



LIGO-G080487-00-Z



Status of Coating Work at Sannio

Giuseppe Castaldi,
Vincenzo Galdi,
Vincenzo Pierro,
Innocenzo M. Pinto,

TWG, University of Sannio at Benevento



LSC/VIRGO Joint Meeting,
Amsterdam NL, sept 21-25, 2008





Summary



- INFN funding for 2nd generation (doped Tantala) optimised coating mirror TNI-prototypes approved;
- Impact of thermoelastic/thermorefractive noise cancellation on coating optimization (aka, *living with a minus sign*).



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INFN Funding Obtained



- INFN funding for 2nd generation (Ti-doped Tantala) optimized-coating mirror prototypes approved by INFN panel-V (September 18, 2008). Money (35 KEU) available jan. 2009.
- This funding originally requested for f.y. 2007 was put on hold, waiting for TNI measurements on 1st generation prototypes (whose design had been completed in November 2006).
- The well known LMA “bubble” problems delayed prototype delivery. Prototype measurements became available Dec. 2007, and were presented to INFN in Feb. 2008.
- Funding release was then recommended by INFN Referees.



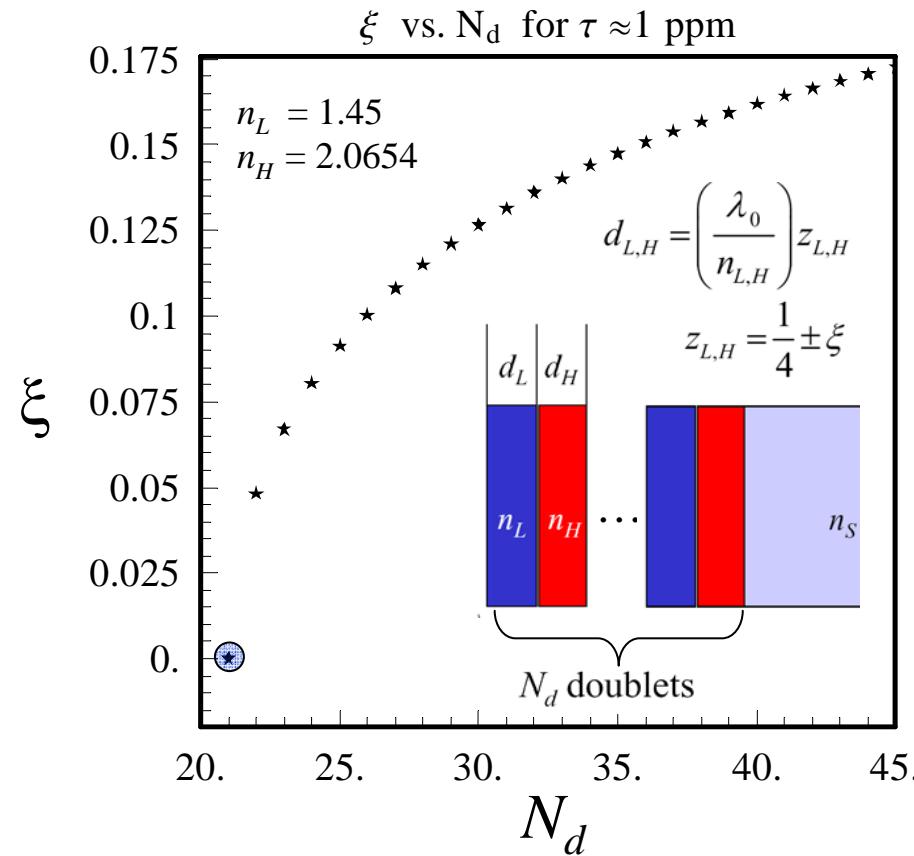
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Coating Optimization: Isoreflective SD Coatings (Bragg, Binary)



