



THE UNIVERSITY
OF ADELAIDE
AUSTRALIA

Hartmann Wavefront Sensing for the Gingin Experiment

Aidan Brooks, Peter Veitch, Jesper Munch

Department of Physics, University of Adelaide

LSC, LLO Mar 2005

LIGO-G050196-00-Z



Layout of Talk

- Thermal distortion and compensation in Adv. GWIs
- Off-axis Hartmann wavefront sensor – design and analysis
- Bench top tests of Hartmann sensor
- Implementation of sensor in the Gingin experiment

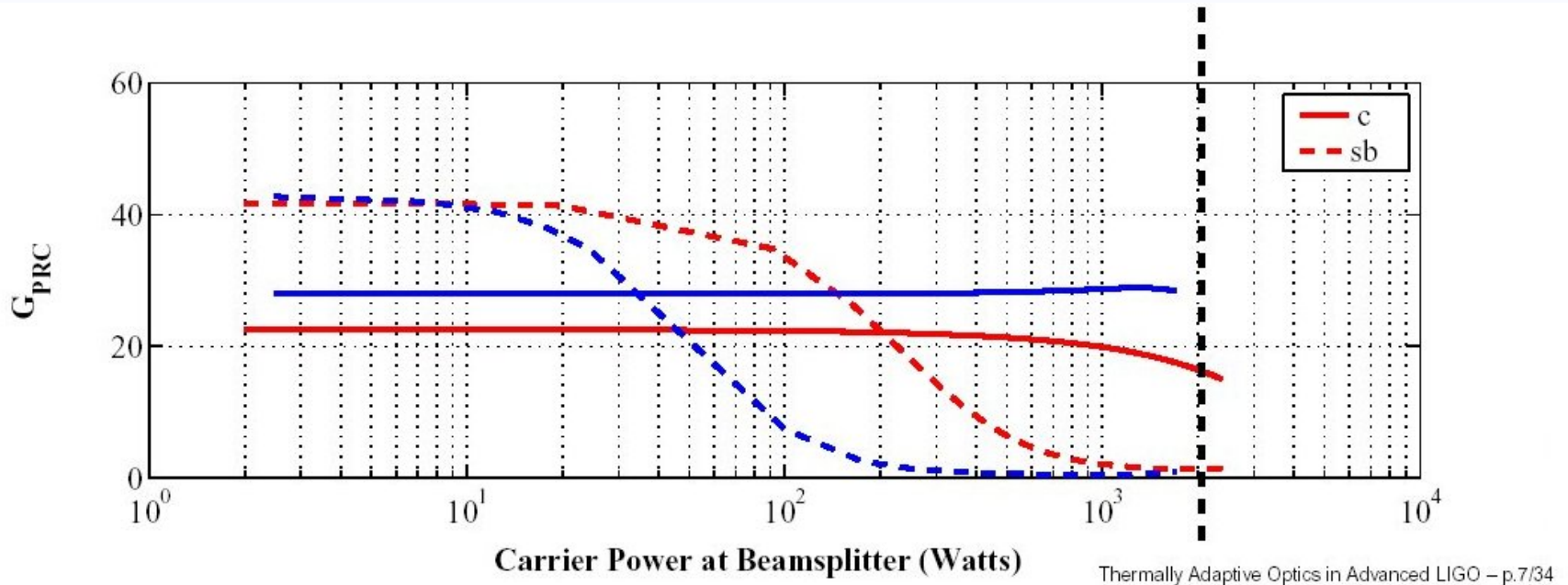
ACIGA Objectives

- Investigate the operation of active thermal compensation systems for use in Adv. GWIs.
- University of Adelaide is providing a sensor to measure thermo-refractive distortion and effectiveness of compensation in the Gingin High Power Test Facility (AIGO).



The Australian International Gravitational Observatory (AIGO)

Crux of Thermal Problem



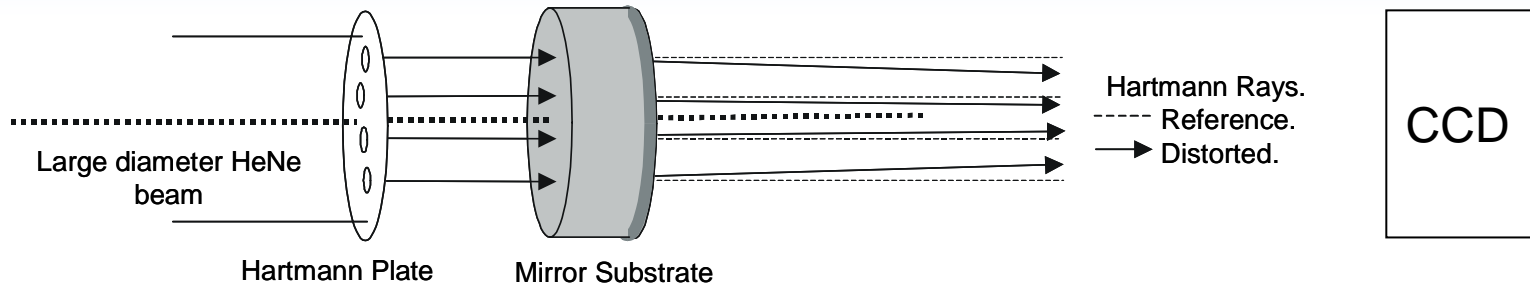
Courtesy of Ryan Lawrence and David Ottaway, MIT

- Figure shows prediction of MELODY model of Advanced LIGO
- Absorbed power, in coatings and substrates, causes thermal lensing
- Sideband power is coupled out of TEM00
- Power recycling cavity eventually loses lock
- Adv. LIGO cannot achieve desired sensitivity unaided

How to Maintain Locked Cavity?

