

ISC

# INTERFEROMETER SENSING AND CONTROL

LSC Meeting  
Hannover Germany  
October 23, 2007

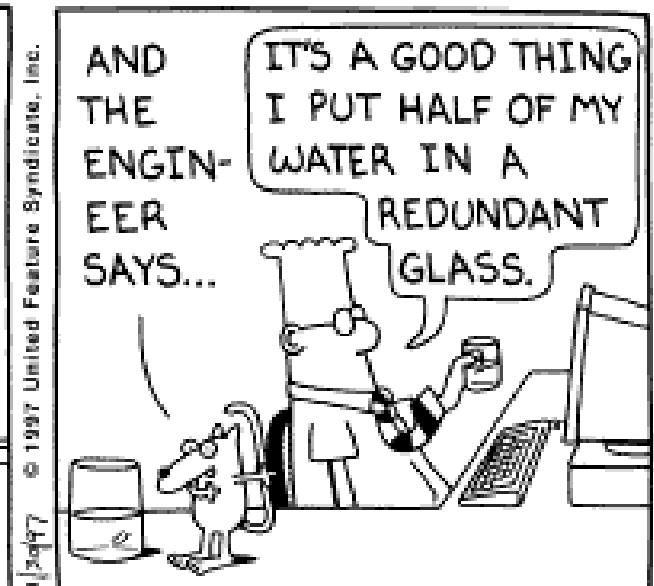
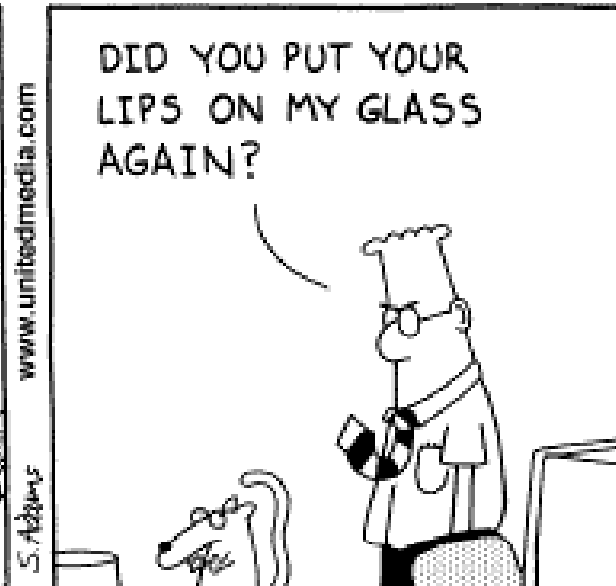
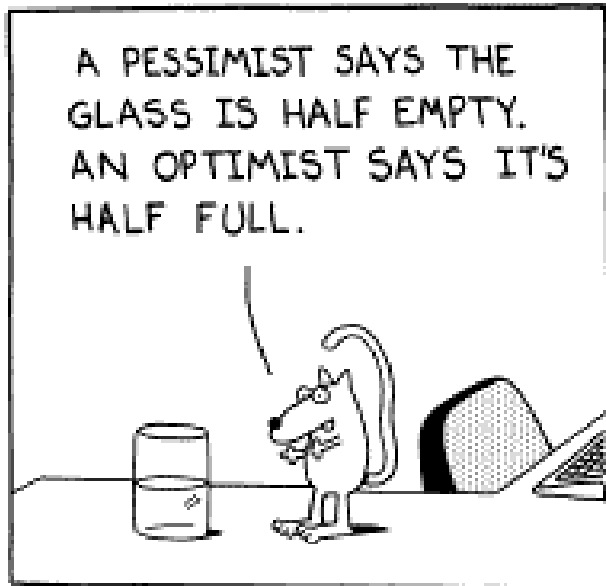
# Outline

- Length Sensing and Control (LSC)
  - Current baseline design (9.4 MHz and 47 MHz)
  - Noise modeling for all length loops
- Lock Acquisition
  - Ideas and modeling status
- Angular Sensing and Control (ASC)
  - Requirements and modeling status

# Baseline design, Guidelines

- No high RF frequencies ( $< 100\text{MHz}$ )
- Good sensitivity for all length DoF
- Should allow the following modes
  - 125 W, no det.: Simple control, 95% of sensitivity
  - 125 W,  $8^\circ$  SR det.: Optimized for NS binaries
  - 4 W,  $55^\circ$  SR detuning: Optimized for BH binaries

# Baseline design, Guidelines



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# Mirror Transmissions

- $T_{ITM} = 1.0\%$  Finesse 620, better for lock acquisition, o.k. for MICH coupling and BS thermal load
- $T_{PRM} = 3.6\%$  Slight over-coupling, better tolerance for unexpected losses
- $T_{SRM} = 12\%$  Optimal tuning for NS and BH binaries, not very critical  
**NO narrow-band tuning without SR mirror swap!**

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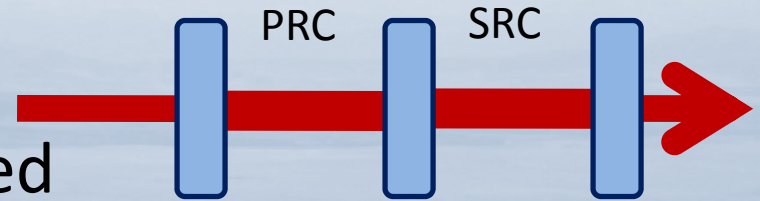
**That's Kindergarten!**  
**(anonymous GEO scientist)**

# Sidebands

- Power Recycling Sideband:  $f_1 = 9.4 \text{ MHz}$ 
  - Resonant in PRC only
  - CARM and PRC sensing
- Signal Recycling Sideband:  $f_2 = 47 \text{ MHz}$ 
  - Resonant in SRC & PRC
  - MICH and SRCL sensing

