

# Status of 100 W Rod System at LZH



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# Outline

## Modeling

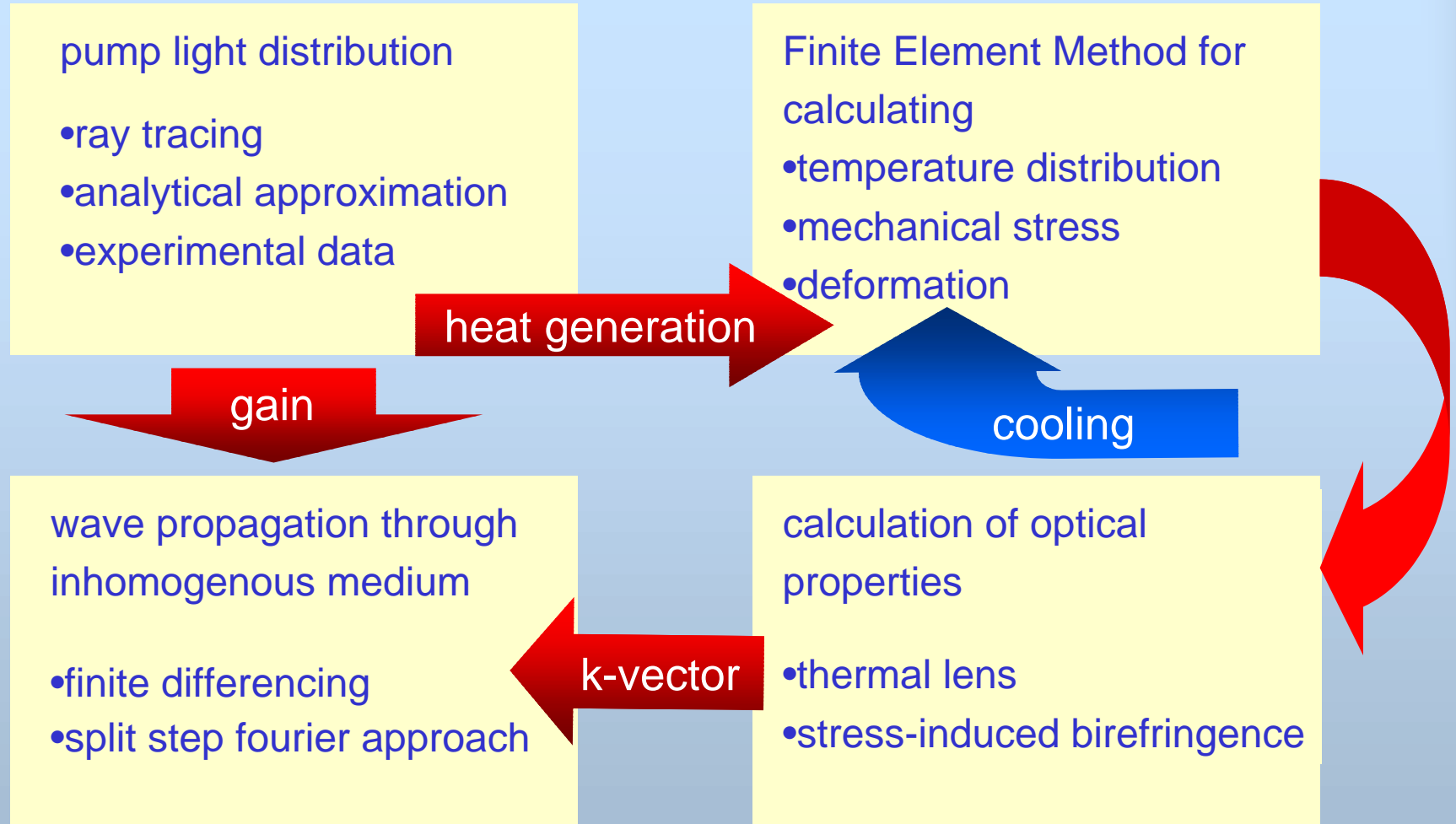
- Overview
- Results

## Experimental results

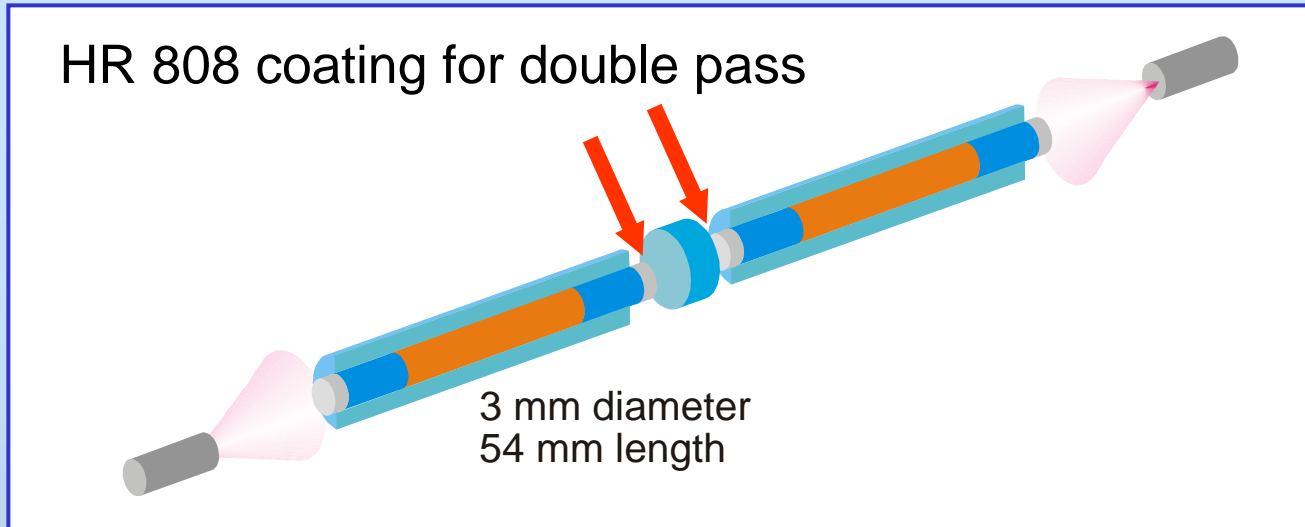
- Integrated Diode Units
- Pump Optics
- Pre-Experiments

## Resumé/Outlook

# Modeling/Overview

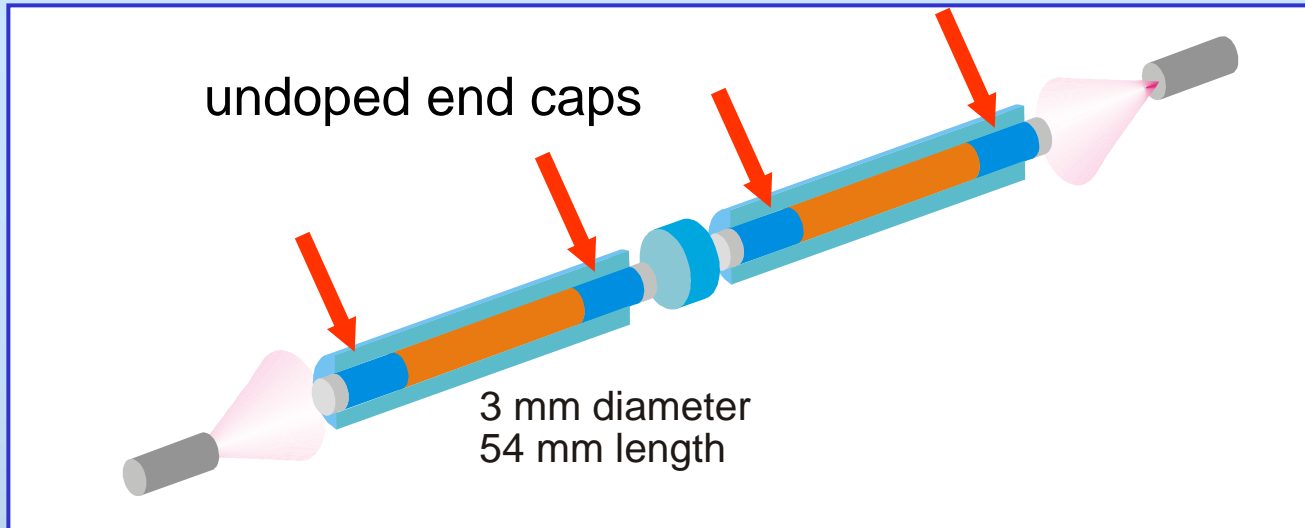


# 100 W Laser Head



- end-pumped rods  
reduce thermal gradient in z-direction

# 100 W Laser Head



- end-pumped rods

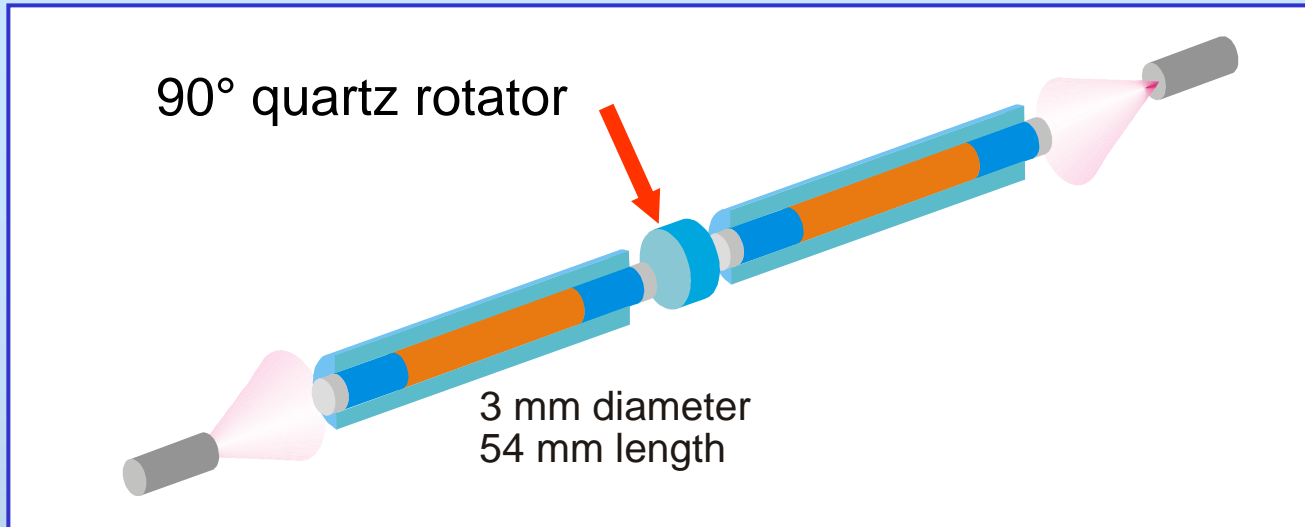
thermal lensing consists of two parts

thermal part via  $dn / dT$

end effect (bulging of end surface)

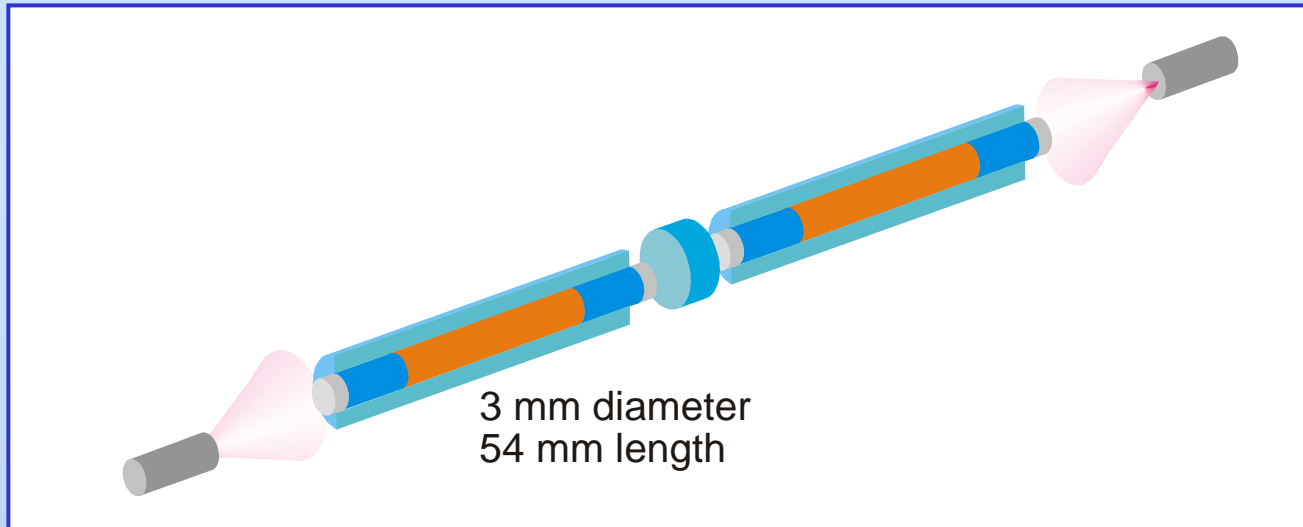
reduced by  
undoped endcaps

# 100 W Laser Head



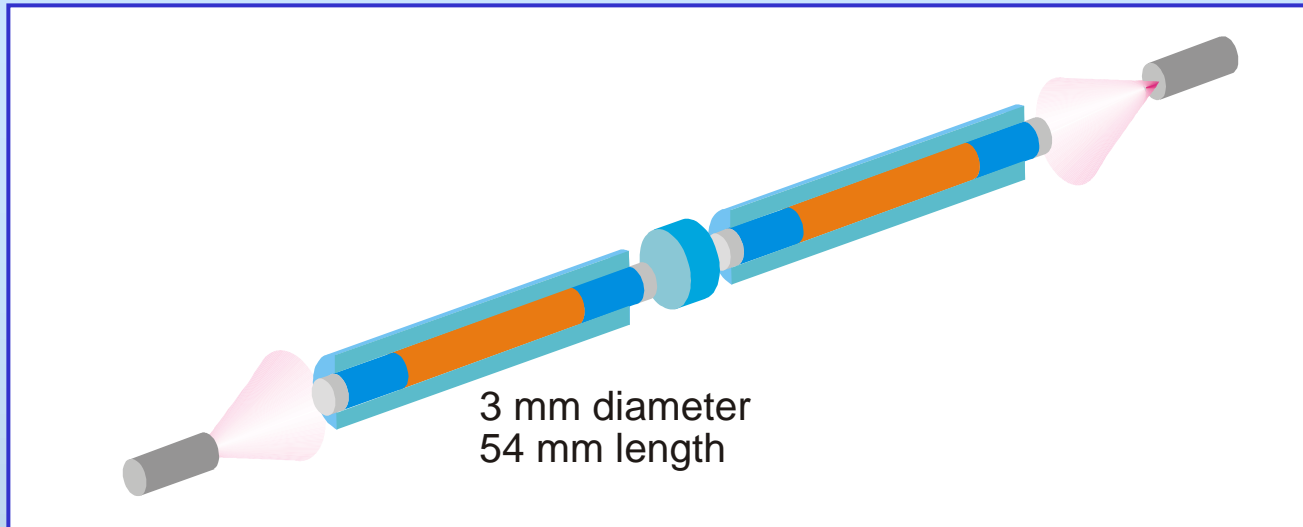
- end-pumped rods
- undoped endcaps reduce absolute temperature and thermal lens
- 90° quartz rotator compensates for birefringence

# Model



assumption:  
cylinder symmetrical pump light distribution

# Model



assumption:

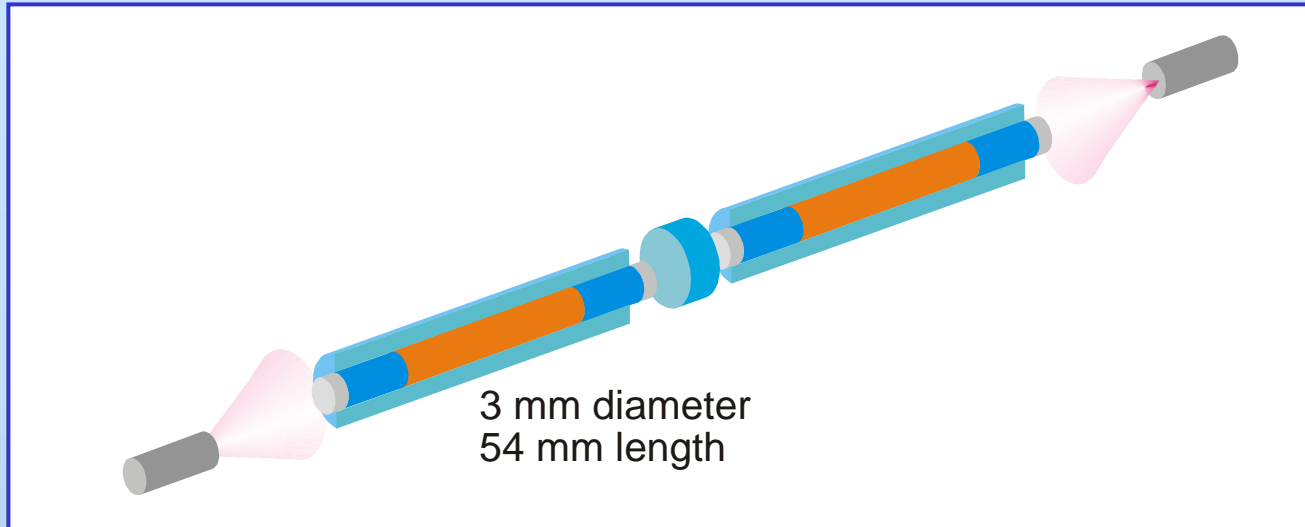
cylinder symmetrical pump light distribution

- model takes into account wavelength/temperature dependent properties

wavelength dependent absorption coefficient



# Model



assumption:

