

LIGO-Quiet Hydraulics 101

LIGO Livingston Observatory

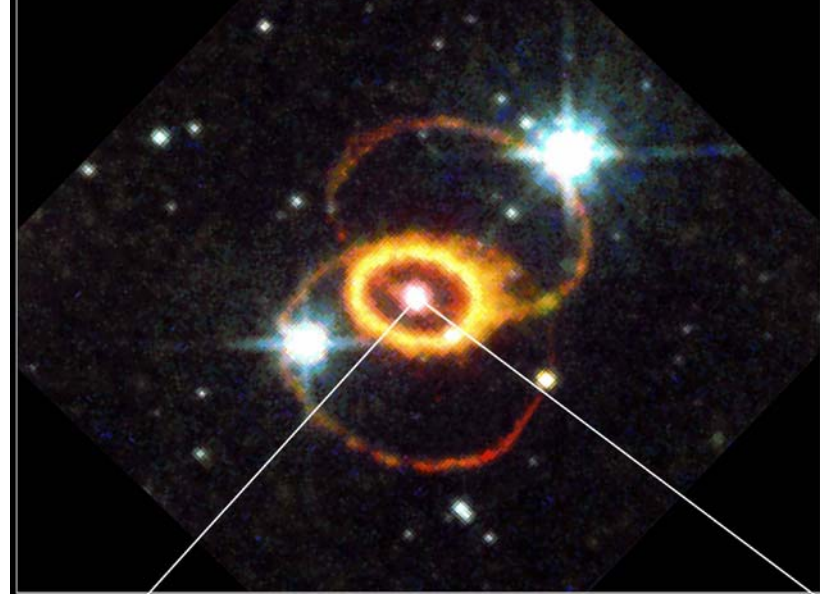
March 5 2004

Dan DeBra, Brian Lantz, Corwin Hardham

Originally prepared for the
Quiet Hydraulics Consultancy Board
Rich Duder, Stephen Osder

LIGO

a new window on the universe



Feb. '94

Sept '94

Mar. '95

Feb '96

Supernova 1987A Explosion Debris
Hubble Space Telescope • WFPC2

PRC97-03 • ST ScI OPO • January 14, 1997 • J. Pun (NASA/GSFC), R. Kirshner (Harvard-Smithsonian CfA) and NASA

Gravitational waves are difficult to detect.

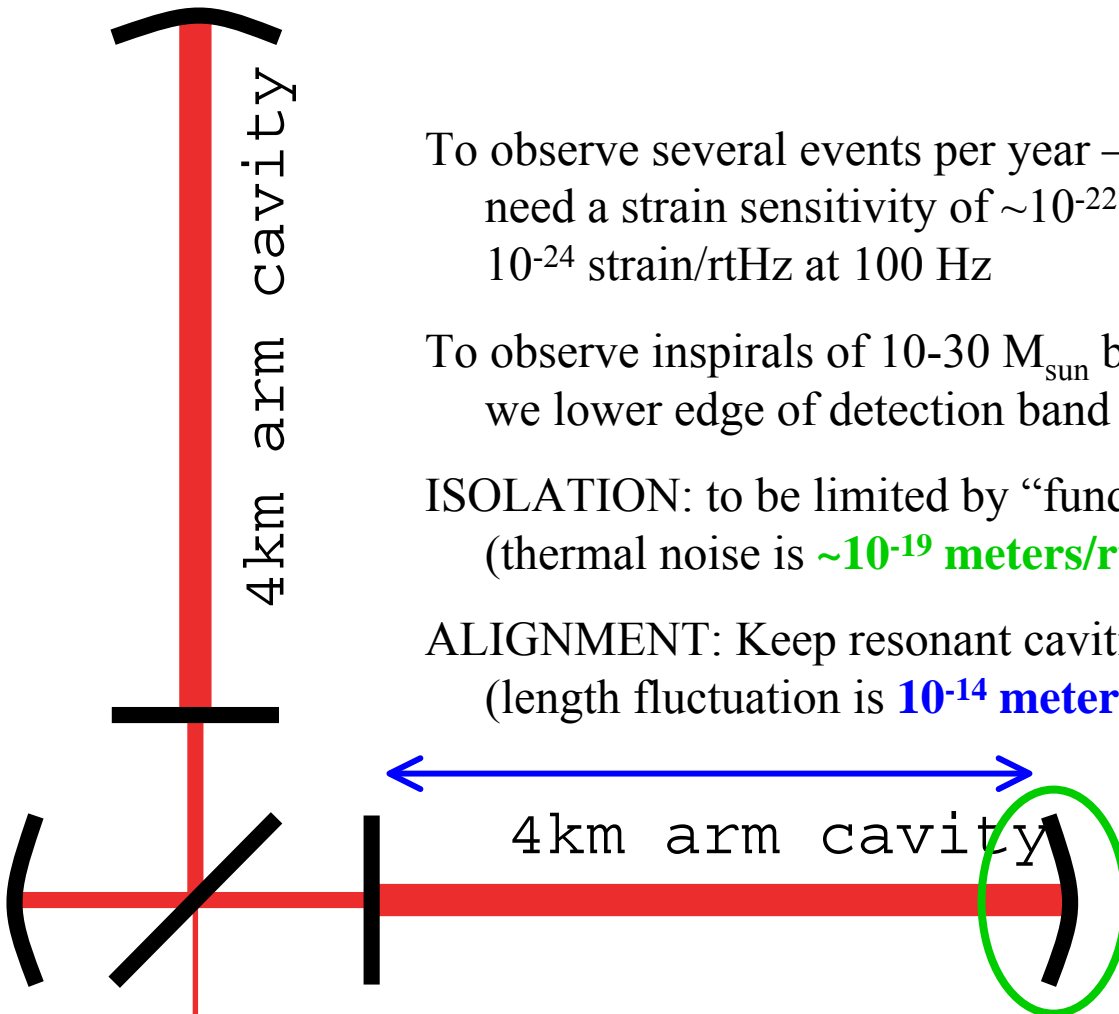
Advanced LIGO specs

To observe several events per year –
need a strain sensitivity of $\sim 10^{-22}$ rms around 100 Hz
 10^{-24} strain/rtHz at 100 Hz

To observe inspirals of $10\text{-}30 M_{\text{sun}}$ black holes
we lower edge of detection band to 10 Hz

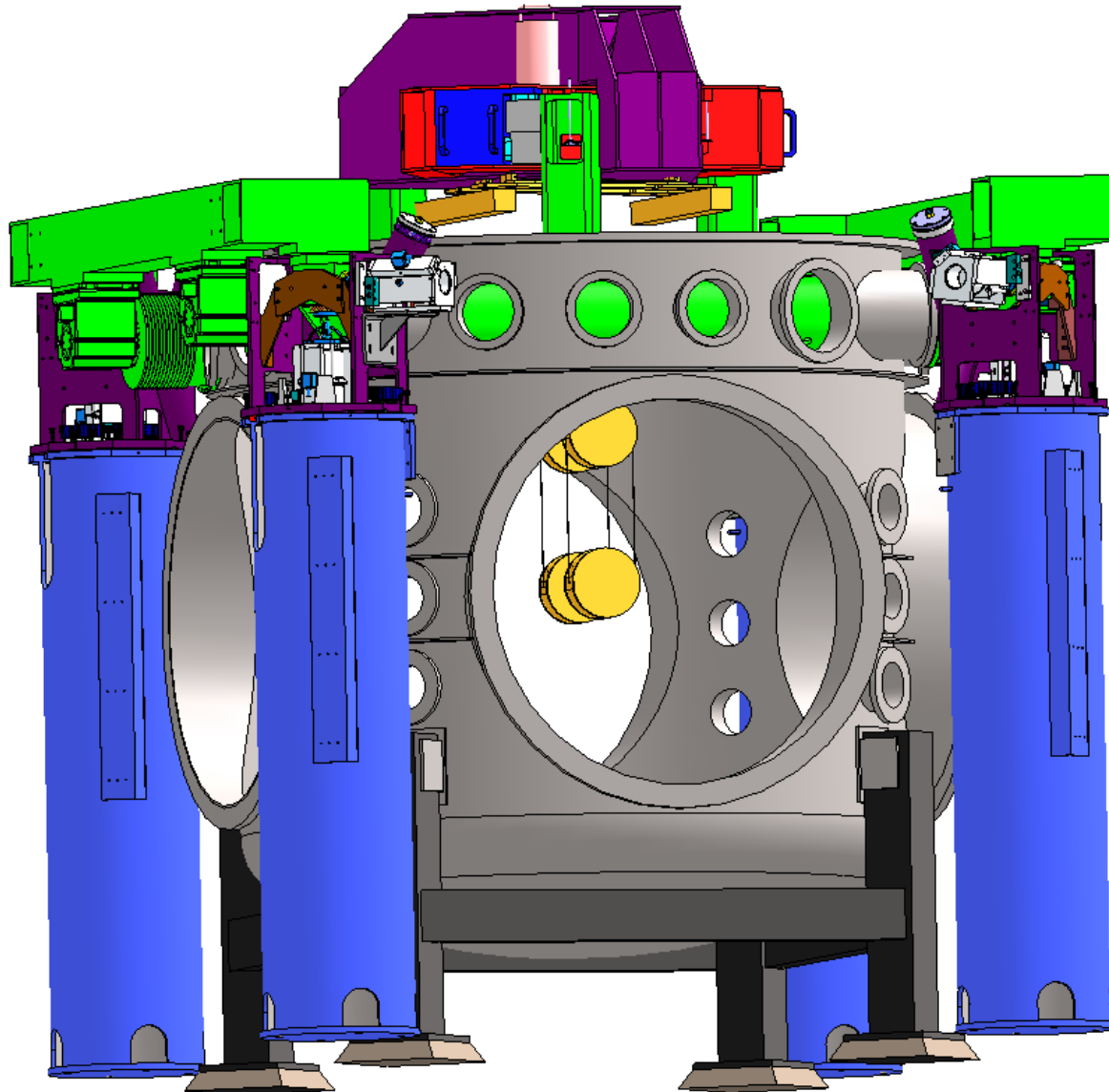
ISOLATION: to be limited by “fundamental” processes
(thermal noise is $\sim 10^{-19}$ meters/rtHz at 10 Hz)

ALIGNMENT: Keep resonant cavities at operating point
(length fluctuation is 10^{-14} meters rms)



G040462-00-R

Advanced LIGO Seismic Isolation and Alignment System



G040462-00-R

Motivation for an External Stage

- Isolation
 - From the micro-seismic peak to 10 Hz
- Alignment
 - Seasonal Temperature Changes, Tides
- Control Reallocation
 - Reduce control effort / noise from inner stages
- High Impedance Support
 - Inner stages react against stiff, damped foundation

Today - My Purpose

A more detailed understanding of how the hydraulic system works

A bit of the history

Some perspective on how Stanford thinks about the system.

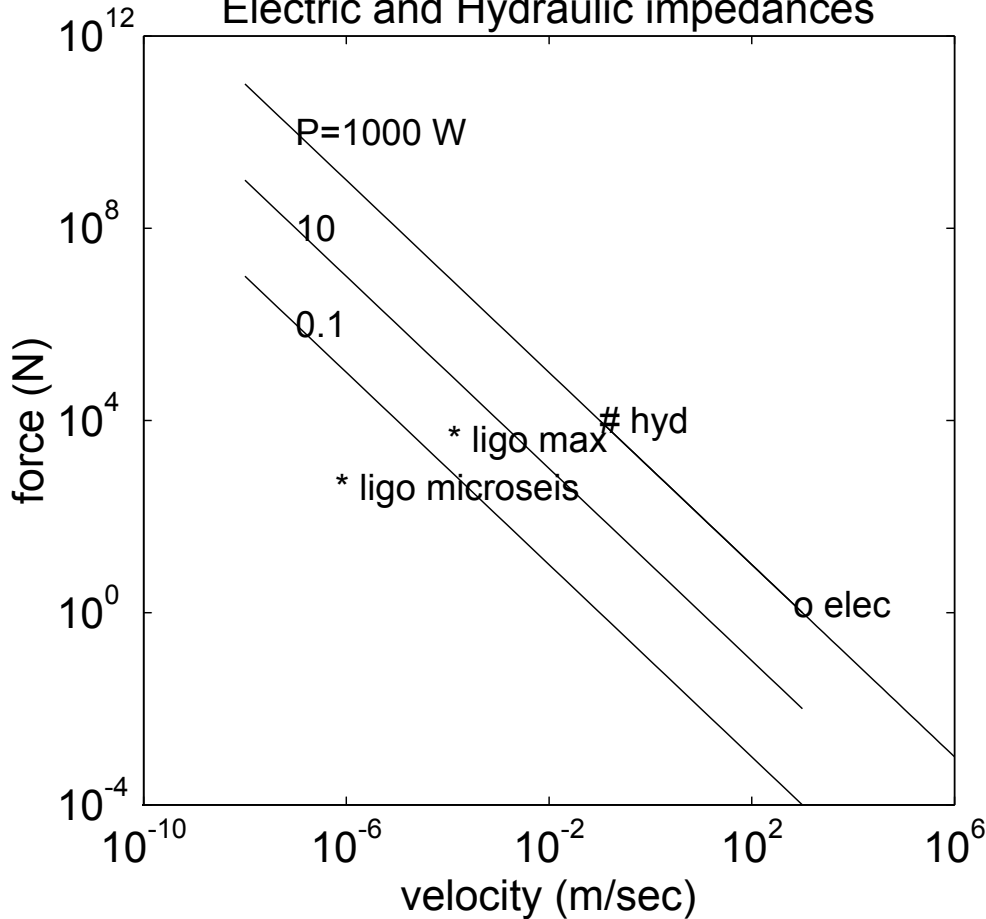
Three cool facts

Performance Requirements

- Range of Motion
 - Mechanical Adjustment: 5 mm
 - Active Control: +/- 1 mm
- Response
 - Initial Response: 1 mm in 12 sec (80 μ /sec)
 - Bandwidth: 0.1 - 10 Hz
- Resolution and Noise
 - Reduce the ground motion by 15 from 0.1 to 3 Hz

Actuators

Ligo Requirements and Electric and Hydraulic impedances



Outer Stage

Laminar Flow Hydraulic

- Well matched to requirement
- easily maintains large offsets
- stiff and well damped

Inner Stages

Electromagnetic

- quiet
- force actuation is independent of position of support
- high bandwidth

Hydraulics is a clear choice for

- Impedance Match
- Inelastic Foundation

Can it provide

- Quiet Actuation (No Stiction)
- Quiet Control (No Turbulence)

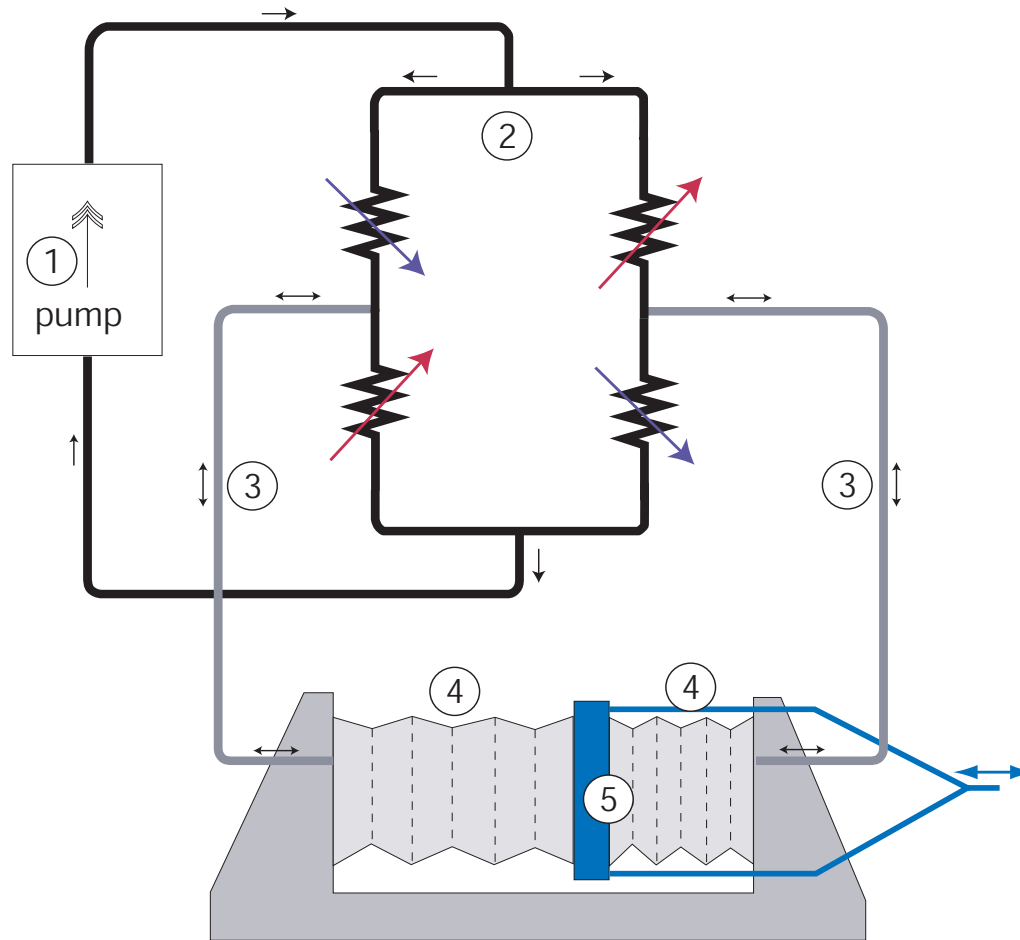
Smooth actuation:

- Elastic Actuator-Bellows, or
- Dynamic Seals (Open system unacceptable)

Quiet operation

- Laminar Flow, and
- Power supply isolation

Quiet-Hydraulic Actuation



History of Valve Development

1. Oostman design for QH machine tools
2. HSC design
3. HSC with modified nozzles
4. Dynamic Valve to the rescue
5. Current design, Valve insert and its role
6. Performance
 1. Freedom from turbulent disturbances
 2. Linearity
 3. Calibration Techniques
 4. Procurement and roles and responsibilities

History of Bellows Actuator

- 1 dof device. Kinematics of elastic decoupling
- Conflict in design: range of motion vs ‘hydraulic’ resonance
- Design principle: don’t depend on control for damping:KIS

Hydraulic resonance damper

- Material and fabrication history
- Leakage and contamination are a design drivers

No threaded joints, all o-ring seals

Weldments where possible

Power Supply Design

- Commercial components except LFR
- LFR (Laminar Flow Resistors)...free of turbulence
- Heat exchanger is the distribution plumbing

End Stations are air-conditioned (a/c)

- Pumps are isolated on pad with a/c machinery
- Fluid choice
 1. High viscosity, $\mu=0.086$ Pa-sec
 2. No mineral oil (optical sensitivity)
 3. Compatible with COTS pumps & components

Schedule

- Introduction
- Motivation and Specs
- The Valve
- The Actuator and Control
- Power Supply

Outline

Description of our requirements for isolation and alignment
Advanced LIGO and Livingston retrofit

Valves

Basic function

laminar flow math

linearization of the control

Distribution System

Parts

Controlling Pump Noise

Controlling Cross-regulation Noise

Advanced LIGO specs

Isolation

ground motion at 10 Hz: $\sim 3 \cdot 10^{-10}$ m/rtHz

requirement at 10 Hz: 10^{-19} m/rtHz

difference is $9\frac{1}{2}$ orders of magnitude

Alignment

microseism at .16 Hz: a few 10^{-6} m

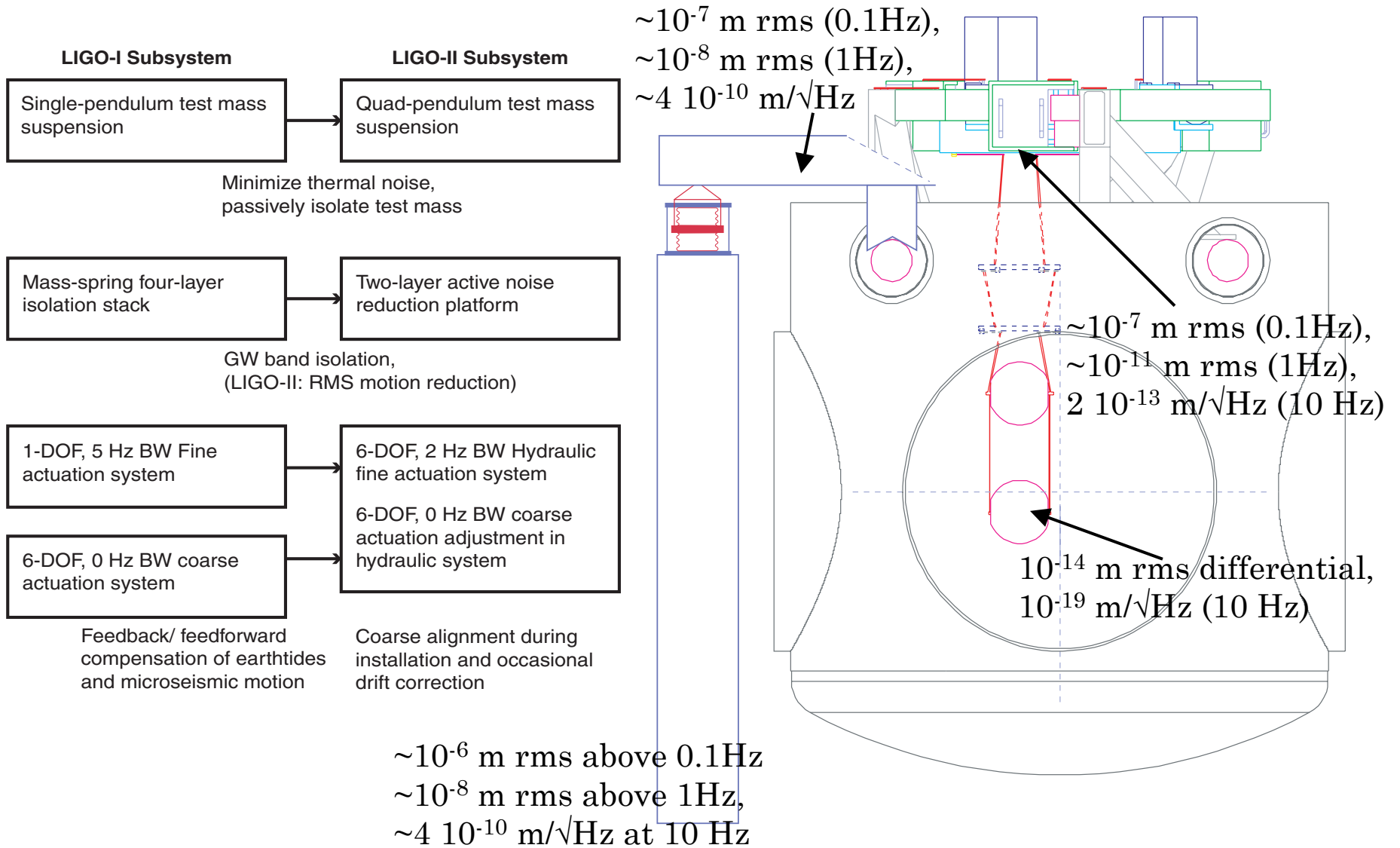
tides: +/- 150 μ m

we'd like (seasons, etc): +/- 1 mm

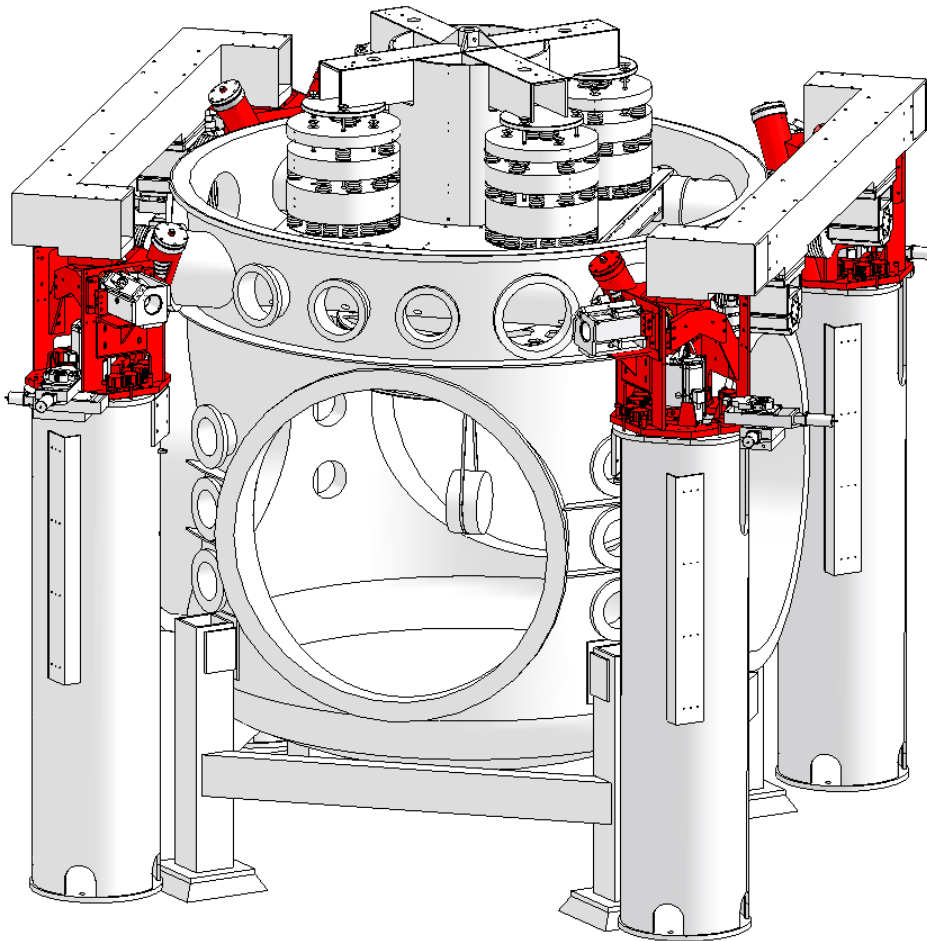
requirement: 10^{-14} m rms

difference is 8 - 11 orders of magnitude

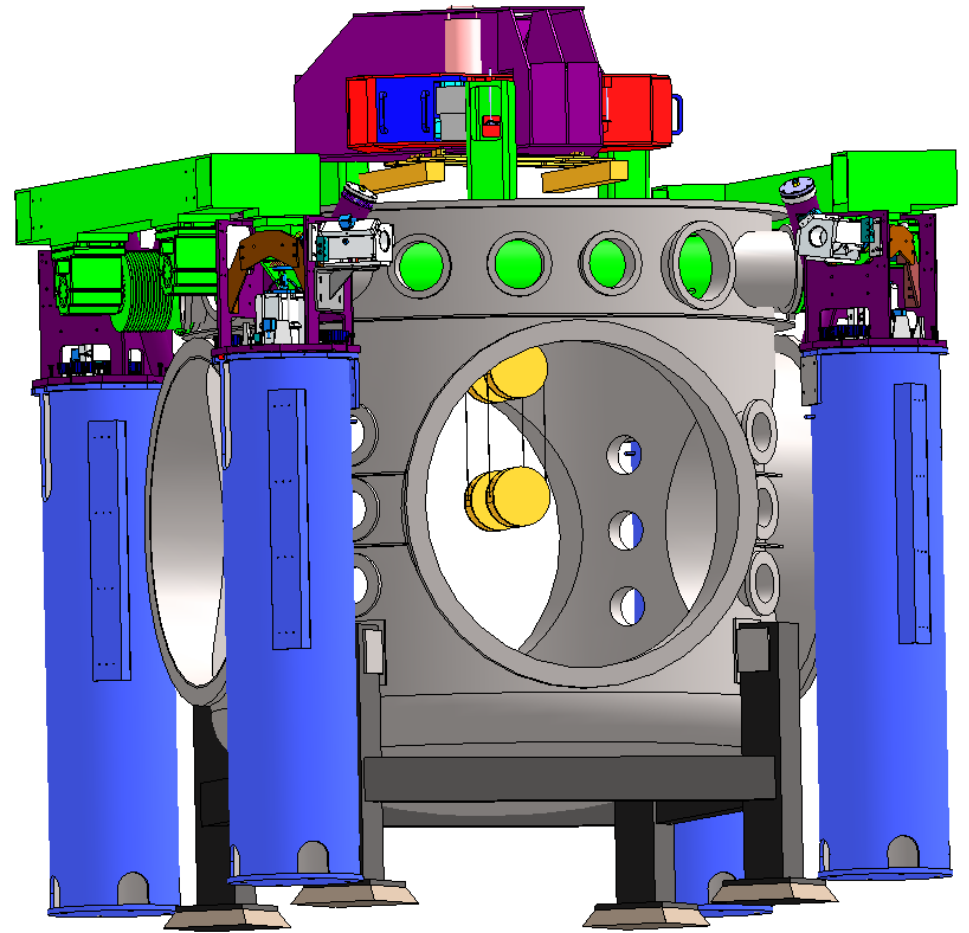
Seven Layers of Isolation and Alignment



Isolation and Alignment Systems



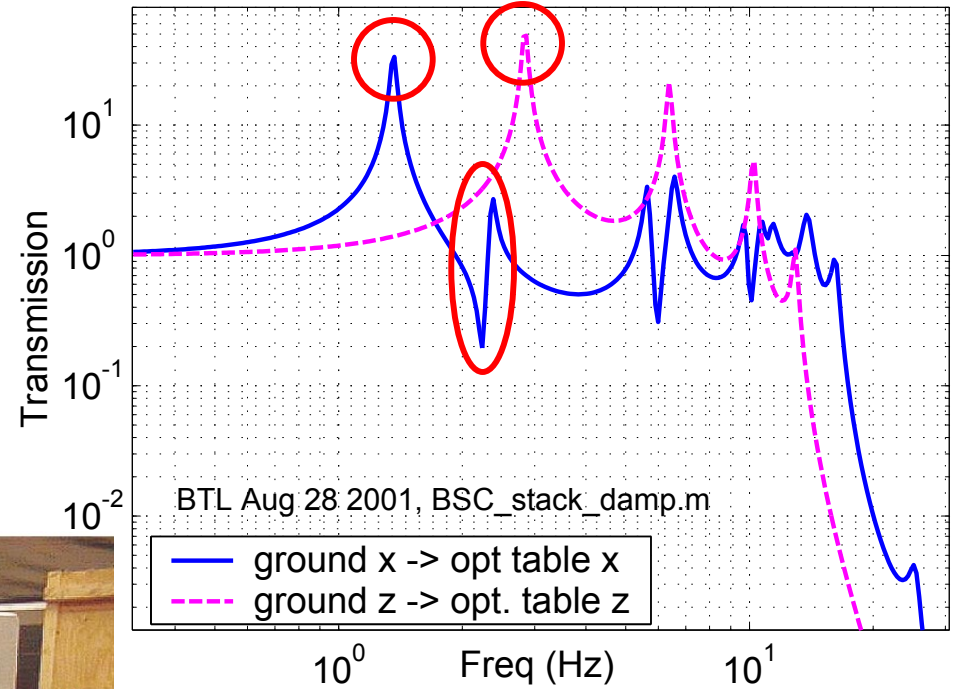
Initial LIGO



Advanced LIGO

Problem with Existing System

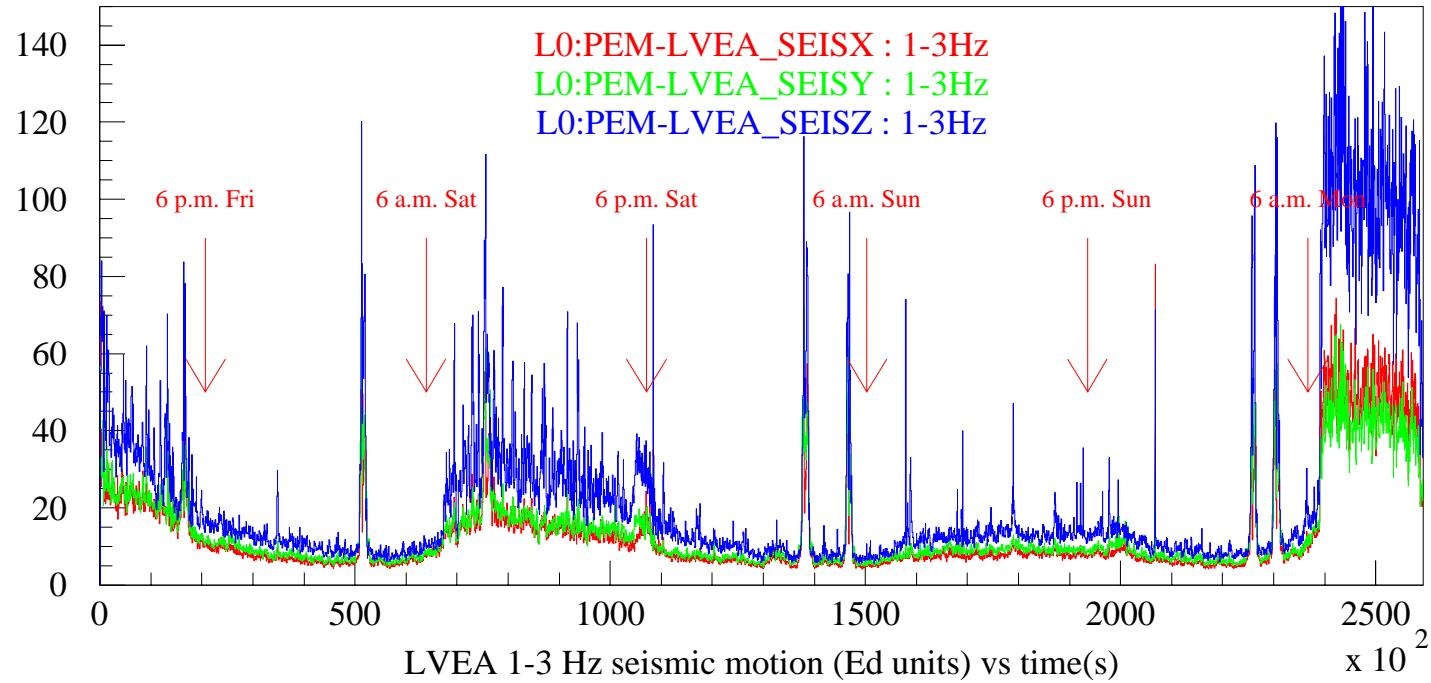
Transfer function of the constant damping Hytec BSC-SEI model (stack+su



Picture courtesy of Eric Ponslet, Hytec Inc.

