



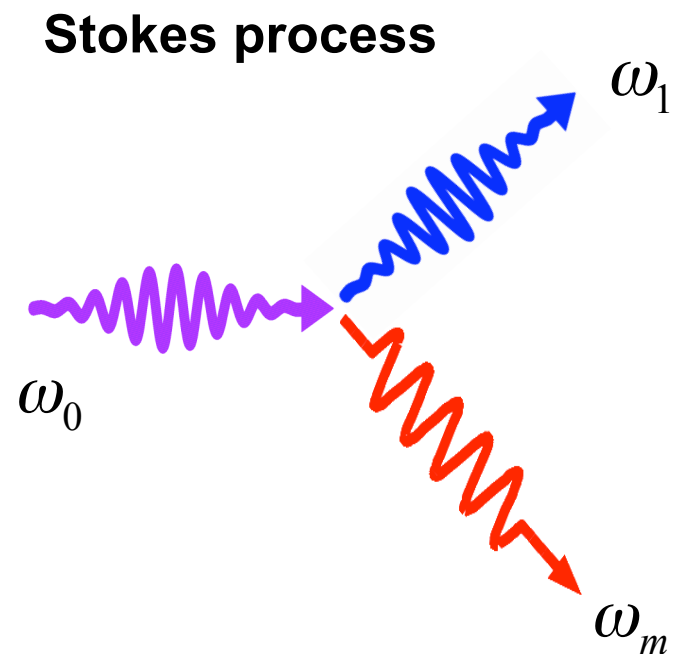
TNI Progress and Status:
Ring Dampers and Aperiodic Coatings

Eric D. Black
LSC Meeting
Aug. 16, 2006

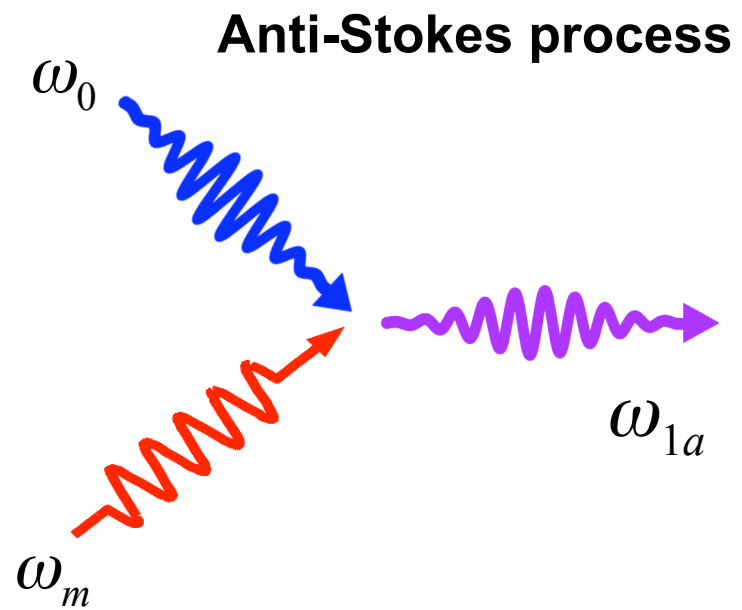
Kenneth Libbrecht, Dennis Coyne
Grad students: Akira Villar, Greg Ogin
SURF: Michael Goldman (Amherst), Matt Seaberg (Bethel),
Cacey Stevens (Southern), Antonella Iuorio (Benevento)