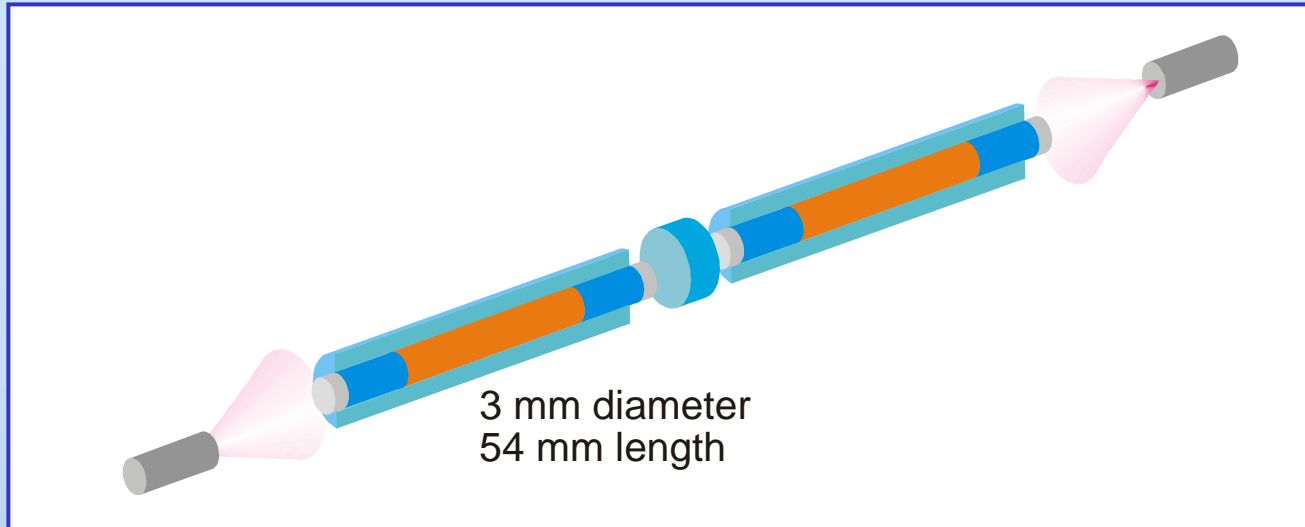
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# Model



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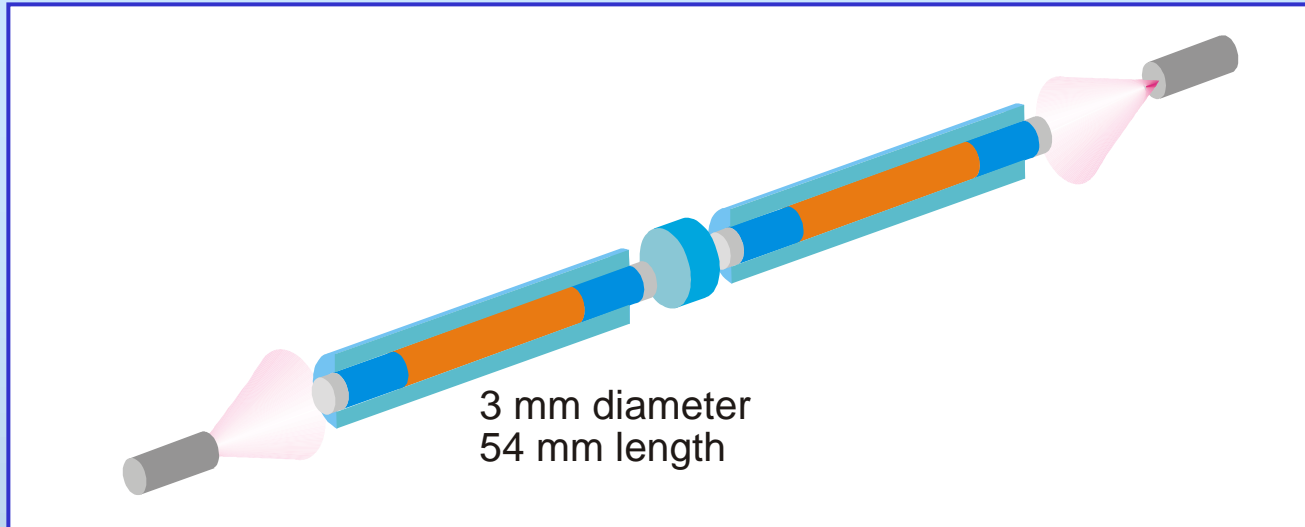
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wavelength dependent absorption coefficient

temperature dependent heat conductivity

temperature dependent expansion coefficient

# Model



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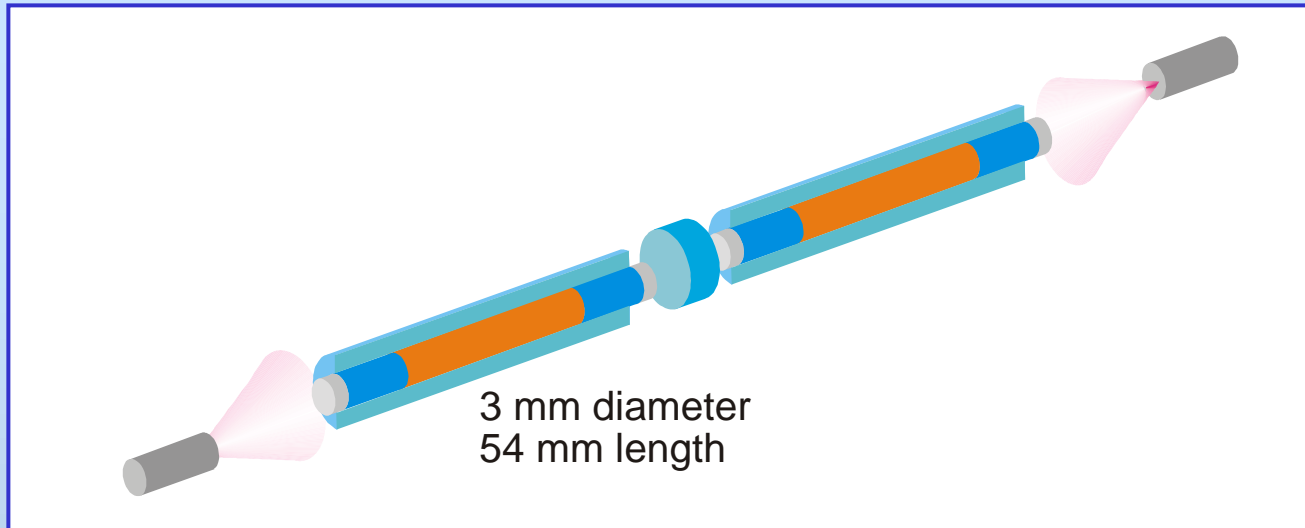
wavelength dependent absorption coefficient

temperature dependent heat conductivity

temperature dependent  $dn/dT$

temperature dependent expansion coefficient

# Model



assumption:

cylinder symmetrical pump light distribution

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wavelength dependent absorption coefficient

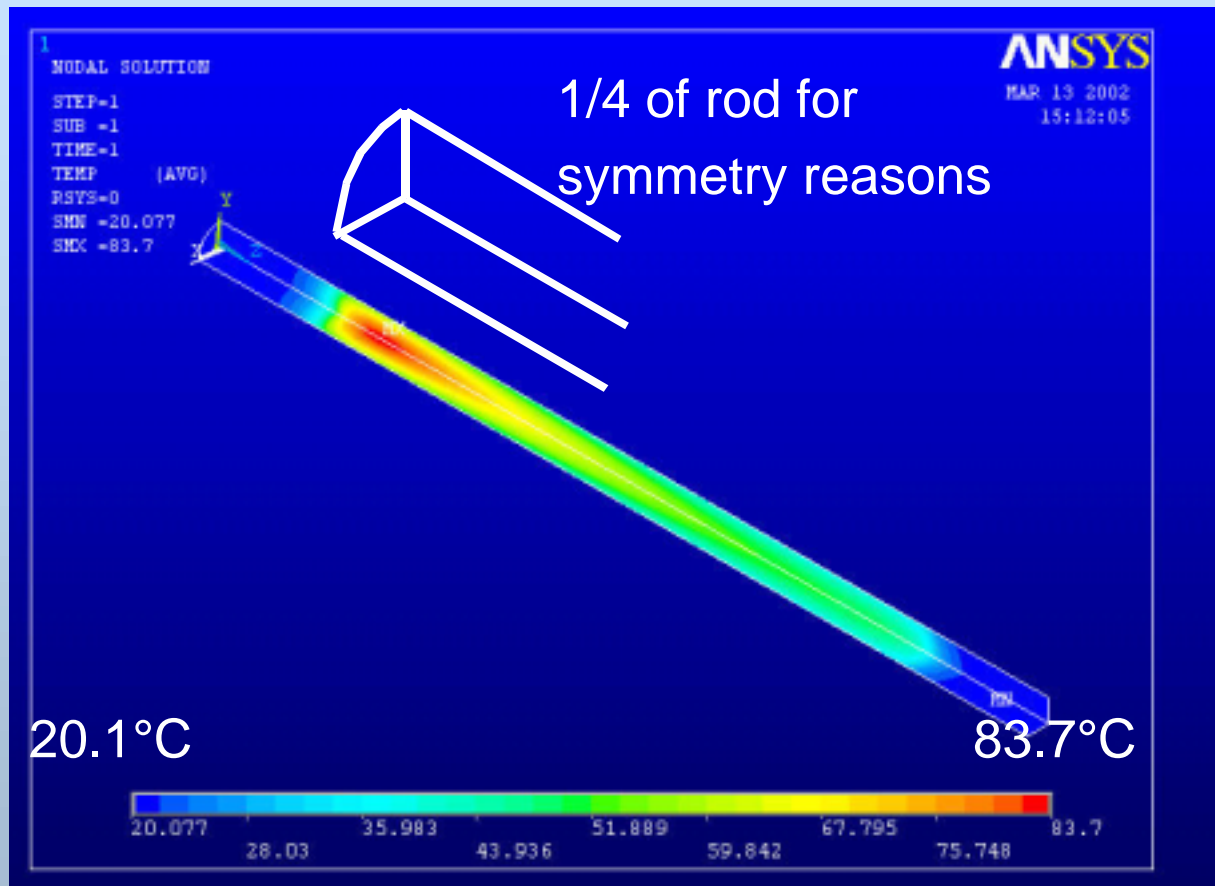
temperature dependent heat conductivity

temperature dependent expansion coefficient

temperature dependent  $dn/dT$

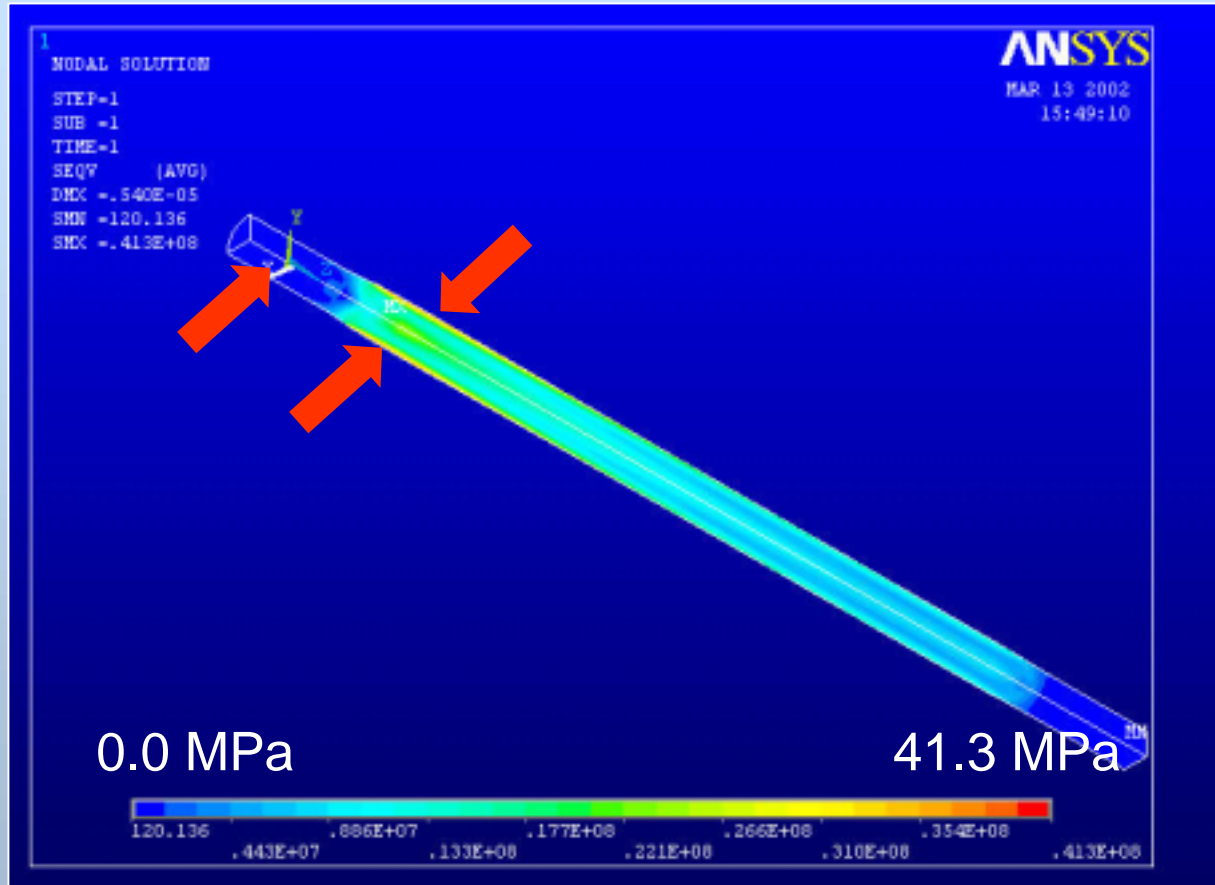
# Thermal Modeling/Temperature Distribution

- solution of time independent heat conduction equation by FEM (ANSYS)



# Mechanical Stress/Von Mises Equivalent Stress

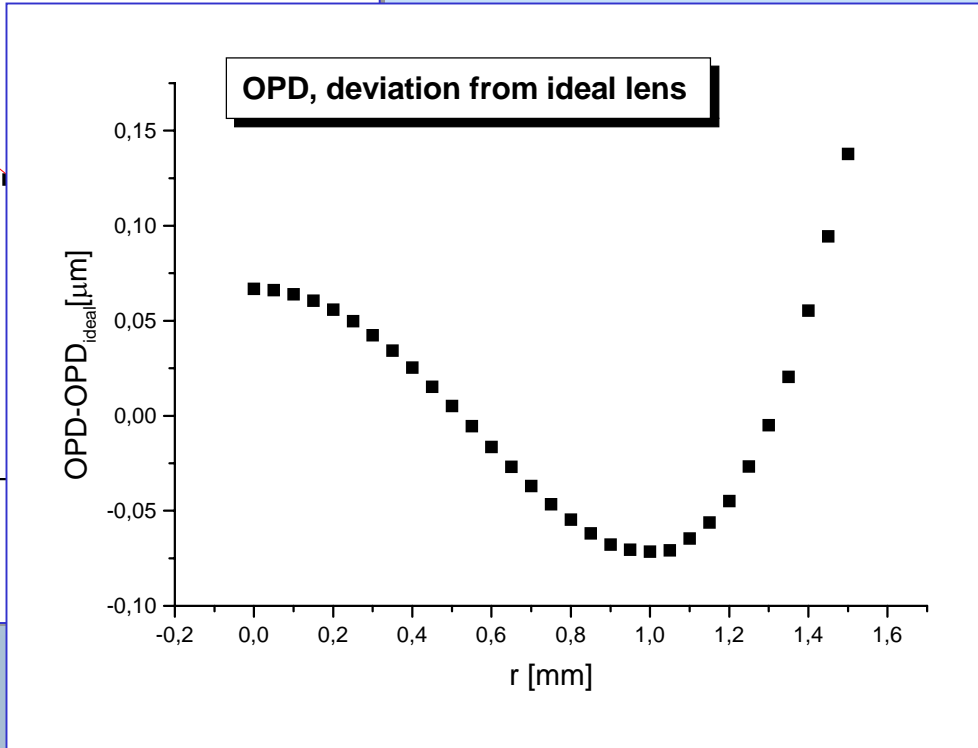
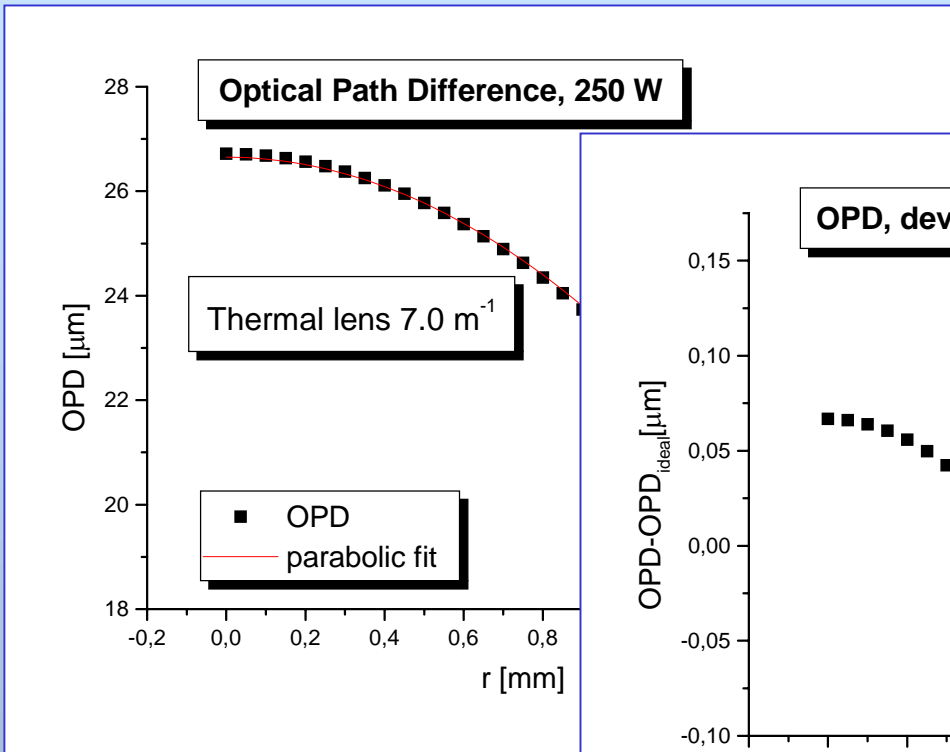
- fracture limit for YAG 130 thru 260 MPa



