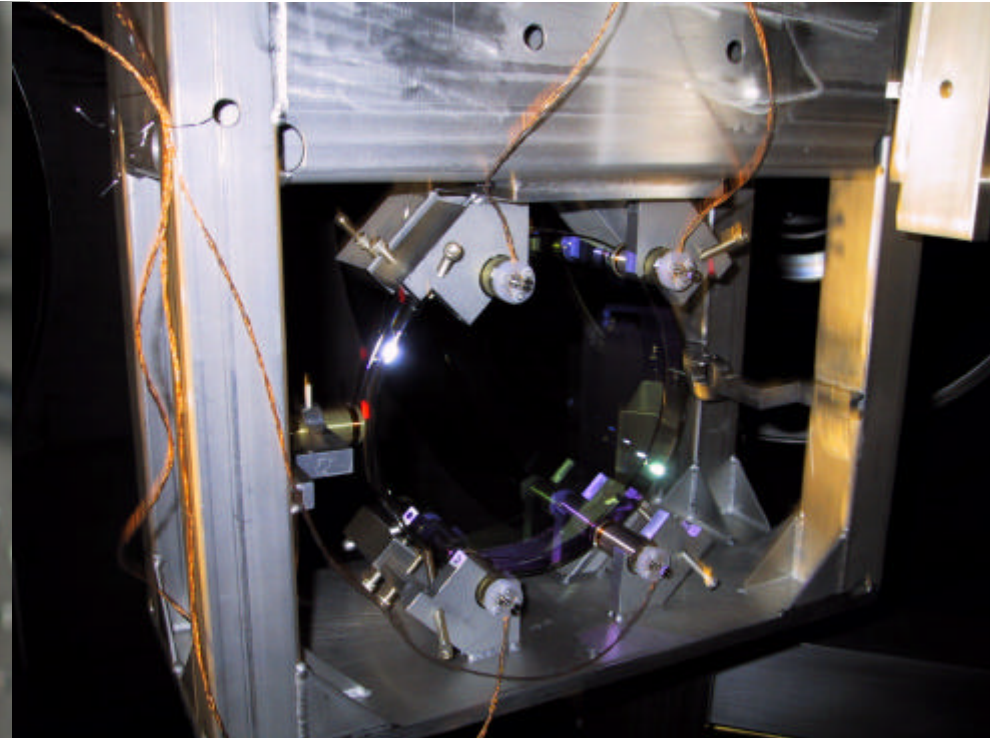
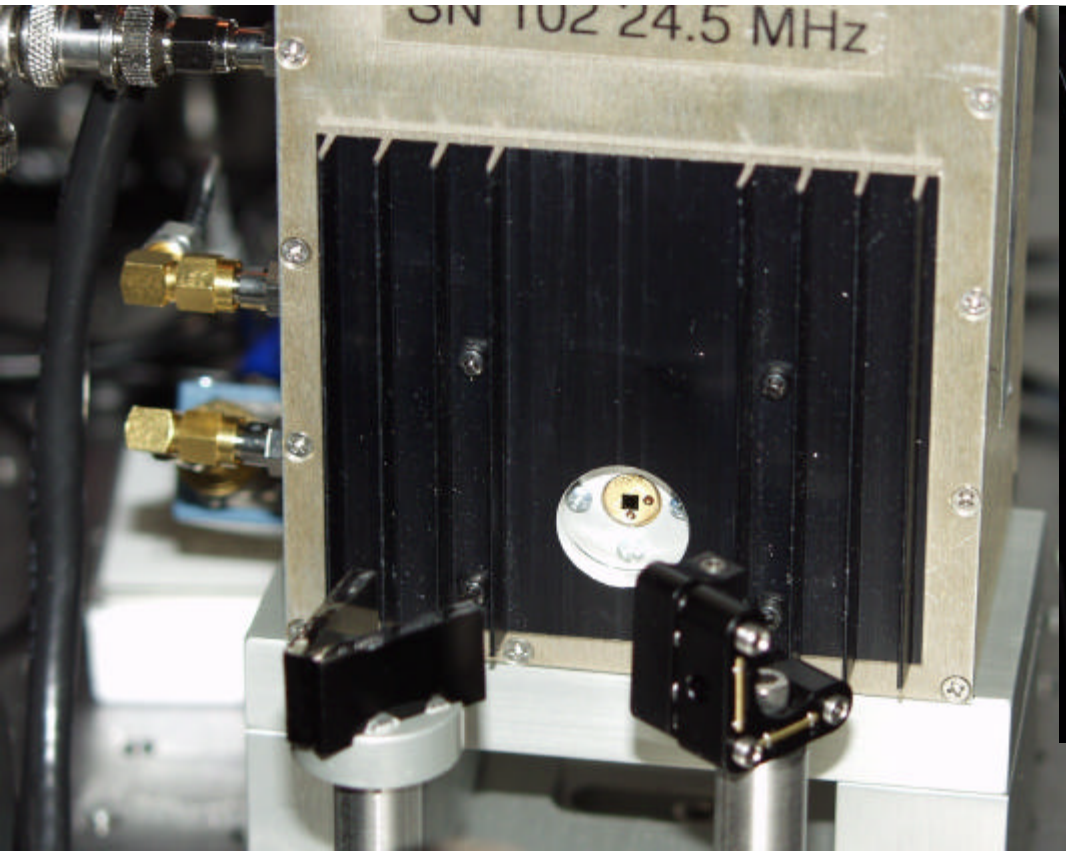




LIGO- I: Breaking the Sensitivity Barrier



March 2nd, 2004

Rana Adhikari

MIT

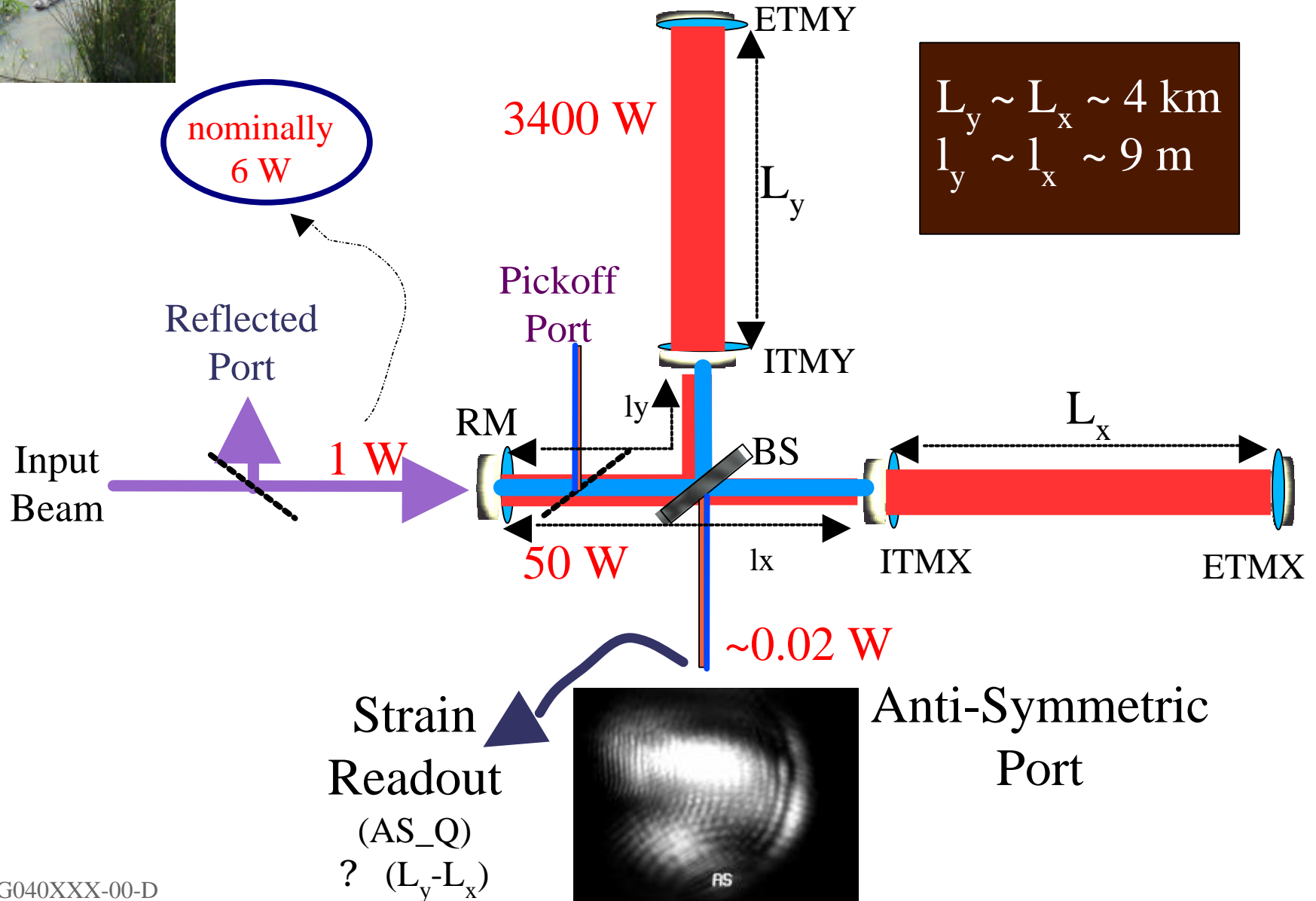
LIGO-G040557-00-D



OUTLINE

- What is the noise in the interferometers now?
- *Where does the SRD Curve come from?*
- What we know about the 'fundamental' noises.
- **Can we ever reach the SRD ?**
- What do we do about it?

