



# **Squeezing for GW Interferometers and Servo Enhanced Cooling in a Optomechanical System**

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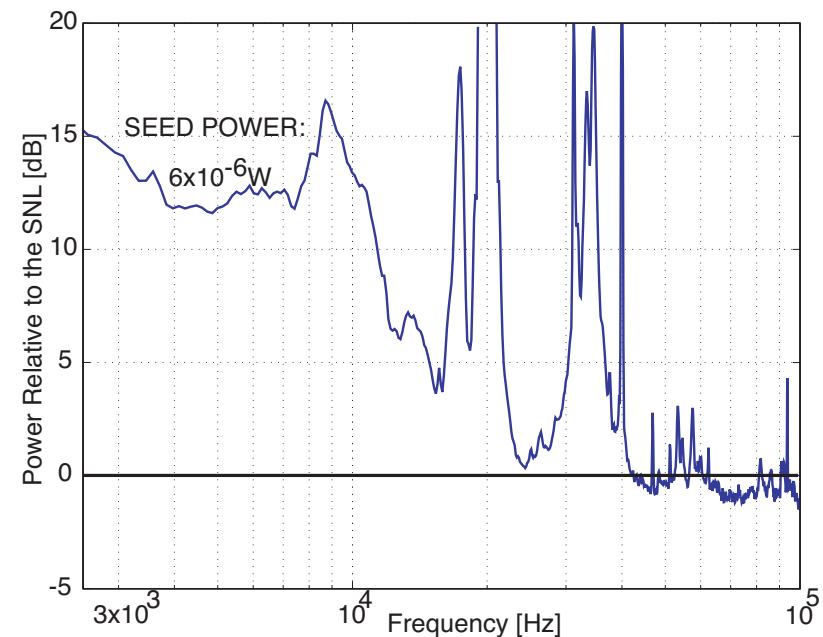
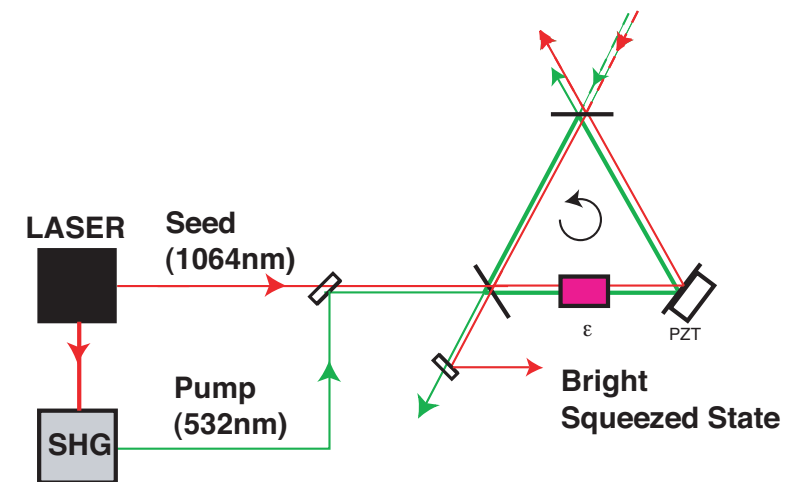
The Australian National University

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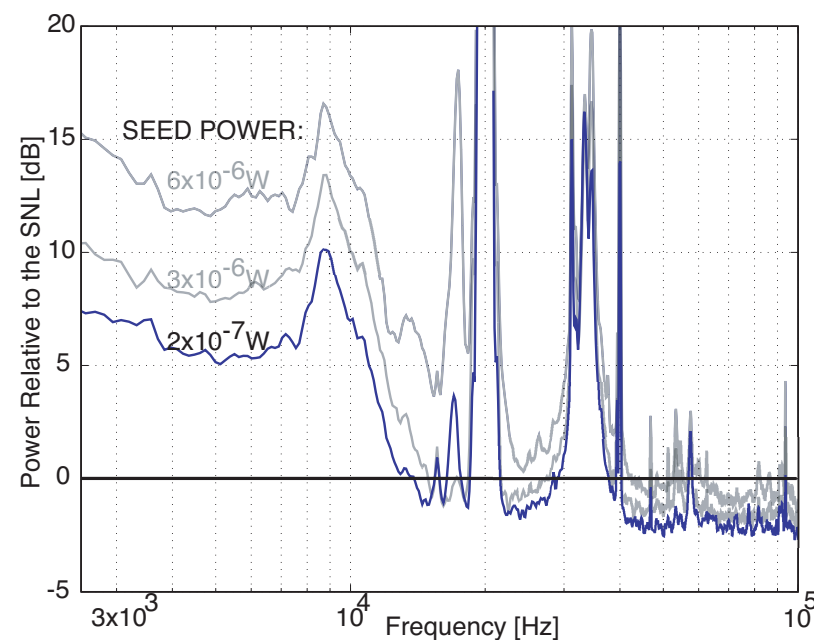
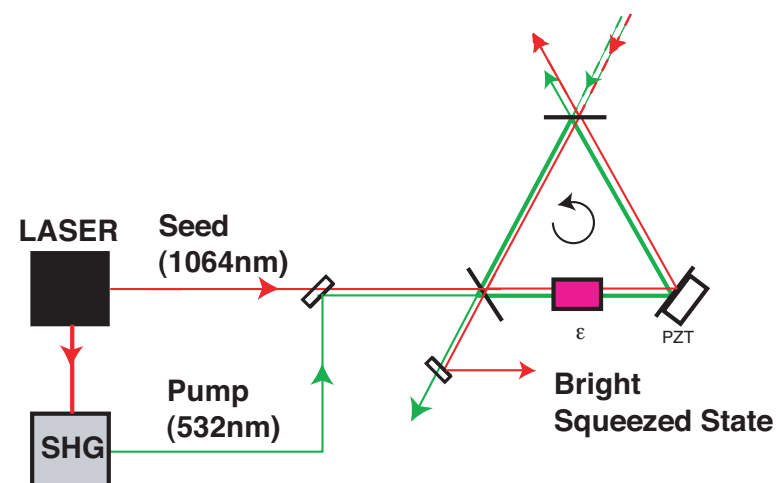
# Producing LF Squeezing

- Use **Parametric Amplification**
- Noise sources that can mask squeezing
  - **Pump** intensity and phase noise
  - **Seed** intensity and phase noise
  - Cavity length fluctuations
- These noise sources **do not couple** to the squeezed state when, operated below threshold and vacuum seeded.



