

## TNI Progress and Status

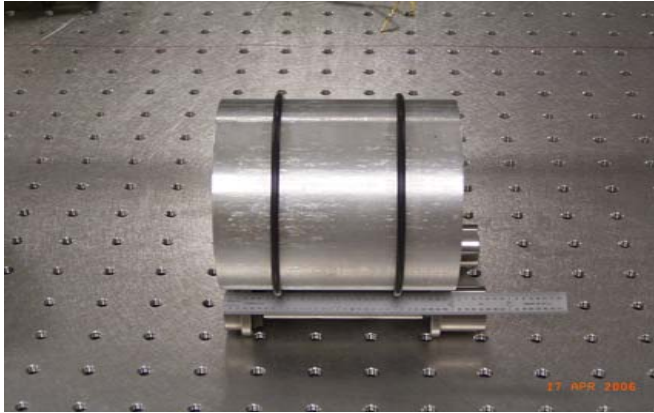
Greg Ogin  
LSC Meeting  
March 22, 2007

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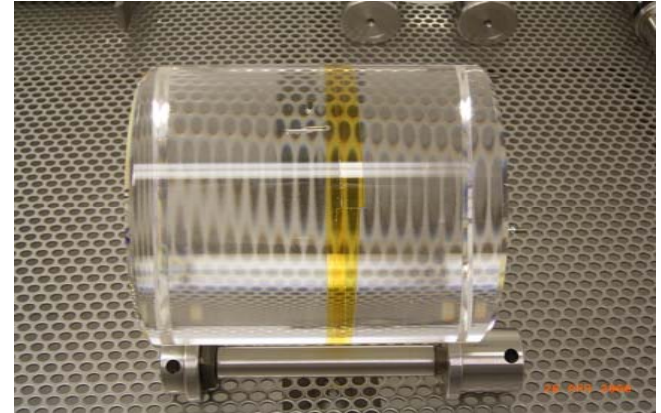
## Current Areas of Activity

- Parametric Instability Damping
- Improved Calibration / Spot Size Measurement
- Aperiodic Coating

