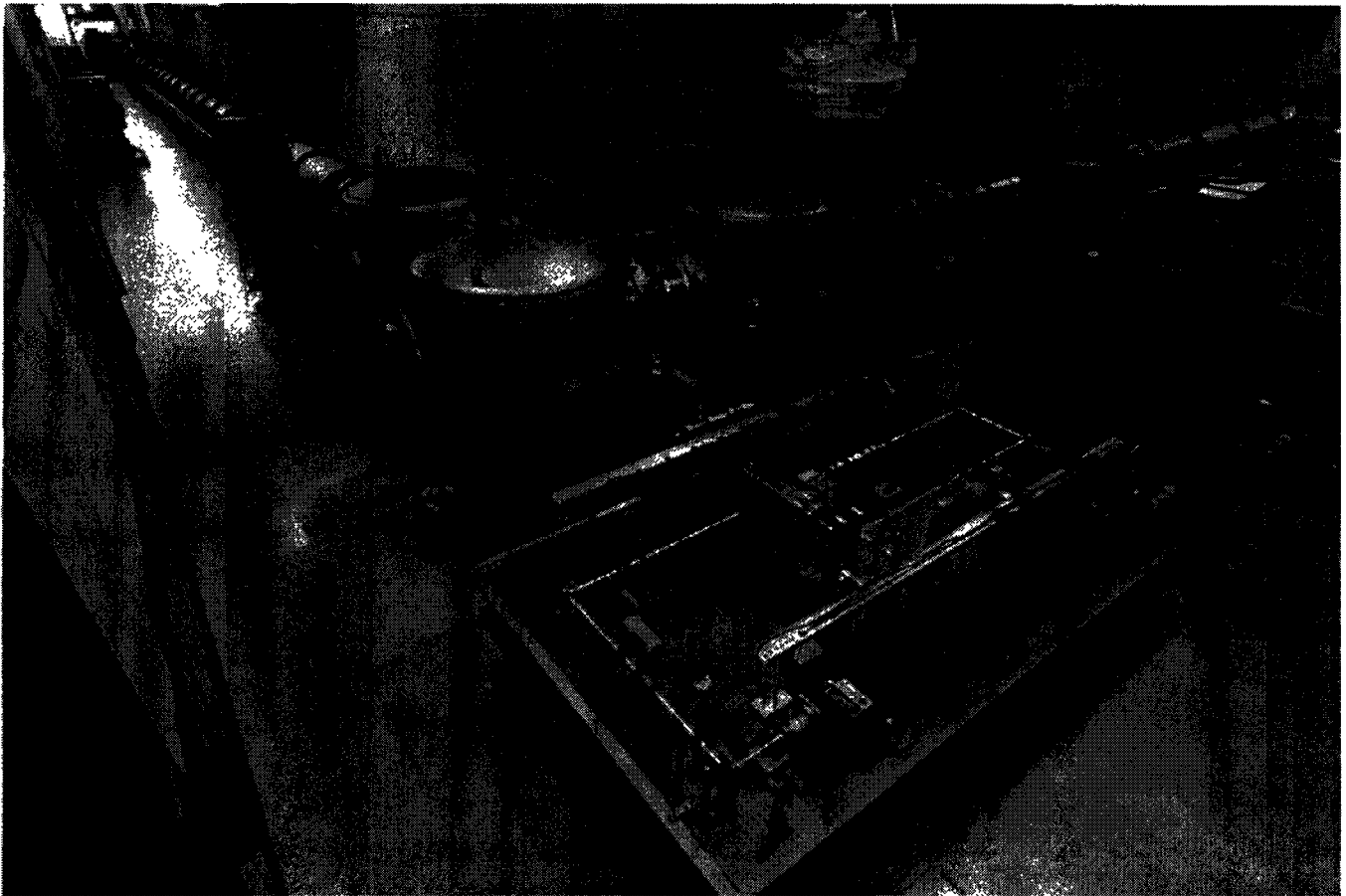


Recent Research on the LIGO 40m Interferometer

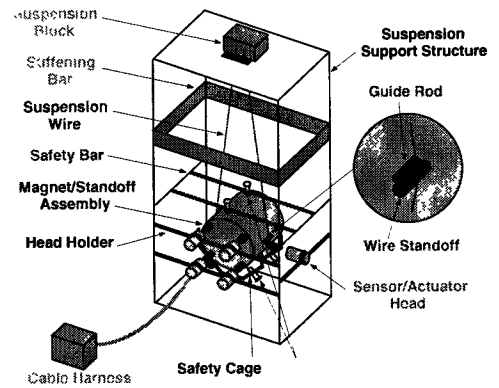


**Seiji Kawamura
(LIGO, Caltech)**

Recent Developments

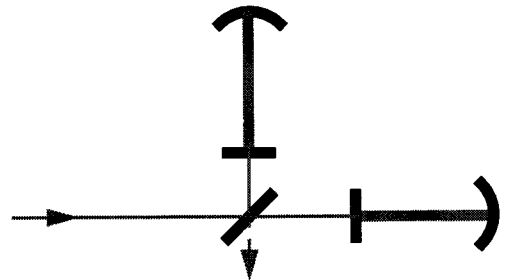
- New Suspension Prototype

›› Installed and tested



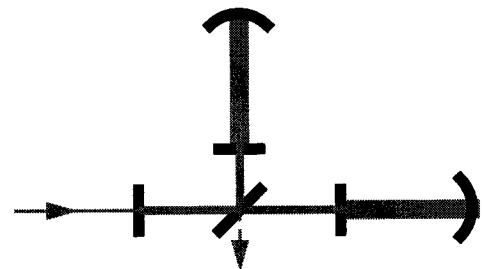
- Recombination

›› Completed



- Recycling

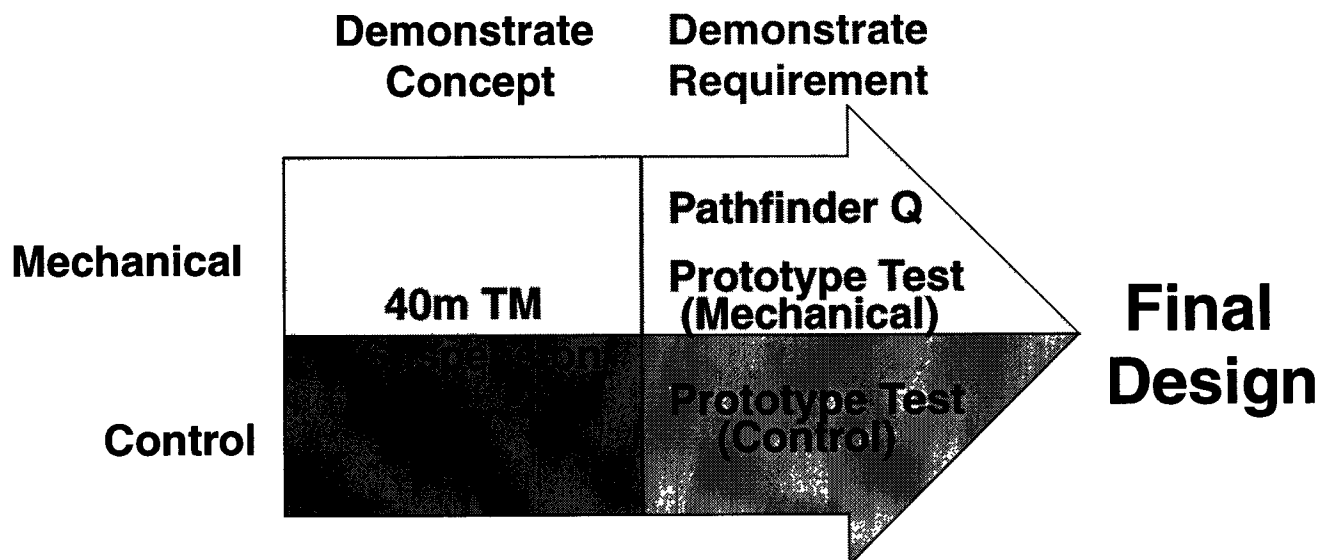
›› Started



Significance of 40m TM Suspension Test

LIGO Large Optics Suspension

(Test Mass, Beamsplitter, Recycling Mirror, Folding Mirror)

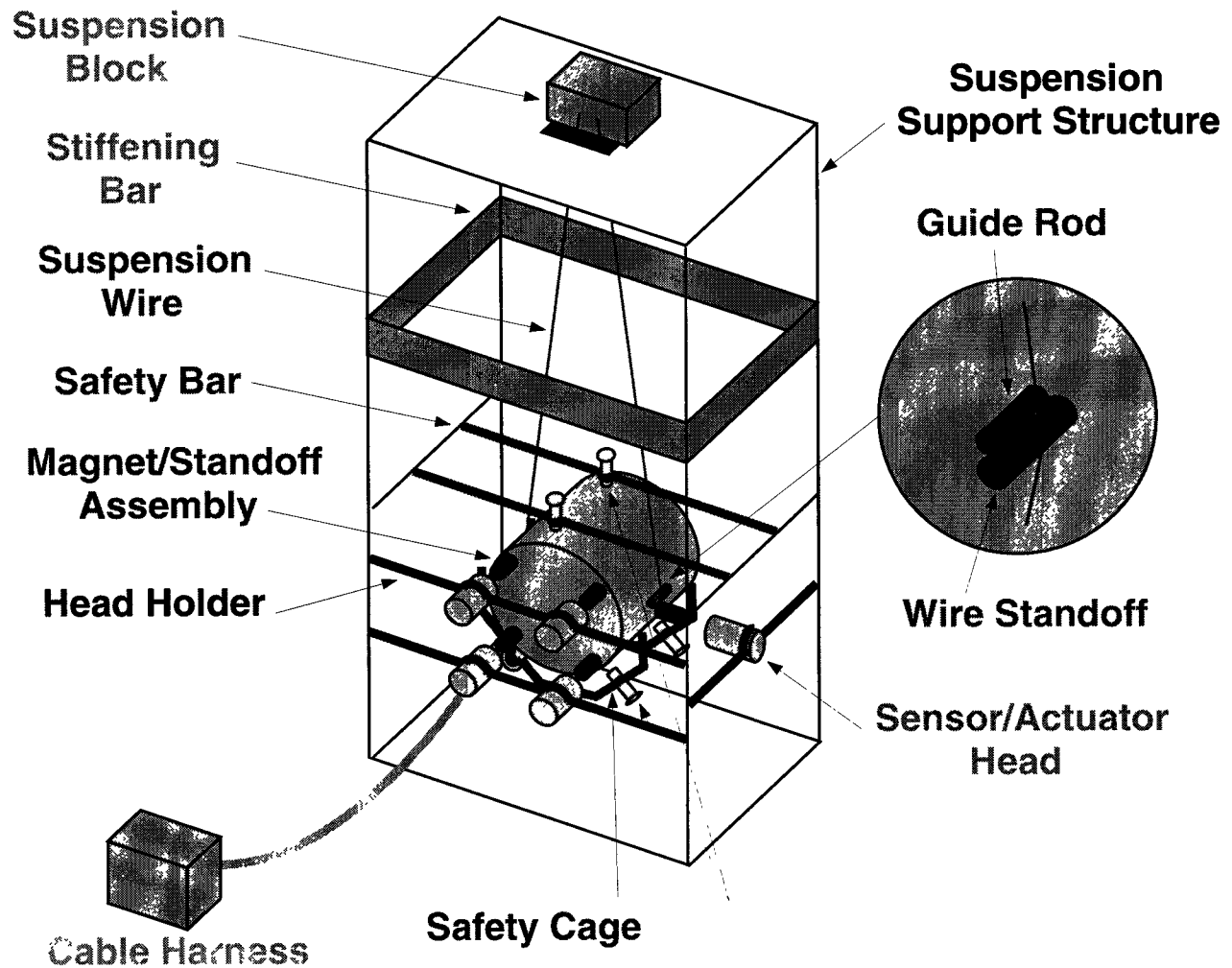


40m Test Mass Suspension

- One prototype was designed, fabricated, installed in the 40m, and characterized.
- New mechanical design worked.
- New control design worked.
- General performance was satisfactory.
- 40m was locked using the LSC (Length Sensing Control) input of the controller.
- 40m sensitivity with the prototype was NOT degraded with and without the LSC input.