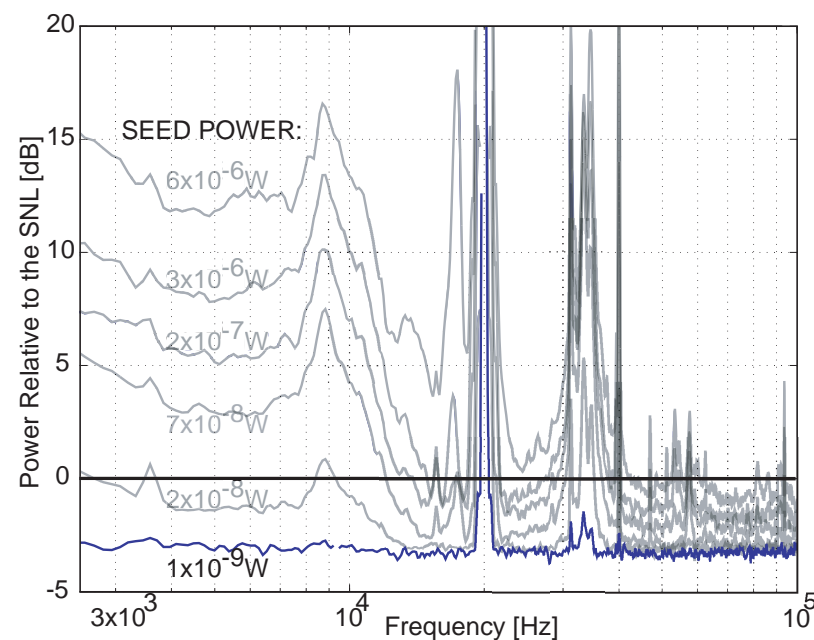
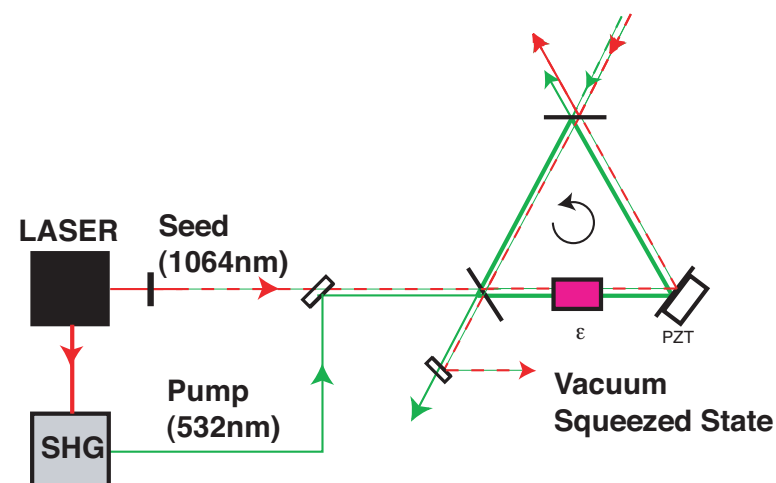
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# Key Technologies

## ■ Doubly Resonant

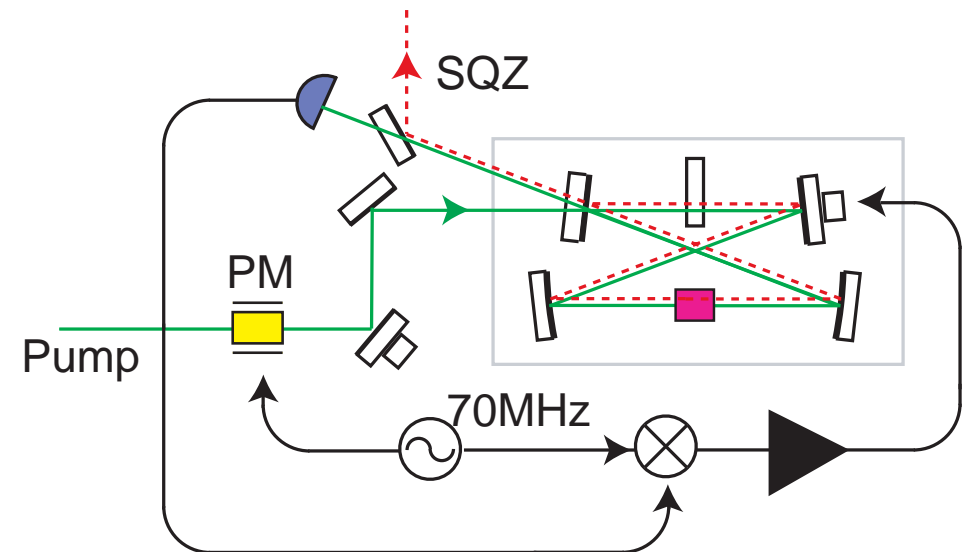
- Use pump for cavity length control
- Large effective pump power
- Extra d.o.f. The relative resonance condition of 532nm & 1064nm