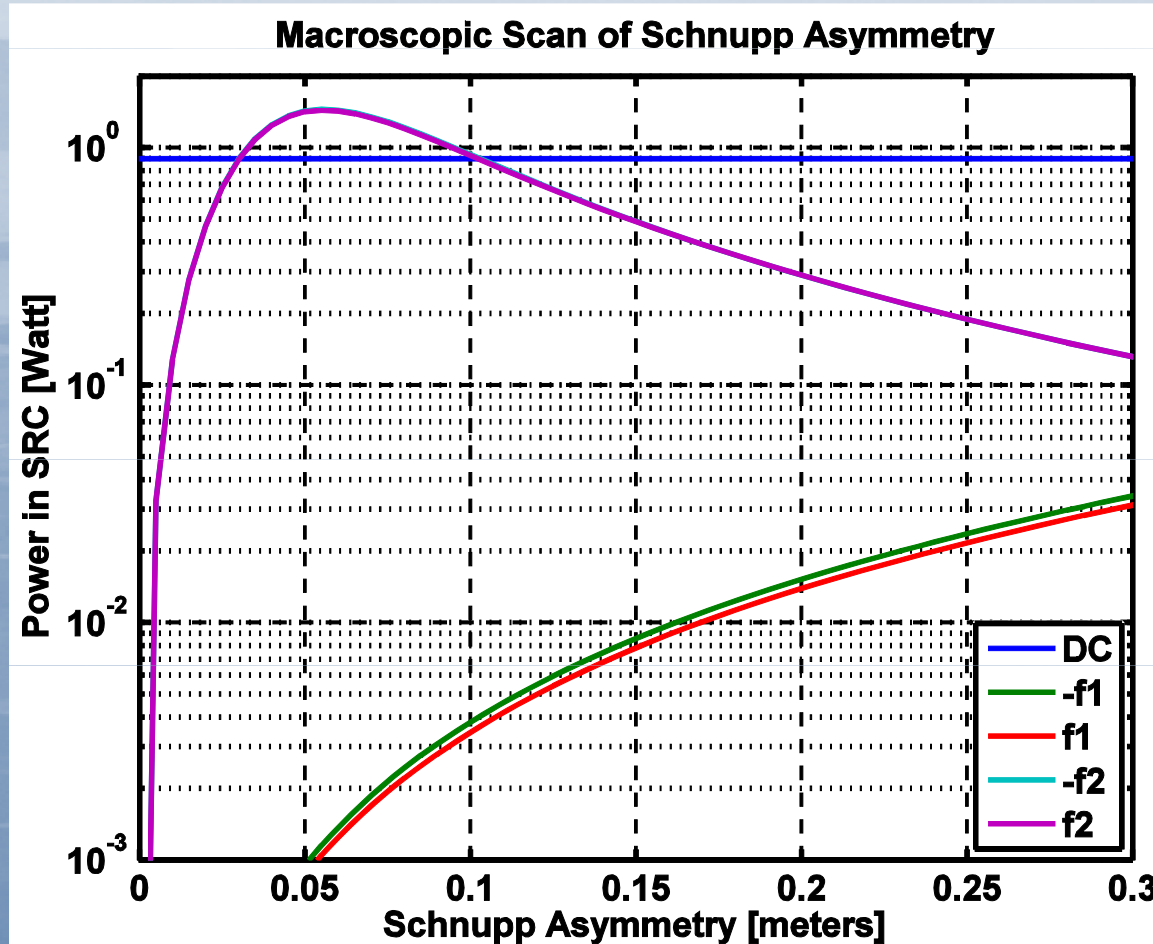
# Schnupp Asymmetry

- Maximize  $f_2$  in SRC
  - Triple cavity critically coupled
- 2 Solutions
  - SRC over- or under-coupled (as seen from PRC)
  - Results in 2 possible Schnupp asymmetries:
    - large :  $l_{asy} = 1 \text{ m}$        $T_{asy} = 0.7$
    - small :  $l_{asy} = 5 \text{ cm}$        $T_{asy} = 1.1e-3$
- **Picked 5 cm** (larger reduction of  $f_1$  in SRC)





# Schnupp Asymmetry



# Cavity length

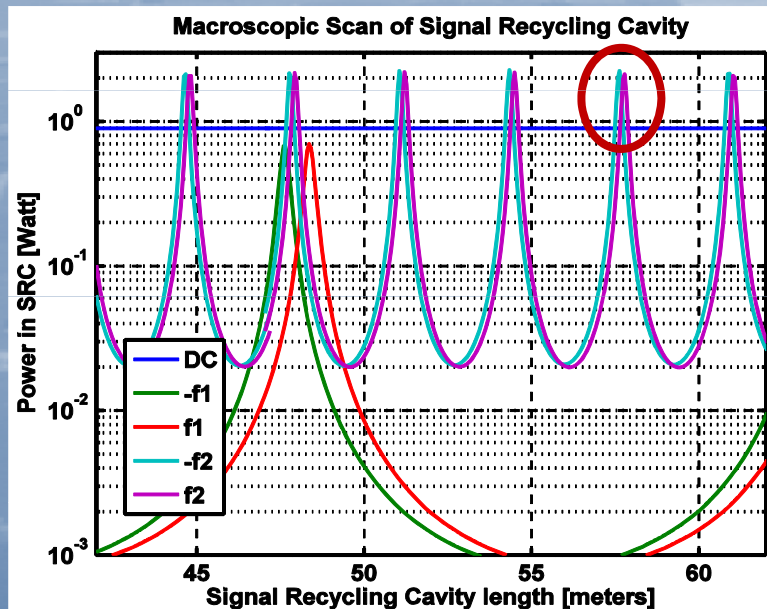
- PRC (stable, folded)

$$l_{\text{PRC}} = \left( N + \frac{1}{2} \right) \frac{c}{2f_1} = 55.815\text{m, for } N = 3$$