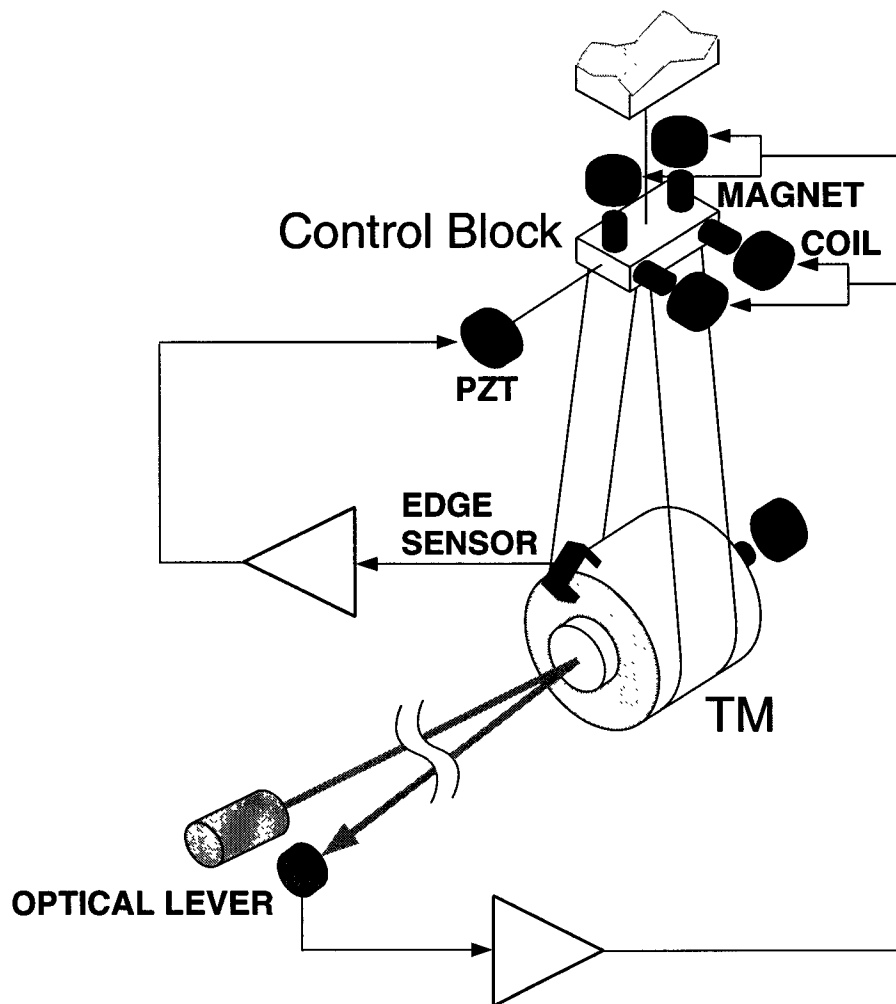
Mechanical System

- Single loop wire
- Modular support structure



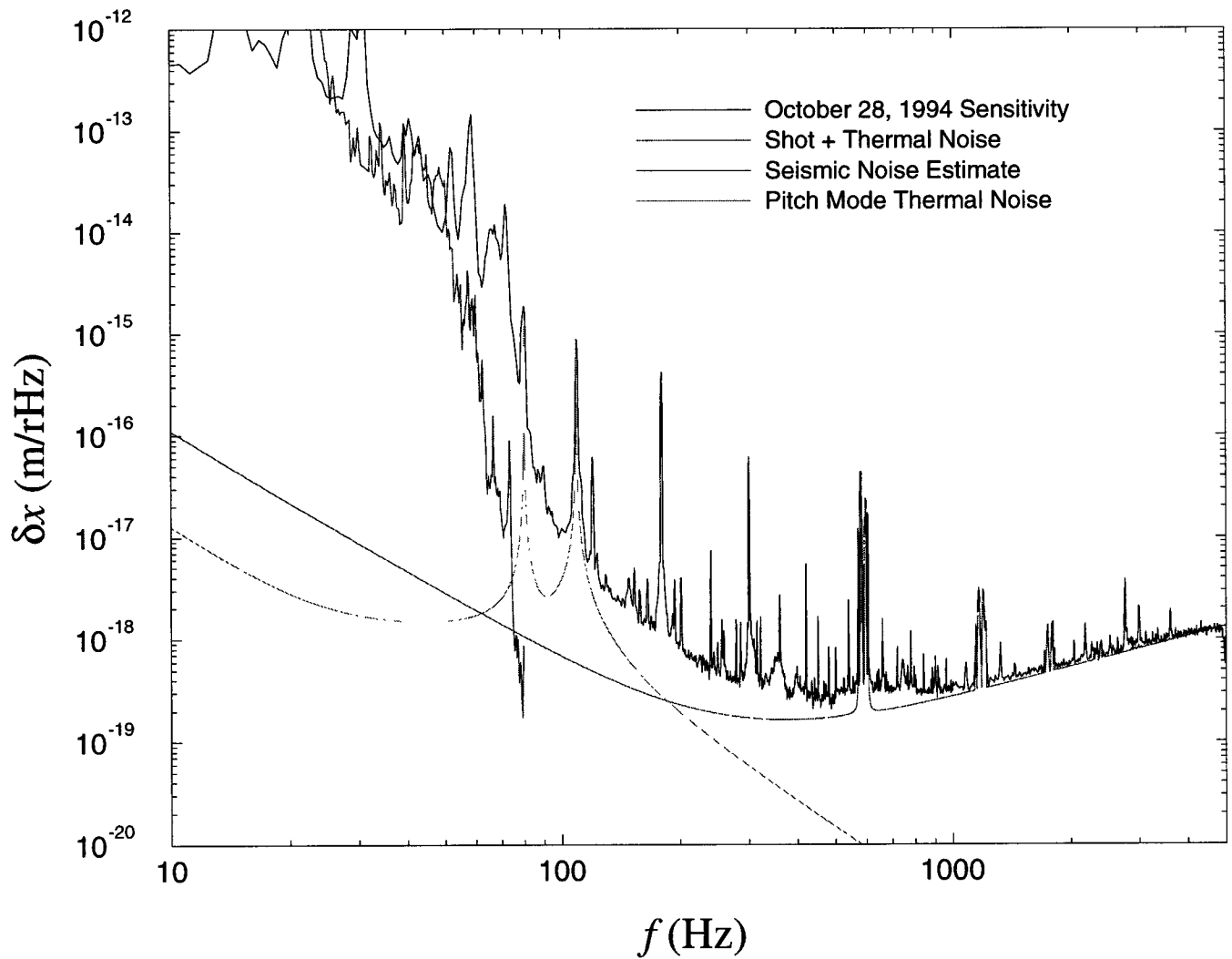
Double Loop Wire Configuration (Old 40m TM Suspension)

- Too complicated mechanical design
- Pitch and yaw mode thermal noise



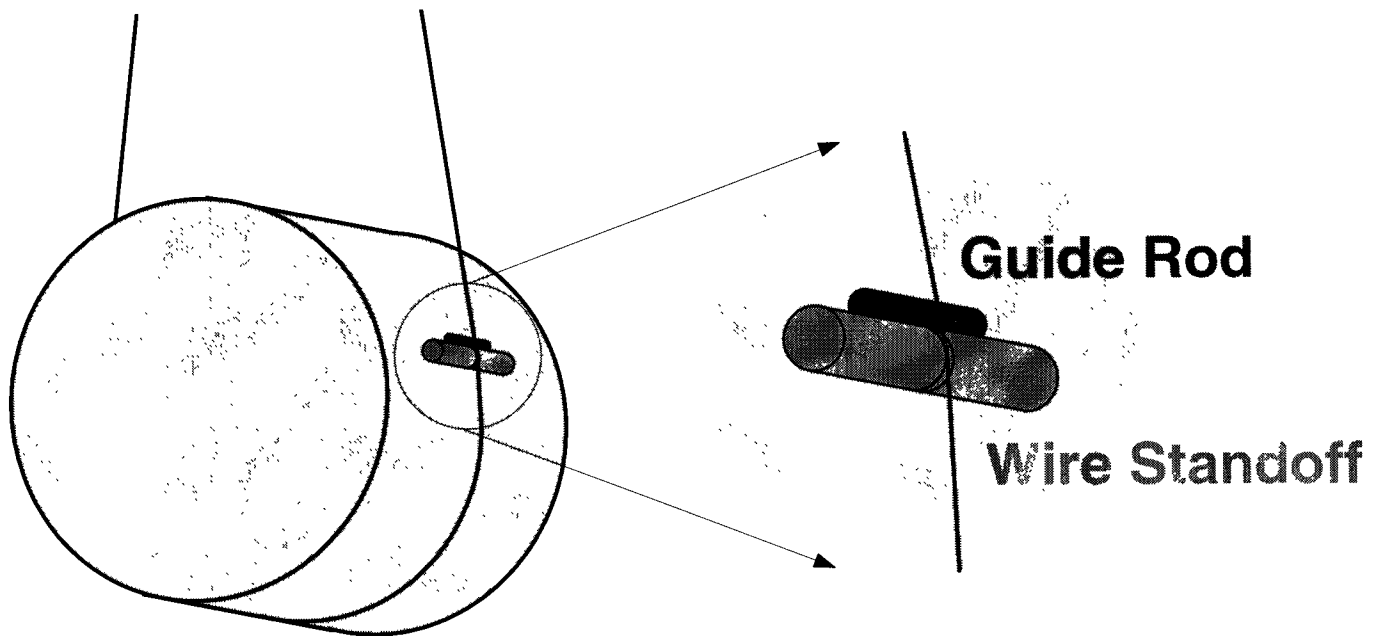
Pitch Mode Thermal Noise

- Measured Q: 2,000 - 3,000

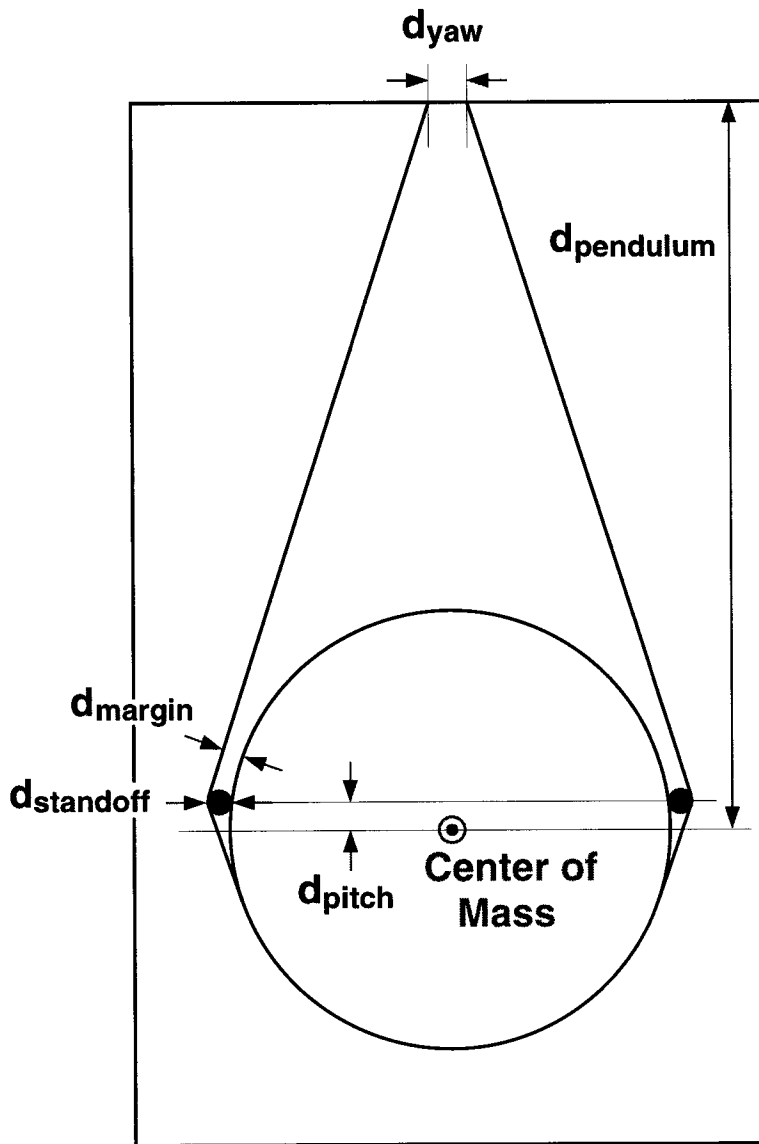


Balancing Test Mass with Single Loop Wire

- Balanced using guide rods and wire standoffs with groove
- Negligible Q degradation due to attachments