## ■ Traveling-Wave cavity

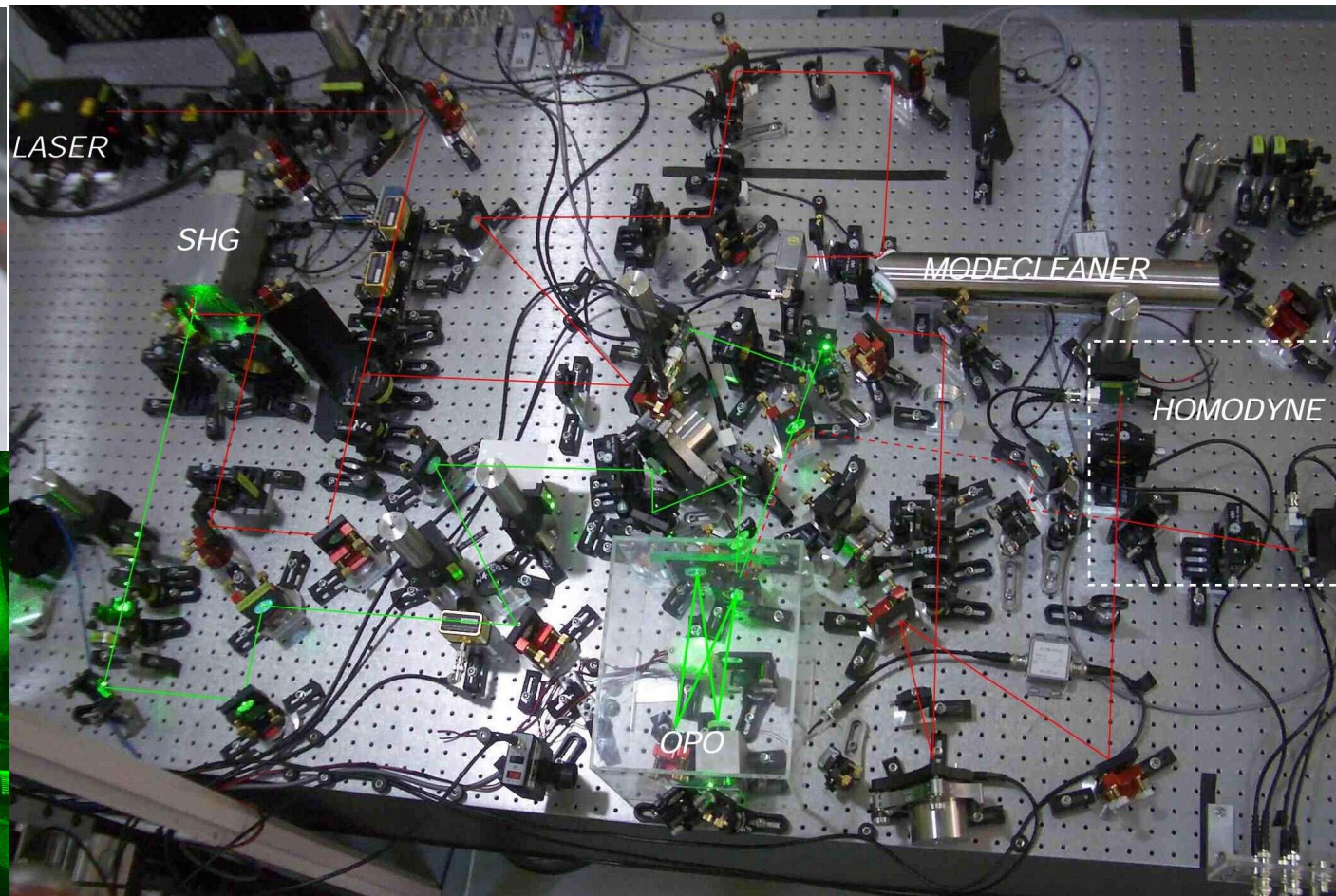
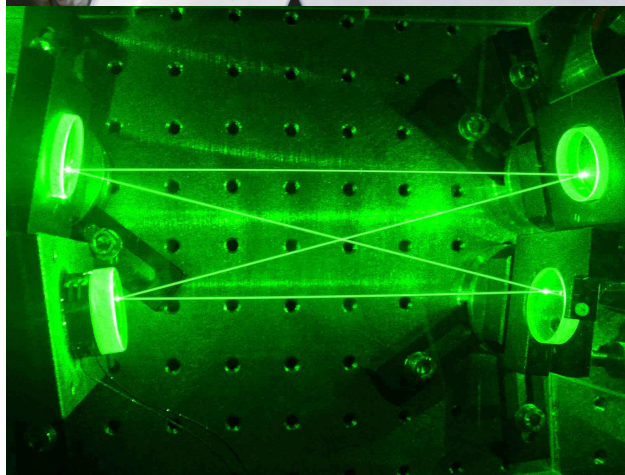
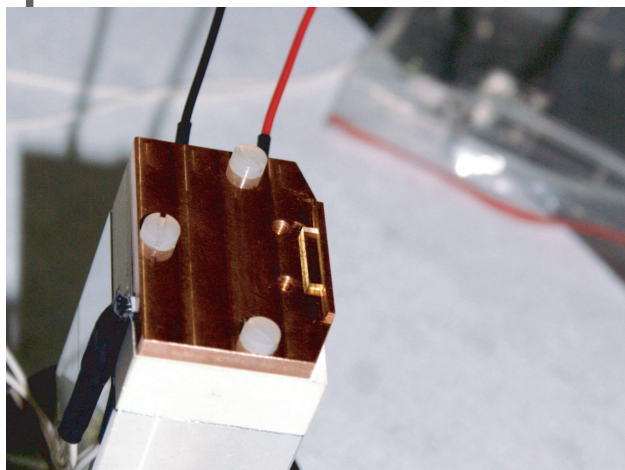
- Isolation from backscatter

## ■ Crystal: Periodically poled potassium titanyl phosphate (PPKTP)

- High nonlinearity, phase matched at 37°C
- No sign of grey tracking.

