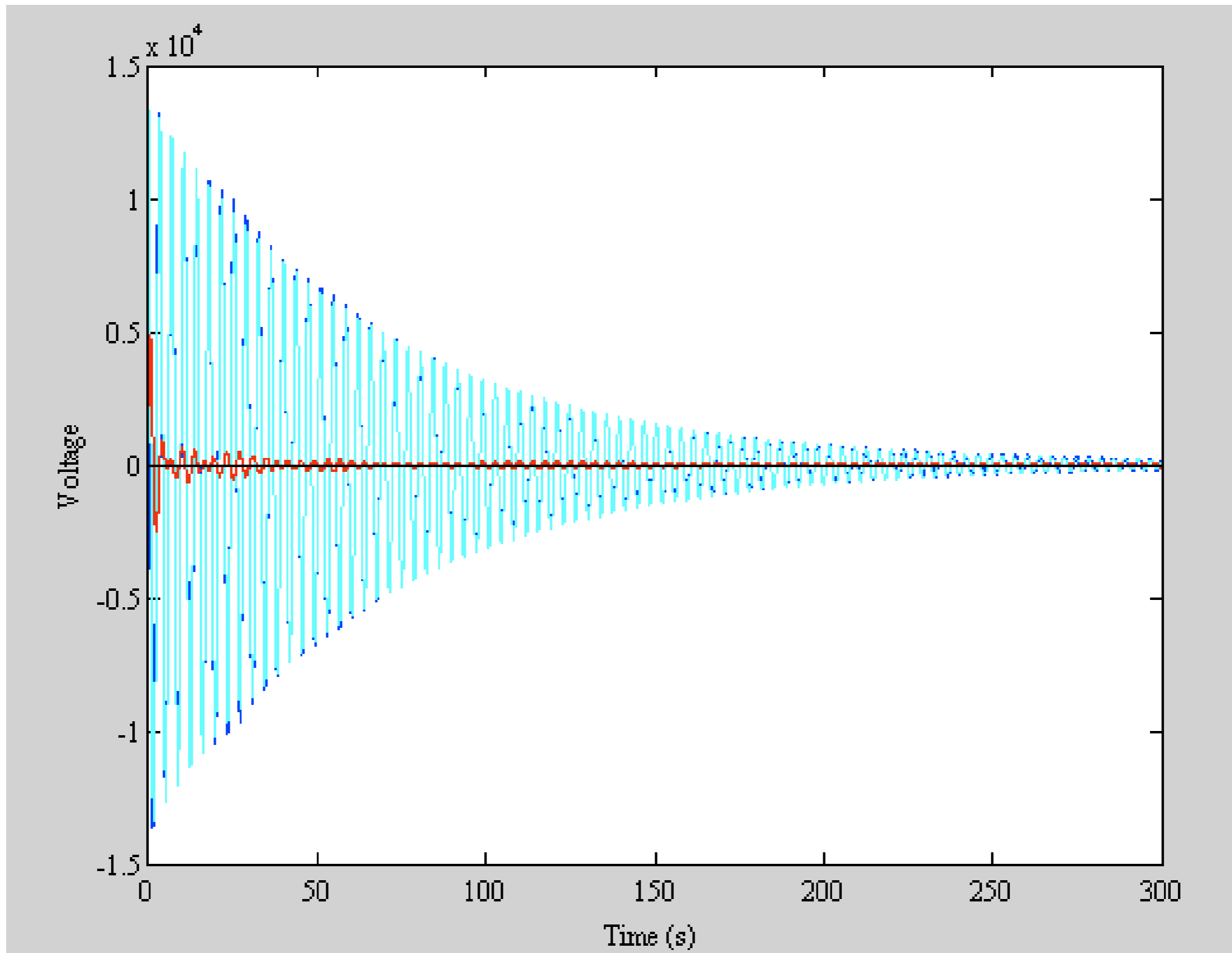




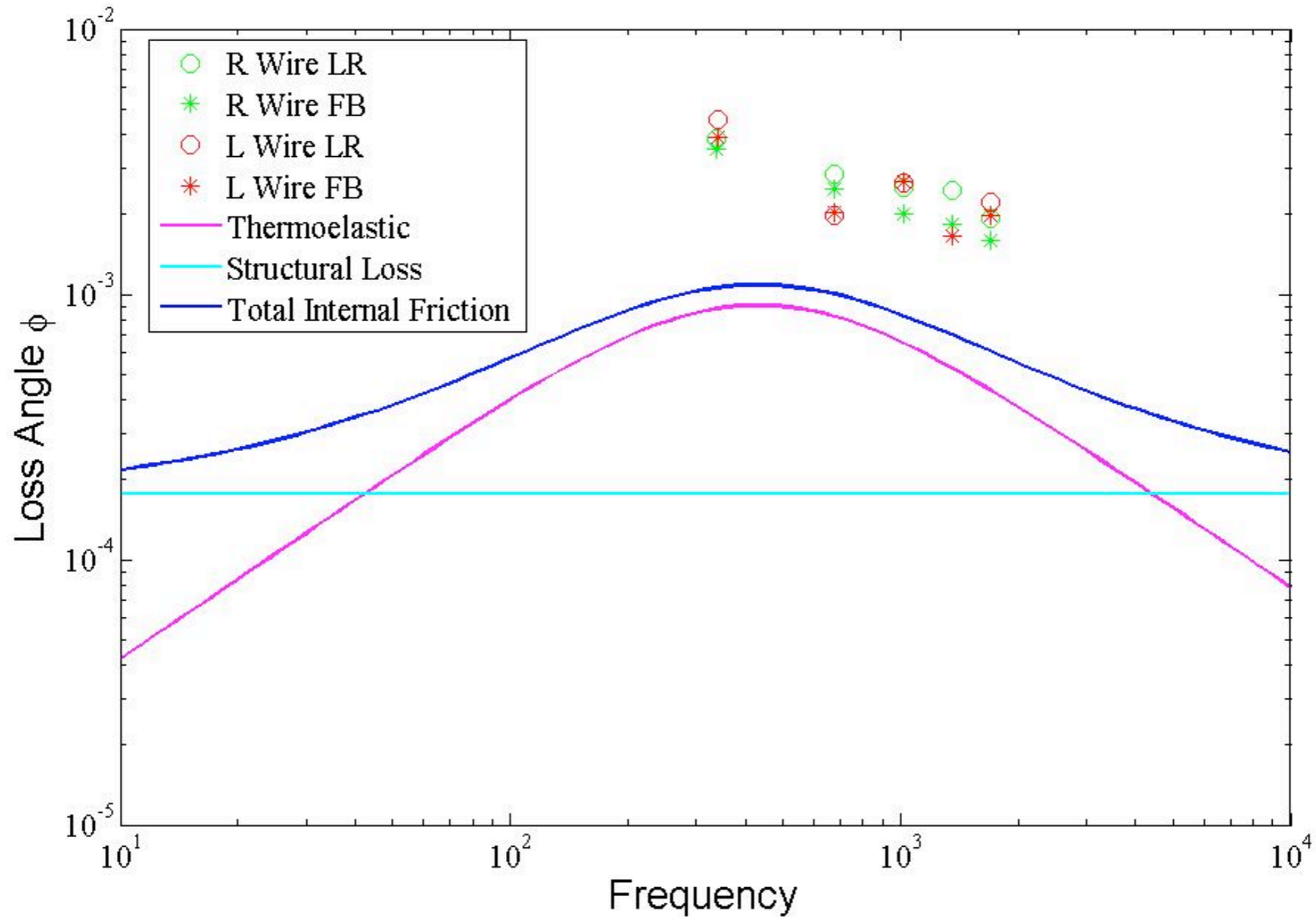
Pathfinder Optic hung in spare frame with wire from the sites. Each wire monitored by eight shadow sensors.



