

Thermal and nonthermal noises in the suspension (recent results of MSU group)

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The promise (Aug. 1998): LIGO II $\Rightarrow h \approx 10^{-22}$, ($\frac{S}{N} = ?$, $\Delta f = ?$, $\tau_{\text{AVER}} = ?$)

The white papers (sept. 1999): LIGO II $\Rightarrow h_f \approx 7 \times 10^{-24} \frac{1}{\sqrt{\text{Hz}}}$
 $h \approx 7 \times 10^{-23}$ for $f_{\text{grav}} \approx 10^{+2} \text{ Hz}$, $\Delta f \approx 10^{+2} \text{ Hz}$

↑
Optimistic estimate based on the model of structural damping

? LIGO III $\Rightarrow h \approx 10^{-23}$?

HOW SMALL THE DISSIPATION IN THE SUSPENSION HAS TO BE?

Pessimistic model for pendulum mode ($H = \text{const}$)

$$F_{\text{grav}} = \frac{1}{2} h L \omega_{\text{grav}}^2 m \geq \frac{S}{N} \sqrt{4k_B T H \frac{1}{\tau}} \quad \text{FDT}$$

$$h = 10^{-22}, L = 4 \times 10^5 \text{ cm}$$

$$\omega_{\text{grav}} = 6 \times 10^2 \text{ s}^{-1}, m = 10^4 \text{ gram}$$

$$\frac{S}{N} = 5, T = 300 \text{ K}, m = 10^{+4} \text{ gram}$$

$$\tau = 10^{-2} \text{ sec}$$

$$F_{\text{grav}} \approx 8 \times 10^{-8} \text{ dyn}$$

$$\tau_m^* = \frac{m}{H} \approx 6 \times 10^{+8} \text{ sec} \approx 20 \text{ years}$$

Quantum "remark"

$$h_{SQL} = \sqrt{\frac{2\hbar c}{m}} \frac{1}{L^2} \approx 7 \times 10^{-23} \quad \text{FOR } \tau = 5 \cdot 10^{-3}, m = 10^{-4} \text{g}, L = 4 \cdot 10^{-5} \text{cm}$$

TWO PINTYPE MEASUR. OF COORDINATE

STANDARD QL
NAIVE QL
STUPID QL

There is no rigorous formula for τ

$$h_{SQL} \approx \sqrt{\frac{4\hbar}{L^2 m \omega^2 c}} \approx 2.5 \times 10^{-23} \quad \text{FOR } \tau \omega = 1, \omega = 6 \cdot 10^{12} \frac{\text{rad}}{\text{sec}}$$

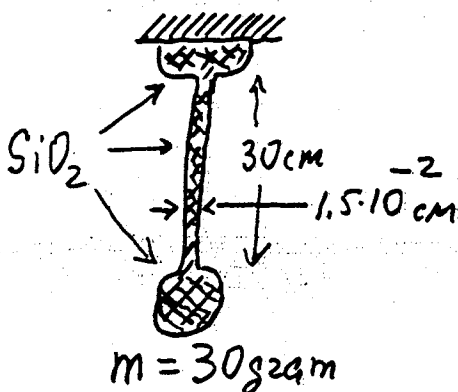
IF $\omega c \gg 1$

$$\frac{2RTc^2}{C_M^*} \Rightarrow C_M^* \approx \frac{2 \cdot 4 \cdot 10^{-14} \cdot (5 \cdot 10^{-3})^2}{10^{-27}} \approx 2 \times 10^9 \text{ sec} \approx 60 \text{ years}$$

Brief "history" of MSU efforts ($t \geq 1991$)

INITIAL KNOWLEDGE: $\left(Q_{\text{PURE SiO}_2} \right)_{\text{INTRINSIC}} \approx 2 \cdot 10^{+7}$

