

# To the practical design of the optical lever intracavity topology of gravitational-wave detectors

S.L.Danilishin, F.Ya.Khalili

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Why we need intracavity topologies?

“Practical” version of the optical lever

The local meter

Conclusion

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Suppose that we have managed to overcome the  
SQL.

What are the next limitations?

## Pumping power

$$\frac{L^2 S_h}{4} \times S_{\text{B.A.}} = \frac{\hbar^2}{4},$$
$$S_{\text{B.A.}} = \frac{8\hbar\omega_p W}{\zeta^2 c L} \frac{\gamma}{\gamma^2 + \Omega^2},$$

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$$\xi^2 \equiv \frac{S_h}{S_h^{\text{SQL}}} = \frac{\zeta^2}{2} \frac{W_{\text{SQL}}}{W} \quad (\text{optimization: } \gamma = \Omega),$$

where

$$S_h^{\text{SQL}} = \frac{4\hbar}{M\Omega^2 L^2}, \quad W_{\text{SQL}} = \frac{McL\Omega^3}{8\omega_o}, \quad \zeta = e^{-R}.$$

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# Optical losses

$$\xi_{\text{loss}}^2 = \sqrt{\zeta^2 \frac{\gamma_{\text{loss}}}{\gamma_{\text{load}} \approx \gamma}},$$

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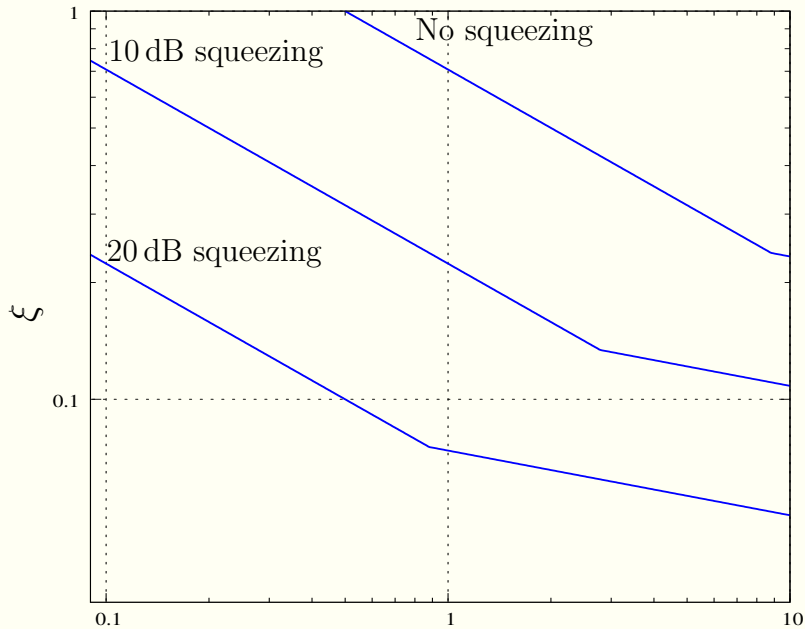
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Smaller  $\xi$ s require  $\gamma > \Omega$ , hence:

$$\xi_{\text{sum}} = \sqrt{\frac{3}{2}} \zeta^{2/3} \left( \frac{\gamma_{\text{loss}}}{2\Omega} \frac{W_{\text{SQL}}}{W} \right)^{1/6} \approx 0.35 \zeta^{2/3} \left( \frac{W_{\text{SQL}}}{W} \right)^{1/6}.$$