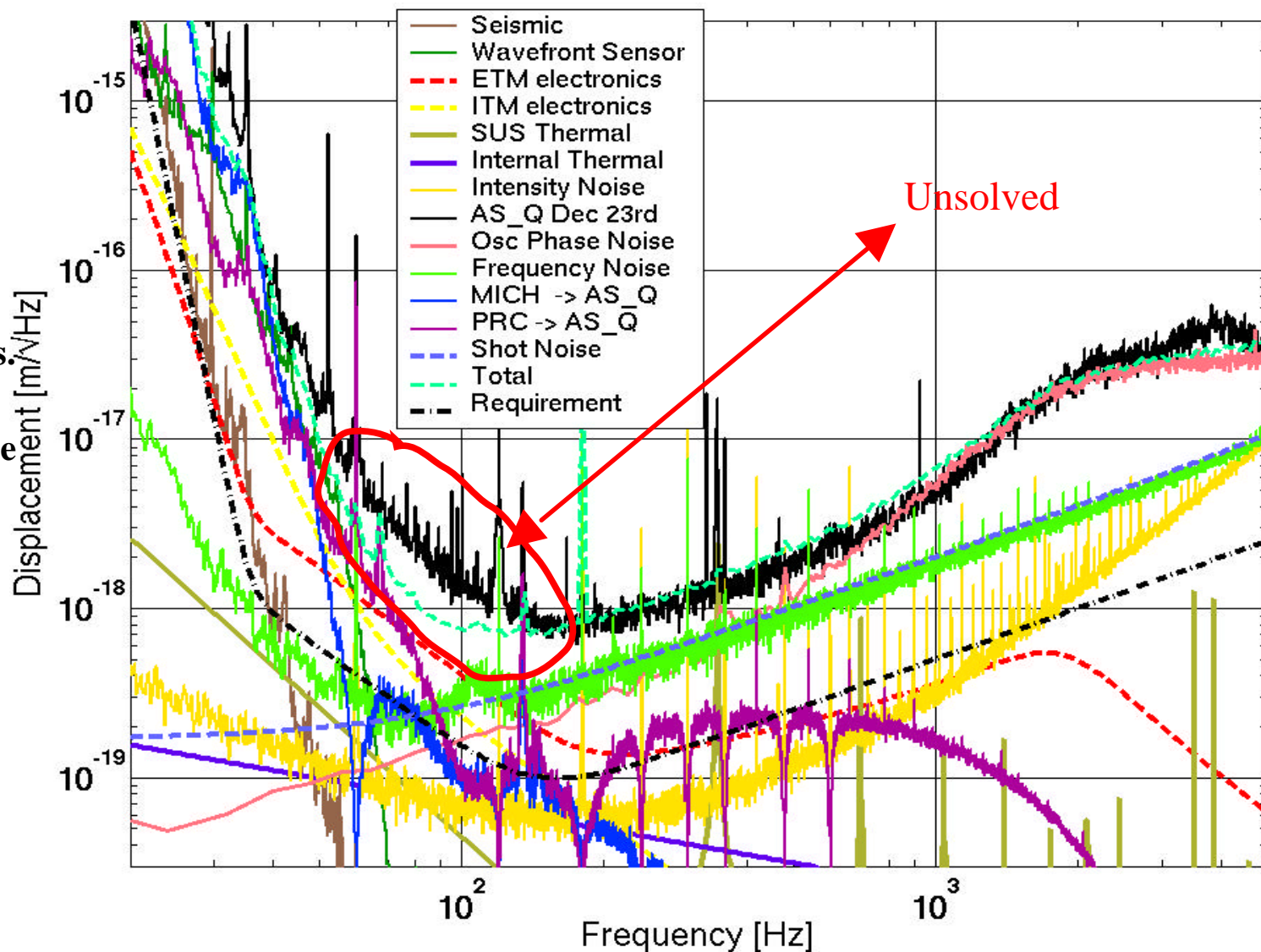
The INTERFEROMETER





The Noise in Livingston

- **~10X higher than design...**
- **~10⁵ X lower than a few years ago.**
- **Most of the noise is explained by the models.**
- **Plans are in place to reduce each noise source above SRD.**

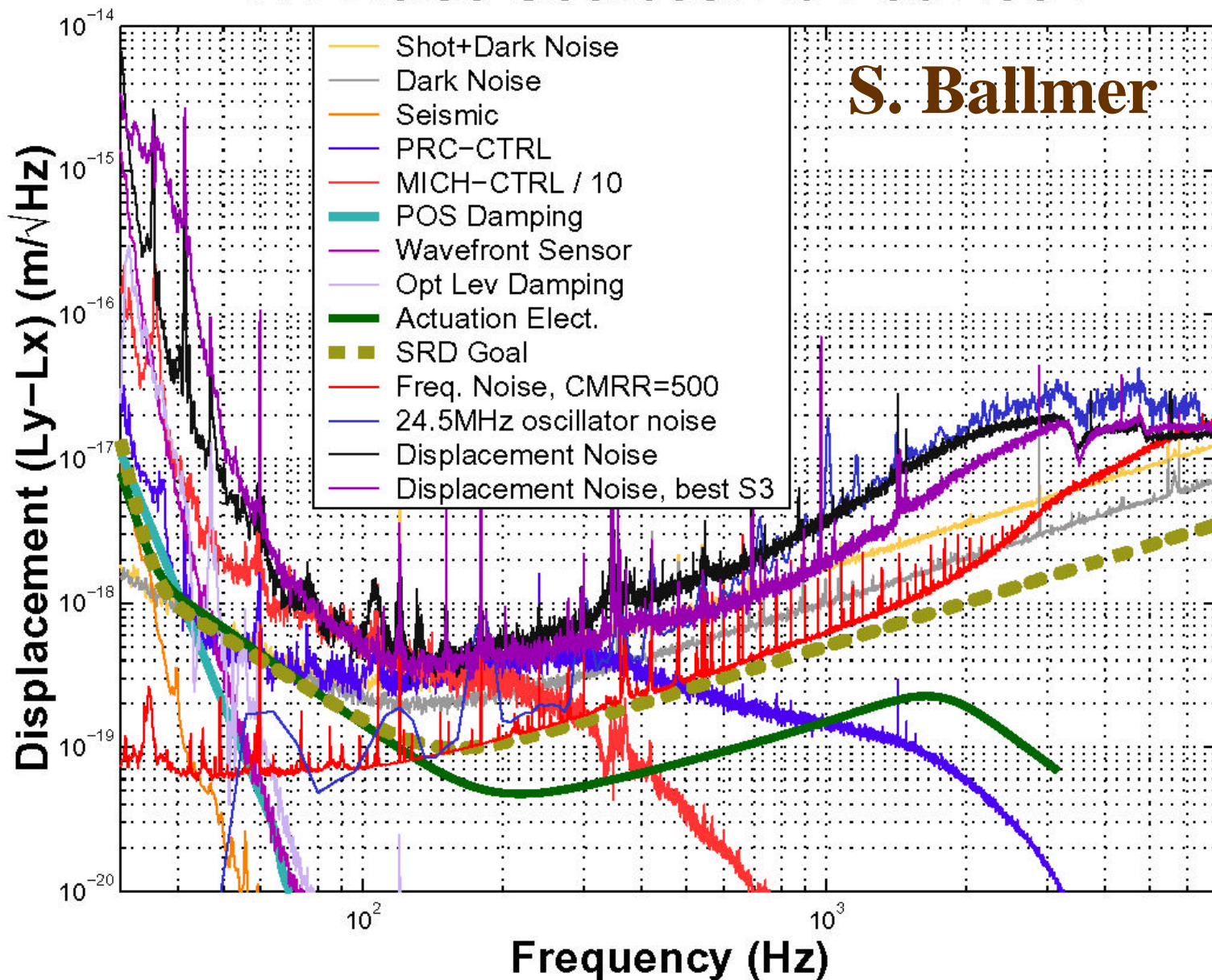




H1 Noise Sources: 23 Feb 2004

S. Ballmer

- 10X higher than design...
- 10^5 X lower than a few years ago.
- Most of the noise is explained by the models.
- Plans are in place to reduce each noise source above SRD.