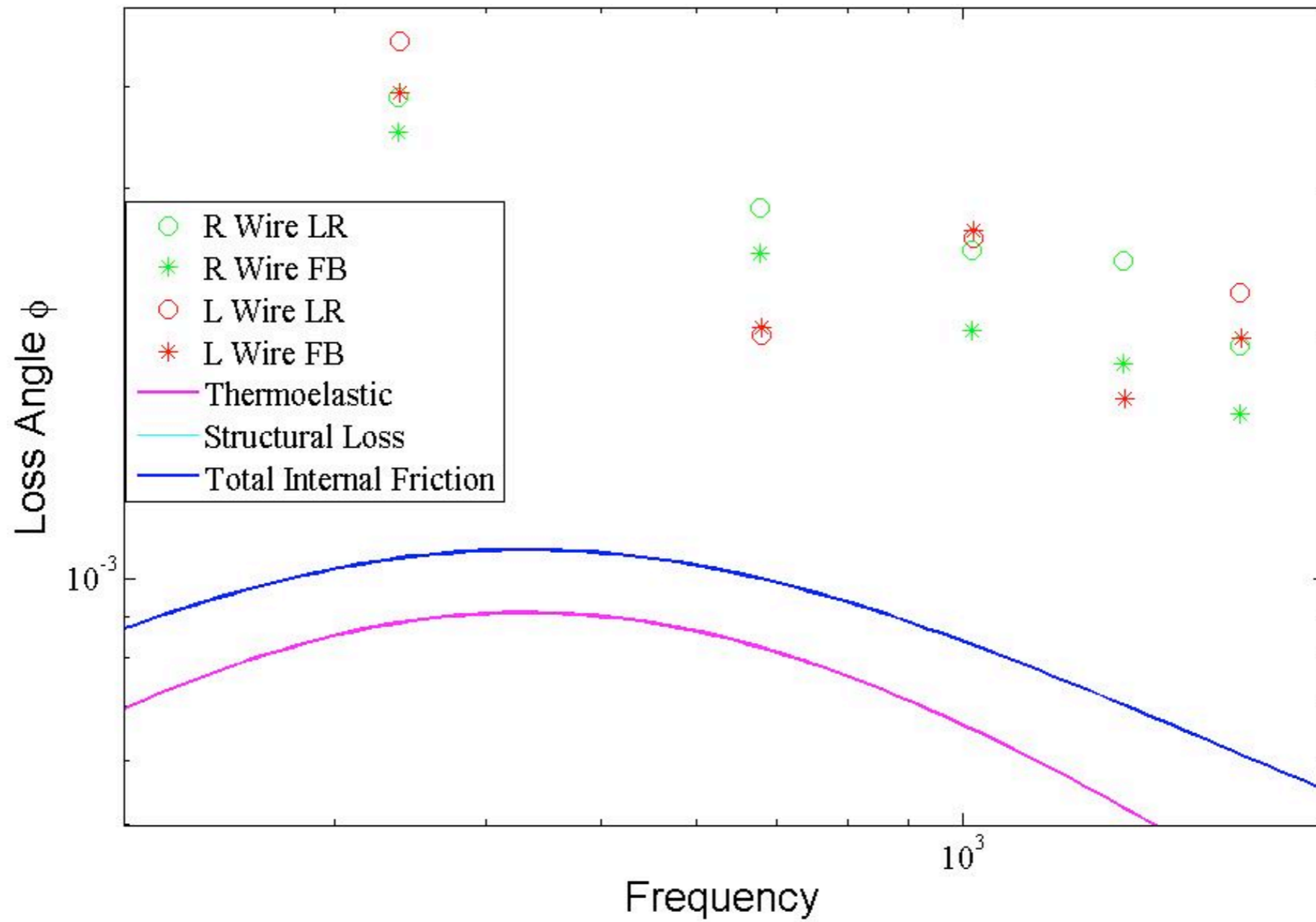
Typical Violin Mode Loss



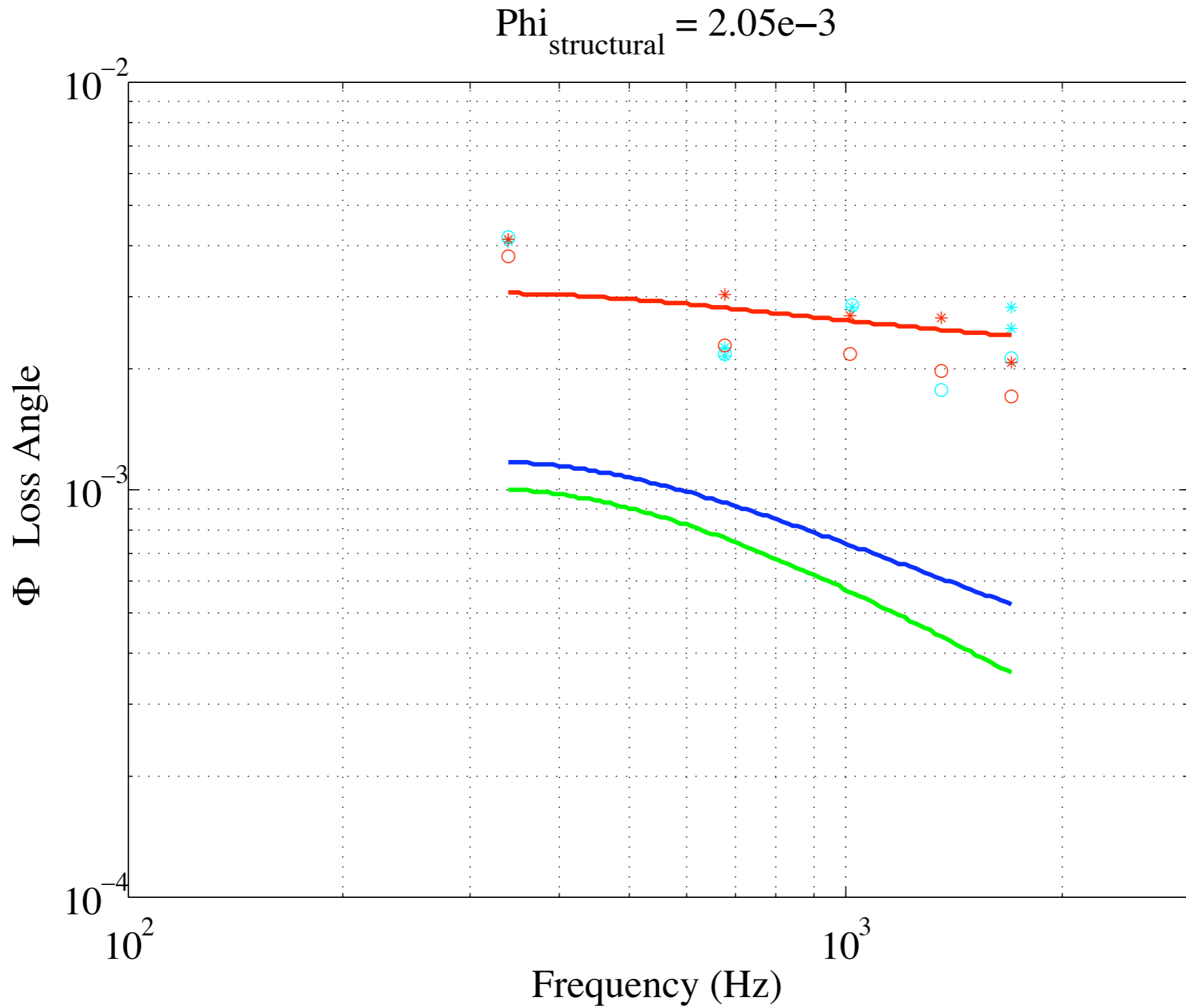
Violin Mode: Reused Clamp



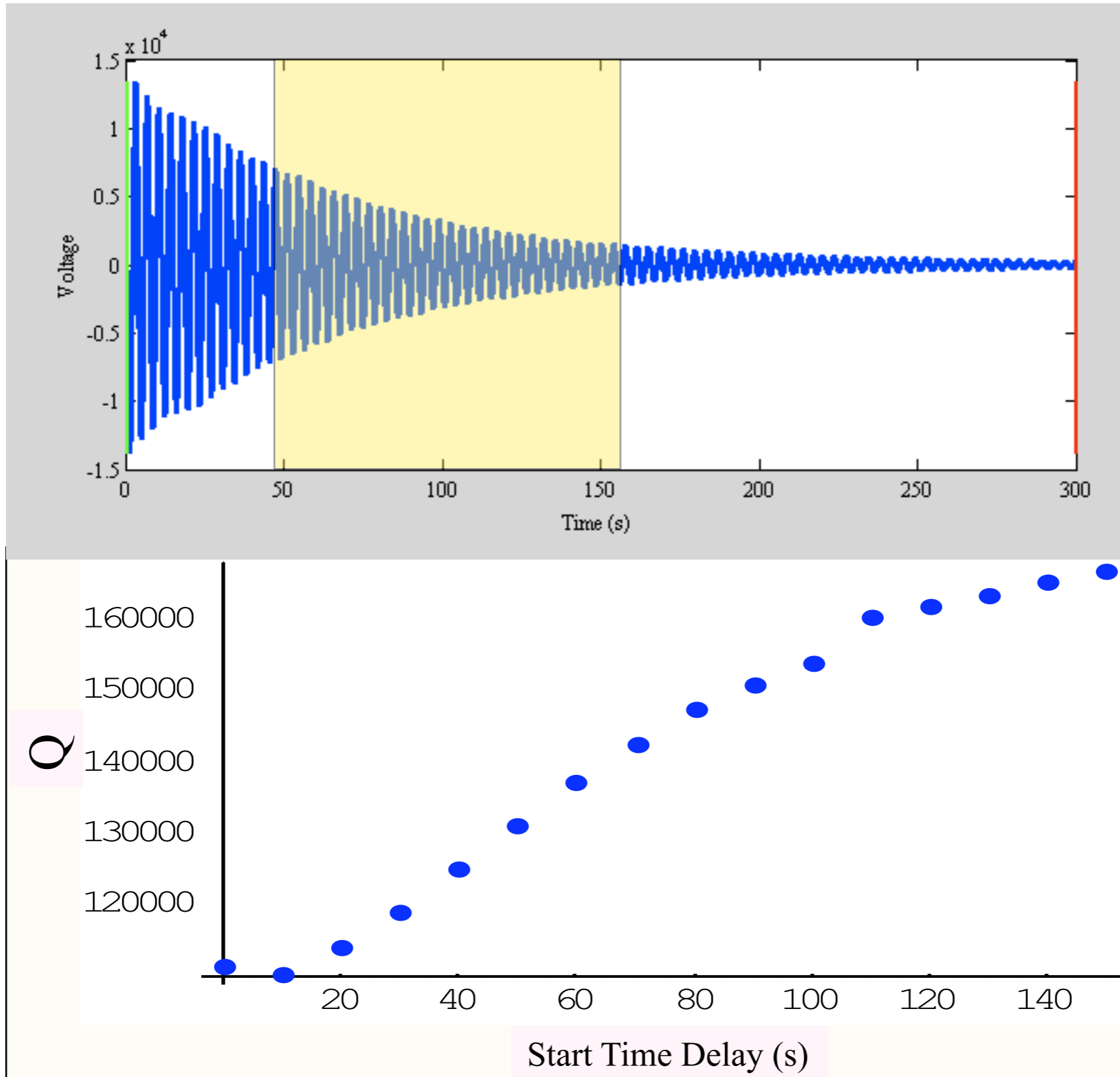
Violin Mode: Reused Clamp



Violin Mode: Reused Clamp



Q vs. Amplitude



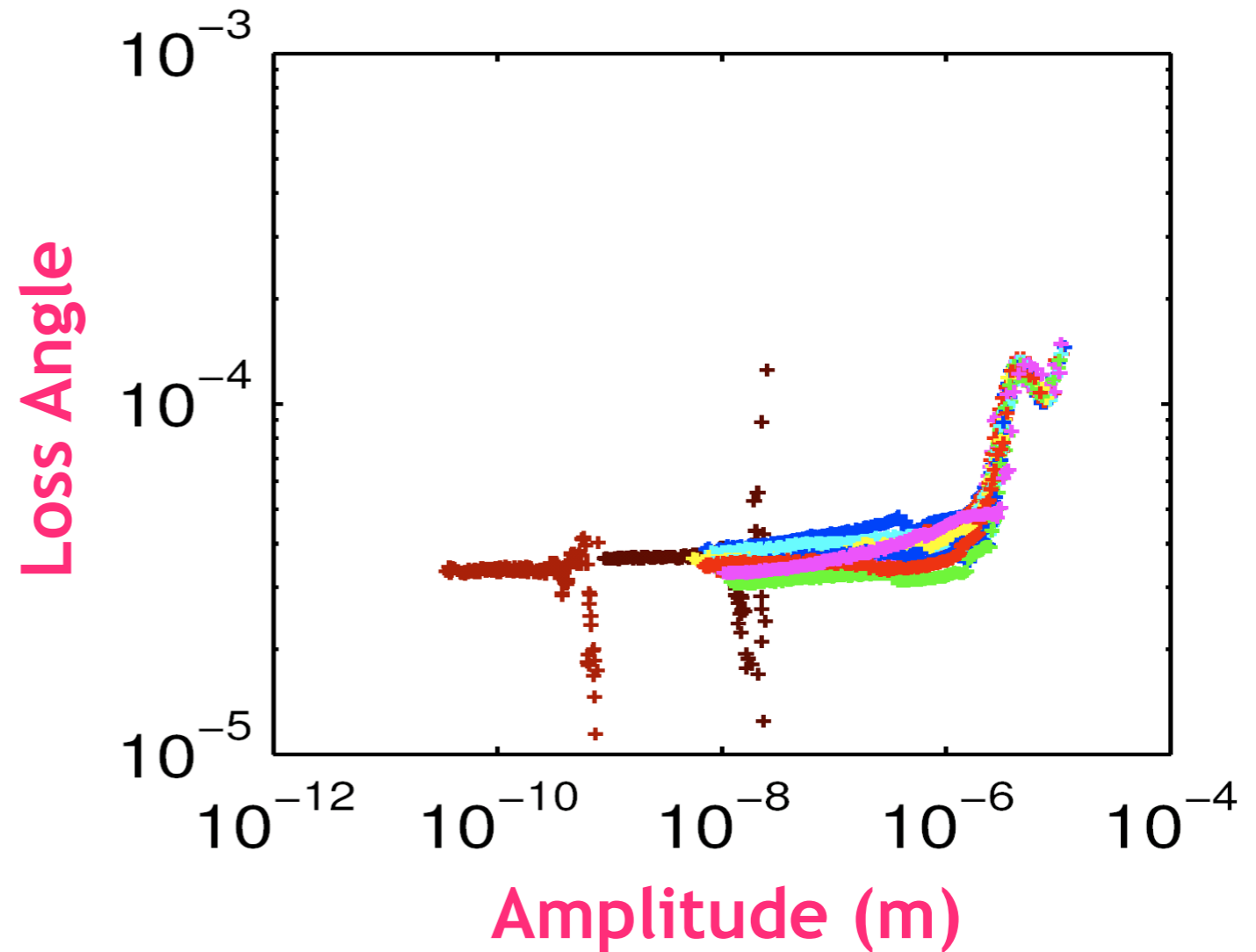
Amplitude Dependence of Loss Angle

Clamp Friction losses

- Rubbing friction at high amplitude
 - Higher loss
 - Amplitude & frequency dependent