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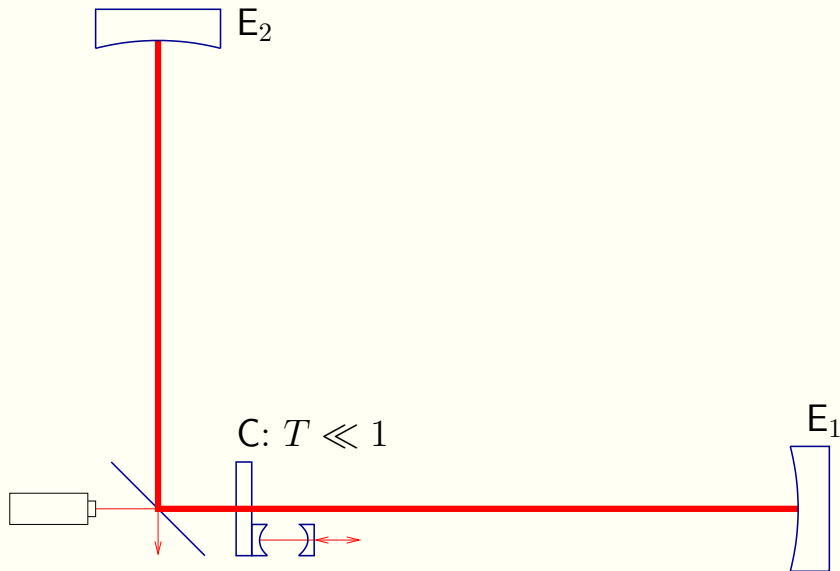
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V.B.Braginsky, F.Ya.Khalili, Phys.Lett.A **218**, 167 (1996).

V.B.Braginsky, M.L.Gorodetsky, F.Ya.Khalili, Phys.Lett.A **232**, 340 (1997).

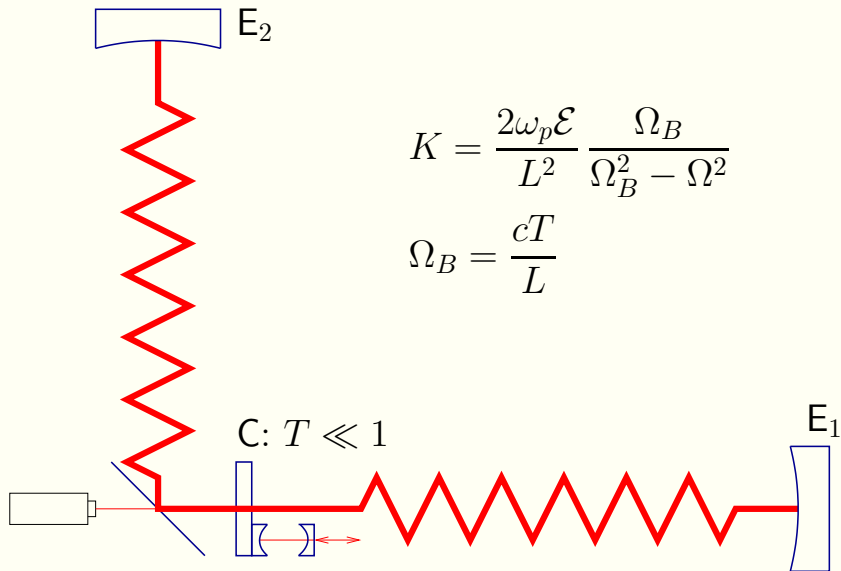
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# Optical bars



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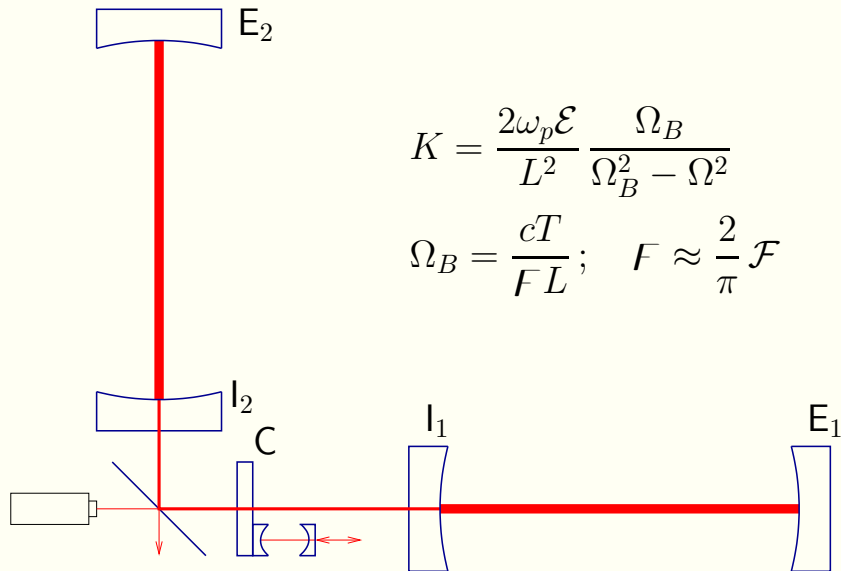
# Optical bars