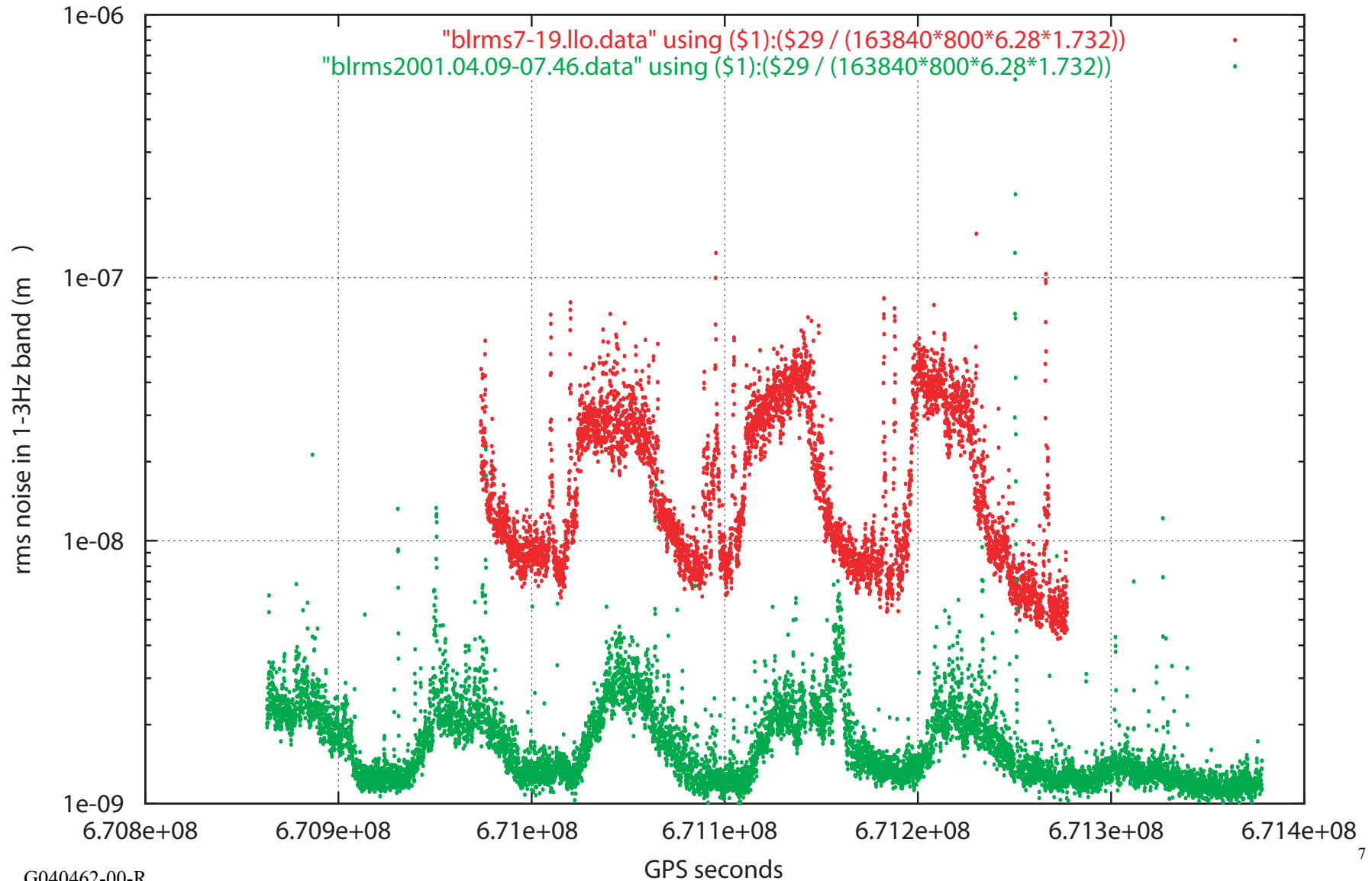
Monday Morning

72 hours of E4 from GPS = 673636586 (Fri May 11, 12:16 p.m. CDT)



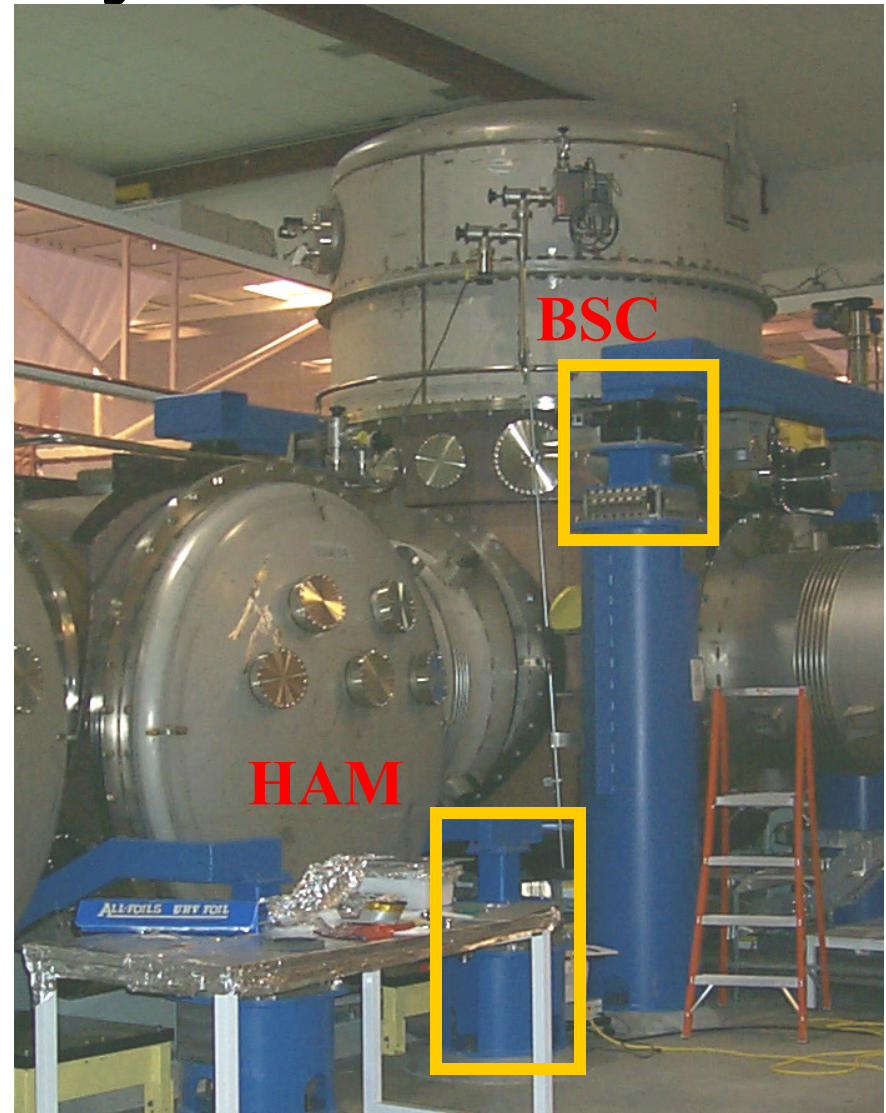
and the Rest of the Time...

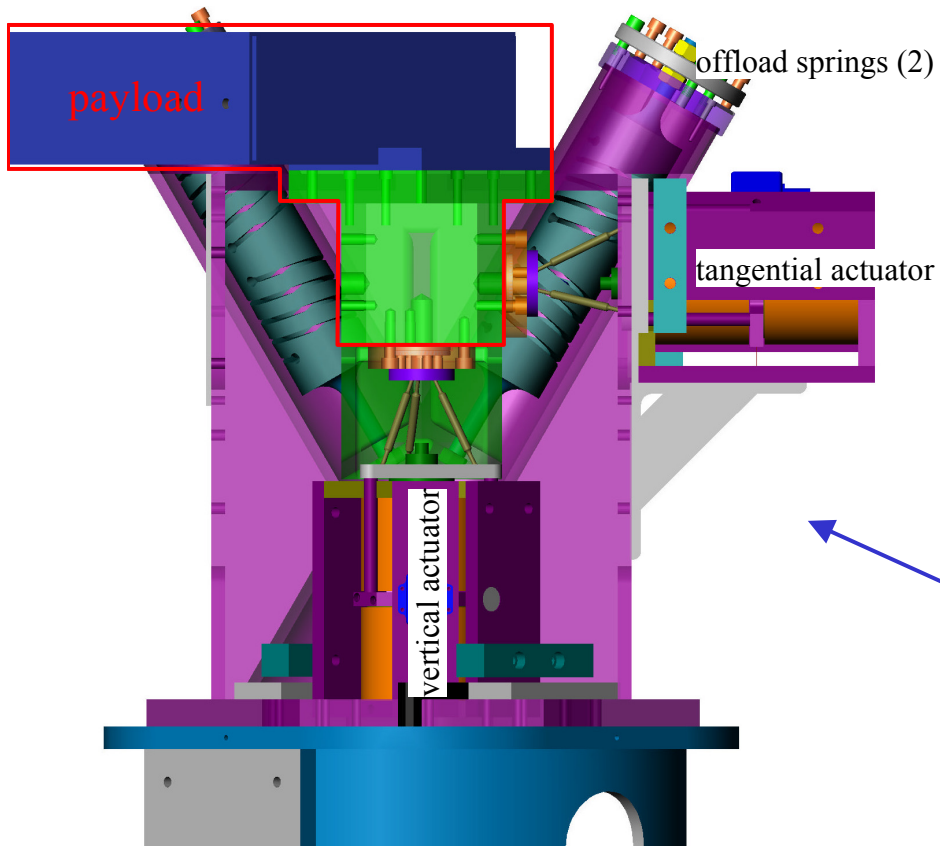
red=livingston, green=hanford



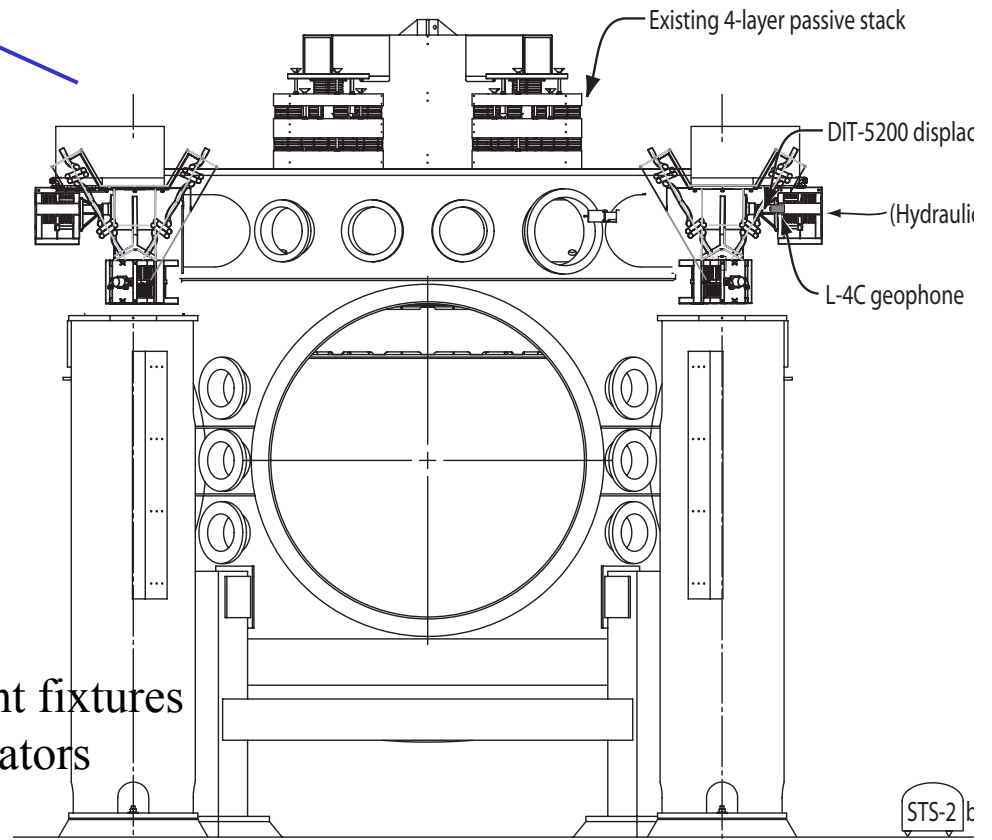
Placement of an External Isolation System

- Install an isolation and alignment system without opening the chambers.
- Replace the coarse and fine actuators which are currently between the pier and the cross beam weldment (which hold the support tubes and support table)
- New system will act to hold support table still in the presence of ground motion





Placement of the Actuators and Offload Springs



All the pier-top components are mounted into a frame

Frame holds:

1 vertical and 1 tangential actuator,
(isolation and alignment in 6 DOF)

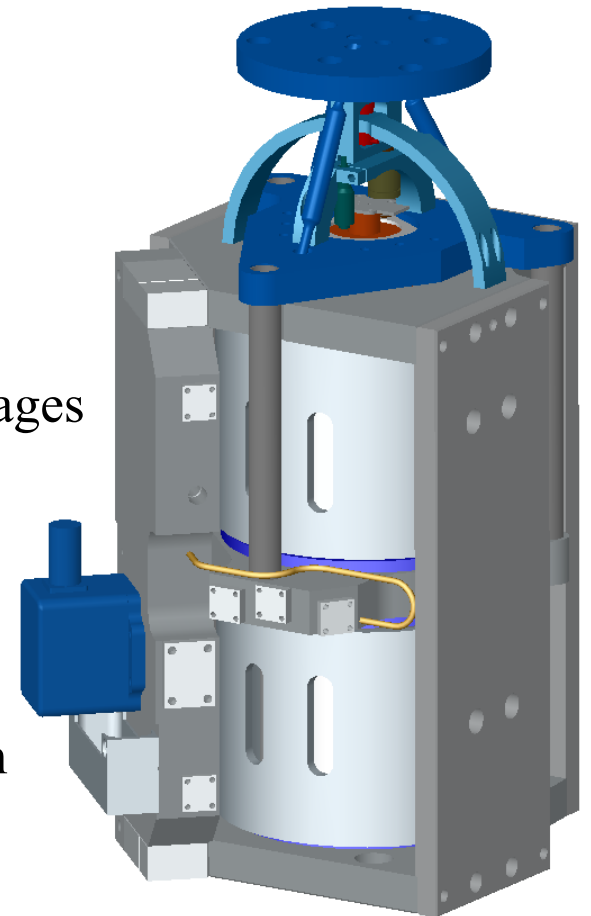
Pair of offload springs and initial alignment fixtures

Sensors which are not included in the actuators

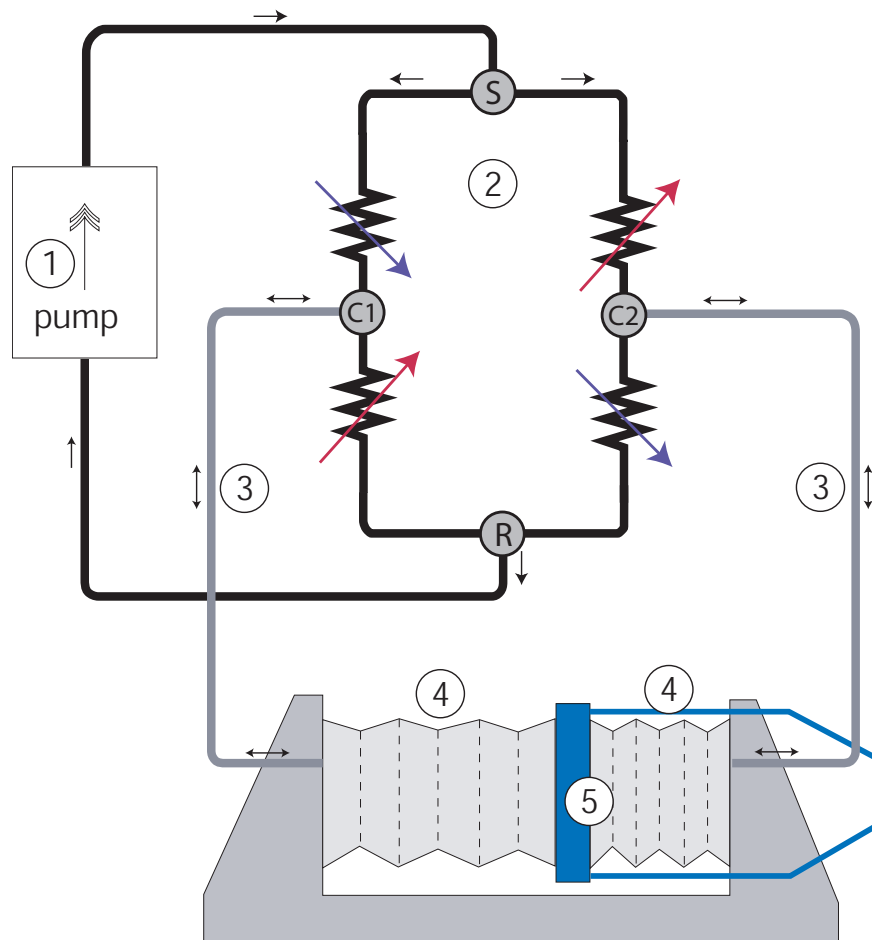
Drawings courtesy of Ken Mason

Motivation for Hydraulic Actuators

- Isolation
 - From the micro-seismic peak to 3 Hz
- Alignment
 - Seasonal Temperature and ground water changes
 - Tidal correction +/- 150 microns ~twice per day
- Control Reallocation (offload authority) from inner stages
 - minimize heat load
 - decrease noise from power supplies
 - maximize available authority
- High Impedance Support
 - Inner stages react against stiff, damped foundation



Hydraulic Actuator Basics



- (1) Pump supplies a constant flow of fluid to the actuator.
- (2) Fluid flows continuously through a hydraulic Wheatstone bridge.
- (3) By controlling the resistance, one generates differential pressure across the bridge, which are connected to
- (4) Differential bellows which act as a stiction-free piston.
- (5) The actuator plate is between the bellows, and is connected to the payload with a flexure stiff in 1 DOF

•Laminar flow

high viscosity (.086 Pa-sec = 86 x water),
 low velocity (80 microns/ sec.),
 fluid path geometry.