I. Torsional mode



$$\omega_M \approx 1.1 \frac{\text{rad}}{\text{sec}}$$

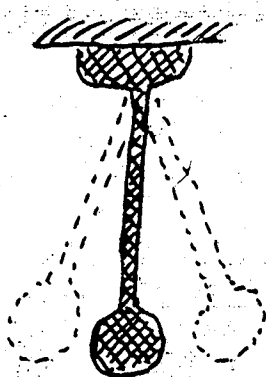
$$C_M^* \approx (1.2 \pm 0.1) \times 10^7 \text{ sec}$$

$$Q_M \approx 7 \times 10^6$$

JETP LETT.
V.55(1992) 432

FIRST EVIDENCE OF THE SURFACE LOSSES

II Pendulum mode



$$m = 30 \text{ g} \approx 3 \times 10^{-2} \text{ kg}$$

$$\omega_M \approx 5.5 \frac{\text{rad}}{\text{sec}}$$

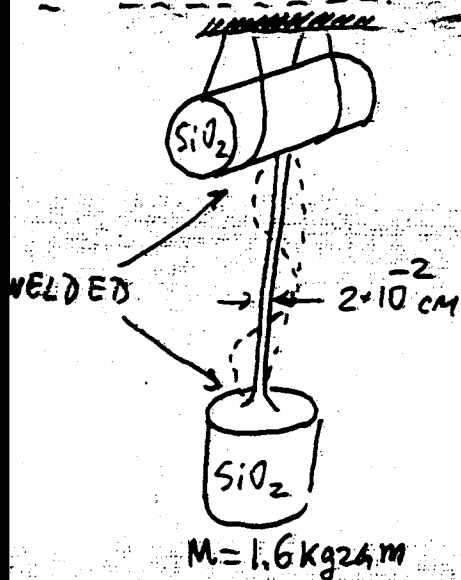
$$\tau_M^* \approx 4.4 \times 10^{+7} \text{ sec} \approx 1.54 \text{ e} 42$$

$$Q \approx 1.3 \times 10^{+8}$$

PHYS. LETT. A

v. 175 (1993), 82

III VIOLIN MODES



$$Q_{\text{BENDING MODES}} \approx 10^6 - 5 \times 10^6$$

(NO 1.6 kg mass)

ANOTHER EVIDENCE OF SURFACE LOSSES

PHYSICS

DOKLADY

v. 345 (1995)

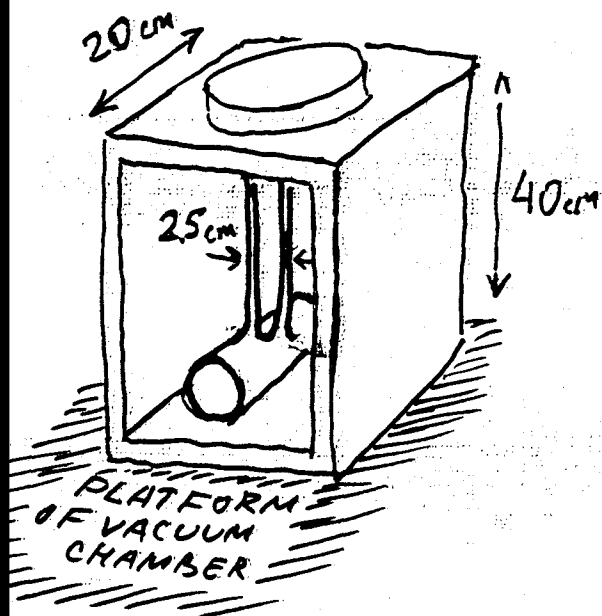
324

$$\omega_{\text{VIOLIN}} \approx 2\pi (1 \times 10^{+3} - 5 \times 10^{+3}) \frac{\text{rad}}{\text{sec}}$$

$$Q_{\text{VIOLIN}} \approx 1 \times 10^{+7} - 1 \times 10^{+8}$$

sufficient to reach $h < 10^{-22}$

IV TORSIONAL-PENDULUM MODE (LOWER FREQUENCY \Rightarrow LOWER RECOIL LOSSES)



$$M = 2 \text{ kg}$$

$$\omega_M \approx 2 \frac{\text{rad}}{\text{sec}}$$

$$\tau_M^* \approx 1 \times 10^{+8} \pm 10\% \approx 3 \text{ YEARS}$$

$$Q_{\text{T-P}} \approx 1 \times 10^{+8}$$

$$Q_{\text{EXPECTED}} \approx 10^{+9}$$

(SEE BELOW)