- Partial slip (slip-stick) at lower amplitude
 - Nearly frequency independent
 - Degrades with multiple measurements

Proper Clamping

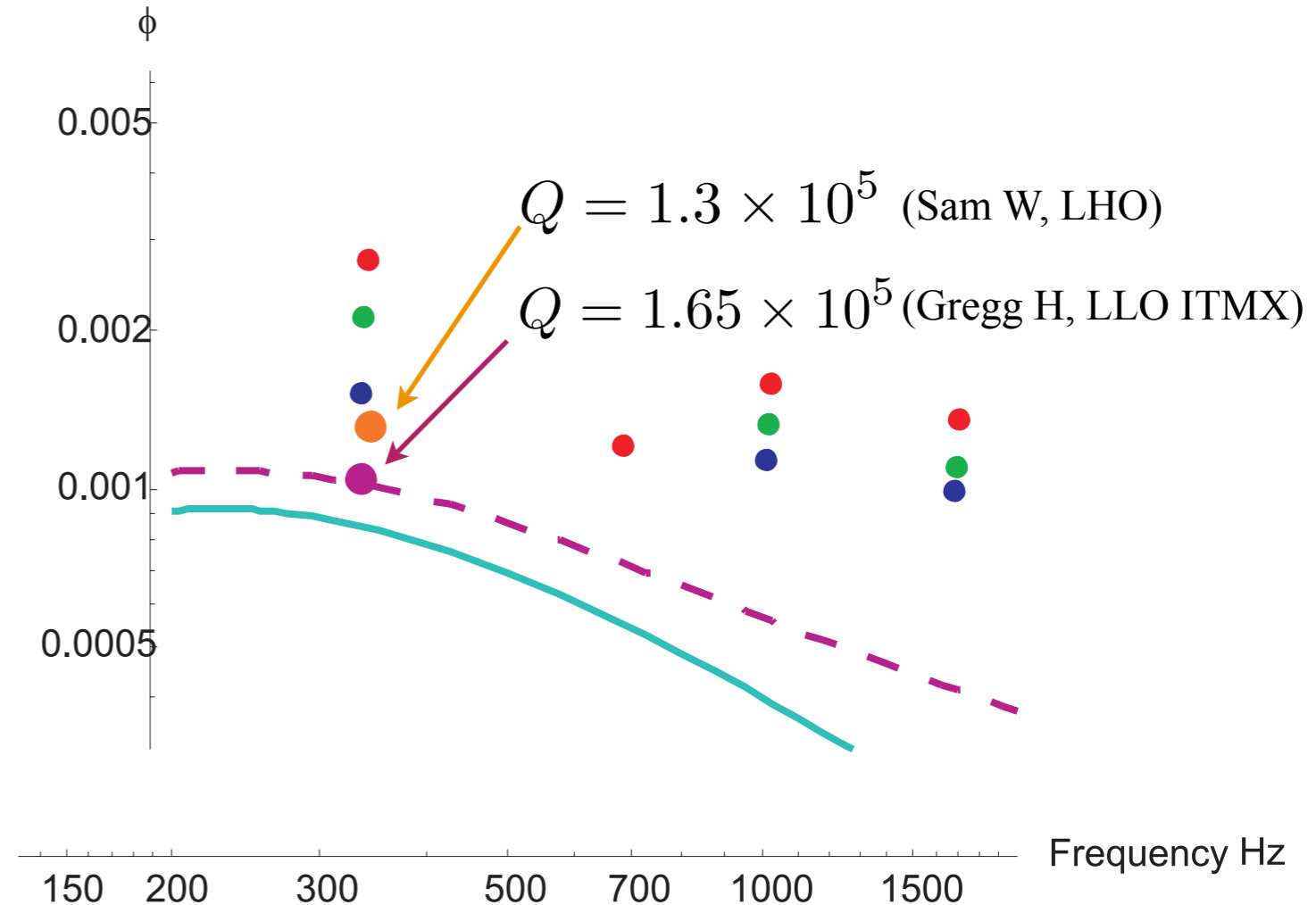
- Clamp should not cause plastic deformation in clamp or fiber
 - Repeatability
 - No time variability
- No Clamp slippage
 - Hardened uniform clamping (collet)
 - Taper fiber ends



Data from Gretarsson thesis
 W wire in Al clamps. Loss is 100 x internal loss.