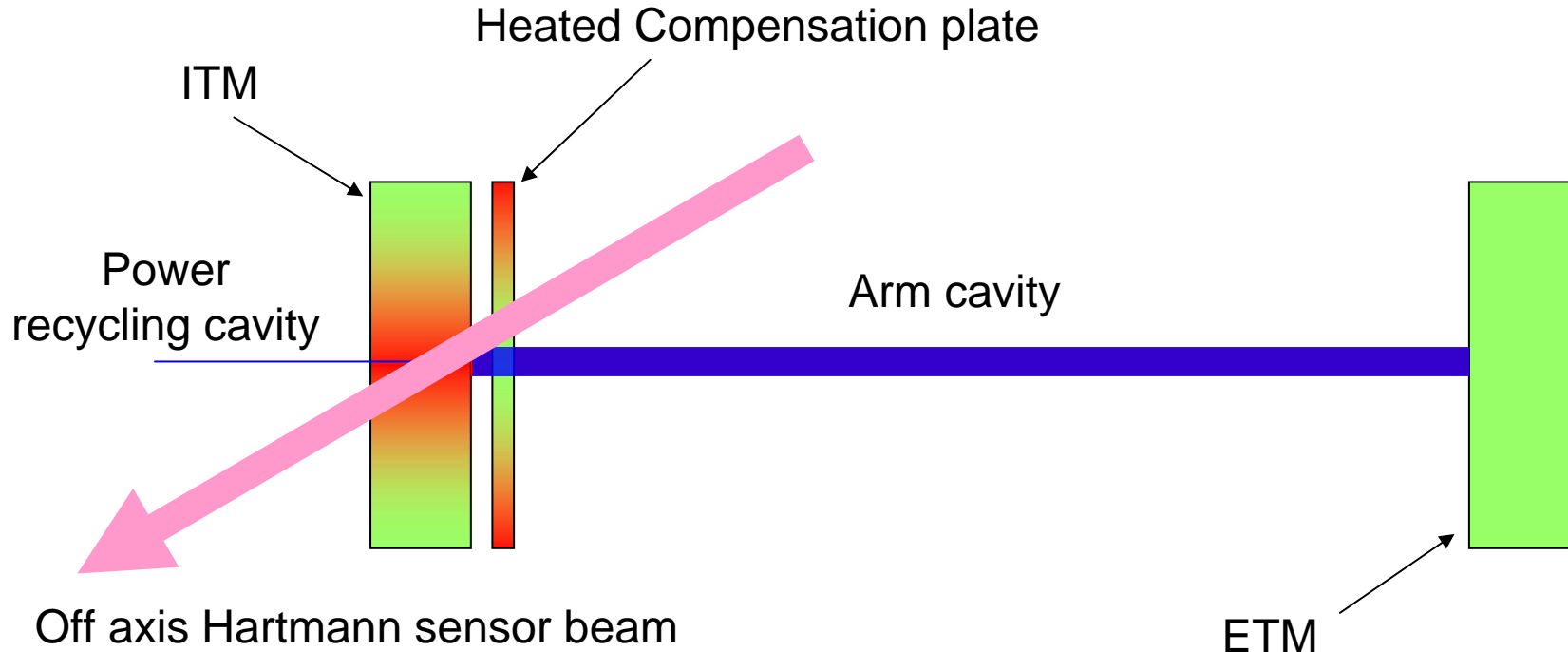
- Measure distortion in ITM with an off-axis wavefront sensor
- Employ active compensation system, reducing distortion to $< \lambda/200$. Heated compensation plate will be used in Gingin experiment
- Hartmann sensor selected
 - not sensitive to alignment
 - simulated sensitivity $< \lambda/1000$