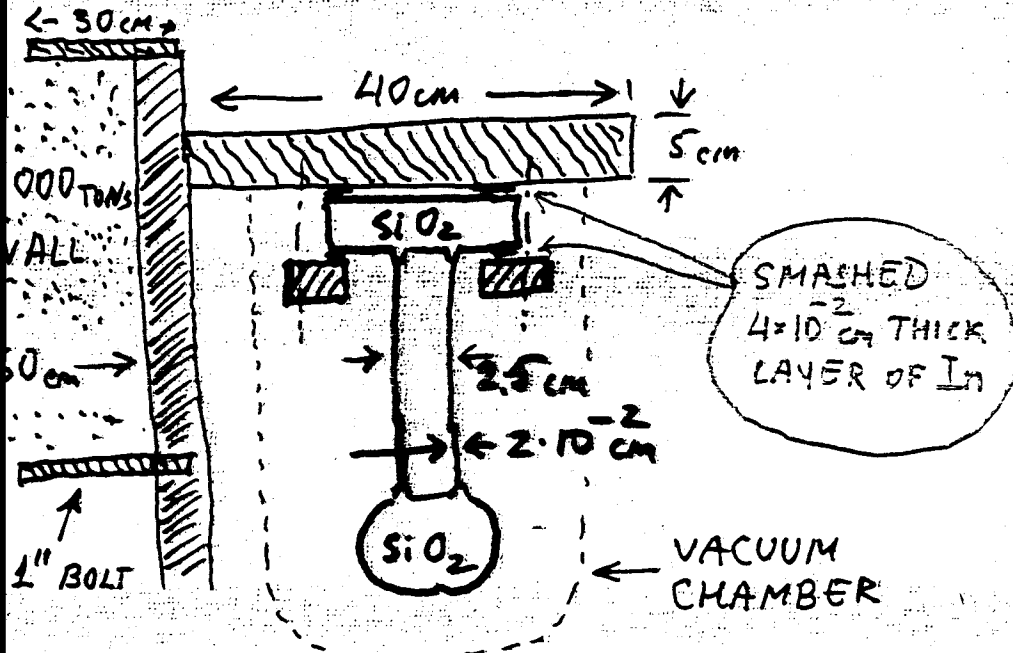
PHYS. LETT. A

v. 218 (1996),

164.

V TORSIONAL-PENDULUM MODE (SECOND ATTEMPT)

- 1) LOWER RECOIL LOSSES
- 2) BETTER VACUUM
- 3) ENFORCED VENTILATION VIA DUST ABSORBER (1-2 orders less dust?)
- 4) SHORTER TIME BETWEEN THE MANUFACTURING OF THE FIBER AND THE INSTALLATION INTO THE CHAMBER
- 5) BACKING (100°-120°C).