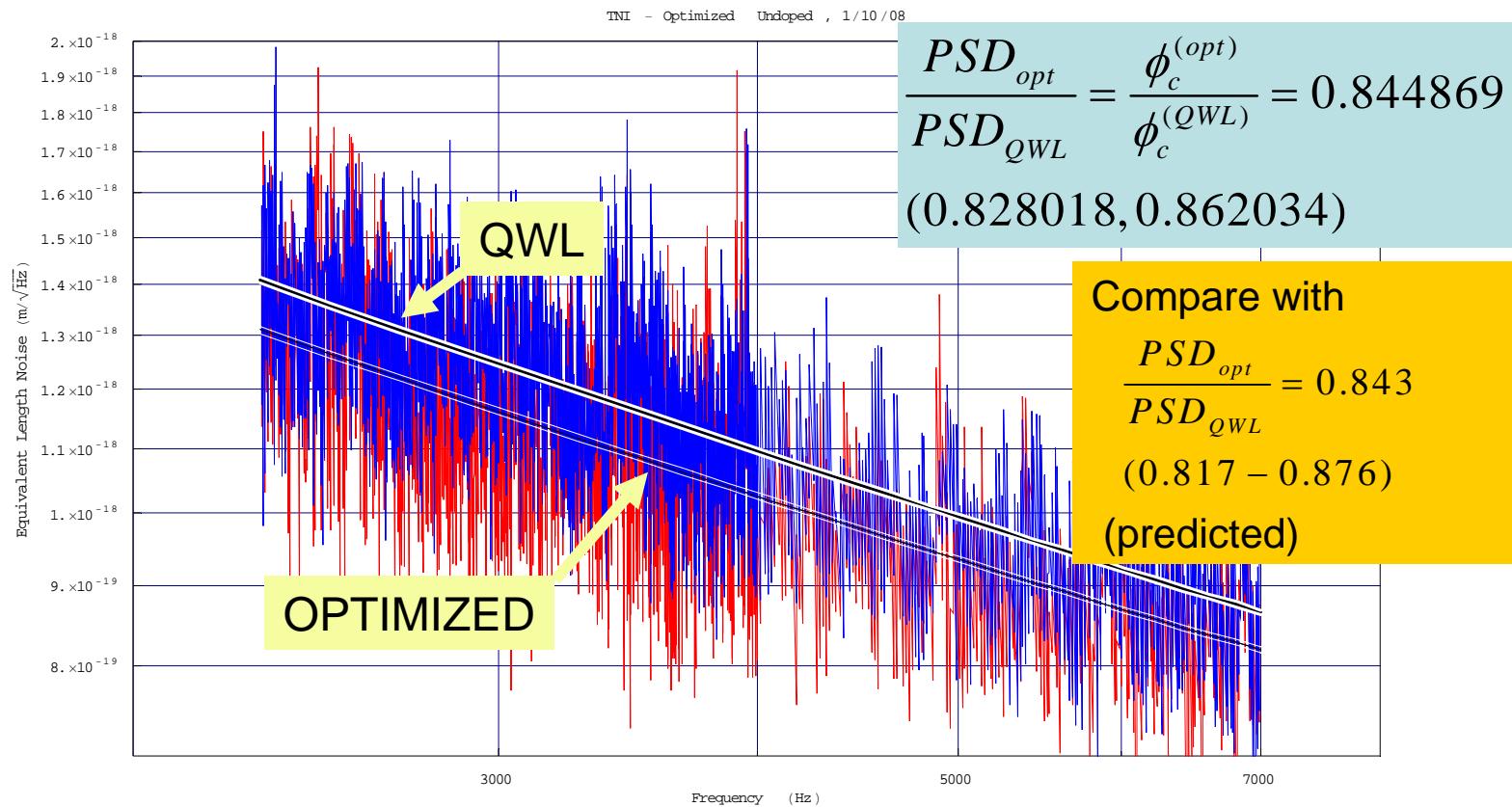
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1st Generation (Plain Tantala) Optimized Coating Prototypes

Courtesy E. Black & A. Villar





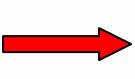
1st Generation Prototypes. Robustness



		N = 16		N = 17		N = 18	
	γ	Plain $\{z_L, z_H\}$ $\{0.330169, 0.169831\}$	Tweaked $\{z_L, z_H\}$ $\{0.330169, 0.169831\}$	Plain $\{z_L, z_H\}$ $\{0.345676, 0.154324\}$	Tweaked $\{z_L, z_H\}$ $\{0.345676, 0.154324\}$	Plain $\{z_L, z_H\}$ $\{0.357797, 0.142203\}$	Tweaked $\{z_L, z_H\}$ $\{0.357797, 0.142203\}$
10		0.896	0.871	0.901 (+0.005)	0.876 (+0.005)	0.912 (+0.016)	0.886 (+0.015)
7		0.866 (+0.003)	0.847 (+0.004)	0.863	0.843	0.867 (+0.004)	0.847 (0.004)
5		0.842 (+0.012)	0.827 (+0.013)	0.833 (+0.003)	0.817 (+0.003)	0.830	0.814

Table of PSD values relative to QWL design with HWL cap (N=14), for various values of $\gamma = \frac{\phi_H}{\phi_L} \frac{n_L}{n_H} \left(\frac{Y_H}{Y_S} + \frac{Y_S}{Y_H} \right)$

$$S_x^{(B)} = C[z_L + \gamma z_H] \quad (z_L, z_H = \text{layer thicknesses in units of local wavelength})$$

N = number of high/low index layers; optimum (minimum noise) syntheses highlighted in yellow. Numbers in brackets are $\{z_L, z_H\}$ (plain design; first line in tweaked design) and $\{z_L, z_N\}$ (second line in tweaked design).
 The N=17 design yields the minimum degradation (in brackets) compared to optimum design,
if γ is allowed to change throughout the interval [5,10].



