



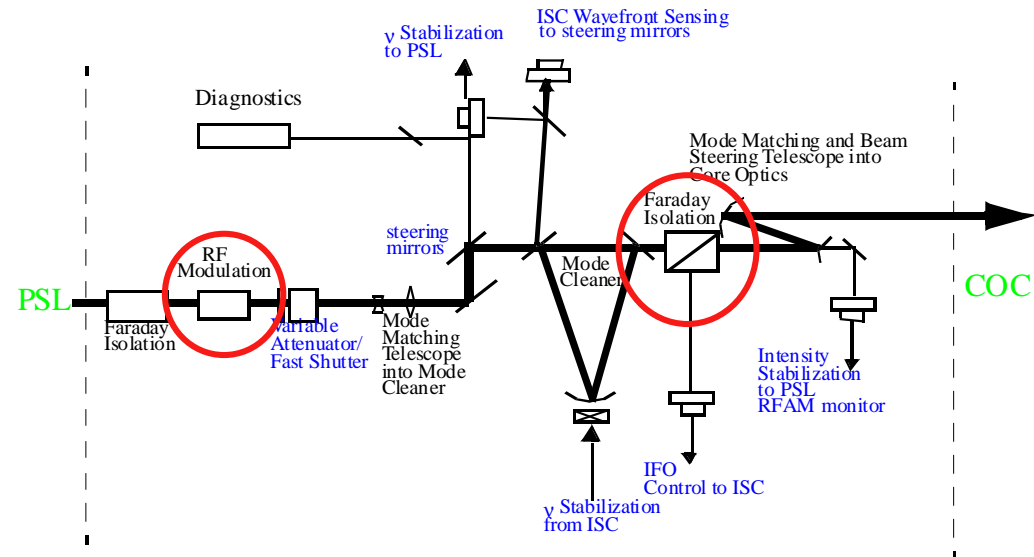
*Thermal Headaches in Advanced
LIGO Input Optics*

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Input Optics Functions

- **RF Modulation**
- **Mode Cleaning**
- **Mode Matching**
- **Optical Isolation**
- **Distribution of Control Beams**
- **Self Diagnostics**



<i>Parameter</i>	<i>LIGO I</i>	<i>Advanced LIGO</i>
Laser Power	8.5 W	180 W (150 W)
Overall IO Efficiency (TEM₀₀)	75%	66%
Optical Isolation	70 dB	(> 85 dB)

The Challenge

Advanced LIGO will operate at 180W CW powers - “presents some challenges”:

- Thermal Lensing --> Modal Degradation

$$\zeta = \alpha L \frac{dn}{dT} P / 2 K \lambda \quad z = 1 + i \zeta$$

$$\vec{E} = M(\zeta, z) \cdot \vec{E}$$

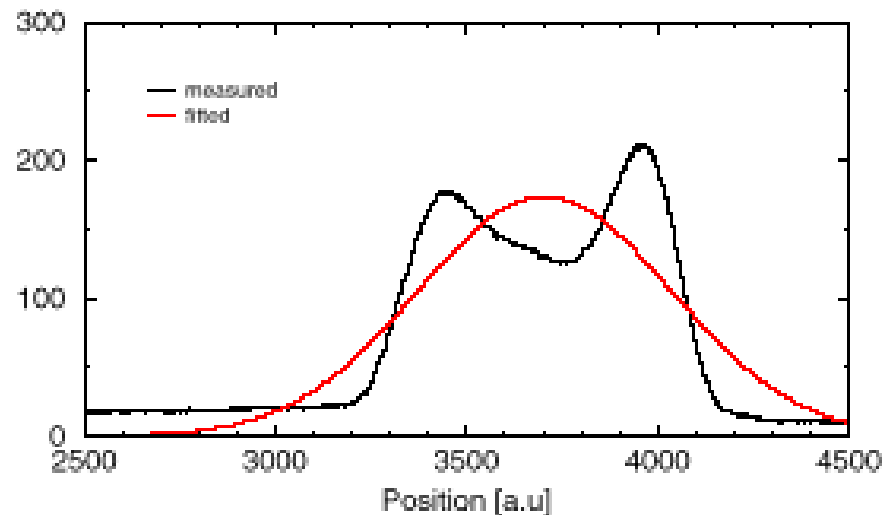
- Thermally induced birefringence

- FI- loss of isolation
- EOM - spurious amplitude modulation

- Damage

- Other (nonlinear) effects (SHG, PR)