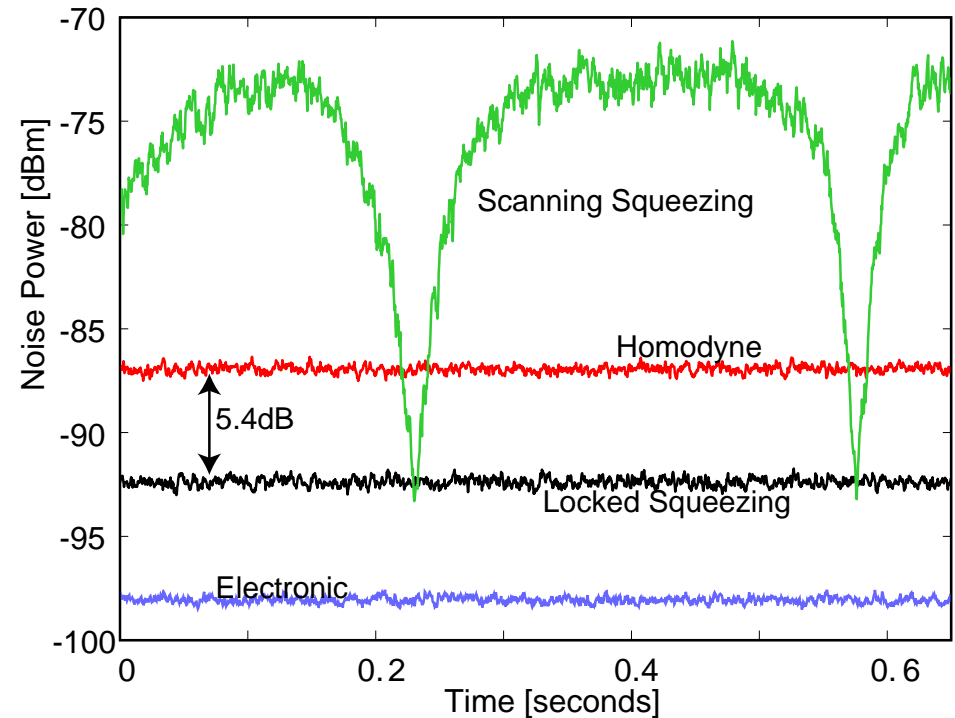


# Photos



# Quadrature Scan

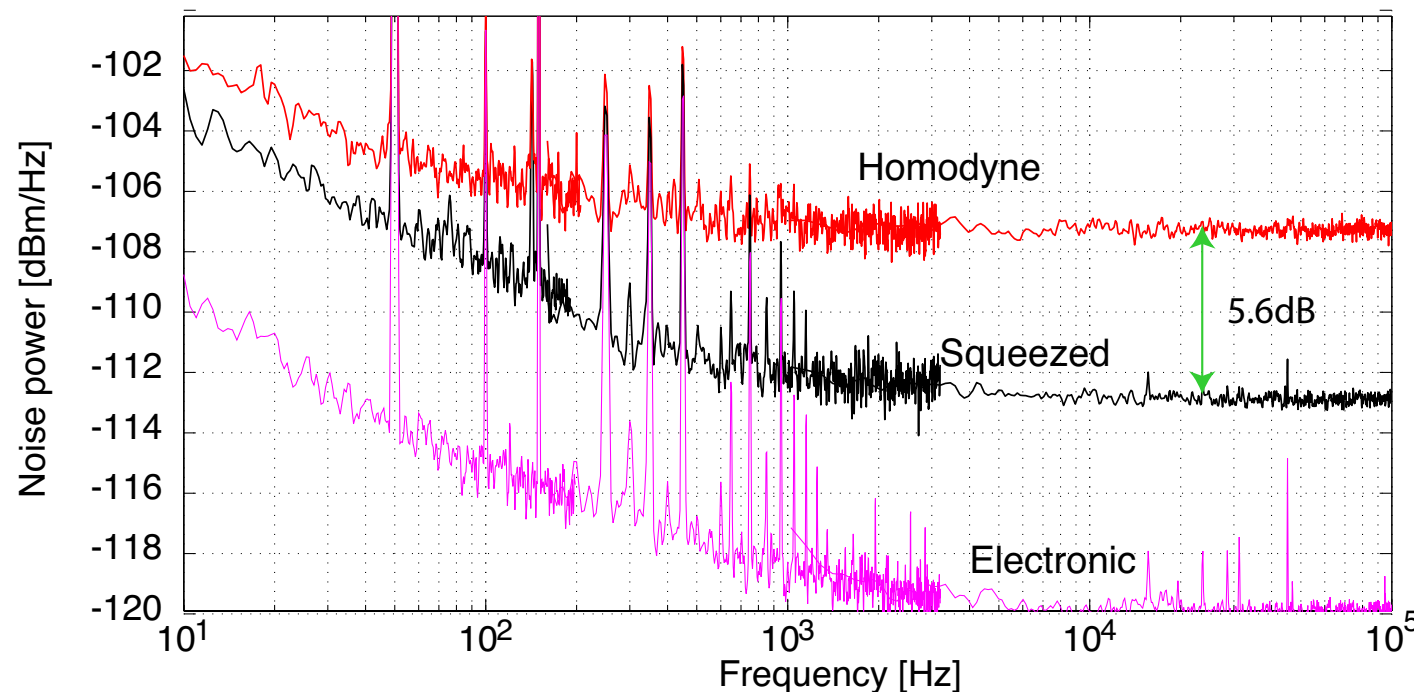
- Measured squeezing = 5.4dB
  - Subtract electronic noise = 6.5 dB
- Total Det efficiency = 83%
  - OPO Escape = 94%
  - photodetector = 93%
  - LO interference = 96%
  - Optics = 99%
- inferred squeezing out of OPO = 8.2dB



Measured at 100 kHz

# Squeezed Vacuum Spectrum

- Locked using quantum noise locking<sup>1</sup>
- Homodyne detector not SNL below few hundred Hz
  - Due to scattered light, beam jitter?
  - Limits measurement of squeezing