Suspension Configuration



$$f_{pendulum} = 0.84 \text{ Hz}$$

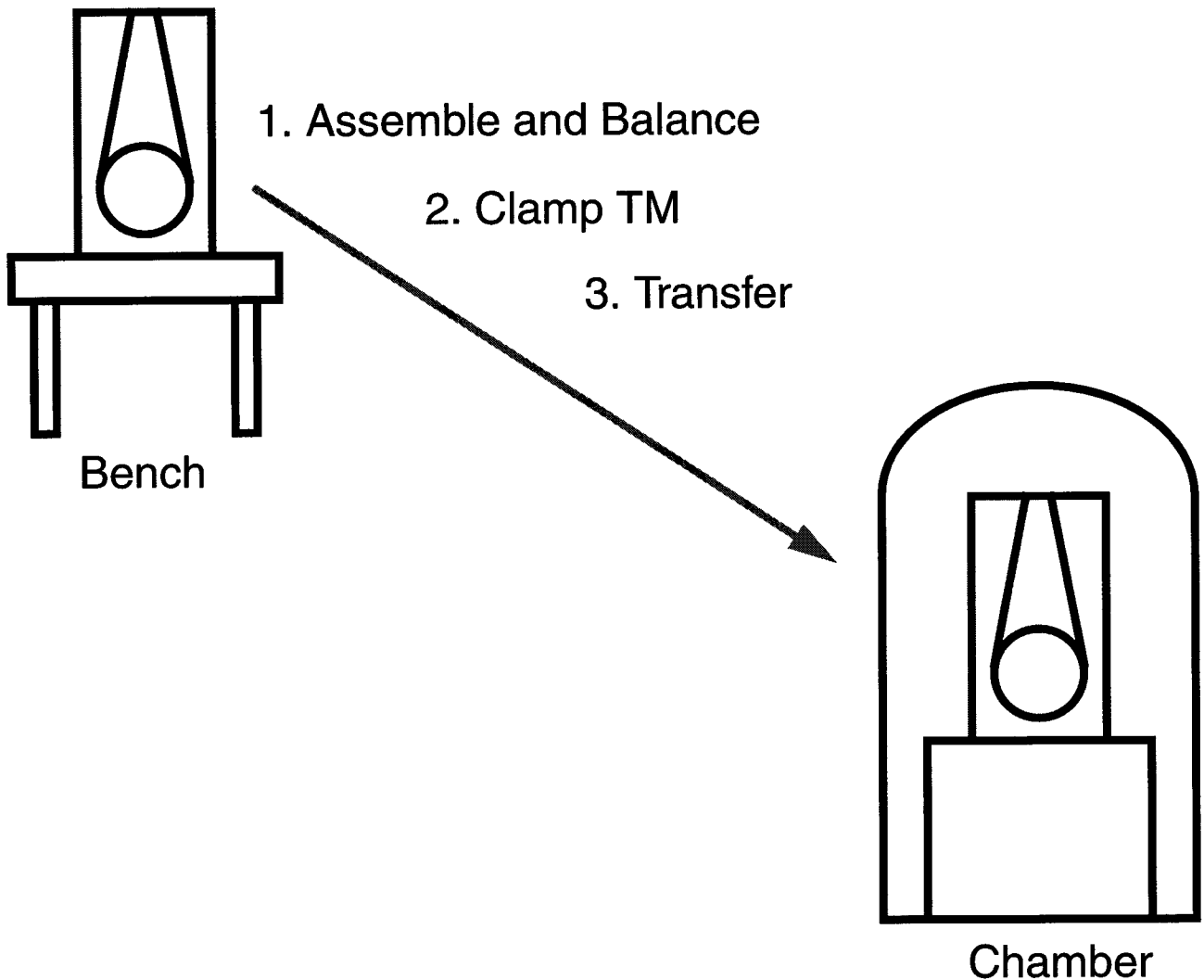
$$f_{pitch} = 0.50 \text{ Hz}$$

$$f_{yaw} = 0.60 \text{ Hz}$$

$$f_{violin} = 548 \text{ Hz}$$

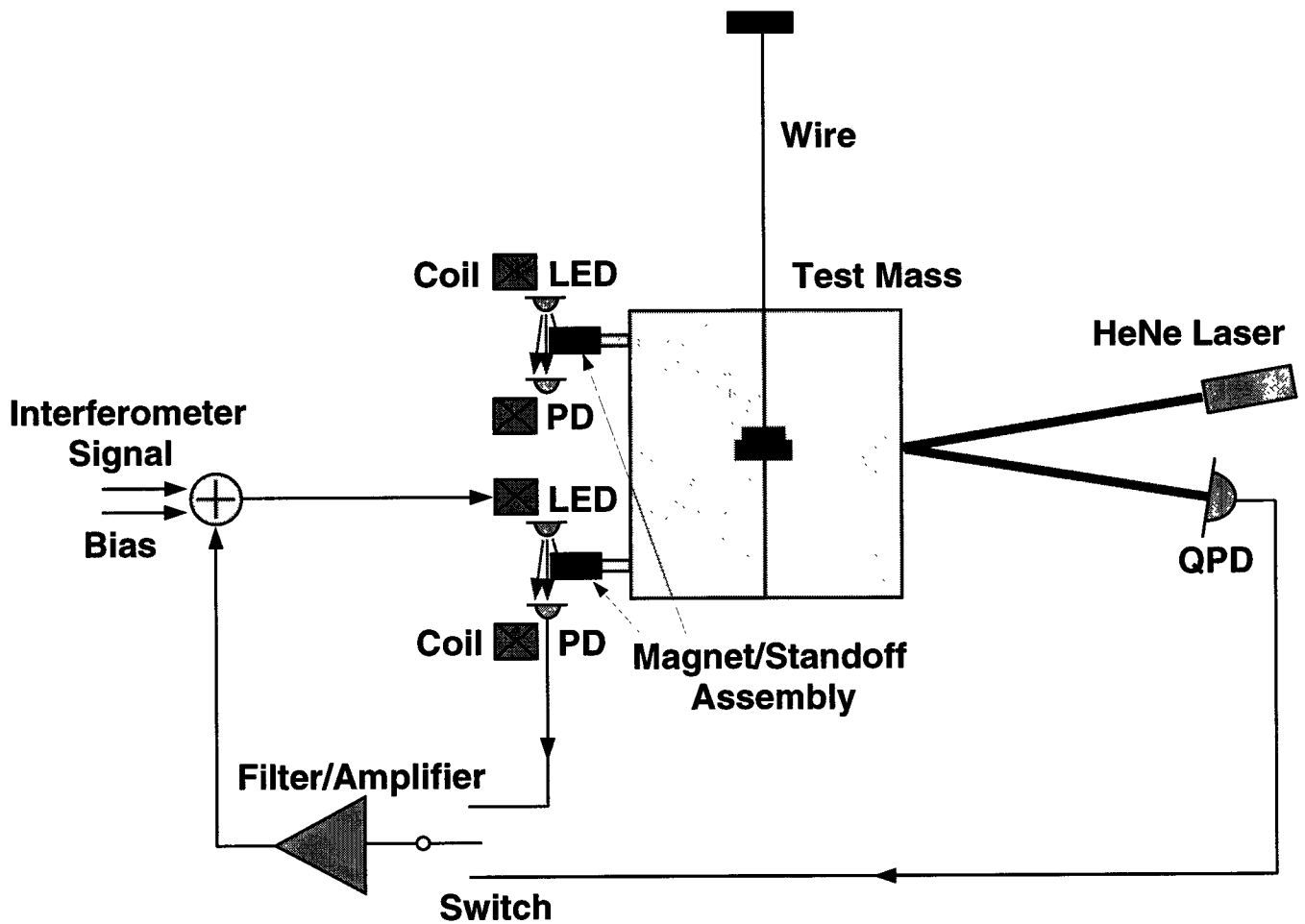
$$f_{vertical} = 11.1 \text{ Hz}$$

Assembly on Bench, Then Transfer into Chamber



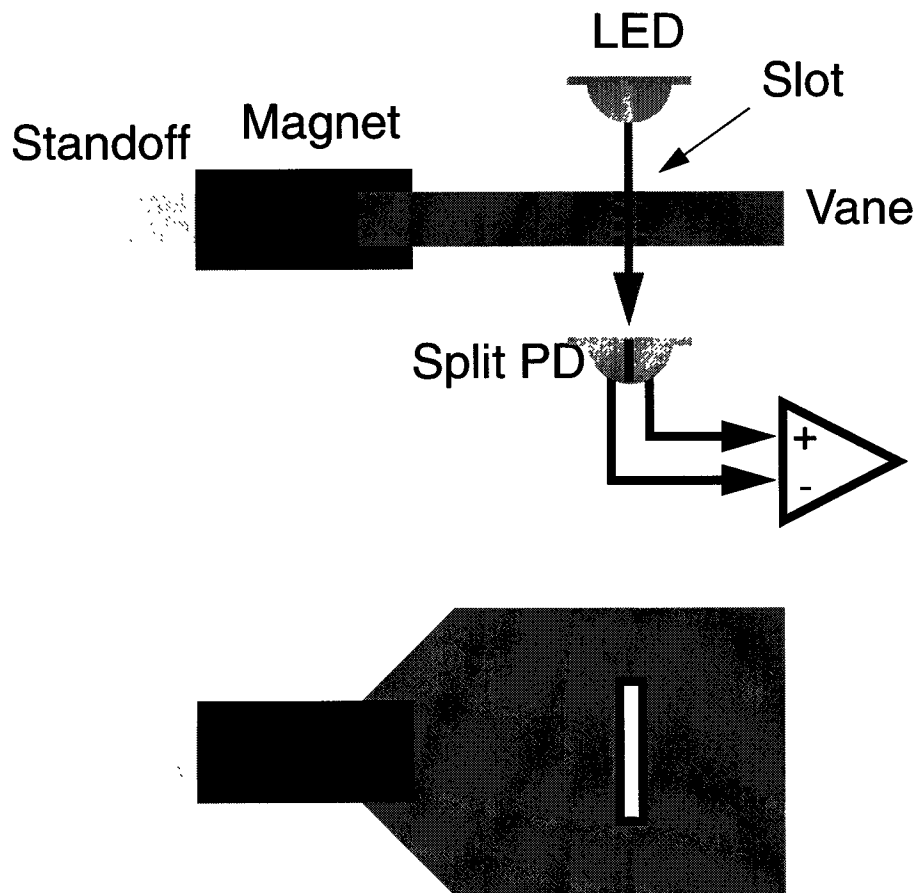
Control System

- Simple edge sensor
- Current-source type driver



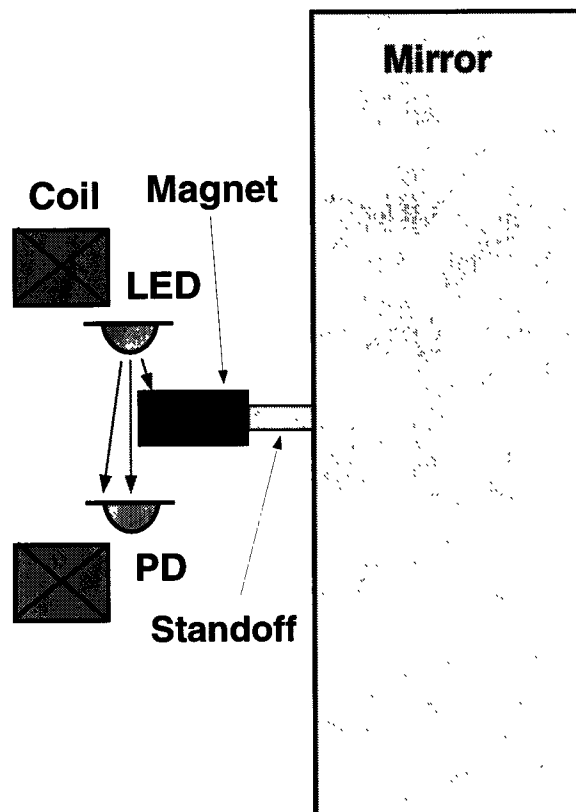
Slot Sensor with Vane (Old BS Suspension)

- Resonant frequency ~ 1 kHz due to the big vane
- Q degraded due to the big vane
- Complicated electronics