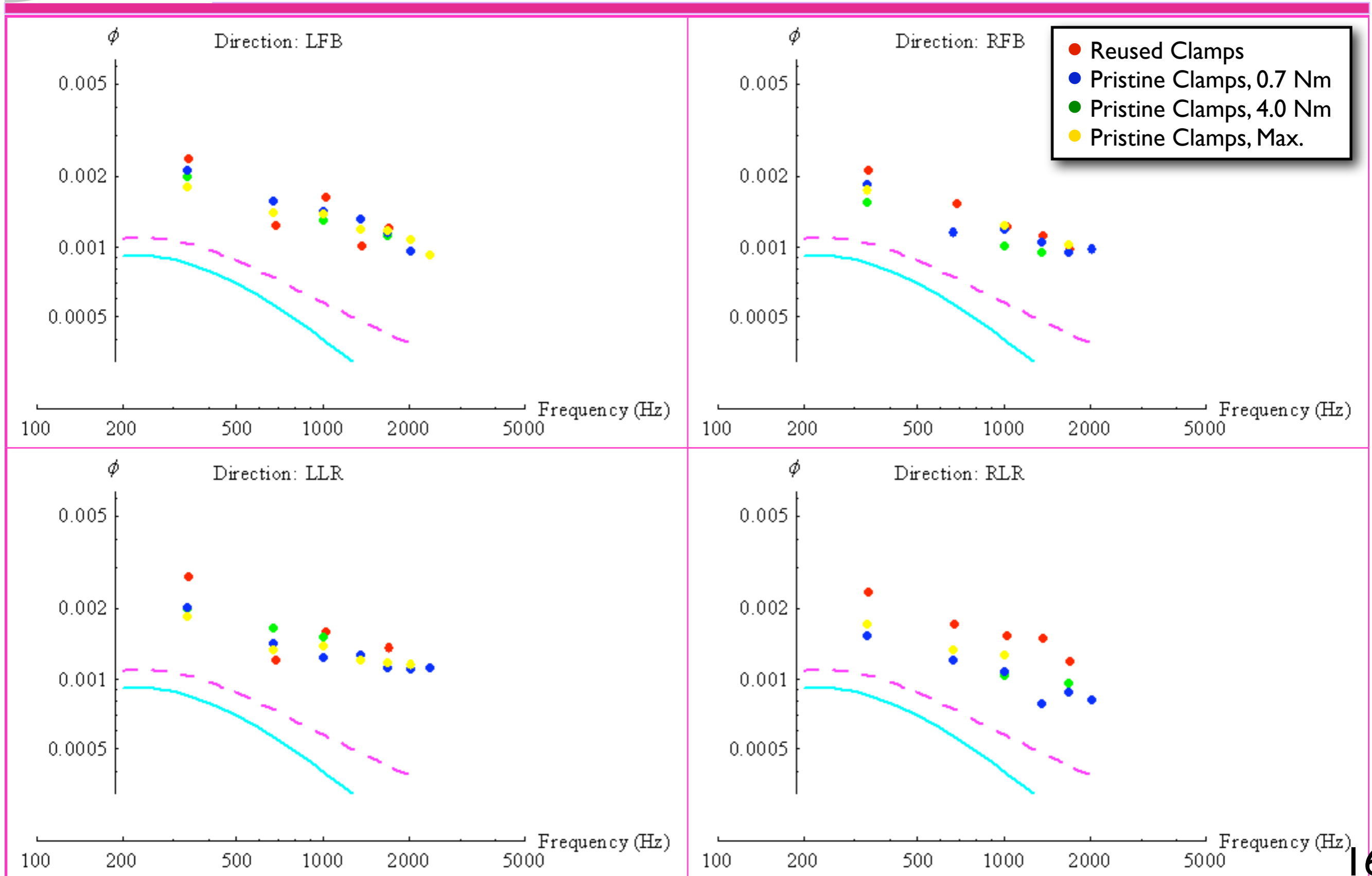
Measurement of Violin Modes at Sites

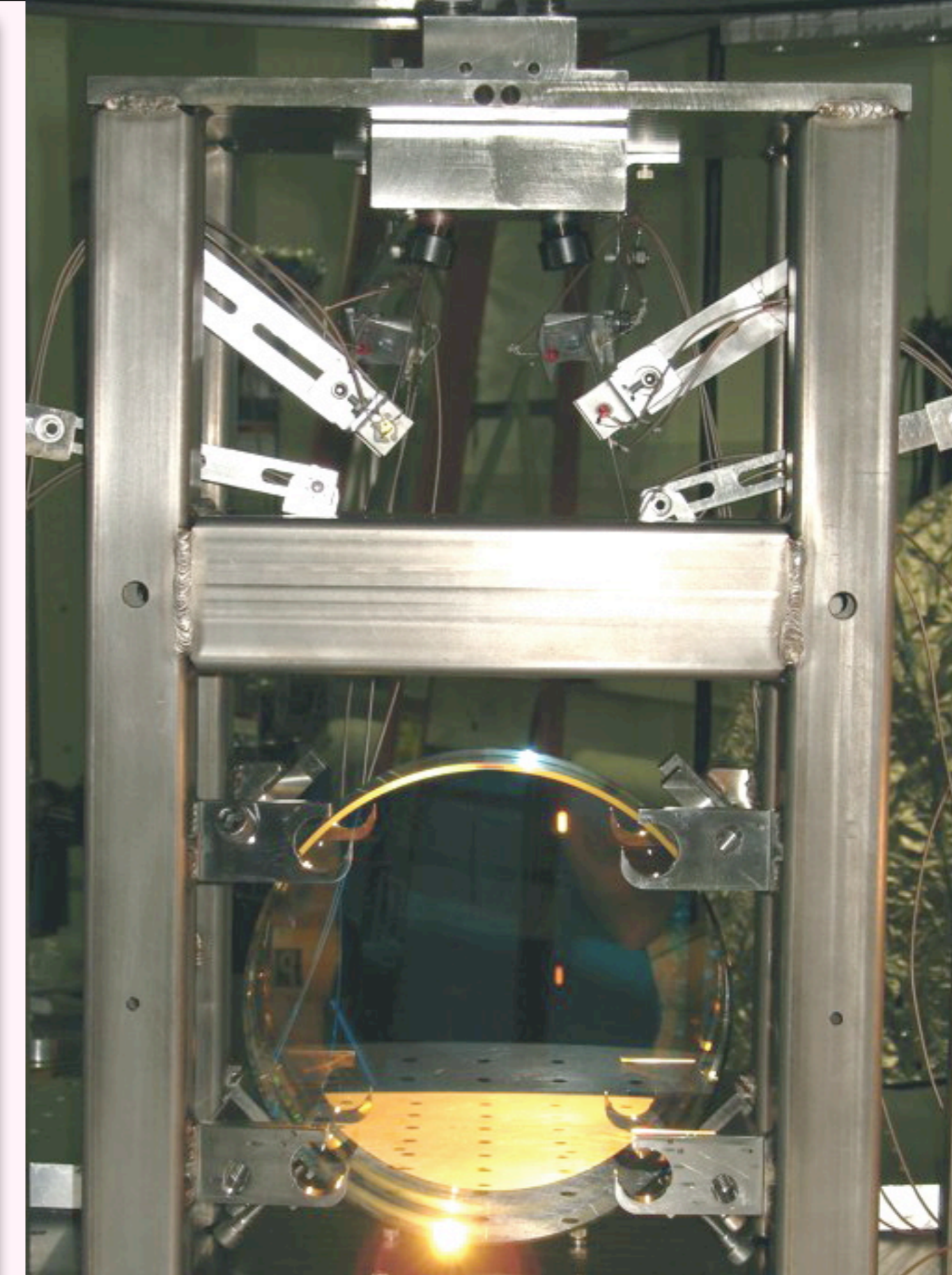
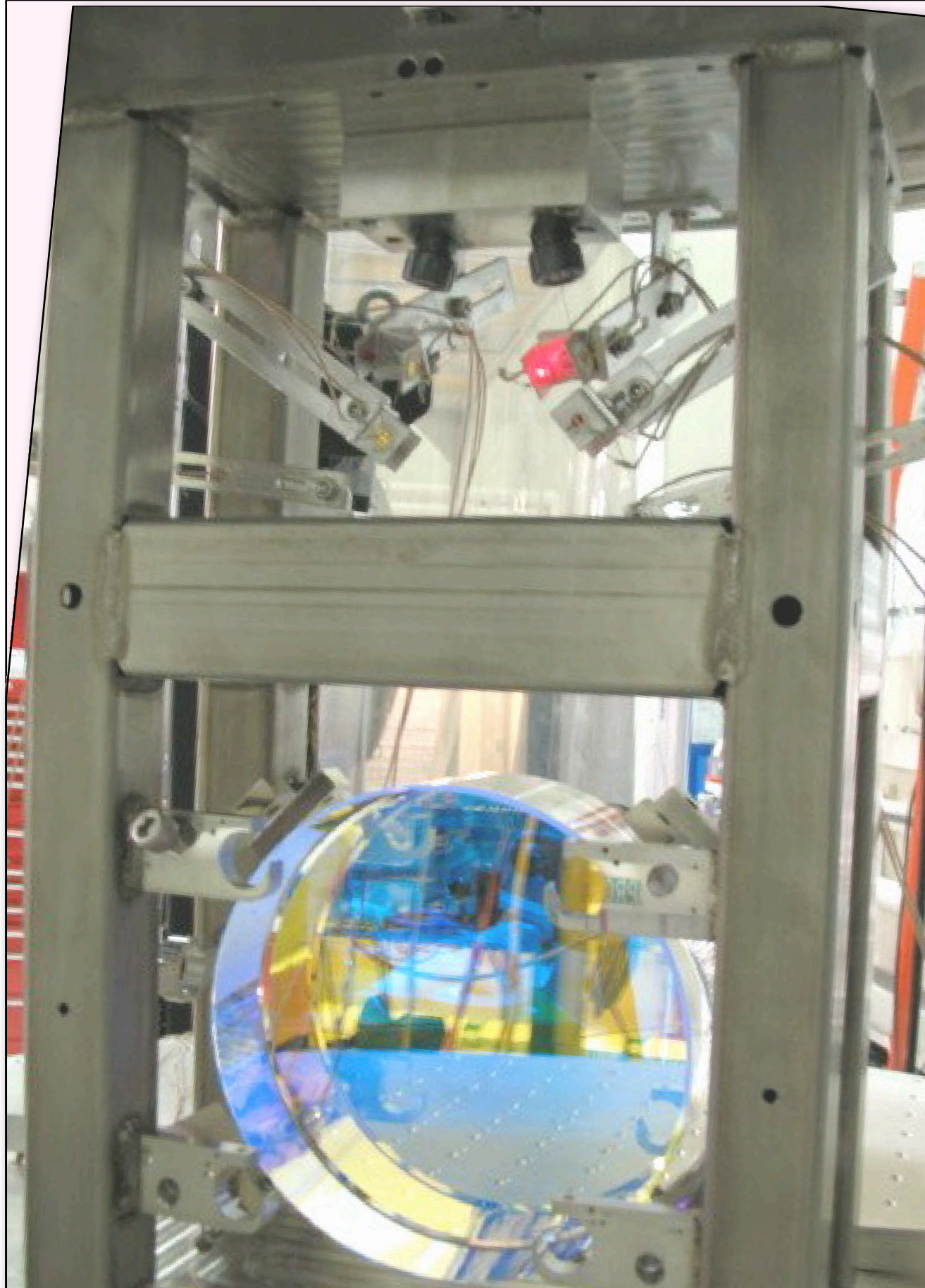
- Measured Q 's are typically lower than the value expected if the loss was only due to the intrinsic loss in the wire (thermoelastic damping and structural loss)
- Mysterious changes in Q
 - Consistent within lock stretch
 - Not consistent between optics
 - Feedback effects? No dependence on optical power
 - Recoil Damping?
 - Clamp Losses?