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Thermooptic Noise



When using doped Tantala (with almost halved loss-angle) thermo-optic noise should be included in the total noise budget.

$$S_{Thermo-optic}^{(\Delta x)} = \frac{2^{1/2} k_B T^2}{\pi r_0^2 \sqrt{\omega k_s \rho_s C_s}} \left(\frac{\Delta x_{TO}}{\Delta T} \right)^2, \quad \frac{\Delta x_{TO}}{\Delta T} = \frac{\Delta x_{TE}}{\Delta T} + \frac{\Delta x_{TR}}{\Delta T}$$

For positive $\alpha_{L,H}$ and $\beta_{L,H}$, the thermoelastic & thermorefractive displacements Δx_{TE} and Δx_{TR} have opposite signs. If added coherently, they *cancel in part* [M. Evans, 2008]

How does this result impact on coating optimization ?



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Thermooptic Noise Cancellation



Formulas:

$$\left(\frac{\Delta x_{TR}}{\Delta T} \right) \quad [\text{V.B. Braginsky et al., Phys. Lett. A271 (2000) 303;} \\ \text{I.M. Pinto et al., LIGO-T070159-00-Z}]$$

$$\left(\frac{\Delta x_{TE}}{\Delta T} \right) = N_d (\tilde{\alpha}_L d_L + \tilde{\alpha}_H d_H), \quad d_{L,H} = \frac{\lambda_0}{4n_{L,H}} (1 \pm \xi)$$

$$\tilde{\alpha}_{L,H} = 2(1 + \sigma_s) \left\{ \frac{\alpha_{L,H}}{2(1 - \sigma_{L,H})} \left[\frac{1 + \sigma_{L,H}}{1 + \sigma_s} + (1 - 2\sigma_s) \frac{Y_{L,H}}{Y_s} \right] - \alpha_s \frac{C_{L,H}}{C_s} \left[\left(\frac{g(\omega)}{g(0)} \right)^{1/2} C_{fsm}^{1/2} \right] \right\}$$

Braginsky & Vyatchanin,
ArXiv:Cond-Mat/0302617 v5

Fejer et al., PRD 70 (2004) 082003

$\equiv \Gamma$



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Updates and Checks



- Sign error in thermorefractive term affecting previous version of our optimization code has been fixed. Other minor bugs fixed.
- Vyatchanin calculation of thermoelastic-noise finite-mirror correction factor has been re-checked ab-initio (V. Pierro); MATHEMATICA code written; Code being checked. Parametric study (what if) under way.
- Accuracy of generalized Braginsky's formula (β_{eff} for non QWL coatings) has been tested OK against brute-force (transfer matrix) calculation (drafting a LIGO-T report).



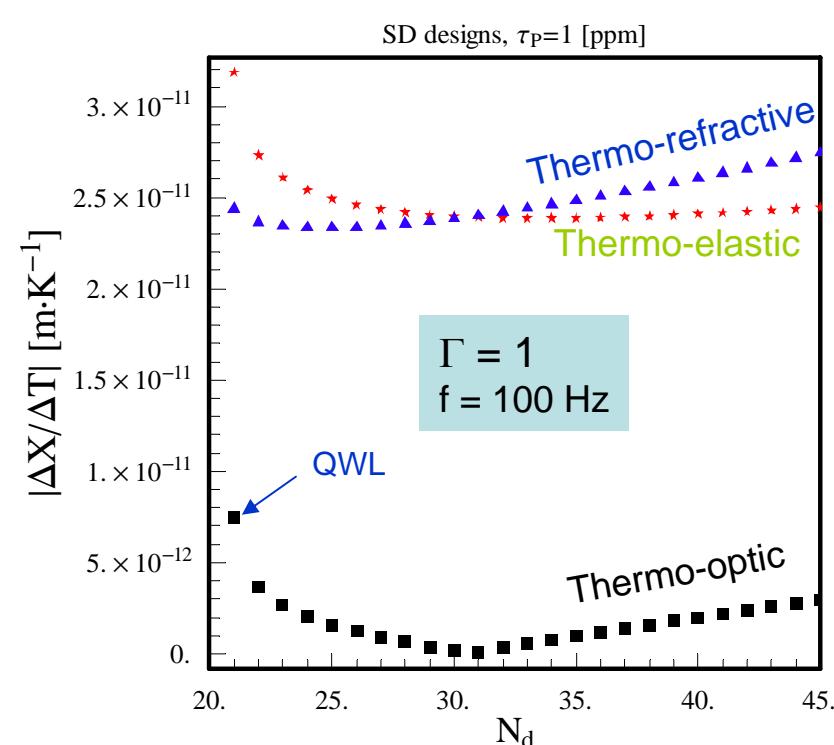
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Isoreflective Coatings: TO Noise Cancellation