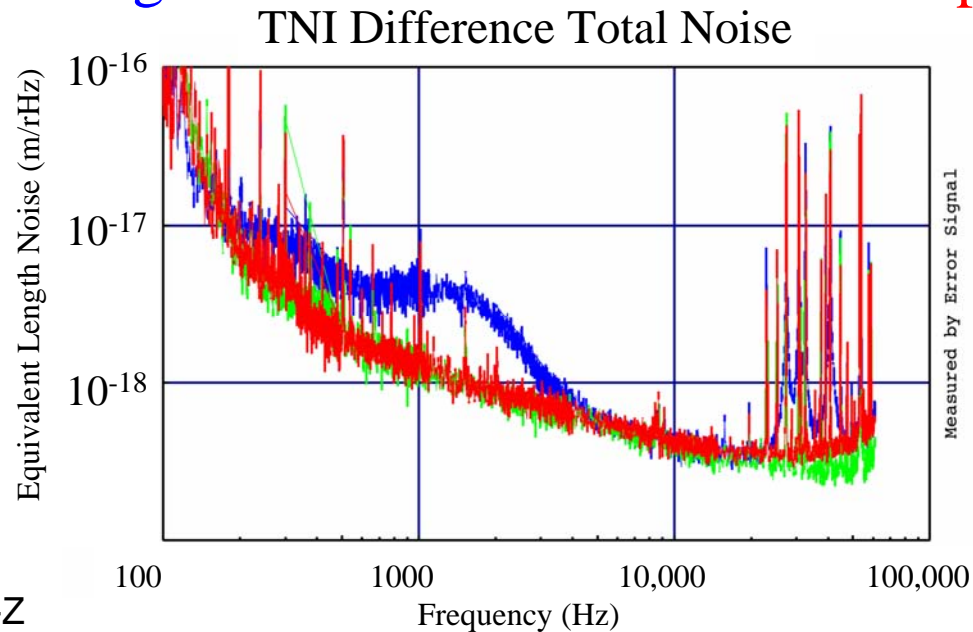
## Initial Q-Suppression Ideas



Buna o-rings

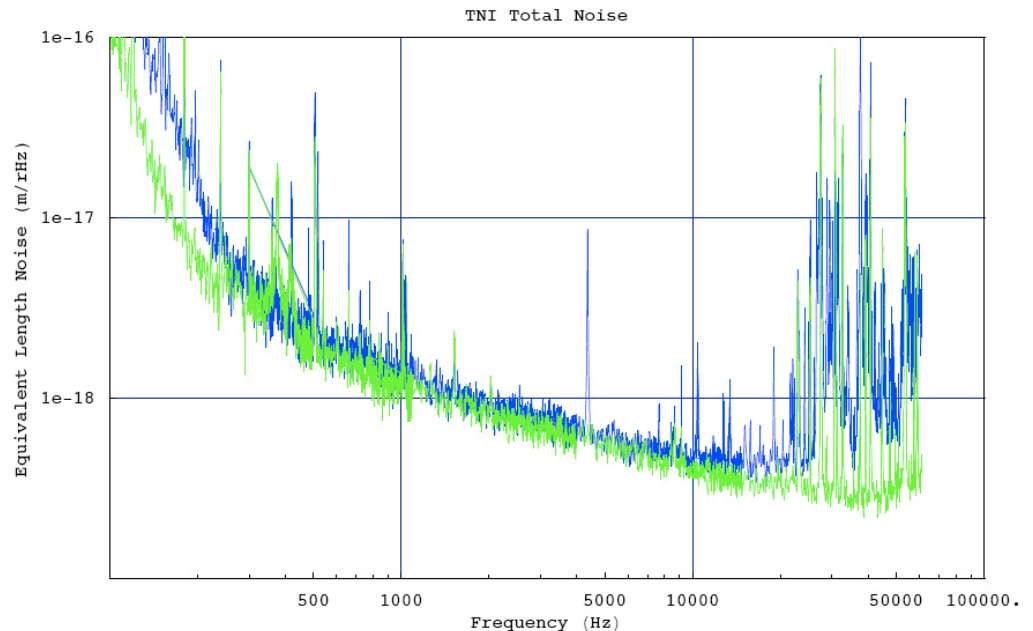
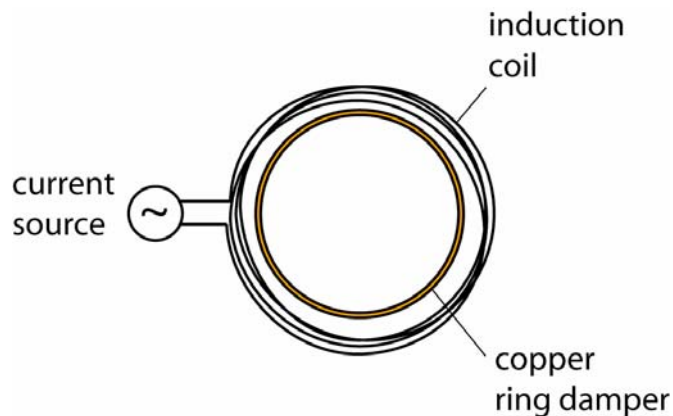
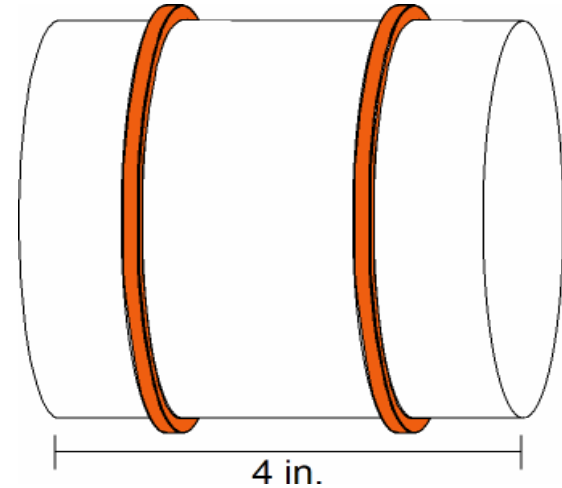


Kapton tape



## Copper Rings

- Monolithic copper rings machined undersized, heated for expansion, then placed around the barrel of the optic.
- Heating to 200°C caused rings to expand sufficiently to slip over mirrors easily, and cool with no apparent damage to the optic.
- Q reduction still good, as with buna
- Broadband noise floor nearly unaffected below ~20kHz.



## Loss Angle Discrepancy

- TNI measurements of loss angle for titania-doped tantala / silica mirror coatings gave different results than those obtained from Q measurements
  - Harry et al, Class. Quantum Grav., **24** (2007) 405-415

TNI:

$$\phi_{eff} = (2.41 \pm 0.15) \times 10^{-6}$$

Q Measurements:

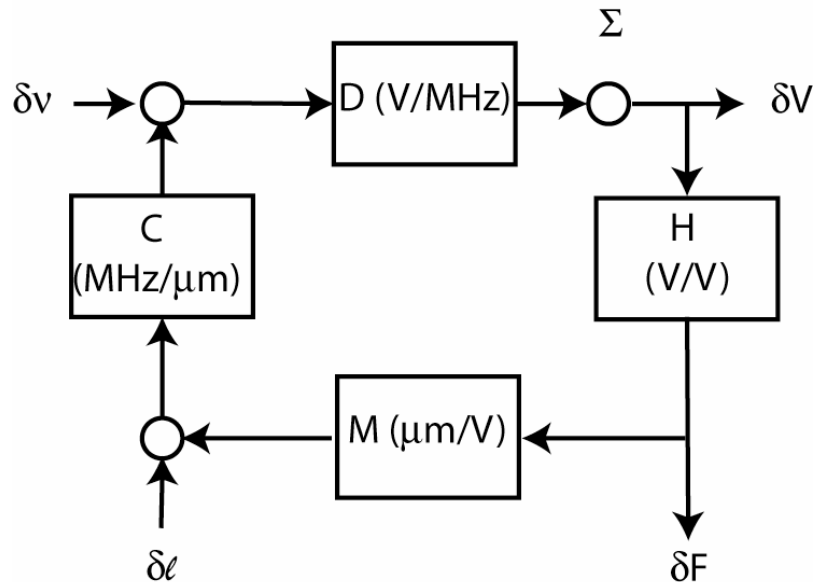
$$\phi_{eff} = (4.0 \pm 0.3) \times 10^{-6}$$

- Discrepancy ~40% is significant.

Relationship between loss angle and length noise:

$$S_x(f) = \frac{2k_B T}{\pi^{3/2} f} \frac{(1 - \sigma^2)}{wY} \phi_{eff}$$

## TNI Calibration



- Extract length noise from error signal

$$\delta \ell = \frac{1 + DHMC}{DC} \delta V$$

- Must know each transfer function accurately!
- Electronic transfer function  $H$  specified by design, verified by direct measurement.