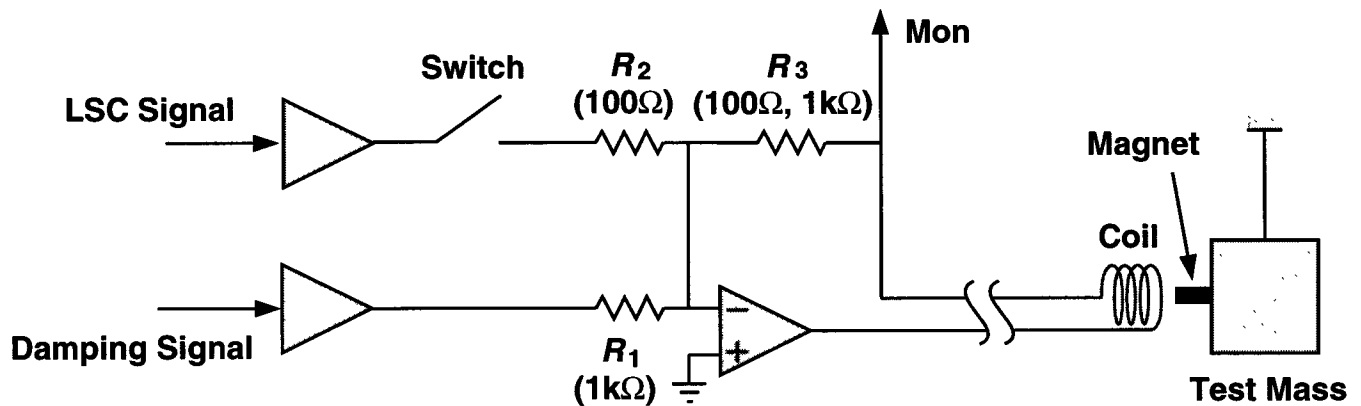
Edge Sensor without Vane

- Resonant frequency ~ 8 kHz
- Reasonable Q
- Simple electronics



Current-Source Type Driver

- No pick-up current into the coil
- Monitor signal free from pick-up.
- No eddy current dragging.
- Switchable between the acquisition mode and operation mode without gain change



Extrapolation to the LIGO

Large Optics Suspension

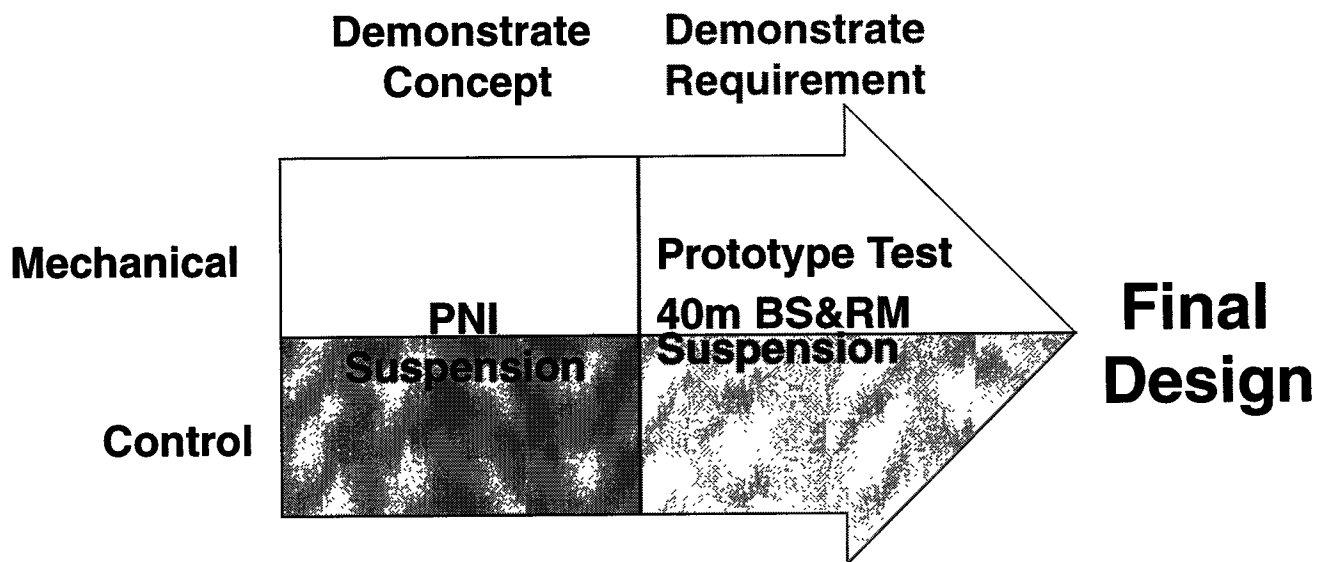
Items	40m TM Suspension or Pathfinder Q measurement	Extrapolated to LIGO	LIGO Requirements
Residual Q when damped	< 3	< 3	< 3
Internal Mode Loss	3×10^{-7}	3×10^{-7}	$< 4 \times 10^{-7}$
Pendulum Mode Loss	2×10^{-5} (Violin Mode)	7×10^{-6}	$< 7 \times 10^{-6}$
Actuator Range ($f < 0.15$ Hz)	44 μ mpp	8 μ mpp	> 80 μ mpp
Driver Noise (at 40 Hz)	6×10^{-19} m/ $\sqrt{\text{Hz}}$	9×10^{-20} m/ $\sqrt{\text{Hz}}$	$< 5 \times 10^{-20}$ m/ $\sqrt{\text{Hz}}$
Sensor Noise (at 40 Hz)	4×10^{-20} m/ $\sqrt{\text{Hz}}$	4×10^{-20} m/ $\sqrt{\text{Hz}}$	(Option) $< 5 \times 10^{-20}$ m/ $\sqrt{\text{Hz}}$

Next...

40m BS&RM Suspension

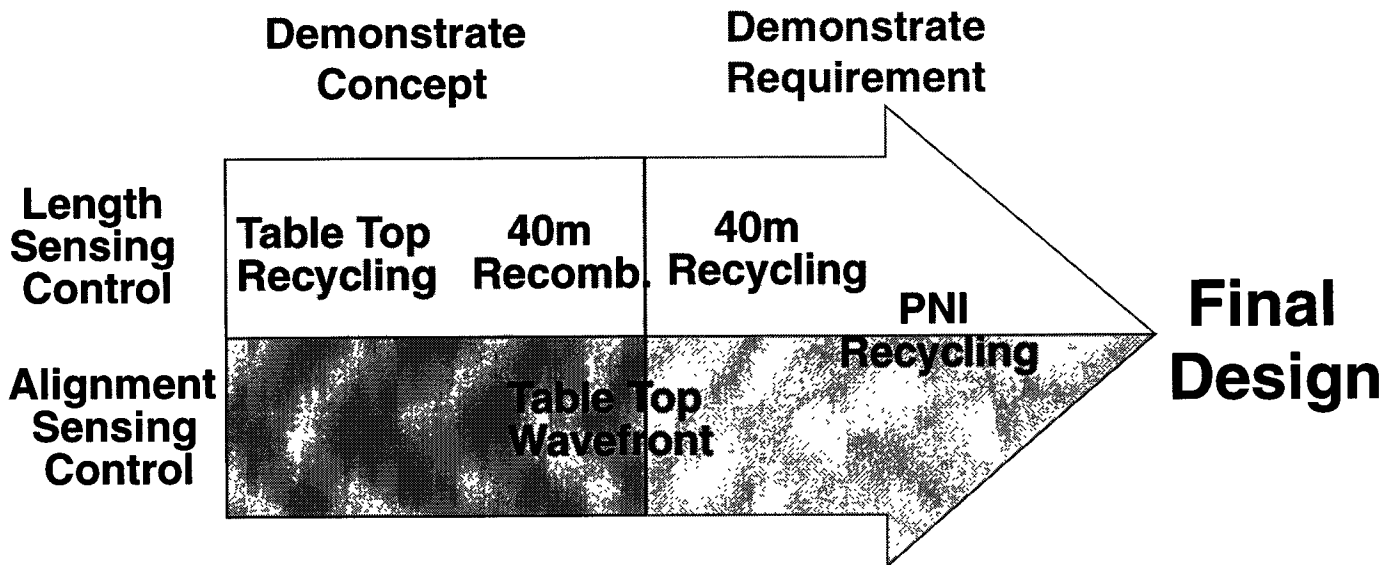
LIGO Small Optics Suspension

(Mode Cleaner Mirror, Steering Mirror)