Doped Tantala

$$\alpha_H = 5.0 \cdot 10^{-6}, \beta_H = 6.0 \cdot 10^{-5}$$

$$\alpha_L = 5.1 \cdot 10^{-7}, \beta_L = 1.5 \cdot 10^{-5}$$

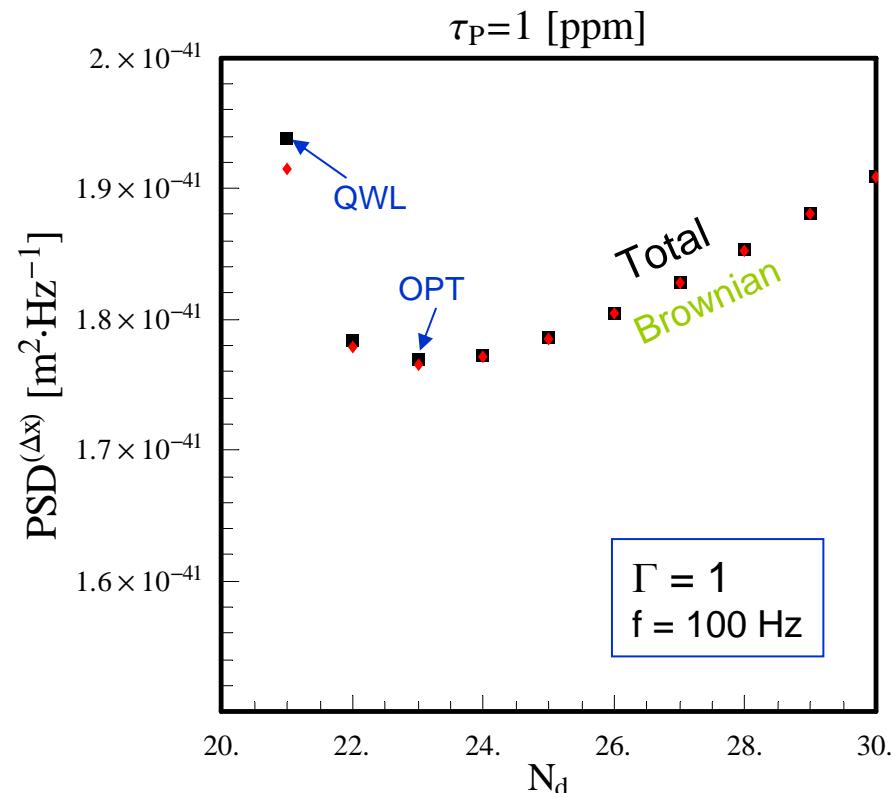


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Optimization still Worth ?



Doped Tantala

$$\alpha_H = 5.0 \cdot 10^{-6}, \beta_H = 6.0 \cdot 10^{-5}$$

$$\alpha_L = 5.1 \cdot 10^{-7}, \beta_L = 1.5 \cdot 10^{-5}$$

Optimal design : $\{Nd = 23, \xi = 0.0688726\}$
 $PSD^{(opt)} / PSD^{(QWL)} = 0.912$
 event rate boost = 1.147