Violin Mode Q 's are inconsistent. Best Q consistent with fundamental mechanical loss.

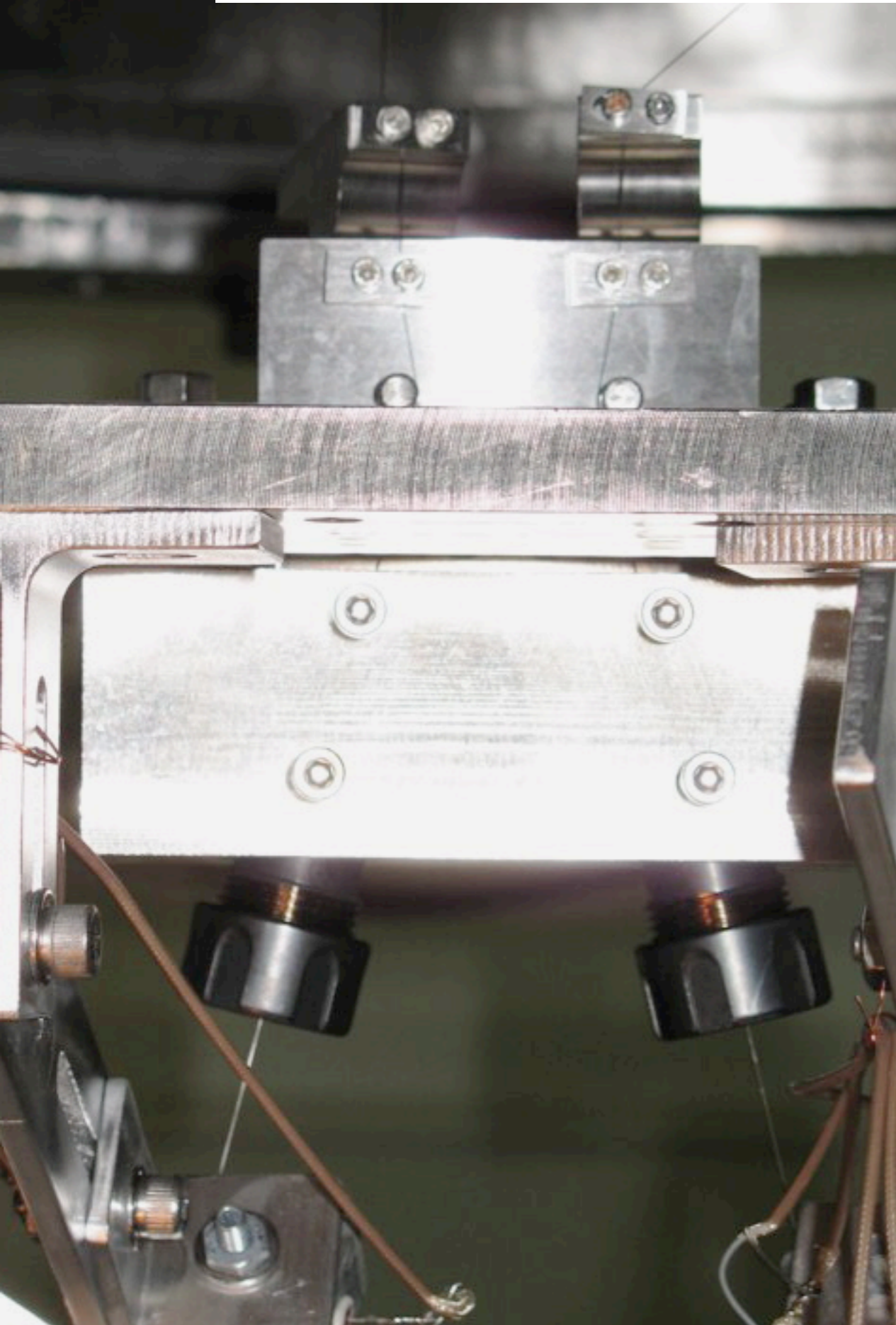
Violin Mode: Pristine Clamp





New DNA Collet Suspension

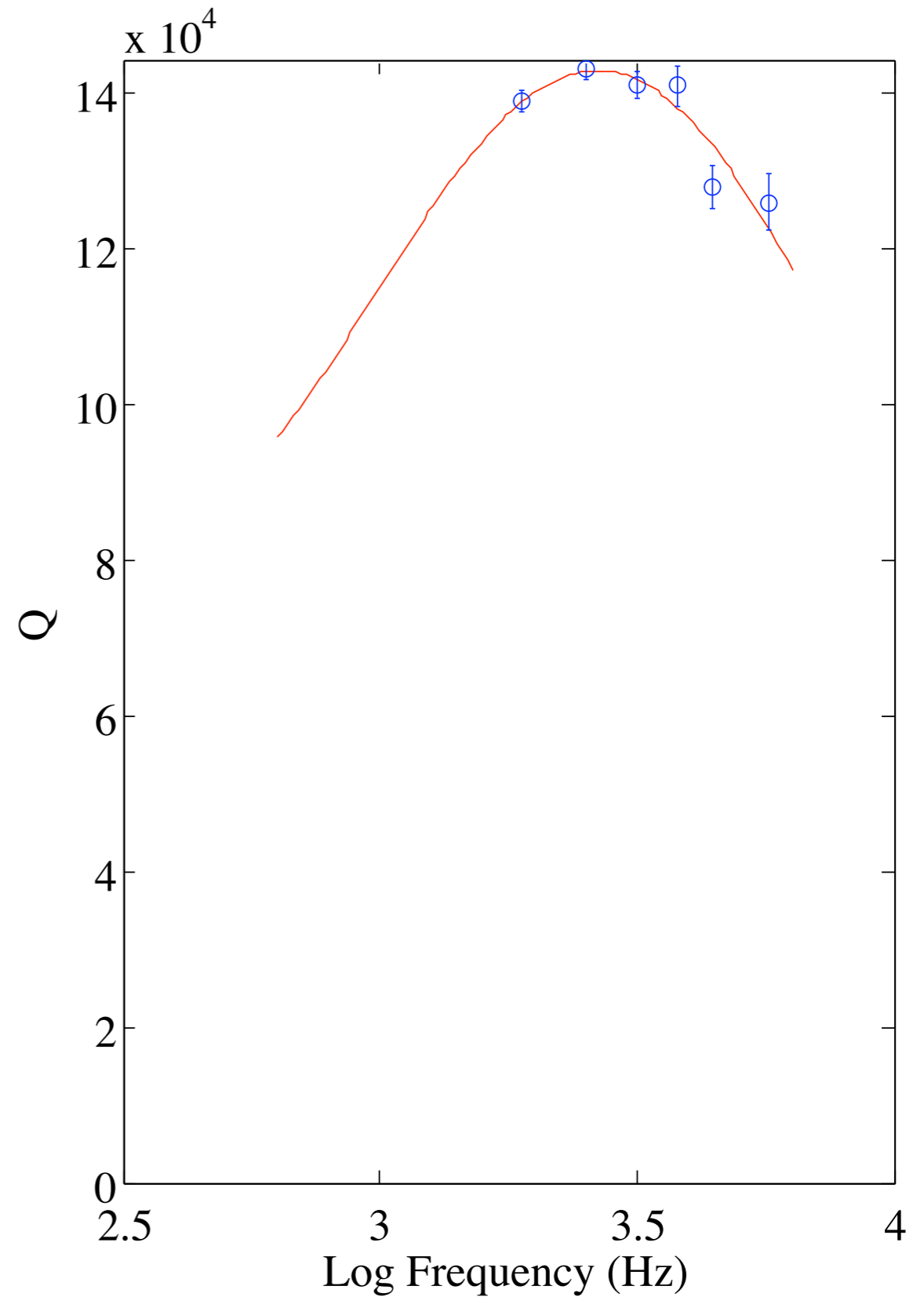
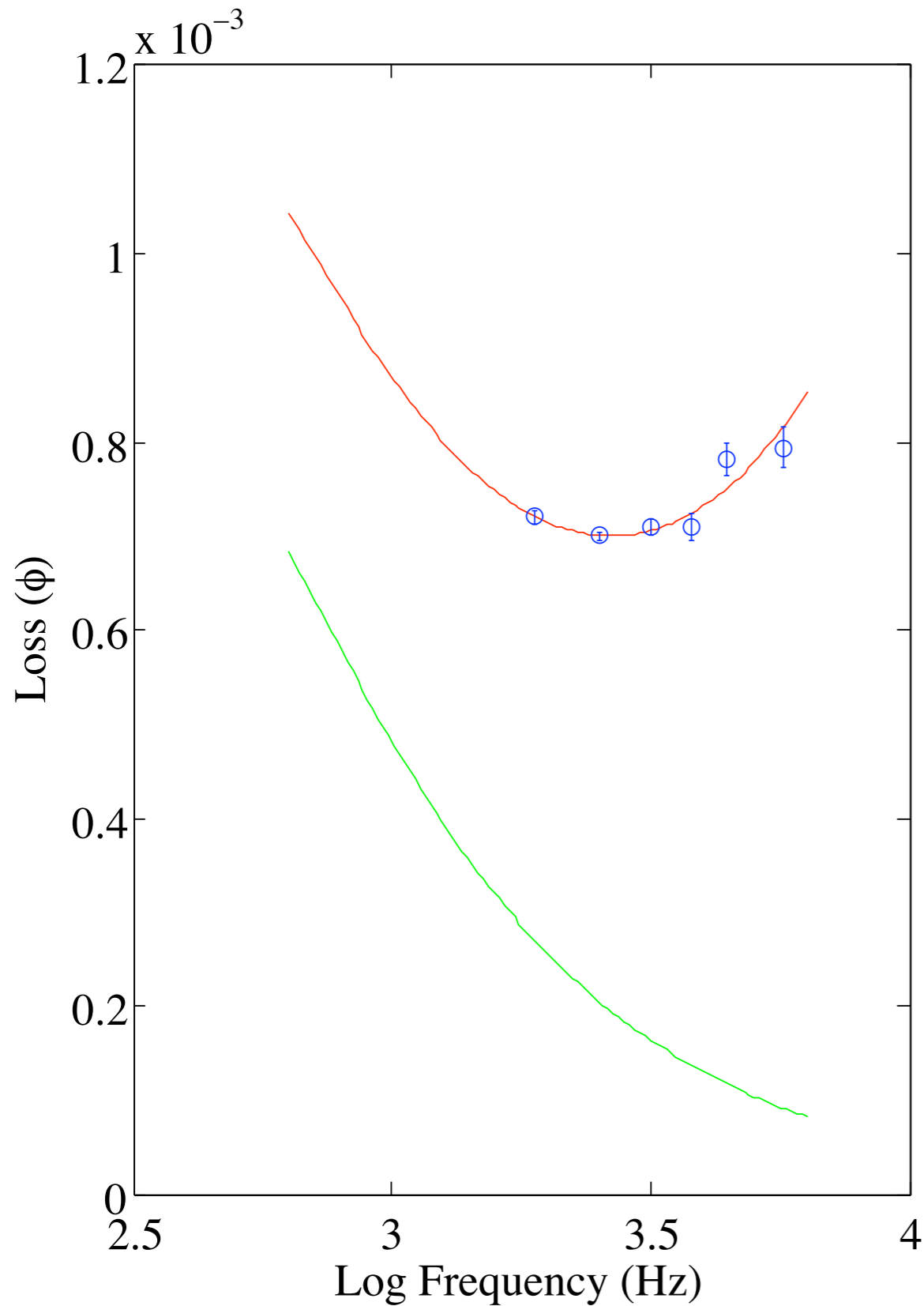
New DNA Collet Suspension



- Spring collets with bore of 0.2–0.3 mm
- Clamping is symmetric