•Motion with flexures

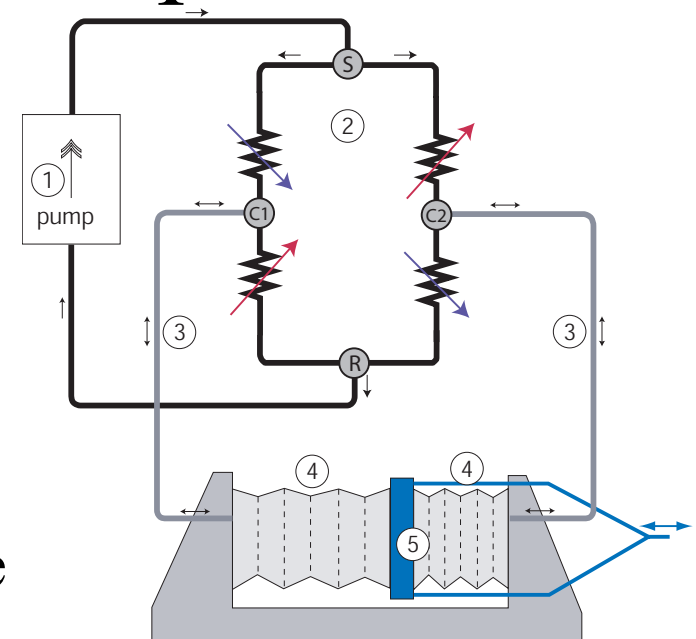
•Offload springs to keep bridge balanced

common mode rejection of pump noise

History of Valve Development

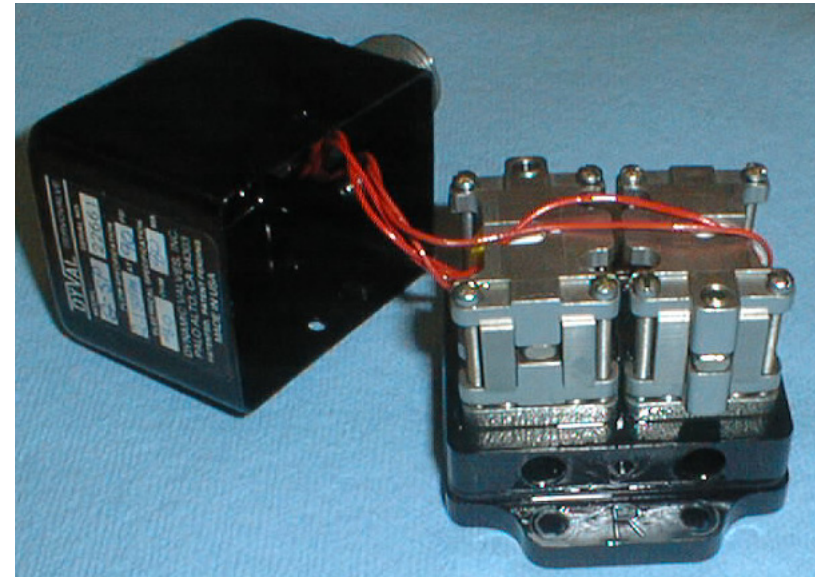
Oostman design for QH machine tools

1. HSC design
2. HSC with modified nozzles
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4. Current design, Valve insert and its role
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 1. Freedom from turbulent disturbances
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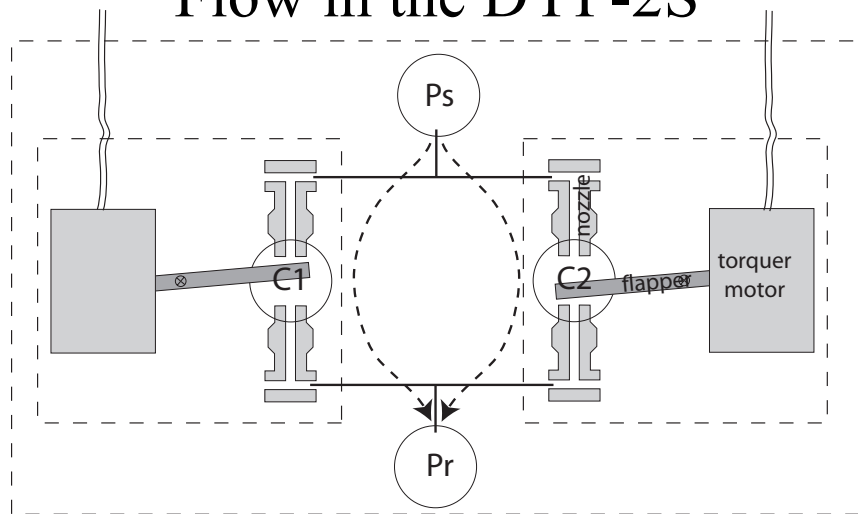
Hydraulic Valve forms the bridge

- Differential bridge in a single valve body
- 4 nozzles – one for each resistor in the bridge
- Original nozzles replaced with custom units shown below right.



Parker DYP-2S valve

Flow in the DYP-2S



DYP-2S valve

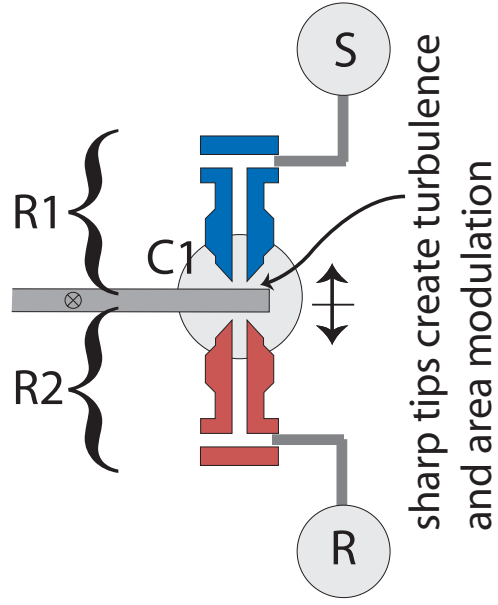
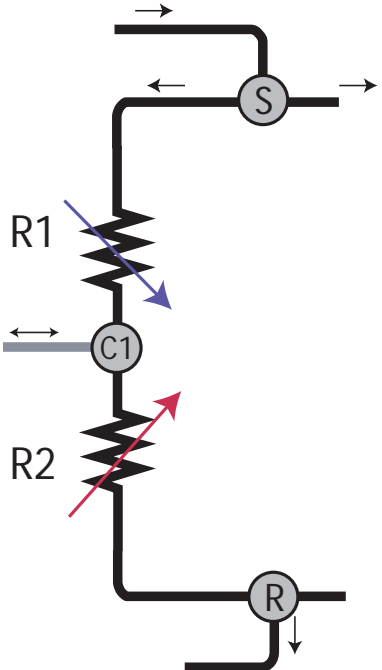
The new nozzle



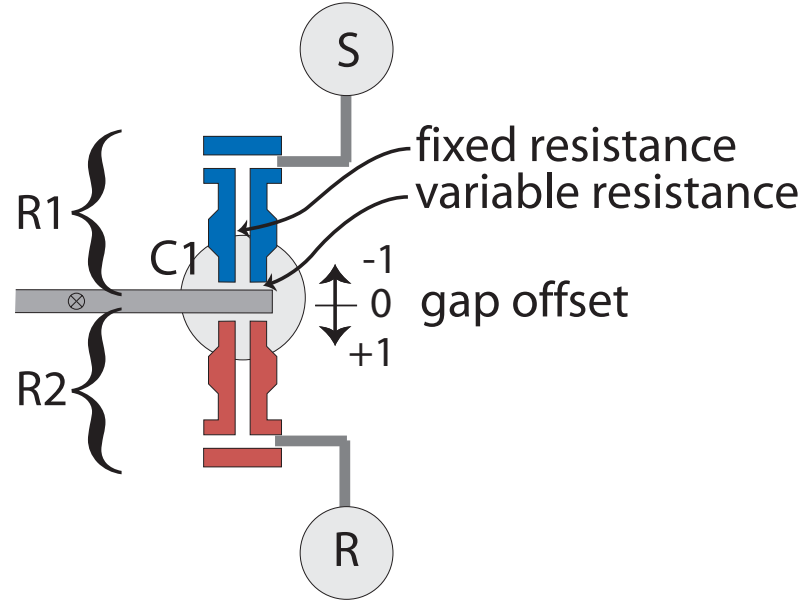
original

new

Nozzles in the Control Valve

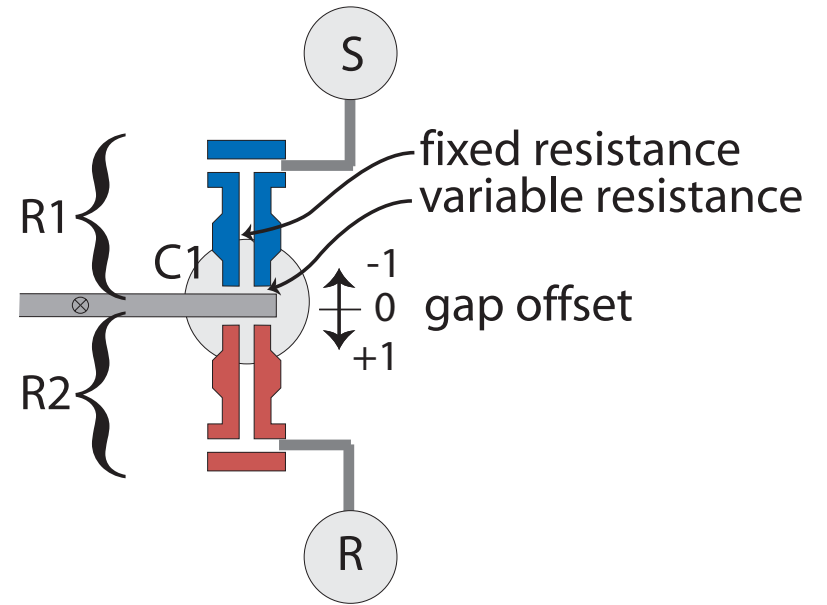
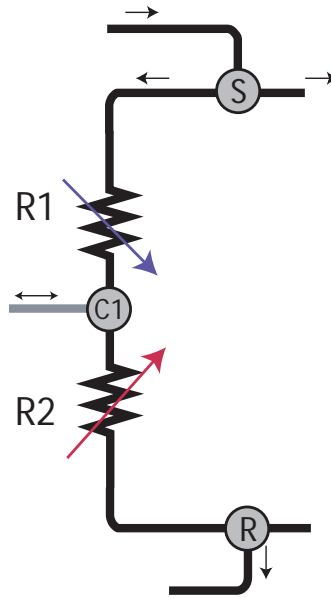


from Parker



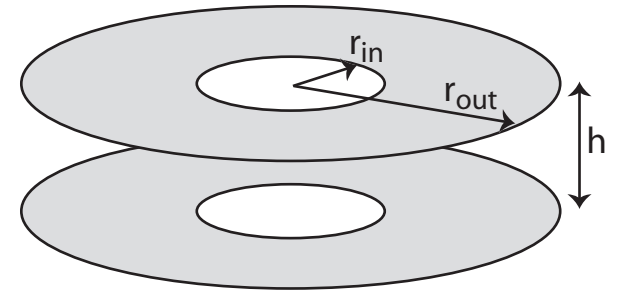
Laminar flow

Nozzle Math



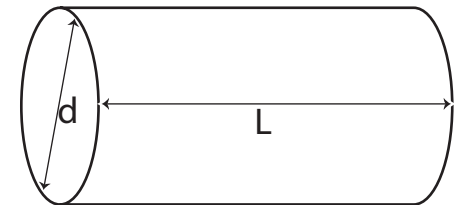
radial flow between
parallel washers

$$R_{washers} = \frac{6\mu}{\pi \cdot h^3} \cdot \ln\left(\frac{r_{outer}}{r_{inner}}\right)$$

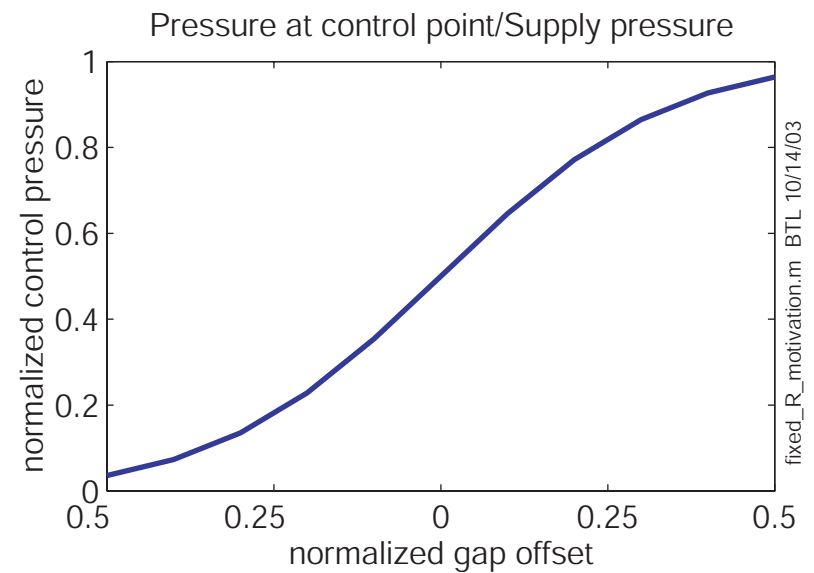
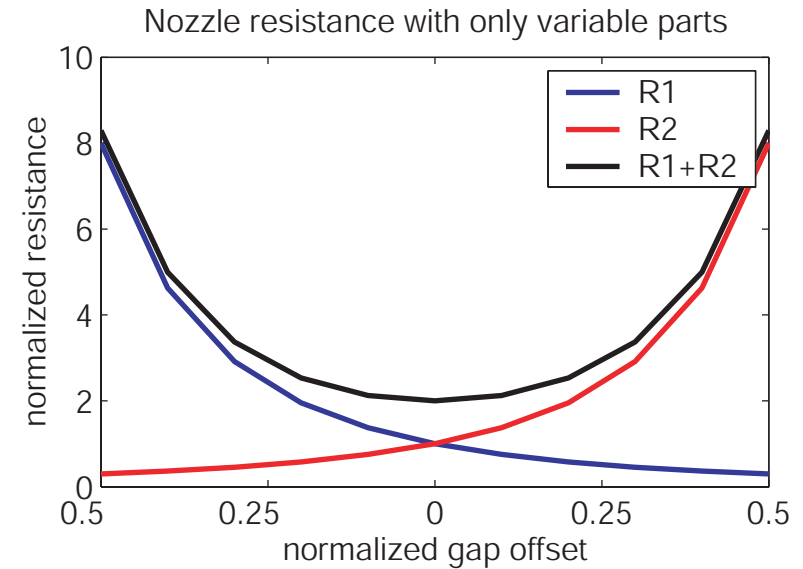
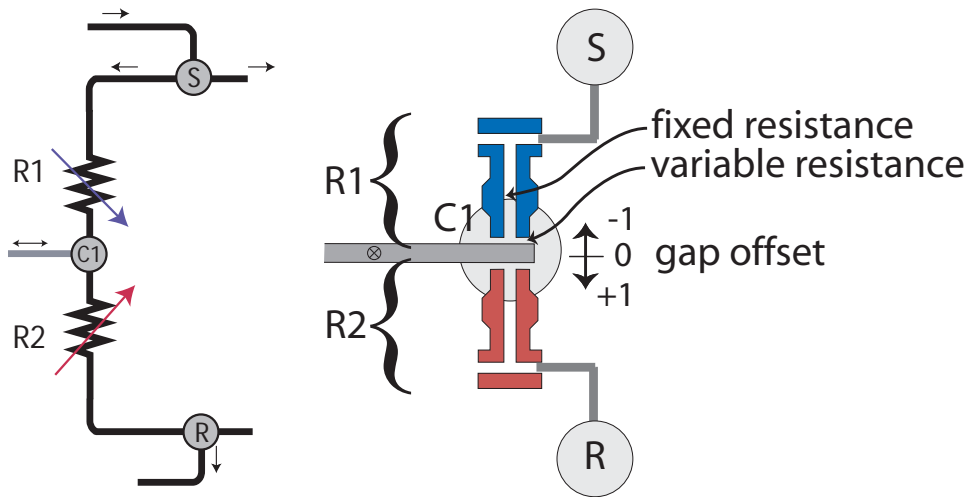