Hartmann Wavefront Sensor

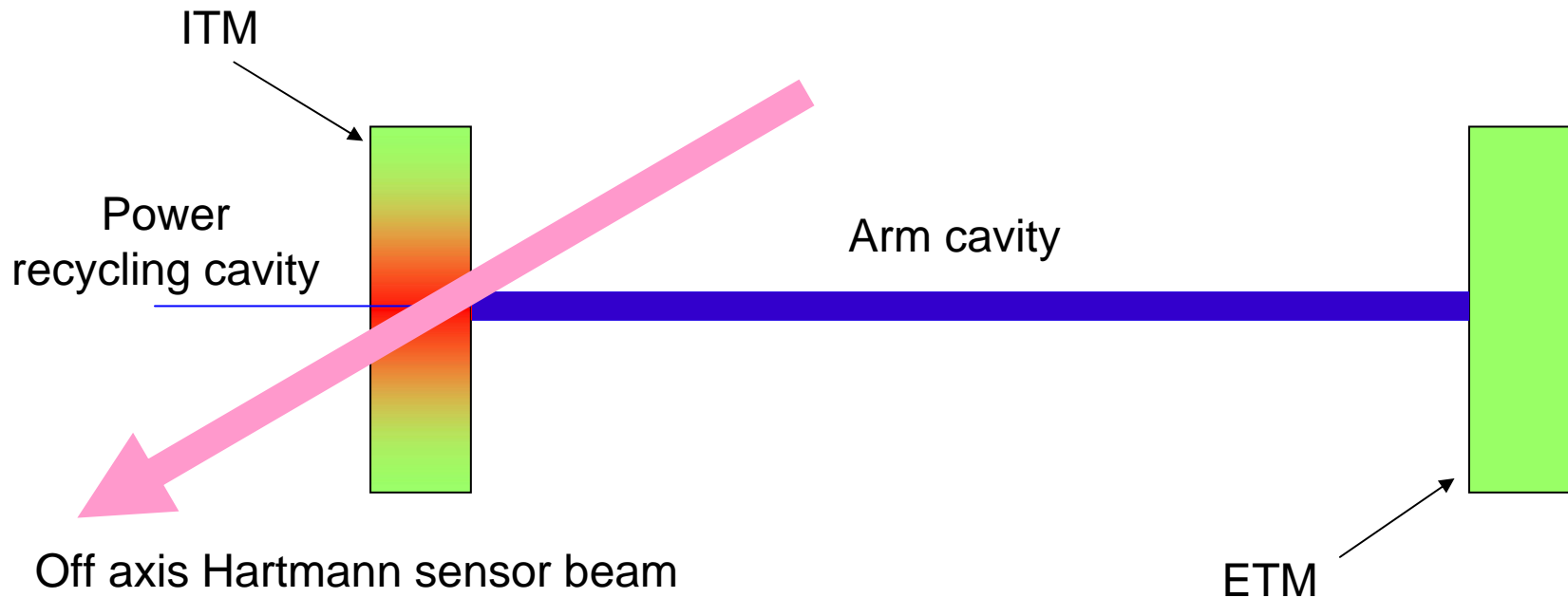


- Each Hartmann ray propagates normal to the wavefront
- Subsequently, rays are incident on a CCD forming a pattern of spots
- Centroid of each spot is found using a 1st moment calculation on spot intensity
- When the wavefront changes, the spots are displaced on the CCD
- Spot displacement is proportional to gradient of the change in wavefront
- Simulated Hartmann measurement had an precision of $< \lambda/1000$

Example of Compensation System

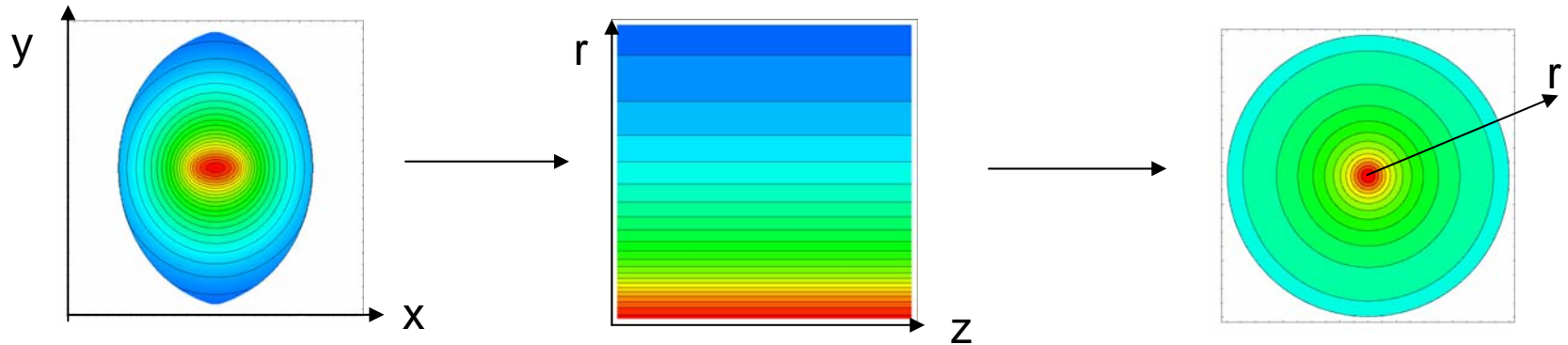


Example of Compensation System



- How do you relate the off-axis OPD to the on-axis OPD?