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# Optical lever

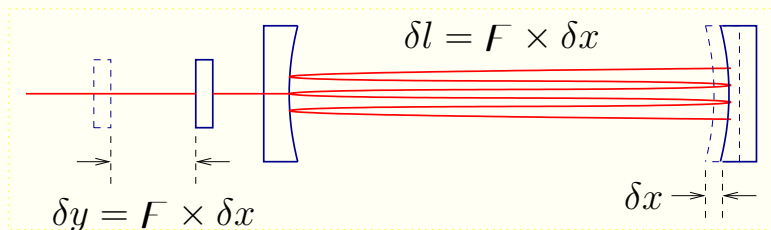


$$K = \frac{2\omega_p \mathcal{E}}{L^2} \frac{\Omega_B}{\Omega_B^2 - \Omega^2}$$

$$\Omega_B = \frac{cT}{FL}; \quad F \approx \frac{2}{\pi} \mathcal{F}$$

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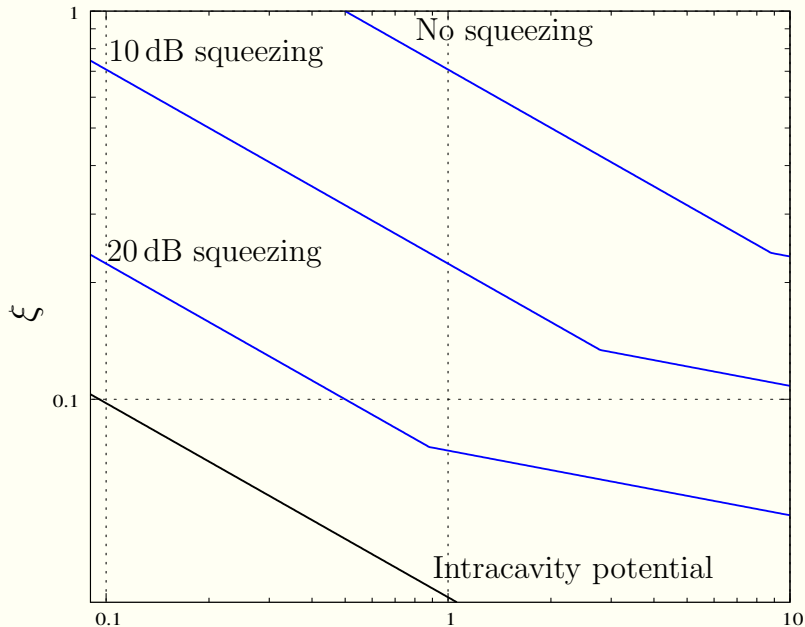
# Optical lever



$$\frac{\delta y}{\delta x} = F,$$

$$\frac{F_{\text{pond } y}}{F_{\text{pond } x}} = \frac{1}{F}$$

(like an ordinary mechanical lever).



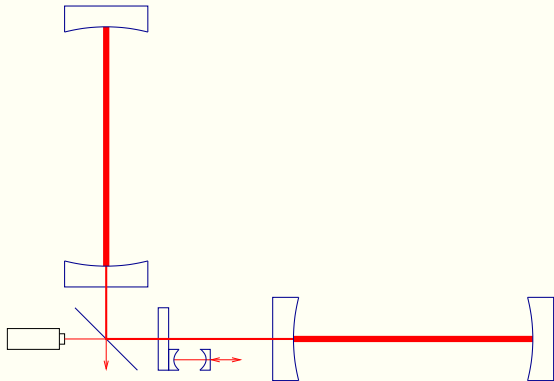
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Why we need intracavity topologies?