Science Requirements Doc: The LIGO-I Sensitivity Goal

Seismic:

“Standard” spectrum

$$h(f) \propto f^{-2}$$

filtered by an isolation stack
and a 1 Hz pendulum

Suspension Thermal:

Viscously damped harmonic
oscillator:

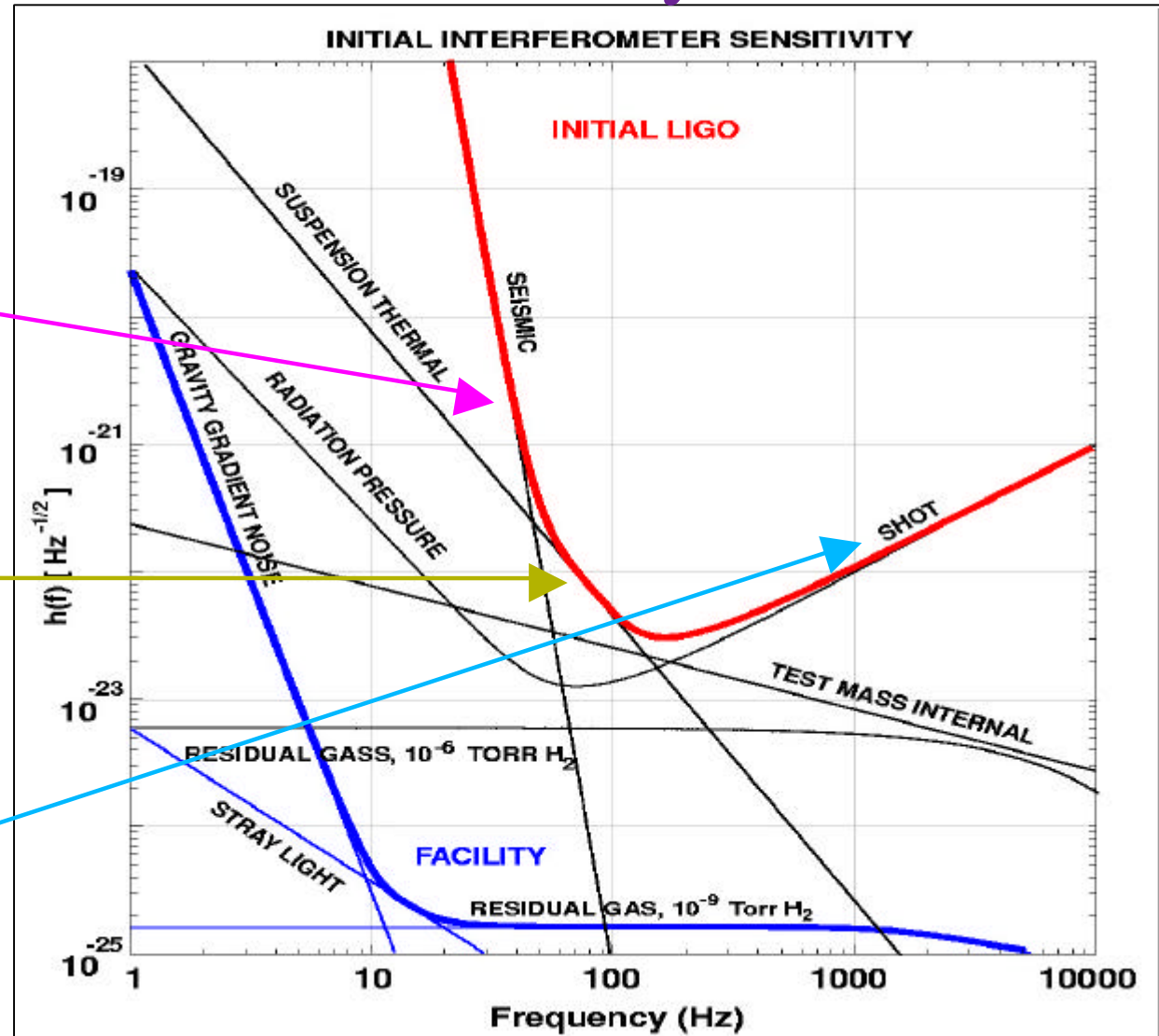
$$h(f) \propto f^{-2}$$

Shot Noise:

'Mediocre' optics give:

- Recycling gain ~ 30
- Contrast $\sim 3 \times 10^{-3}$

$$h(f) \propto f^{-1}$$



Seismic Noise



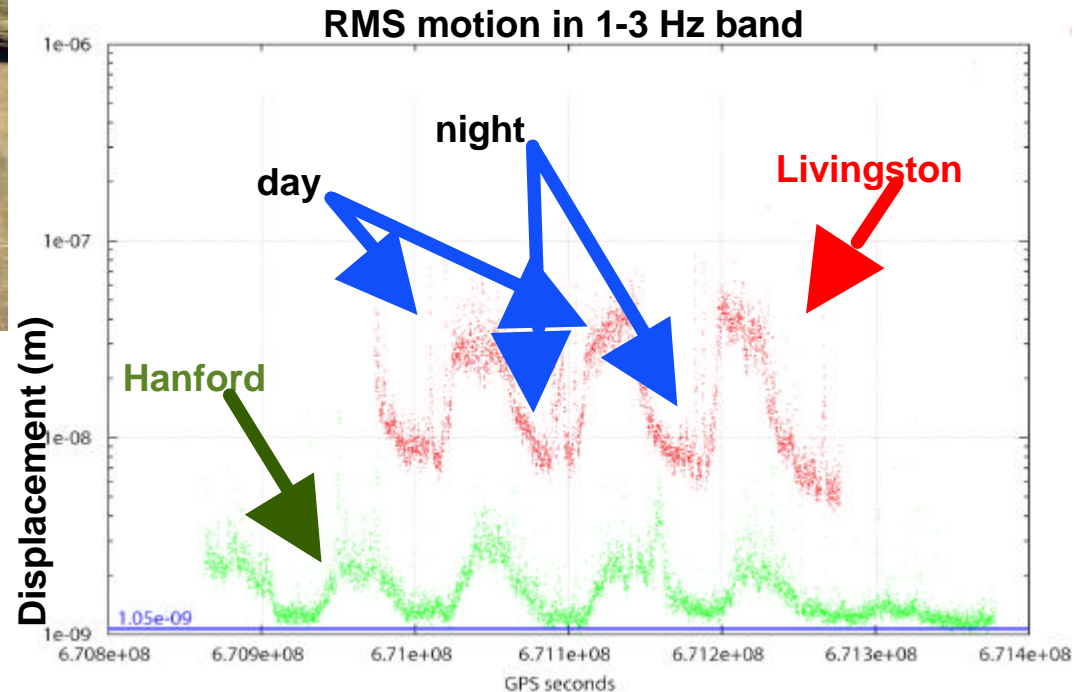
Seismic noise in GW band is mostly independent of human activity.

Variability is mostly for $f < 10$ Hz



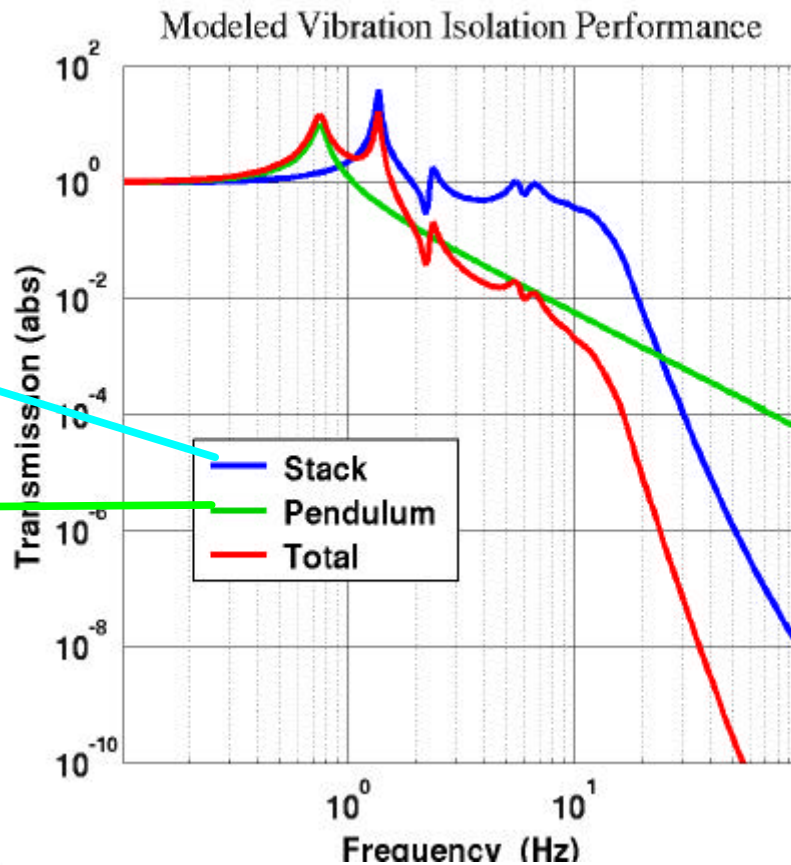
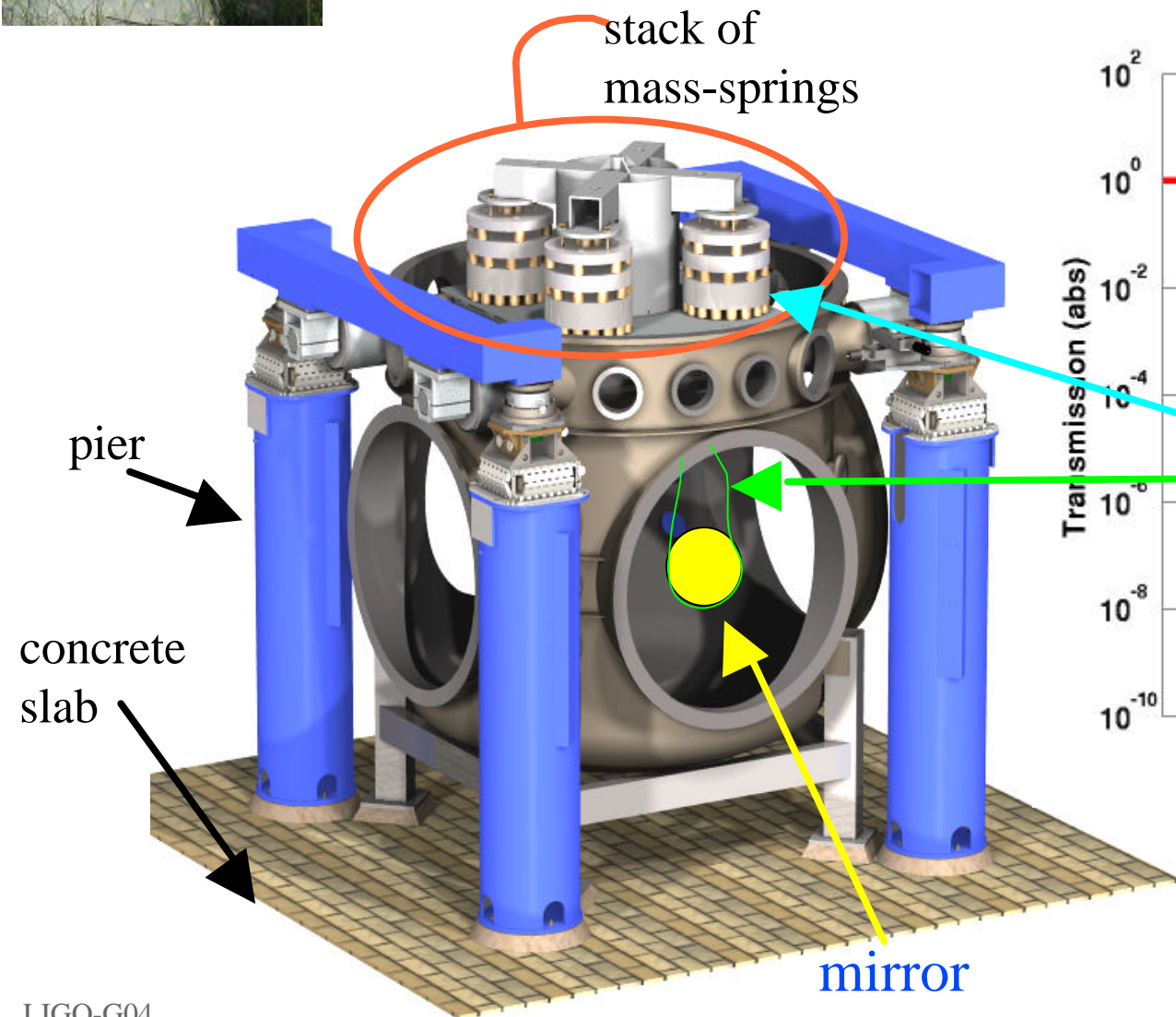
Large day/night variability due mostly to noise made by people:

- Logging
- Traffic
- Construction



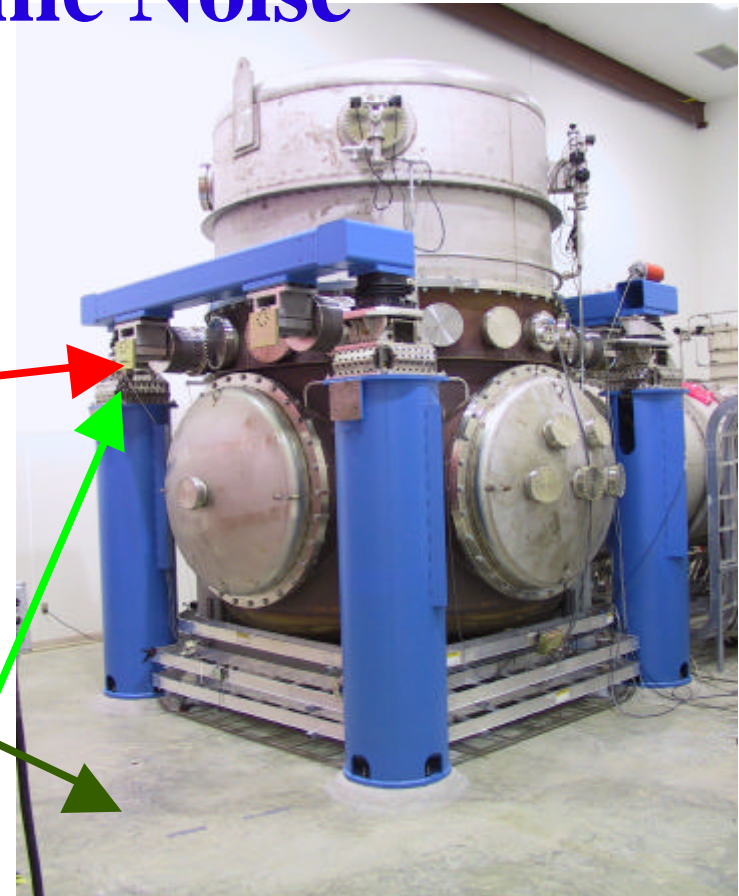
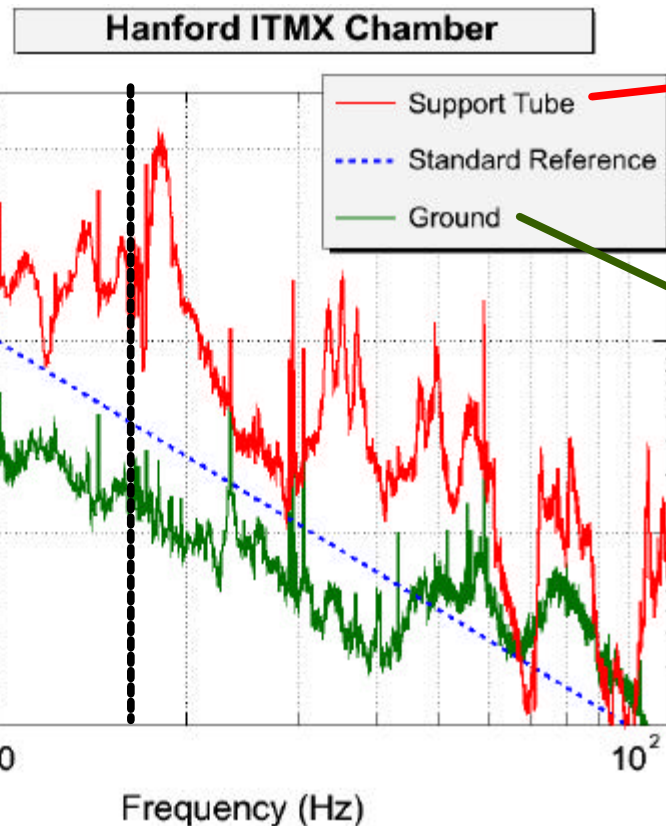


Seismic Noise



Measurements: Seismic Noise

- Ground noise is higher than expected.
- $0.1 < f < 4$ Hz excess @ LLO: Hydraulic Pre-Isolator
- $f > 5$ Hz narrow features from HVAC at both sites. Being investigated at LHO.



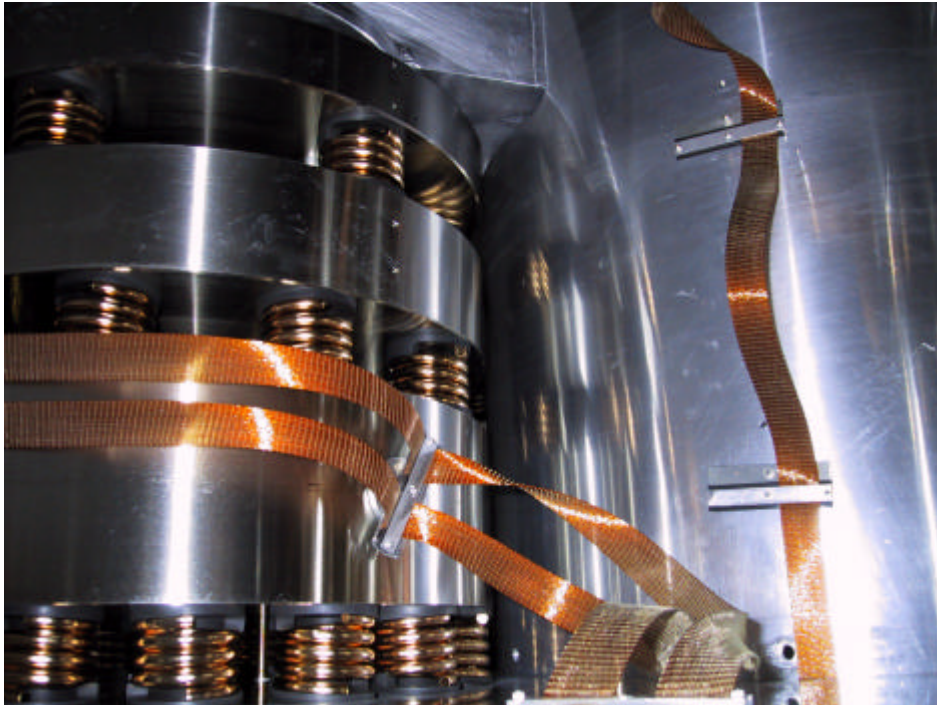
Accelerometers at the top of the piers are **10-100x** noisier than the ground at some frequencies from 10-100 Hz!

Studies at LASTI say that its mostly tilt. Could also be partly acoustic above 30 Hz.