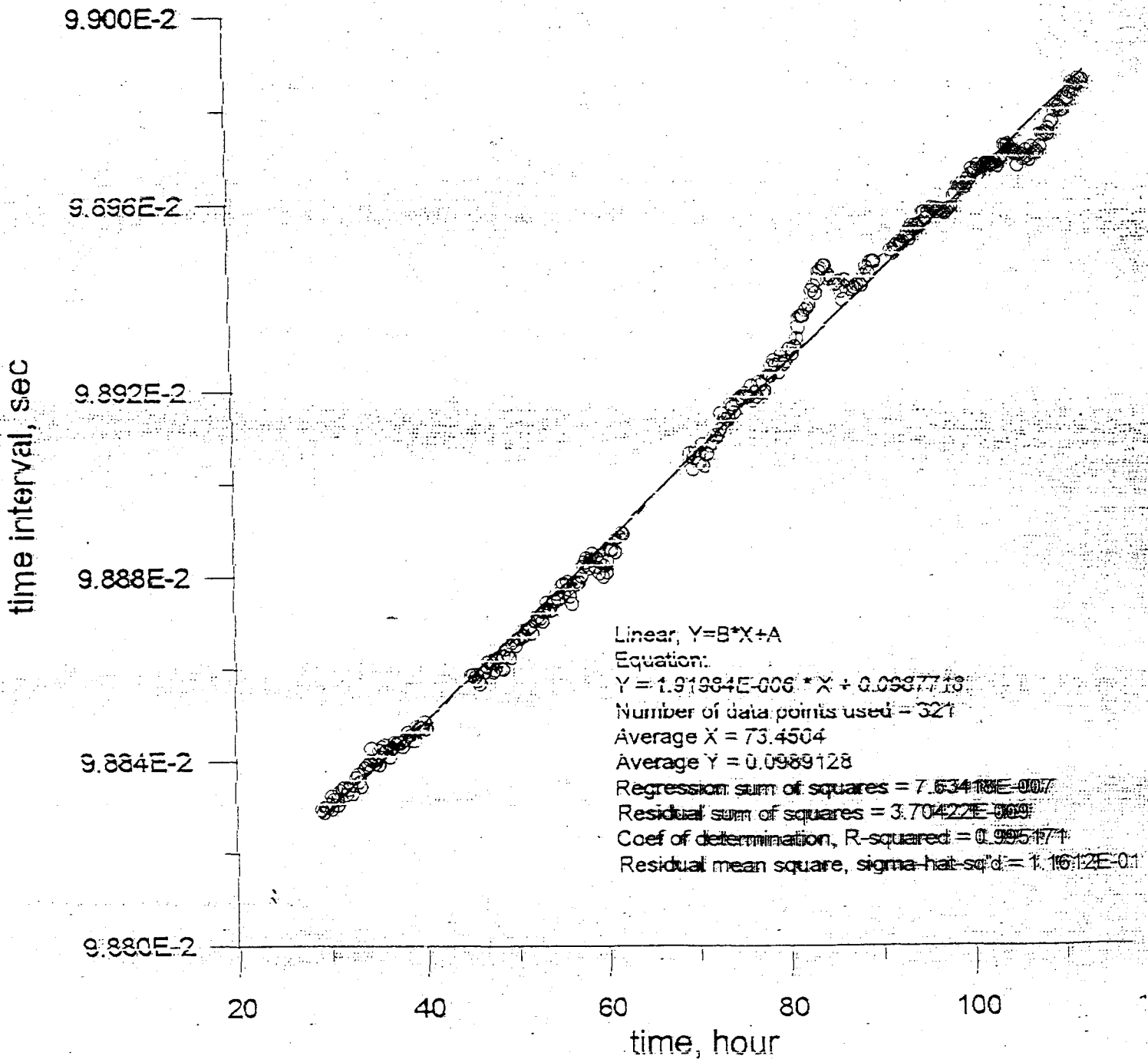
THE RESULTS:

$m = 2 \text{ kg}$ (ETCHED PINS)
 $\omega_m = 2\pi \times 0.34 \frac{\text{rad}}{\text{sec}}$
 $\tau_{T-P}^* \approx 1.86 \times 10^{+8} \text{ sec} \approx 6 \text{ YEAR}$

 $Q_{T-P} \approx 2 \times 10^{+8}$

$m = 0.5 \text{ kg}$ (J. HOUGH ET AL BONDED PINS)
 $\omega_m \approx 2\pi \times 1.17 \frac{\text{rad}}{\text{sec}}$
 $\tau_{T-P}^* \approx 6.3 \times 10^{+7} \text{ sec} \approx 2 \text{ YEARS}$

 $Q_{T-P} \approx 2.3 \times 10^{+8}$



V.P. MITROFANOV, K.Y. TOKMAKOV

$\tau_M^* \approx 1.86 \cdot 10^{+8} \text{ sec} \approx 6 \text{ years}, Q_M \approx 2 \cdot 10^{+8}, \text{ MARCH } 2^{\text{nd}}, 1998$

