

# Thermal noise in dielectric mirror coatings: calculation and optimization

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# Sorts of phase noise in multilayer coating

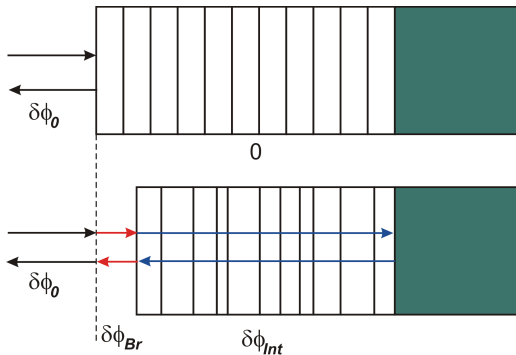
$$d\Phi = -sd\theta - u_{ik}d\sigma_{jk} + \mu dN + \dots$$

$$\begin{array}{cccc} \frac{\partial u_{ik}}{\partial \theta} \delta \theta & \frac{\partial n}{\partial \theta} \delta \theta & \frac{\partial u_{ik}}{\partial \sigma_{jk}} \delta \sigma_{jk} & \frac{\partial n}{\partial \sigma_{jk}} \delta \sigma_{jk} \\ \downarrow & \downarrow & \downarrow & \downarrow \\ \frac{\partial d}{\partial \theta} \delta \theta & \frac{\partial n}{\partial \theta} \delta \theta & \delta d & \frac{\partial n}{\partial d} \delta d \end{array}$$

- Thermoelastic noise
- Thermorefractive noise
- Brownian (surface displacement) noise
- Photoelastic (Acoustooptic) noise
- Interference dephasing



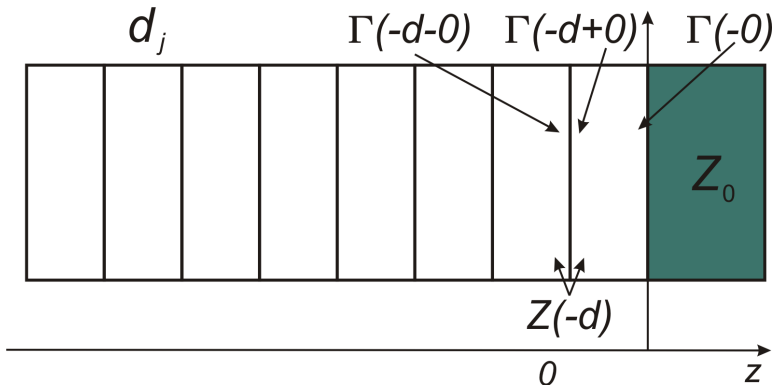
# Interference dephasing.



$$\delta\varphi = -2k_0 \sum_{j=1}^N [A_j n_j - n_e] \delta d_j - B_j \delta n_j$$



# Method



- Impedances are continuous on dielectric borders
- Reflection coefficient experiences jump on dielectric borders, but continuous between borders



## Noisy mirror: interferential part.

- Temperature and mechanical stress influence reflection phase through layer thicknesses and refraction indexes.
- $\delta d_j$ :  $\varphi_i \rightarrow \varphi_i - 2k_0 \delta n_i d_i - 2k_0 n_i \delta d_i$ .
- $\delta n_j$ :  $\eta_i \rightarrow \eta_i (1 + \delta \eta_i)$
- Expand all formulas to the first order of  $\delta d_j$  and  $\delta n_j$ :



## Mathematical results.

$$\Gamma'_m = \Gamma_m \left( 1 + \sum_{j=1}^{m-1} \prod_{k=j+1}^m f_k Z_{k-1} \left( i\Delta_j - \mu_j \frac{\delta n_j}{n_j} \right) - f_m \nu_m \frac{\delta n_m}{n_m} \right)$$

where

$$Z_k = \frac{2\Gamma_k e^{i\varphi_k}}{1 - \Gamma_k^2 e^{i2\varphi_k}};$$

$$f_k = \frac{2\eta_k Z_{k-1}}{Z_{k-1}^2 - \eta_k^2};$$

$$\Delta_j = -2k_0 \delta n_j d_j - 2k_0 n_j \delta d_j;$$

$$\nu_k = \frac{Z_{k-1}^2 + \eta_k^2}{Z_{k-1}^2 - \eta_k^2}; \quad \nu_1 = 1;$$

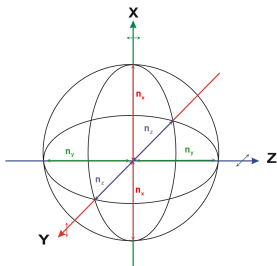
$$\mu_k = \left( f_k \nu_k + \frac{1}{Z_k} \right);$$