- Conversion factor  $C$

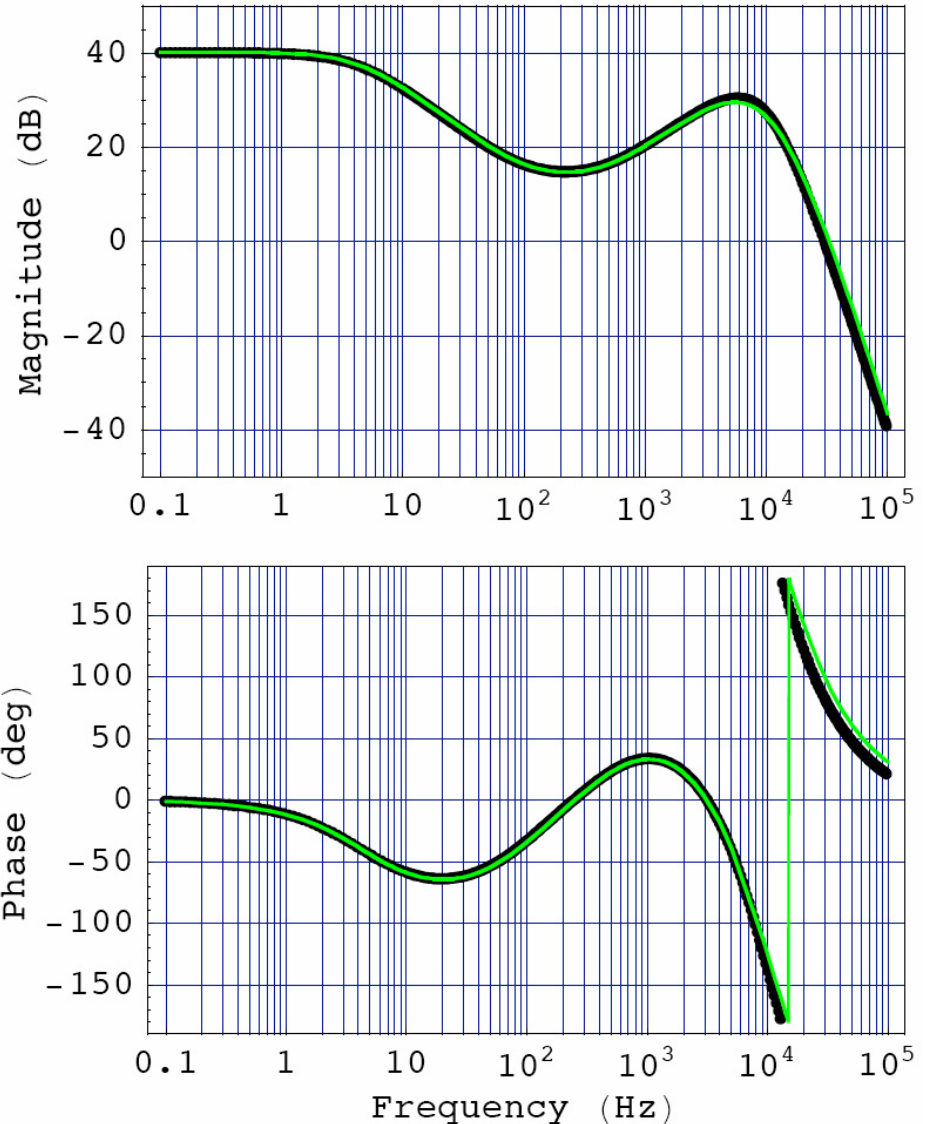
$$C = \frac{V}{L}$$

- Discriminant  $D$  and mirror response  $M$  each measured two different ways.
- Additional tests localize noise within the test cavities.
  - Scaling with laser power
  - Scaling with modulation depth

# Previous Model for H, w/ Measured Parameters

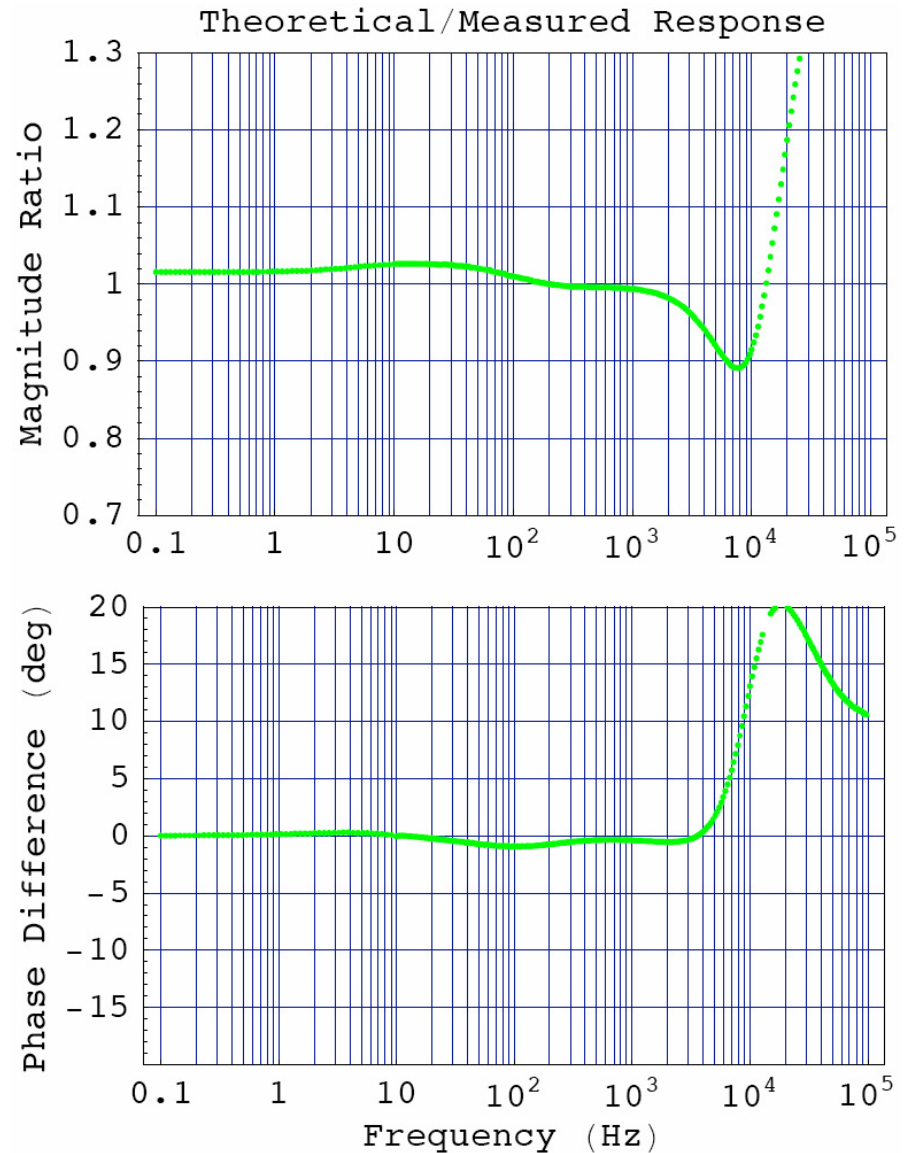
$$H(f) = g_1 \times 1.7 \times 60 \times \frac{1 + i\frac{f}{105}}{1 + i\frac{f}{4.6}} \times \frac{1 + i\frac{f}{470}}{(1 + i\frac{f}{11000})}$$

NAC H



## Reasonably Accurate

- Within a few percent of the measured response all the way up to 3 kHz.
- Negligible contribution to error in D.