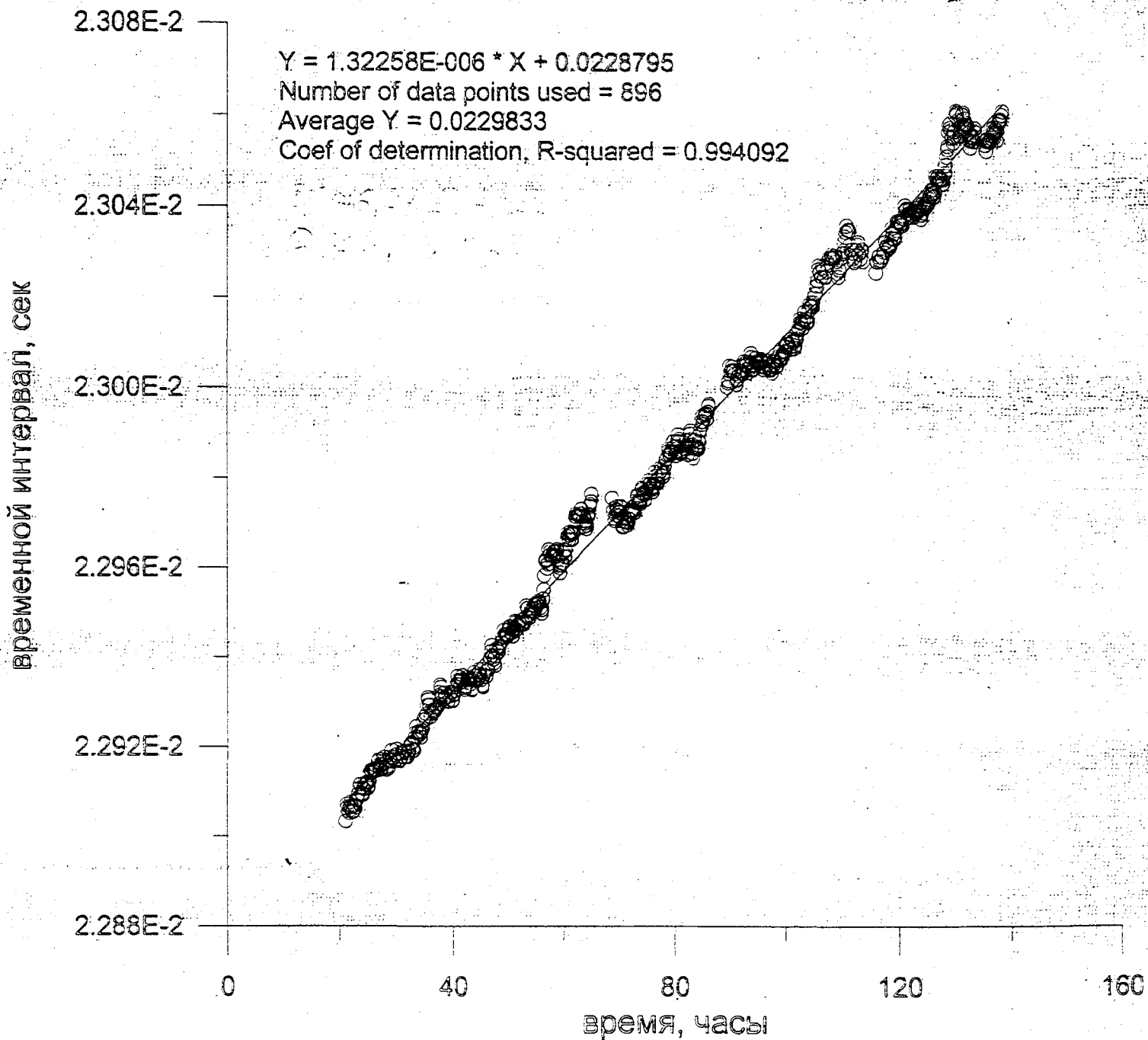
$$\tau^* = \frac{9.9 \cdot 10^{-2}}{1.92 \cdot 10^{-6}} \cdot 3600 = 1.86 \cdot 10^8$$

21. MAY, 1999

V. P. MITROFANOV, K. V. TOKMAKOV

$$Q_M^* = 6.3 \times 10^7 \text{ sec}, \quad Q_M = 2.3 \times 10^8$$

(JIM HOUGH GLEED SUSPENSION)