Acousto-Optic Coupling

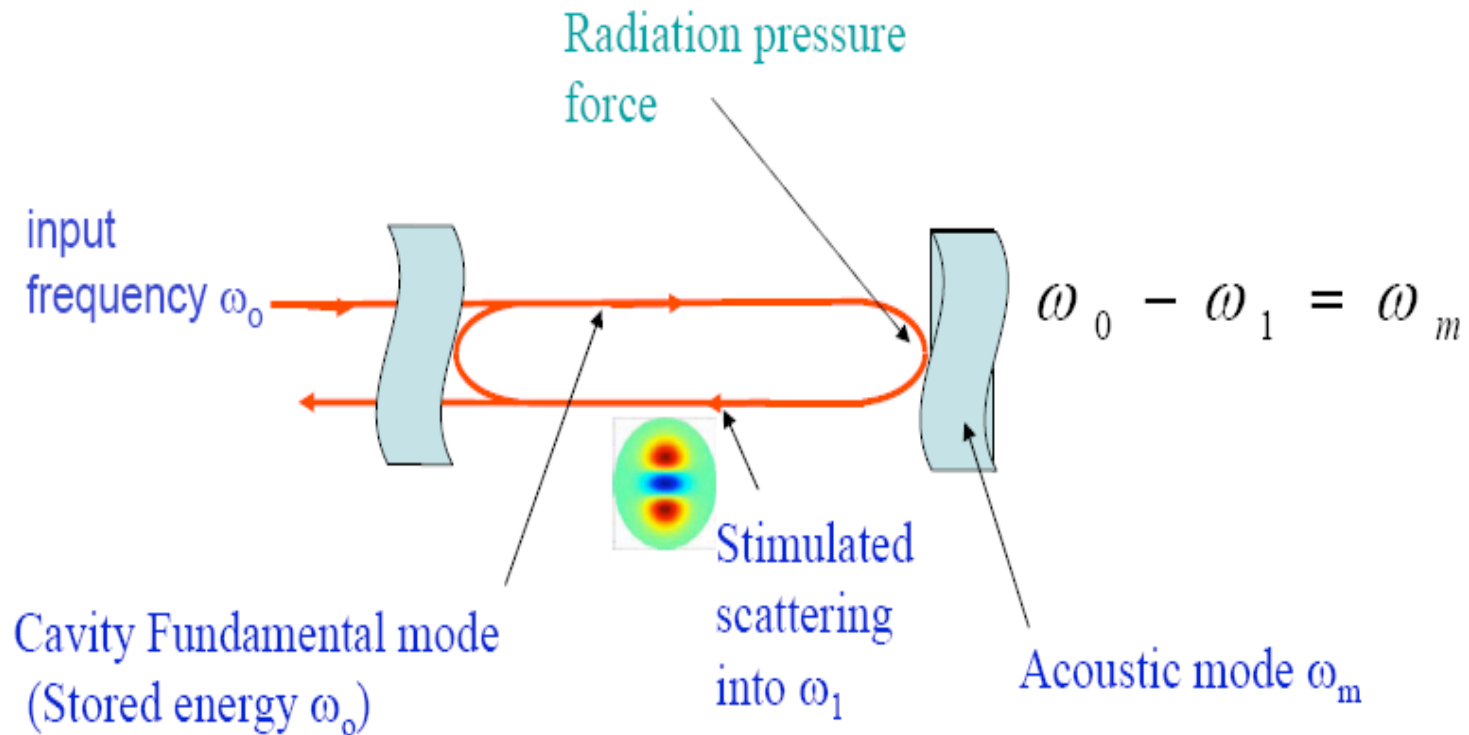


$$\omega_1 = \omega_0 - \omega_m$$



$$\omega_{1a} = \omega_0 + \omega_m$$

Parametric Instability





Condition for Instability

$$R \approx \frac{2PQ_m}{McL\omega_m^2} \left(\frac{Q_1\Lambda_1}{1 + \Delta\omega_1^2 / \delta_1^2} - \frac{Q_{1a}\Lambda_{1a}}{1 + \Delta\omega_{1a}^2 / \delta_{1a}^2} \right) > 1$$

Stokes Mode

Anti-Stokes mode

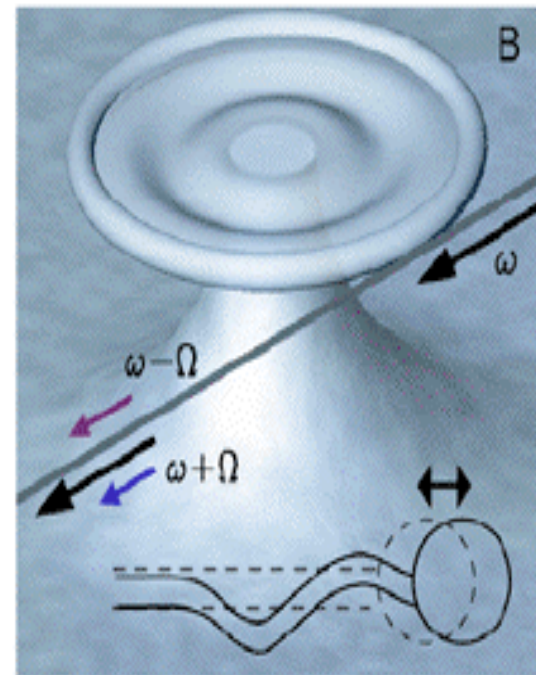
Ju, et al. G050325-00 who got it from
Braginsky, et al. Phys. Lett. A 305, 111 (2002)