- SRC (stable, folded)

$$l_{\text{SRC}} = M \frac{c}{2f_2}, \text{ but not } Q \frac{c}{2f_1}$$

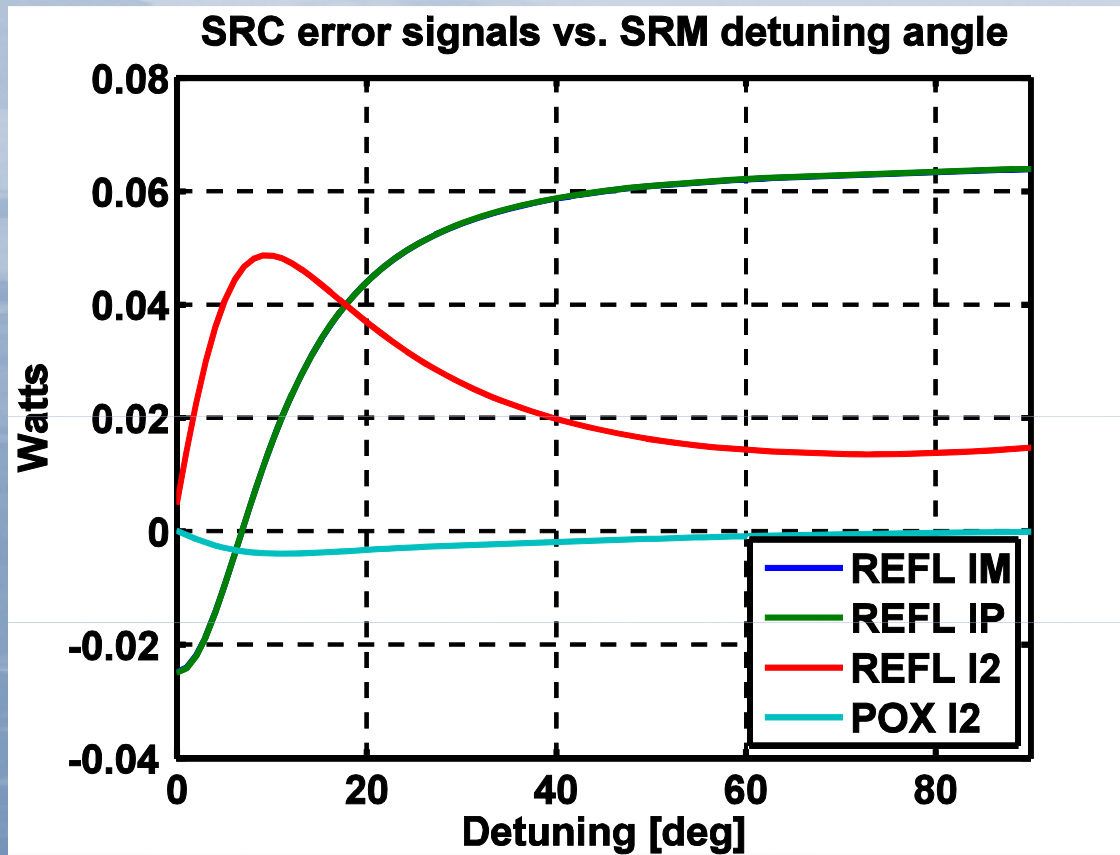
$$= 57.410\text{m, for } M = 18$$



# Error Signals

- DARM      AS DC      DC readout
- CARM      REFL I1       $f_1$  in reflection
- PRCL      POX I1       $f_1$  at pick-off
- MICH      POX Q2       $f_2$  at pick-off ITMX
- SRCL      REFL IM / IP      Demod at  $f_2 \pm f_1$
- REFL I2 / POX I2       $f_2$  any port (no det.)

# Error Signals for SRC



# Sensing Matrix in Watt/meter at 1kHz

125 Watt, 8° SR detuning

Port	CARM	DARM	PRCL	MICH	SRCL
AS DC	5.7e+05	<b>3.4e+09</b>	2.5e+06	8.8e+06	9.9e+06
REFL DC	3.8e+06	1.4e+06	1.8e+07	1.9e+06	2e+06
REFL I1	<b>1e+08</b>	2.2e+06	8.8e+07	4.1e+06	2e+03
REFL Q1	1.6e+04	5e+02	5.5e+04	1.4e+04	52
REFL I2	1.2e+07	1e+06	2.3e+07	2.7e+06	9.8e+05
REFL Q2	2.3e+06	2.8e+05	3.5e+06	1.1e+07	7.1e+04
REFL IM	5.4e+04	2.2e+03	<b>2.5e+07</b>	7.3e+05	<b>3.3e+06</b>
REFL QM	1.3e+04	5.4e+03	5.8e+06	2e+06	5.6e+05
REFL IP	5.4e+04	2.2e+03	2.5e+07	7.2e+05	3.3e+06
REFL QP	1.3e+04	5.5e+03	5.8e+06	2e+06	5.6e+05
POX DC	2.5e+03	5.9e+07	2.3e+05	1.5e+05	9e+04
POX I1	8.4e+05	2.7e+06	<b>7.3e+06</b>	6.4e+04	1.1e+04
POX Q1	2.6e+02	2.3e+03	1.2e+03	1e+04	3.6e+02
POX IM	61	21	8.2e+03	7.5e+03	2.8e+04
POX QM	2.4e+02	19	9e+04	7.5e+03	4.9e+03
POX IP	62	21	8e+03	7.6e+03	2.8e+04
POX QP	2.4e+02	19	9e+04	7.3e+03	4.9e+03
POX I2	4.6e+05	1.3e+06	1.5e+06	1.8e+05	1.1e+05
POX Q2	2e+05	6.4e+05	8.2e+05	<b>9.8e+05</b>	1.6e+04