Modal Analysis of Off-Axis OPD



$$\varphi(x, y) = \sum a_i g_i(x, y)$$

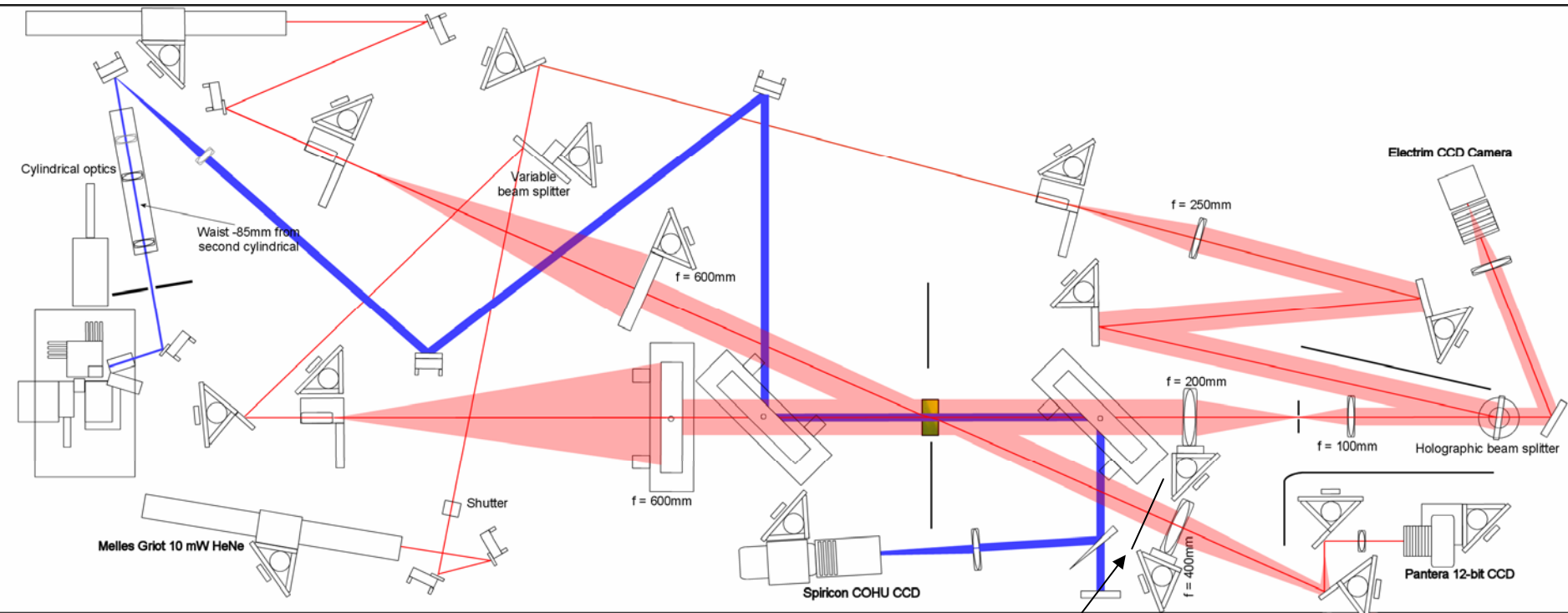
$$n(r, z) = \sum a_i f_i(r, z)$$

$$\varphi(r) = \sum a_i F_i(r)^*$$

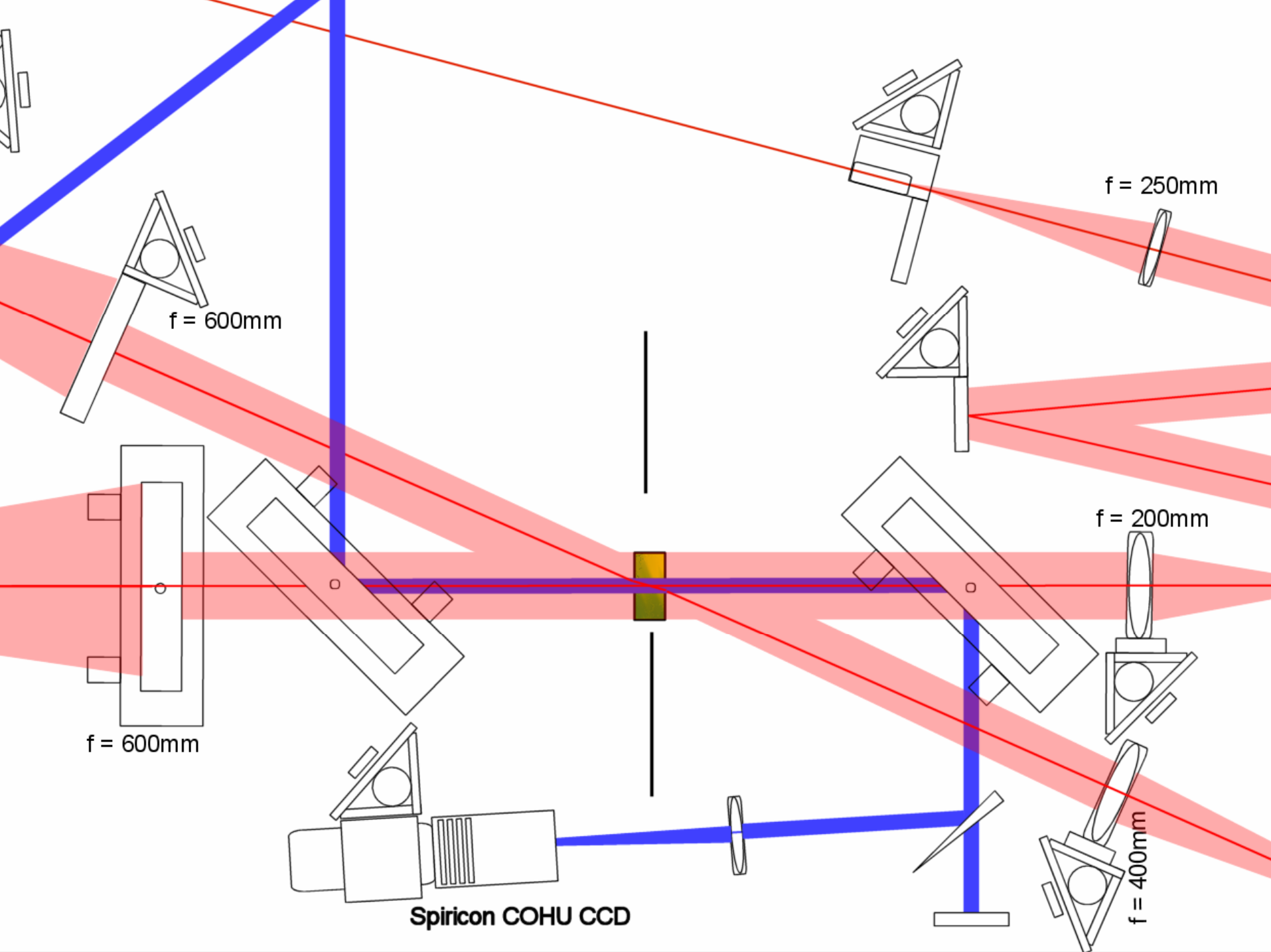
- Functions $g_i(x, y)$ are path integrated versions of $f_i(r, z)$
- Parameters a_i found by a least squares fit of off-axis OPD to functions $g_i(x, y)$
- Ideally, both sets $\{f(r, z)\}$ and $\{g(x, y)\}$ are orthogonal and there exists a simple path integral relating them
- No ideal sets have been found – currently using a small set of non-orthogonal functions (Gaussians) for $f(r, z)$