Finite Mirror Correction



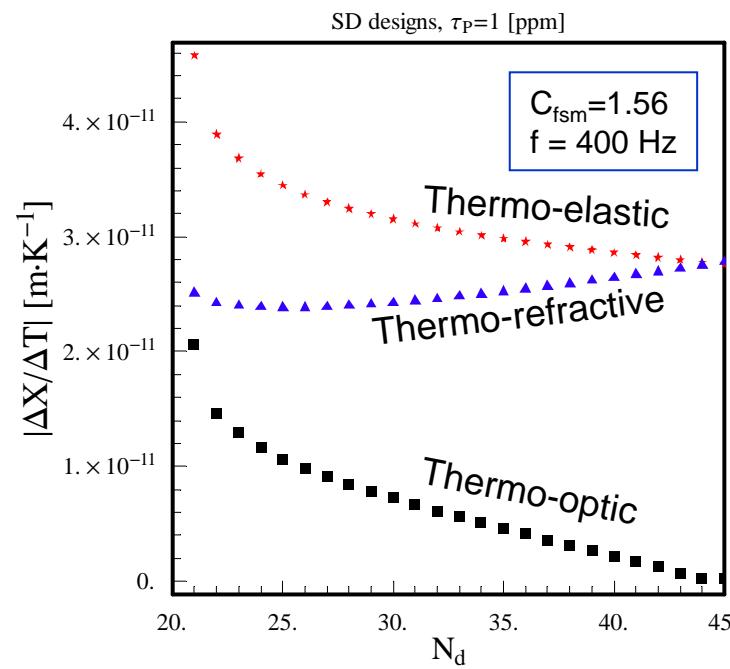
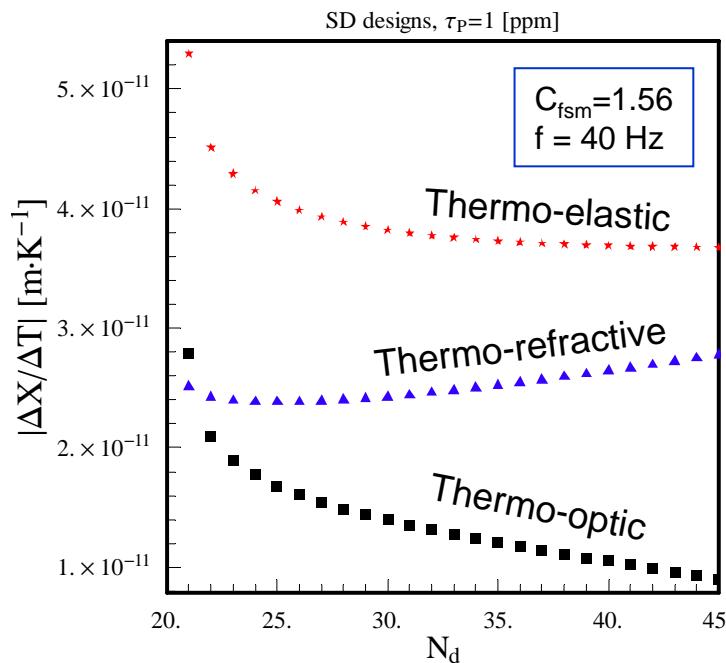
[Braginsky & Vyatchanin, ArXiv:Cond-Mat/0302617 v5]

$$R_{sub} = 0.194 \text{ m}, H_{sub} = 0.115 \text{ m}, r_{beam} = 0.06 \text{ m}$$

Doped Tantala

$$\alpha_H = 5.0 \cdot 10^{-6}, \beta_H = 6.0 \cdot 10^{-5}$$

$$\alpha_L = 5.1 \cdot 10^{-7}, \beta_L = 1.5 \cdot 10^{-5}$$



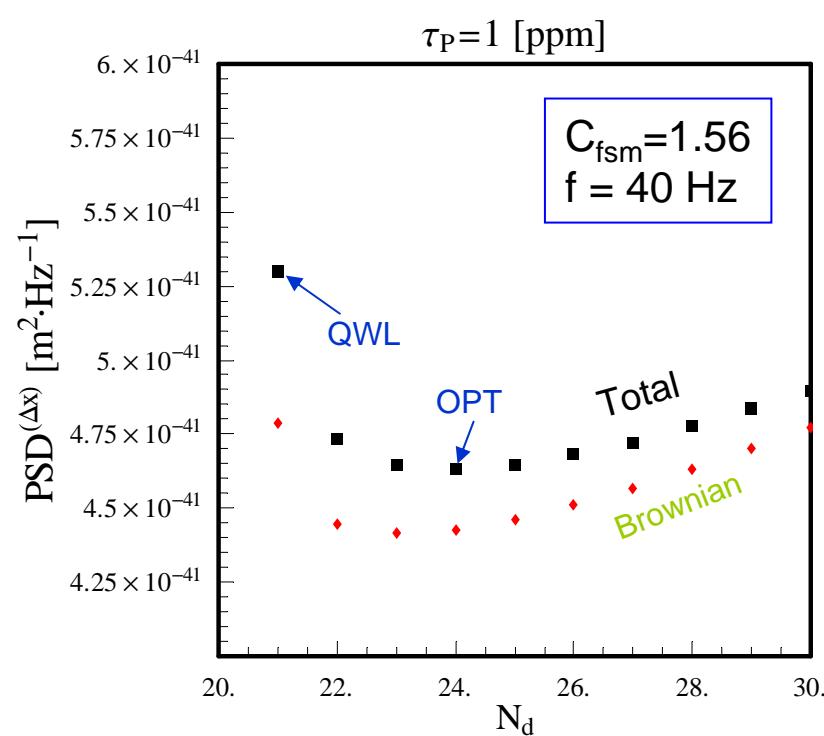
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Finite Mirror Correction