# SRC to DARM coupling via Radiation Pressure

- SRC to DARM coupling:
  - SRM displacement noise modulates carrier returning to BS from anti-symmetric side
  - Causes power imbalance in arms
  - Couples to DARM via radiation pressure
- Drives SRM displacement noise requirements
- Requires SRC to DARM correction path (for SRC sensing noise)
- **SRC sensing is critical!**

# Correction paths

- Old trick: feed known noise in Aux loops to DARM
  - Cancels optical couplings
- Needed with  $\sim 1\%$  accuracy for
  - MICH loop (coupling :  $1/\text{Finesse}$ )
  - SRCL loop (coupling: radiation pressure)
    - Need to track arm power with 1% accuracy

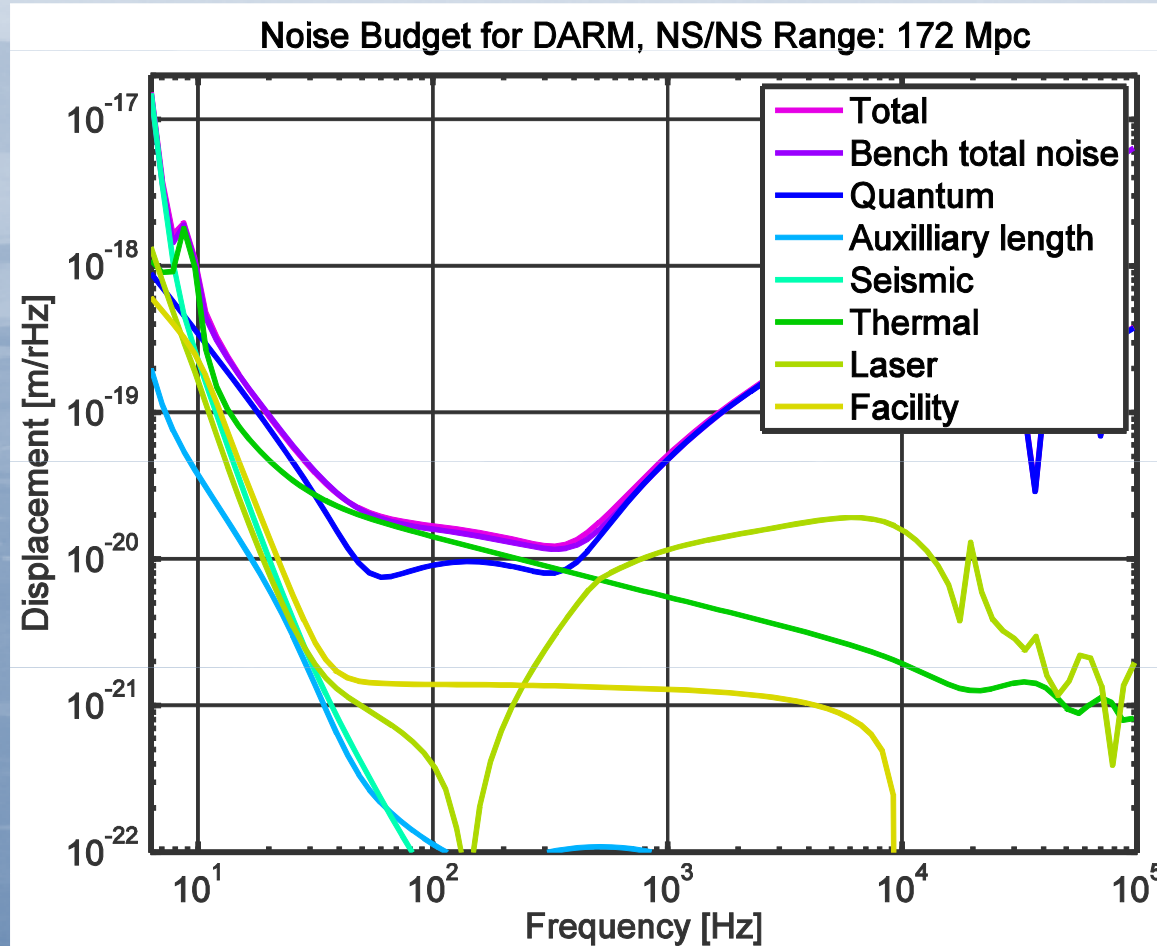
# Noise Modeling

- Done with:
  - *Optickle* (see Matt Evans' talk)
  - *loopticke* add-on for closed-loop system, noise propagation & plotting
- Includes
  - Quantum noise at all ports (Shot & Rad. pressure)
  - Seismic noise at all large optics
  - Thermal (Suspension & Mirror)
  - Laser (Freq., Intensity, Oscillator phase & ampl.)
  - Facility (Residual Gas & Gravity Gradient)