Experimental Verification

- Parametric *damping* (anti-Stokes) studied by Blair's group
 - PRL 74, 1908-1911 (1995).
- Effect observed in micro-cavities by Vahala group
 - Phys. Rev. Lett. 95, 033901 (2005)
- Also by Mavalvala in a suspended mirror cavity at MIT
 - LIGO-P050045-00-R (Oct. 27, 2005)

Microtoroidal optical resonator



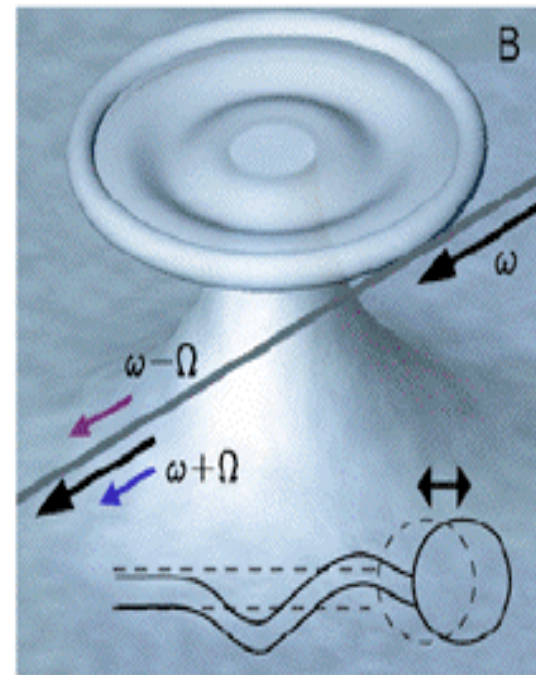


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How do we eliminate parametric oscillations in AdLIGO without spoiling our low thermal noise floor?

Microtoroidal optical resonator





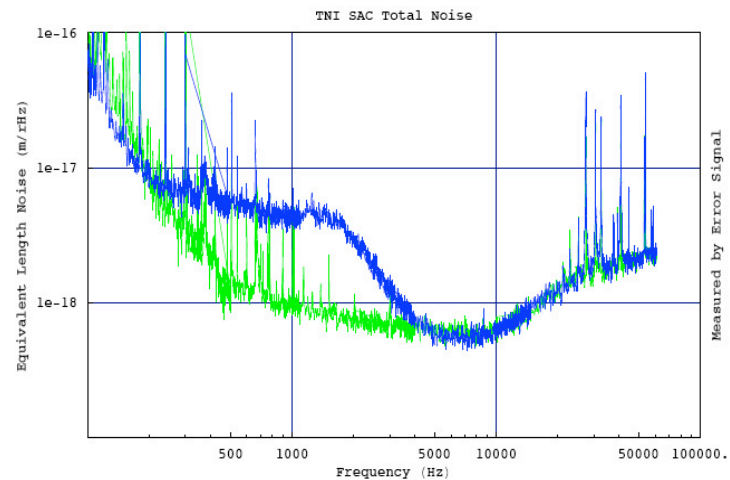
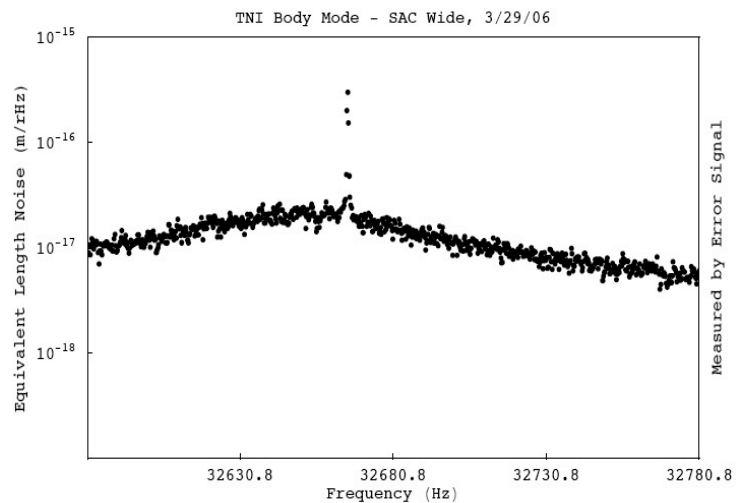
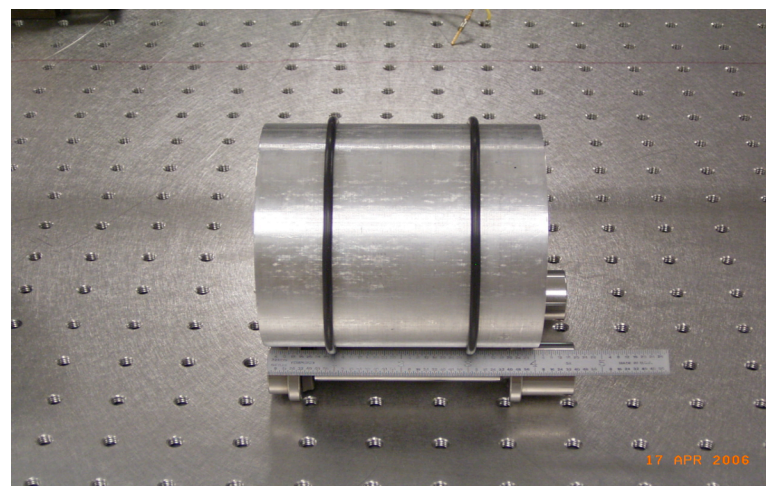
Possible Solutions