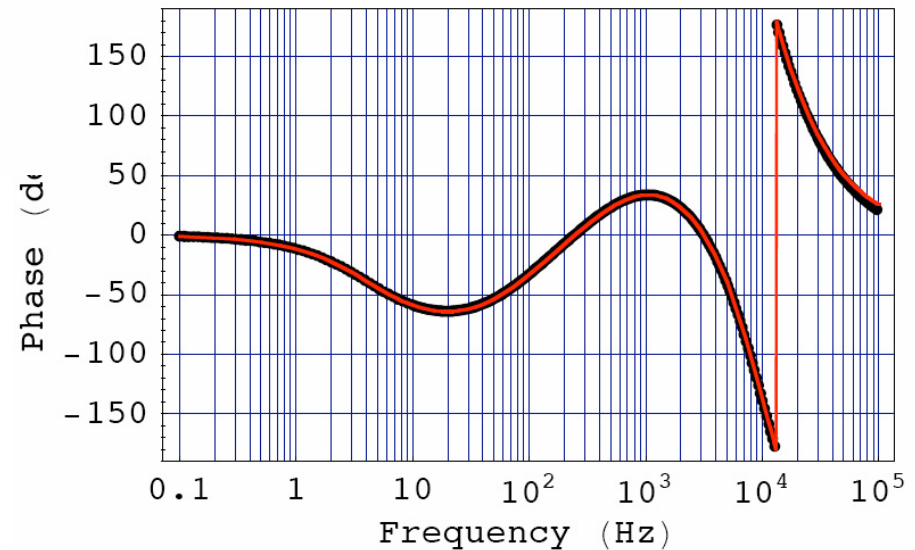
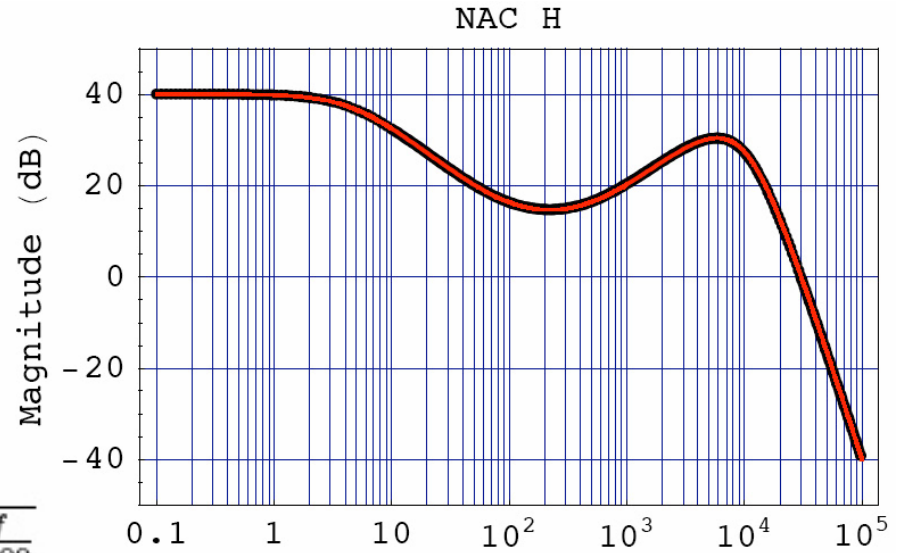