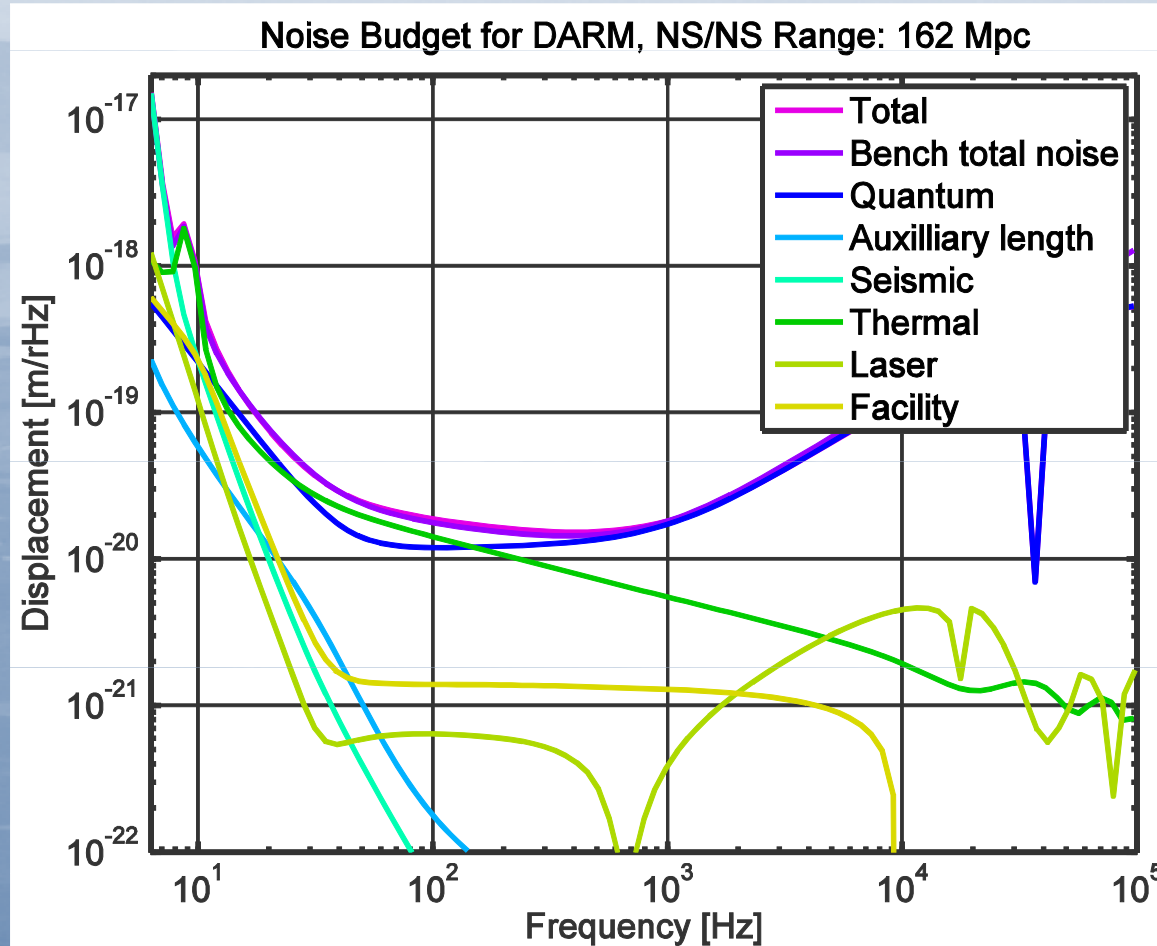


# Noise Budget DARM



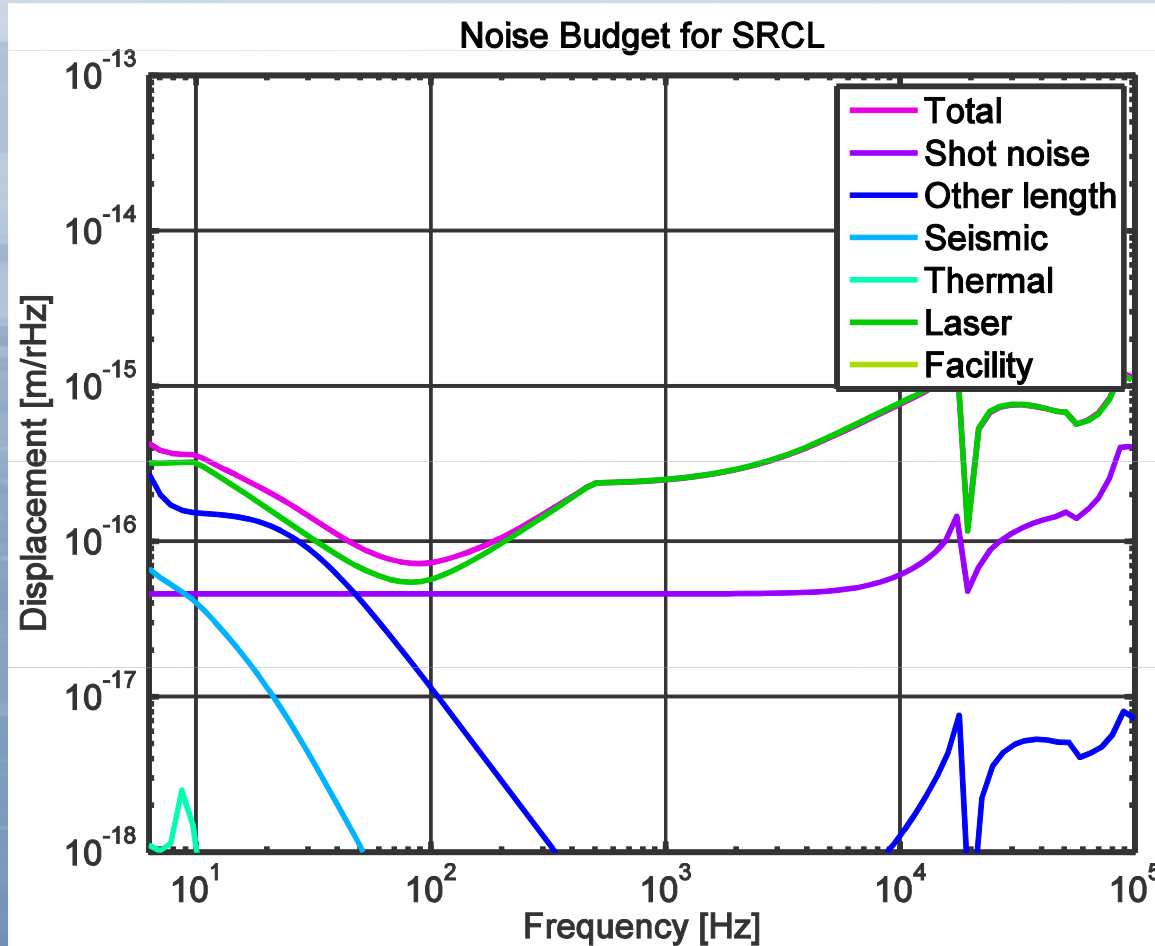
8° SR det.