* $F_i(r)$ is the integral of $f_i(r, z)$ along the z-axis

Off-Axis Bench Top Test

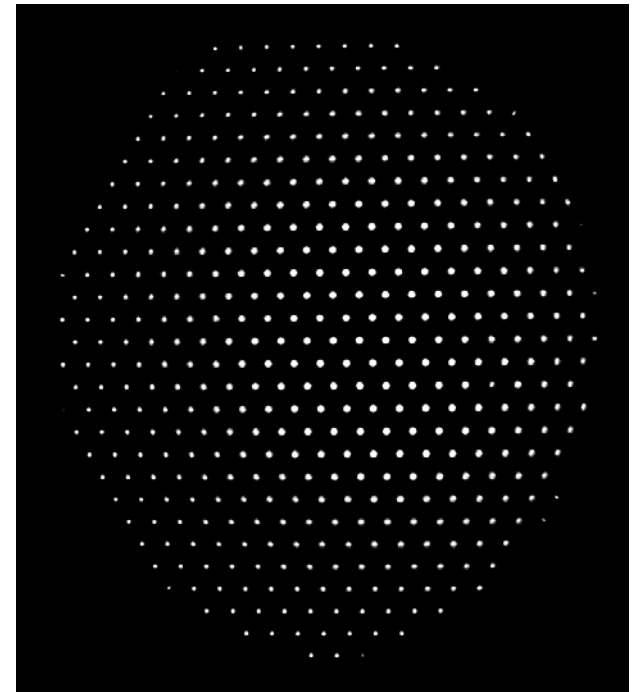


Hartmann plate



Results – Angular Noise

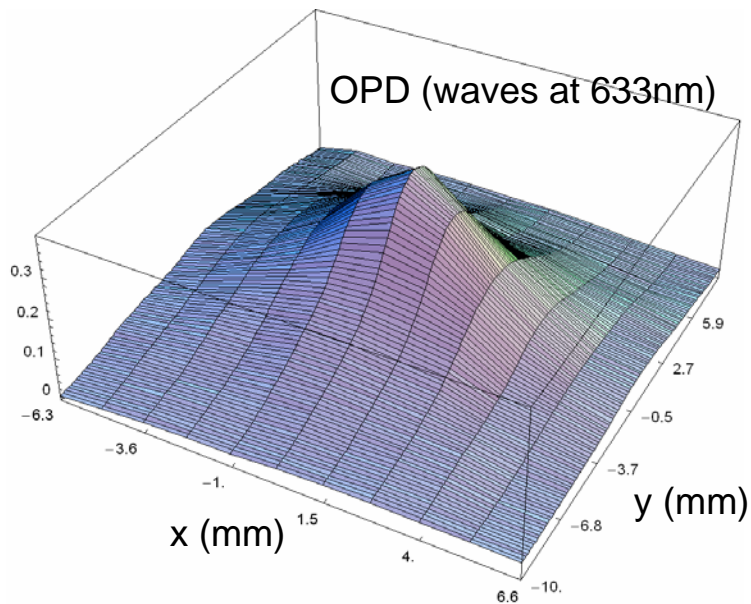
- Differences in successive images yield the angular noise of the Hartmann sensor
- Minimum detectable angle
 $\approx 3.5 \mu\text{radians}$
- Min OPD $\approx \lambda/200$ (based on .9mm separation between holes in Hartmann plate)



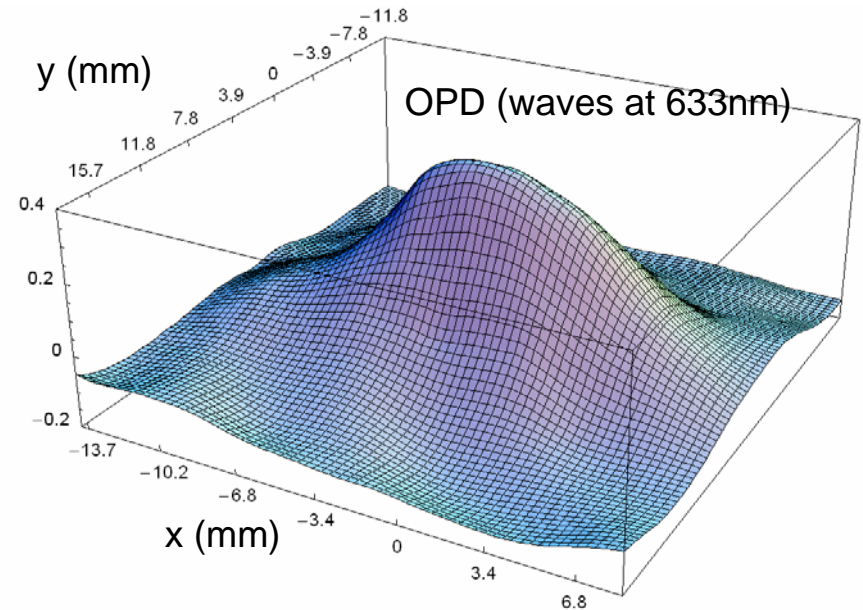
Hartmann spot pattern

Coincidence Measurement – Raw Data

On axis OPD (interferometer)