Significance of Recombination at 40m

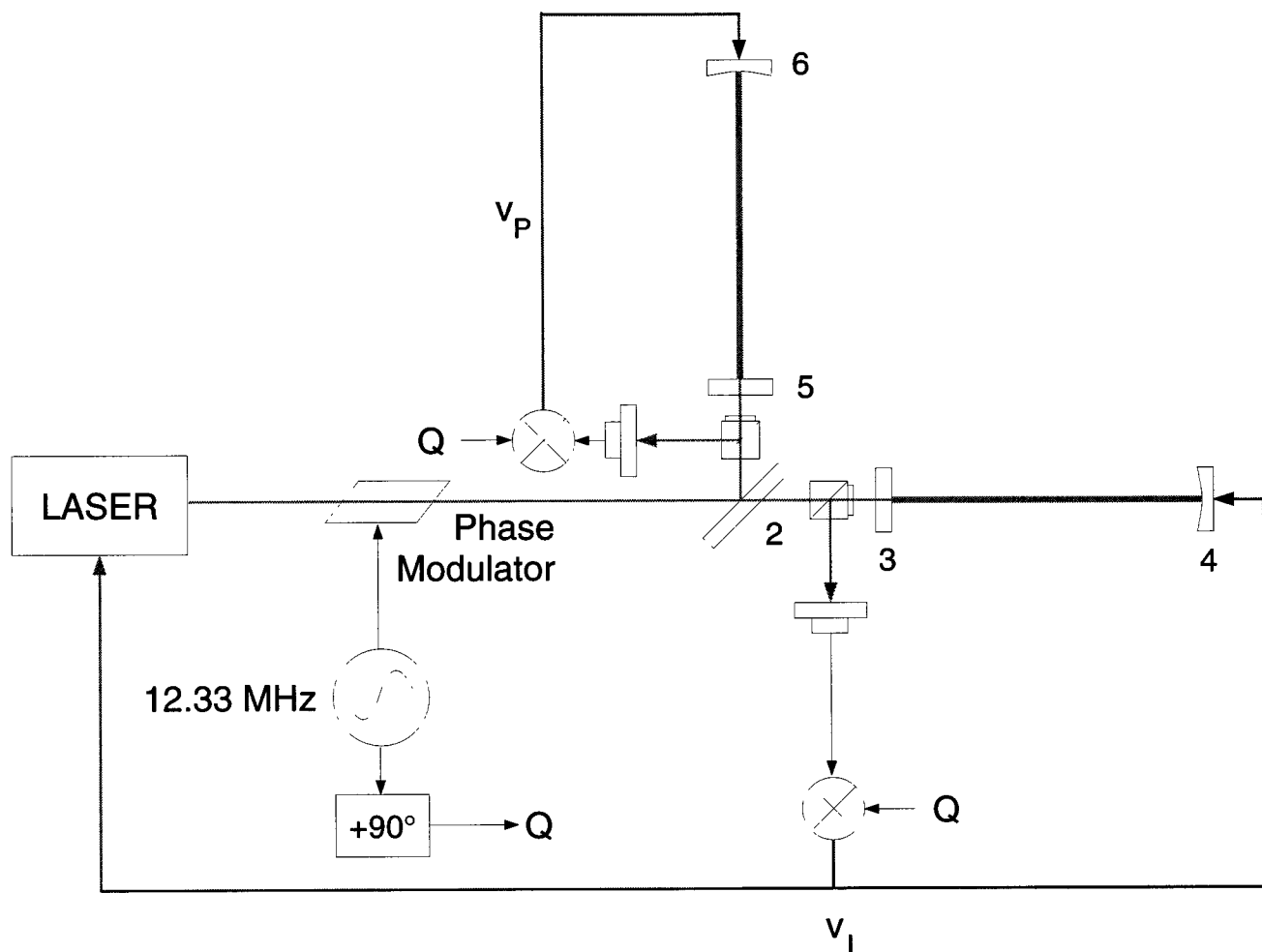
LIGO Interferometer Sensing/Control



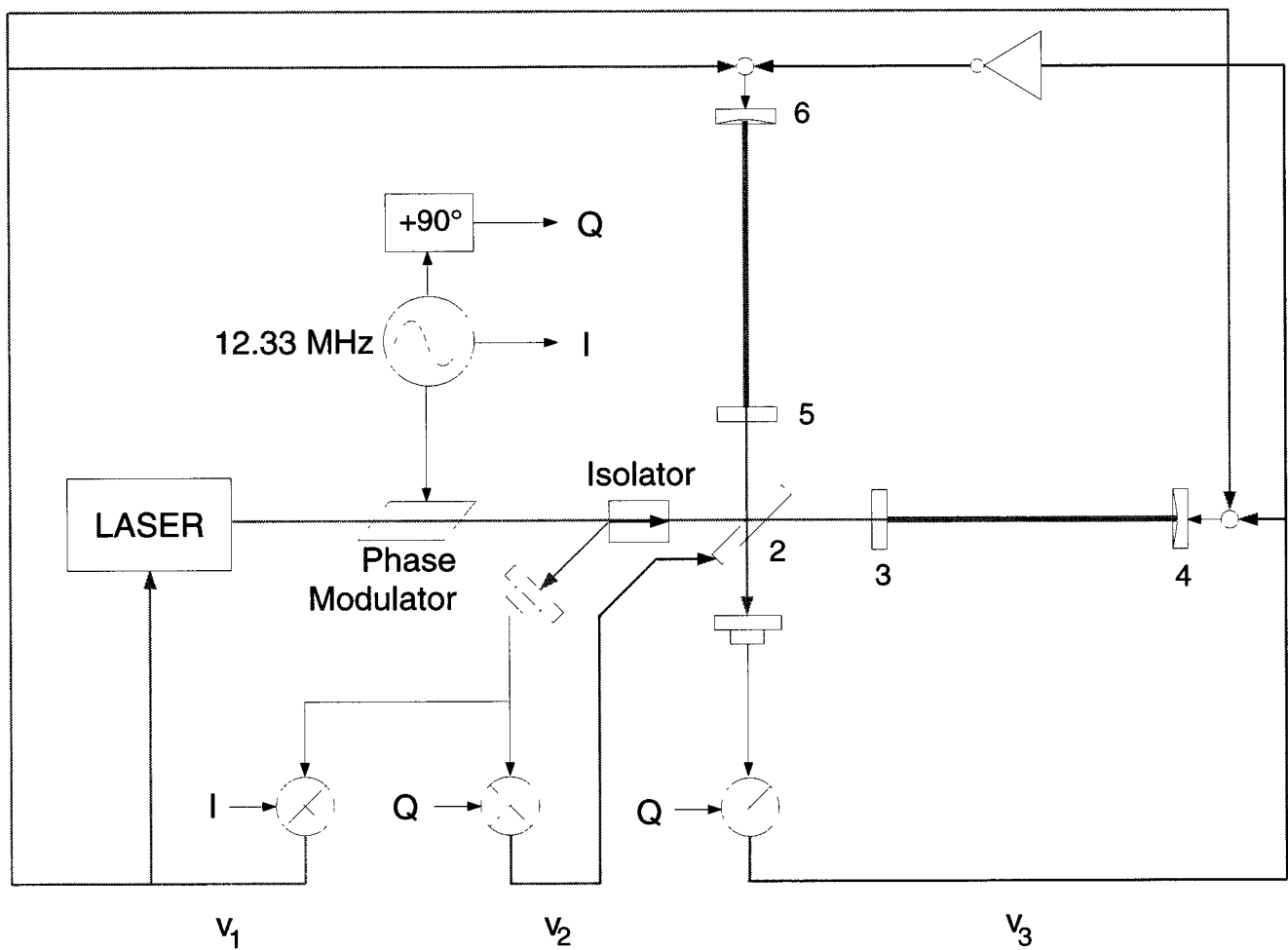
Recombination at 40m

- First demonstration of an optical topology in a suspended interferometer which is extensible to the initial LIGO interferometer.
- Many sources of noise were successfully controlled as predicted.
- Valuable experience was gained in lock acquisition.

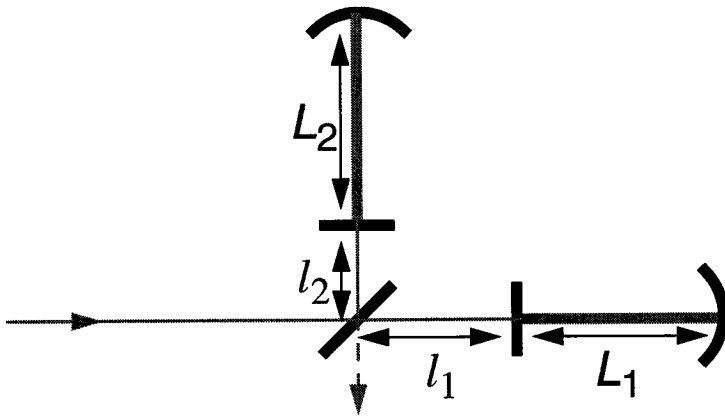
Fabry-Perot Interferometer



Fabry-Perot Recombined Servo Topology



Matrix of Discriminants



$$\Phi_+ = \frac{4\pi}{\lambda} (L_1 + L_2 - \Delta_+^{\text{DC}})$$

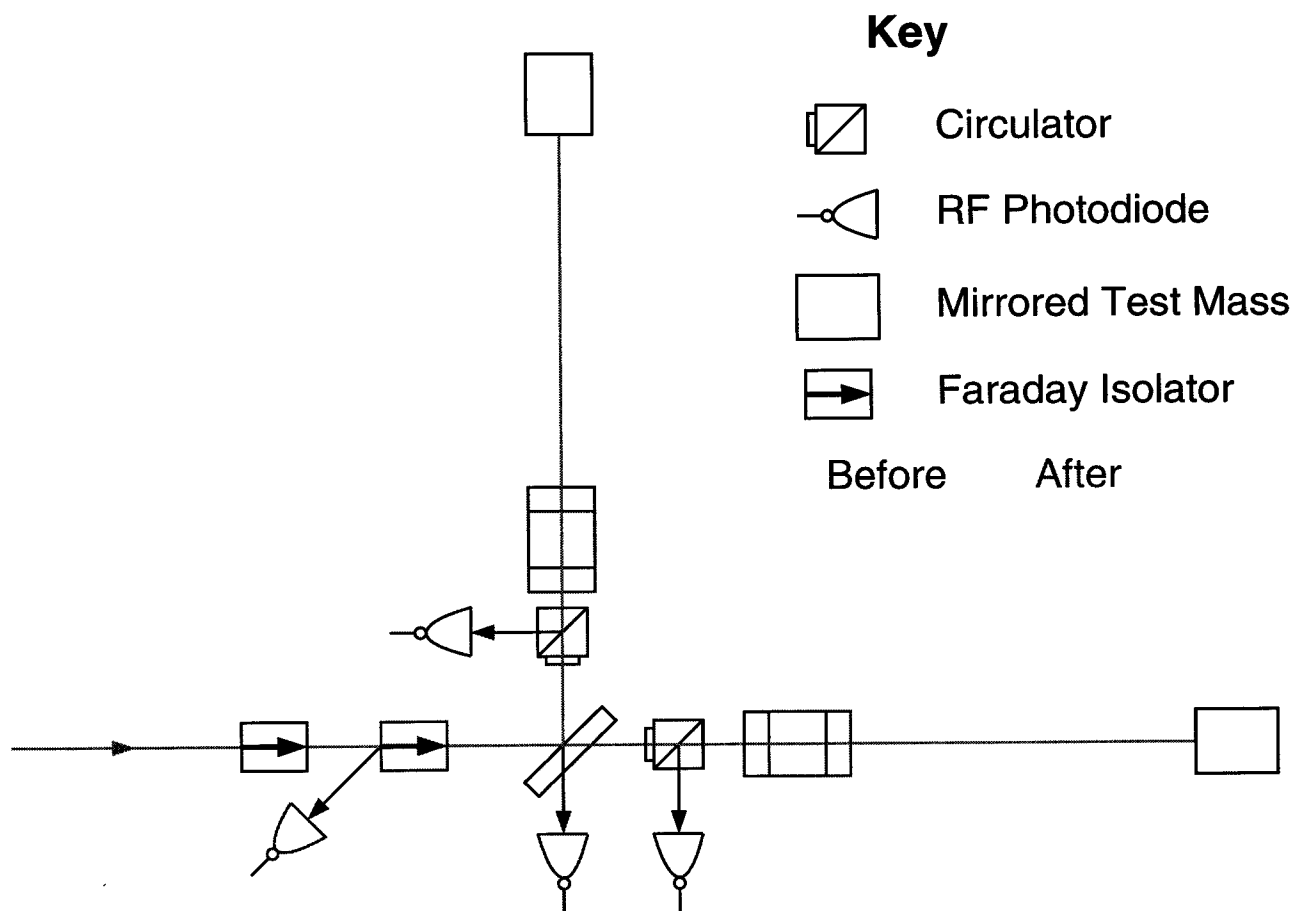
$$\phi_- = \frac{4\pi}{\lambda} (l_1 - l_2 - \delta_-^{\text{DC}})$$

$$\Phi_- = \frac{4\pi}{\lambda} (L_1 - L_2 - \Delta_-^{\text{DC}})$$

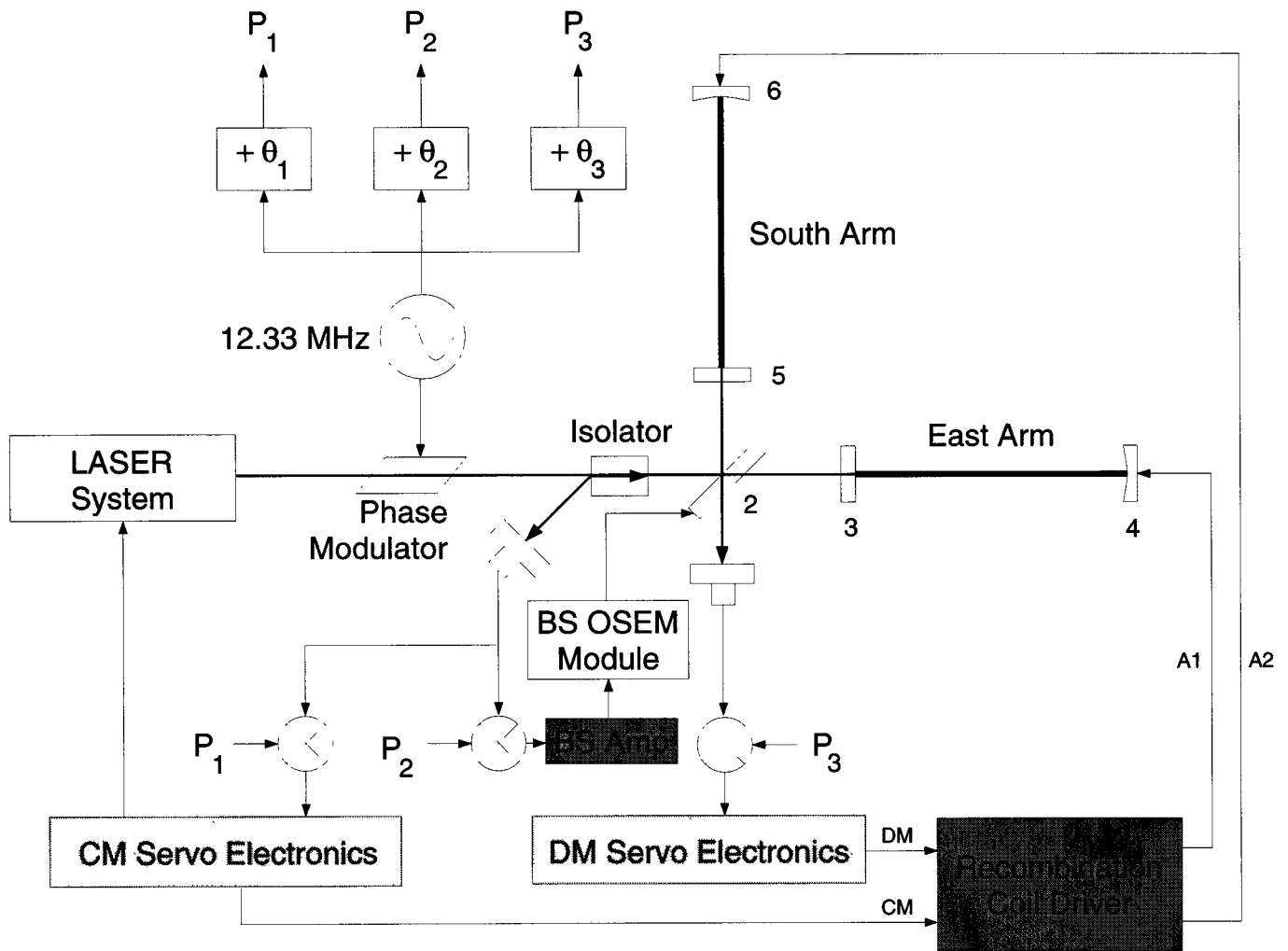
	∂v_1	∂v_2	∂v_3
$\partial \Phi_+$	-7.8	0	-2.2×10^{-1}
$\partial \phi_-$	2.3×10^{-4}	1.9×10^{-4}	-1.9×10^{-4}
$\partial \Phi_-$	2.5	1.6×10^{-8}	1.0

›› Normalized so that $\partial v_3 / \partial \Phi_- = 1$.