- Active feedback
- Thermal detuning
- Q reduction



Buna O-Rings

- Buna, 1/8" thick, undersized diameter (3.25")
- Q reduction is too large to measure by ringdown: can't excite modes
- Substantial increase in the noise floor from 200Hz to ~4kHz
- Still thermal noise limited above 5kHz

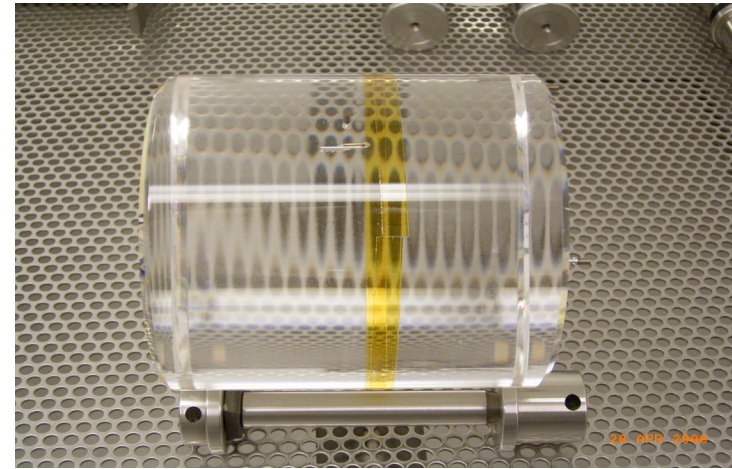


G060448-00-Z

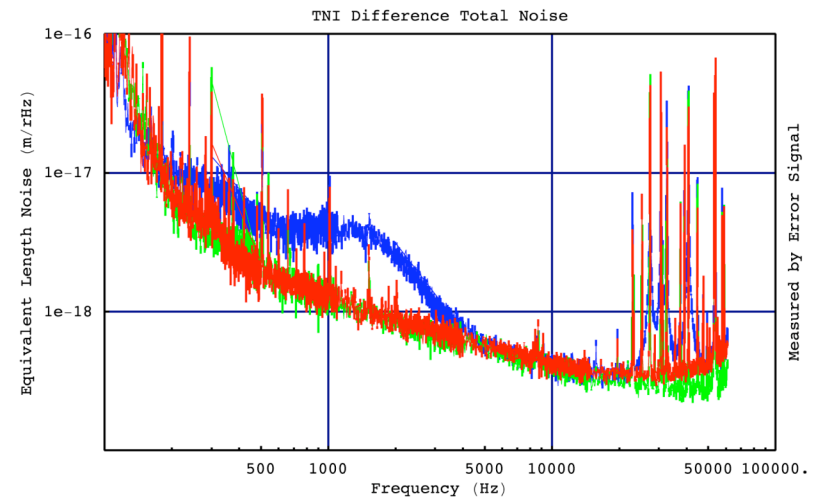


Kapton Tape

- Essentially massless, to avoid “waving” modes seen with buna.
- Lossy strip closely approximates models of Gras, Blair, et al.
- No observed increase in the noise floor
- Q reductions range from factor of 2 to none at all