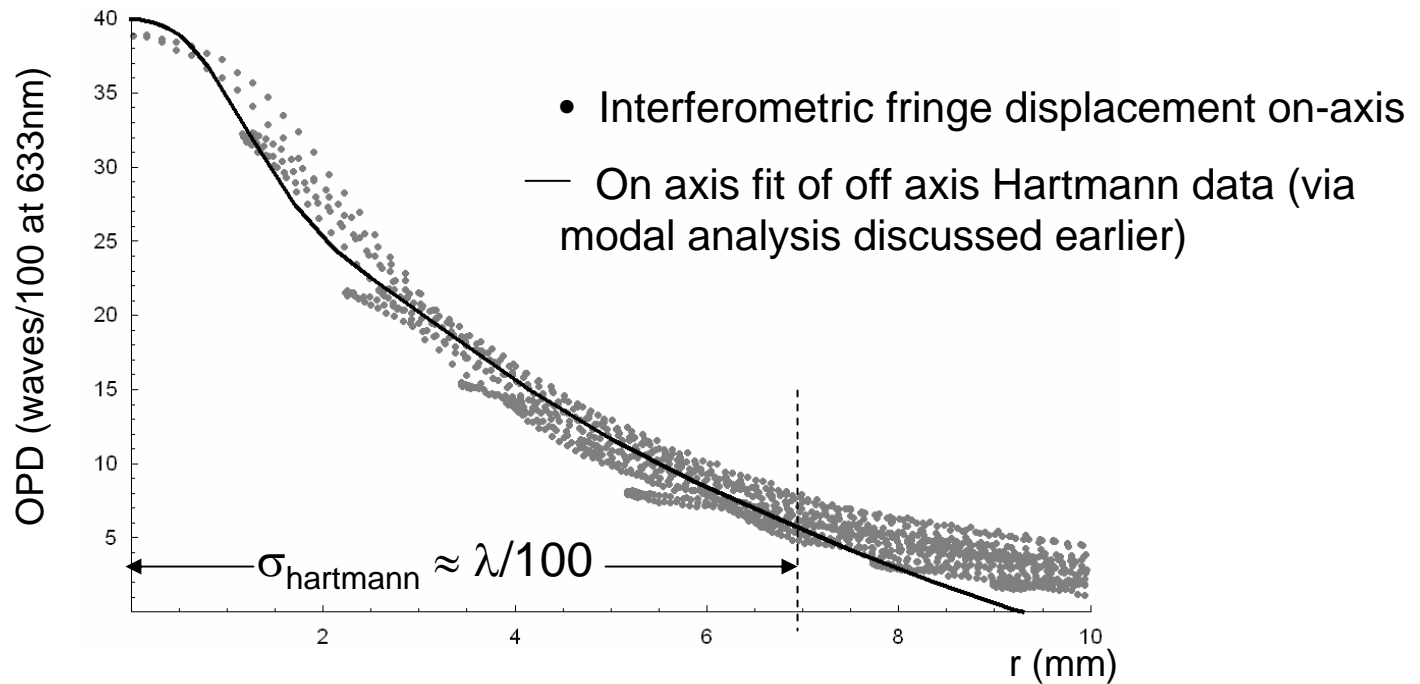
Off axis OPD (Hartmann)
(reconstructed from gradient map)



Sanity Check on data

- ✓ OPD's roughly the same size
- ✓ Off-axis OPD elongated in the x direction as expected

Results – Radial OPD



- On-axis distortion is elliptical (minor axis = 90% major axis)
- Systematic error since analysis assumes axial symmetry
- Worst case analysis: ignore systematic error, average elliptical data to circle. In this case standard deviation between on-axis data and analyzed Hartmann data $\approx \lambda/100$

Sensitivity of Hartmann sensor

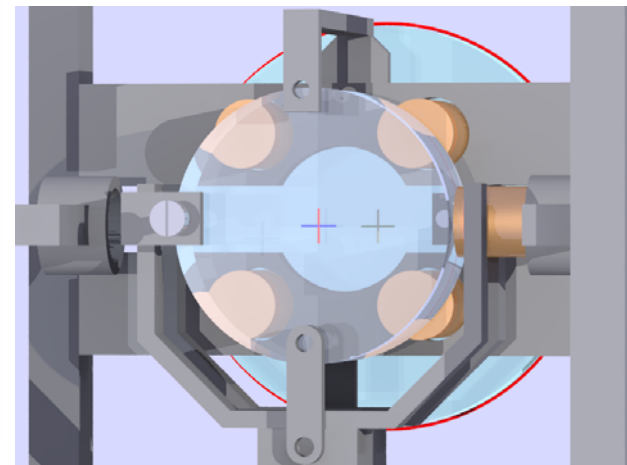
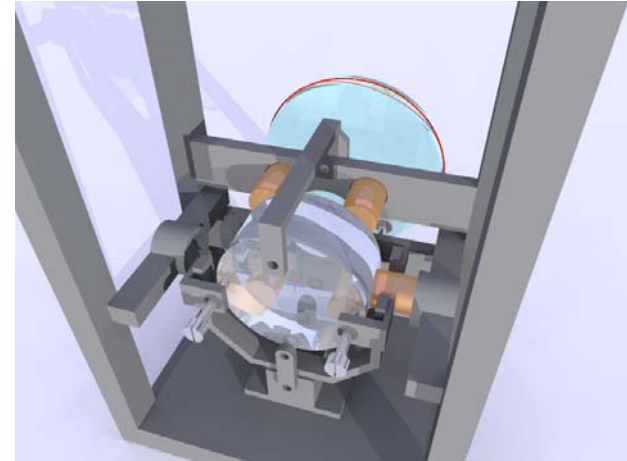
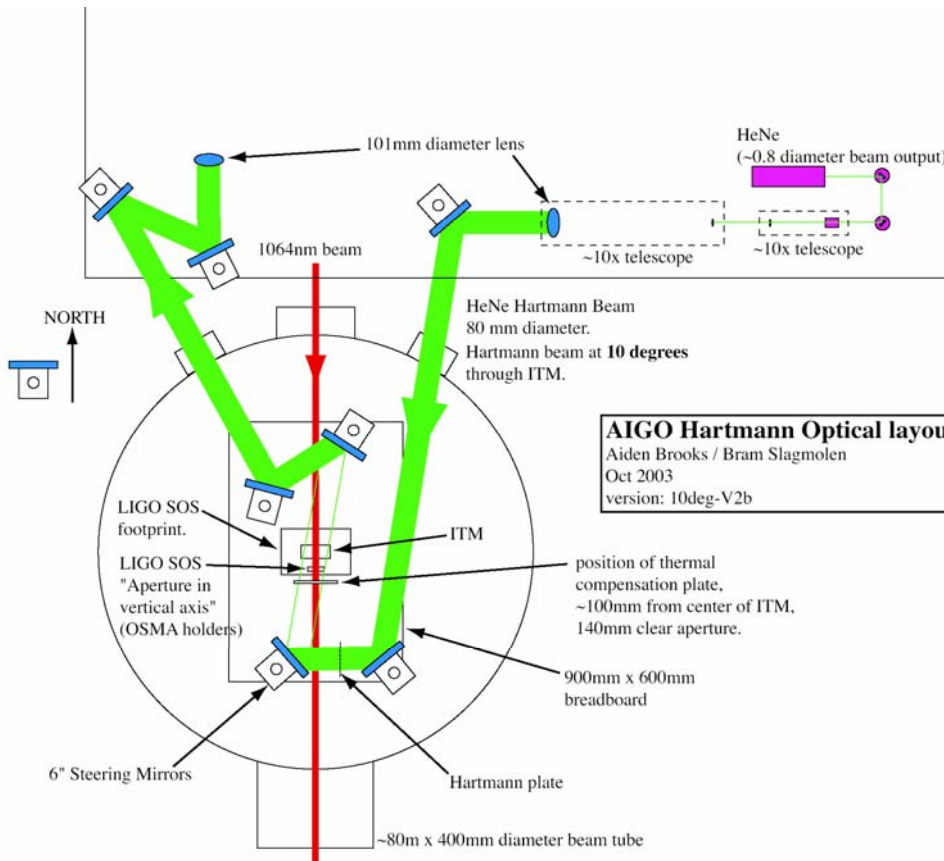
Precision