Doped Tantala

$$\alpha_H = 5.0 \cdot 10^{-6}, \beta_H = 6.0 \cdot 10^{-5}$$

$$\alpha_L = 5.1 \cdot 10^{-7}, \beta_L = 1.5 \cdot 10^{-5}$$

Optimal design : $\{N_d = 24, \xi = 0.0827096\}$

$$PSD^{(opt)} / PSD^{(QWL)} = 0.874$$

event rate boost = 1.223



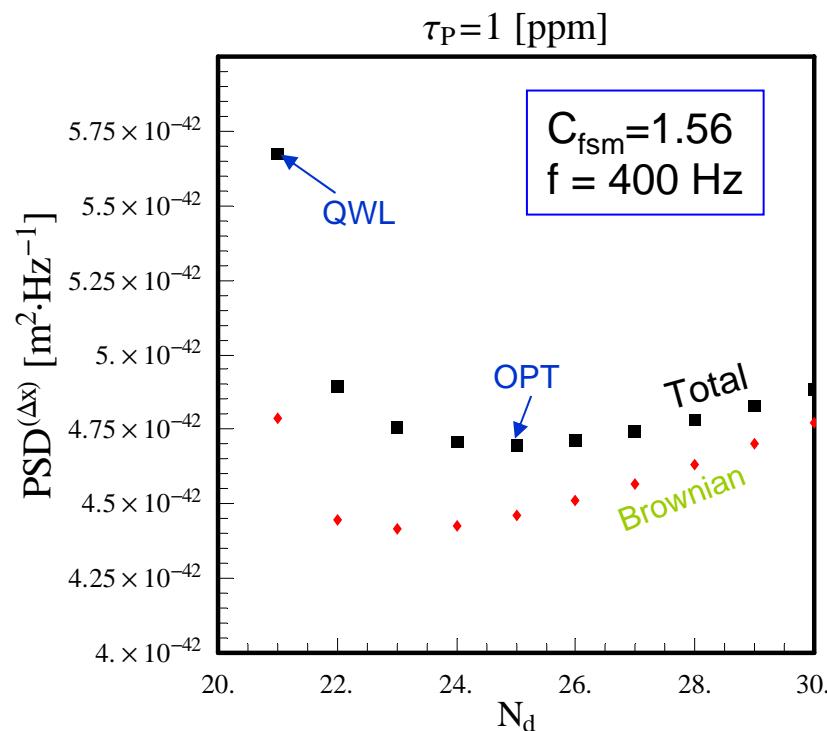
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Finite Mirror Correction



Doped Tantala

$$\alpha_H = 5.0 \cdot 10^{-6}, \beta_H = 6.0 \cdot 10^{-5}$$

$$\alpha_L = 5.1 \cdot 10^{-7}, \beta_L = 1.5 \cdot 10^{-5}$$

Optimal design : $\{Nd = 25, \xi = 0.0937243\}$
 $PSD^{(opt)} / PSD^{(QWL)} = 0.827$
event rate boost = 1.327



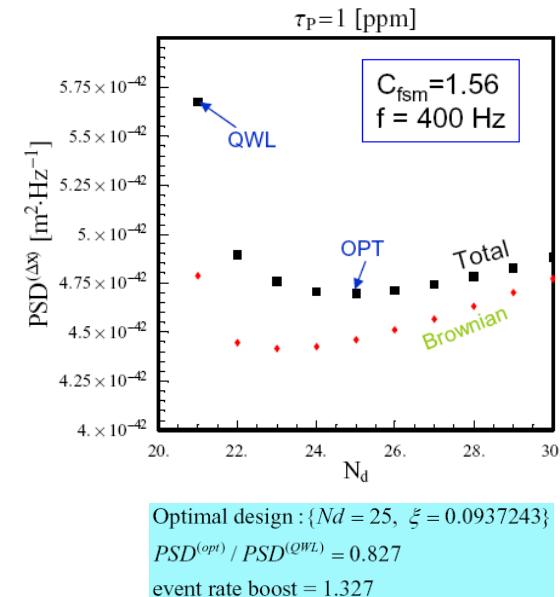
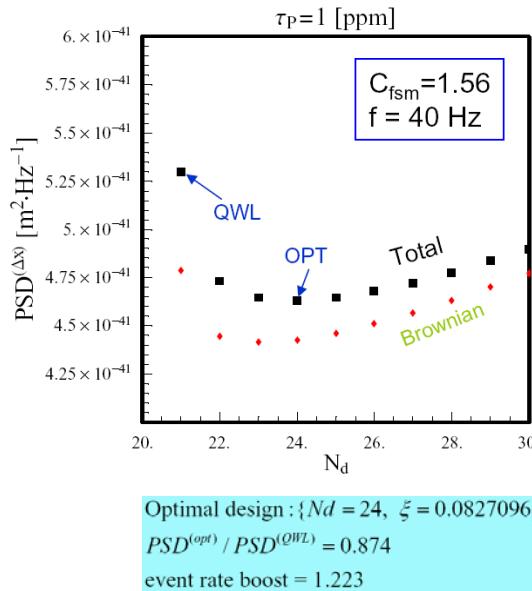
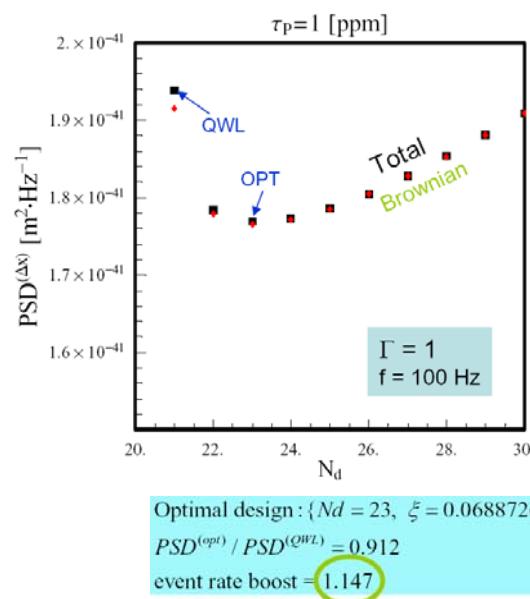
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Finite Mirror Correction