- Hardened Tool Steel has no plastic deformation
- Clamping should be **Repeatable!**



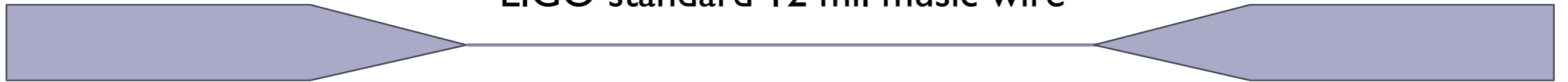
Violin Mode: Collet Clamp



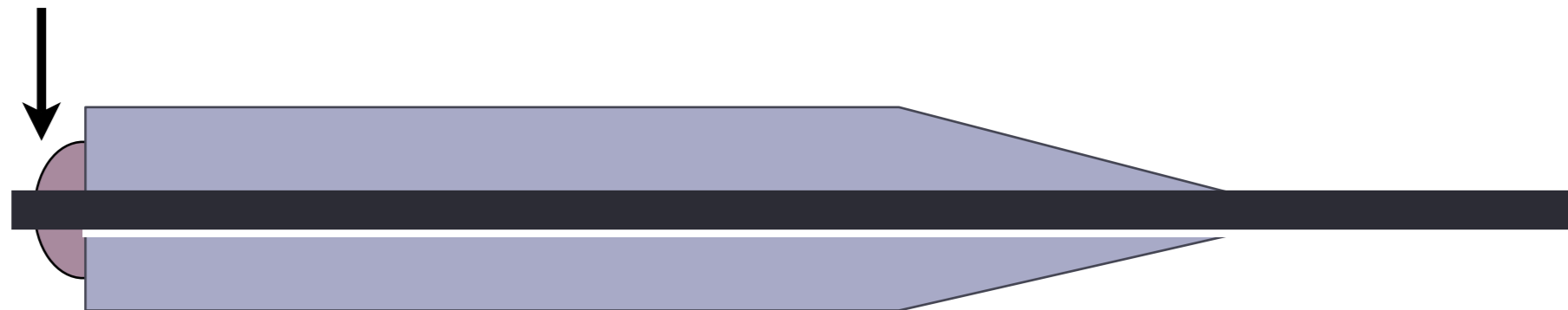
Tapered Wire Suspension

Tapered Rod of similar temper steel

LIGO standard 12 mil music wire



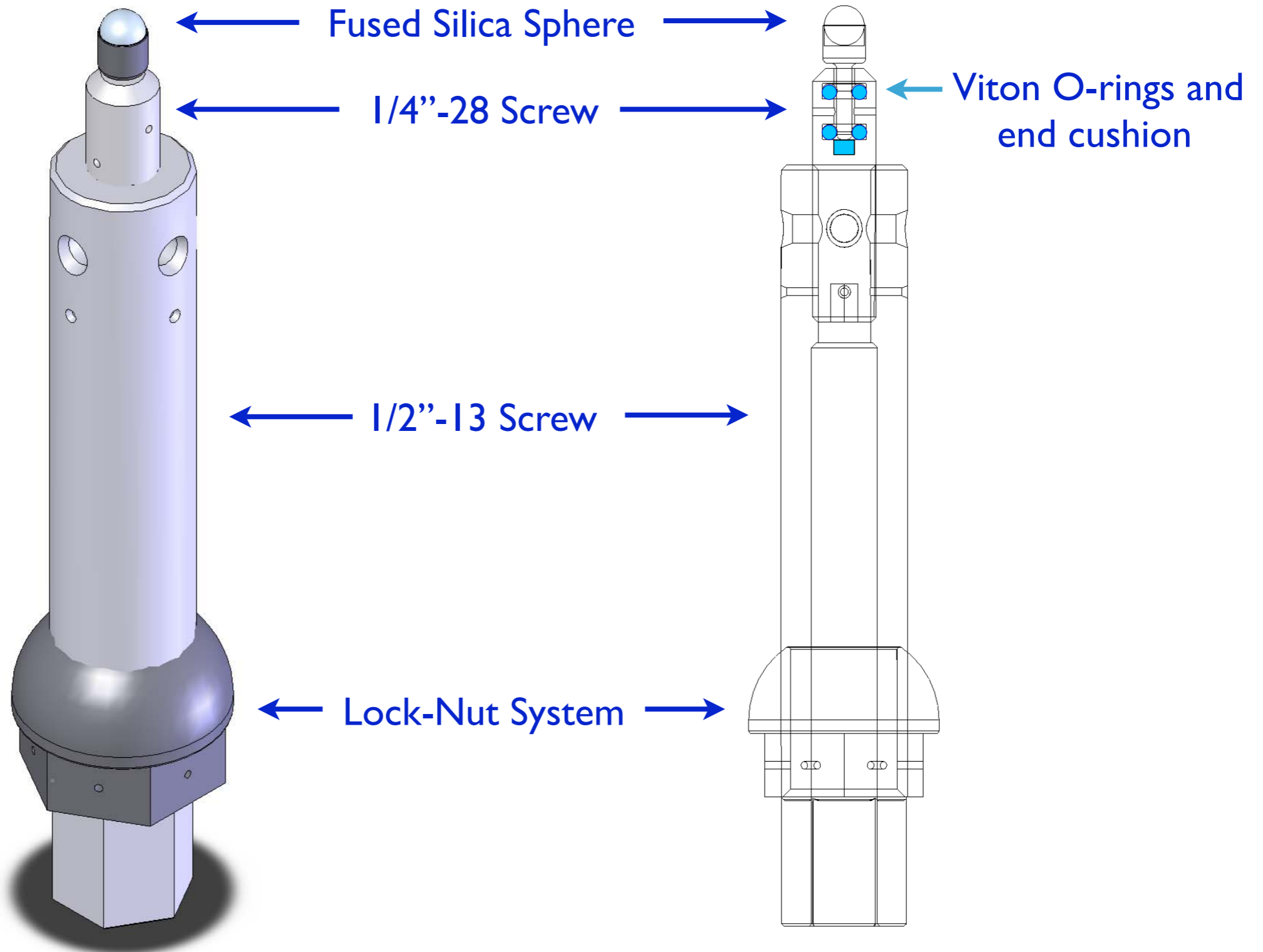
Assembled using shrink fit with end spot weld