# Thermal Lens/Abberations

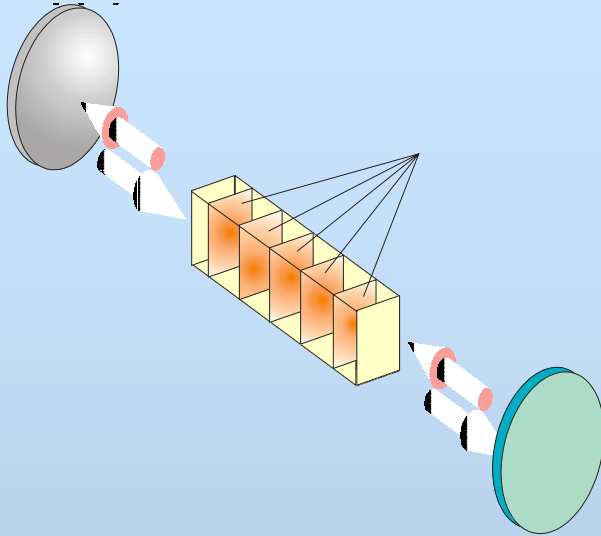
$$Opt.Path = \int_0^L dz n(x, y, z; T)$$

$$D(r) = -\frac{d^2}{dr^2} OPD(r, \phi)$$

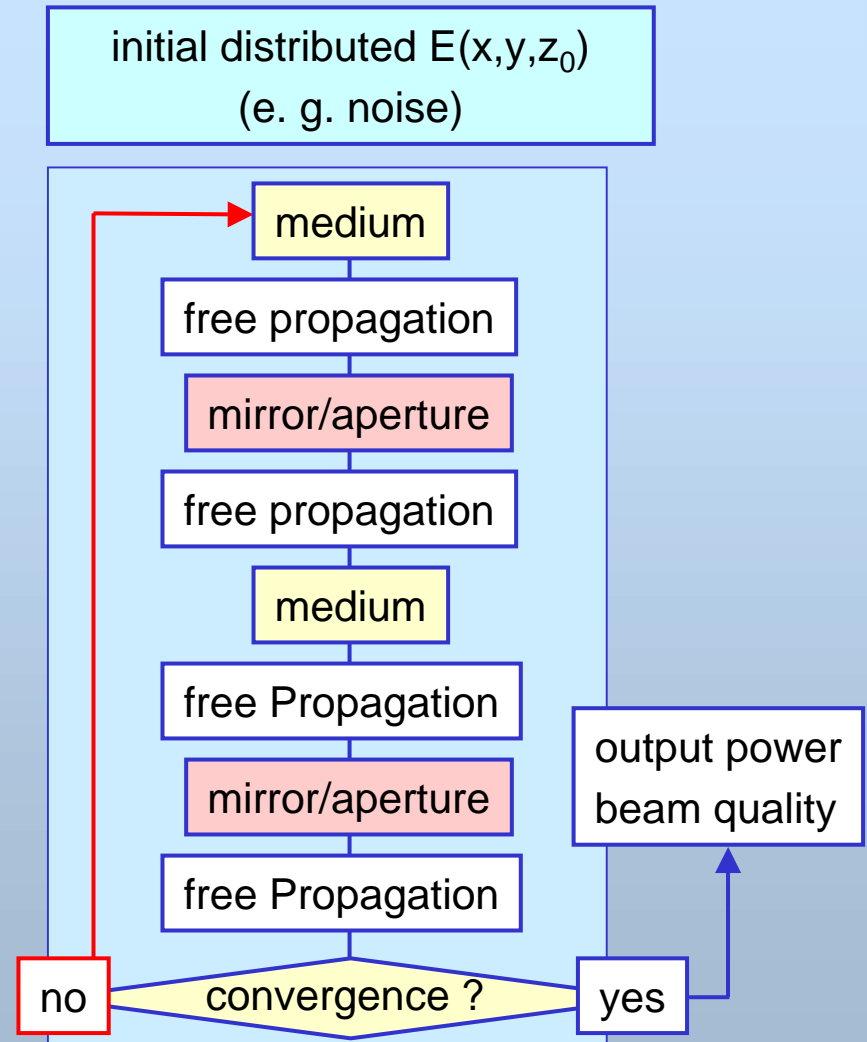


# Fox/Li Approach

Iterative Solution of Kirchhoff integral equations



- inhomogeneous distributed gain, refractive index, birefringence concentrated in gain/phase sheets
- propagation between gain/phase sheets and in free space described by FFT propagator

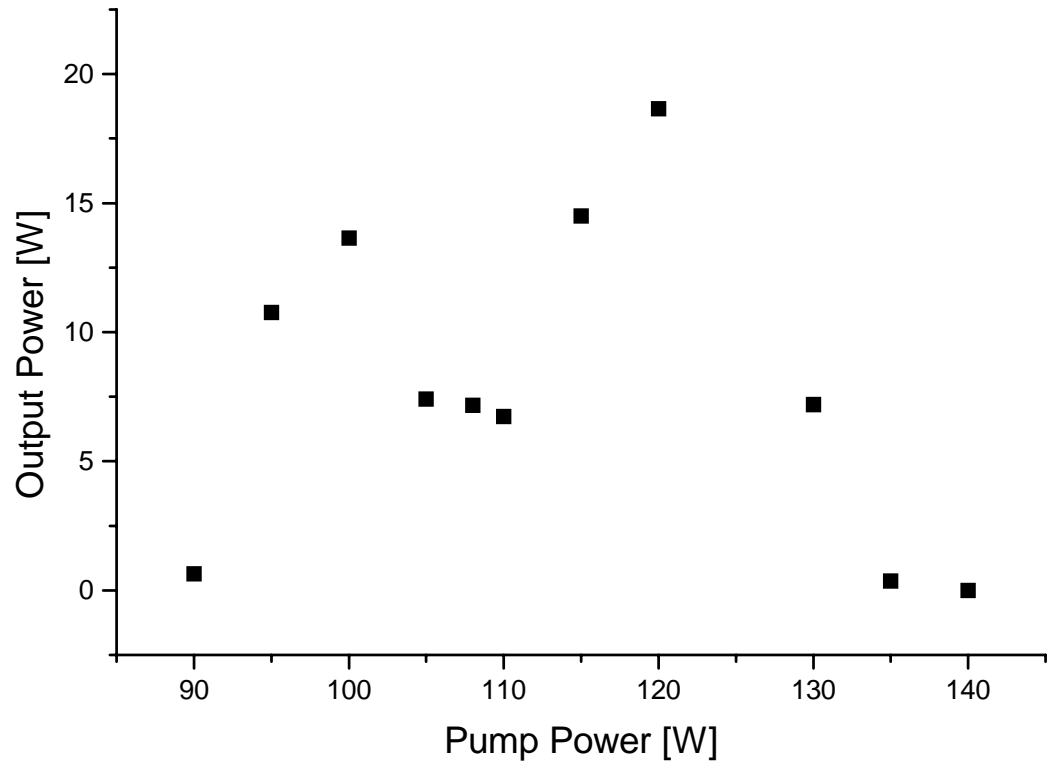
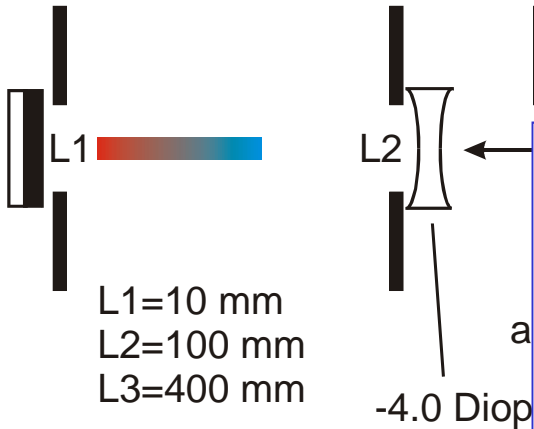




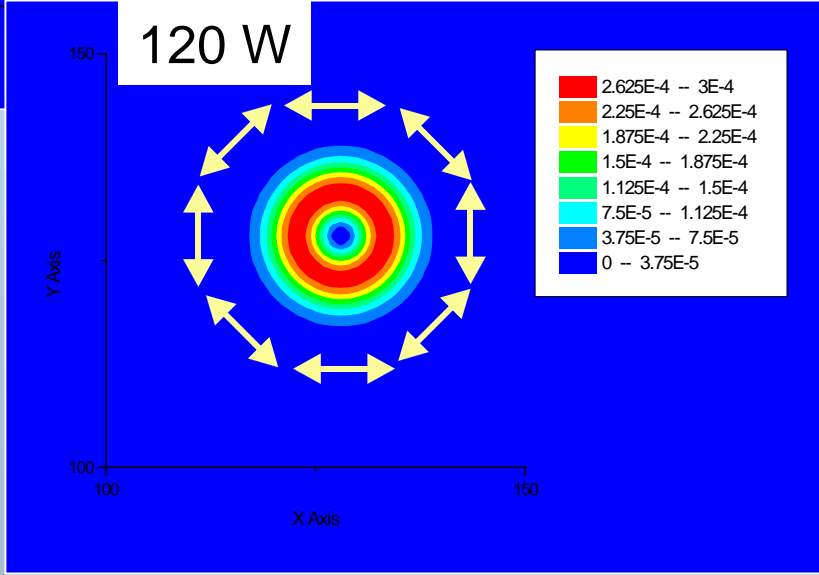
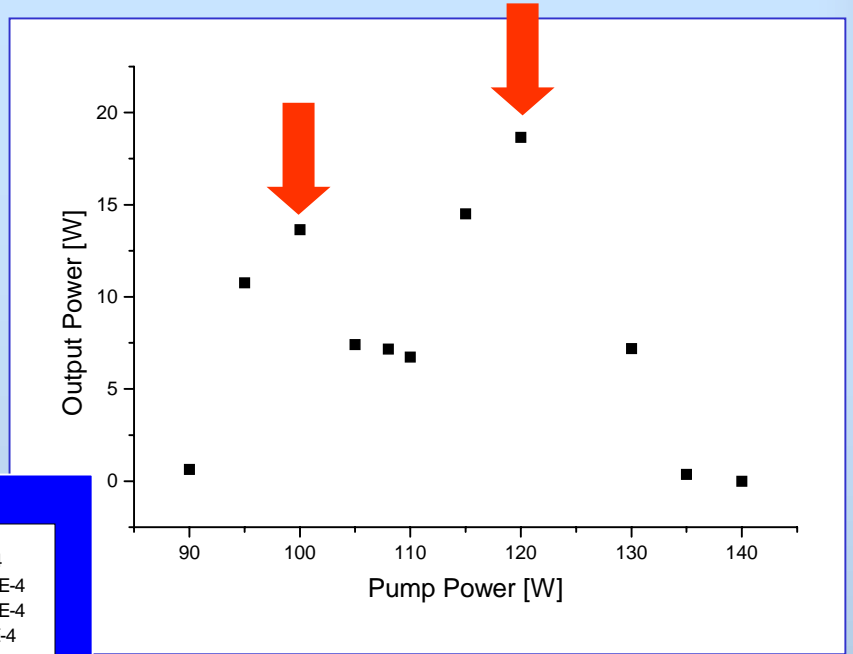
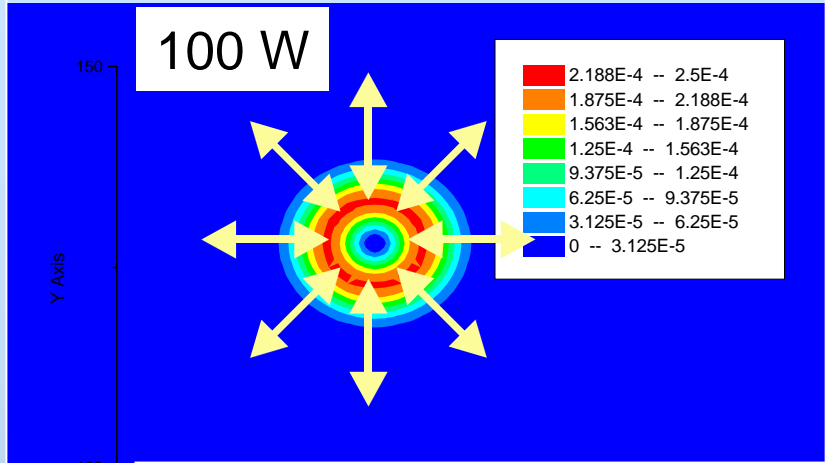
# First Results

test resonator (plane-plane)