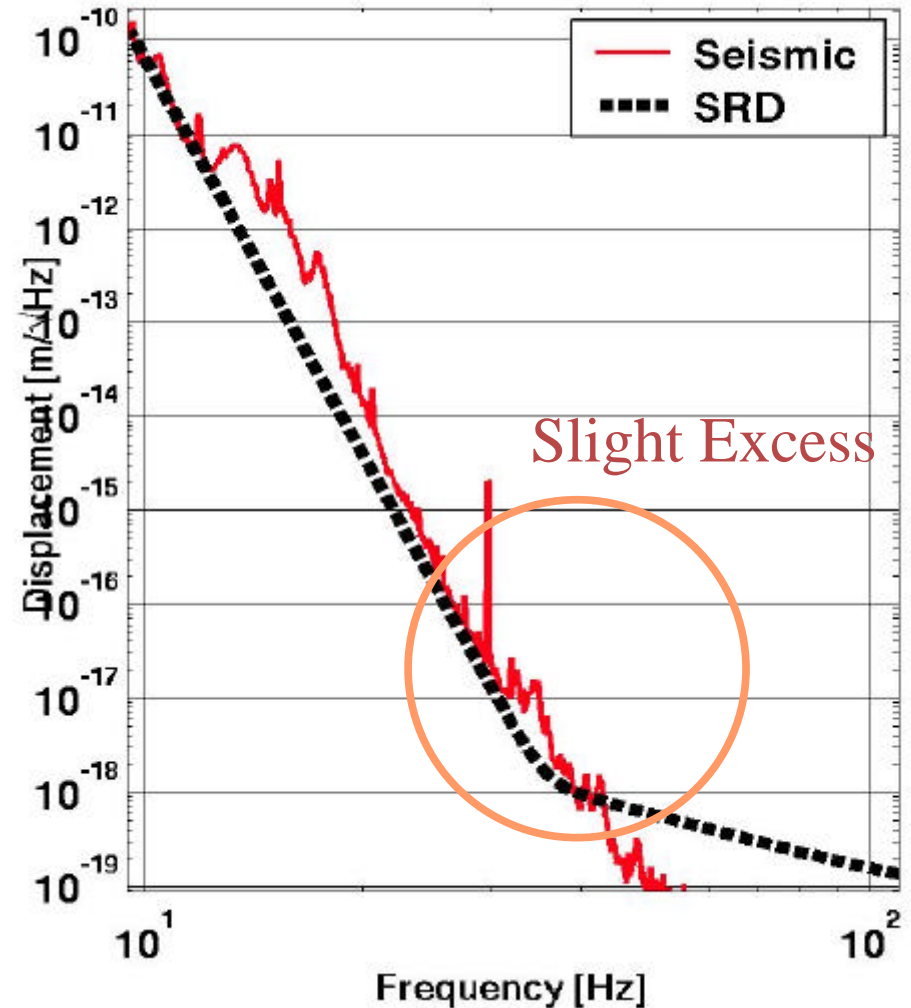


Measurements: Seismic Noise

- ➔ Take measurements at the top of the piers.
- ➔ Use the Hytec BSC model and the locally damped suspension model to get the TF.



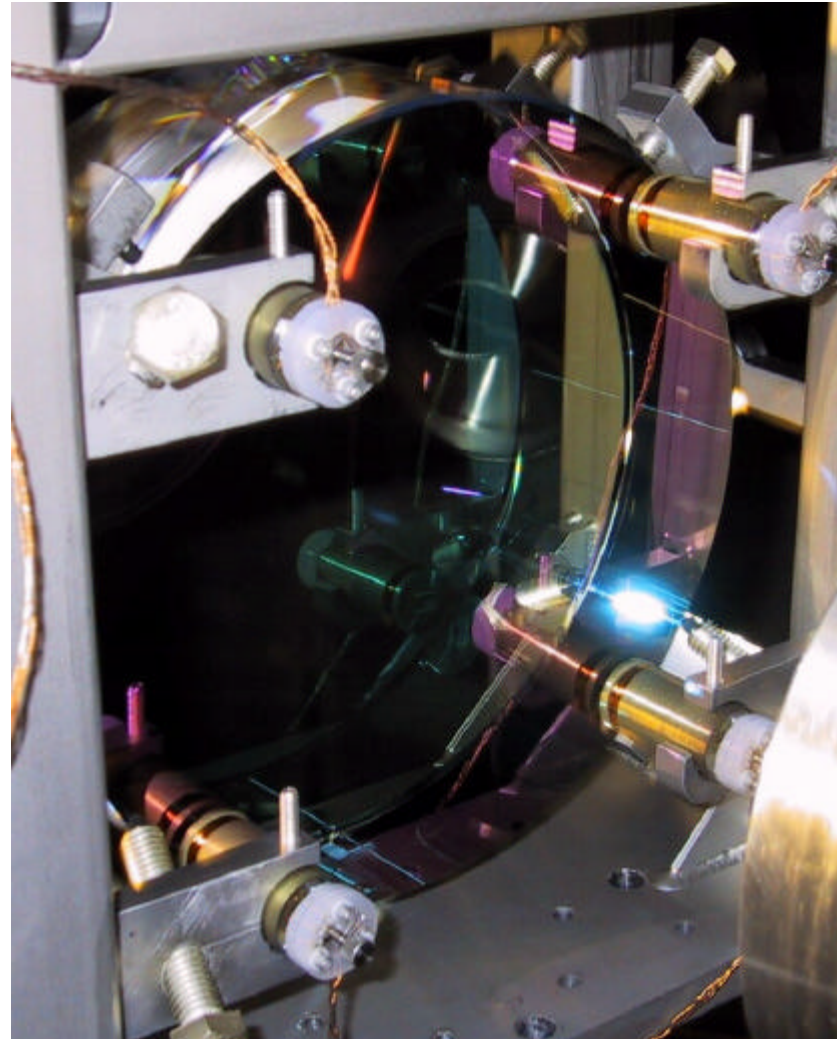
L1 Differential Arm Displacement Noise





Test Mass Thermal Noise I

Measurements:



- ➔ Need to know the loss angle in the mirror substrate and in the coating.
- ➔ Measure ~ 10 Q's on every test mass mirror.
- ➔ Use highest Q to set lower limit on internal loss of the fused silica substrate. Assumes coating loss does not contribute to the highest Q mode.
- ➔ Use energy ratios from Dennis' FEA voodoo to get the loss angle of the coating.
- ➔ Take loss angles of the substrate and coating, plugin to formula from A. Gretarsson's thesis to get test mass displacement
- ➔ Method verified by experiment --- *K. Numata, et al. PRL (2003)*
- ➔ **This method gives a lower strain noise than what's obtained by doing the traditional summation over normal modes.**

Details in Gregg Harry's March 2003 LSC Talk

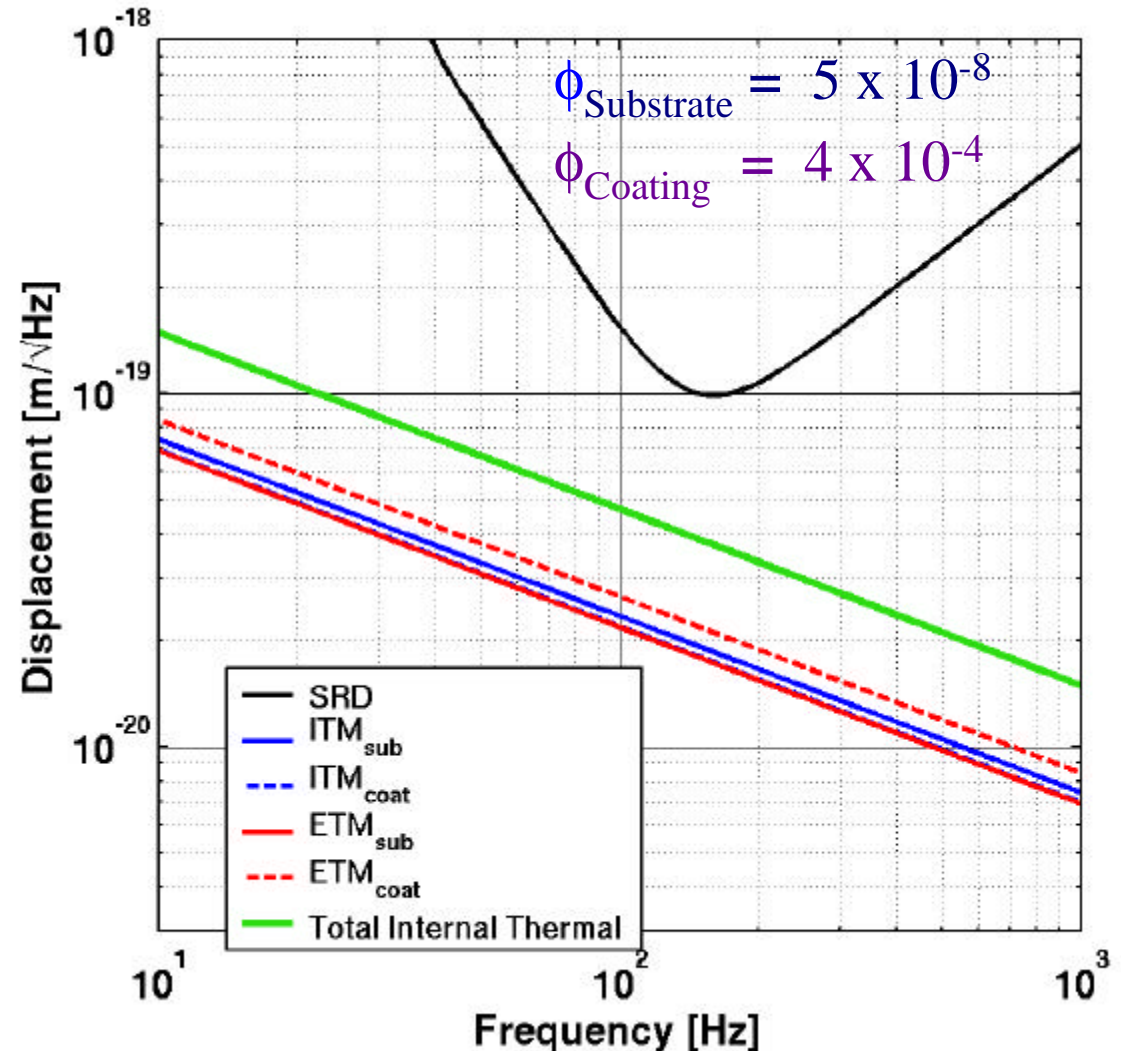
Results: $\phi_{\text{Substrate}} < 1 \times 10^{-7}$
 $\phi_{\text{Coating}} \sim < 4 \times 10^{-4}$