Robust (conservative) design possible (here, $N_d=24$) yielding nearly maximal noise reduction irrespective of actual value of C_{fsm} and f



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Sign of $\beta_{L,H}$



A simple model

$$\frac{dn}{dT} = \frac{(n^2 - 1)(n^2 + 2)}{6n} (\phi - 3\alpha)$$

Lorentz-Lorenz factor

$\phi = P^{-1} dP / dT$, $P \equiv$ mean polarizability

Volume expansion coefficient

Linear expansion coefficient

[L. Prod'homme, Phys. Chem. Glasses, 1 (1960) 119]

More sophisticated models account for the wavelength dependence of the polarizability, and hence of the sign of dn/dT ...

[G. Ghosh, Optics Letters, 19 (1994) 1391]

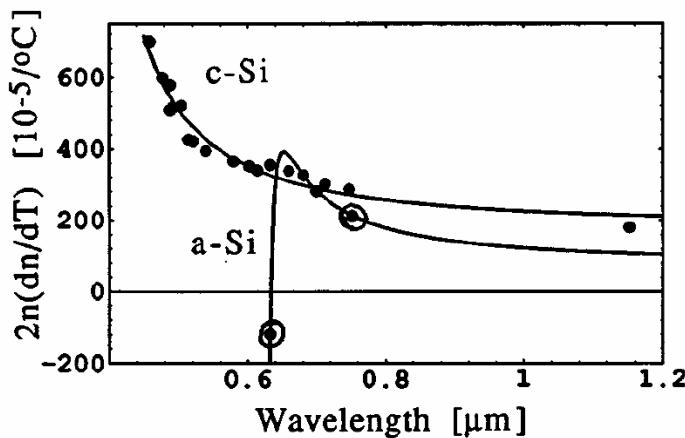
Sign depends on whether $\phi \gtrless 3\alpha$



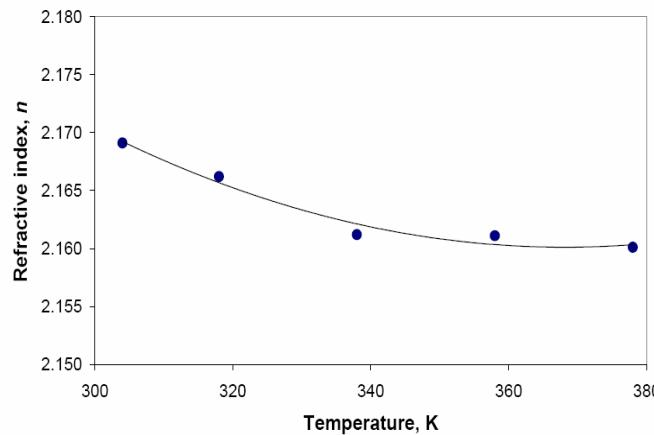
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Wavelength dependent sign of dn/dT
in amorphous Silicon [G. Ghosh Appl.
Phys. Lett., 66 (1995) 3570]