flow along a pipe

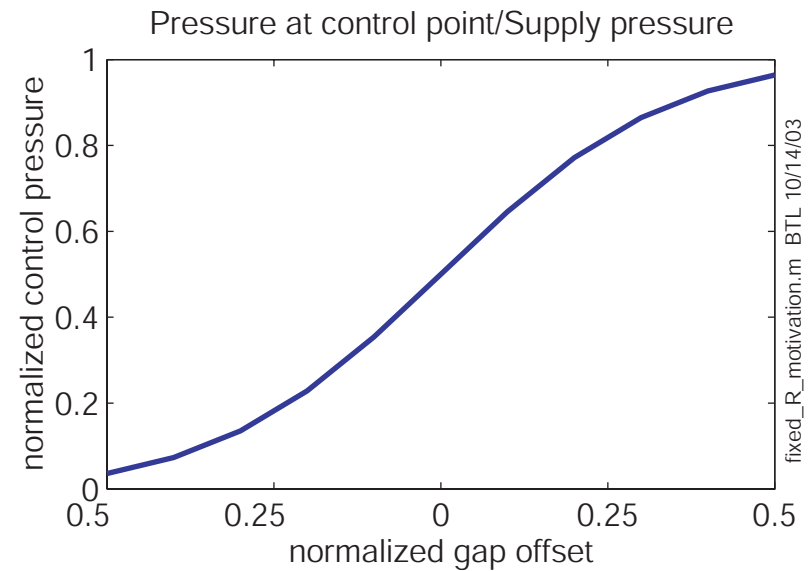
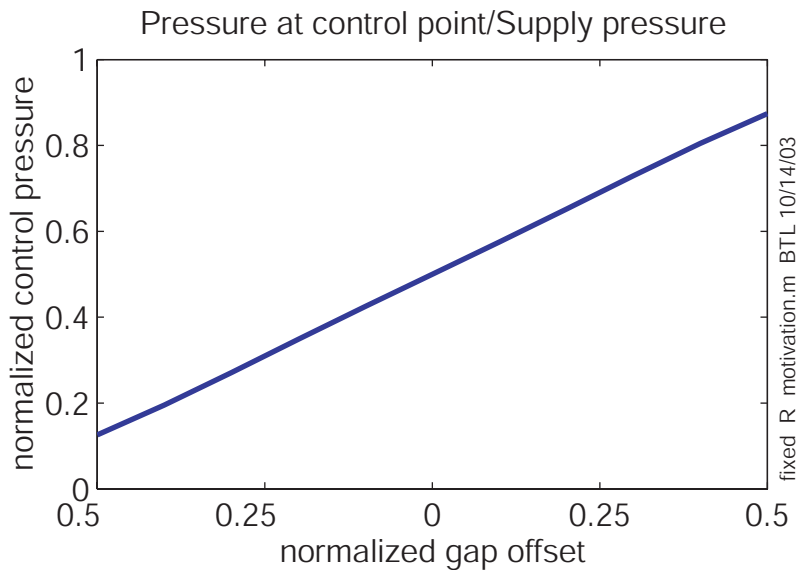
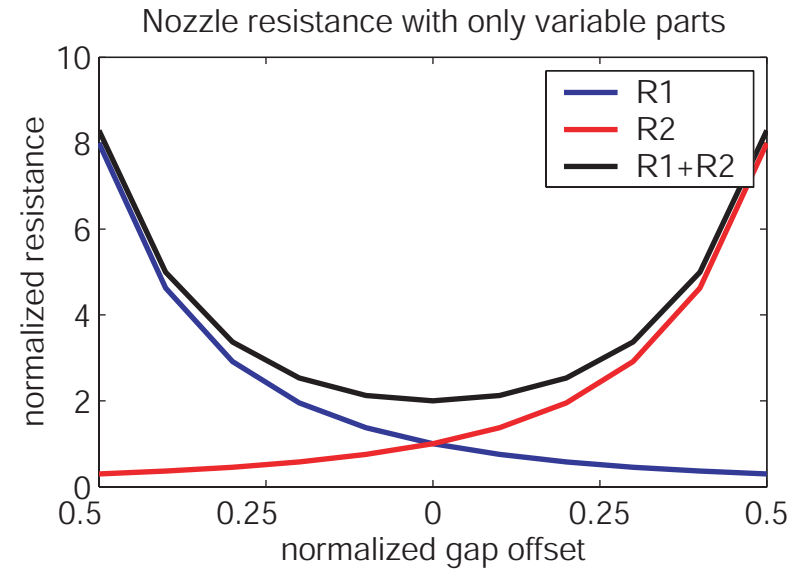
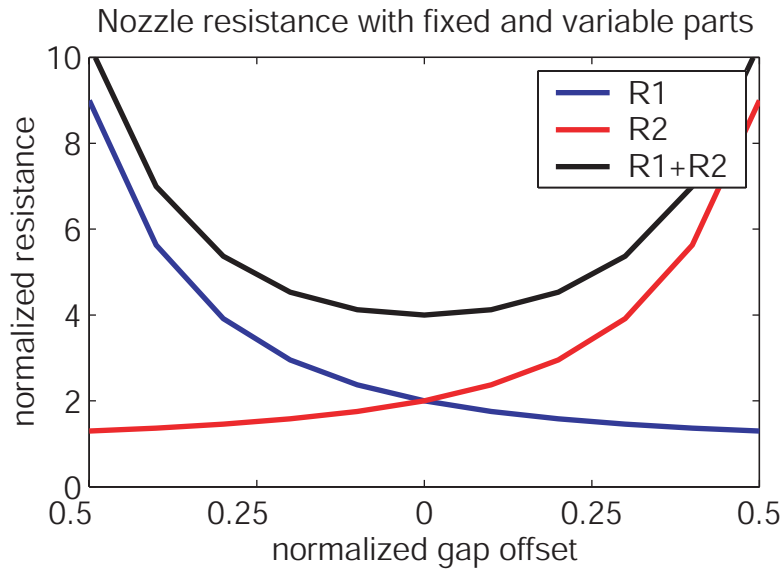
$$R_{pipe} = \frac{128\mu L}{\pi \cdot d^4}$$



Nozzle with no fixed resistance

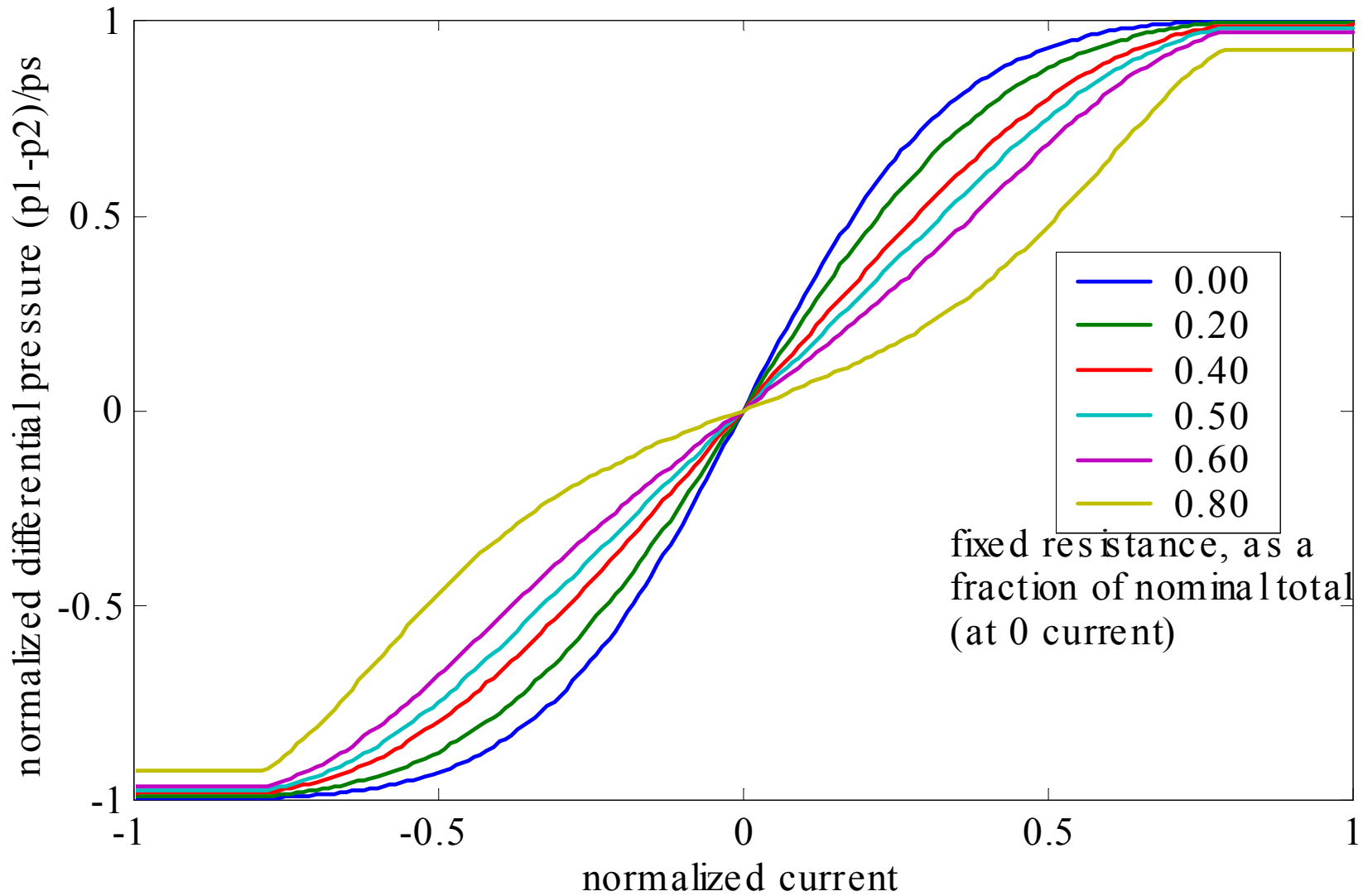


With and without fixed resistance



Choosing Nozzle Parameters

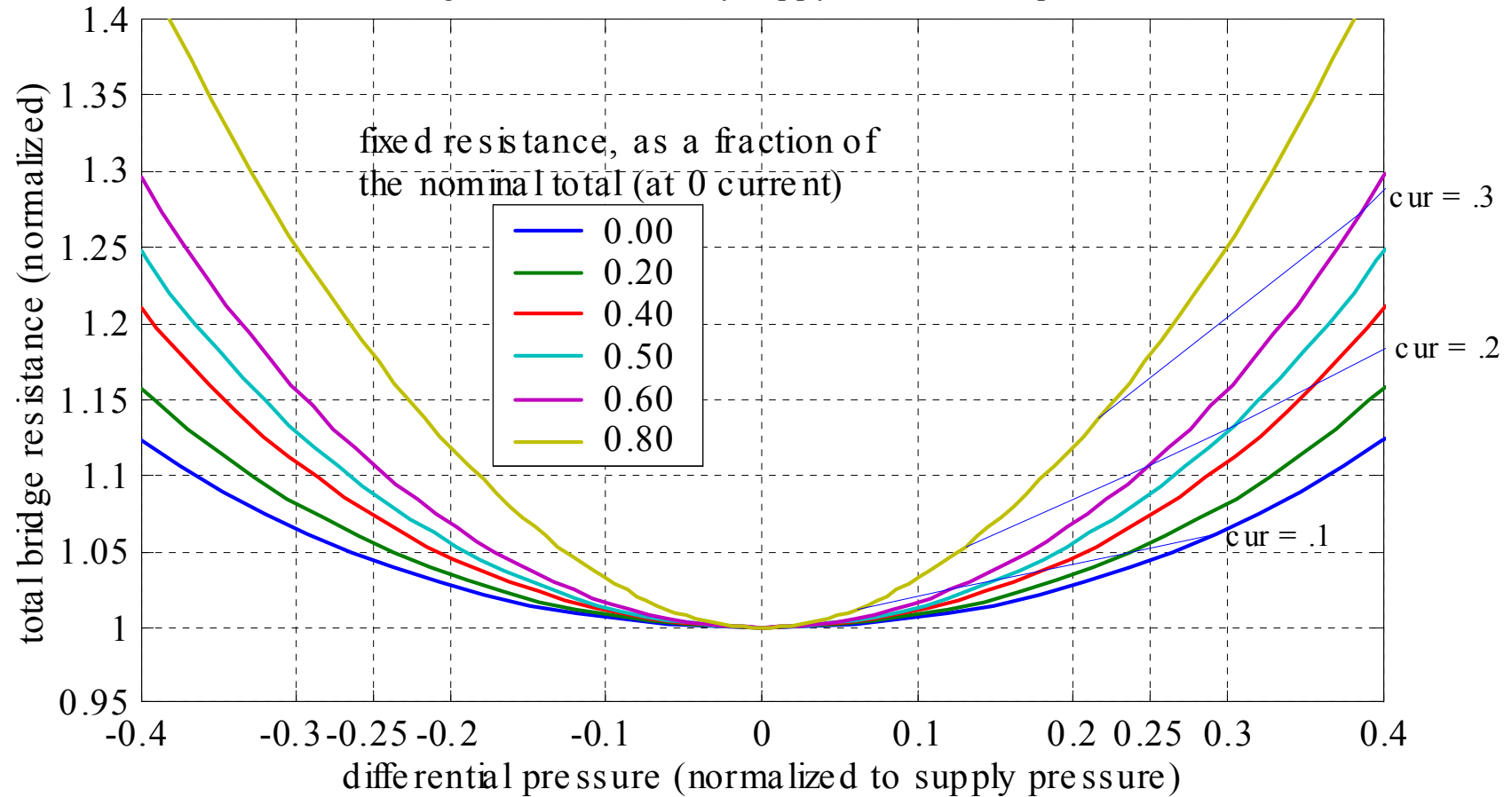
Control pressure as function of control current and fixed resistance



fixed resistance, as a fraction of nominal total (at 0 current)

load impedance of actuator

Bridge resistance seen by supply vs. differential pressure



Setup and Calibration of the Valve

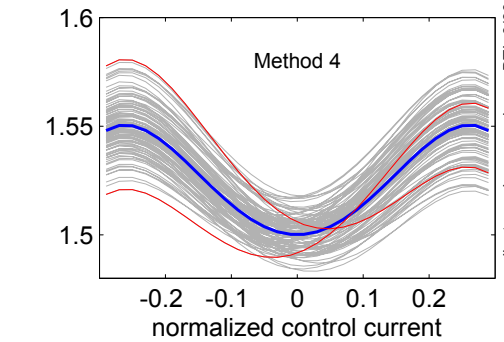
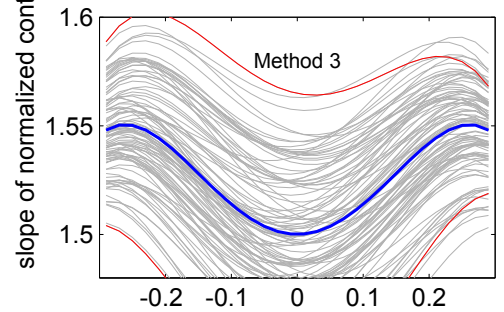
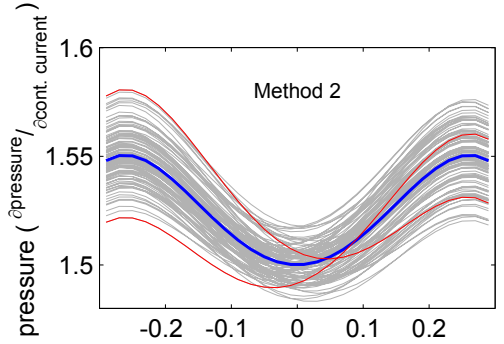
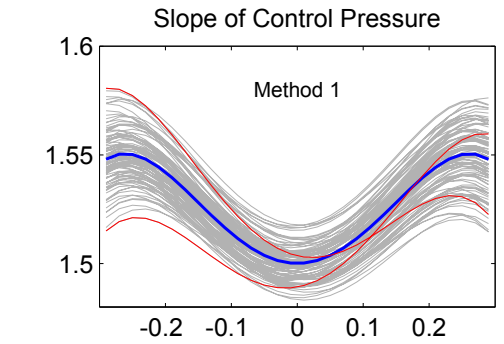
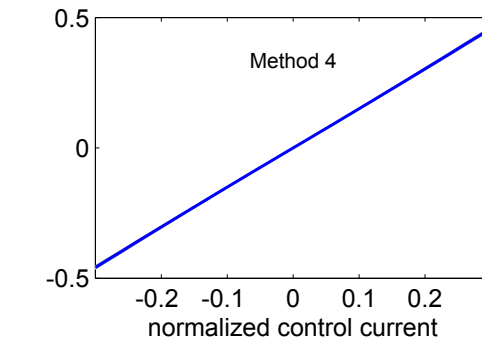
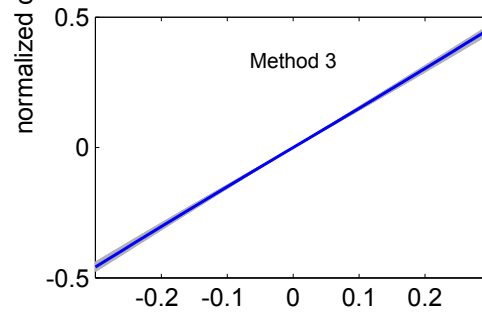
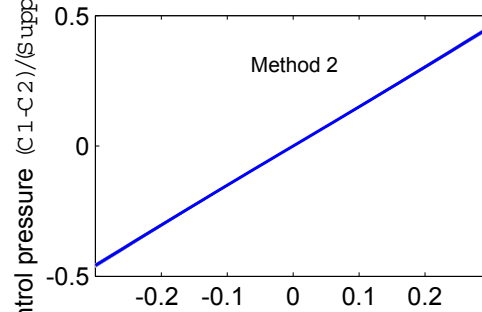
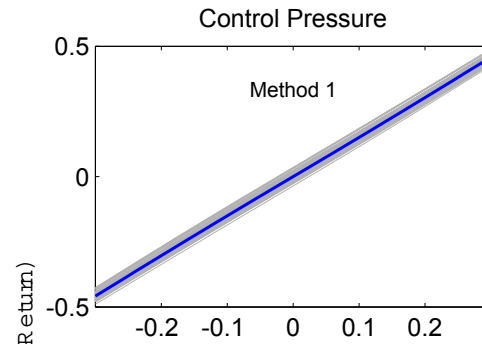
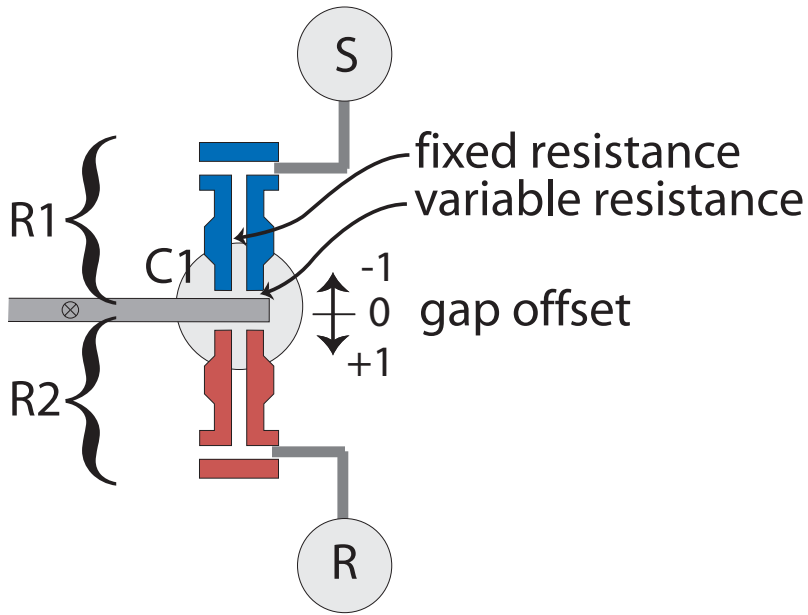
Nozzles must be set to the correct offset from the flapper
nozzles come have built-in 10-56 fine thread for adjustment in-situ

We are making a calibration station to do the nozzle setup, and measure
the pressure recovery vs. control current (in the lab)

Matching the fixed resistance gives self-calibration immunity to viscosity
changes.