(1)



# Photoelasticity.

## INDICATRIX



- $\sum B_{ij} x_i x_j = 1$

## Optical indicatrix

$$\Delta B_\lambda = \rho_{\lambda\mu} u_\mu$$

## Perpendicular refraction indexes

$$\delta n_x = -\frac{n_0^3}{2} \rho_{13} \frac{\delta d}{d}$$

$$\delta n_y = -\frac{n_0^3}{2} \rho_{23} \frac{\delta d}{d}$$





# Physical results.

## Perturbed reflection coefficient

$$\Gamma'_{N+e} \approx \Gamma_{N+e} (1 + \delta\Gamma_{Int}) e^{i\delta\varphi_{Int}}$$

## Phase perturbation

$$\delta\varphi_{Int} = \sum_{j=1}^N \Im [\alpha_j] \delta d_j,$$

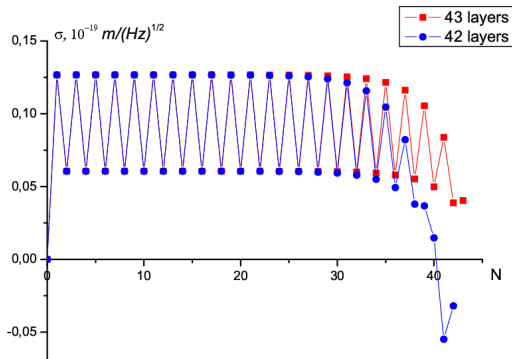
## Amplitude perturbation

$$\delta\Gamma_{Int} = \sum_{j=1}^N \Re [\alpha_j] \delta d_j,$$

$$\alpha_j = -2k_0 n_j \left( 1 - \frac{n_j^2}{2} p_{13} \right) \prod_{k=j+1}^{N+e} f_k z_{k-1} (i + \mu_j)$$



# Noise distribution through layers



- Interferencial part is significant on depth of penetration
- Photoelasticity acts as correction to refraction index.



# Spectral density.

- Each layer's  $\delta d$  is independent, e.g.  
 $\langle \delta d_{2j}^2 \rangle = \sigma_{d0}^2$ ,  $\langle \delta d_{2j+1}^2 \rangle = \sigma_{d1}^2$ ,  $\langle \delta d_j \delta d_k \rangle = 0$ .

## One layer spectral density.

$$\langle \delta d_j^2 \rangle = \sigma_{dj}^2 = \xi_j(\omega) \phi_j d_j$$

- where

$$\xi_j = \frac{4\theta}{\omega} \frac{1}{\pi R^2} \frac{E_j^2 (1 + \sigma_s)^2 (1 - 2\sigma_s)^2 + E_s^2 (1 + \sigma_j)^2 (1 - 2\sigma_j)}{E_s^2 E_j (1 - \sigma_j^2)},$$

Yu. Levin, *Phys.Rev. D* **57**, 659-663 (1998),



# Results

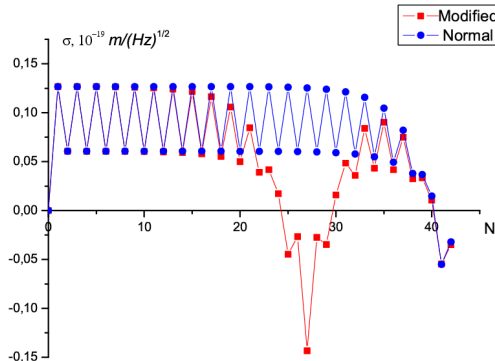
## Quartz-tantala mirror noises

Type	42 Layers	""Standart""	43 Layers
Transmittance, ppm	2.28	1.08	0.54
Brownian $10^{-20} \text{m}/\sqrt{\text{Hz}}$	6.44	6.46	6.54
With interference	6.21%	6.81%	5.5%
With photoelasticity	7.45%	5.42%	4.28%
Modified cap	7.45%	--	4.02%

- Values relative in columns
- ""Standart"" here is  $\lambda/4 + \lambda/2\text{cap}$  mirror of 42 layers total.



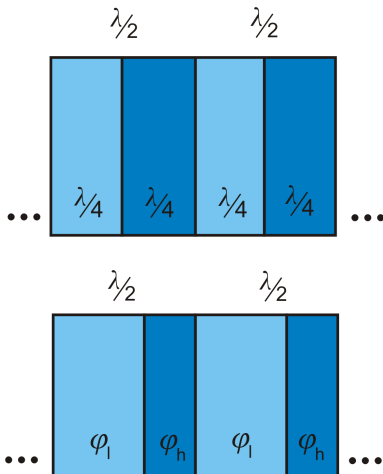
# Layer-corrector inside the mirror.