No ring damper
Buna o-ring
Kapton tape





“Waving” modes of rings

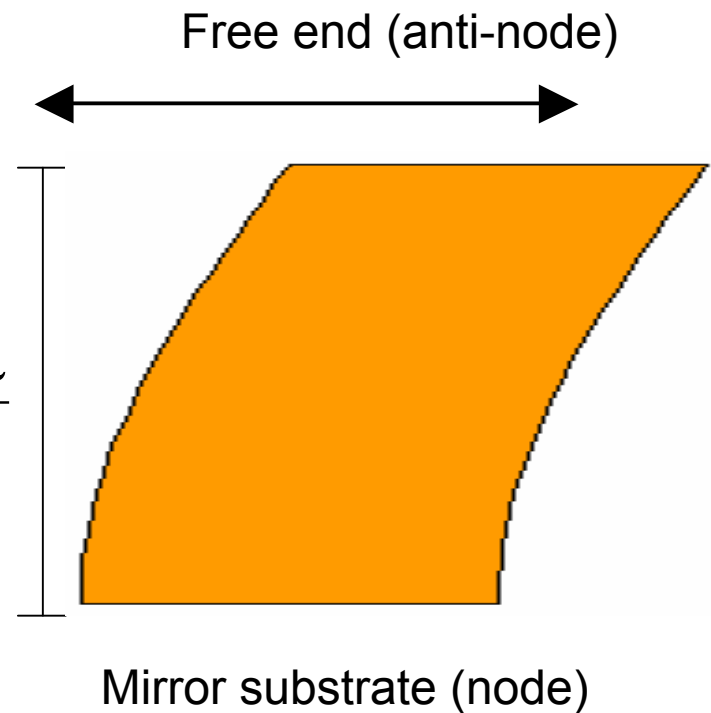
Shear wave equation (transverse waves)

$$\frac{\partial^2 y}{\partial x^2} = \frac{\rho}{G} \frac{\partial^2 y}{\partial t^2}$$

$$d = \frac{\lambda}{4}$$

→ wave speed $v = \sqrt{\frac{G}{\rho}}$

$$f_n = \frac{2n-1}{4d} \sqrt{\frac{G}{\rho}}$$

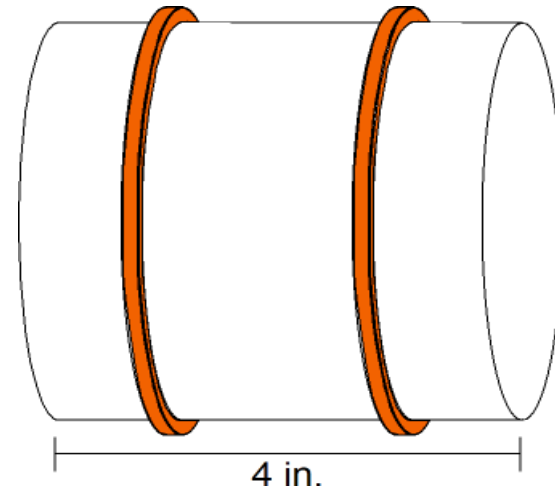


Predicts fundamental $f = 145$ kHz for 4 mm copper ring
 - Well out of thermal noise region