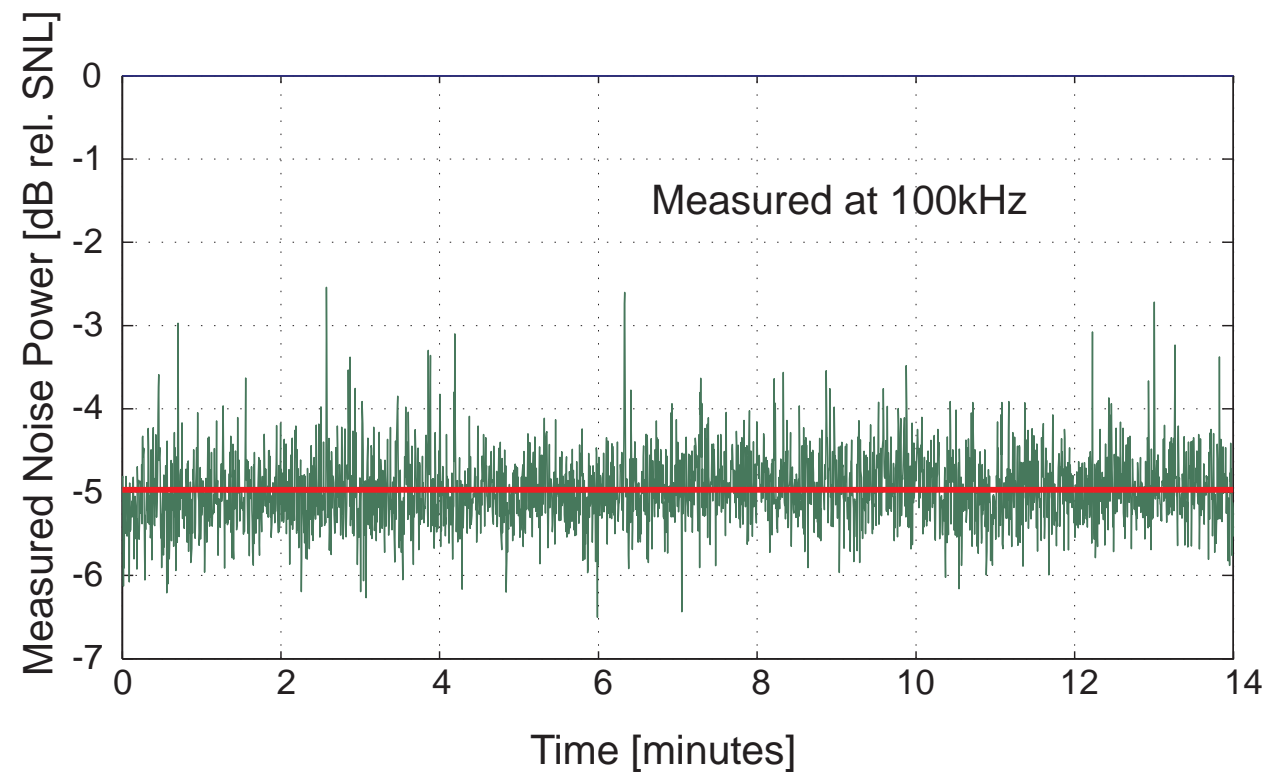


[1] McKenzie, Mikhailov, Goda, Lam, Grosse, Gray, Mavalvala and McClelland **JOB** (2005)