Modifications for Recombination



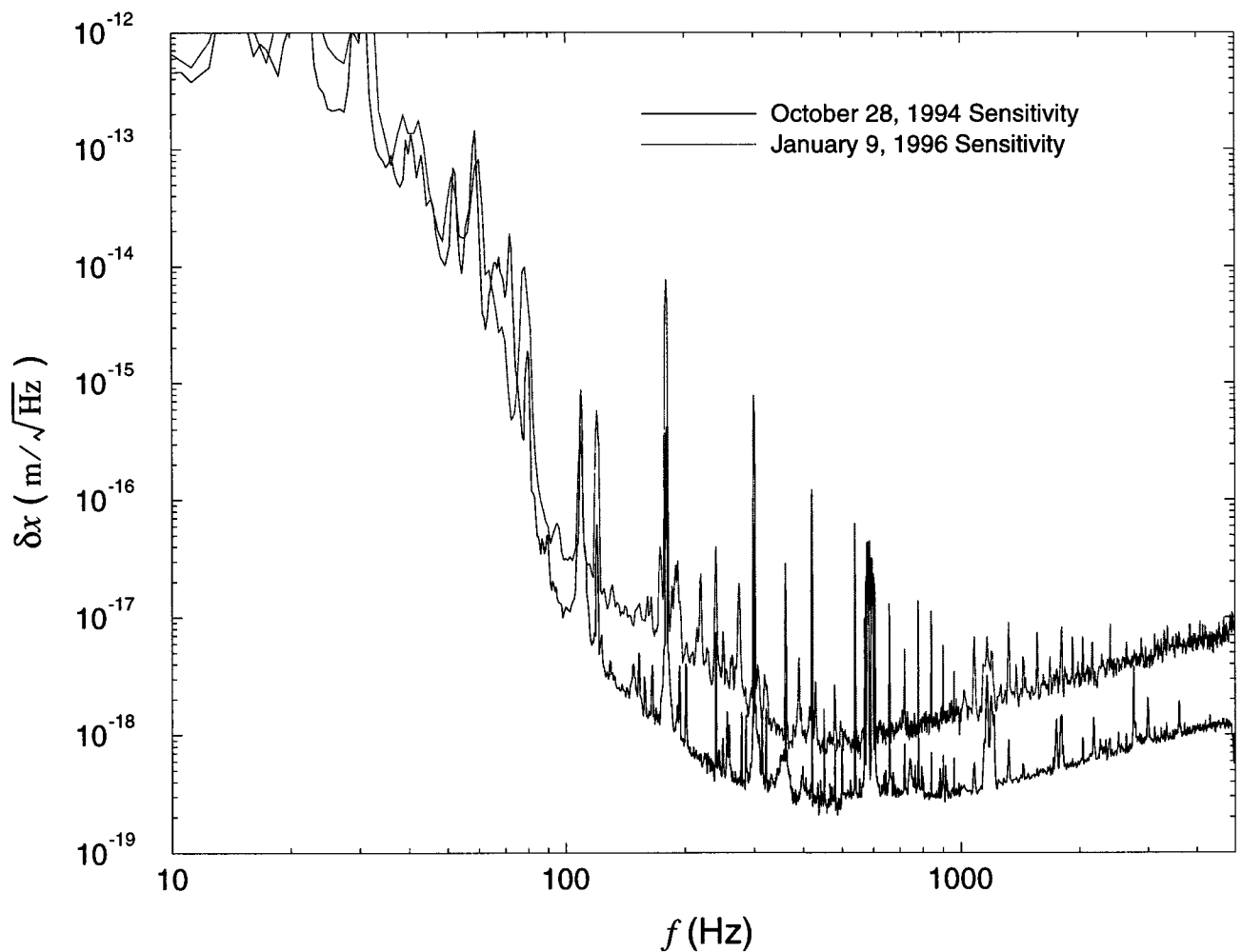
Control System



Interferometer Parameters

Quantity	Symbol	Value
Mirror (power) transmissions	T_2	0.45
	T_3	280 ppm
	T_5	300 ppm
	T_4, T_6	12 ppm
Loss in each mirror	L_3, L_4	110 ppm
	L_5, L_6	56 ppm
Asymmetry	δ	50.8 cm
Modulation frequency	f_{mod}	12.33 MHz
Modulation index	Γ	0.7 - 1.49
Contrast defect	$1 - C$	0.03

Recombination Sensitivity Comparison



Shot Noise Sensitivity Limits

- Differential mode displacement equivalent to shot noise in the differential mode signal:

$$\overline{S_{\Delta}}(f)^{1/2} = \frac{\sqrt{3E_+^2 + E_{DC}^2}}{2k|E_2|E_+} \frac{(1 - r_3 r_4)^2}{T_3 r_4} \sqrt{1 + \left(\frac{2\pi f}{\omega_c}\right)^2}$$

- Apparent differential mode motion due to shot noise in the common mode signal:

$$\left(\frac{S_{\Phi_+ \rightarrow \Phi_-}(0)}{S_{\Phi_-}(0)}\right)^{1/2} \approx \left(\frac{P_S}{P_A}\right)^{1/2} \left(\frac{\eta_A}{\eta_S}\right)^{1/2} \frac{\partial v_3 / \partial \Phi_+}{\partial v_1 / \partial \Phi_+} \sim 0.1$$

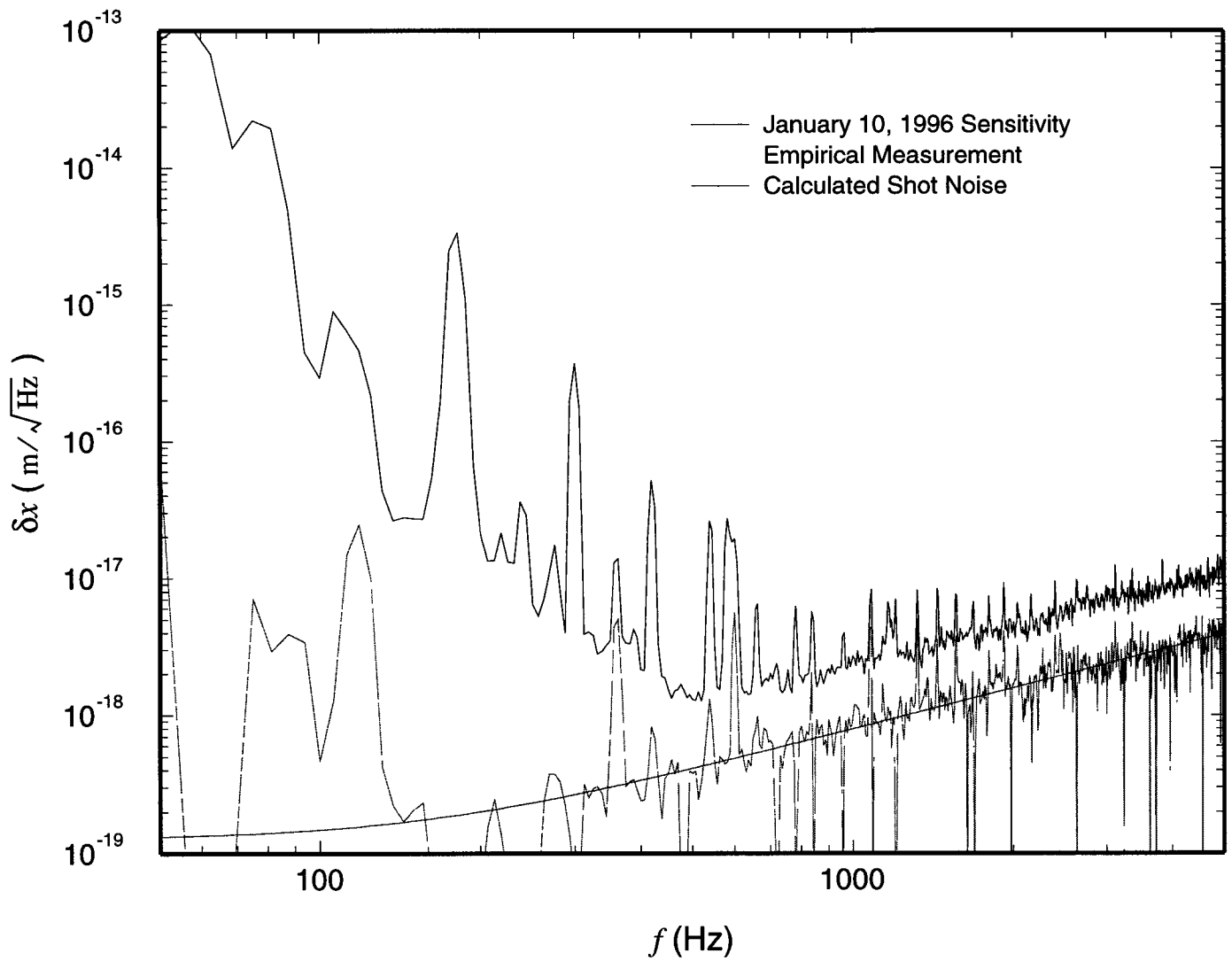
›› Not a problem at any frequency.

- Apparent differential mode motion due to shot noise in the beam splitter signal:

$$\left(\frac{S_{\phi_+ \rightarrow \phi_-}(0)}{S_{\phi_-}(0)}\right)^{1/2} \approx \left(\frac{P_S}{P_A}\right)^{1/2} \left(\frac{\eta_A}{\eta_S}\right)^{1/2} \frac{\partial v_3 / \partial \phi_-}{\partial v_2 / \partial \phi_-} \sim 3$$

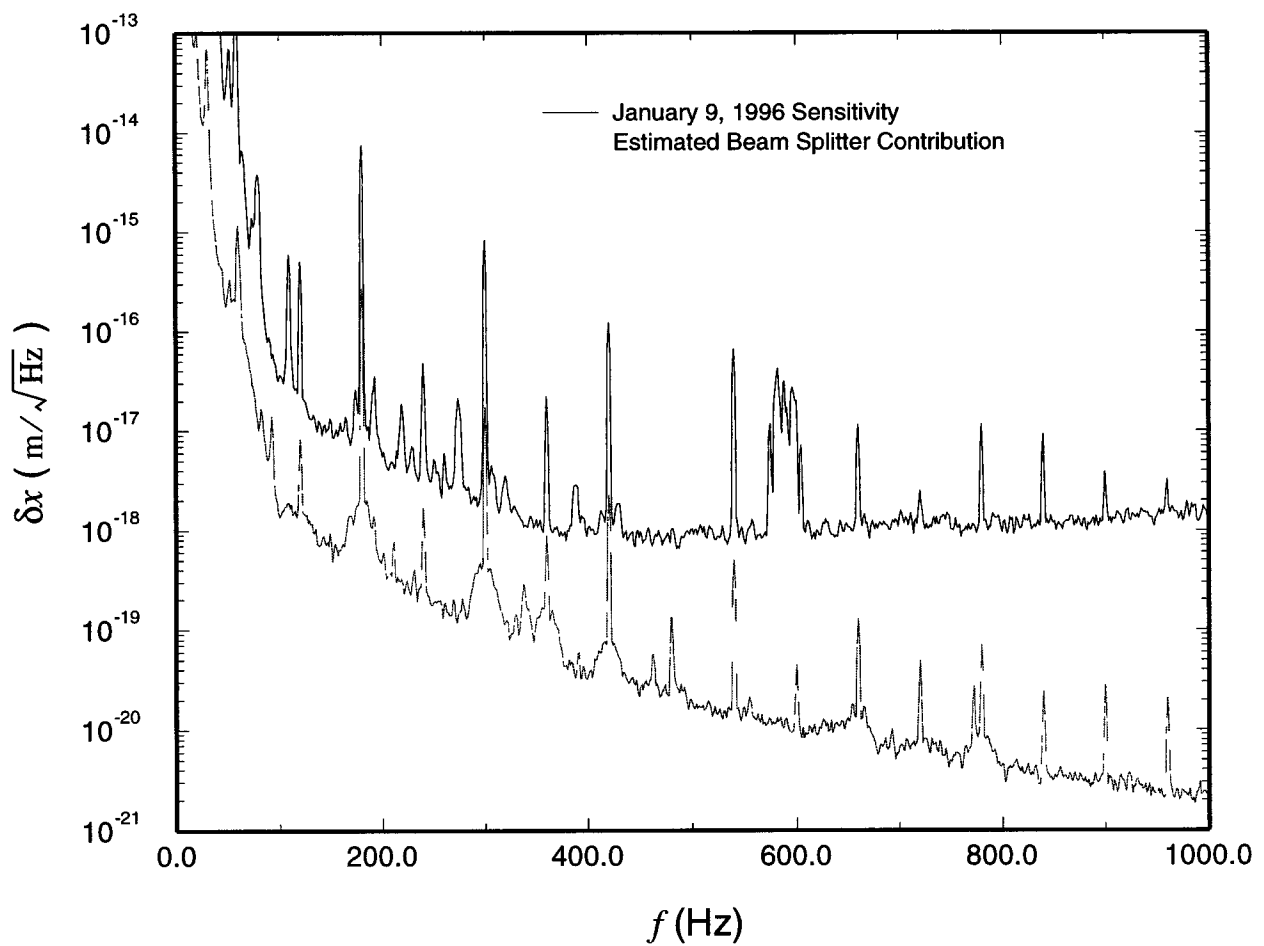
›› Potential problem. Requires tailoring of beam splitter servo.