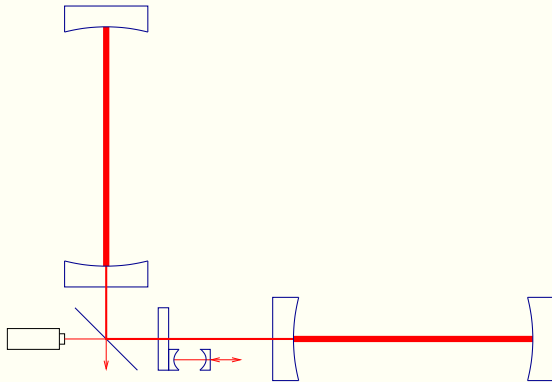
“Practical” version of the optical lever

The local meter

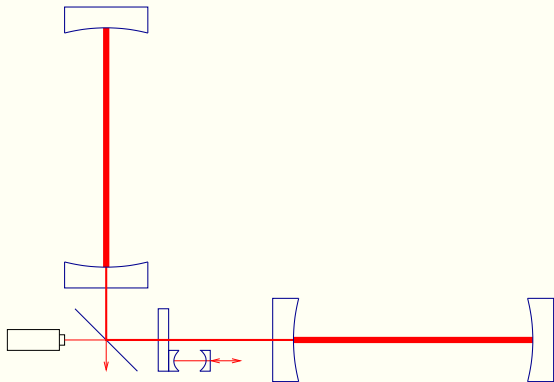
Conclusion



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**The main disadvantage:** non-symmetry  
⇒ vulnerability to the pumping power  
fluctuations.

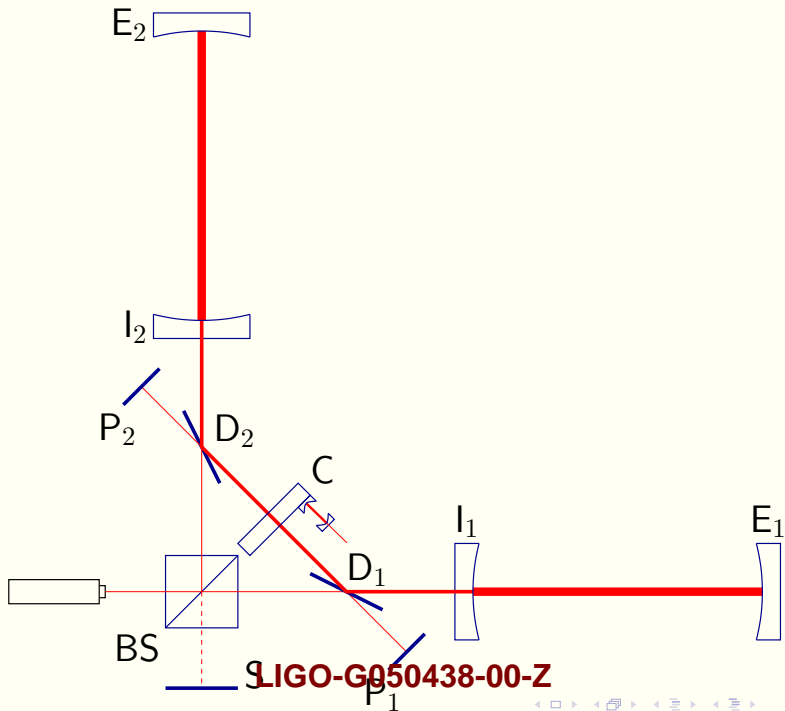


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 $\Rightarrow$  vulnerability to the pumping power fluctuations.