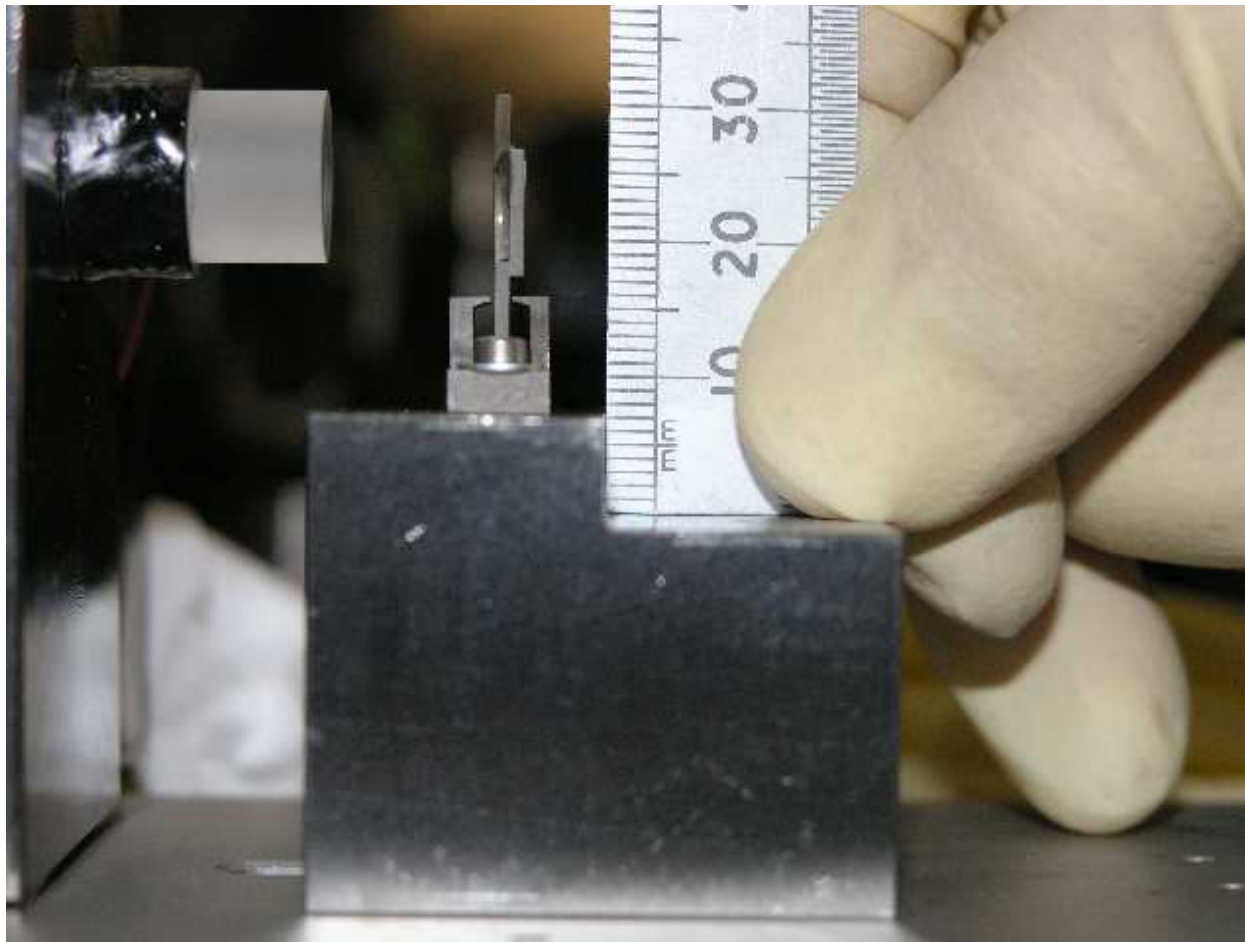
# Lock stability

- Good stability
- Limited by range of actuators/temperature stability of Lab



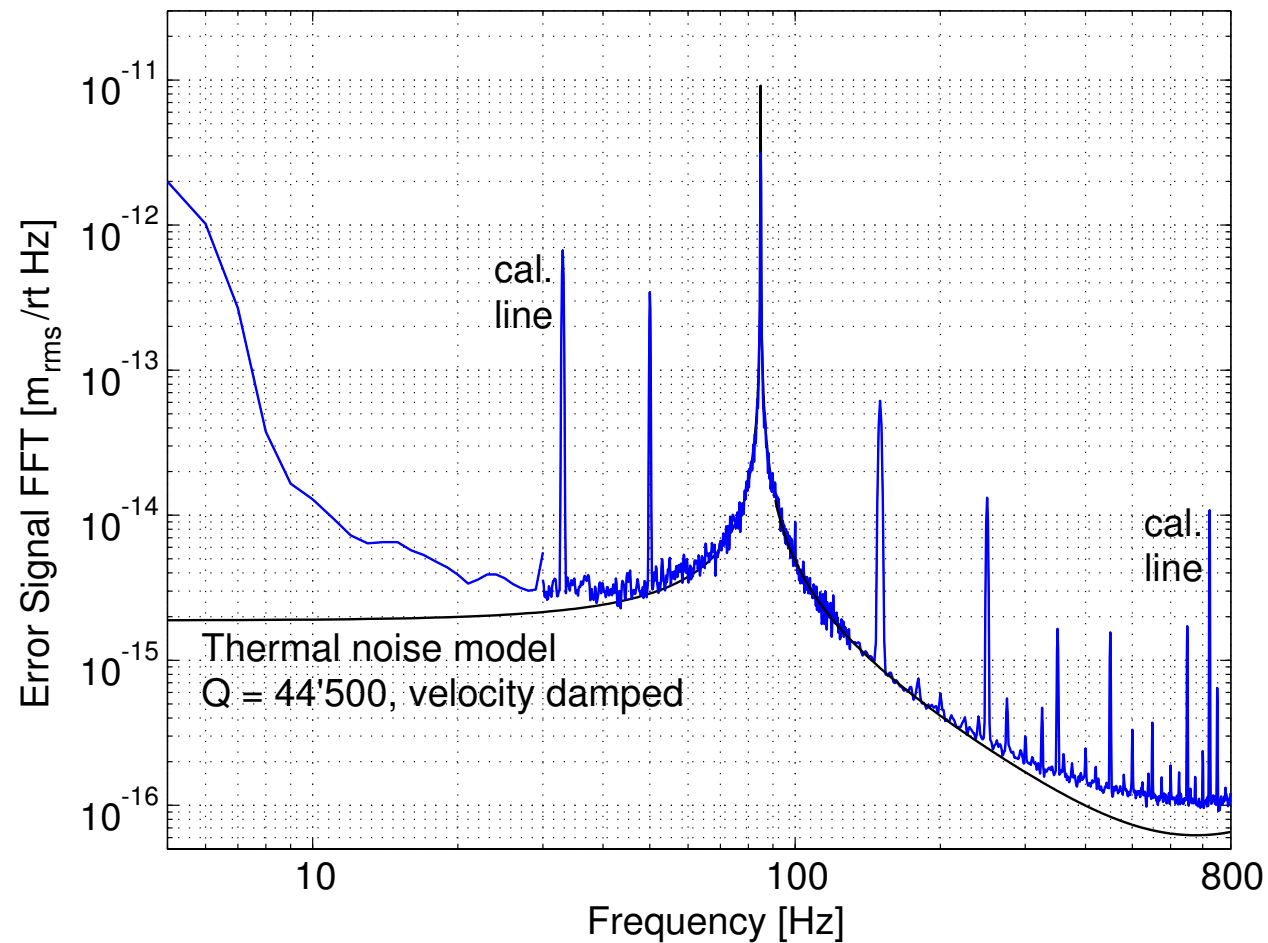
# Suspension TN measurement

Small mirror mounted on soft niobium flexure



# Thermal Noise Measurement

- Fits velocity damped model
- Measurement with small detuning



# Servo enhanced cooling of a flexure

- A detuned cavity gives rise to an optical spring,  $k_0$
- Servo interaction with the cavity response modifies the optical spring<sup>1,2</sup>

The magnitude of the optical spring becomes

$$k_g = \frac{k_0}{\sqrt{1 + 2G_0 \cos(\psi) + G_0^2}}$$

$\psi$  = loop phase,  $G_0$  = loop magnitude. The phase is rotated to

$$\theta_{\text{opt}} = \tan^{-1} \left( \frac{G_0 \sin(\psi)}{1 + G_0 \cos(\psi)} \right)$$

This allows optical cooling well inside the cavity linewidth

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[1] Mullavey, ANU honors thesis (2006), [2] Schediwy *et al*, LSC Tech Review (2006)

# Servo enhanced cooling of a flexure

The optical spring modifies the flexure thermal noise spectrum;

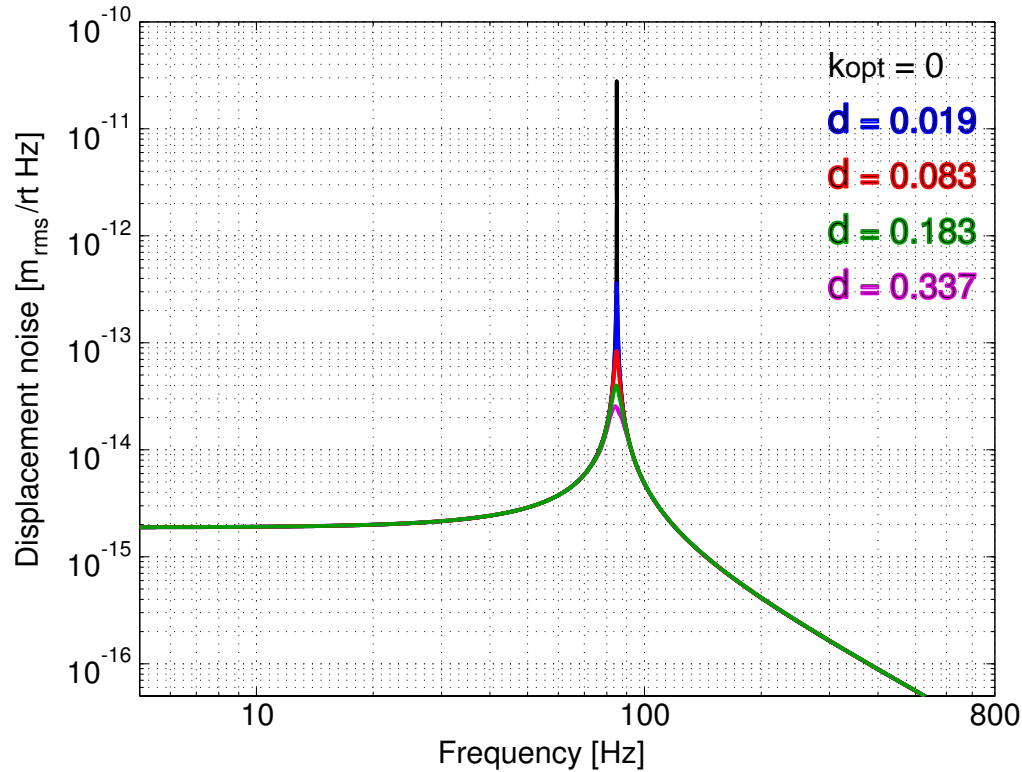
$$\hat{x}_{th}^2 = \frac{4 k_B T \phi \omega_0^2}{m \omega \left[ (\omega^2 - \omega_0^2 - k_g \cos(\theta_{opt})/m)^2 + (\phi \omega_0^2 + k_g \sin(\theta_{opt})/m)^2 \right]}$$

$T$  - temperature,  $\phi$  - loss angle  $m$  - mass,  $\omega_0$  - resonance freq.