Test Mass Thermal Noise I

Predictions:

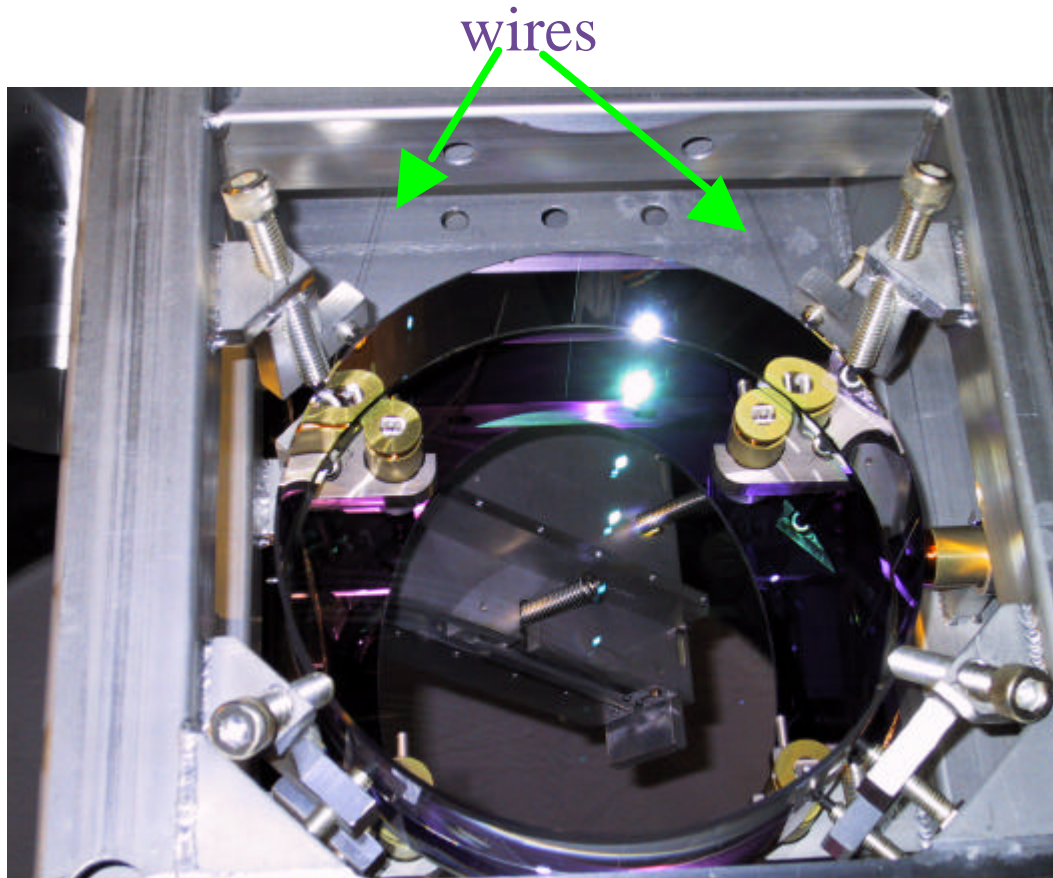
- Can calculate the thermal noise contributions from the substrate and coating separately.
- ETMs have **twice** as many coating layers as the ITMs.
- Beam is slightly bigger on the ETMs.
- $x_{\text{coating}}(f) \propto (\text{thickness})^{1/2} * (\text{spot size})^{-1}$
- $x_{\text{substrate}}(f) \propto (\text{spot size})^{-1/2}$
- **~2x lower** than SRD estimate





Suspension Thermal Noise I

Not Viscous Damping



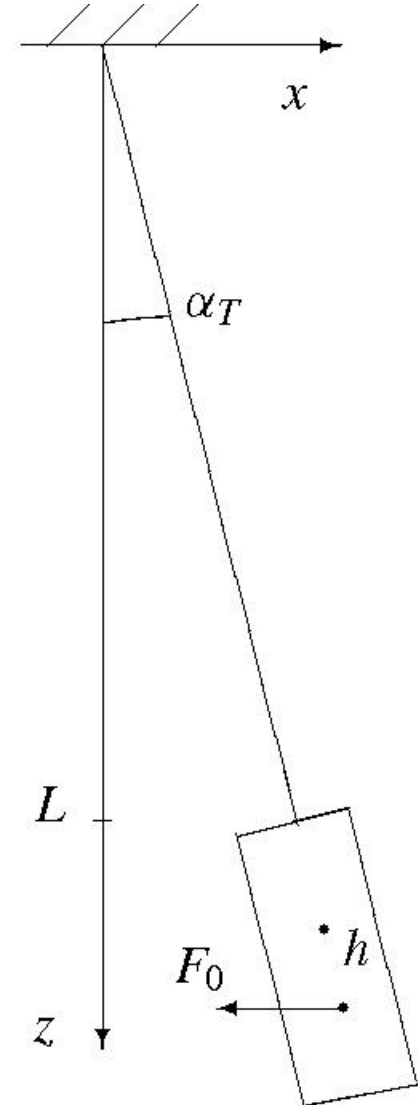
- SRD estimate assumed a viscously damped harmonic oscillator: $x(f) \propto f^{-2}$.
- We know now that its due to internal friction of the steel wire: $x(f) \propto f^{-5/2}$.
- 'Low' loss steel music wire:
 $\phi_{\text{wire}} \sim 5 \times 10^{-4} - 1.3 \times 10^{-3}$

Suspension Thermal Noise II

Finding the Sweet Spot

- Pitch & Piston thermal noise are correlated.
- Both caused by thermal forces generated where the wire bends.
- Calculate both, move the beam, minimize the readout noise.
- Reduces coupling from bottom part of the wire *at some frequencies*.
- $d \sim 1 \text{ cm}$
- $x_{\text{sus}}(f)$ reduced by $\sim 20\%$

Braginsky, Levin, Vyatchanin (1999)
Gonzalez (2000)