We have developed a method to give the best response in the presence of
small variations in the fixed resistance

Best Method



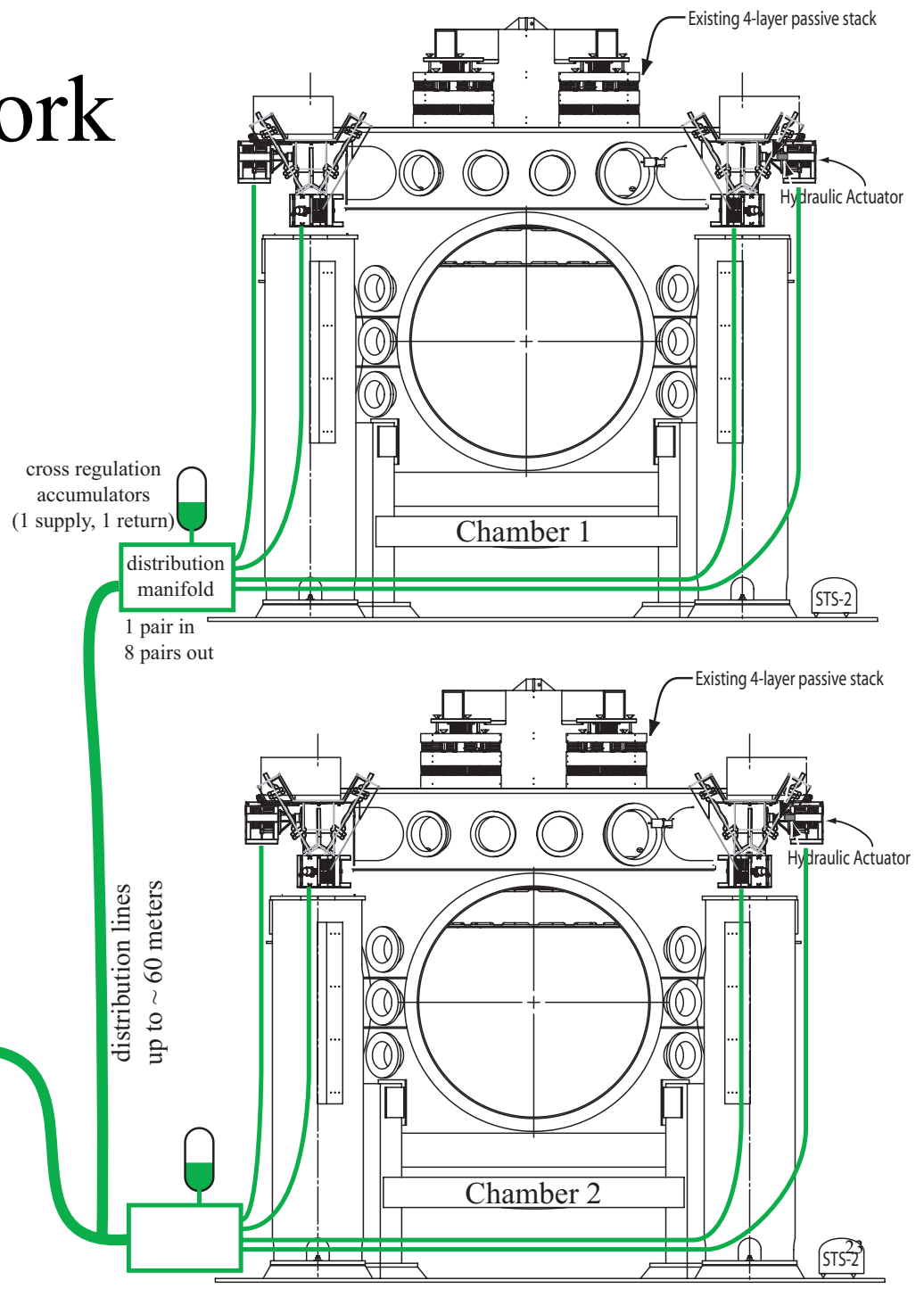
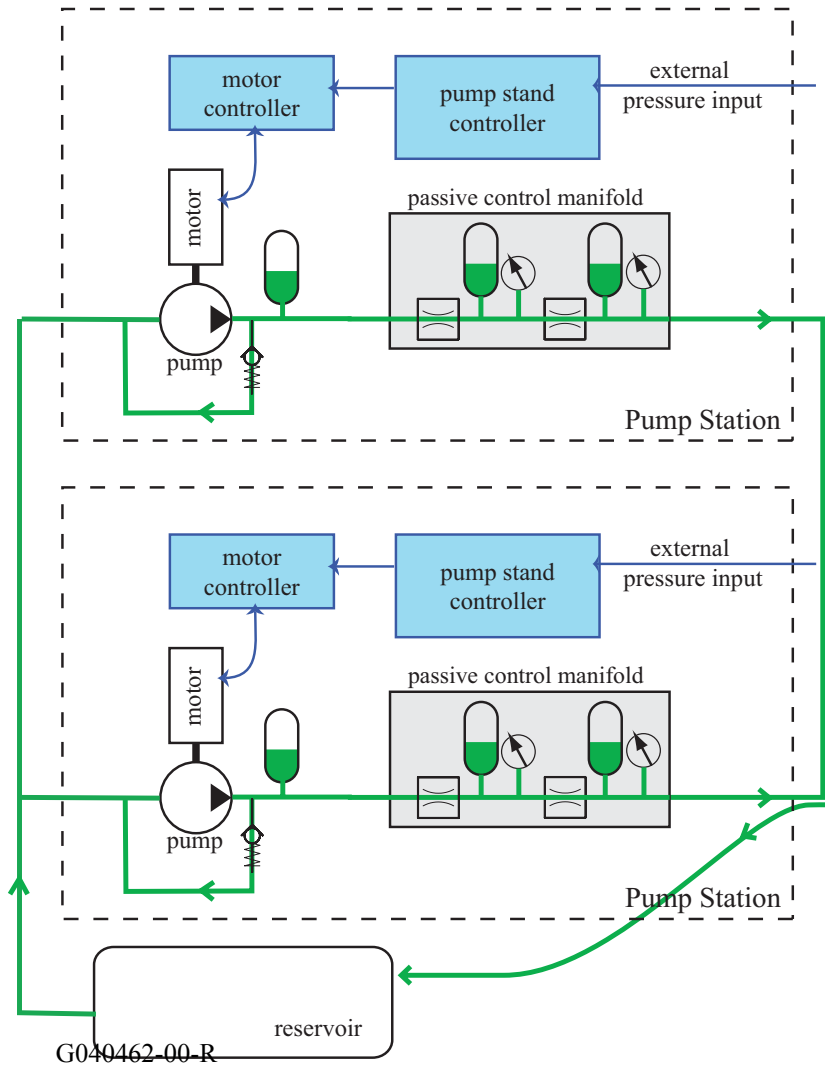
adjust_random_nozzles.m BTL 9/30/03

see *Calibration of the Modified DYP-2S Valves*, Brian Lantz
G040462-00-R

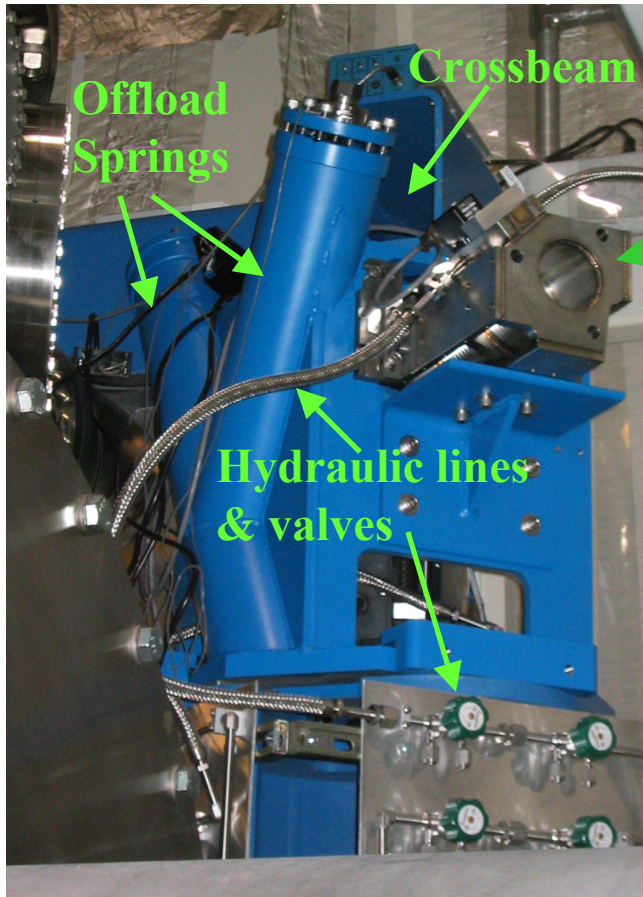
Valve conclusions

- Valve is a critical, non-standard part.
- Simple modification to existing valves can be done.
- New nozzles are:
 - quiet
 - linear
 - susceptible to temperature variations, but addressed by:
 - 1) temperature control of the room
 - 2) closed loop control of the actuator
 - 3) closed loop control of the pressure drop across actuator
- Custom nozzles require custom installation fixture

Distribution Network



Hydraulic Installation



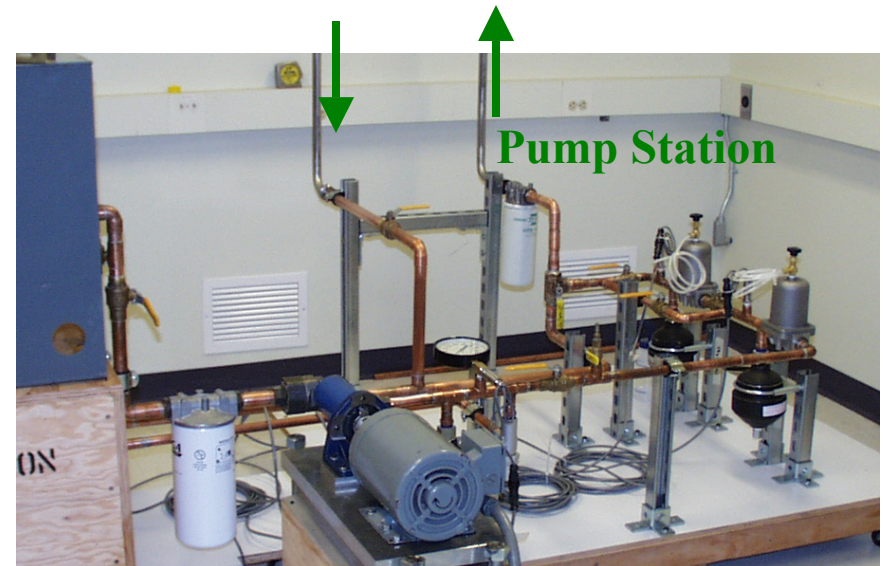
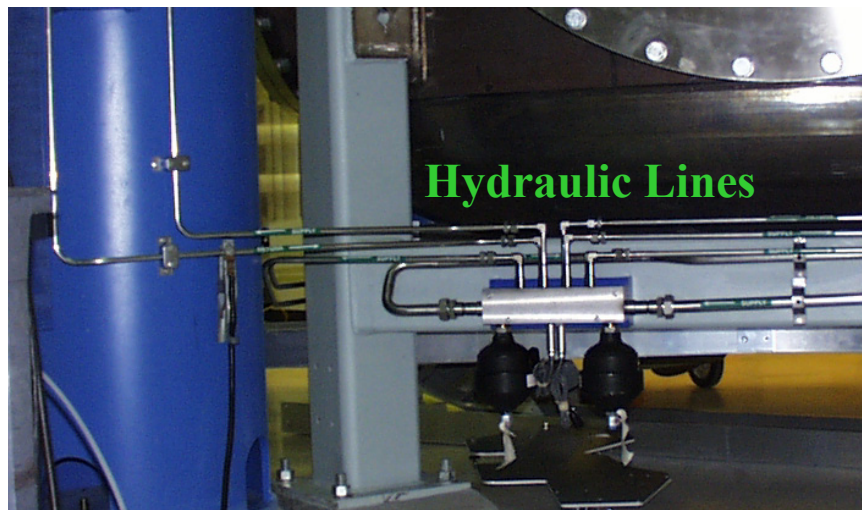
Horizontal Actuator

A green arrow points from the text 'Horizontal Actuator' to a component on the right side of the blue assembly.

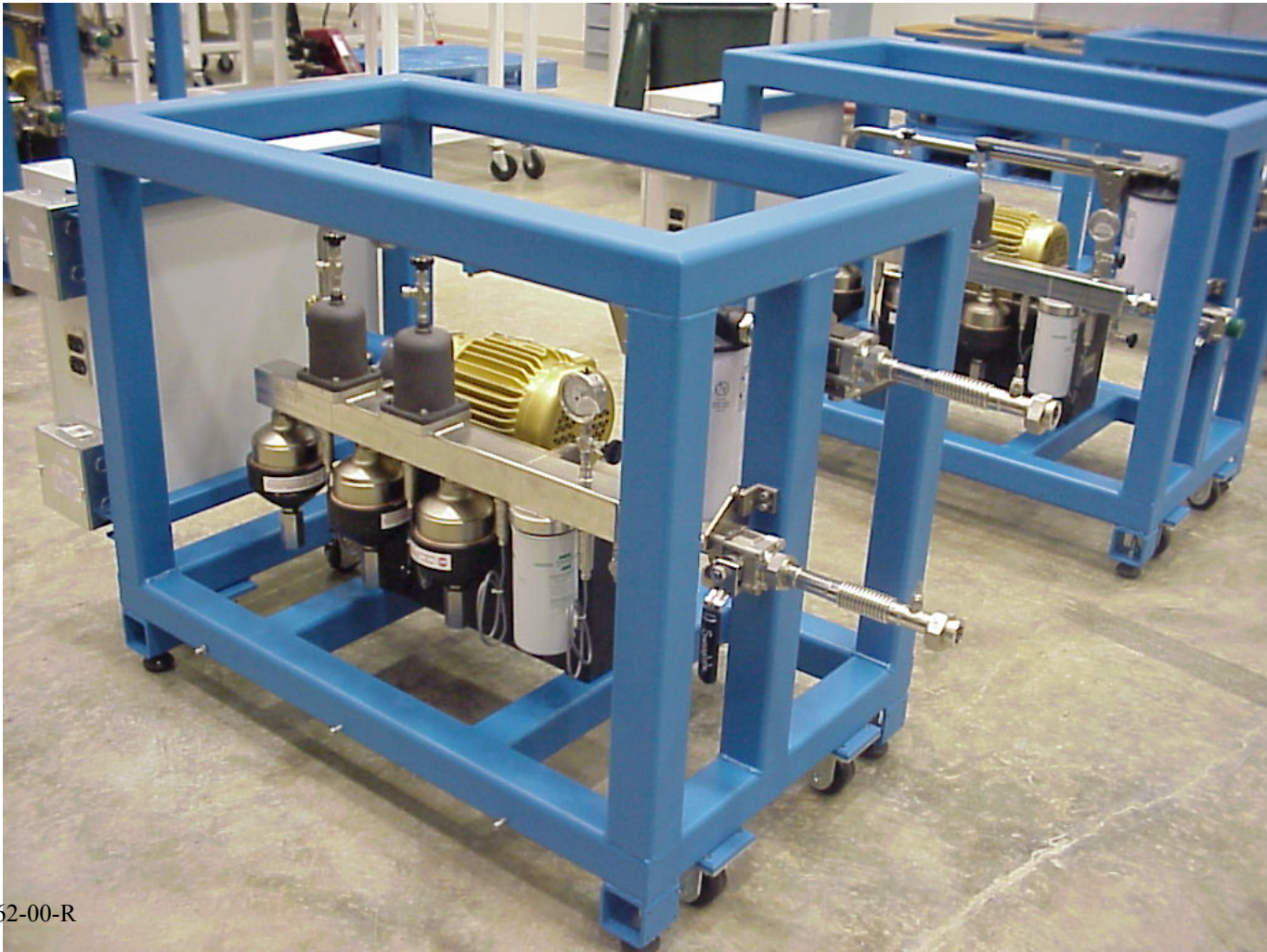


fun!