**Additional disadvantages:**

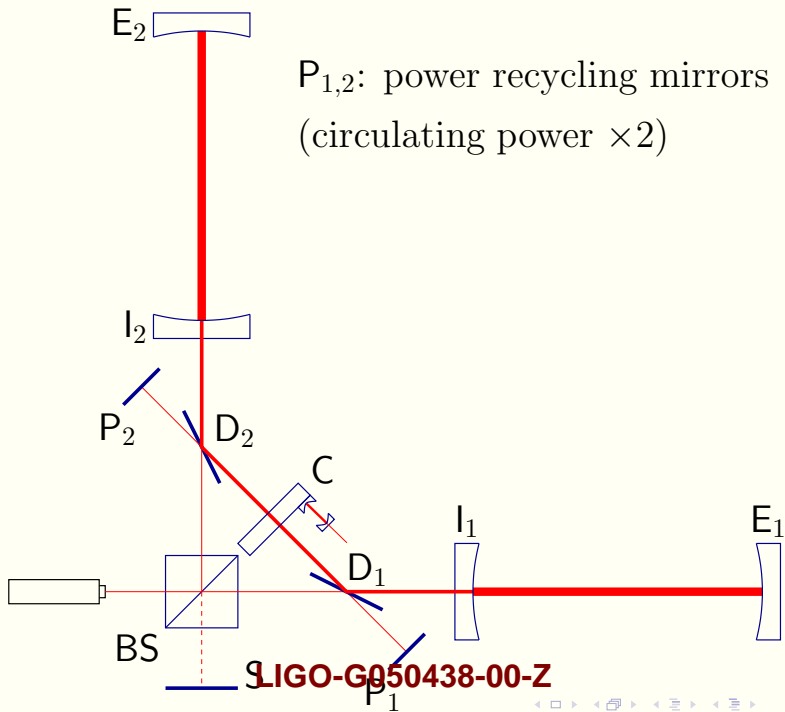
only half of the pumping power enters inside;  
input port  $\Rightarrow$  additional “hole” for noise.

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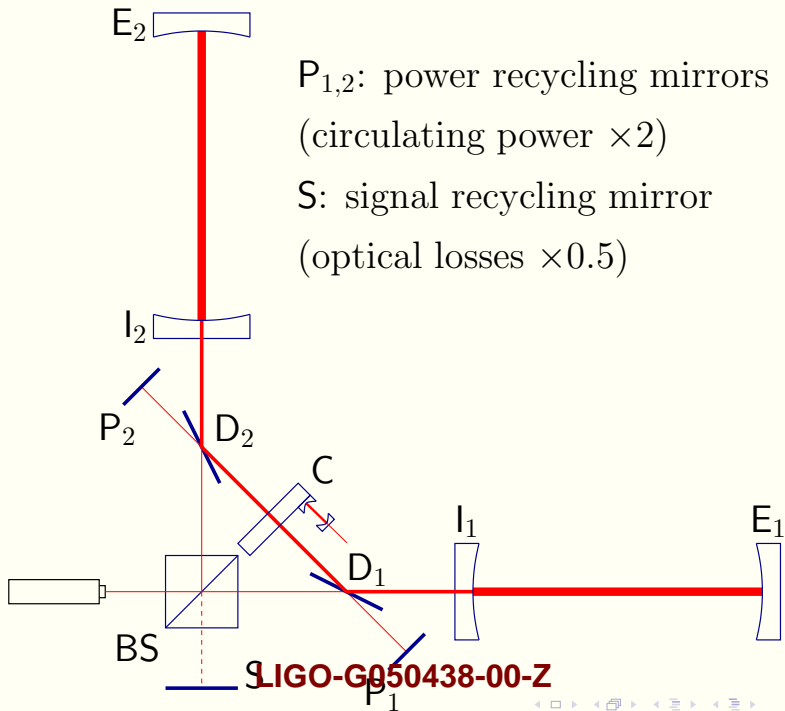


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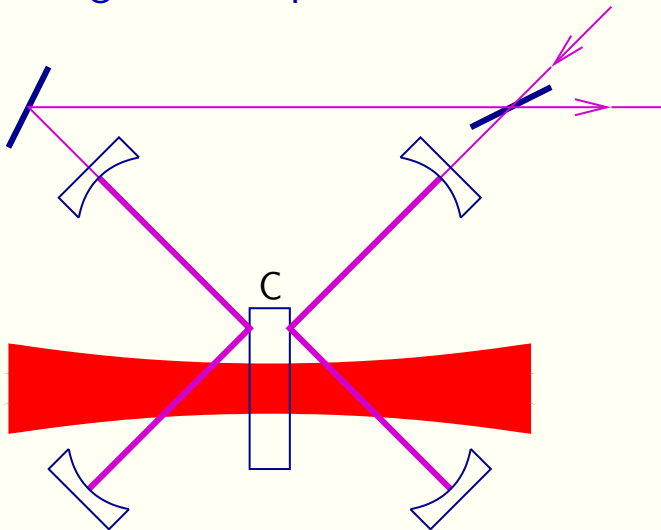
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- ▶ ???