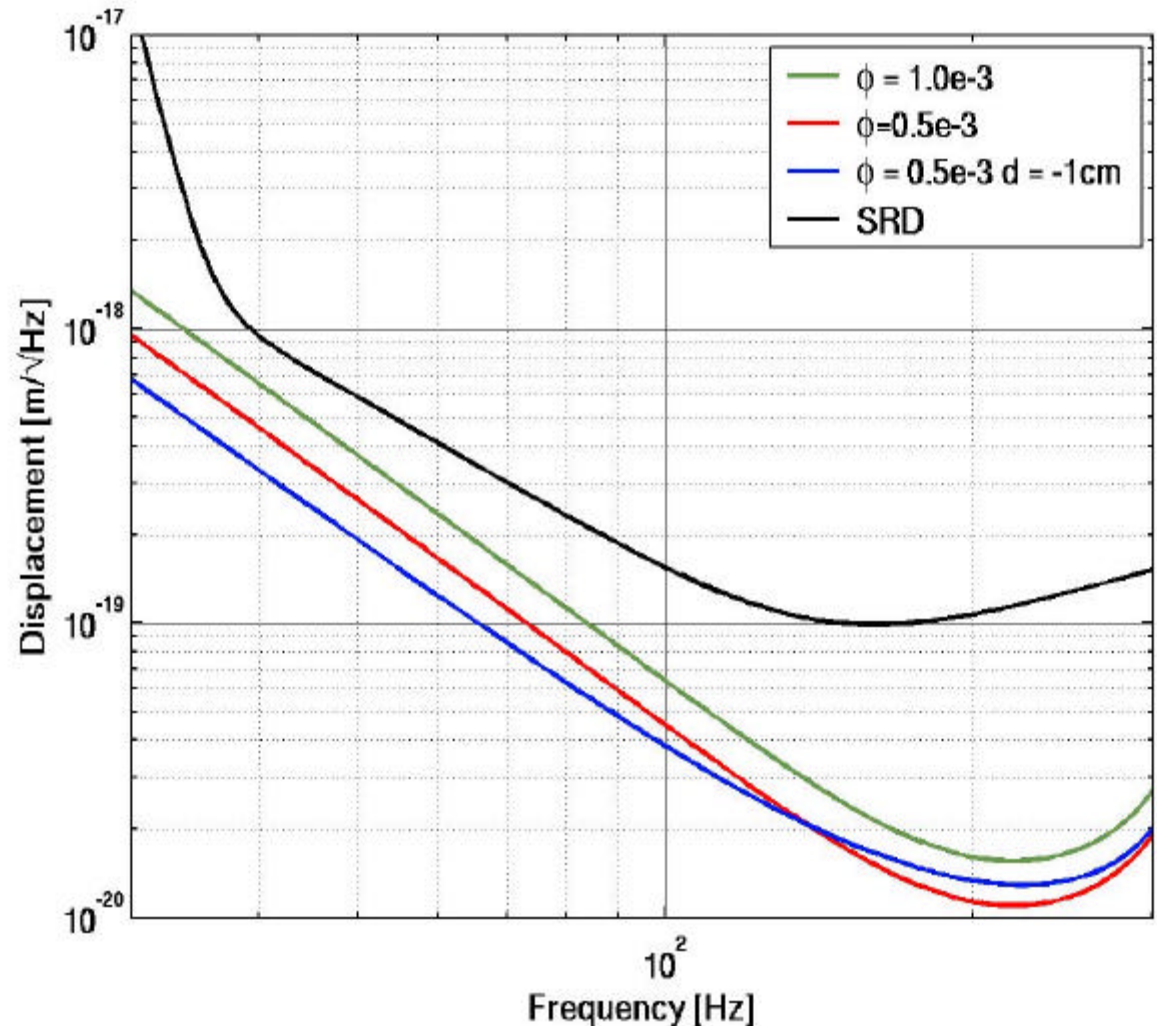




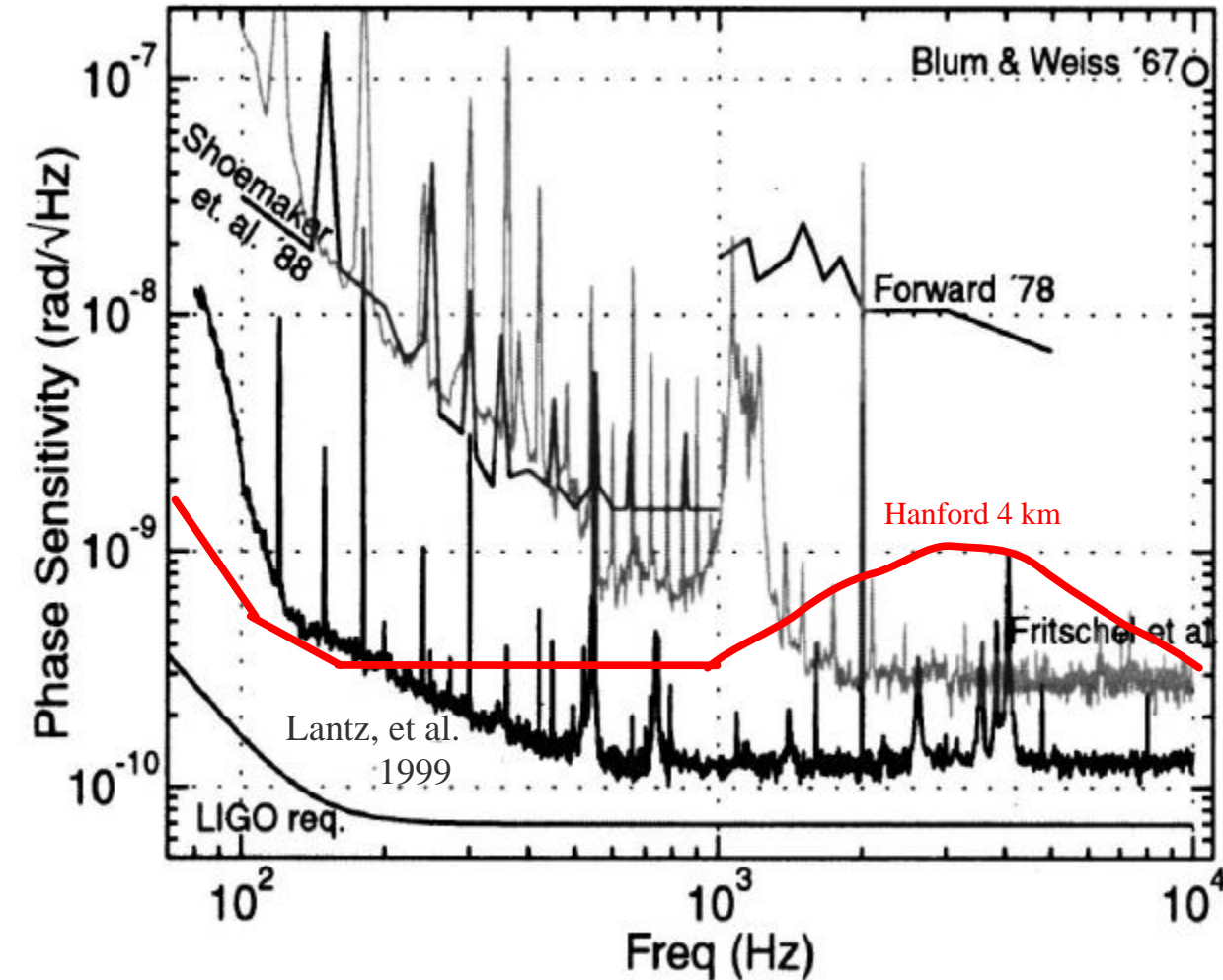
Measurements:

Suspension Thermal Noise I

- ➔ Assumes NO loss except for the internal wire friction:
Good clamps, no rubbing.
Not yet verified.
- ➔ High upper limit of 1.3×10^{-3} set by measuring in lock linewidth of violin modes.
- ➔ Linewidths limited by temperature drift of ~ 1 deg.
- ➔ Violin mode ringdown measurements take minutes, not hours.
- ➔ *Need to remove systematics:*
amplitude dependence, servo feedback.
- ➔ **May turn out to be $\sim 3\text{-}4\times$ less than SRD.**



Shot Noise



- Gaussian, white noise in the detected photocurrent from the random photon arrival rate.
- By using high power in the IFO we get a large optical phase gain: **many Watts/Radian**
- But we need to reduce the **spurious light** which makes shot noise but doesn't help the signal strength.
- **SRD curve makes some assumptions about both:**
- **Laser Power** x **Buildup**
- **Spurious light due to imperfect dark fringe.**



Why is the sensitivity (above 100 Hz) not better?

- ? **Low Optical Gain:** Low laser power, low sideband transmission, and poor overlap.
- ? **The noise is too high:** The Dark port is not dark. The mismatched SB and the mismatched carrier make shot noise.

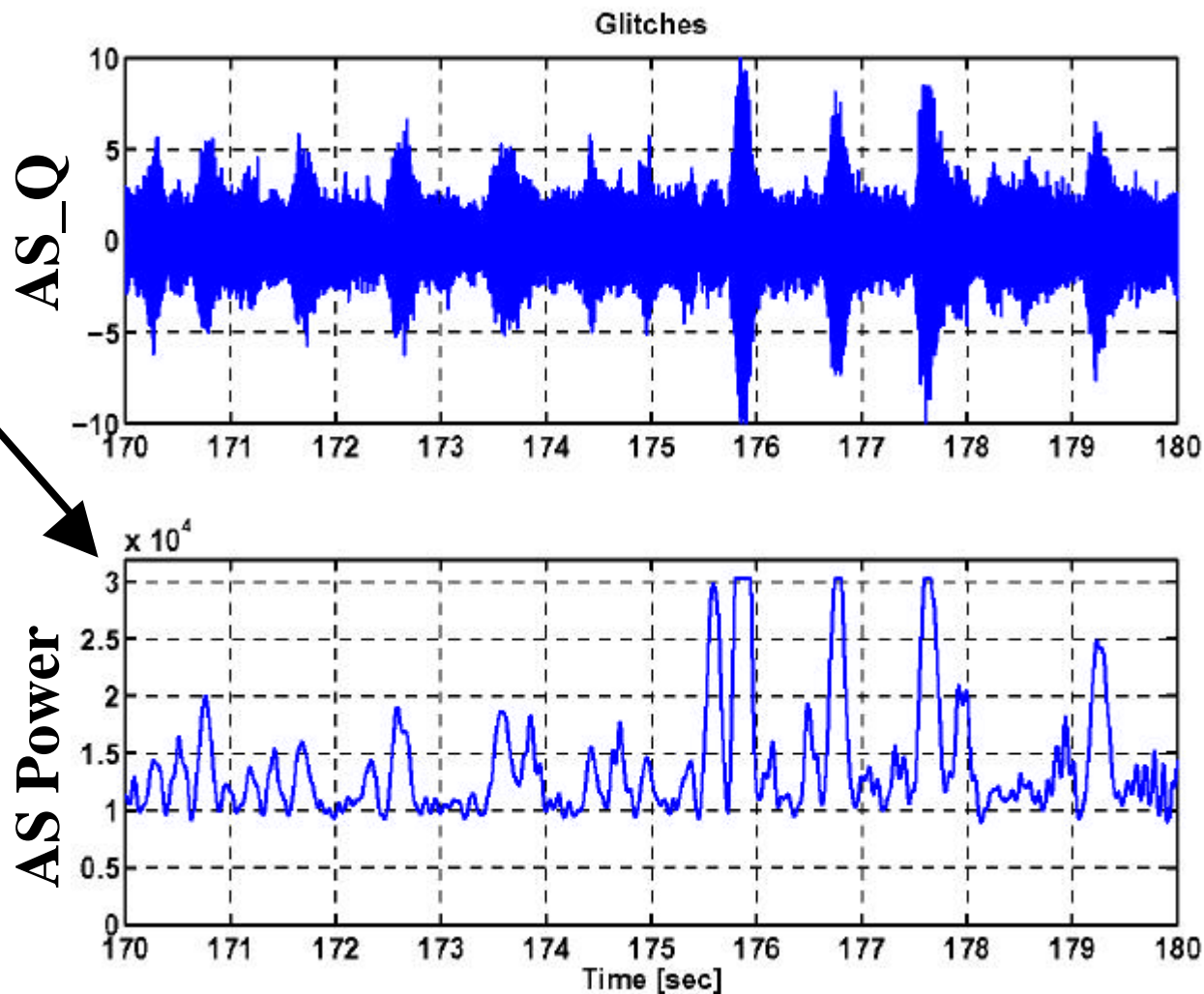


Measurements: Shot Noise

Angular fluctuations can cause large power fluctuations.