The word 'fun!' is written in green and enclosed in a green oval. Three small green circles are positioned above the man's head in the adjacent image.



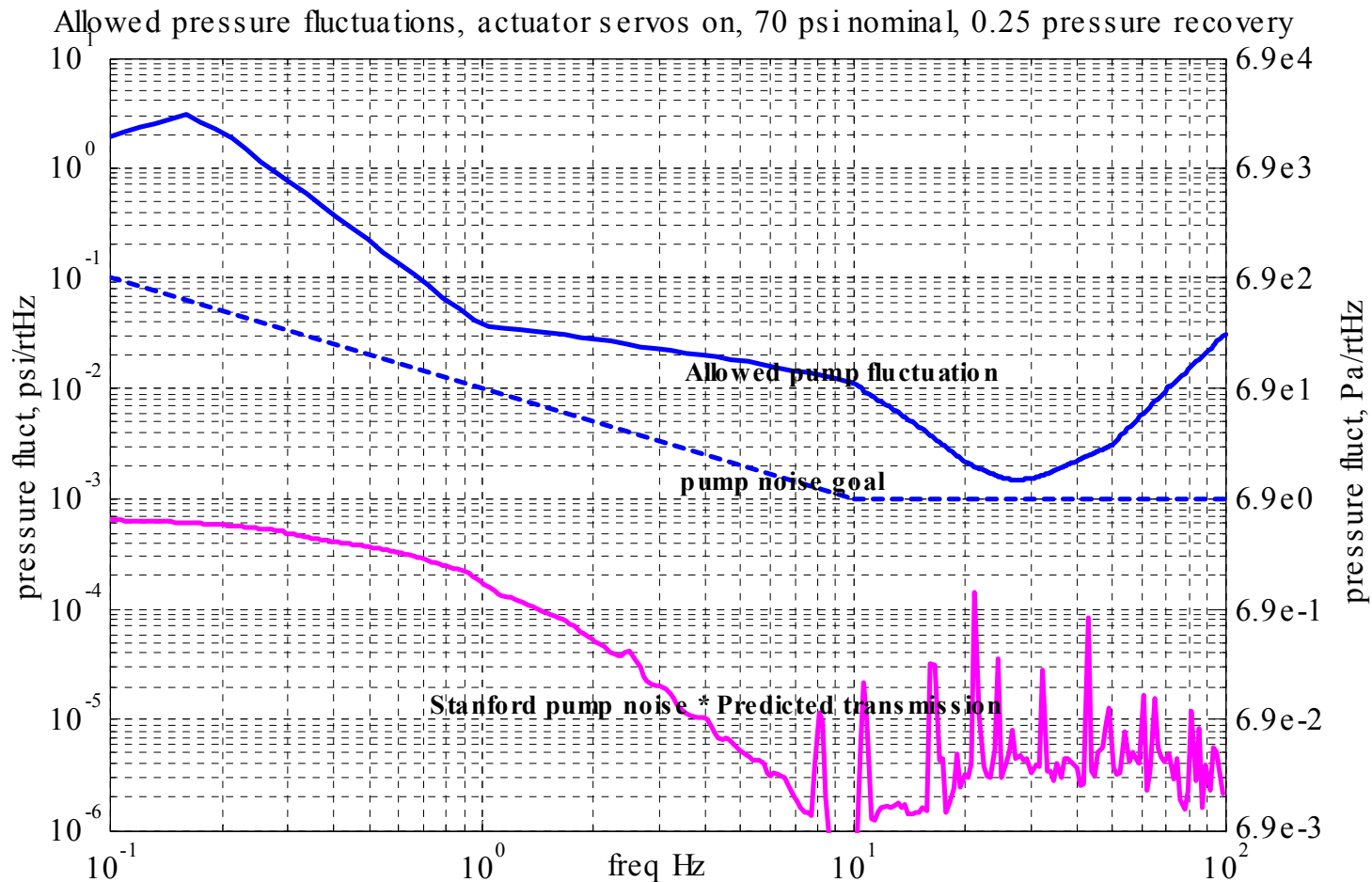
Pumps at LLO



G040462-00-R

Allowed pump noise

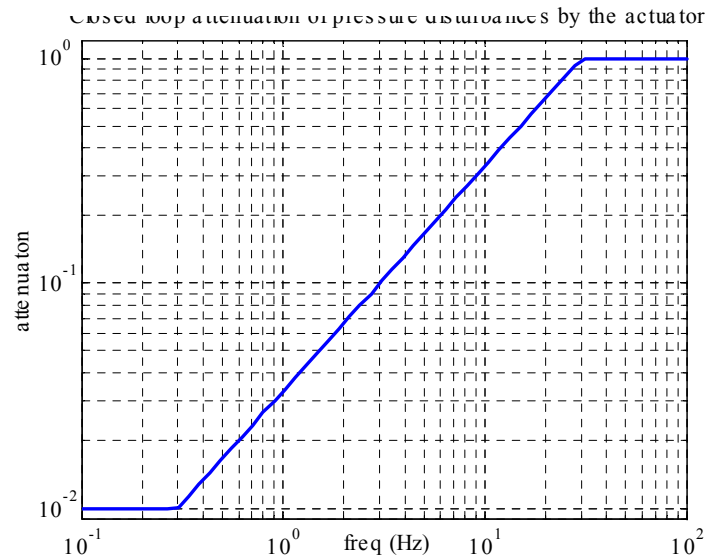
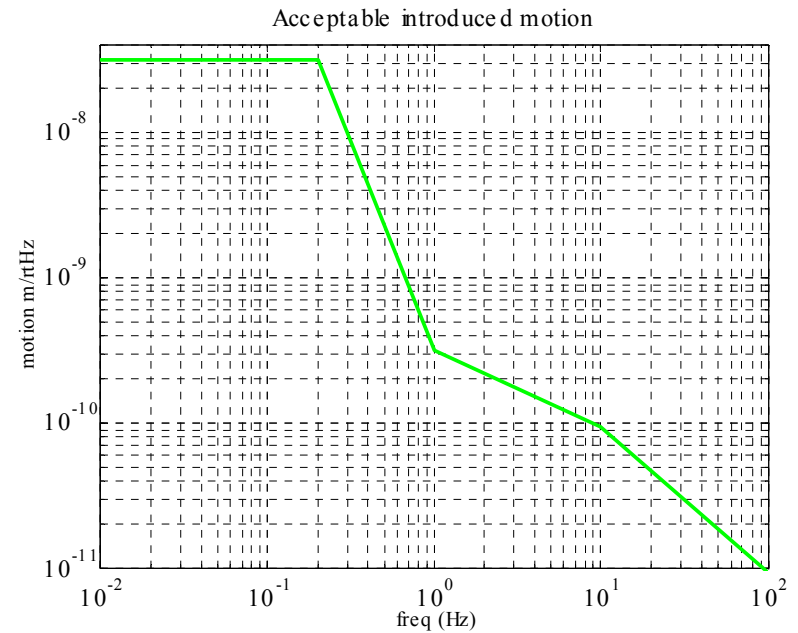
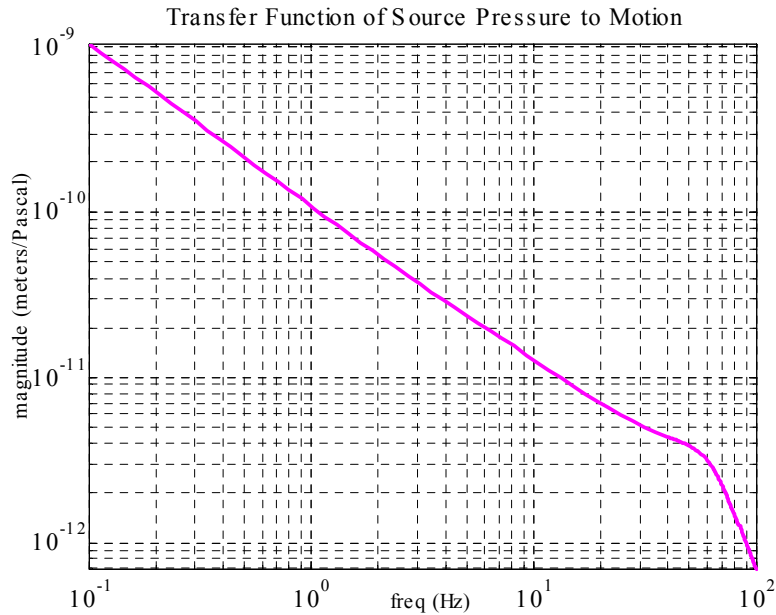
- Bridge offset couples pressure noise into actuator motion
- Active control reduces actuator noise
- Pressure noise * coupling * loop_attenuation <= acceptable motion



final_allowed_noise_5w_noise.e.fig

March 28 2002

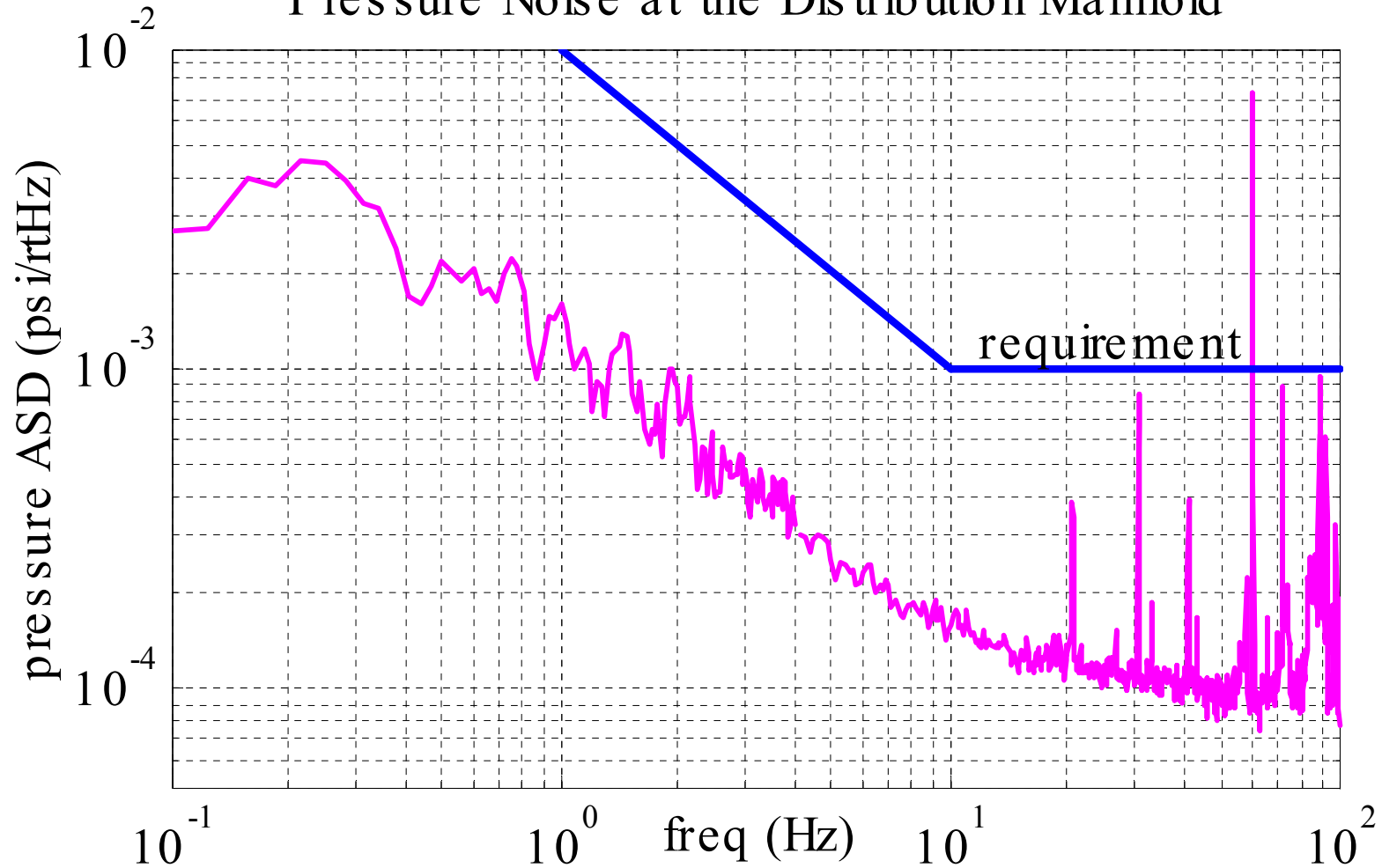
Calculating Allowed Pump Noise



described in
Allowed Pump Noise,
 Brian Lantz, Corwin Hardham,
 Dan DeBra, Jan 31 2002.