LiNbO₃ at 30W:



5 x 5 x 40 mm LiNbO₃ EOM - thermal lensing is:

- severe
- position dependent

Characterization of thermal lensing

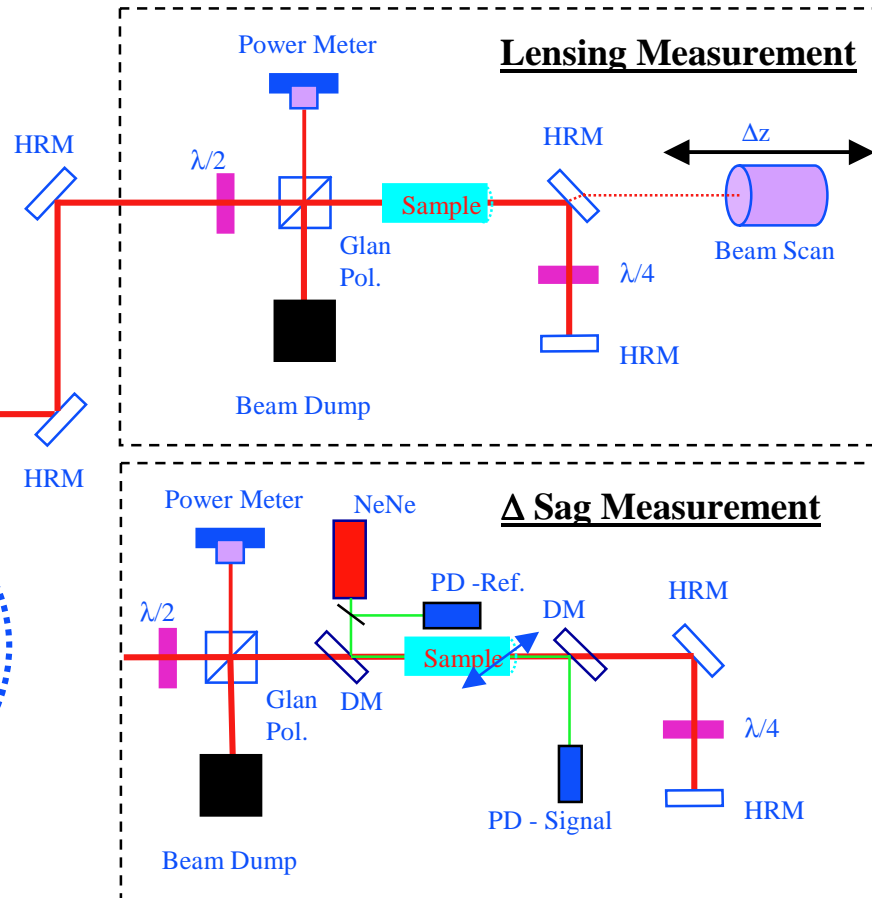
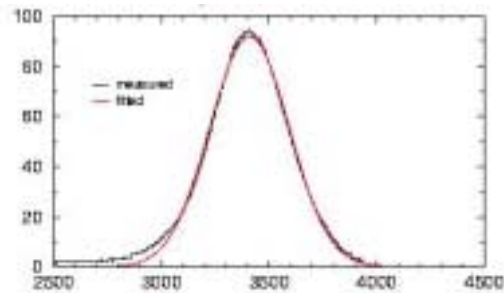
Samples:

TGG: Litton [111]
 10 mm diameter,
 20 mm length

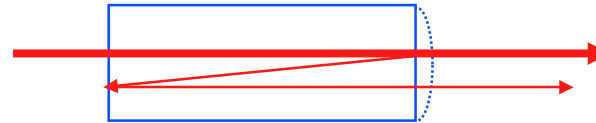
LiNbO₃: Leysop,
 5 x 5 x 40 mm

50 W Nd:YLF

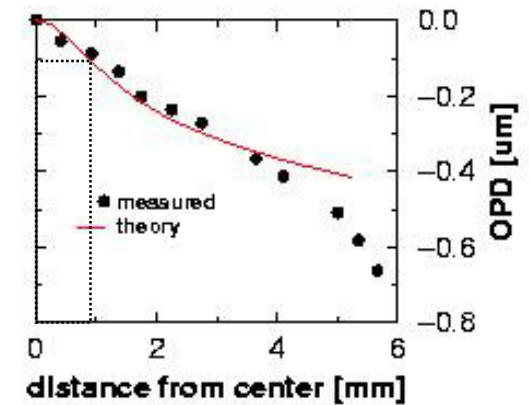
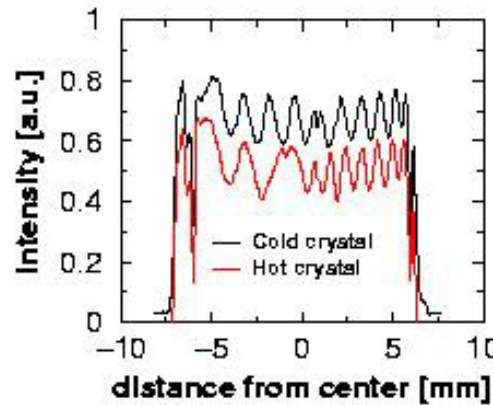
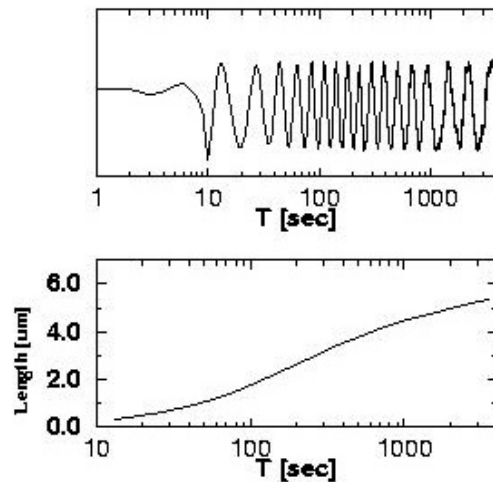
$\lambda = 1053 \text{ nm}$