# Possible design of the optical local meter



Thomas Corbitt *et al*, "Ponderomotive Squeezing",  
LIGO Document G040147-00 (2004)

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## Parameters used for the estimates

Local mirror mass	$M_C = 1 \text{ g}$
Circulating power	$w = 10 \text{ kW}$
Optical losses	$A_{\text{local}}^2 = 5 \times 10^{-6}$

Thomas Corbitt *et al*, “Ponderomotive Squeezing”,  
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# Spectral variation measurement

Small-scale version of the KLMTV topology.

Rather gedanken than realistic scheme, but provides a good comparison point for other schemes.

H.J.Kimble *et al*, Physical Review D **65**, 022002 (2002)

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# Spectral variation measurement

$$\xi_{\text{meter}}^2 \approx \frac{1}{2F^2} \frac{M}{M_C} \frac{w_{\text{SQL}}}{w},$$

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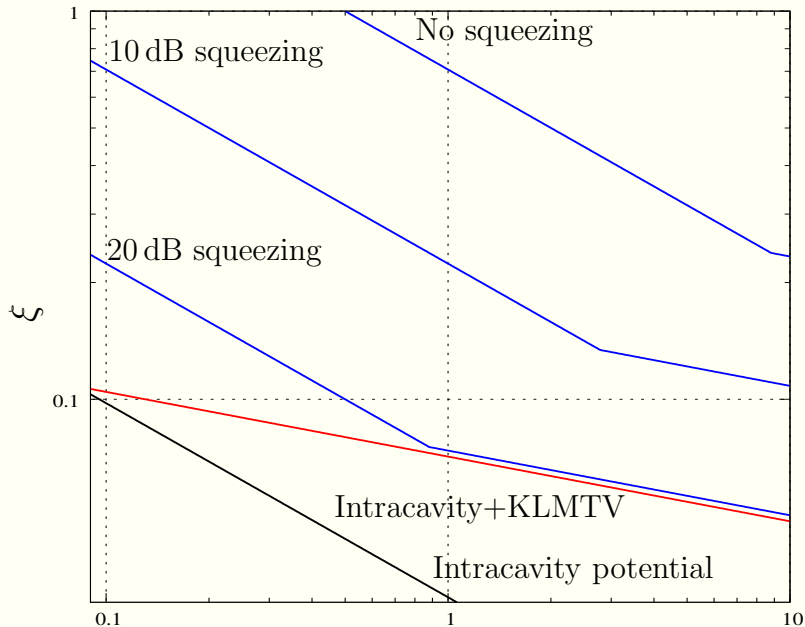
$$W \geq \frac{F^2 M_C}{8 M} W_{\text{SQL}},$$

$$\xi_{\text{loss}}^2 = \sqrt{\frac{A_{\text{local}}^2}{T_{\text{local}}^2}}.$$

$$\Rightarrow \xi_{\text{meter loss}}^2 = \frac{\xi_0^2}{2} \left( \frac{W_{\text{SQL}}}{W} \right)^{1/3},$$

where  $\xi_0^2 = \frac{3}{2} \left( \frac{M_C c^2 A_{\text{local}}^2 \Omega^2}{22 w w_0} \right)^{1/3} \approx 0.1.$