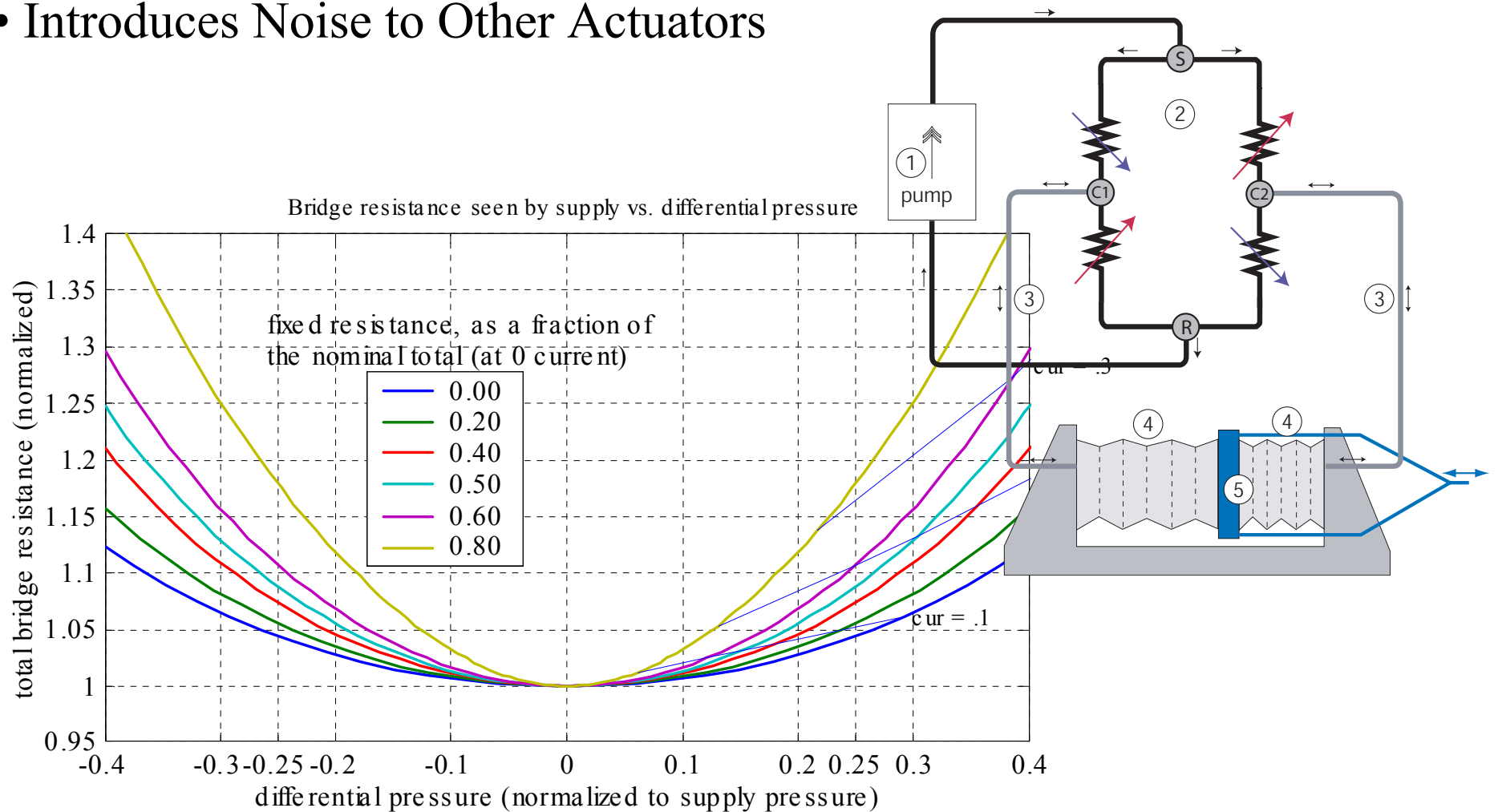
Measured noise at LASTI

Pressure Noise at the Distribution Manifold



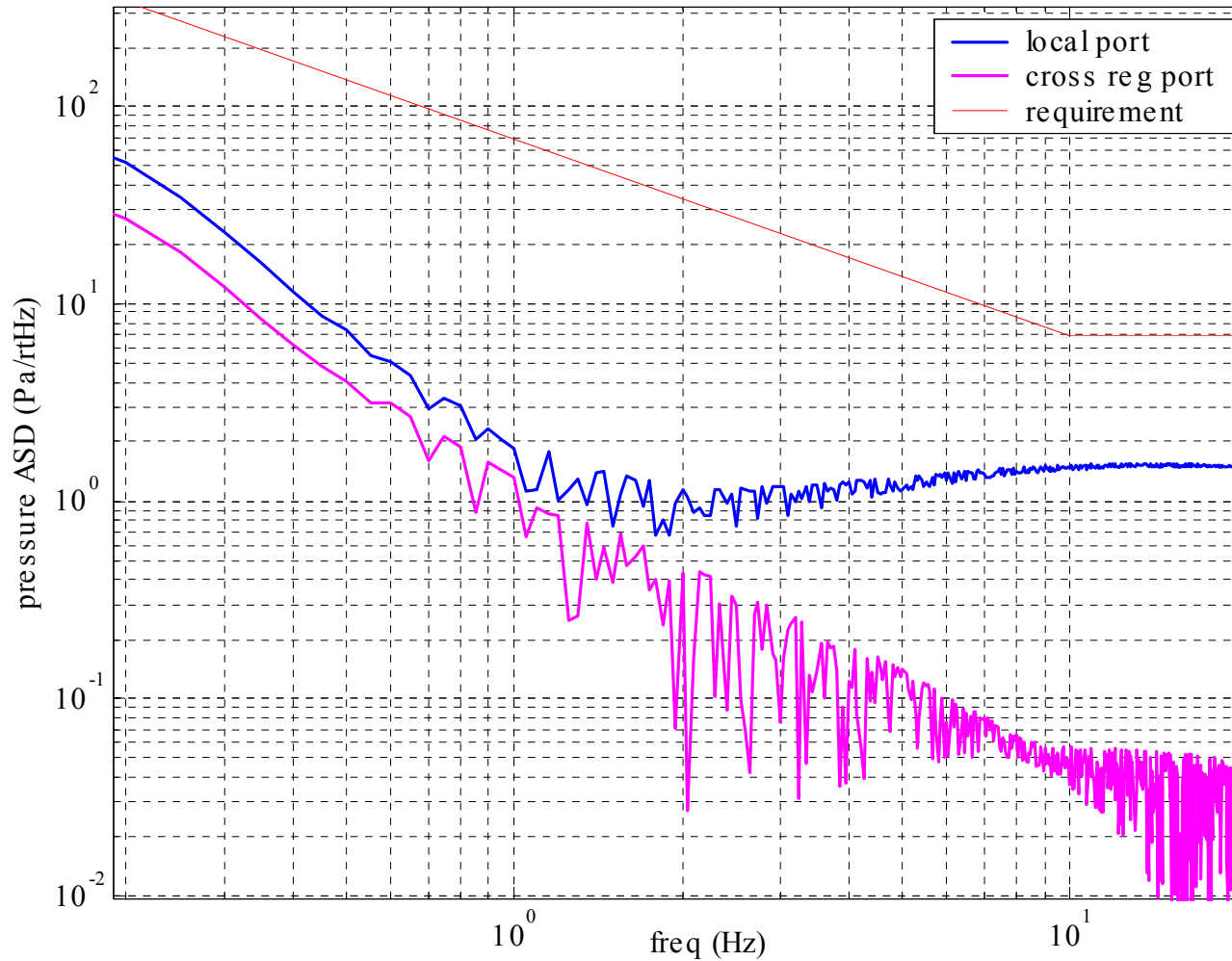
Cross Regulation Noise

- Bridge offset couples actuator drive into changing Load Resistance
- Load Change = flow & pressure change at Distribution Manifold
- Introduces Noise to Other Actuators



Modeled Effect of Cross-Regulation Accumulator

Cross Regulation Accumulator Filters Pressure Fluctuations



Comments on Distribution System

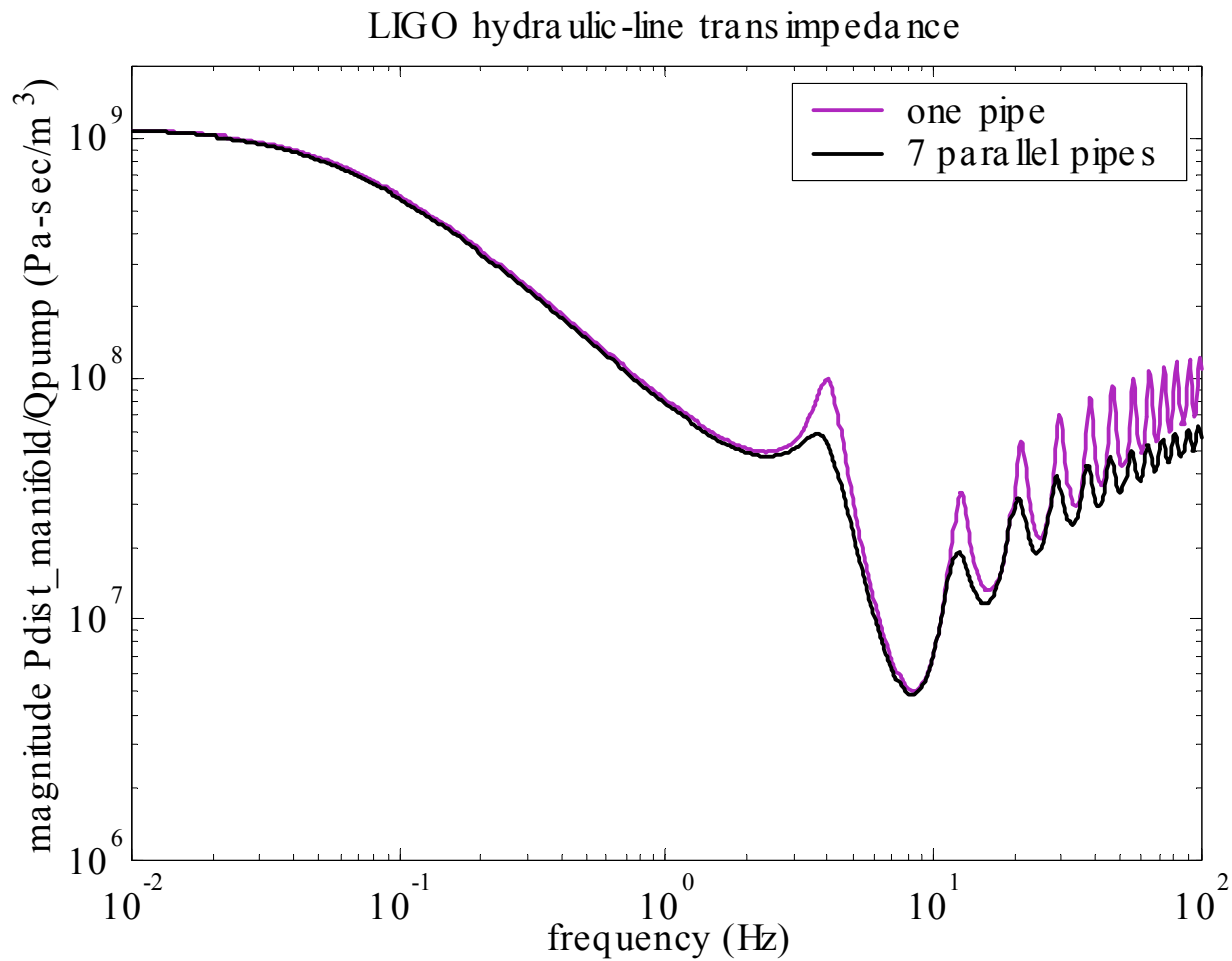
2 stages of passive filtering + pump speed control seems sufficient

Cross modulation between actuators controlled by manifold accumulators

pipe dynamics are interesting (and not discussed here)

pump station is all COTS, except laminar flow resistors

Pipeline dynamics are interesting



Sensors – our two types

Inertial Sensors

A class of commercial instruments called seismometers (geophones are a common type of seismometer)

Substantially more quiet than the ground between 0.1 and 100 Hz (and provide useful information at 0.01 Hz to 1000 Hz)

Relative Displacement Sensors

measure the distance between stages

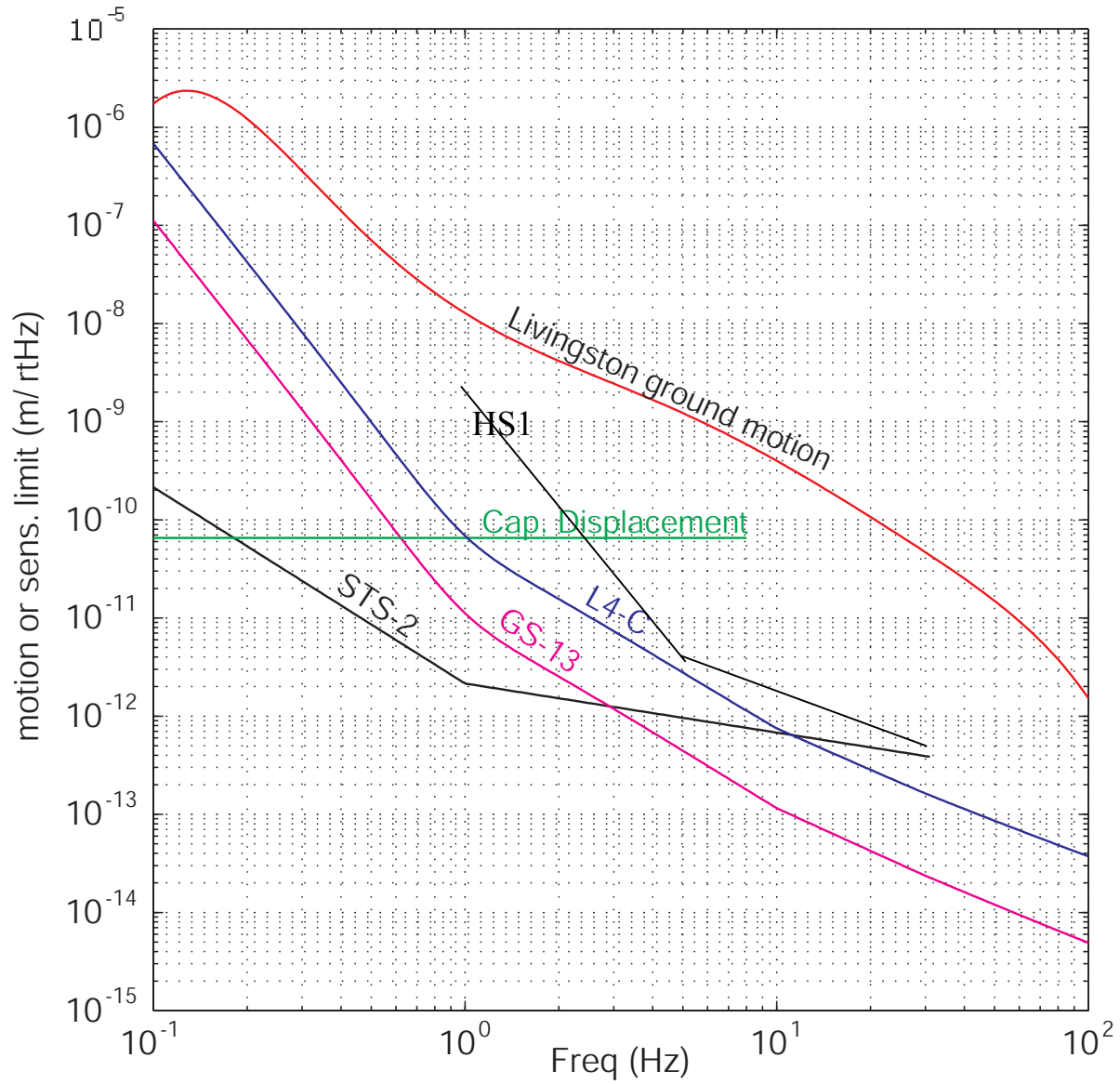
eliminate low frequency loop crossover (replace with blending)

provide alignment information

help with tilt control

relate inertial information between stages

Sensor noise



A Few Inertial Sensors



Streckeisen STS-2
 ~\$14k 3 DOF
 120 sec period
 ~26 cm x 23 cm d
 13 kg
 active force balance



Geotech GS-13
 ~\$6k 1 DOF
 1Hz
 ~38 cm x 17 cm d
 10.4 kg
 passive w/ preamp

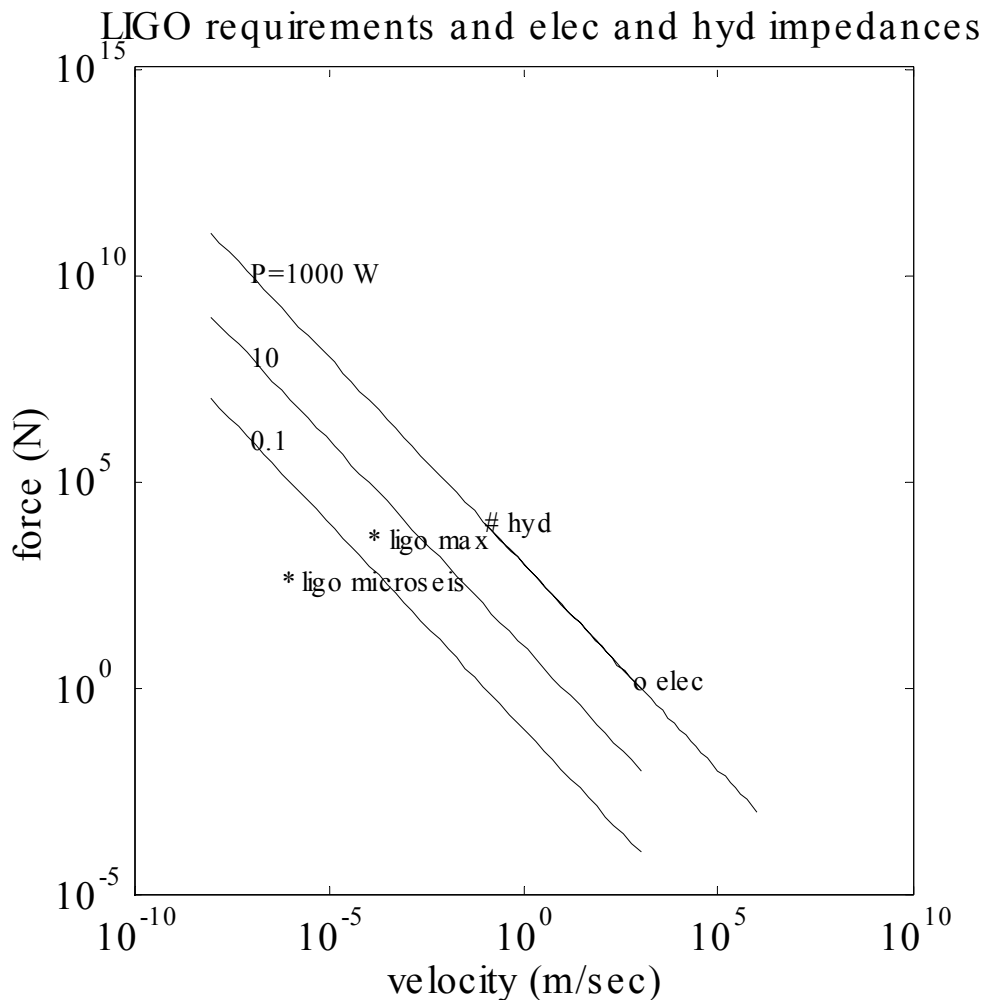


Sercel L-4C
 ~\$1.1k 1 DOF
 1 Hz
 13 cm x 7.6 cm d
 2.15 kg
 passive



Geospace HS1
 ~\$70 1 DOF
 4.5 Hz
 7.2 cm x 6.7 cm d
 1/4 kg
 passive

Actuators



Outer Stage

Laminar Flow Hydraulic
































- Well matched to requirement (range and noise)
- easy to hold large offsets
- stiff and well damped

Inner Stages

Electromagnetic

- quiet
- force actuation is independent of position of support
- high bandwidth

Design Trades

Parameter Performance	Specification		Design				Related Parameter		
	$\delta=1\text{mm}$	$\Delta t=10\text{ sec}$	$P_s=5\text{ bar}$	$\beta=2\text{e}3\text{ bar}$	$R = 5\text{e}10\text{ Pa-sec/m}^3$	$A=.01\text{ m}^2$	$V=3\text{e-}4\text{ m}^3$	$m=1\text{e}3\text{ kg}$	$k=4\text{e}6\text{ N/m}$
1) Hydraulic Resonance $\omega_n^2 = \frac{2A^2\beta}{mV}$ 									
2) Damping $\zeta = \frac{1}{RA} \sqrt{\frac{m\beta}{2V}}$ 									
3) Bridge Power Dissipation $P_b = \frac{P_s^2}{R}$ 									
4) Acquisition Power $P_{acq} = \frac{k\delta^2}{\Delta t}$ 									
5) Microseism Power $P_\mu = k\delta\delta_s w_s$ 									
6) Microseism vs. Bridge $\frac{P_{acq}}{P_b} = \frac{k\delta\delta_s\omega_s R}{P_s^2}$ 									
7) Microseism vs. Acquisition $\frac{P_\mu}{P_{acq}} = \frac{\delta_s\omega_s\Delta t}{\delta}$ 									

Candidate Actuators

	Force	Velocity	Stiffness	Displacement	Stiction	Hysteresis	Mechanical Noise
Hydraulic	High	Low	Med	Med	Low	Low	Low
Ball Screw	High	Low	High	High	High	Low	High
Linear Motor	Med	High	Low	High	Low	Low	Low
Piezo or Magnetostriction	High	High	High	Low	Low	High	Low

Organizational Responsibilities

Caltech: Administer the project, engineering staff, research.

MIT: Research, LASTI.

LASTI: LIGO vacuum system, user facility for Advanced LIGO final prototypes.

Stanford: Research for Advanced LIGO, LSC member, Engineering Test Facility.

LIGO Livingston Observatory (LLO): One of the two US observatories (see also Hanford, GEO, Virgo, TAMA, ACIGA), destination of system

LSU: Research for Advanced LIGO, LSC member, near LLO