Optical Path Difference Measurements



Thermal Expansion
of TGG at 50W



Theory: Hello-Vinet

P=50 W

Absolute ΔL (hot - cold): 10 μm

ΔOPD (1/e intensity): ~ 100 nm \longrightarrow 250 nm @ 125W

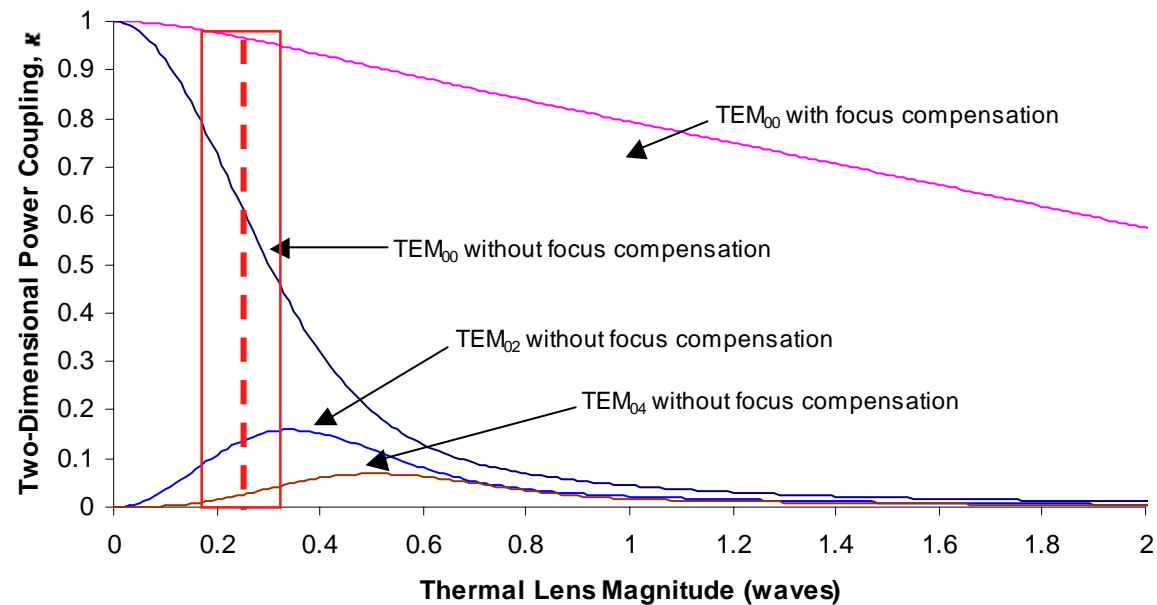


Optical Path Difference Measurements

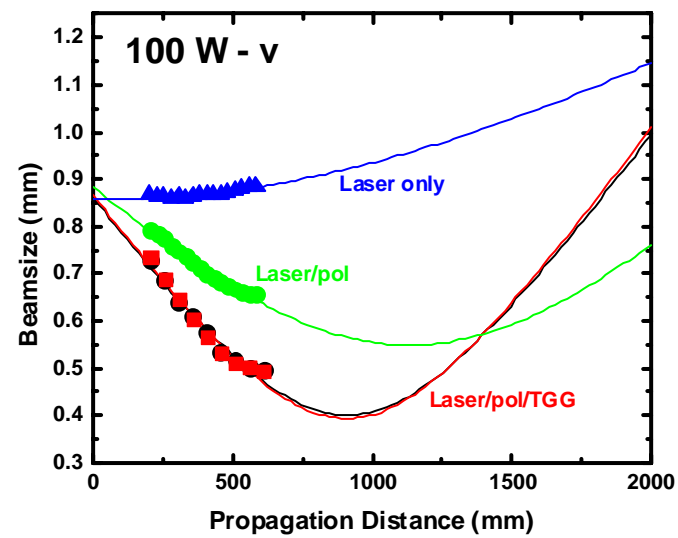
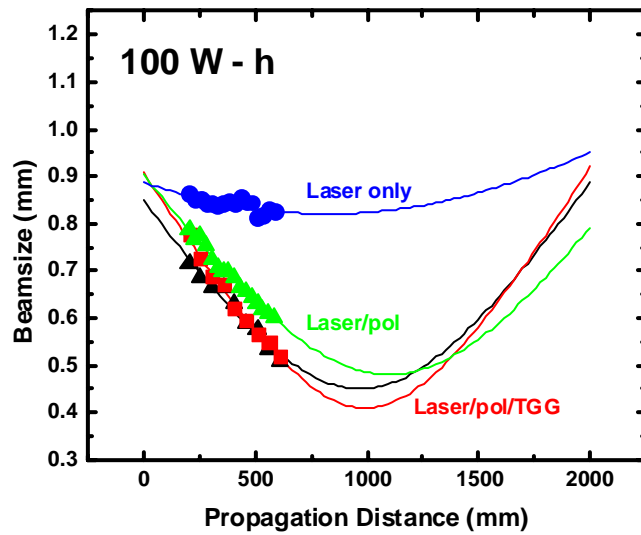
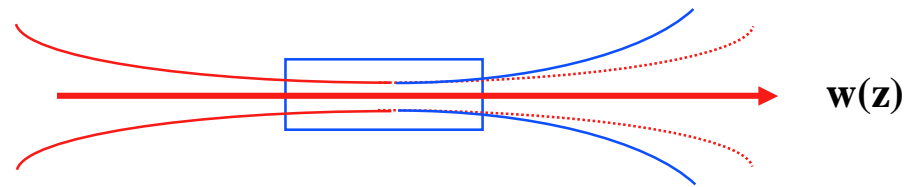
$$c_x(\psi_{aberrated}, \psi_m) = \int_{-\infty}^{+\infty} \psi_m(x) \cdot \psi_{aberrated}^*(x) dx$$