# Noise Budget DARM



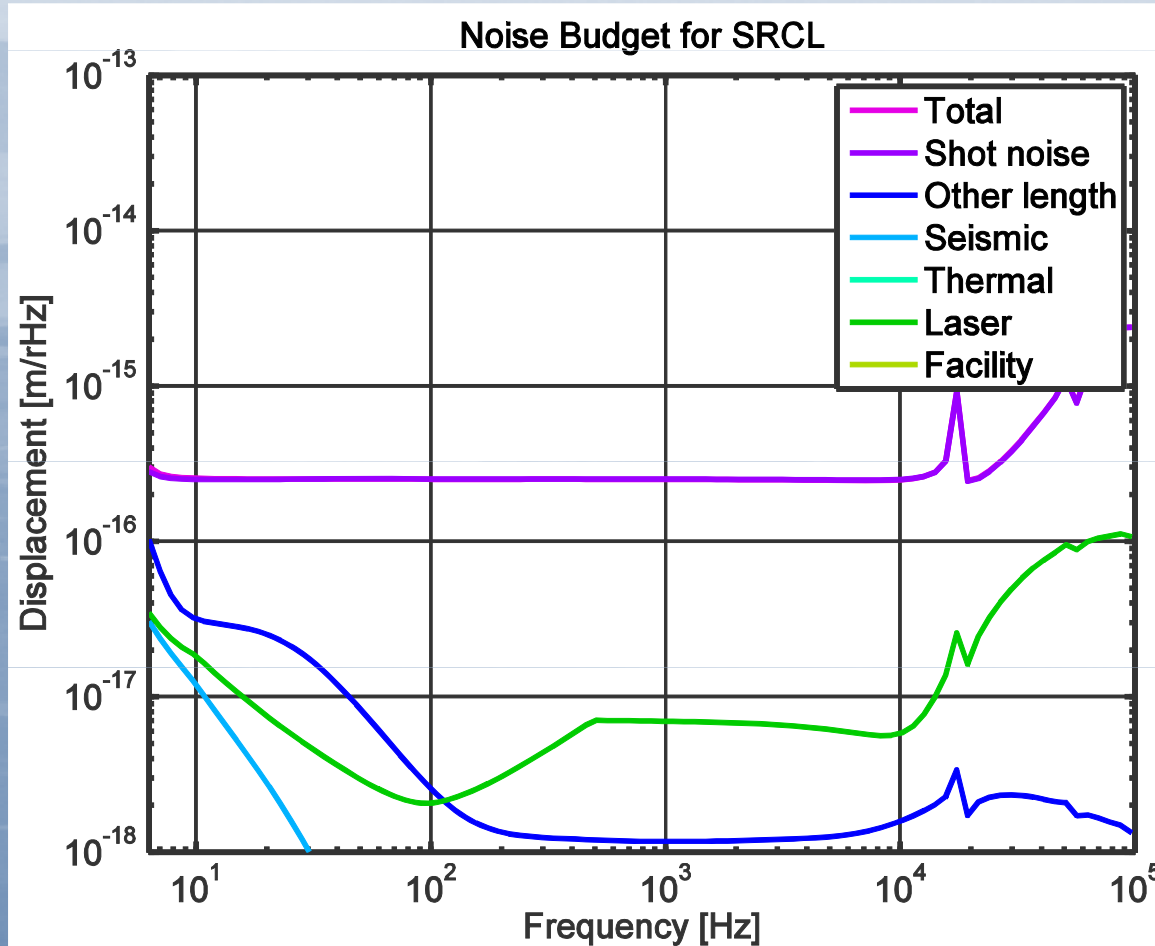
no SR det.

# Noise Budget SRCL



8° SR det.

# Noise Budget SRCL



no SR det.

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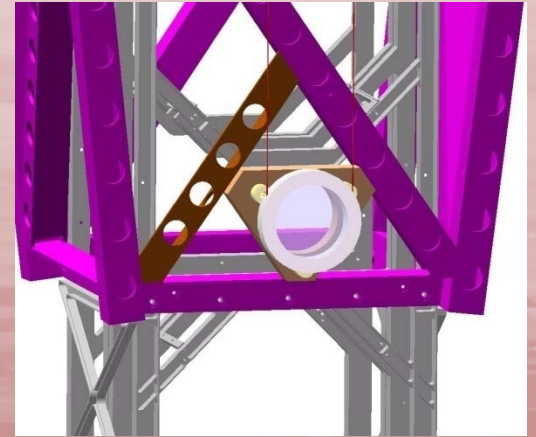
# Lock Acquisition for AdvLIGO

(BroadBand configuration)