Shot Noise Estimate

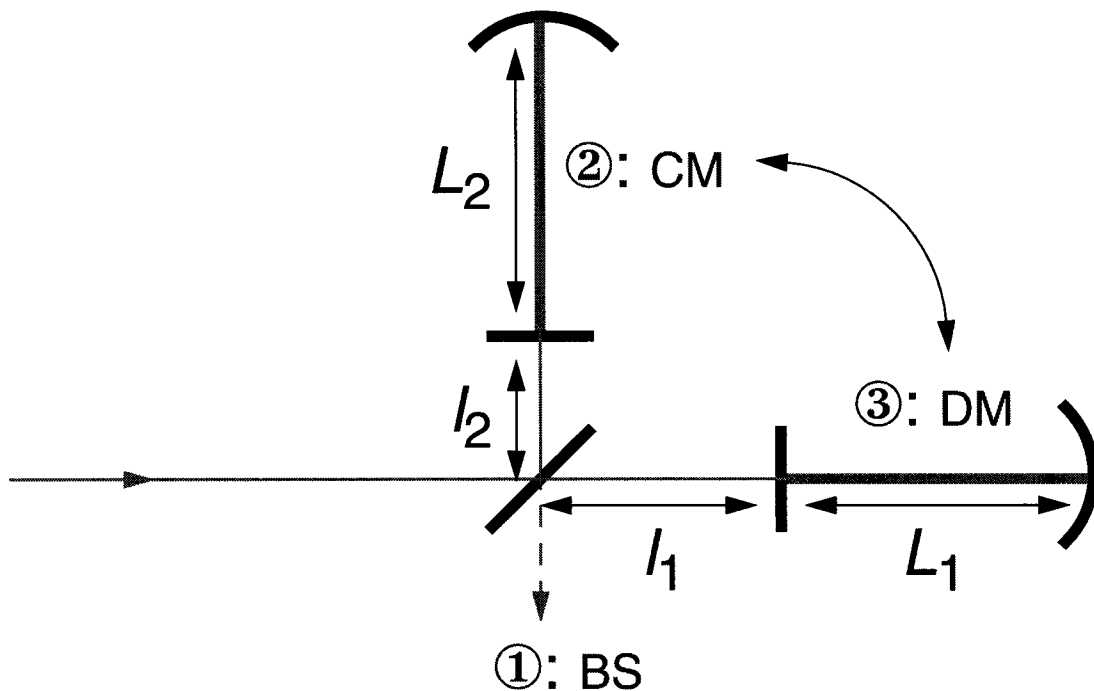


Beam Splitter Motion

- BS motion directly couples.



Lock Acquisition Sequence



- Common mode and beam splitter servos NOT disrupted by movement of the out of lock arm.

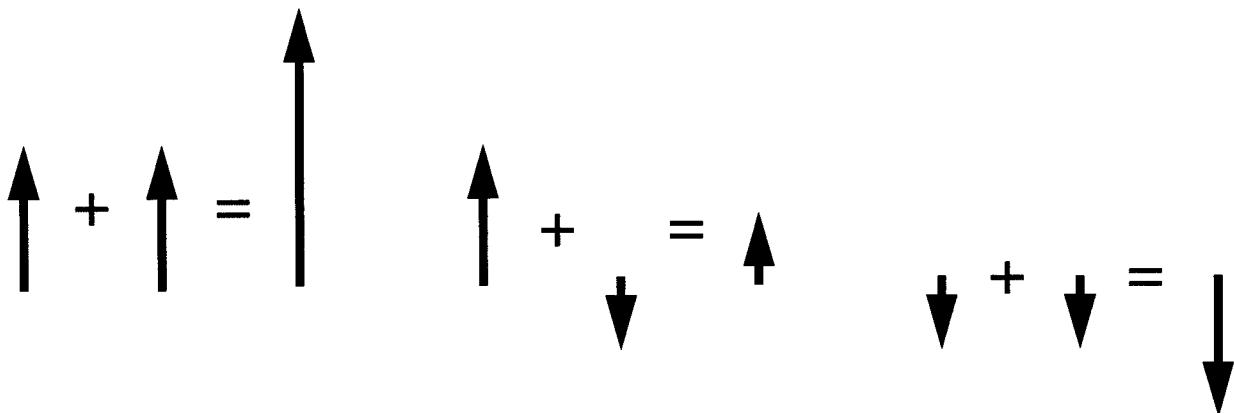
Beam Splitter Sign Reversal

- The beam splitter error signal can reverse sign in going from one arm and the beam splitter in lock to the entire interferometer in lock.

Neither Arm Locked

One Arm Locked

Both Arms Locked



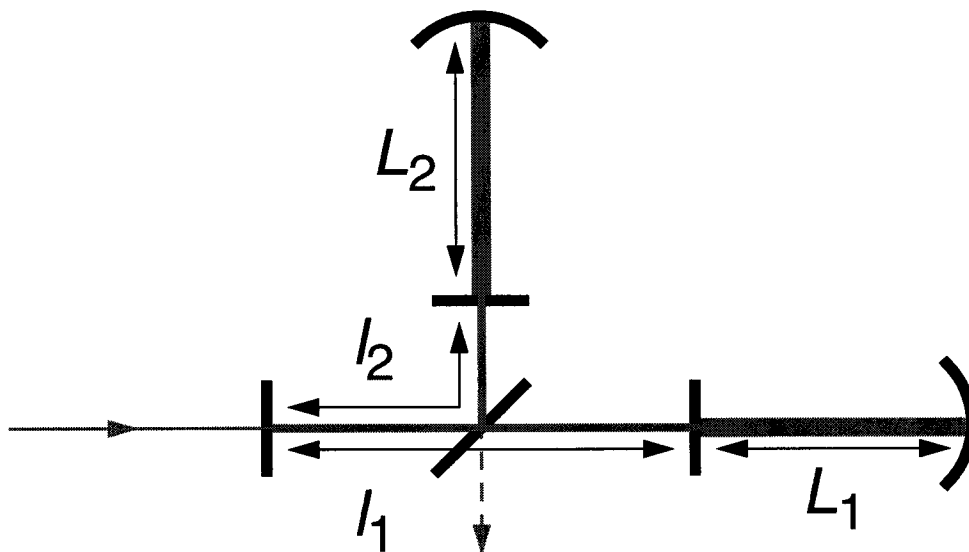
- Three methods to correct this:
 - ›› Poor mode matching into arm cavities (Initial case)
 - ›› Reverse sign of feedback signal when both arms in lock
 - ›› Increase modulation depth (Used for most measurements)

Allowable RMS Deviations

Phase	Distance, m	Explanation
$\Phi_+ < 1.6 \times 10^{-4}$	$\Delta_+ < 7 \times 10^{-12}$	arm cavity power
$\phi_- < 8.9 \times 10^{-2}$	$\delta_- < 4 \times 10^{-9}$	maintain dark fringe
$\Phi_- < 2.9 \times 10^{-6}$	$\Delta_- < 1 \times 10^{-13}$	maintain dark fringe

- Seismic motion of the suspended optical components must be suppressed to this level by the servos.
- The first and second arm servos in the Fabry-Perot configuration met the requirements for the common and differential mode and were used with little modification for recombination.
- The beam splitter servo was designed for recombination to meet the above requirement.

Recycled Interferometer



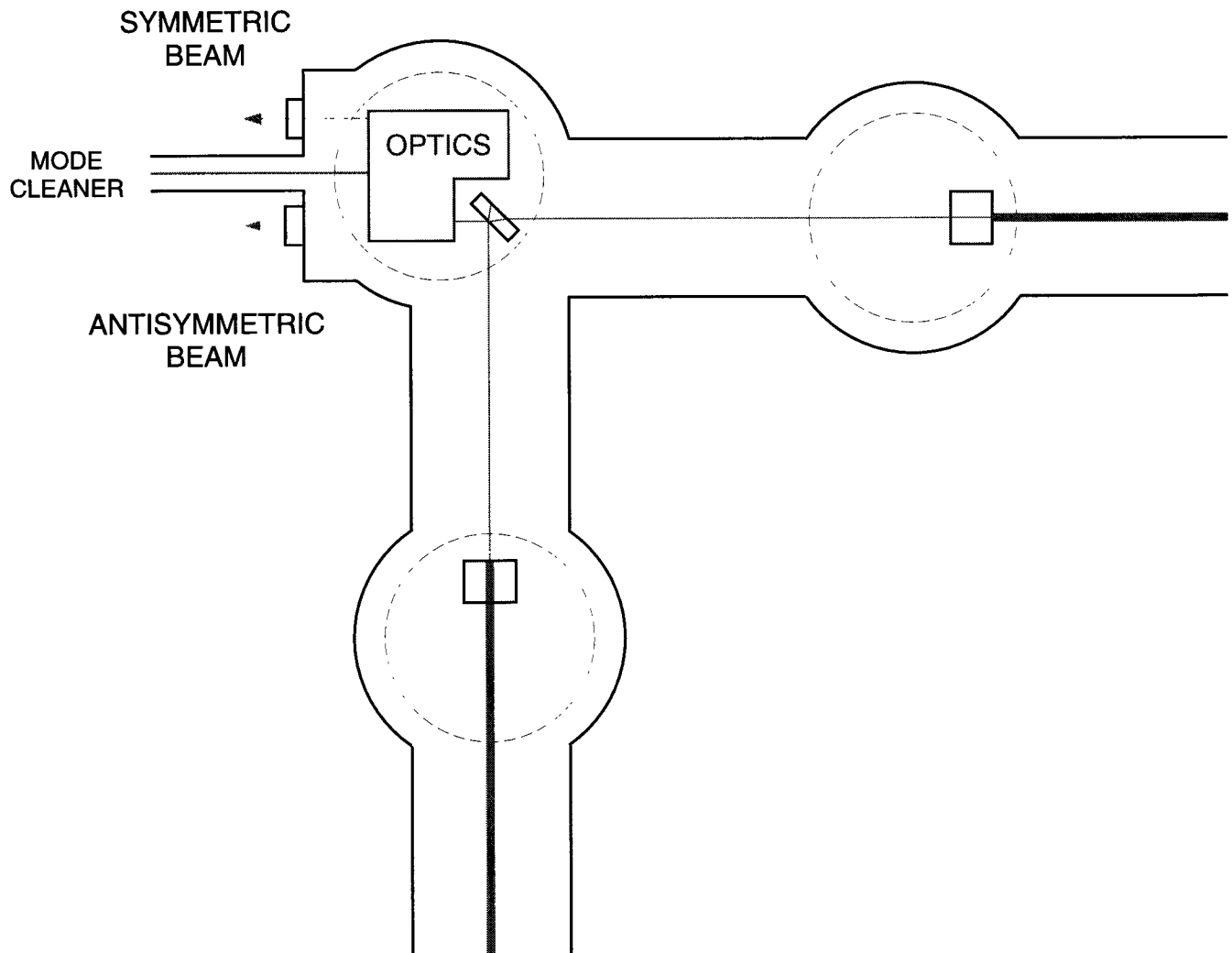
- Degrees of Freedom:

- ›› Common mode arm length = $L_1 + L_2$
- ›› Differential arm length (GW signal) = $L_1 - L_2$
- ›› Recycling cavity length = $l_1 + l_2$
- ›› Michelson near-mirror difference = $l_1 - l_2$

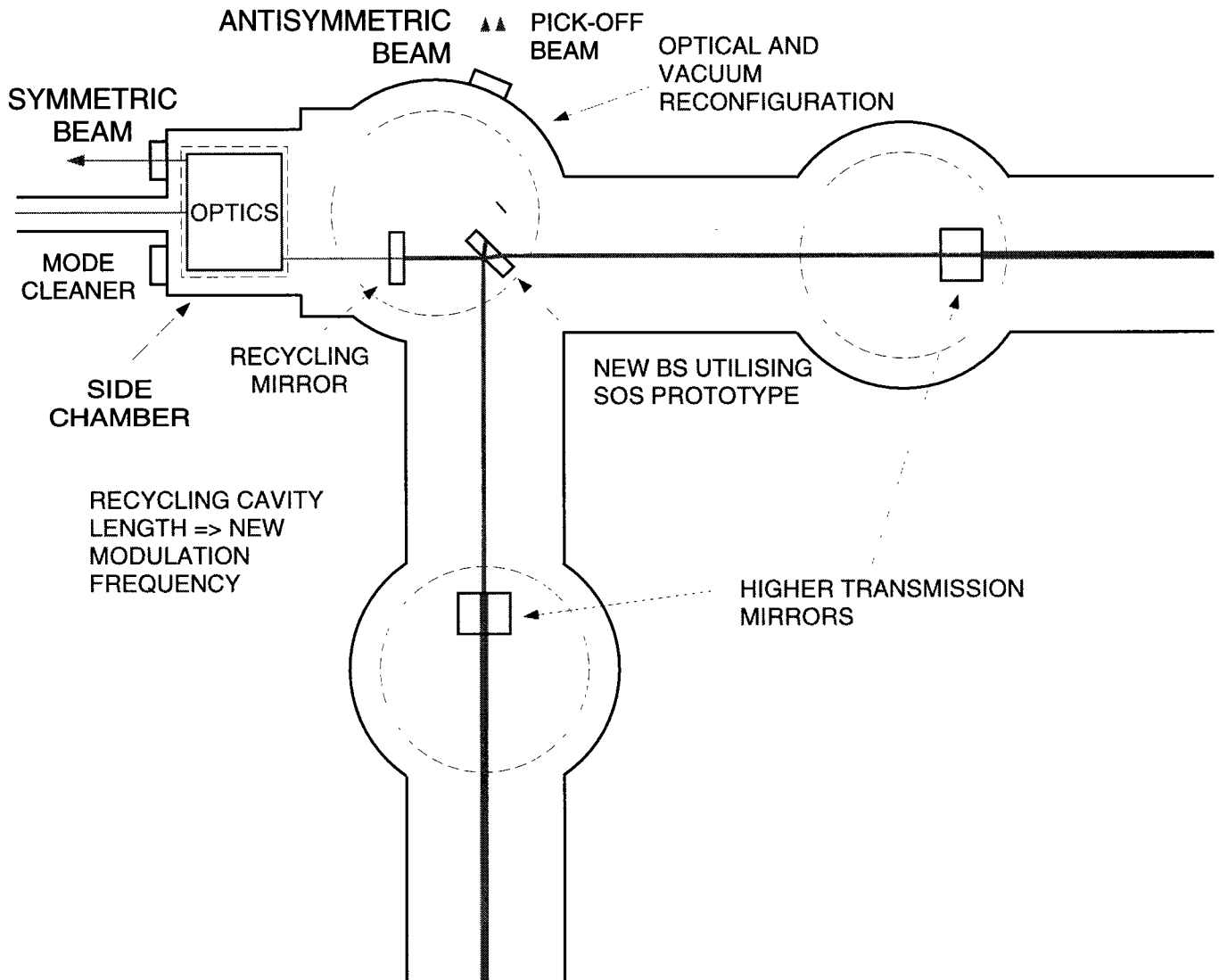
Steps Required to Achieve Recycling

- Change vertex masses for ones of higher transmission
 - ›› completed; currently in shakedown phase following this change
- Reconfigure vacuum envelope with installation of side chamber and reconfigure optical layout including replacement of present beamsplitter with SOS prototype
 - ›› task scheduled to start mid-November
- Change modulation frequency
 - ›› new reference source built to LIGO specifications
- Install recycling mirror
 - ›› scheduled for end of March

Optical Configuration (Recombination)

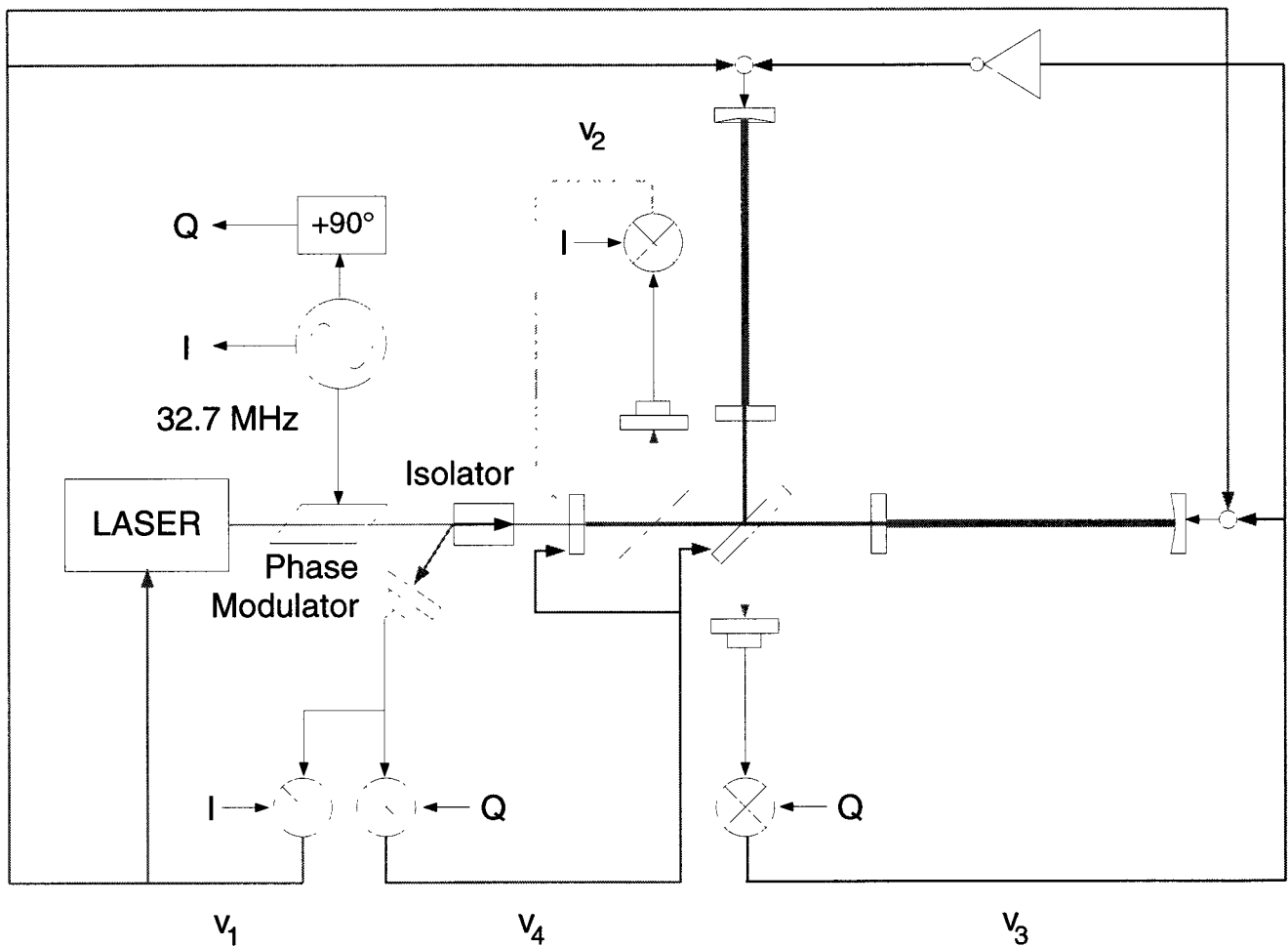


Optical Configuration (Recycling)

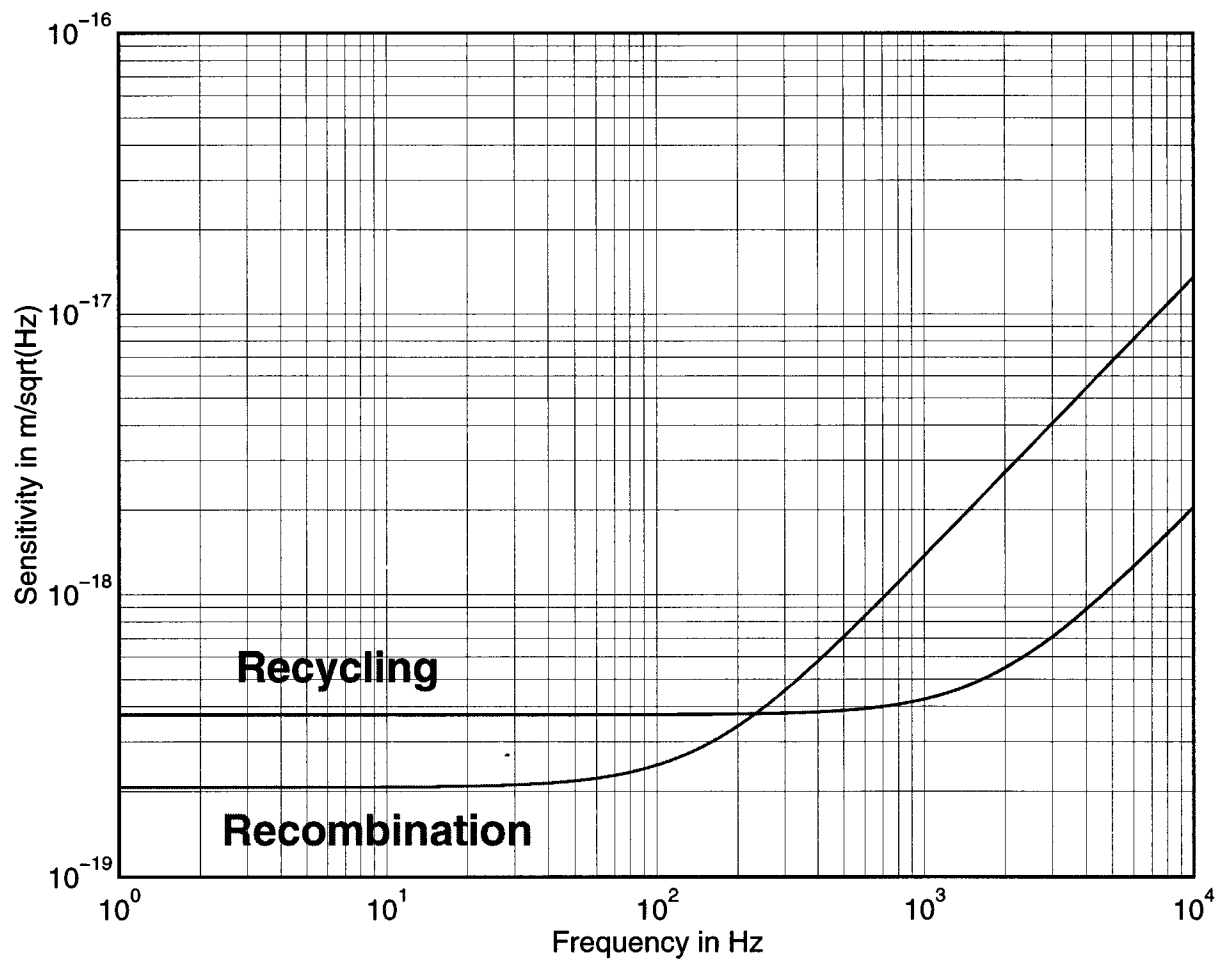


Control System (Recycling)

Optical and Servo Topology for the Recycled 40-m Interferometer



Predicted Shot Noise Sensitivity



Conclusion

- New 40m TM suspension prototype successfully tested
- LIGO small optics suspension prototype is ready to try for the 40m BS
- First demonstration of an optical topology in a suspended interferometer which is extensible to the initial LIGO interferometers
- Recycling with the initial LIGO configuration started in the 40m