Mansell, et al., Appl. Opt., 2001

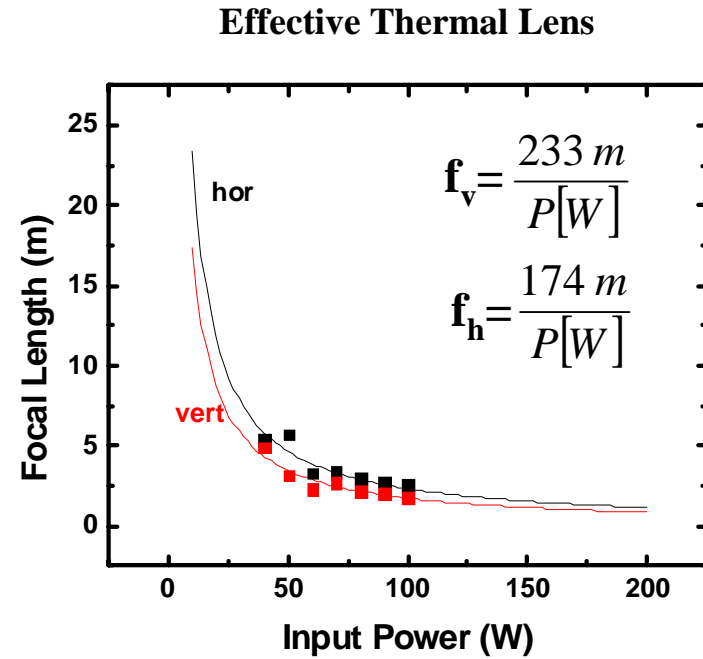
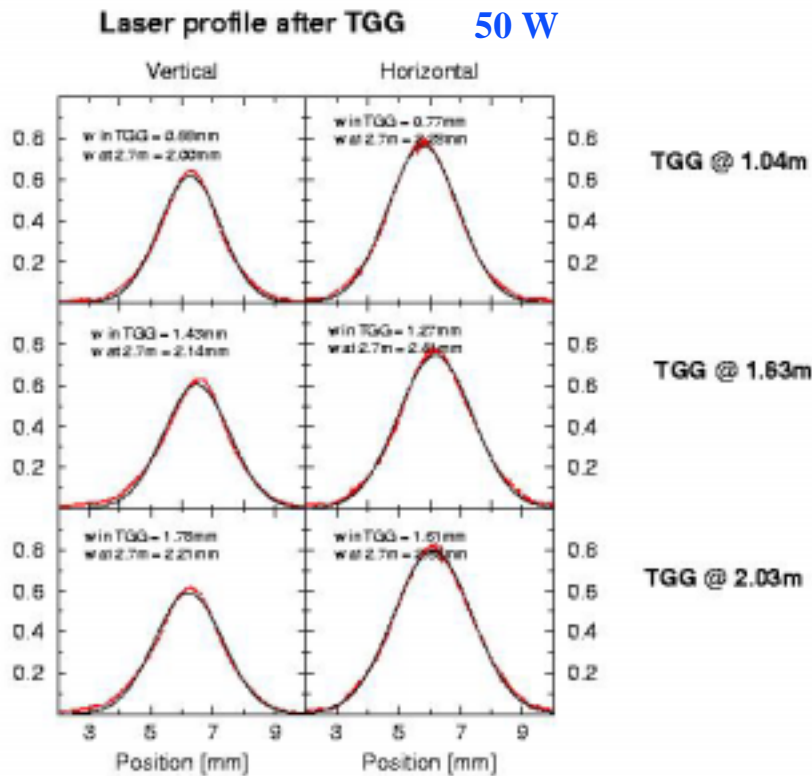
$$\kappa = [c_x(\psi_{aberrated}, \psi_m) \cdot c_x^*(\psi_{aberrated}, \psi_m)] \cdot [c_y(\psi_{aberrated}, \psi_n) \cdot c_y^*(\psi_{aberrated}, \psi_n)] = \kappa_x \cdot \kappa_y$$