•mode diameter in rod 1 mm

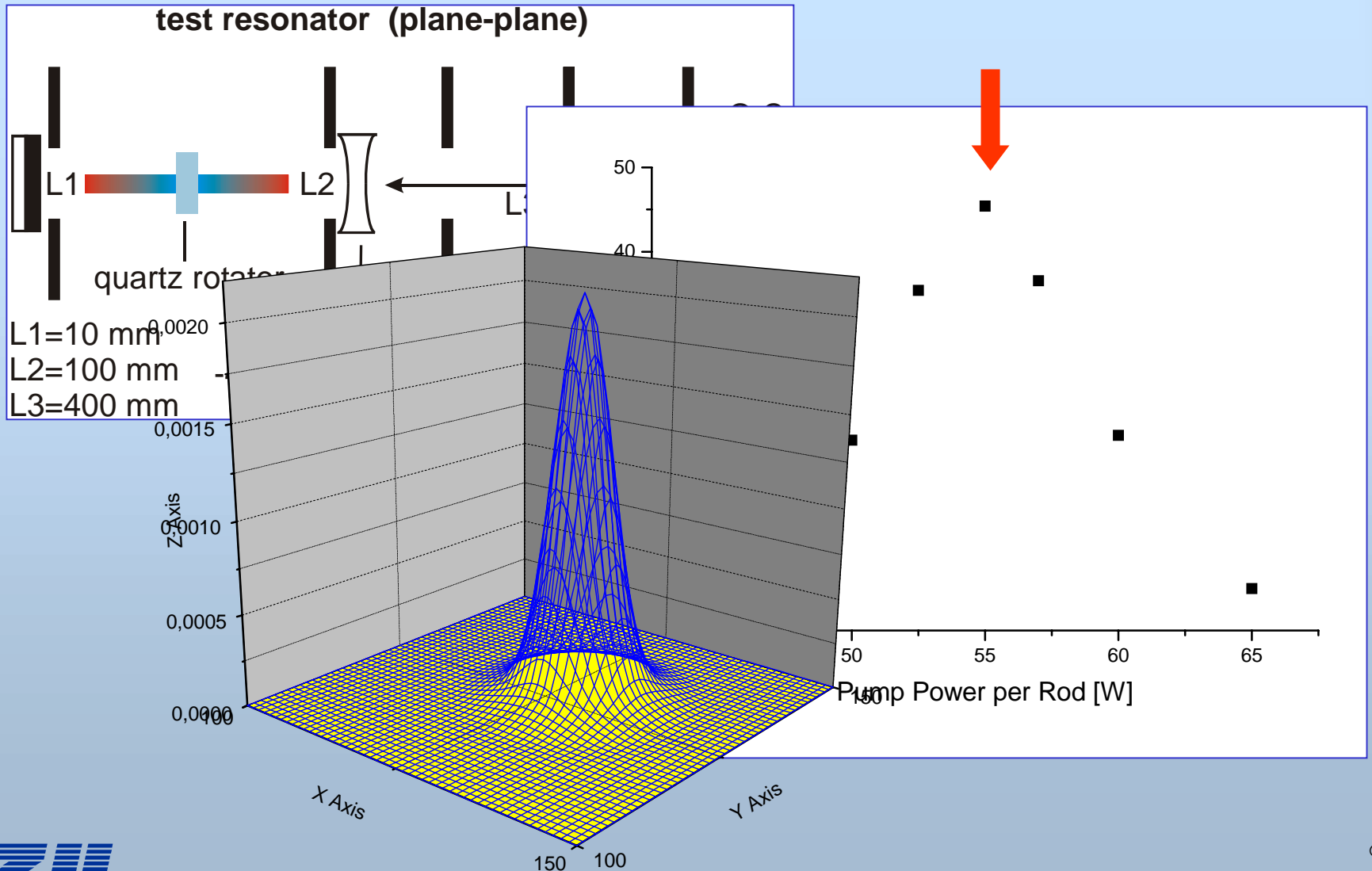


# First Results

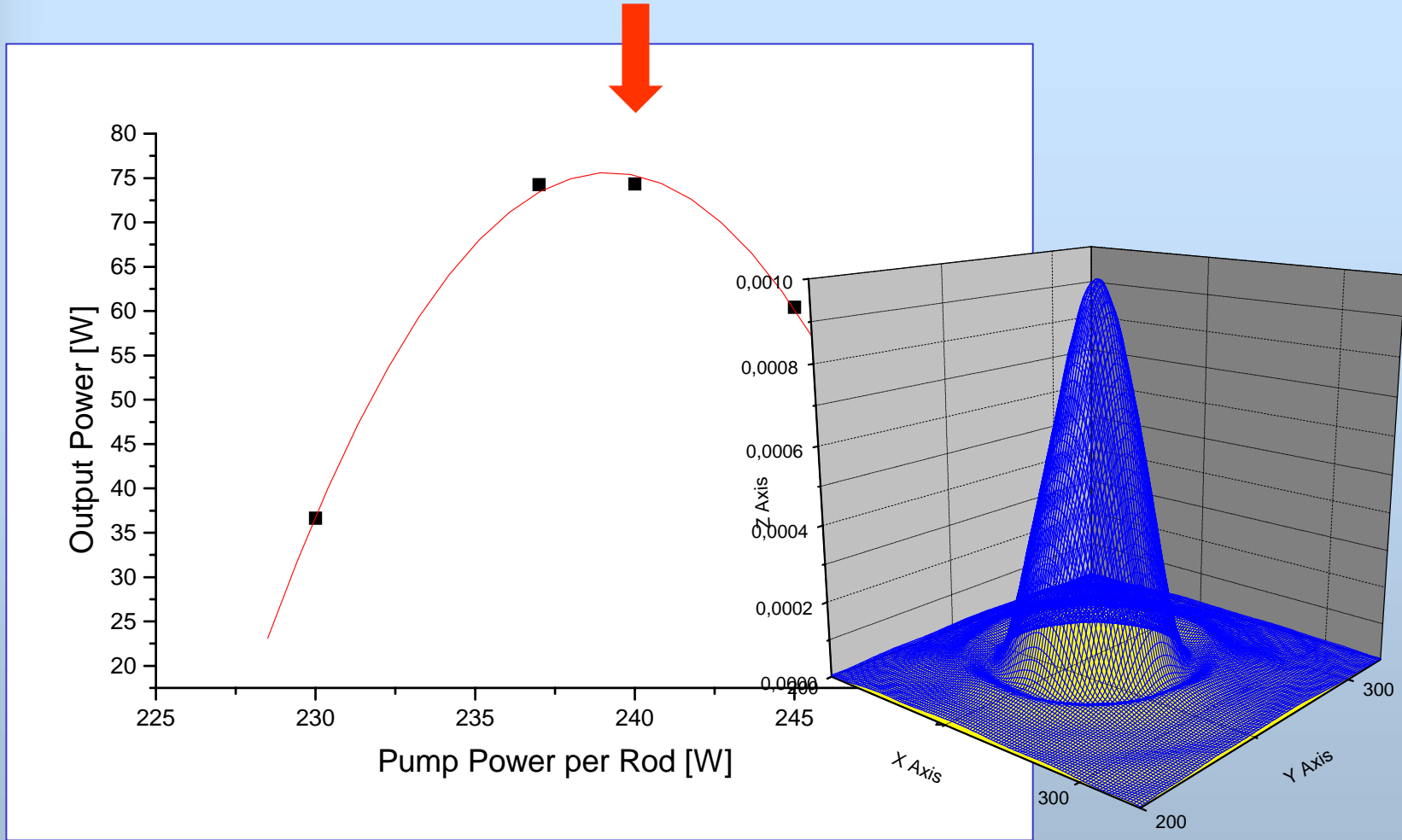


•polarisation eigenstates

# First Results/Birefringence Compensation

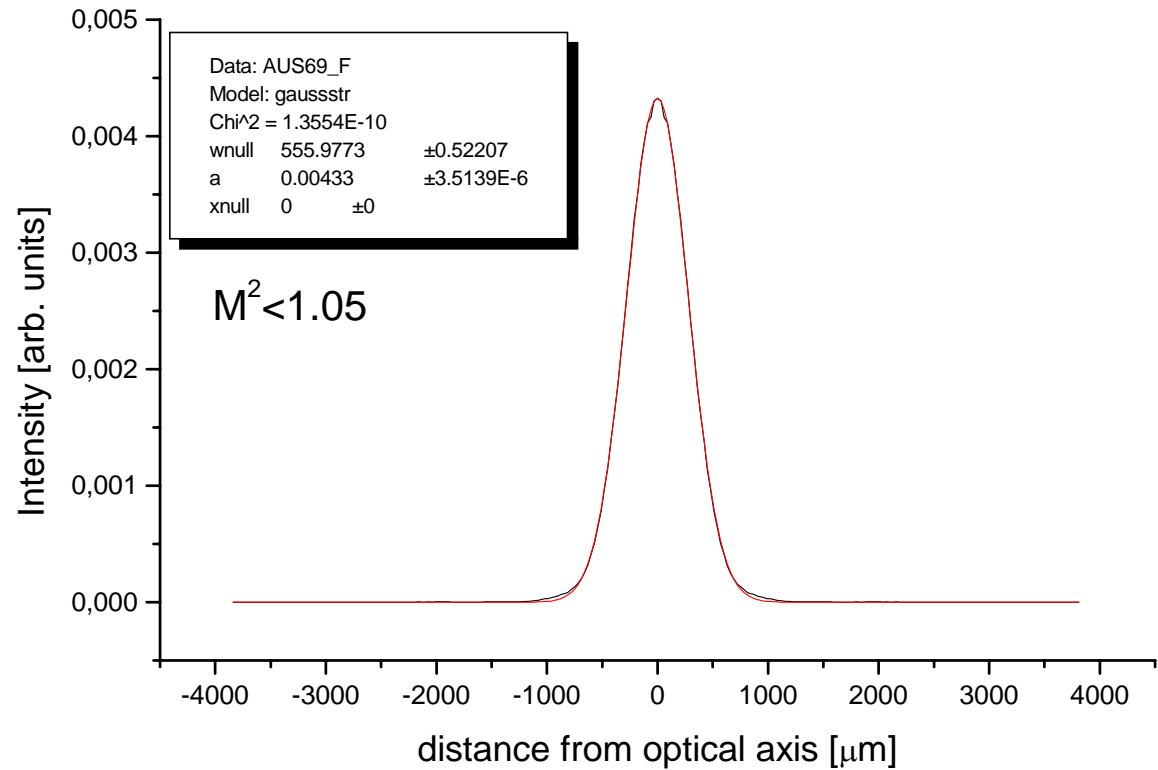
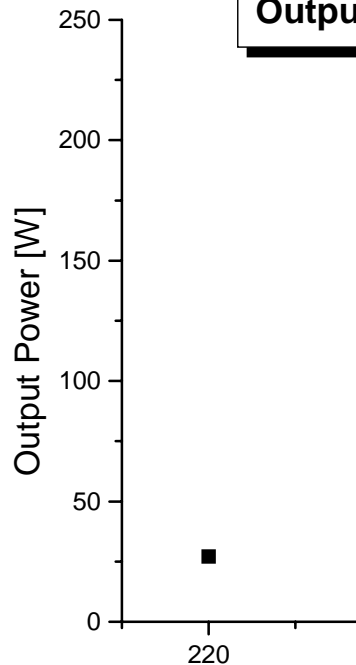


# First Results/100 W Head

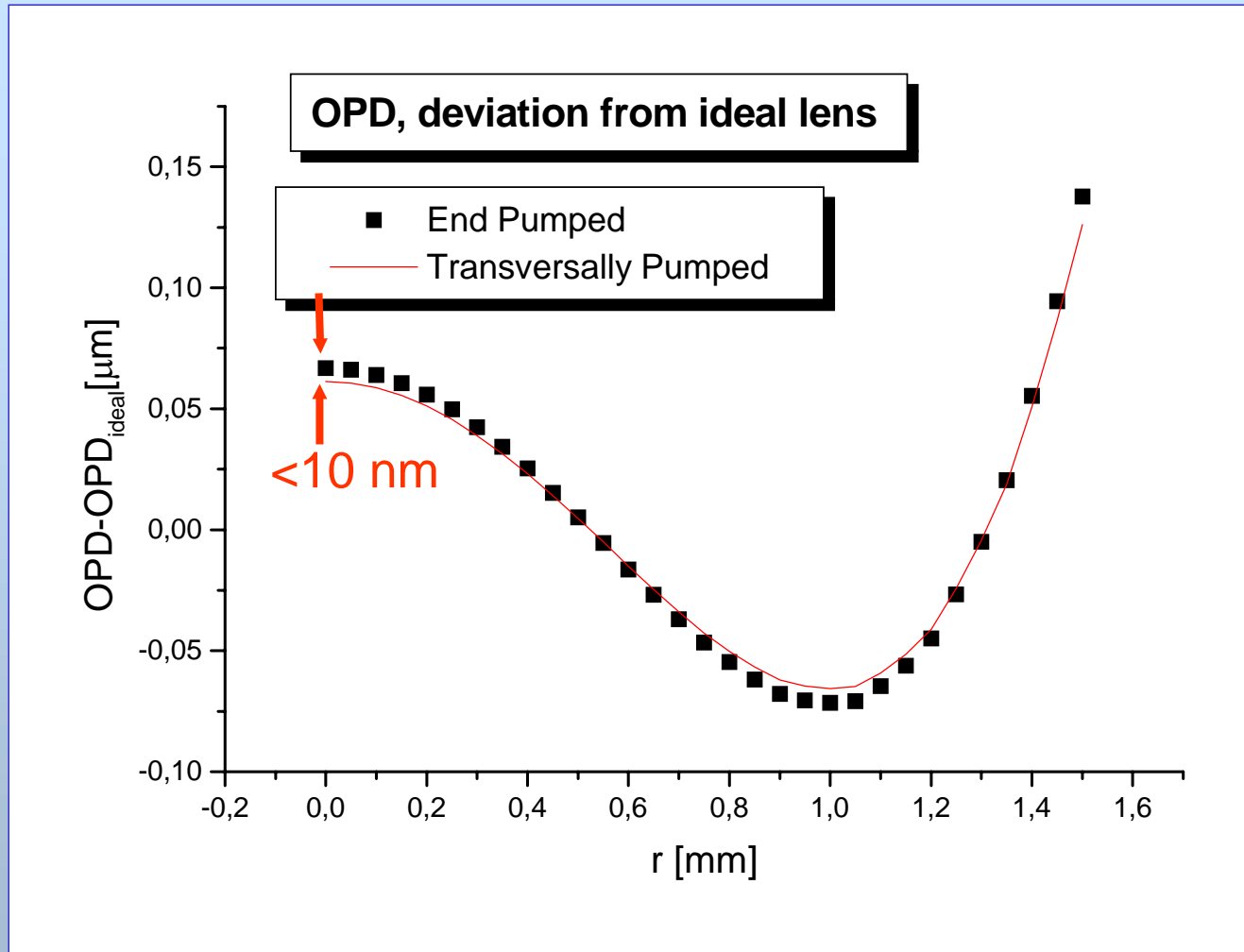


# First Results/100 W Head w/o Abberations

**Output Power vs. Pump Power**

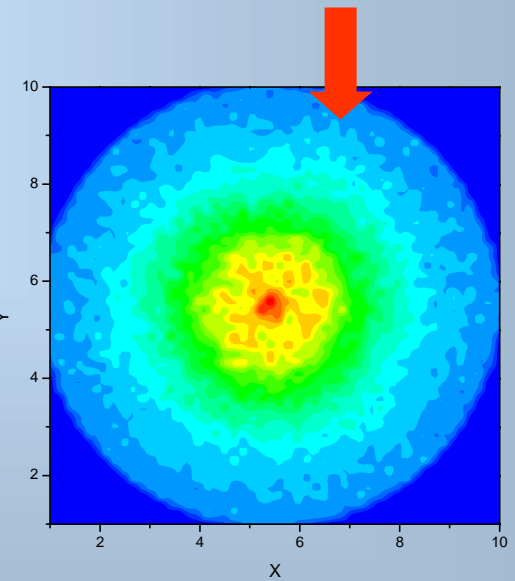
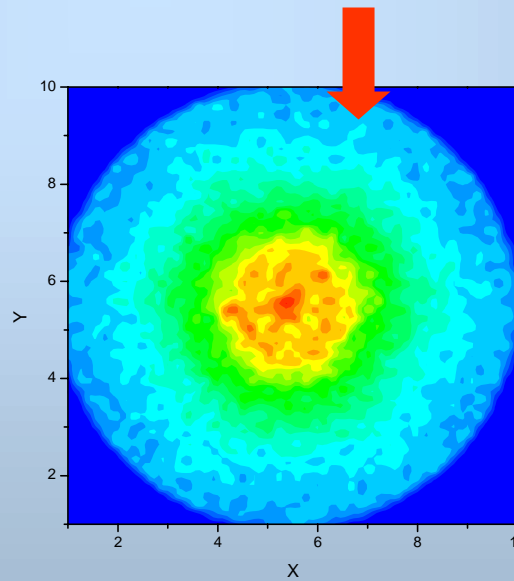
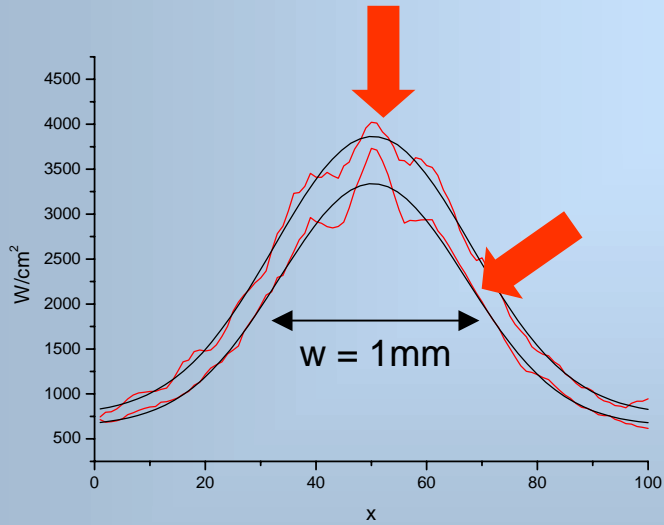
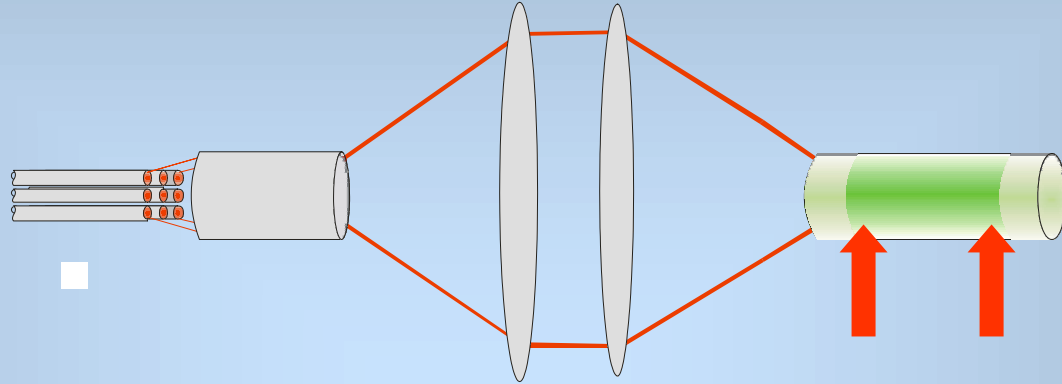


# Abberations/End Pumped vs. Transversally Pumped



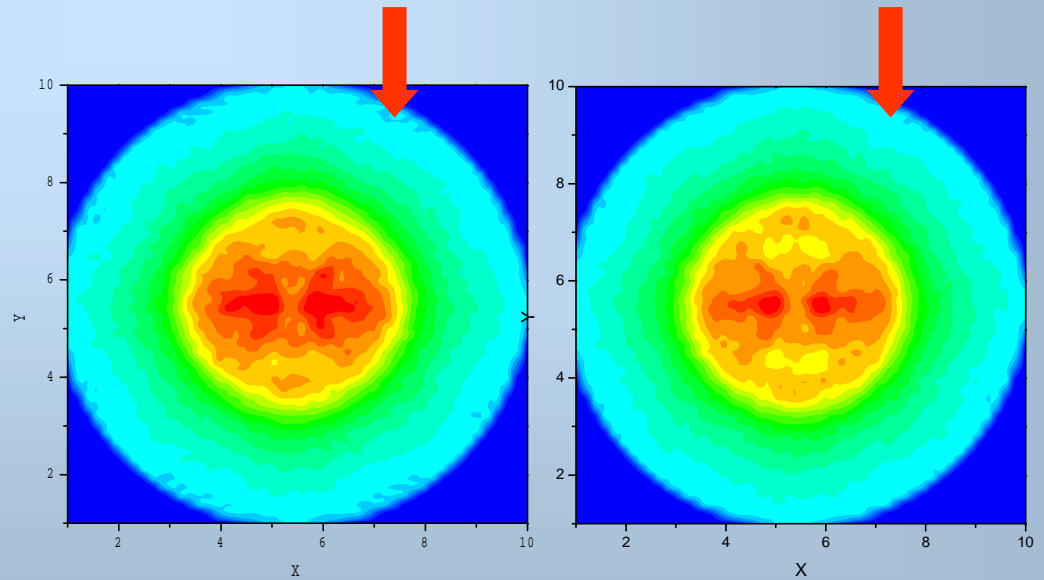
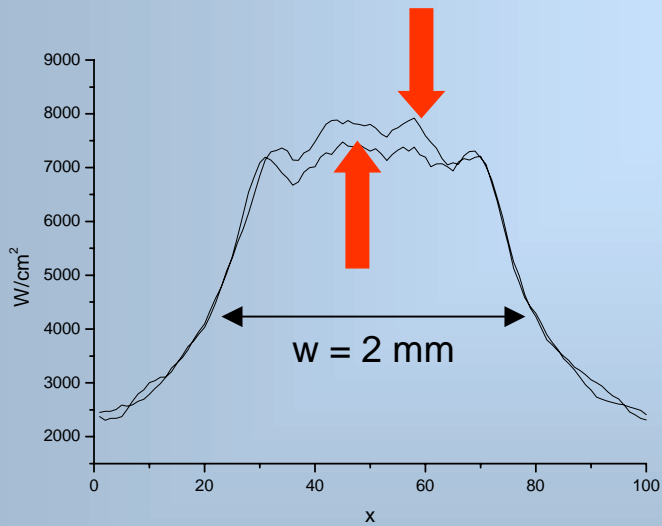
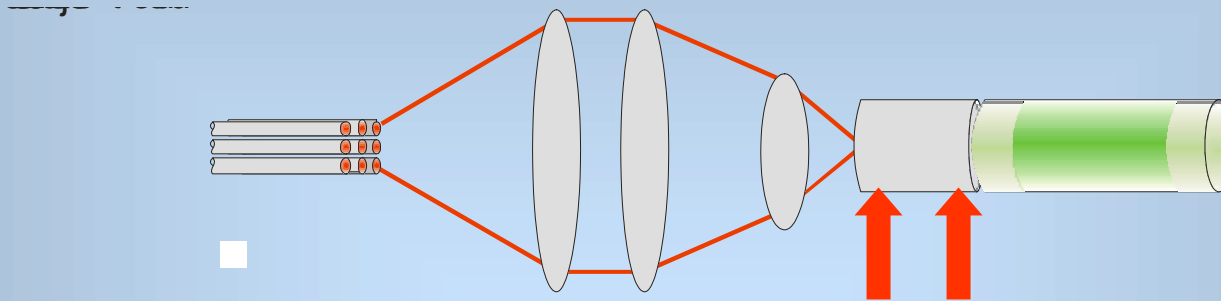
# Pump Concepts

## mode selective pumping



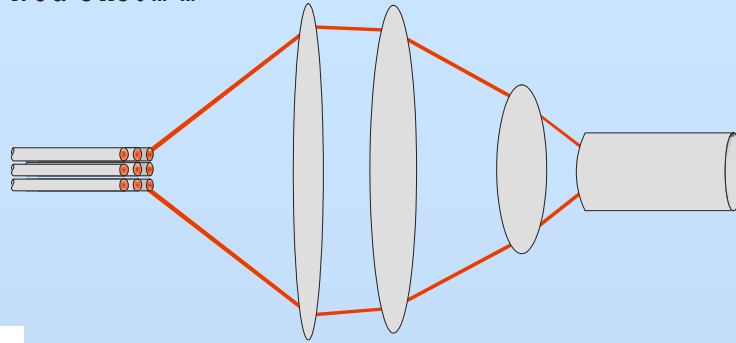
# Pump Concepts

## mode selective pumping

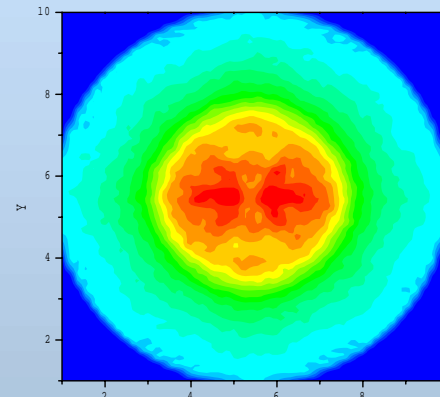
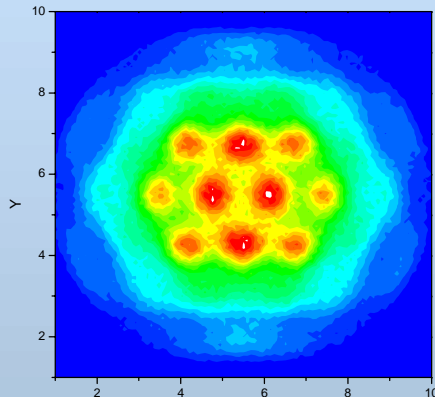