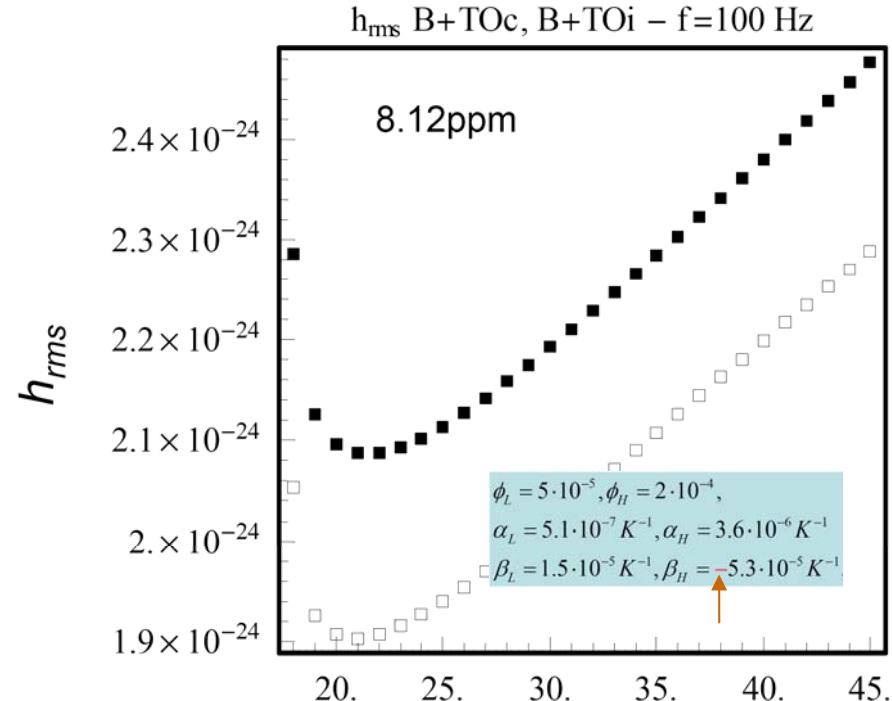
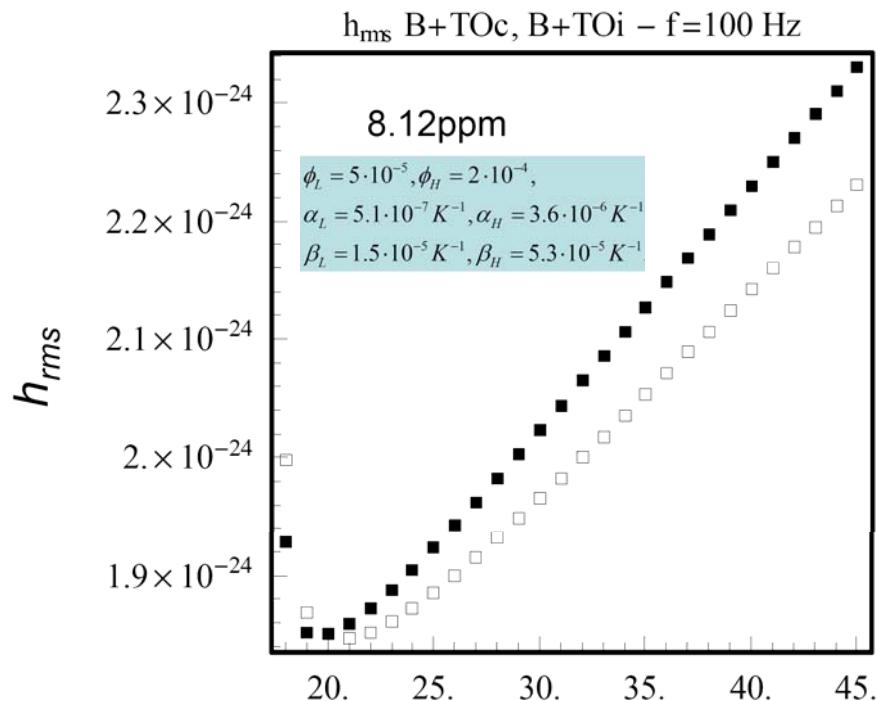
Temperature dependence of n . Titanium dioxide film at 632nm [H. Xie et al., SIMTech Reports, 9 (2008) 29]

- dn/dT in $\text{SiO}_2-\text{TiO}_2$ films with different TiO_2 concentrations at various annealing temperatures found to change from positive to negative as TiO_2 concentration increases [H. Hirota et al., Jpn. J. Appl. Phys., 44 (2005) 1009]

and more...



Flipping the β_H Sign



Both cases, $N_d = 21$ nearly-optimal



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Tentative Conclusions



- Partial cancellation between the thermoelastic and thermorefractive noise occurs if $\alpha_{L,H} > 0$ and $\beta_{L,H} > 0$.
- The QWL design *does not* yield the best cancellation;
- Uncertainties in the values of the thermoelastic and thermorefractive parameters and inclusion of the finite mirror correction factor affect the amount of noise reduction achievable through optimization. A worst-case event-rate boost $\sim 15\%$ may be expected (doped Tantala).
- A robust (conservative) design seems possible, in view of the *broad* minimum exhibited by the PSD vs N_d curves, yielding close-to-maximal noise reduction over a broad range of material parameters and substrate geometries.



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