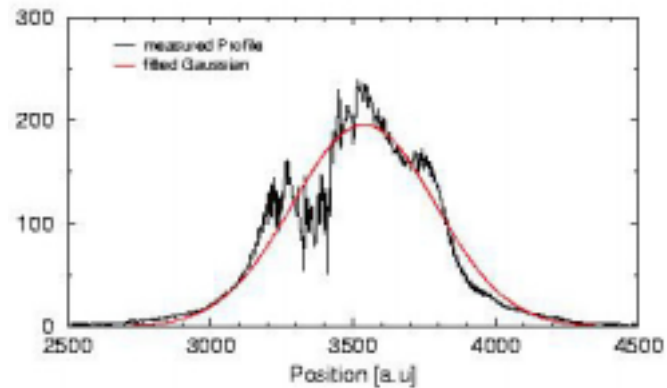
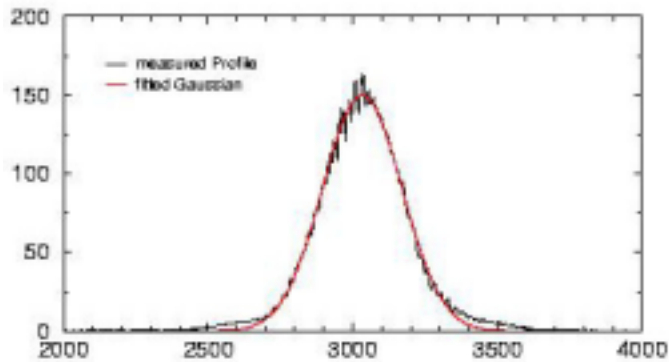
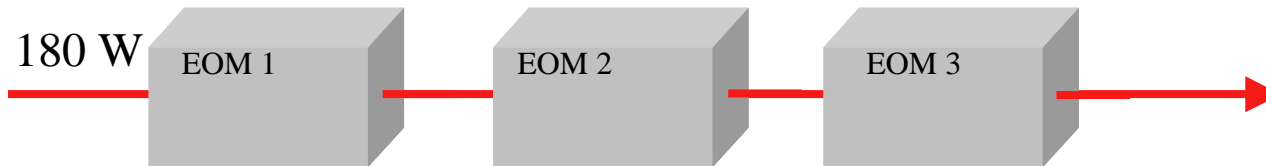
Propagation Measurements I



Propagation Measurements II



Thermal Lensing in LiNbO₃

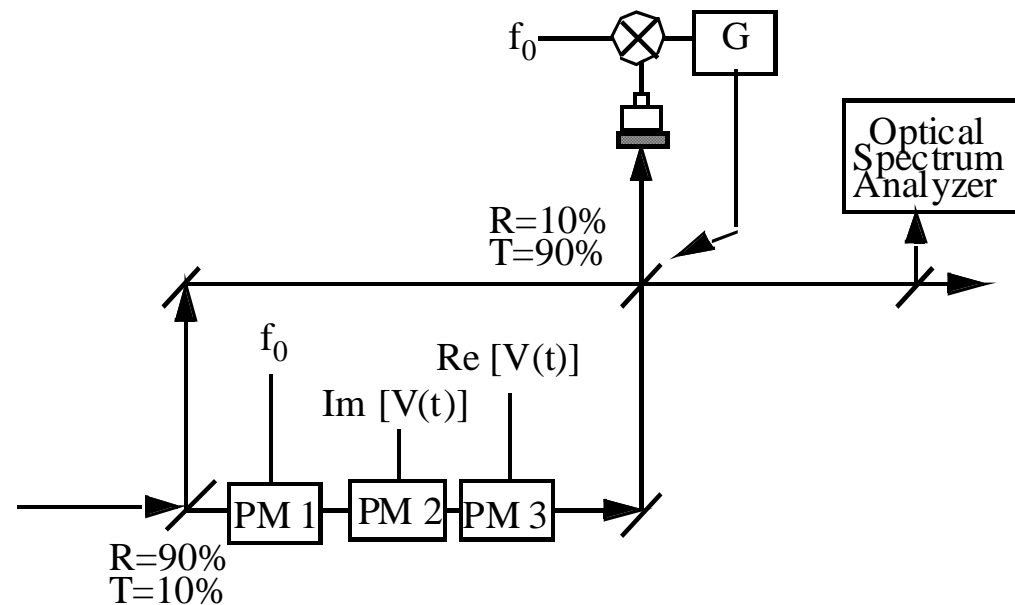


- KTP does work; 300 W CW power, 1064 nm (H. Injeyan, TRW); RTA should also work (lower loss tangent)