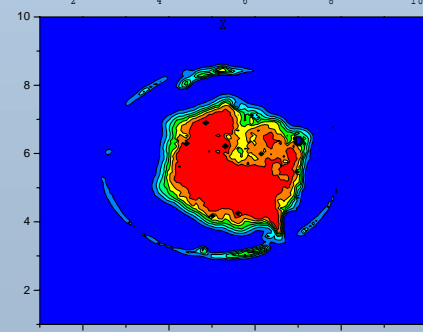
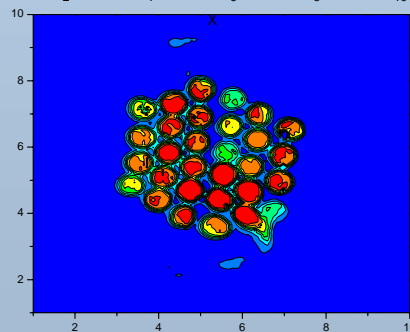
# Homogenization of Pump Light



simulation  
10 x 800  $\mu\text{m}$



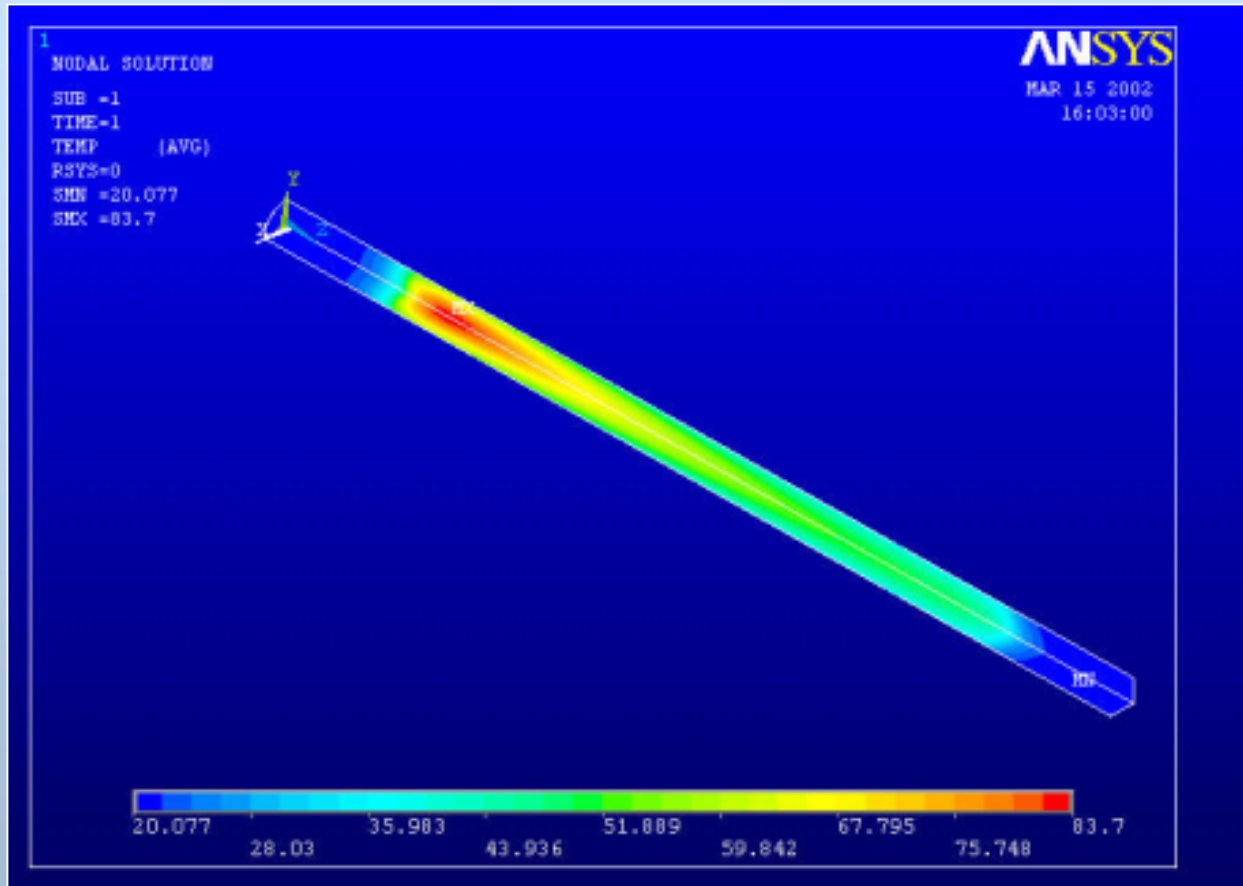
measured  
30 x 800  $\mu\text{m}$



# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

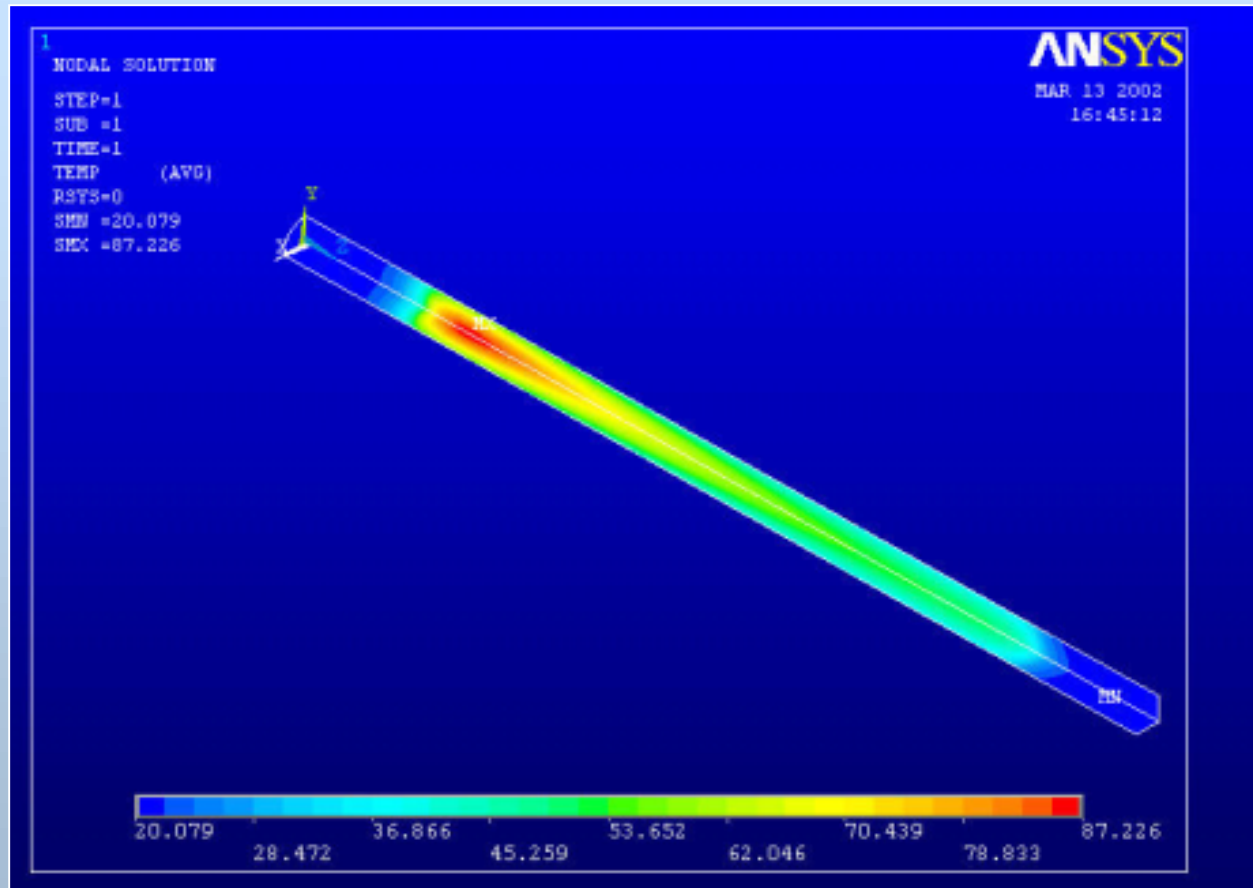
5000  $\mu\text{m}$



# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

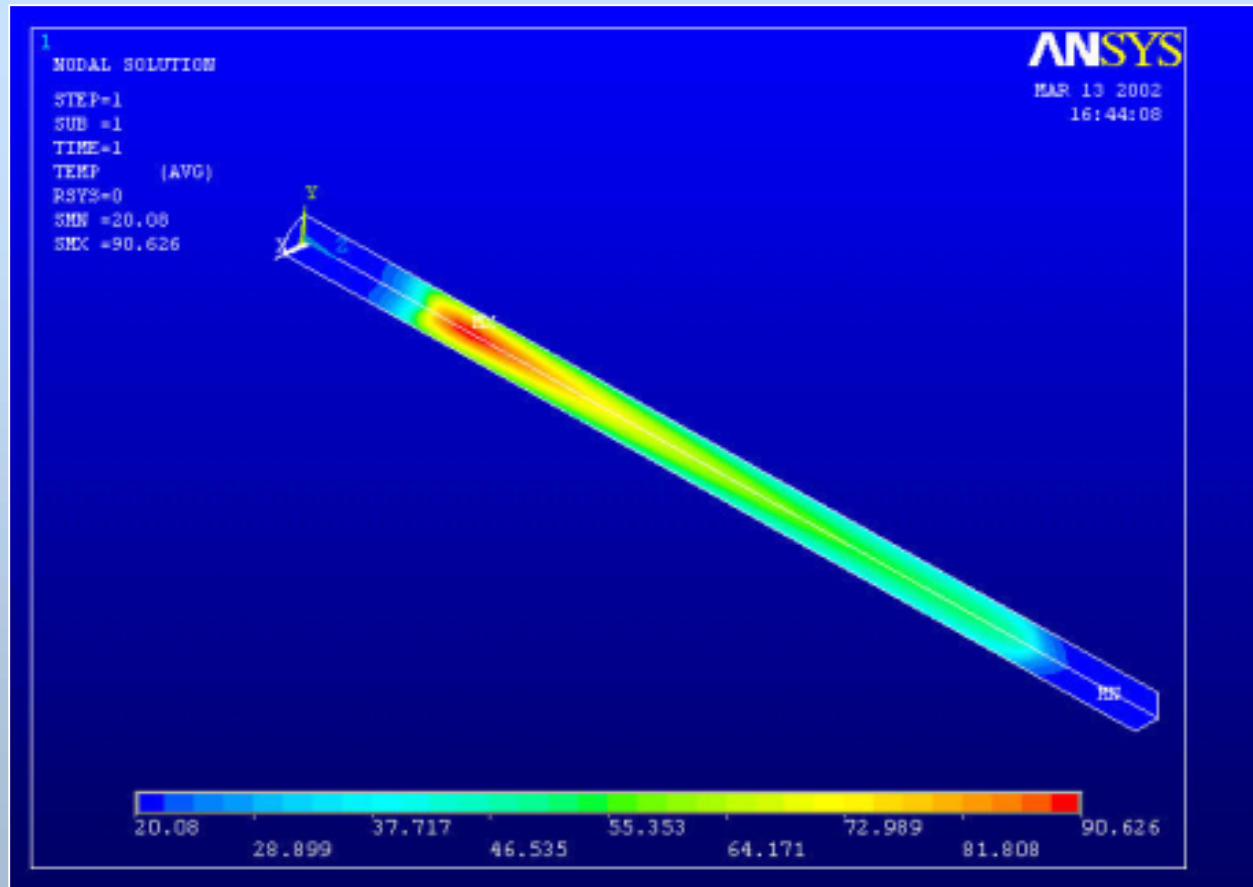
2000  $\mu\text{m}$



# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

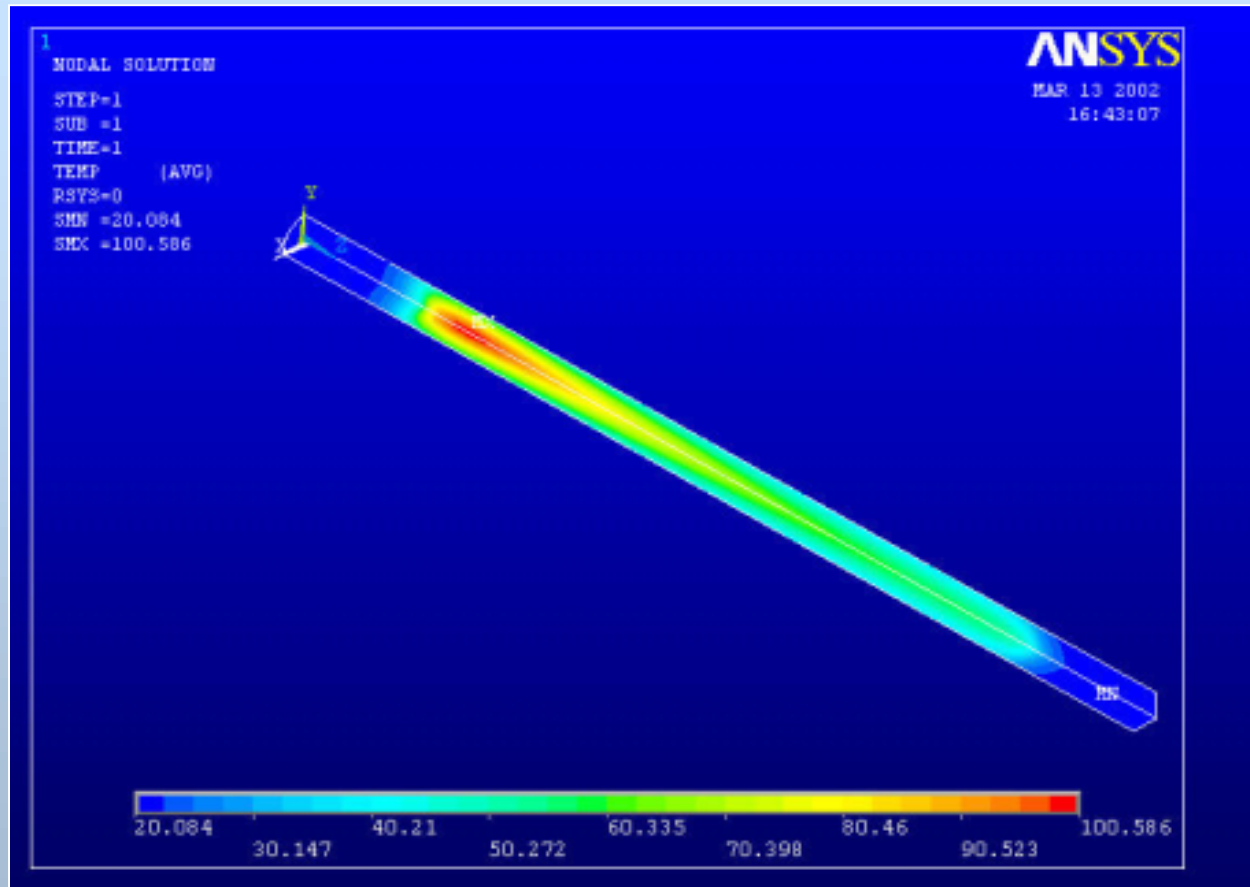
1500  $\mu\text{m}$



# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

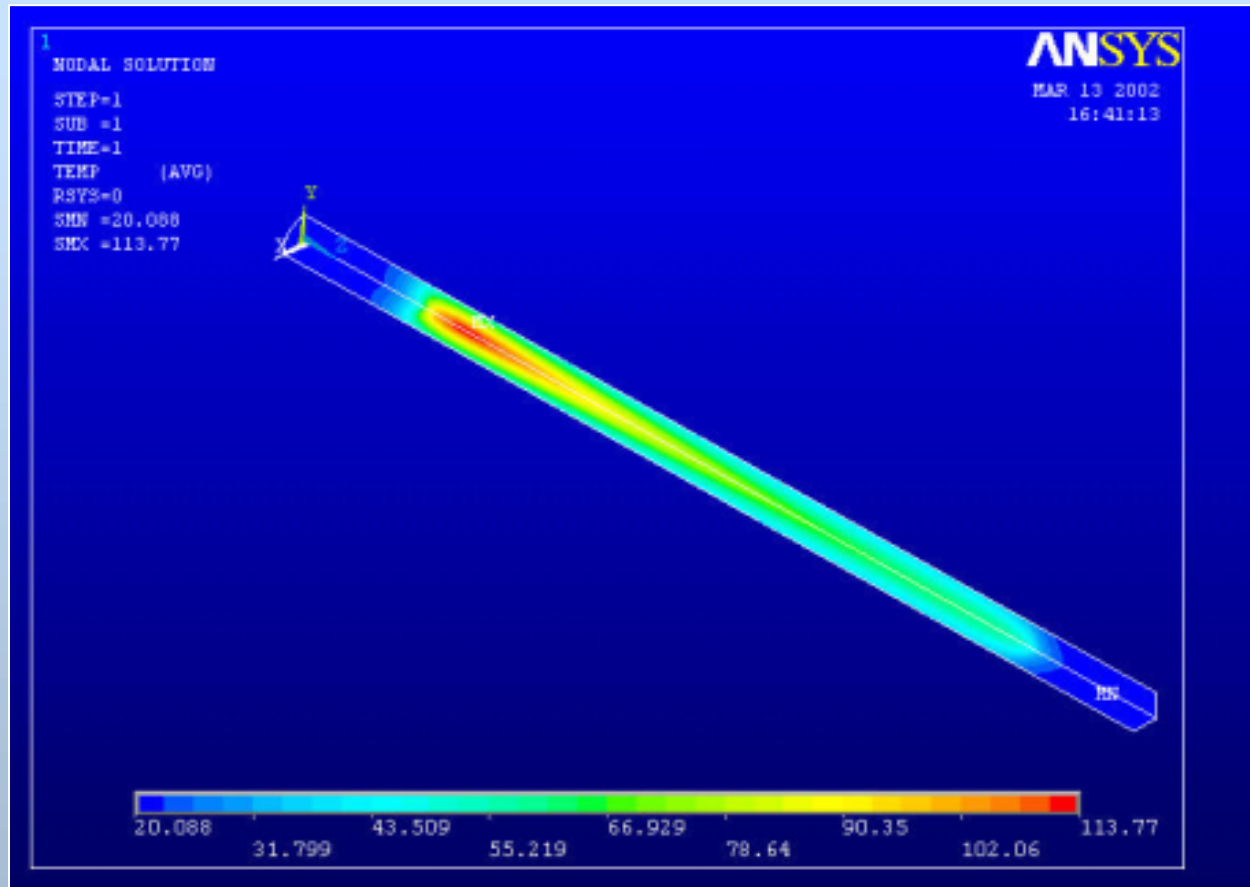
1000  $\mu\text{m}$



# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

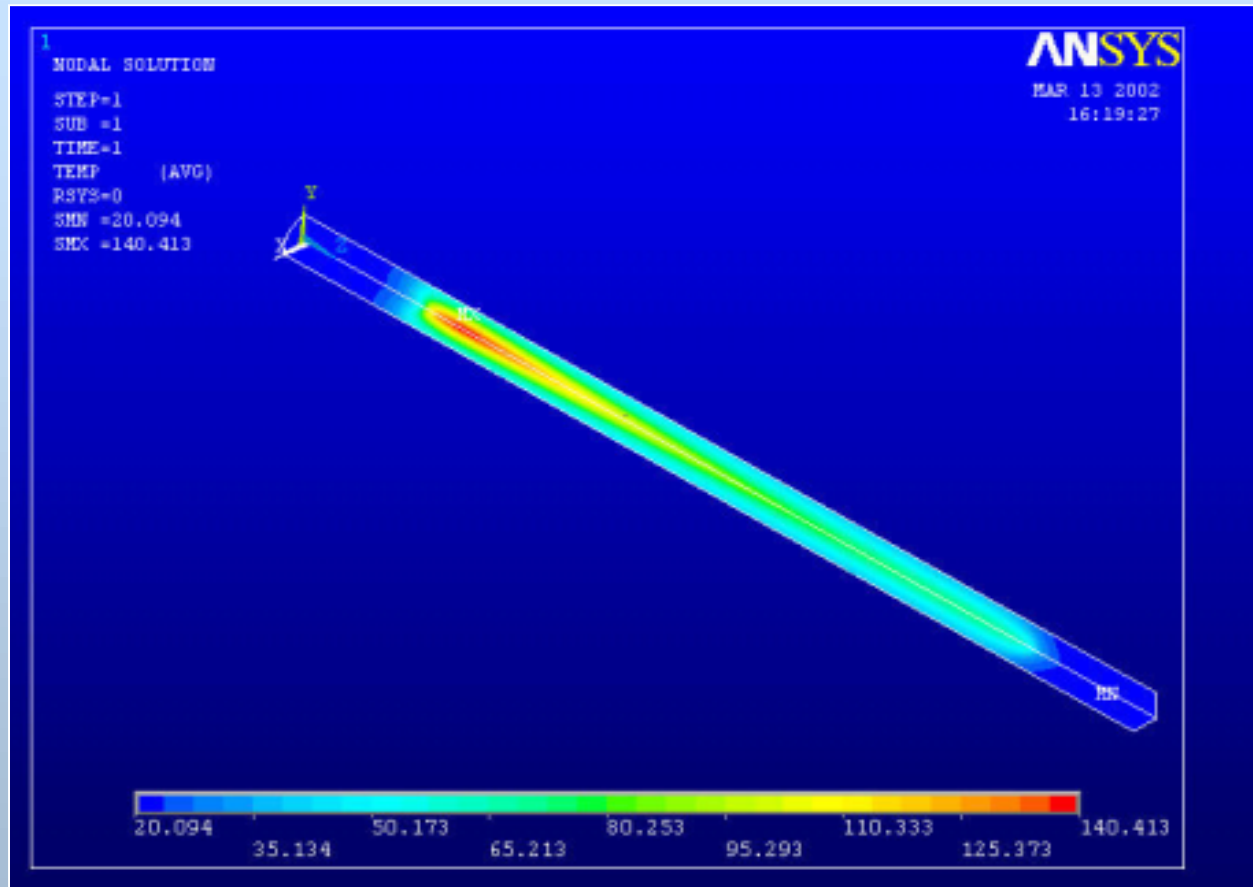
750  $\mu\text{m}$



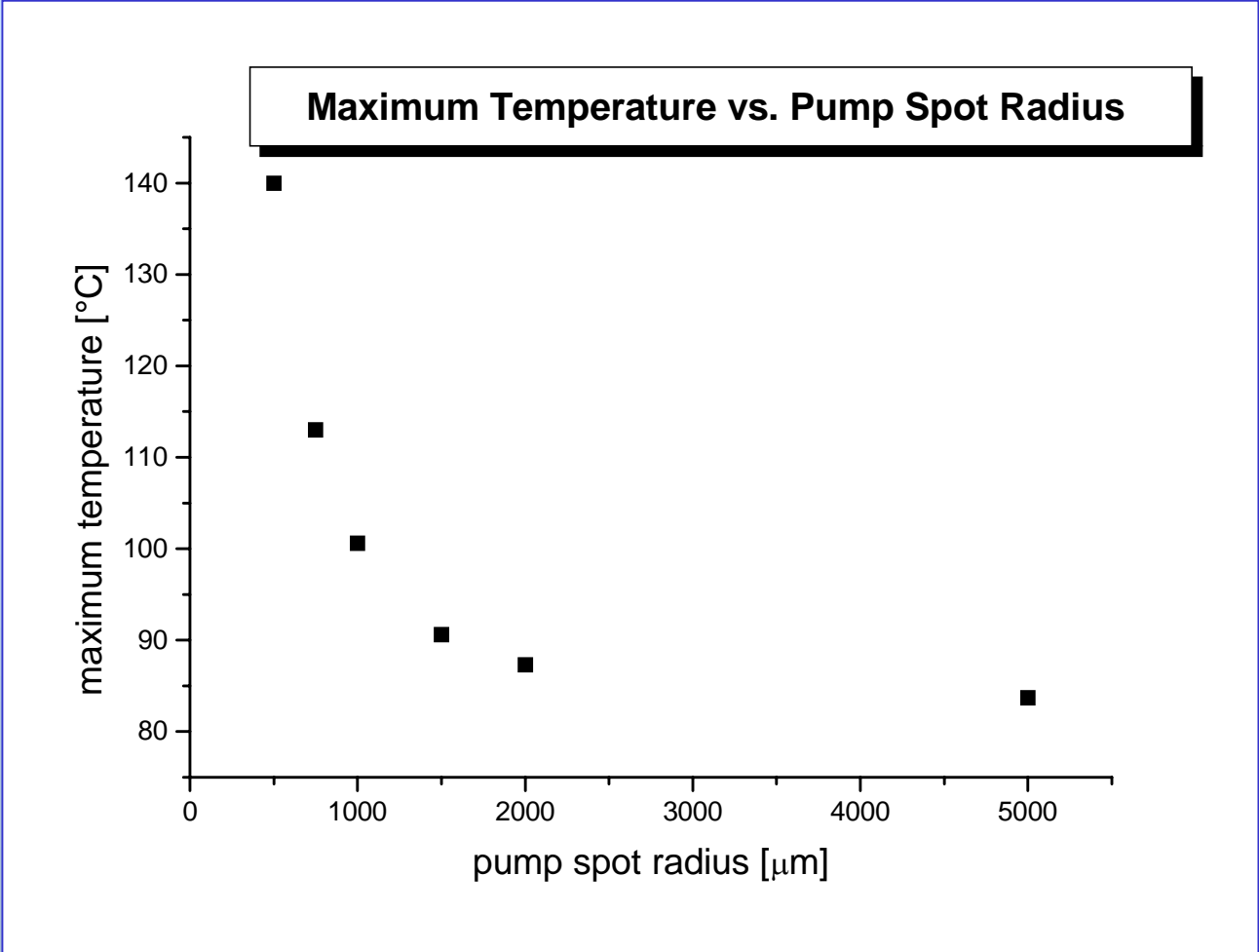
# Thermal Modeling/Temperature Distribution

varying with pump spot diameter (pump power kept constant)

500  $\mu\text{m}$



# Thermal Modeling/Maximum Temperature

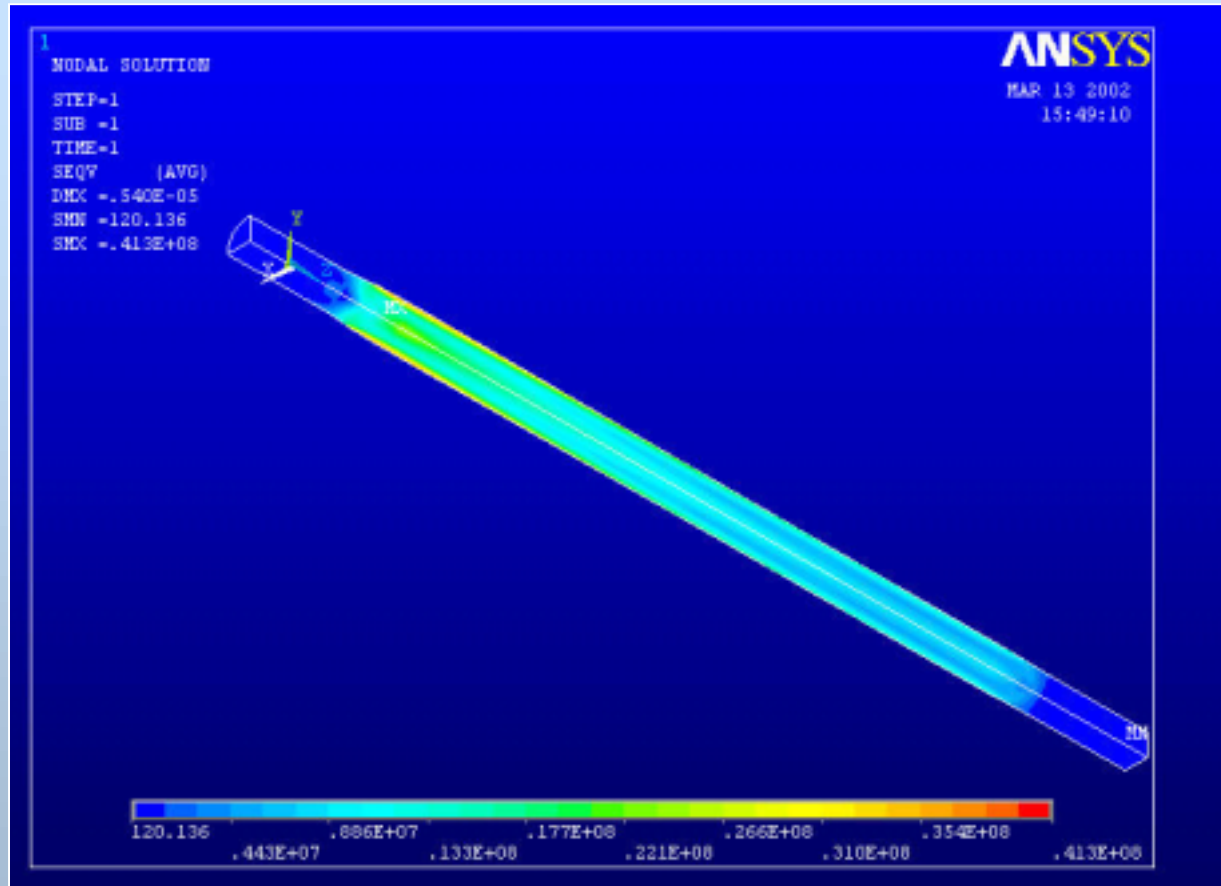




# Von Mises Stress

varying with pump spot diameter (pump power kept constant)

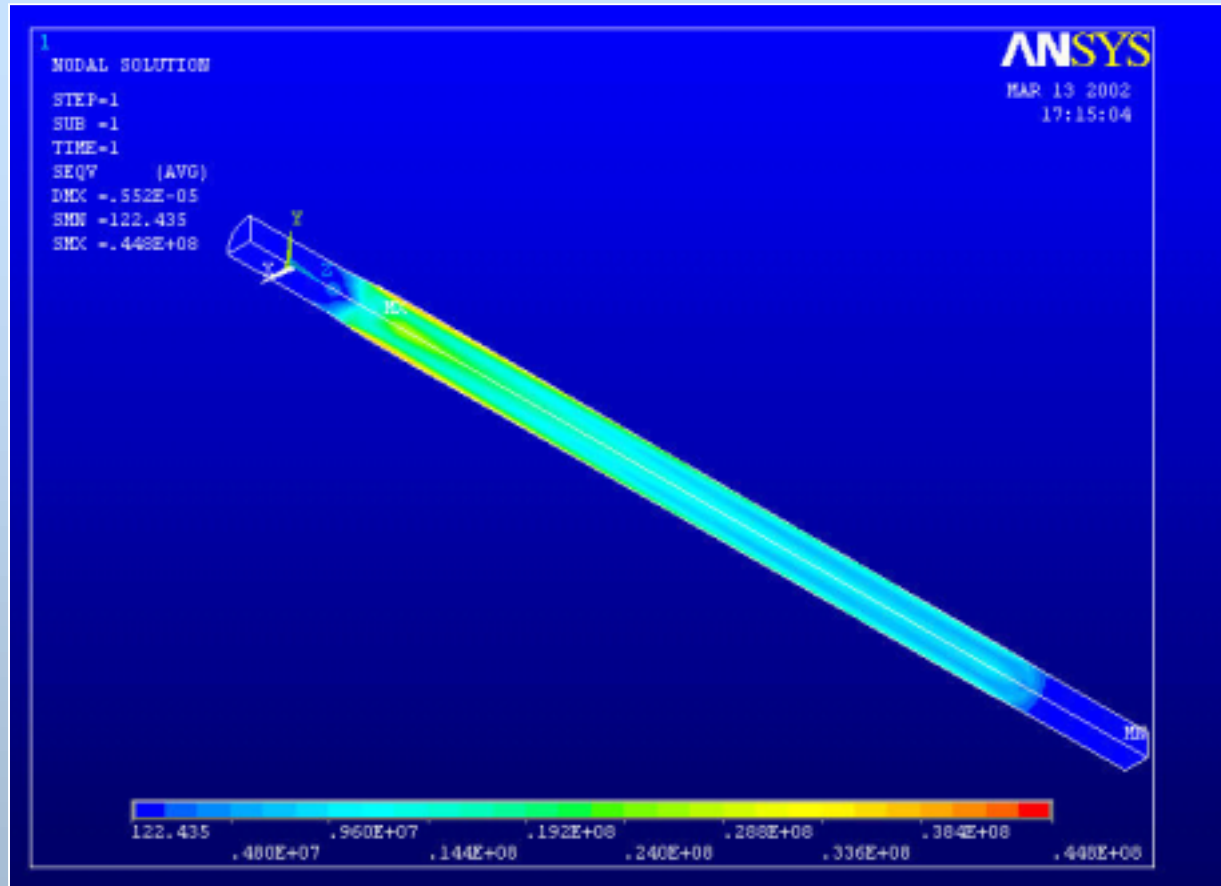
5000  $\mu\text{m}$



# Von Mises Stress

varying with pump spot diameter (pump power kept constant)

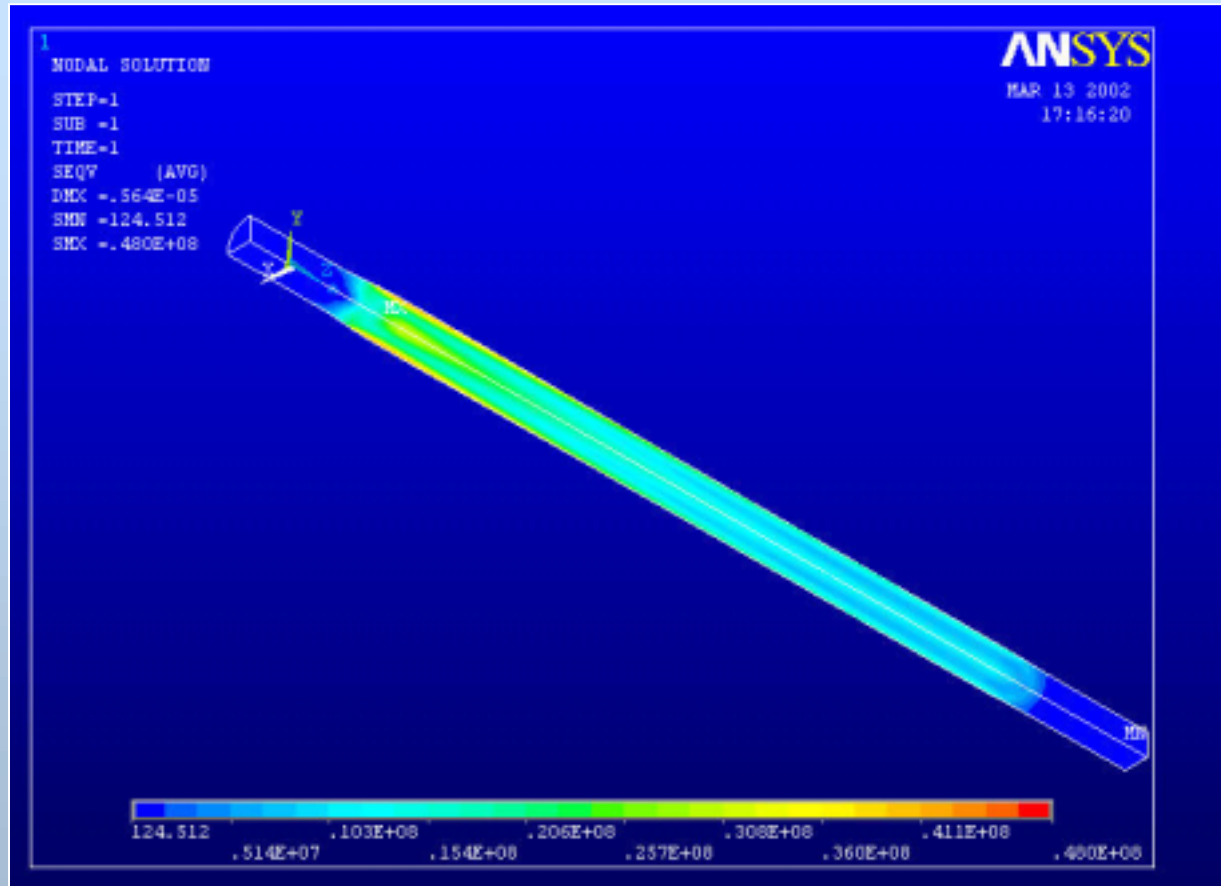
2000  $\mu\text{m}$



# Von Mises Stress

varying with pump spot diameter (pump power kept constant)