Copper rings

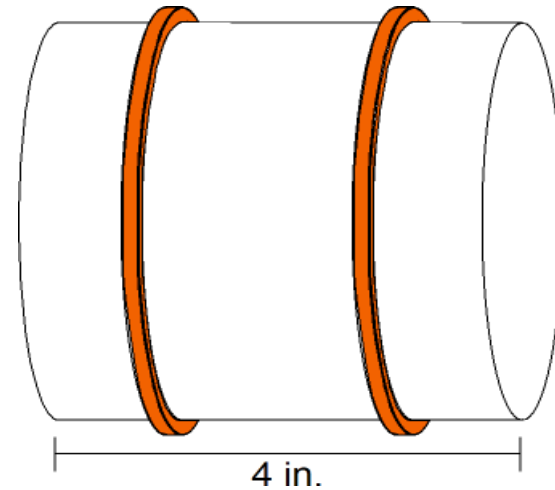
- Buna, kapton results tell us
 - Need mass to damp mirror Q's
 - Need “waving” mode well above the measurement band
- Ultimate plan was to use monolithic rings, expanded by heating for installation
- Use screw tension for prototypes





Copper rings

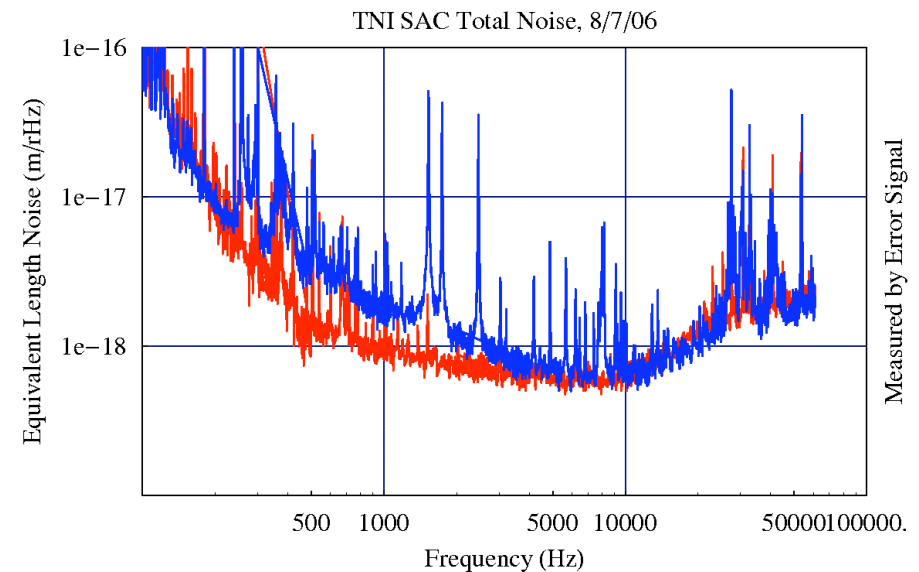
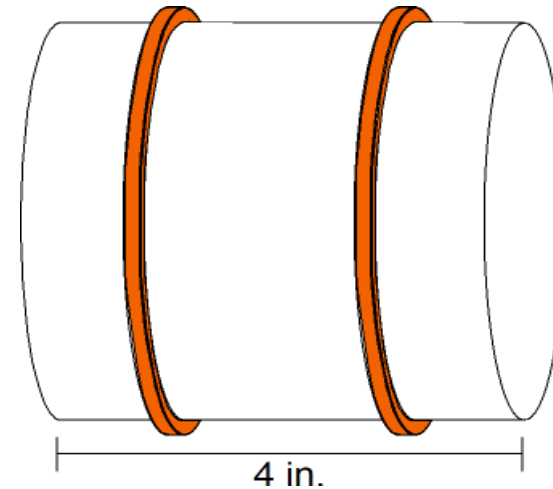
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- Q's were reduced below our ability to excite the modes, as with buna.
- Noise floor increases, showing both new modes and additional broadband noise.





Aperiodic Coatings

- Goal: reduce high-loss material in HR coating by varying layer thickness, while preserving phase relationship for reflection
- Collaboration with
 - Vincenzo Galdi and Innocenzo Pinto at Benevento (coating design),
 - LMA at Lyon (fabrication and loss measurements), and
 - Sheila Rowan at Glasgow (loss measurements)
- Gains from and design of optimization depend on how different the loss angles are between high- and low-index materials.

$$1 \leq \phi_{Ti-Ta_2O_5} / \phi_{SiO_2} \leq 5$$

- We have well-confirmed measurements of $\phi_{Ti-Ta_2O_5}$, but not for ϕ_{SiO_2}
- Once we have a firm number for ϕ_{SiO_2} design can proceed.
- Once we have a design, LMA will fabricate a coating, and the TNI will measure its noise.