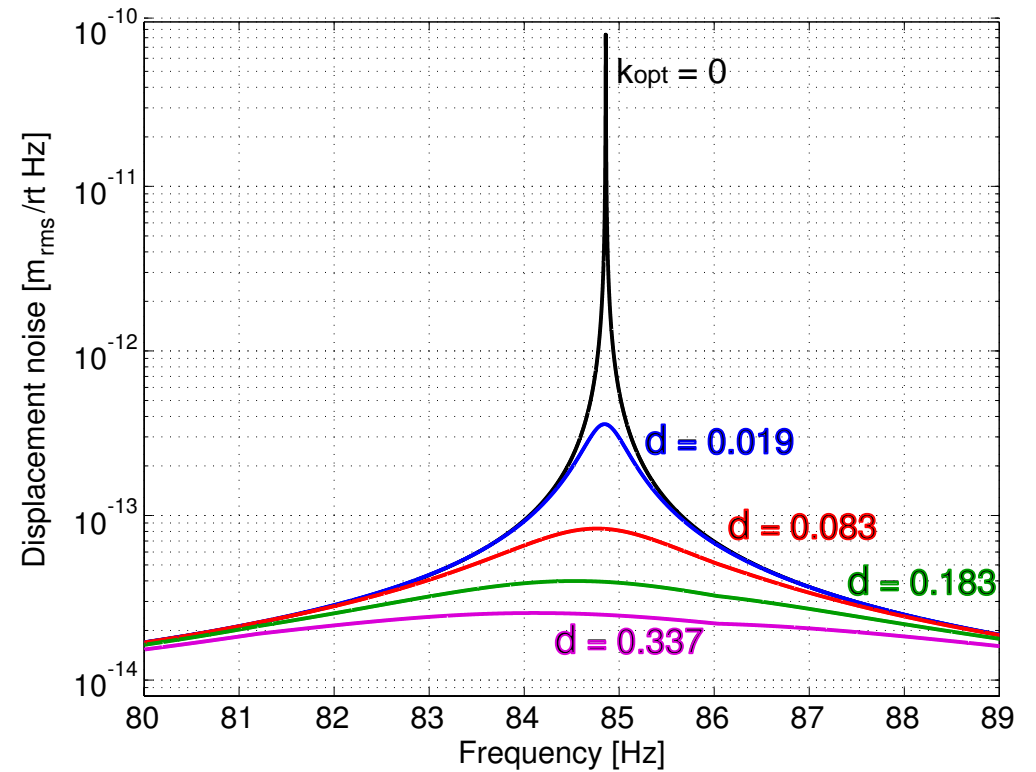
- Spring can be stiffened/weakened  $\propto \cos \theta_{opt}$
- Spring can be damped/anti-damped  $\propto \sin \theta_{opt}$

# Theory

Thermal noise model for  $P = 30\text{mW}$



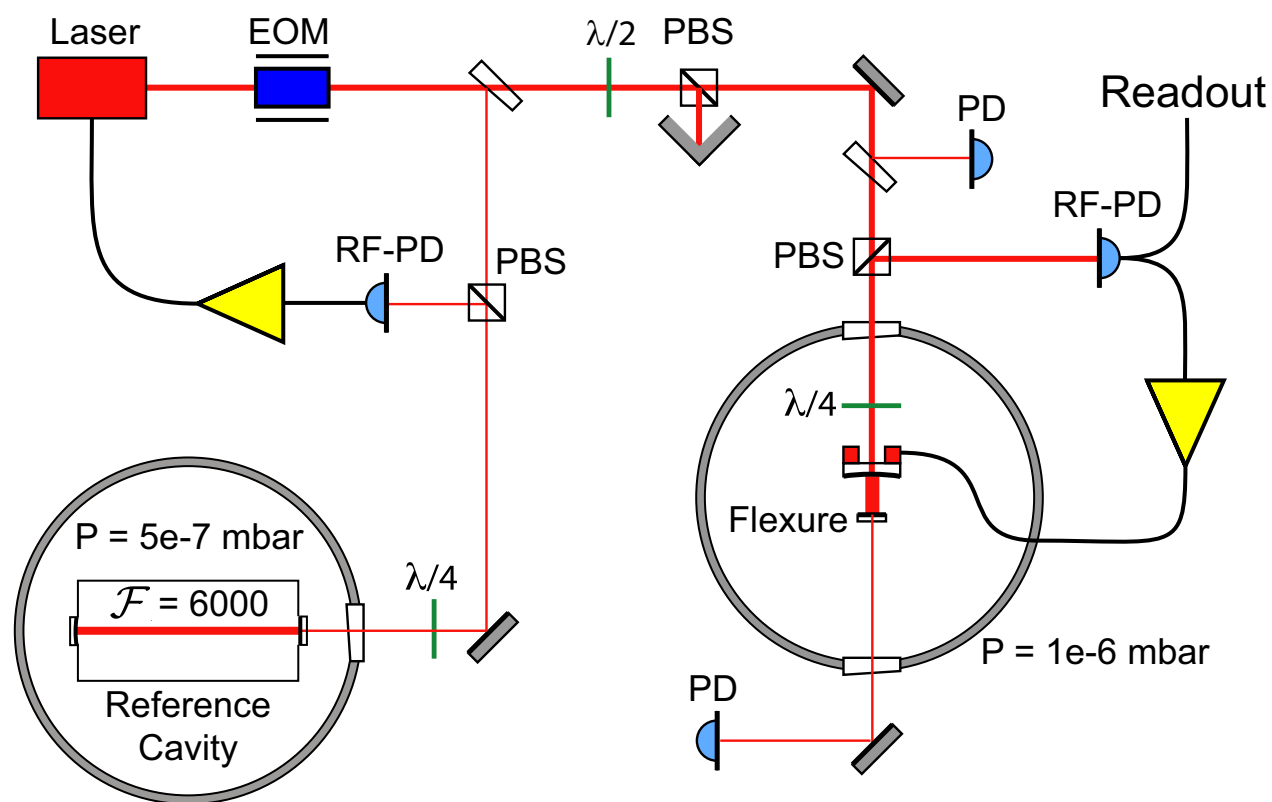
Thermal noise model for  $P = 30\text{mW}$



Here  $d$  is detuning.  $d = 1 \Rightarrow$  Half-width at half max.