# New Formula - Verified by Measurement

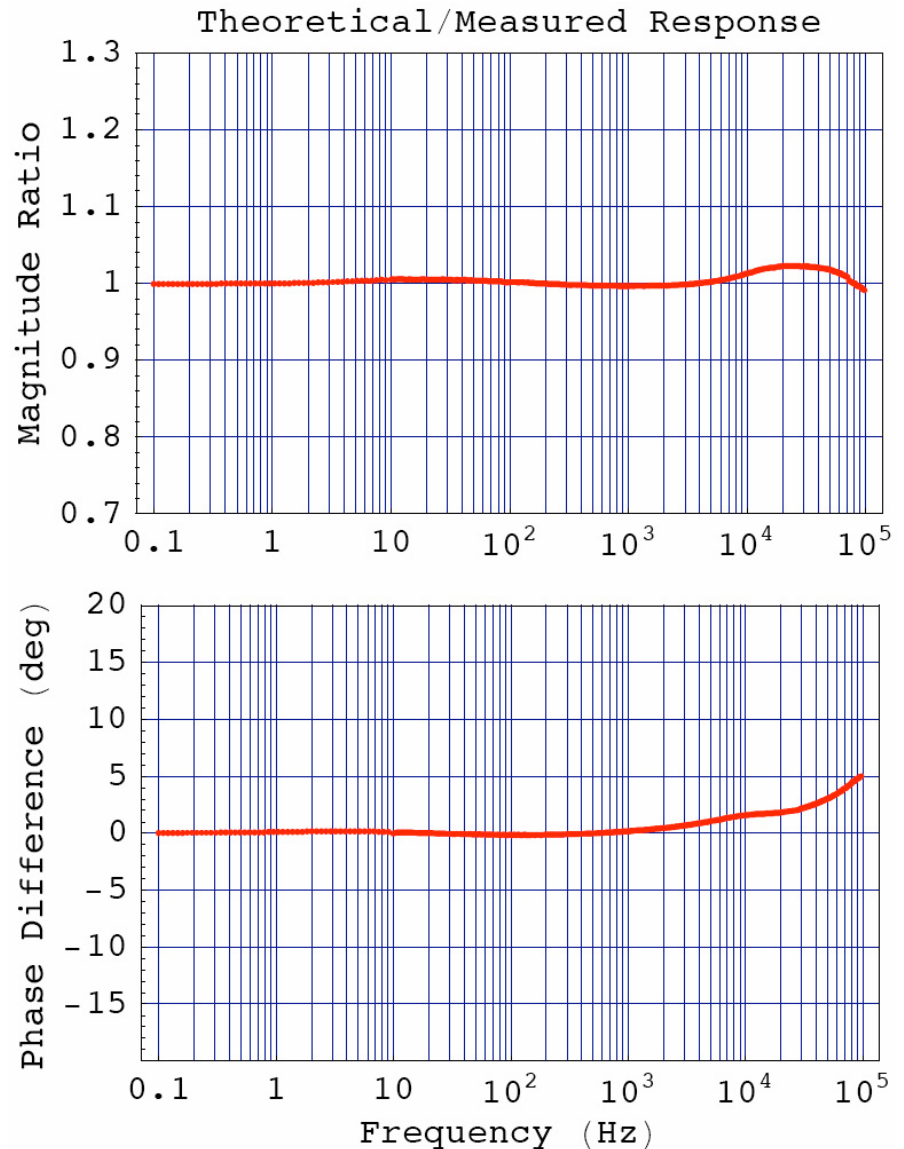
$$H(f) = g_1 \cdot 98.7 \cdot \frac{1}{1 + i \frac{f}{10400}} \times \frac{1}{1 - (\frac{f}{10300})^2 + i \frac{f}{7000}}$$

$$\times \frac{1 + i \frac{f}{102}}{1 + i \frac{f}{10600}} \times \frac{1 + i \frac{f}{475}}{1 - (\frac{f}{204})^2 + i \frac{f}{4.57}}$$



## Very Accurate

- Within 1% of measured response up to about 10 kHz
- Negligible contribution to error.
- Using to reanalyze the undoped and doped coating noise data along with a more accurate value for C.