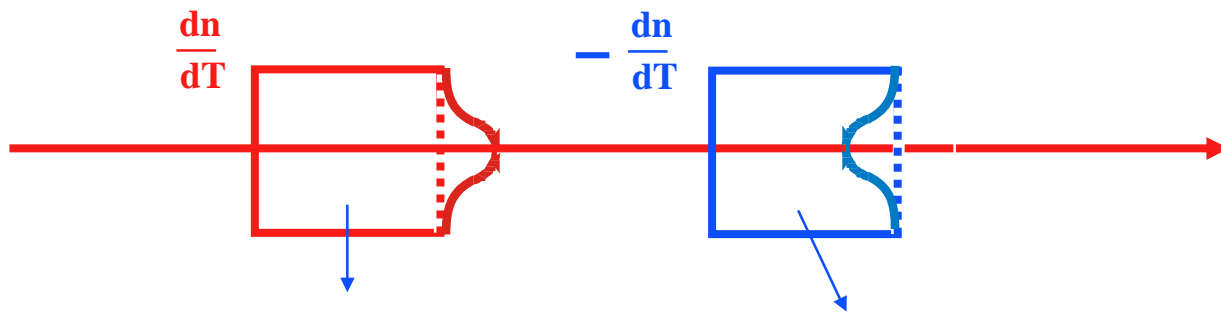
E-O Modulation in Advanced LIGO

Alternative Method: Mach-Zehnder modulation --> architecture problem



Prototype developed for initial LIGO detectors, but not well characterized
>> R&D effort

Power Independent Compensation of Thermal Lensing



$$\begin{bmatrix} TEM_{\bar{0}} \\ TEM_{\bar{2}} \\ \dots \end{bmatrix} = \begin{bmatrix} M(\zeta, z) \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ \dots \end{bmatrix} \quad \begin{bmatrix} 1 \\ 0 \\ \dots \end{bmatrix} = \begin{bmatrix} M^{-1}(\zeta, z) \end{bmatrix} \begin{bmatrix} TEM_{\bar{0}} \\ TEM_{\bar{2}} \\ \dots \end{bmatrix}$$

$$\zeta = \alpha L \frac{dn}{dT} P / 2 K \lambda$$

$$z = 1 + i\zeta$$

α = absorption coefficient

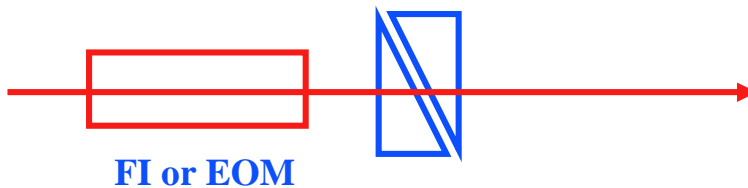
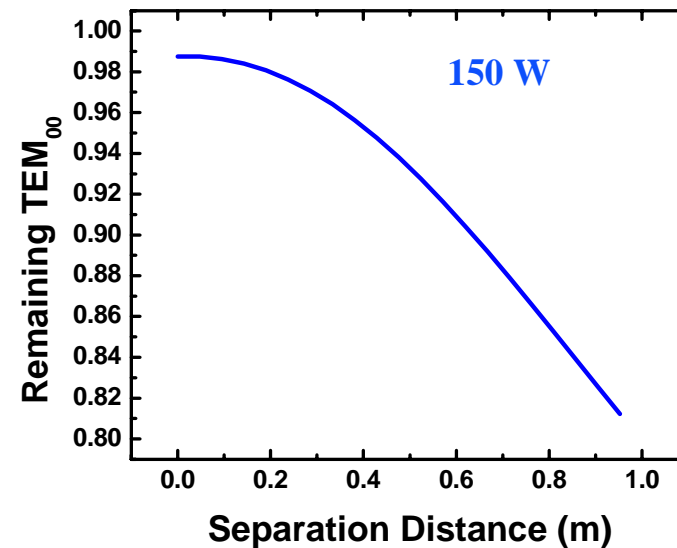
K = thermal conductivity