New Directions

- Test wire collets, without galling
- Test tapered wires held in collets
- Test Ribbons
- Test for and correct friction at the standoff (HARD)
- Investigate other materials
- Tests for recoil damping (Easy test. Unlikely source of problem.)
- Use apparatus to test new earthquake stops

New Earthquake Stops



LIGO-Virgo Thermal Noise Meeting

Saturday, 7 October 2006 at Virgo Observatory

LIGO Speakers

- **Jim Hough** – *Future research directions*
- **Sheila Rowan** – *Next generation materials*
- **Gregg Harry** – *Coating thermal noise*
- **Eric Black** – *Thermal Noise Interferometer*
- **Stuart Reid** – *Coating and bonding thermal noise*
- **Andri Gretarsson** – *Thermorefractive noise*
- **Alastair Heptonstall** – *Silica suspensions*
- **Vincenzo Galdi** – *Genetic algorithms*
- **Juir Agresti** – *Mesa Beams*
- **Steve Penn** – *Silica substrates*

The End

Noise Budget

Estimate for thermal noise assuming the suspension noise for all test mass is the same as our result.

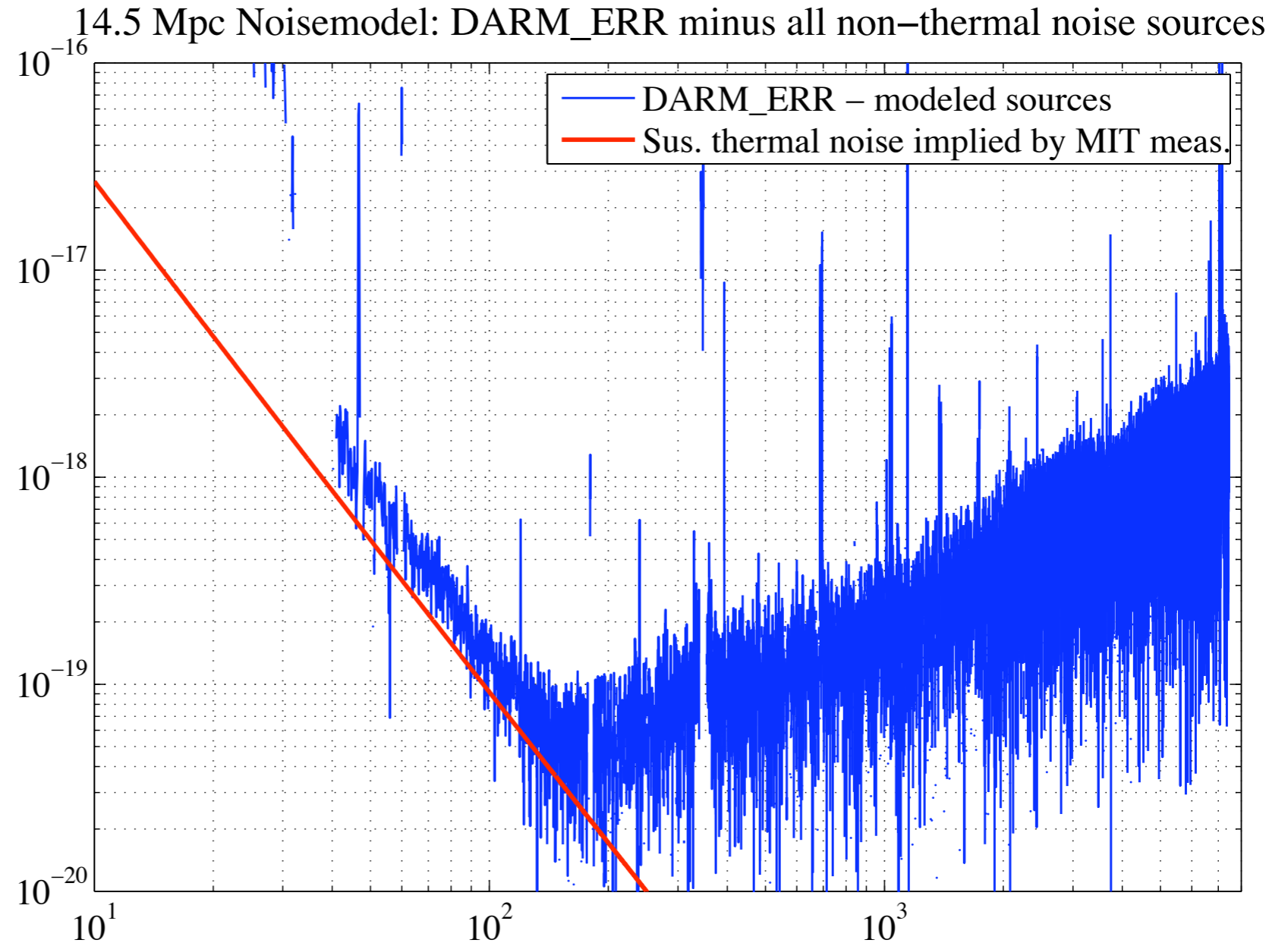
$$\phi = 2 \times 10^{-3}$$

Worst loss seen from measurements of violin mode at the sites is

$$\phi = 1.1 \times 10^{-2}$$

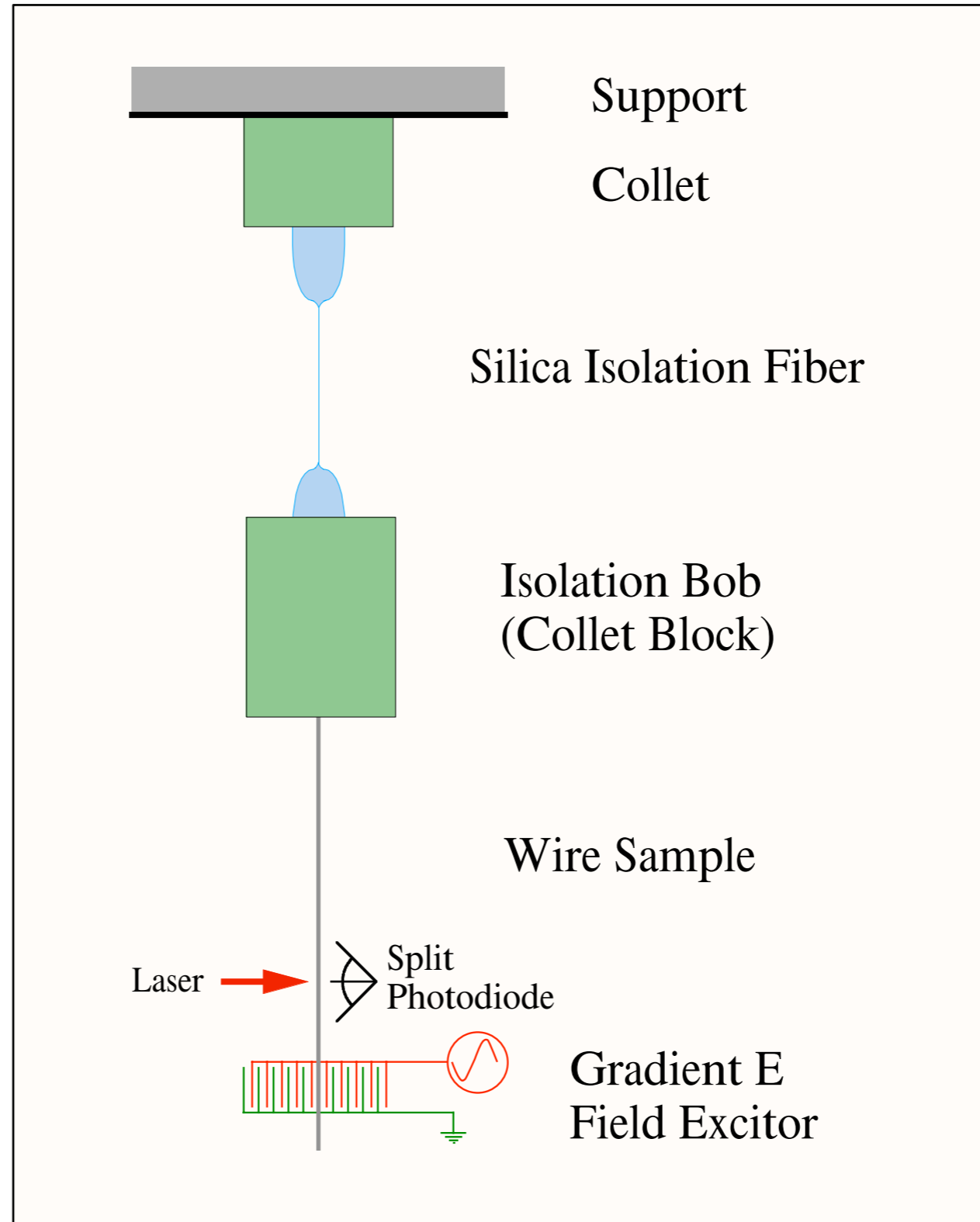
Best fit to observed 40-100 Hz noise is

$$\phi \approx 7 \times 10^{-3}$$



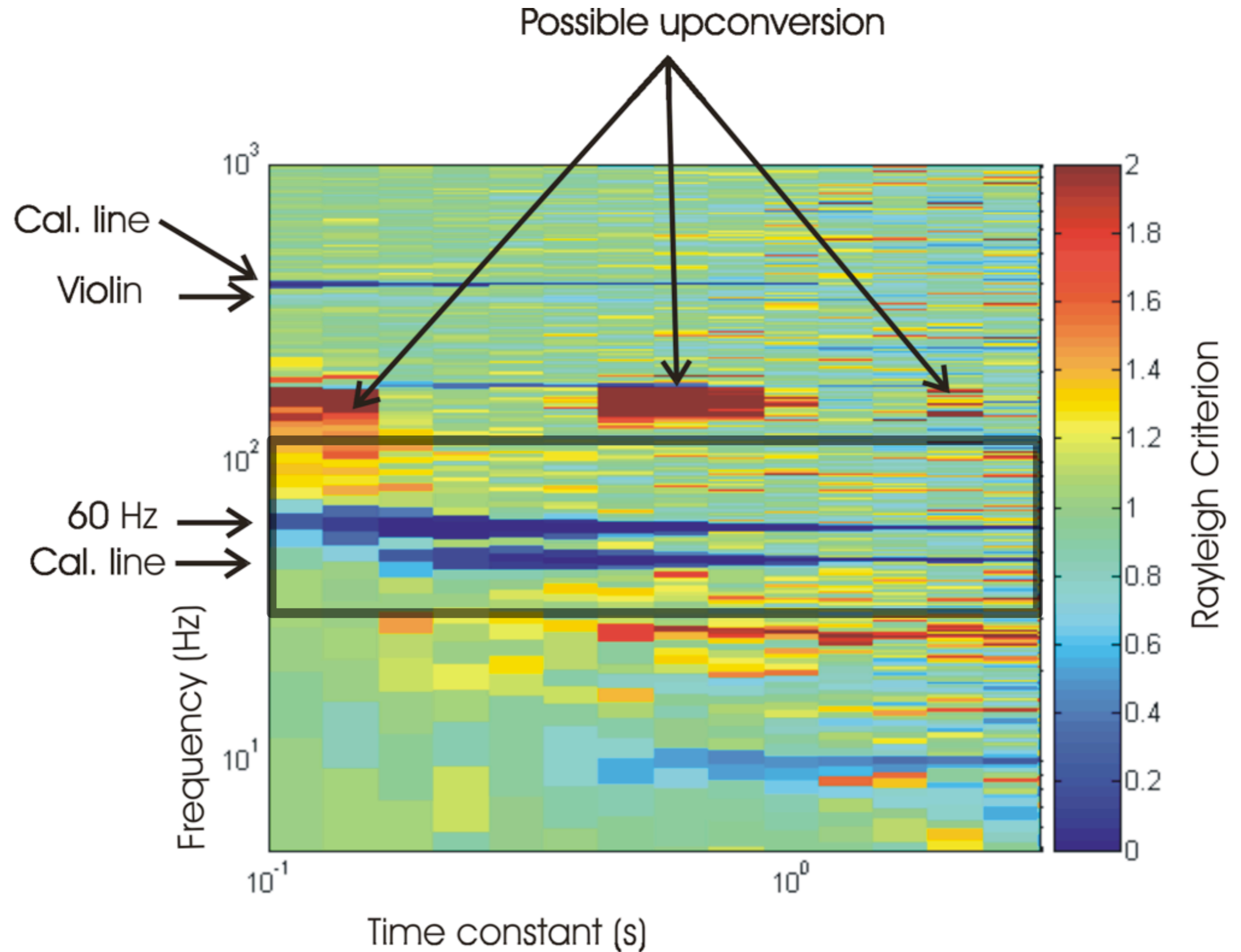
Strong indications that Suspension thermal noise is a major contributor to the 40–100 Hz excess noise.

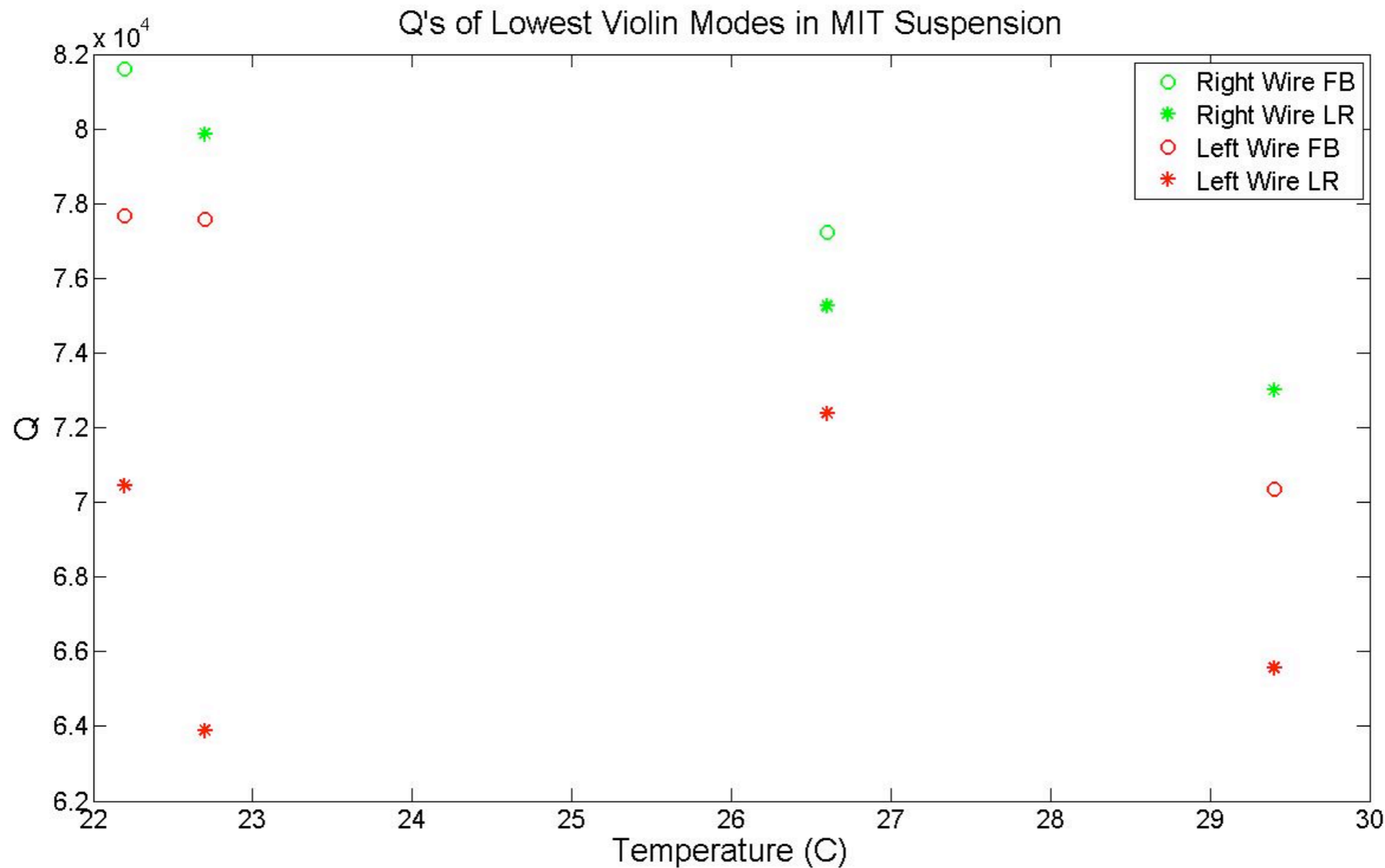
Mechanical Loss in Wires



Test for NonGaussian Noise

Rayleigh Monitor indicates no major departure from Gaussian noise in 40–100 Hz region.





- Does not seem to be a correlation with temperature
- Calls into question recoil damping model to explain Q variation at sites



- Measurements on spare cage at ERAU
- Transfer function on top plate
- Compare frequencies with model and measurements at Caltech
- Verify temperature dependance
- Will attempt to modify frequency structure by clamping mass on cage