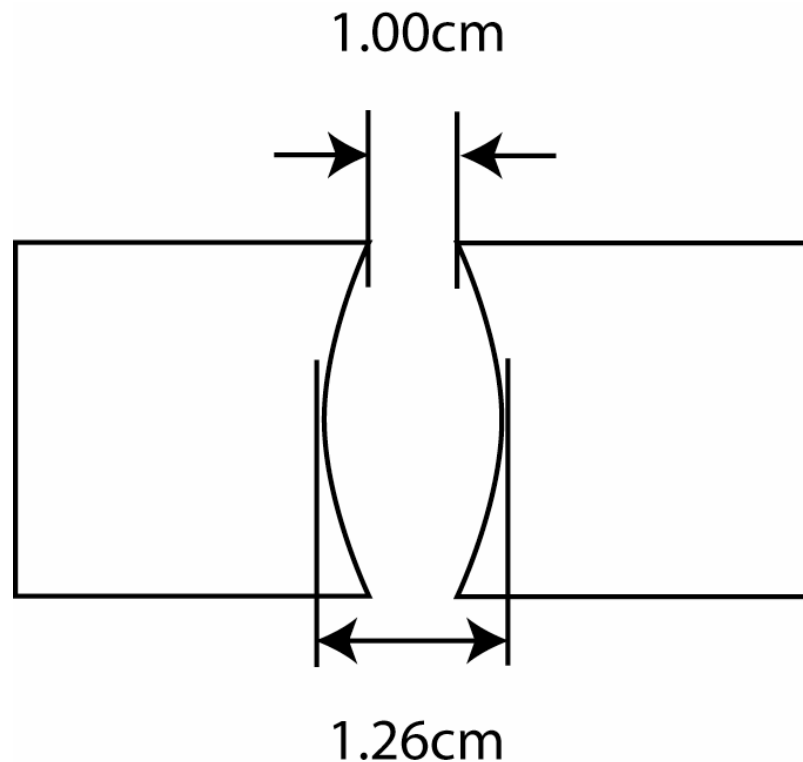
## Spot Size and Coating Thickness

- Need to know both spot size and coating thickness to extract loss angle
- Had been using  $w = 160 \mu\text{m}$
- Optical, physical measurements give  $w = 163 \pm 10 \mu\text{m}$  (still being refined)
  - Leads to expected  $\sim 4\%$  increase in  $\phi$  (denominator has  $w^2$ )
- Had been using  $d = 4.26 \mu\text{m}$  (REO): Undoped coating thickness
- Actual value is  $d = 4.515 \mu\text{m}$  (LMA): Doped coating thickness
  - Leads to a 6% reduction in  $\phi$
- Net effect is a change in  $\phi$  which is on the order of the uncertainty in this number.

$$S_x(f) \approx \frac{2k_B T (1 - \sigma^2)}{\pi^{3/2} f w Y} \left\{ \phi_{sub} + \frac{2}{\sqrt{\pi}} \frac{d}{w} \left( \frac{1 - 2\sigma_c}{1 - \sigma_c} \right) \phi_{coat} \right\}$$

## Cavity Length L

- Mirror radius of curvature had been neglected!
- Increases cavity length by 26%.
- Taking center of mass shift into account gives a suspended cavity length of 1.24cm.
- This would give a spot size of  $163.6\mu\text{m}$ , in agreement with optical measurement.
- This change decreases C, raising the equivalent length noise
- Still working numbers, but this is the right order of magnitude to account for loss angle discrepancy