- H. J. Kimble, Phys. Rev. Lett. **101**, 260602 (2008).
- Noise suppression by 15%, increasing transmittance.
- Attempt to add layers for restoring transmittance neglects the effect.



# Modifying silica-tantala ratio.



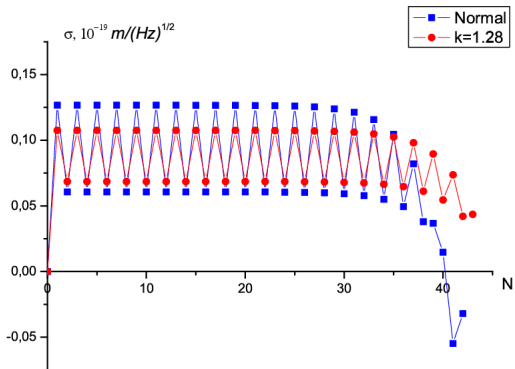
- Tantala is more "noisy"

$$\gamma = \frac{\sigma_{ta}^2}{\sigma_{si}^2} = \frac{\xi(Y_{ta}, \sigma_{ta})\phi_{ta}n_{si}}{\xi(Y_{si}, \sigma_{si})\phi_{si}n_{ta}}$$

- Reduce tantala thickness, preserving " $d_{si} + d_{ta} = \lambda/2$ " ( $\varphi_l + \varphi_h = 2\pi$ ).
- Increase number of layers preserving transmittance.



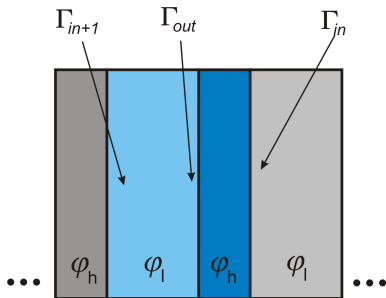
# Modifying silica-tantala ratio.



- Suppression efficiency is lower 5% for LIGO parameters from GWINC. ( $\gamma = 4.6$ )
- For  $\gamma = 7$  efficiency is 8.6%, which coincides with experiment of A. V. Villar (*Phys. Rev. D* **81**, 122001)



# Optimal coating.



- $\Gamma_{in} = \Gamma_0 e^{i\varphi_0}$

$$\varphi_0 \approx \frac{\pi - \varphi_h}{2} - g^2 \sin(\varphi_h)$$

- $\arg[\Gamma_{in+1}] = \varphi_0$  for max gain

- "' $d_{si} + d_{ta} = \lambda/2$ '" is not optimum.

$$\varphi_l = 2\pi - \varphi_h - 2 \sin(\varphi_h) g^2$$

$$g = \frac{n_h - n_l}{n_h + n_l}; \quad \varphi = 2k_0 n d$$





## Analytical approach.

- Beginning from  $N > 3$   $T = \beta(\varphi_h, \varphi_c) \alpha^N(\varphi_h) \epsilon(\varphi_e)$
- First 3 pairs do not work in interferential part.
- Full brownian noise can be obtained in form

### Full Brownian noise.

$$\frac{\sigma_{Full}^2}{A} = \frac{\ln T_0 - \ln \beta - \ln \epsilon}{\ln \alpha} (\gamma \varphi_1 + \varphi_2) + \varphi_c - \varphi_2 + \\ + E(\gamma \varphi_\epsilon + \varphi_{\epsilon 2}) + \varphi_0 - \varphi_{0\epsilon} + \frac{\sigma_{Int}^2}{A}$$



# Optimization results.

## Quarts-tantala mirror efficiencies

Type	Standart	A. Villar	Our method
Transmittance, ppm	277.6	277.7	276.8
Brownian (displacement)	0%	8.27	8.36%
With interference	11.1%	17.3%	17.4%
With photoelasticity	8.3%	16.2%	16.3
Relative	0	8.6%	8.7%

- Values relative to standart  $\lambda/4 + \lambda/2$  cap mirror Brownian (displacement) noise
- $\sigma_{Standart} = 144 \times 10^{-20} \text{ m}/\sqrt{\text{Hz}}$  ( $\omega = 2700 \text{ Hz}$ )



# Conclusion.

- Interference and photoelastic correction is 4 to 7 %
- Amplitude noise is small
- Double layers could be less than half-wavelength  
( $\varphi_l + \varphi_h = 2\pi - 2g^2 \sin(\varphi_h)$ )
- Optimisation efficiency is 5 to 8.7% depending on  $\gamma$