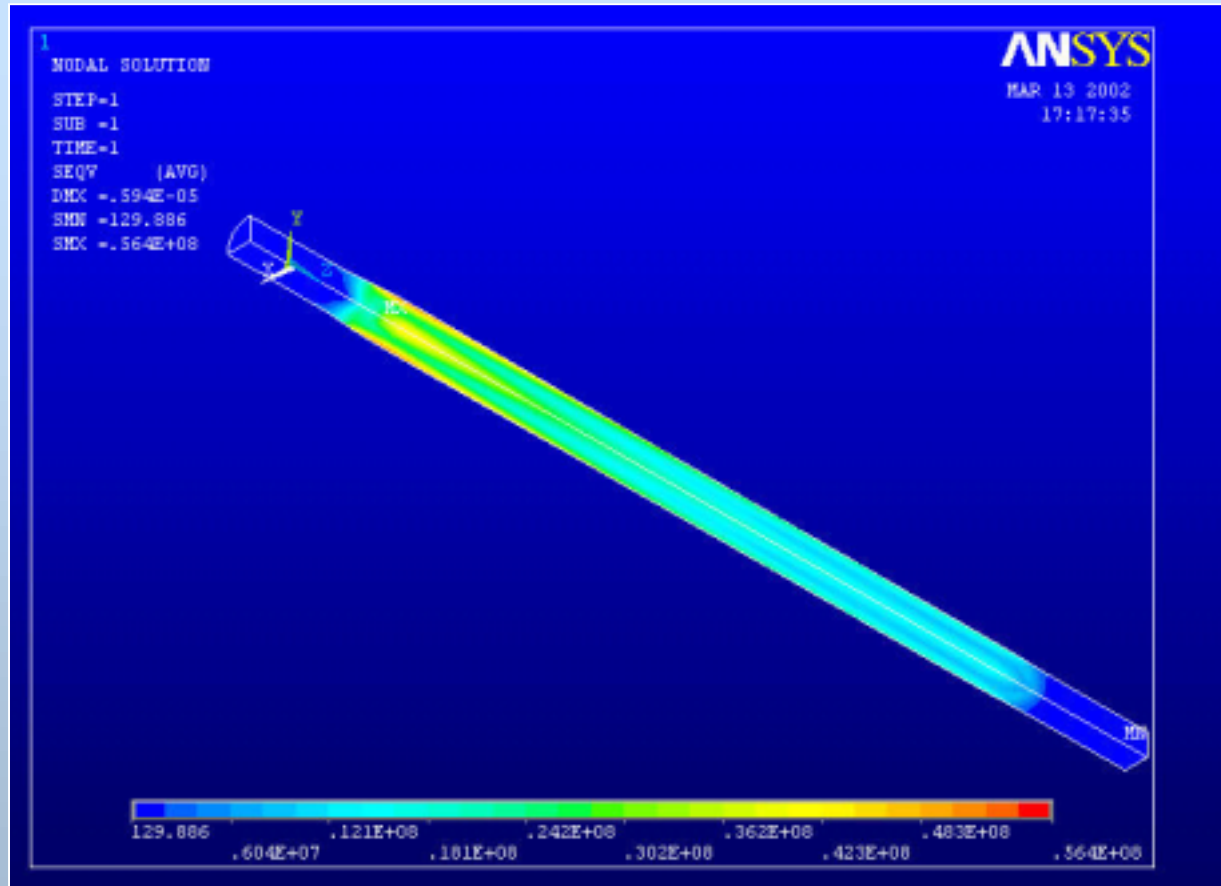
1500  $\mu\text{m}$



# Von Mises Stress

varying with pump spot diameter (pump power kept constant)

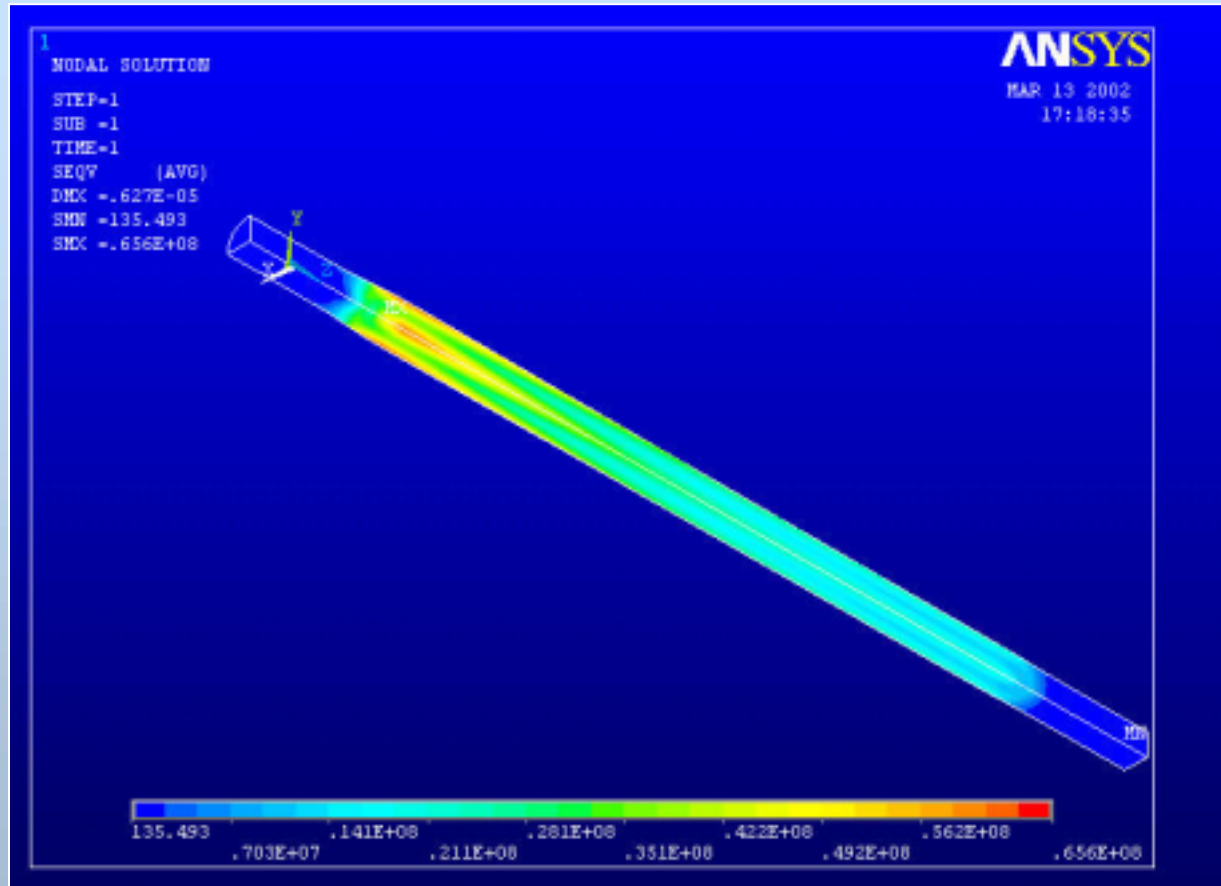
1000  $\mu\text{m}$



# Von Mises Stress

varying with pump spot diameter (pump power kept constant)

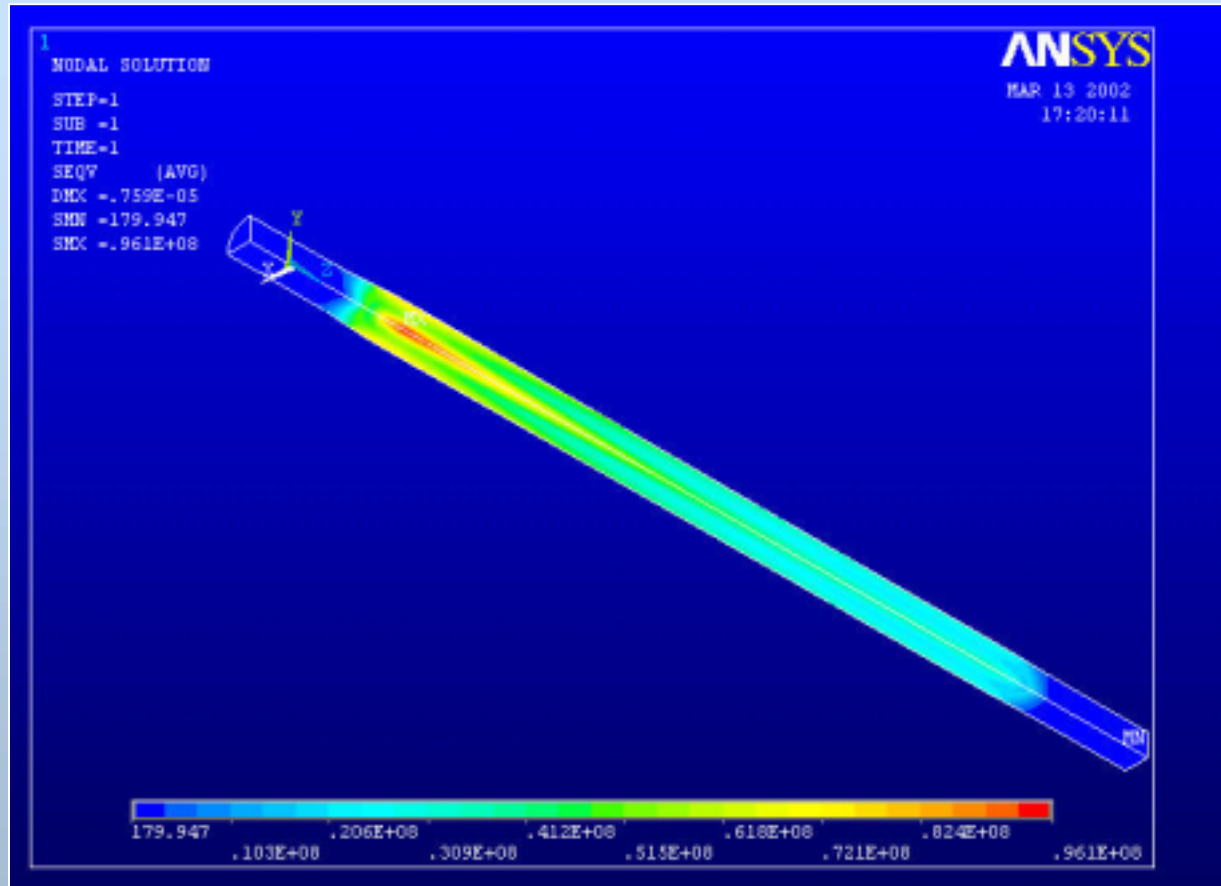
750  $\mu\text{m}$



# Von Mises Stress

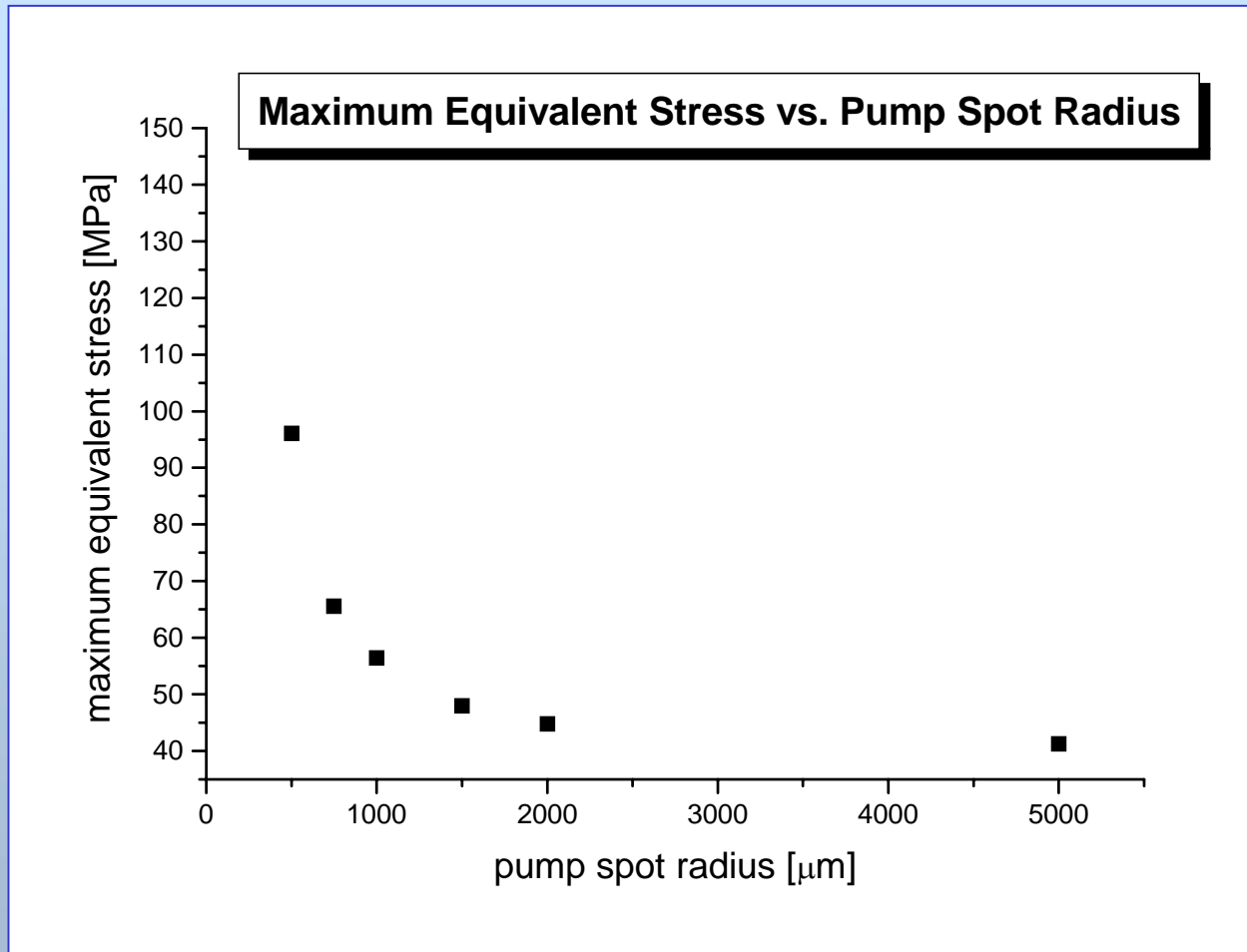
varying with pump spot diameter (pump power kept constant)

500  $\mu\text{m}$

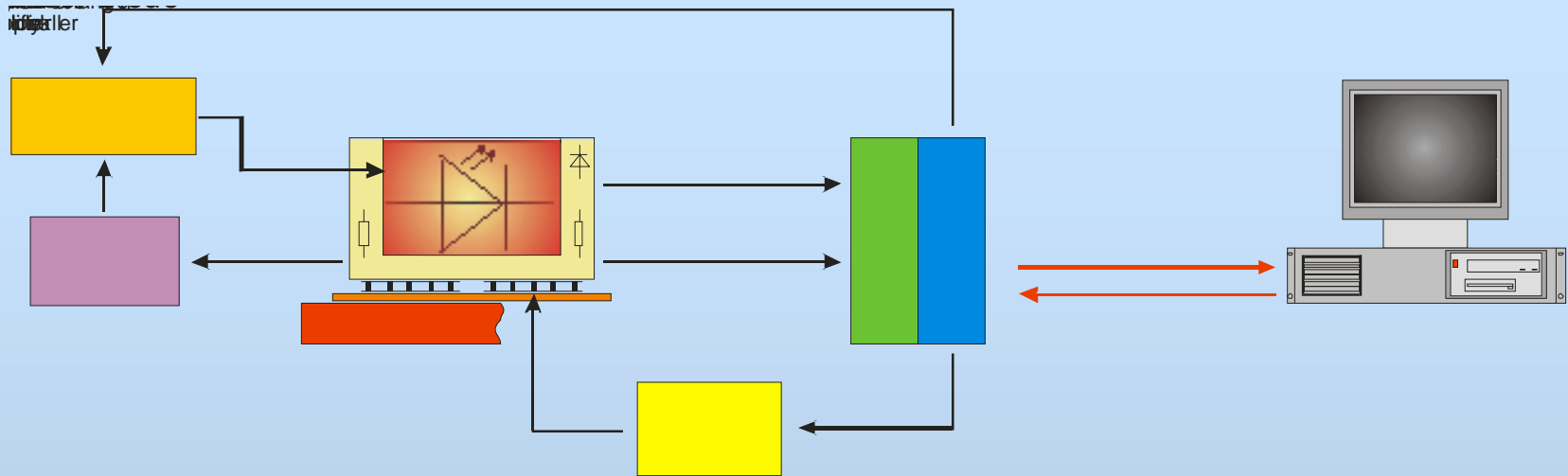


# Mechanical Stress/Von Mises Equivalent Stress

varying with pump spot diameter (pump power kept constant)