$$C = \frac{v}{L}$$

$$\delta l \approx \frac{\delta V}{DC}$$

$$S_x(f) = \frac{2k_B T (1 - \sigma^2)}{\pi^{3/2} f w Y} \phi_{eff}$$

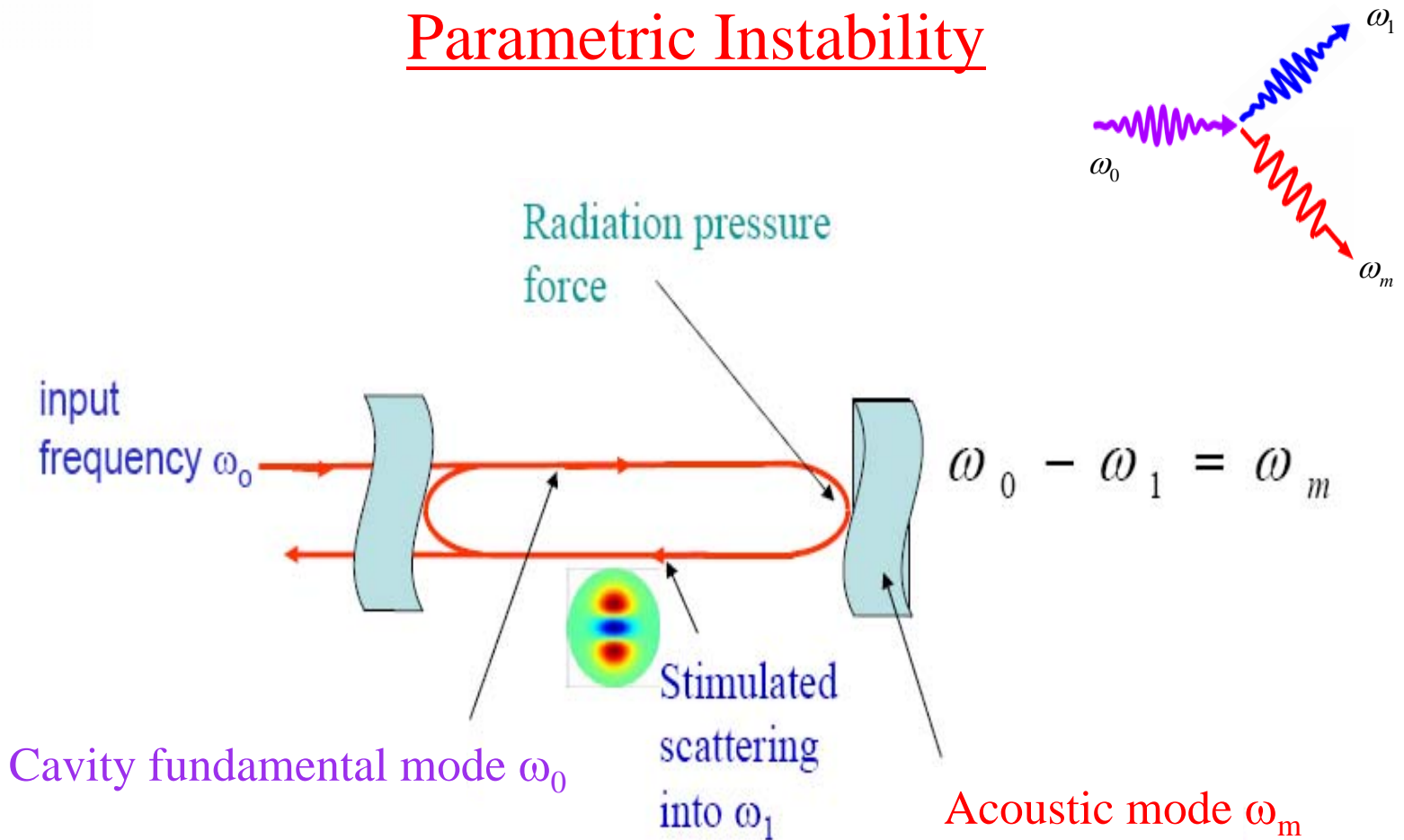
## Aperiodic Coatings

- Goal: reduce high-loss material in HR coating by varying layer thickness, while preserving phase relationship for reflection
- Collaboration with
  - Vincenzo Galdi and Innocenzo Pinto at Benevento (coating design),
  - LMA at Lyon (fabrication and loss measurements), and
  - Sheila Rowan at Glasgow (loss measurements)
- We have a design for an aperiodic coating using silica and UN-doped tantala.
- Currently waiting on fabrication by LMA - as soon as we get new coatings, we will measure actual noise at TNI.
- There have been issues with fabrication. LMA is working on resolution.

## Summary

- Parametric instability
  - Copper rings reduce mechanical Q with small noise floor increase
- Calibration of instrument
  - Improved electronic transfer function
  - Precise measurements of cavity length and spot size are in progress
  - Corrected cavity length value for transfer function, should significantly reduce discrepancy in  $\text{TiO}_2$ -doped  $\text{Ta}_2\text{O}_5$  coating loss angle measurements
- Aperiodic coatings
  - Currently in fabrication

# Parametric Instability



## Condition for Instability

$$R \approx \frac{2PQ_m}{McL\omega_m^2} \left( \frac{Q_1\Lambda_1}{1 + \Delta\omega_1^2 / \delta_1^2} - \frac{Q_{1a}\Lambda_{1a}}{1 + \Delta\omega_{1a}^2 / \delta_{1a}^2} \right) > 1$$

↑
↑  
 Stokes Mode                      Anti-Stokes mode

Ju, et al. G050325-00 who got it from  
 Braginsky, et al. Phys. Lett. A 305, 111 (2002)



## Optical Measurement of $w_0$

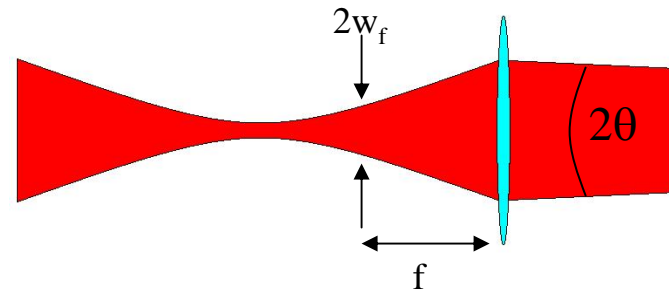
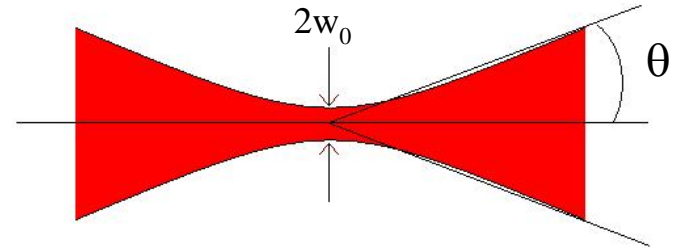
- Gaussian beam waist size is equivalent to spreading angle:

$$\theta = \frac{\pi w_0^2}{\lambda}$$

- ISO standard (11146-1) for measuring spreading angle (using a lens of focal length  $f$ ):

$$\theta = \frac{w_f}{f}$$

- Preliminary results:  $w = 163 \pm 10 \mu\text{m}$
- Large error due to issues measuring focal length of lens, will be resolved soon.



## Direct Measurement of L

- Performed direct measurement of mirror separation at edges using calipers
- Faces were slightly tilted, but geometrically deduce separation at center to be  $\sim 1.216$  cm
- This corresponds to a beam waist of  $162.3 \mu\text{m}$  - consistent with other results