The comparison with the "theory"

$$Q_{T-P}^{-1} \approx \frac{\pi G \tau^4}{m g a^2} \Phi_G + \frac{1}{l} \sqrt{\frac{\pi \Upsilon \tau^4}{2 m g}} \Phi_Y$$

$$G = 3 \times 10^{11} \frac{\text{dyn}}{\text{cm}^2}$$

$$a = 2.5 \text{ cm}$$

$$\Upsilon = 7 \times 10^{11} \frac{\text{dyn}}{\text{cm}^2}$$

$$\tau = 1 \times 10^{-2} \text{ cm}$$

$$m = 2 \times 10^{-3} \text{ g} \approx 2 \pi$$

$$l = 25 \text{ cm}$$

$$\left. \begin{array}{l} \Phi_G = \Phi_Y = 1.4 \cdot 10^{-7} \\ \text{FROM EXPERIMENT} \end{array} \right\}$$

$$\left. \begin{array}{l} Q_{T-P} \approx 2 \cdot 10^{+9} \\ \text{EXPERIMENT} \end{array} \right\}$$

POSSIBLE EXPLANATIONS $[(Q_{T-P})_{\text{MEASUR}} \approx 2 \cdot 10^{+9}]$

1. Nonperfect isolation (coil losses), I_n ?
2. Nonsufficient backing (mud on surface: $H_2O + SiO_2$)
3. Additional losses on the pins (rough surface + sedimentation)
4. Dust particles (16 particles detected by a touch in "postmortem" examination of the fiber)

THE RESERVES (SEE THE FORMULA ABOVE)

1. $\frac{G_F}{\Upsilon} = 4 \times 10^{-3}$ IN THE MEASUREMENTS, BUT "VIRGIN" FIBERS
ACCEPT $\frac{G_F}{\Upsilon} \approx (2-3) \times 10^{-2}$! (O.A. Okhizimenko)
2. $\tau^4 \rightarrow a b^3$ (ribbon) \rightarrow may give factor 3-6 for Q
3. $l = 25 \text{ cm} \Rightarrow l = 250 \text{ cm}$.

$\rightarrow Q \approx 10^{10}$ IS NOT A CRAZY NUMBER (IF ONE HAS ENOUGH MONEY AND PATIENCE)

STRATEGIC RESERVE: THE SUBTRACTION OF BROWNIAN

MOTION: "HOW TO REDUCE THE SUSPENSION THERMAL NOISE WITHOUT IMPROVING THE Q 'S IN THE PENDULUM AND VIOLIN MODES": 2 orders (GR-QC/9805031)

The problem of the nonthermal noise (excess noise) (FDT is a big illusion)

An assumption:

Probably (?) the main source of nonthermal noise is very stressed wire (fiber) in the suspension.

The results:

1) The tungsten wires are very noisy (strong excess noise above the thermal one) even when $\frac{\sigma_{APPL}}{\sigma_{BREAK}} \approx 0.3$

(Phys. Lett. A 227 (1997), 159)

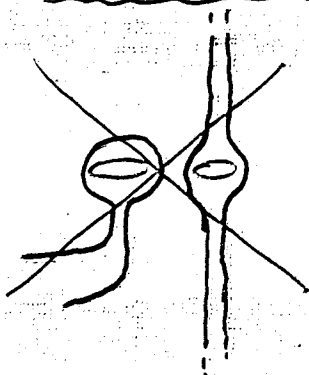
2) The steel wires are (5-8) times less noisy than the tungsten ones, but if $\frac{\sigma_{APPL}}{\sigma_{BREAK}} \approx 0.3$ this noise may mimic $h \approx 5 \cdot 10^{-21}$

$$\sqrt{\Delta X_{THERM}^2} \approx \underline{2 \cdot 10^{-10} \text{ cm}}, \quad \Delta X_{METER} \approx \underline{2 \cdot 10^{-11} \frac{\text{cm}}{\sqrt{\text{Hz}}}}$$

(Phys. Lett. A 246, (1998), 479)

NOISE IN SiO₂ FIBERS?

The goal is $\Delta X_{meter} \approx 10^{-13} \frac{\text{cm}}{\sqrt{\text{Hz}}}$ and do not damage the VIRGINITY of the SiO₂ fiber ($t \approx 1999, 2000$)



THIS VERSION OF
METER FAILED

new version of meter is
in process of assembling.

If our calculations are correct

then $\underline{\Delta X} \approx \underline{1 \cdot 10^{-15} \frac{\text{cm}}{\sqrt{\text{Hz}}}}$ and

the VIRGINITY will not be damaged