- SPI/ PRN - Scenario in which we can control the arm position within a few nm
- 40m technique: “lock acquisition path” defined by detuning the arm cavities (CARM offset)



*Reasonable hypothesis of being able to approach the operating point starting with CARM off resonance and moving it to the working point*



- Search for “good” error signals during the “lock acquisition path” (*Optickle*)
- Test of the designed control scheme in the time domain (*E2E*)

# Lock Acquisition for AdvLIGO

(BroadBand configuration)

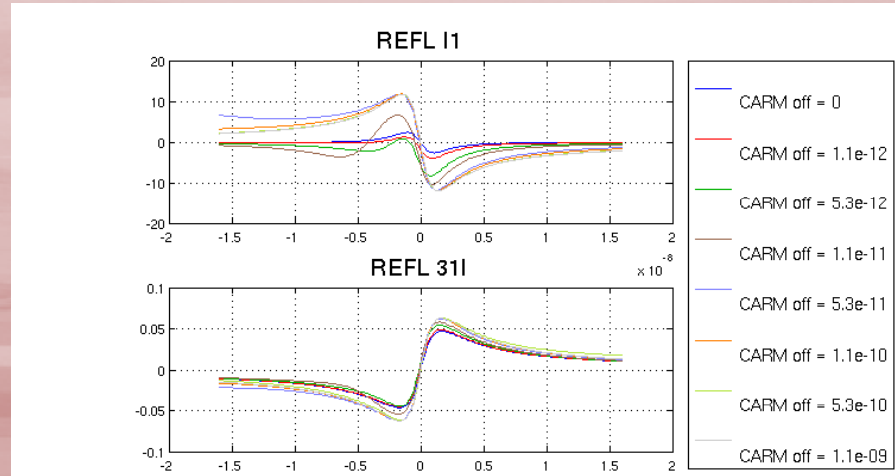
Modeling, by Lisa Barsotti

- Starting point for lock acquisition: arm cavities off resonance

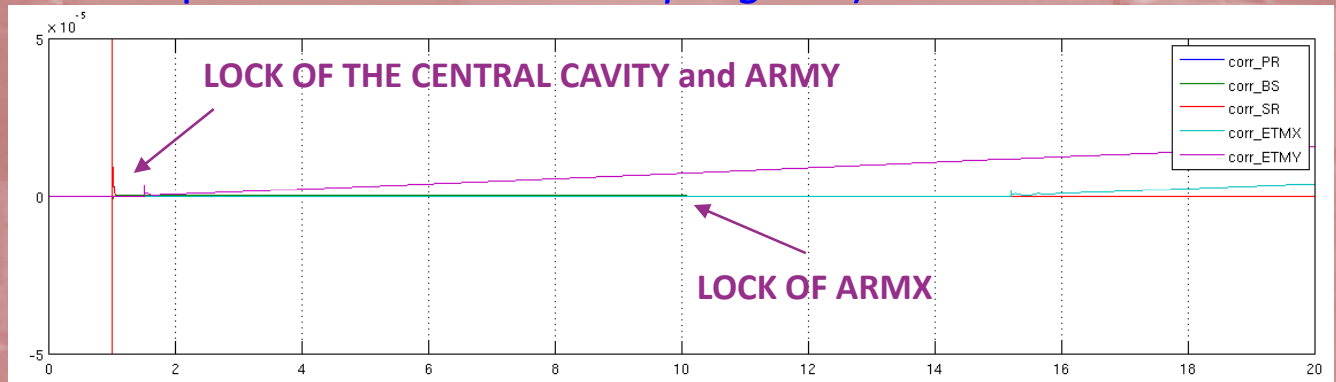
- Signals at the reflection port (REFL) demodulated at  $3x f_1$  &  $3x f_2$ : good error signals for the central cavity (PRCL, MICH, SRCL)

→ independent from arm cavity pos.

- Locking simulation, using *Optickle* adiabatically (full lock acquisition sequence test in E2E – *in progress*)



Lock of the cavities off resonance



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# ASC Requirements

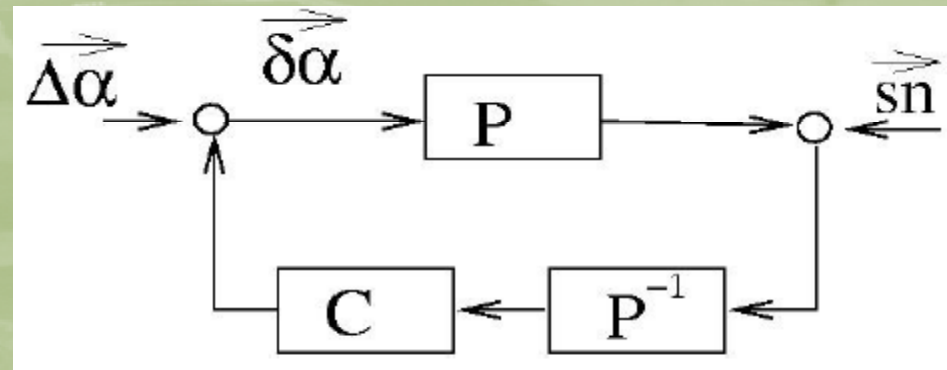
- RMS stability:  $10^{-9}$  rad RMS (TM's)  
 $10^{-8}$  rad RMS (BS, RM's)
  - Beam jitter driven
  - Assures centering:  $\Delta l < 100\mu\text{m}$
- Same sidebands  $f_1$  &  $f_2$