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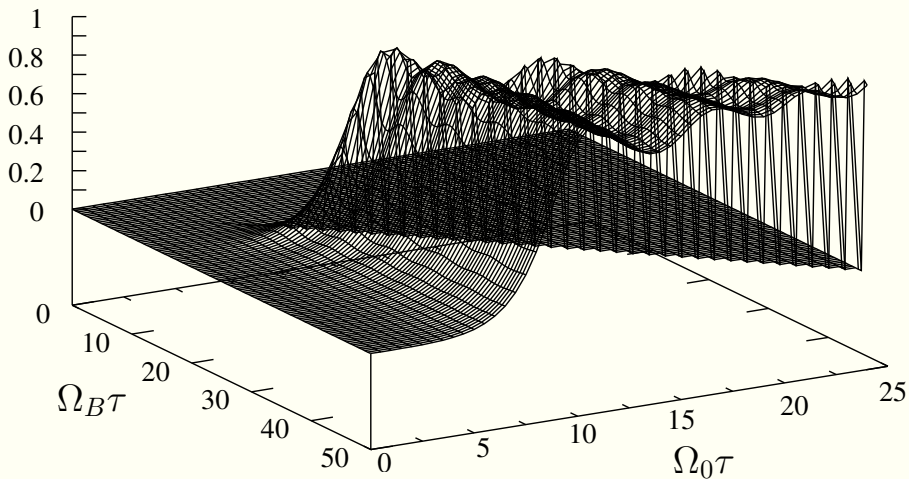
## Discrete sampling variation measurement

$$\xi_{\text{DSVM}}^2 = \frac{720}{\pi^4} \frac{1}{\mathcal{G}(\Omega_{B\tau}, \Omega_0\tau)} \frac{1}{F^2} \frac{M}{M_C} \frac{w_{\text{SQL}}}{w},$$

$$W \gtrsim 60 F^2 \frac{M_C}{M} W_{\text{SQL}}$$

(Yanbei Chen has the explanation for these weird numeric factors)

# Plot of $\mathcal{G}(\Omega_{BT}, \Omega_0\tau)$



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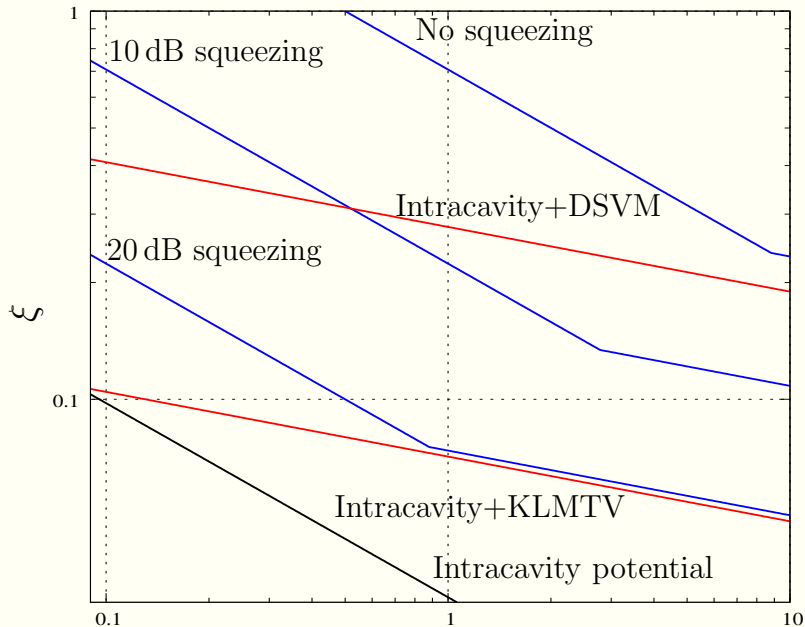
$$\xi_{\text{loss}}^2 = \sqrt{\frac{A_{\text{local}}^2}{T_{\text{local}}^2}},$$

$$\Rightarrow \xi_{\text{meter loss}}^2 \approx \xi_0^2 \left( \frac{720 \times 60 W_{\text{SQL}}}{\pi^4 W} \right)^{1/3},$$

instead of  $\xi_{\text{meter loss}}^2 = \frac{\xi_0^2}{2} \left( \frac{W_{\text{SQL}}}{W} \right)^{1/3}$ .

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2. Both kinds of the “supporting” devices require approximately the same level of the experimental technology.
3. However, intracavity topologies promise better sensitivity, especially if the pumping power  $W < W_{\text{SQL}}$ .
4. Unfortunately, none of the mechanical QND schemes known today can fully realize potential sensitivity of intracavity topologies.

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