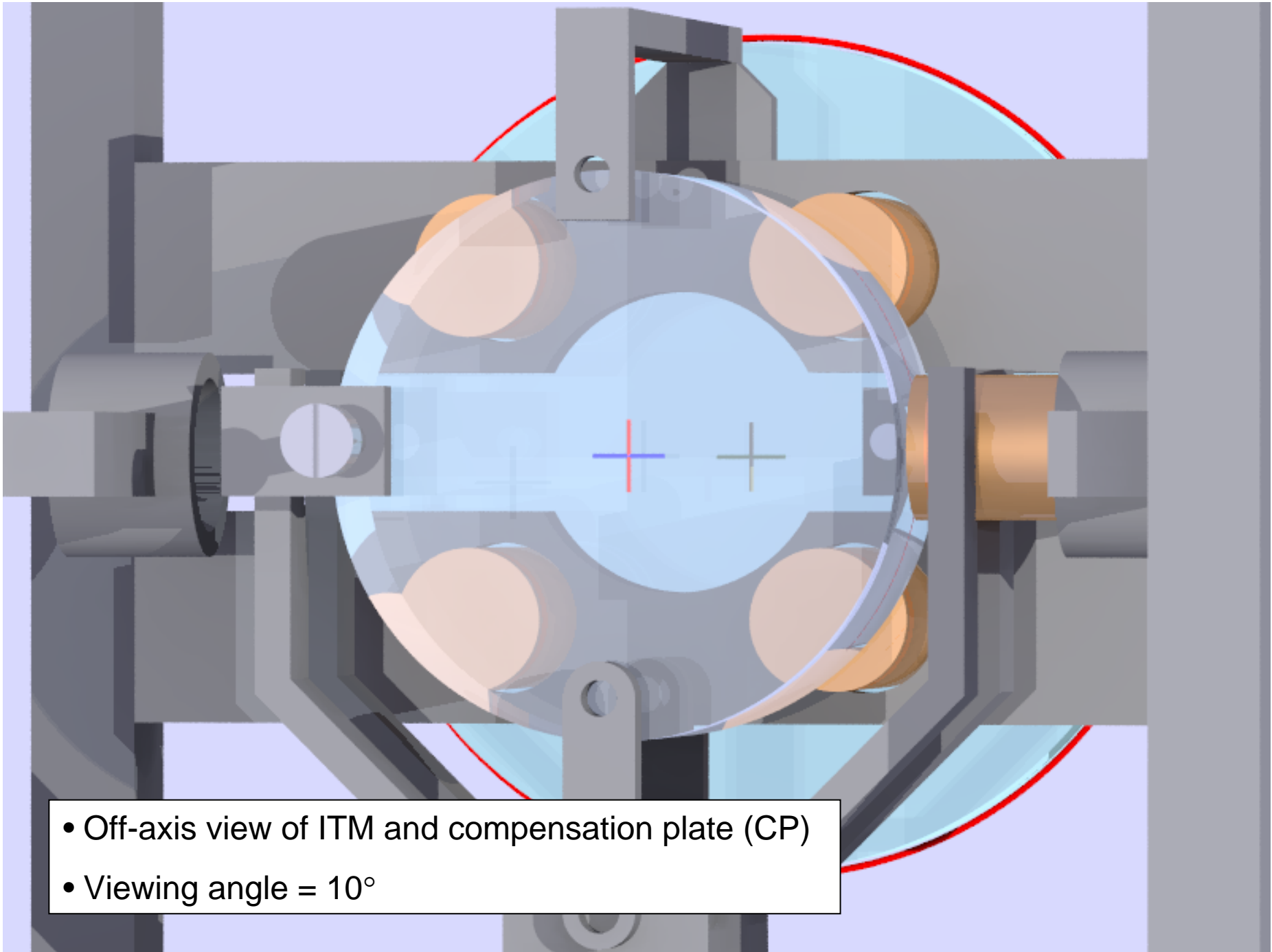
Required	$< \lambda / 200$
Simulated	$< \lambda / 1000$
Experiment	$< \lambda / 100$