Must reduce this:

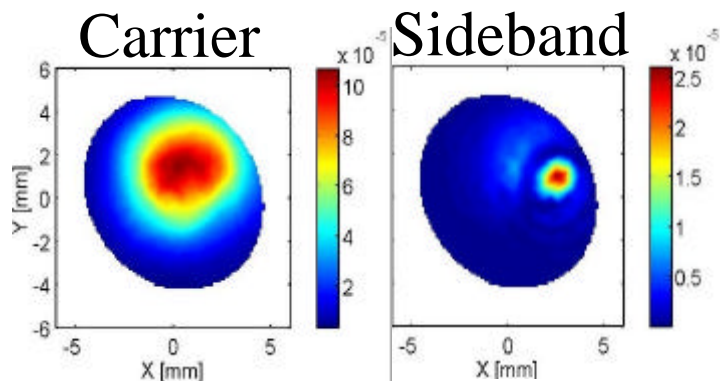
- Better angular controls
- Seismic isolation (HEPI)
- Output mode cleaner





Shot Noise

Thermal Lensing:



Poor overlap in Cold IFO

- ➔ Measured power gains ($\sim 45-50$) are higher than the design (30). Limited by the excess scatter loss on the test masses (~ 70 ppm/mirror).
- ➔ Measured contrasts (L1 = 30 ppm, H1 = 700 ppm) better than SRD (3000 ppm).
- ➔ New output mode cleaner will remove all higher order contrast defects.
- ➔ Residual contrast defect will be TEM_{00} defect (6 ppm) due to loss imbalance (L1 ~ 70 ppm, H1 ~ 35 ppm).
- ➔ RF modulation depth then lowered to optimize SNR. Goes to ~ 0.15 radians from ~ 0.45 radians (design)
- ➔ Assumes 100% sideband transmission to AS port. Original requirement is $> 75\%$.
- ➔ Means perfect thermal compensation (TCS) and all SB power in TEM_{00} mode.
- ➔ 'Hot' off the press: H1 SB transmission $\sim 87\%$

example image
of hot PRM
goes here

Good overlap in Hot IFO

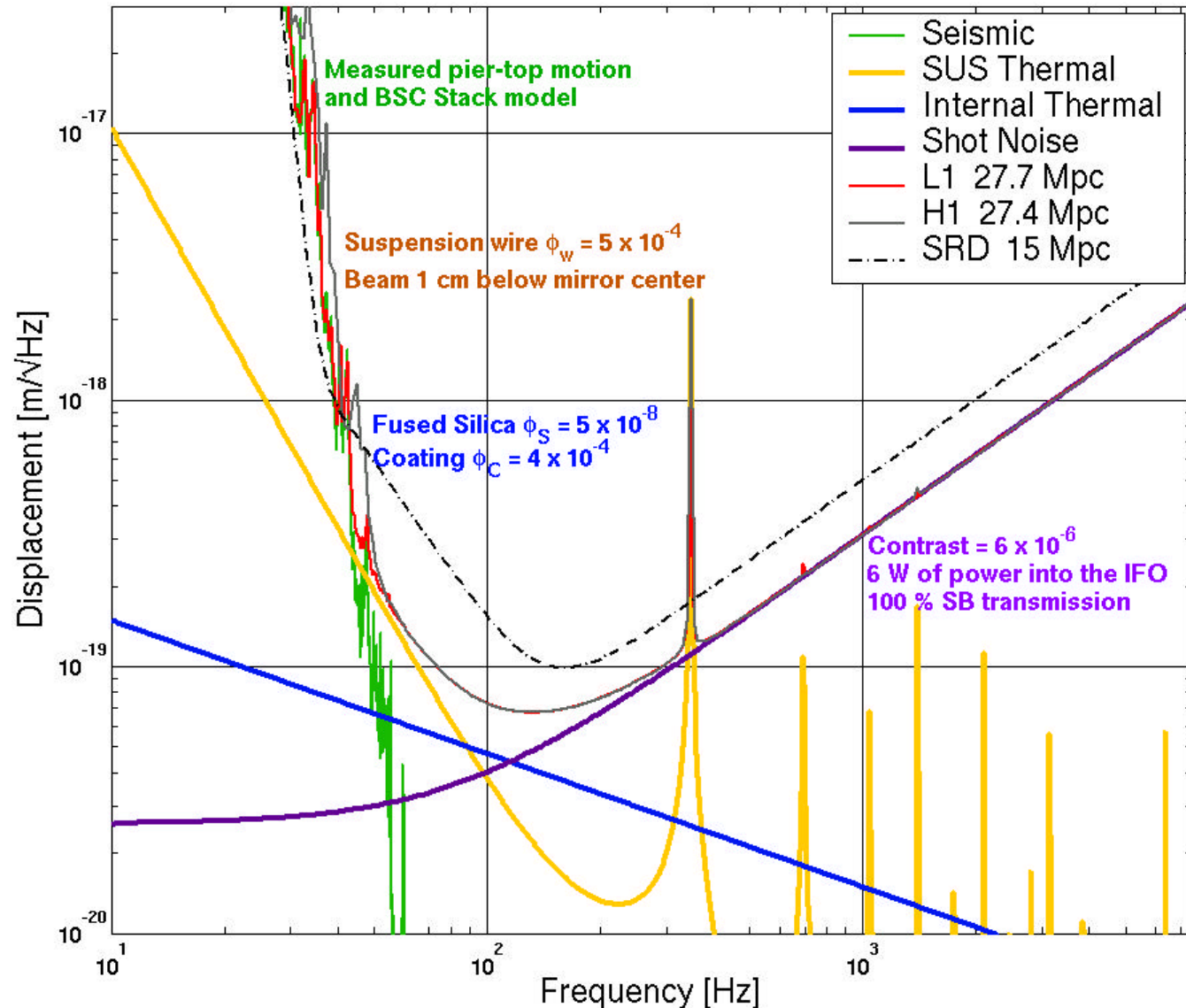
The TCS is doing a fairly good job of correcting the phase front curvature error in the PRM.

- Daniel Sigg, Hanford elog Feb 27th, 2004



The Noise Spectrum

- ➔ Identical Thermal Noise assumed for both IFOs
- ➔ Slightly more seismic noise in Hanford than in Livingston !
- ➔ Nice improvement in NS/NS Inspiral Range.
- ➔ S4? S5?





Summary

- * *What is the noise in the interferometers now?*
 - **Mostly known. Not unfixable.**
- * *Where does the SRD Curve come from?*
 - **Conservative estimates that look pretty close.**
- * *What do we know about the 'fundamental' noises?*
 - **The Seismic may be a little high, the others look good.**
- * *Can we ever reach the SRD ?*
 - **Yes, but that's easy.**
- * *What do we do about it?*
 - **Continue as planned, re-evaluate technical sources**

+ next page...



Near Term Measurements: Characterize Thermal Noise

- ➔ Continue **internal mode Q measurements** on all 3 IFOs to get better handle on losses. So far only a few optics have gotten several Q's measured. Also, no substantial Q measurements on Super Polished ETMs (L1 & H2) .
- ➔ Even worse situation on Suspension thermal noise. Need to **measure the first 3 harmonics of the violin modes** on *every* test mass. Needs to be done at low amplitudes and with no servo feedback.
- ➔ Maybe look for anharmonicity in the violin modes to establish that its internal friction.



Near Term Noise Reduction: Optical Phase Noise

- Thermal Compensation
- **Apply heat** to make $T_{SB} > 75\%$
- **Tweak up lasers** for $> 8W$ into the MC
- REFL signal goes down with heat: Implement NRSB scheme to increase phase sensitivity at REFL port. Reduces frequency noise.
- POB SNR goes like $\sim P_{in} * (G_{SB})^2$:
- \rightarrow 20x reduction of POB noise.



Near Term Noise Reduction: Oscillator Phase Noise

- Oscillator noise is OK: 4×10^{-7} rad/rHz
- Coupling is ~**100X** higher than design.
- LO & RF SB follow *different* paths.
- Custom low noise OCXO: 1×10^{-8} rad/rHz
- LO filter to symmetrize the RF paths.



Big Payoff !

100 X more mass
for a small noise reduction