# Experimental/Diode Temperature Control



laser diode JENOPTIK 30 W, fiber coupled, NA 0.22; 800  $\mu\text{m}$

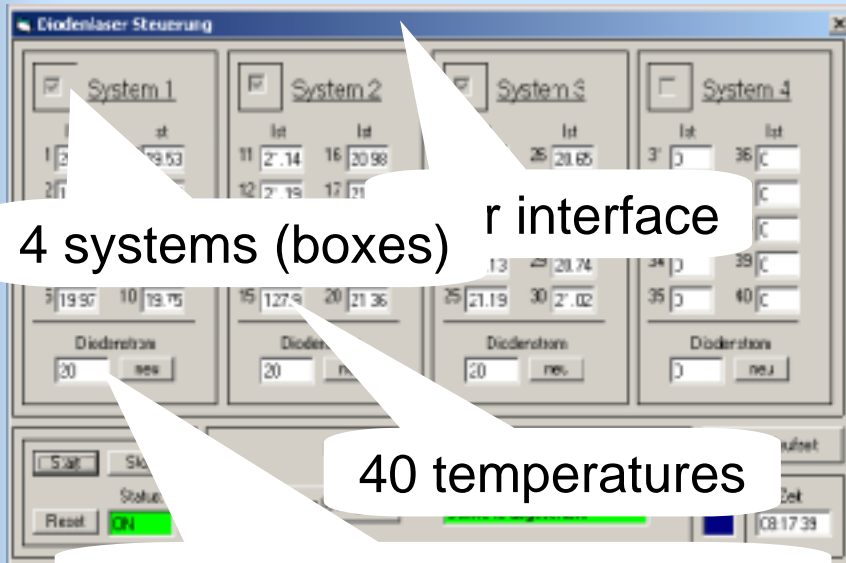
temperature resolution: 0.01K

temperature fluctuations: 2-3 digits

→temperature stability better than 0.05K



# Experimental/Diode Box

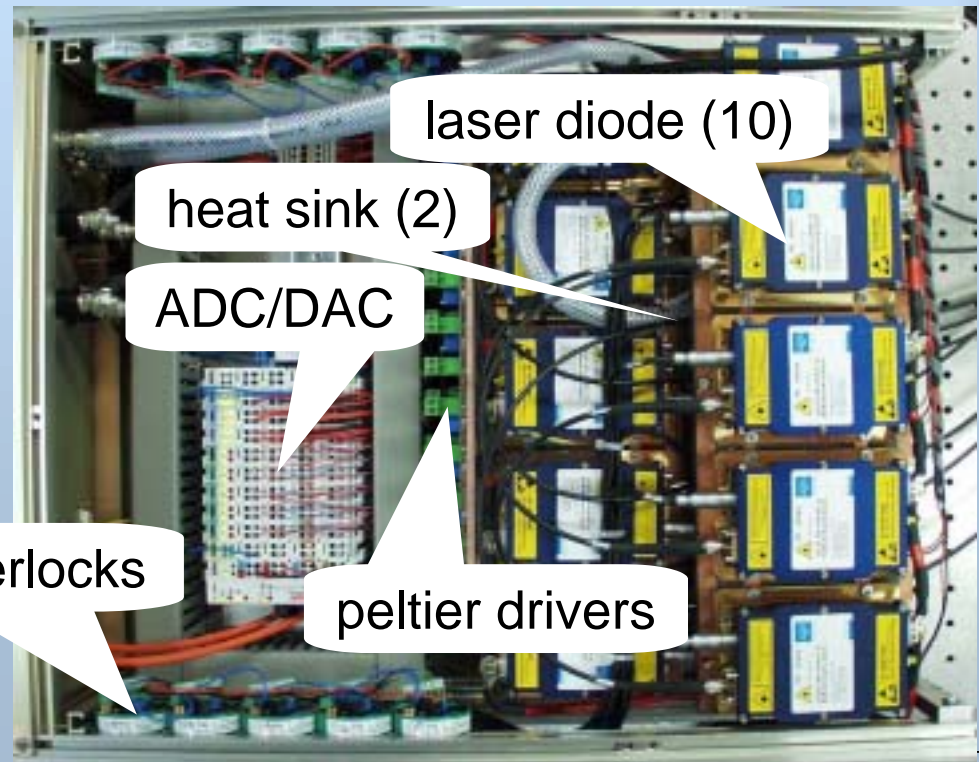


4 systems (boxes) r interface

40 temperatures

4 current controls (1 per box)

- 4 boxes
  - each 10 X 30 W fiber-coupled diodes
- 1200 W pump Power



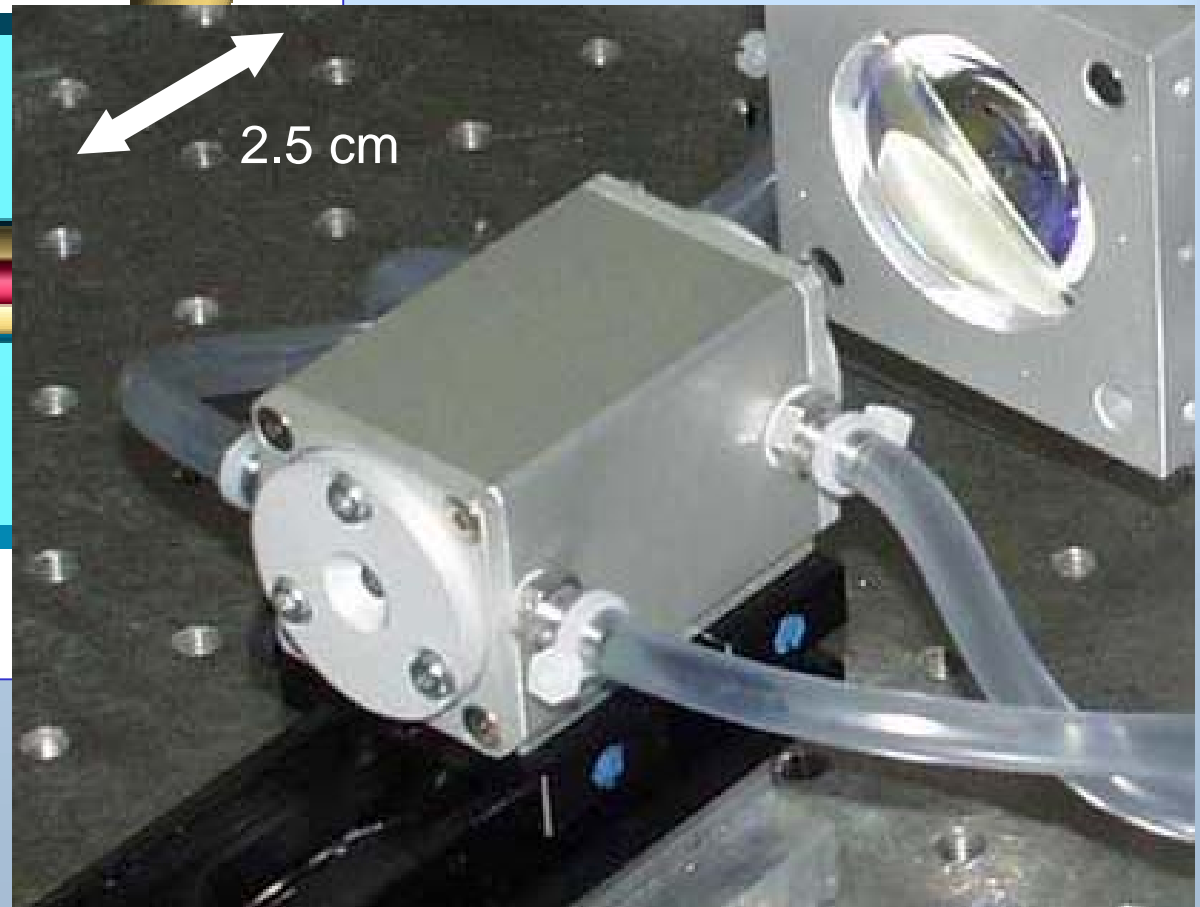
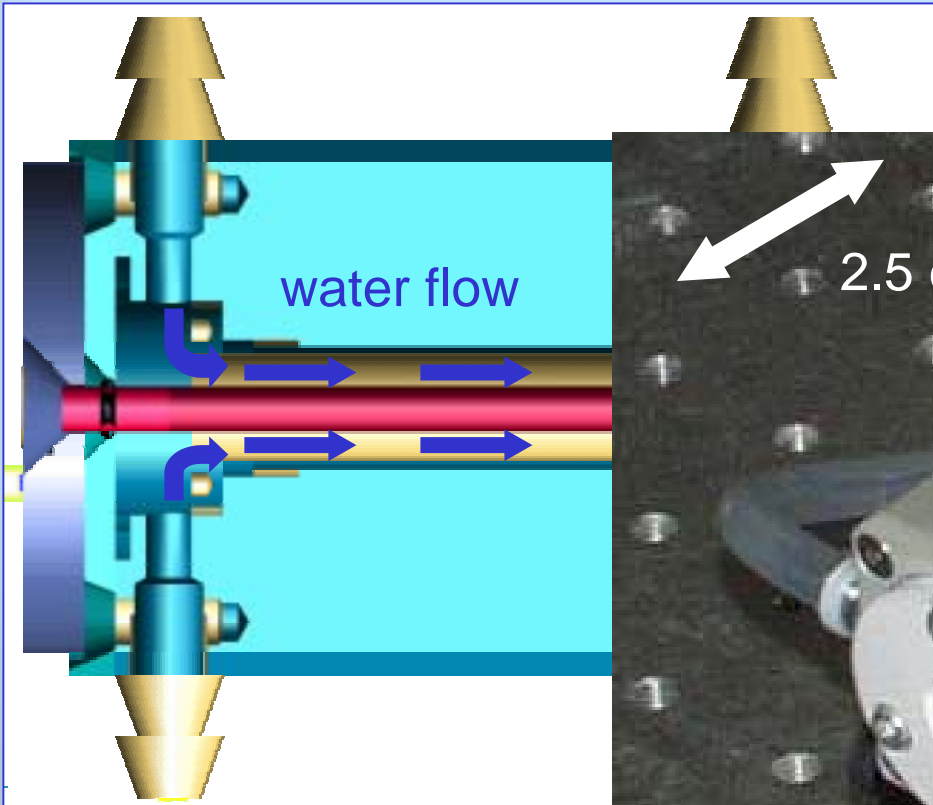
upcoming:

- 40 diode power measurements
- laser power control for each diode

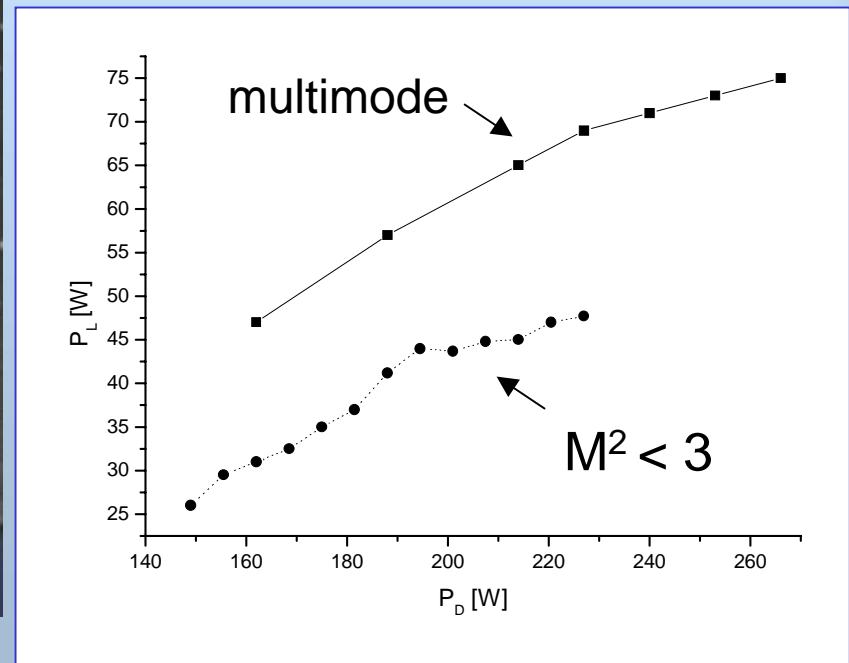
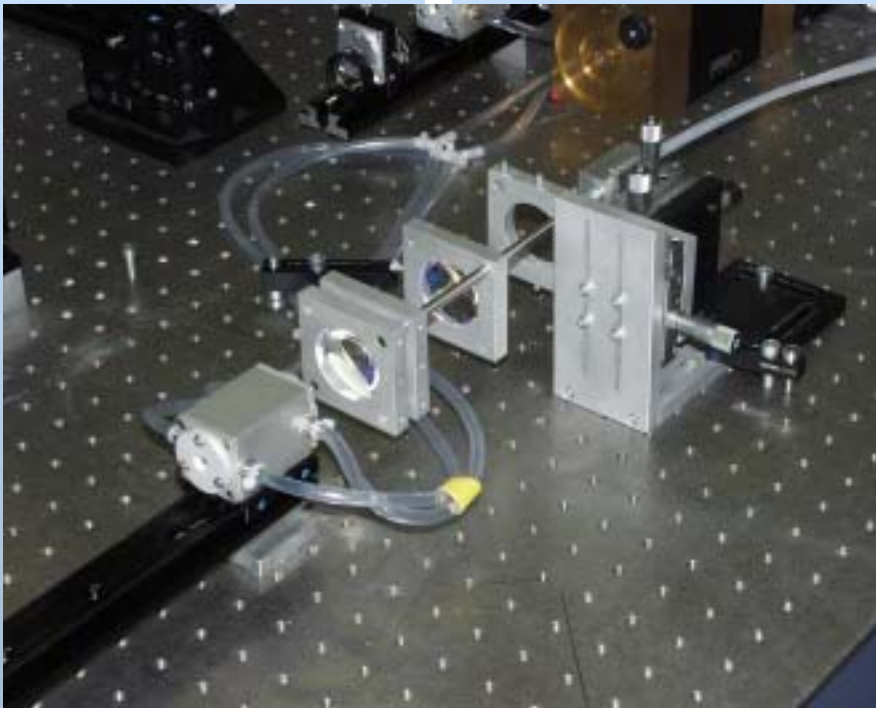
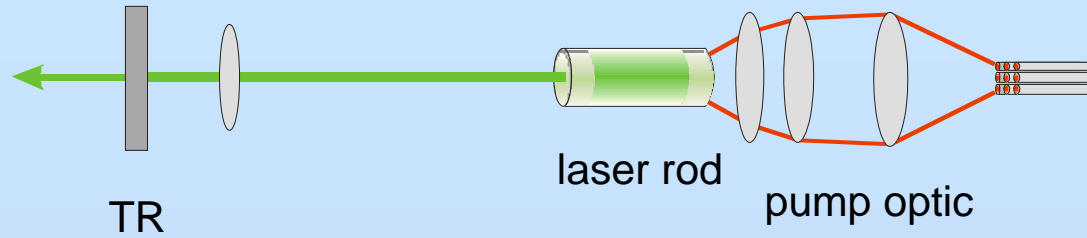
overtemp interlocks

peltier drivers

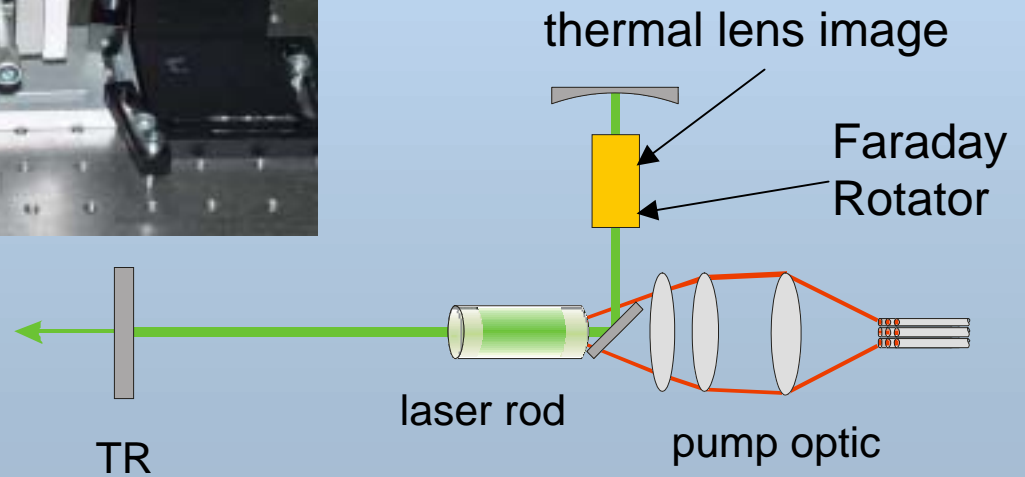
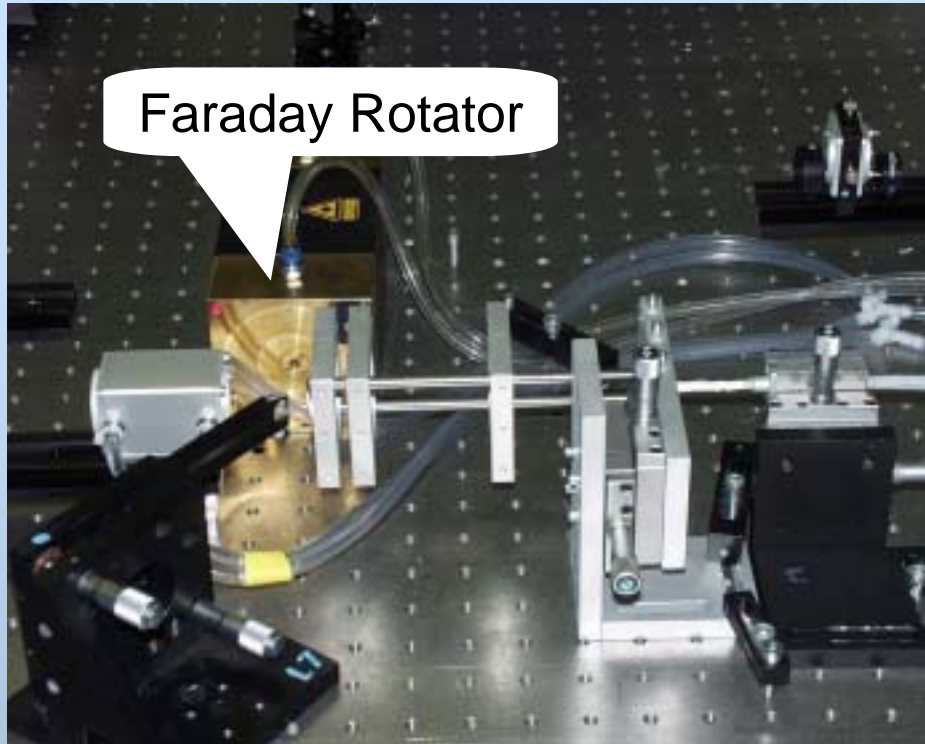
# Pump Chamber



# Pre-experiments



# Birefringence Compensated Resonator



# Resumé

## •Modeling

- 100 W of output power will be achievable
- abberations will have to be compensated for
- abberations are comparable in end pumped and transversally pumped rod

## •Experimental

- 4 diode boxes have been set up (1200 W of pump power)
- temperature stabilization works
- pump light homogenization has been demonstrated
- 45 W single mode and 75 W multi mode laser has been demonstrated (single rod, no compensation)

# Outlook

- optimize overlap of pump light distribution and mode diameter
- compare calculated aberrations to experiment (Shack-Hartmann sensor, diploma thesis P. Huke)
- evaluate conductive cooling (coating of rod's shell)
  - reduce aberrations (lower absolute temperature)
  - avoid contact of cooling fluid with rod
- compensate for aberrations



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