Issues to address before final experiment at Gingin

- Systematic errors: - number/type of fitting functions
- elliptical heating beam
- Random errors: - air currents – use tent?
- can illumination of Hartmann plate be more uniform?
- precision of interferometer

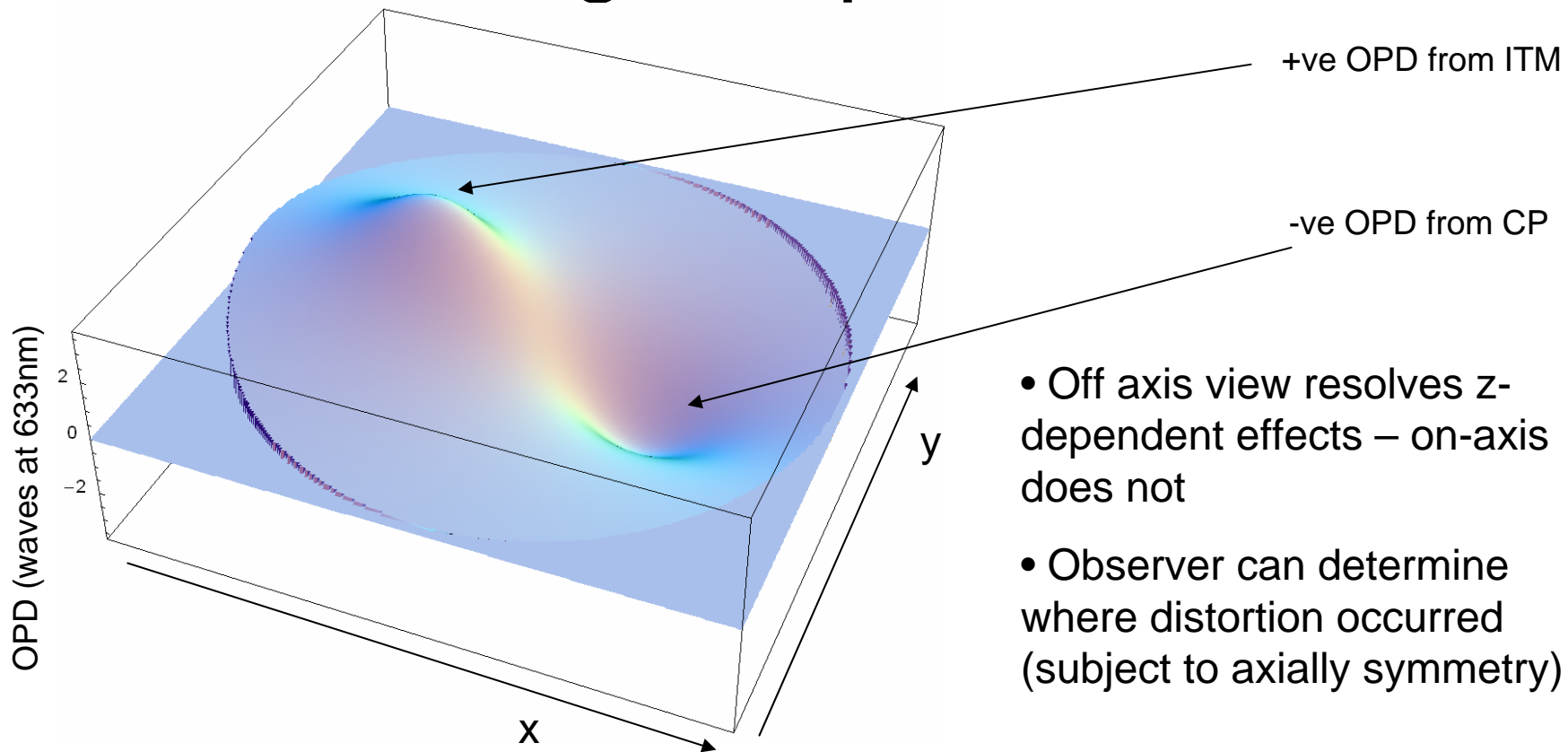
Gingin Experiment Design





- Off-axis view of ITM and compensation plate (CP)
- Viewing angle = 10°

Prediction of Off-Axis OPD for Gingin Experiment



- Off axis view resolves z-dependent effects – on-axis does not
- Observer can determine where distortion occurred (subject to axially symmetry)

- Distortion and compensation recorded in a single measurement
- Analyzed data can be used as an error signal for CP

Closing remarks

- Current off-axis Hartmann sensor has achieved accuracy of approximately $\lambda/100$ in the lab.
- Should be able to improve this by addressing issues covered earlier.

Gingin installation schedule

MAR-APR '05	Installation of Hartmann beam steering optics and compensation plate
MAY-JUN '05	Test of Hartmann system <ul style="list-style-type: none">- on-site sensitivity test- measure compensation plate OPD
JUL-DEC '05	ITM distortion and compensation plate combined phase measurement