# ASC Requirements

- NS/NS (8° SR detuning)
  - TM:  $8 \times 10^{-15} \text{ rad/rtHz}$  @ 10Hz,  
 $4 \times 10^{-16} \text{ rad/rtHz}$  @ 30Hz,  
 $2 \times 10^{-16} \text{ rad/rtHz}$  @ 50Hz
  - RM:  $3 \times 10^{-12} \text{ rad/rtHz}$  @ 10Hz  
(independent of beam size!)
- **→ No safety margin!**

# ASC modeling

- **Based on Valera Frolov's code**
  - all signals still scaled with 6cm beam size
  - results for recycling cavity mirrors need to be multiplied by  $\sim 30$  (beam size ratio on mirrors)
- **Shot noise: not yet fixed.**
  - Still some factor 2 type uncertainty
  - have theory but not implement it yet



# ASC modeling

- **NS/NS Case: Pin= 125W (Current status)**

– Loop Gain:      3Hz    3            RM    1  
                          10Hz   1                    0.3  
                          30Hz   0.3                   0.03

- **Simulation:**

frad/rtHz	Port	Sensor	3Hz	10Hz	30Hz
PR	BP f1	0.8	0.4	0.2	0.03
SR	DP f2	105	52	24	3
DITM	DP f2	0.3	0.26	0.17	0.08
CITM	BP f1	0.9	0.7	0.47	0.22
DETM	DP f2	0.1	0.09	0.06	0.03
CETM	BP f1	1.6	1.2	0.8	0.37

- **Requirements(frad/rtHz):**

– 10Hz: 8 (TM)    30Hz: 0.4 (TM)            10Hz: 3000 (RM)

# Conclusion

- LSC: 9.4 MHz and 47 MHz modulation scheme for detuned and non-detuned case looks o.k.
- Locking: Use SPI / PRN for arms  
3f signals
- ASC: First modeling suggests it's doable,  
but no margin  
More work needed

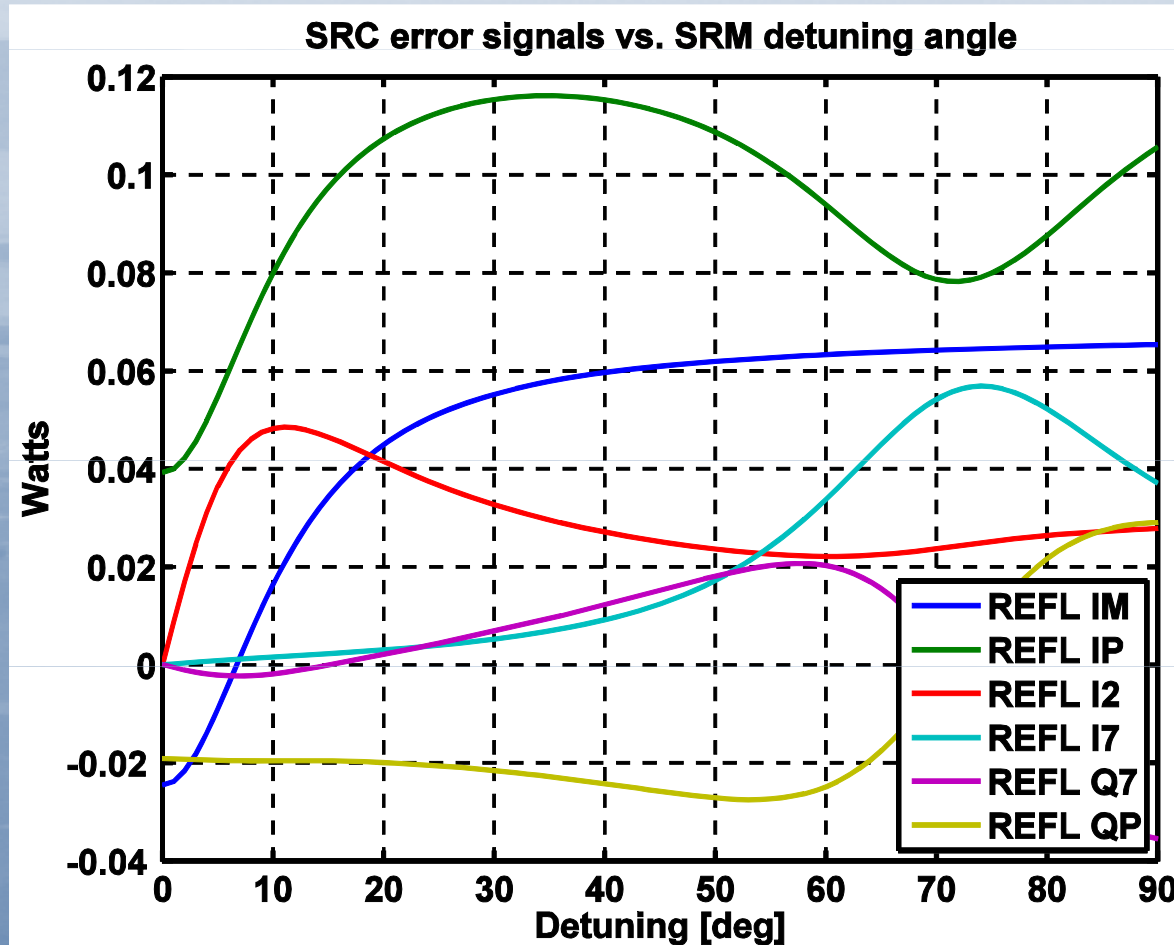
ISC

THE END

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- SRCL      REFL IM / IP      Demod at  $f_2 \pm f_1$
- REFL I2 / POX I2       $f_2$  any port (no det.)
- REFL I7       $f_7 = 7 \times f_1$ ; Option for large detuning ( $55^\circ$ )

# Error Signals for SRC



With  $f_7$  sideband



# Mirror Transmissions