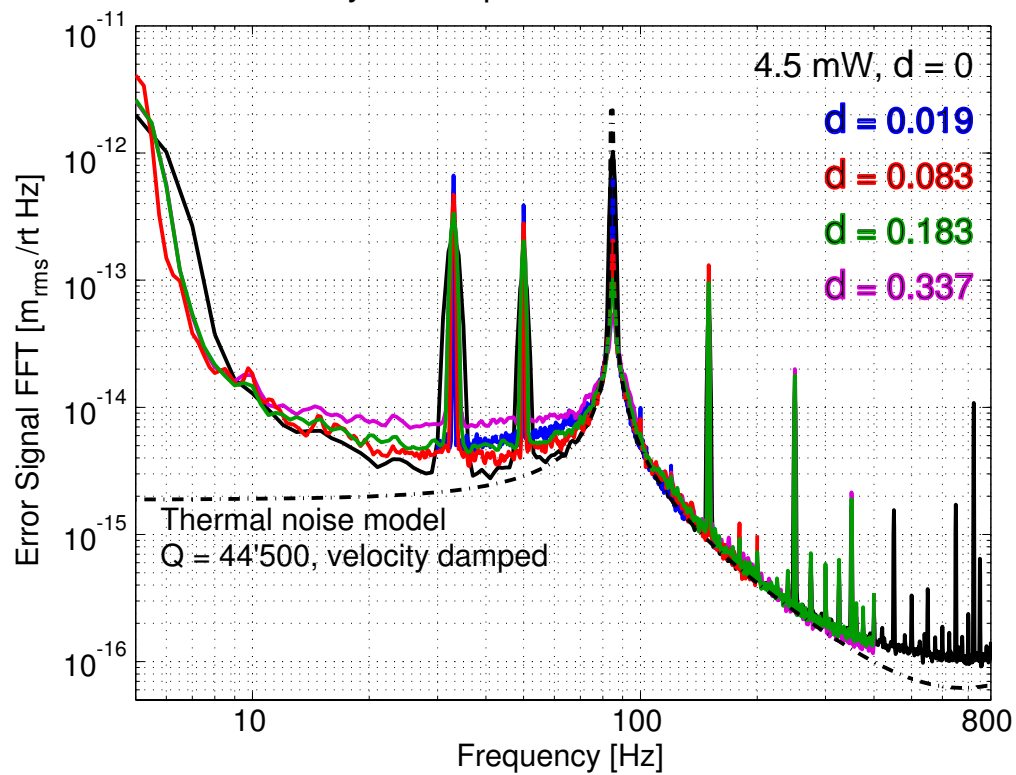
# Experimental setup

- Frequency stabilization via a monolithic reference cavity
- Test cavity controlled using PDH, 300  $Hz$  bandwidth
- Variable input power ( $0 - 200 mW$ ), cavity detuning ( $\delta = 0 - 0.5$ )

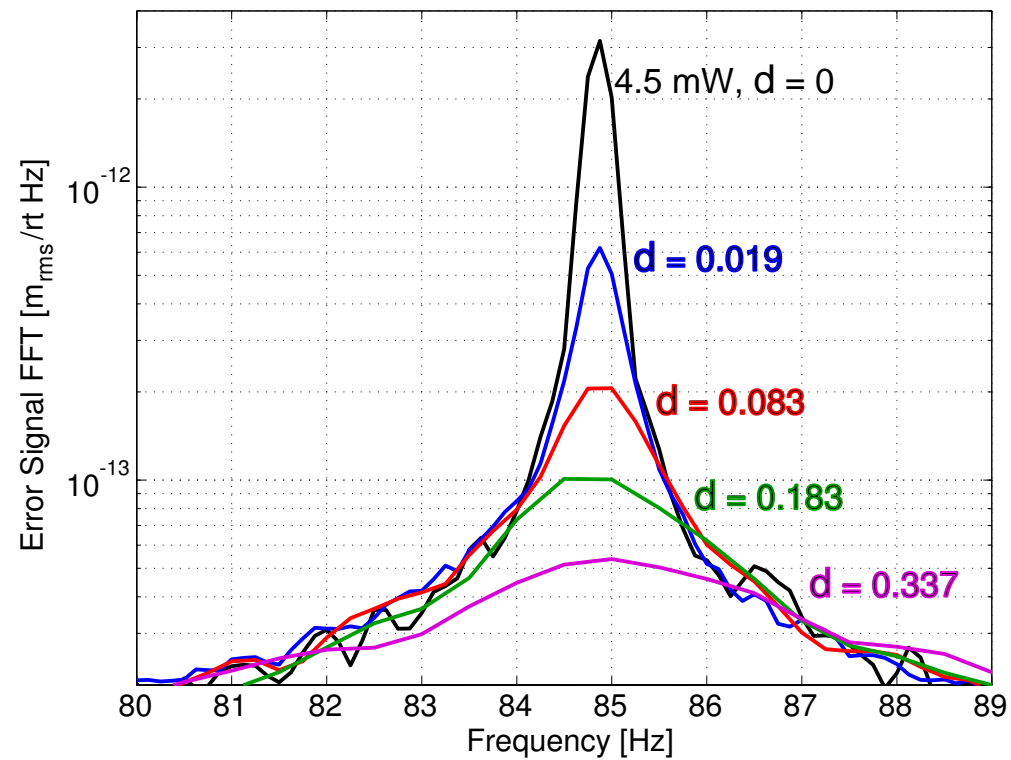


# Data

Cavity noise spectrum for  $P = 30\text{mW}$



Cavity noise spectrum for  $P = 30\text{mW}$



Effective temperature is 82mK





# Summary

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- Nice squeezer design
- Stable low frequency squeezing
- Measurement of suspension thermal noise
- Servo enhanced cooling of thermal noise to 82mK