$$\begin{bmatrix} M(\zeta, z) \end{bmatrix} = \begin{bmatrix} \frac{1}{\sqrt{z}} & \frac{-i\zeta}{\sqrt{2z^{3/2}}} & \dots \\ \frac{-i\zeta}{\sqrt{2z^{3/2}}} & \frac{2-\zeta^2}{2z^{5/2}} & \dots \\ \dots & \dots & \dots \end{bmatrix}$$

Thermal Lensing Compensation

Modeled using Melody

Parameter	TGG	FK51
α (m^{-1})	2×10^{-1}	1×10^{-1}
K (W/m K)	7.4	0.9
dn/dT (C^{-1})	$+2 \times 10^{-5}$	-6×10^{-6}
Length (mm)	20	15.9

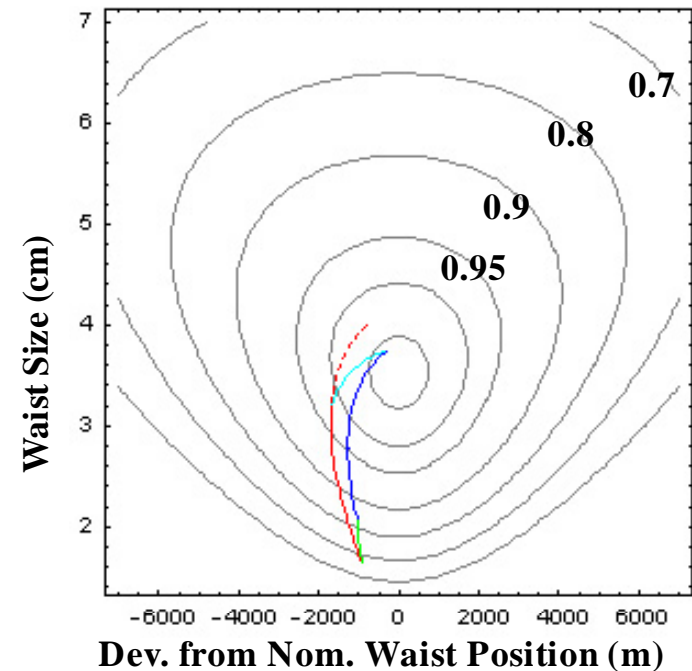
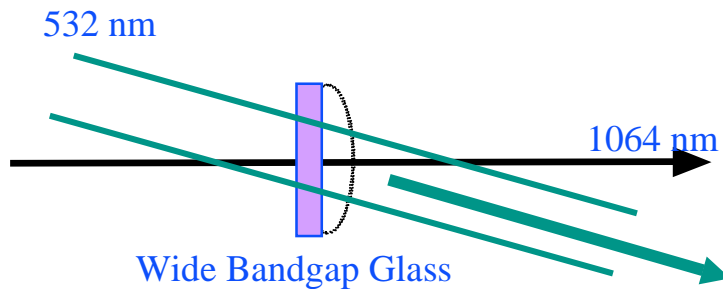


Thermal Lensing Telescope

Similar to current LIGO Telescope

- 2 mirror design (vacuum envelope constraints)
- Accommodates wide range of mode matching parameters
- All large (20 cm) optics

• in-situ adjustment with feedback





R&D Issues Still to be Faced

- Modulator Development:
 - RTA performance
 - MZ modulation
- Isolator Development:
 - Full FI system test (TCFI, EOT)
 - Possible thermal compensation ($-dn/dT$ materials)
- Telescope Development:
 - in-situ mode matching adjustment