

# Matched filter analysis of burst waveform injections

**M. Sung for the LSC**

Louisiana State University, Baton Rouge, LA, 70803 USA

E-mail: [sung@phys.lsu.edu](mailto:sung@phys.lsu.edu)

**Abstract.** Hardware injections provide us with a crucial tool for proving that we understand the response and performance of the LIGO detectors. Since we have complete knowledge of the injected waveform and detailed measurements of the detector response function, we are able to predict and confirm the instrument response. During the S5 science run of LIGO, various burst-type waveforms are being injected. We have analyzed the first seven months of these injections, using optimal matched filters derived from the injection waveforms. We have confirmed that most of the responses follow the predictions and have measured the accuracy of the estimated arrival time. In addition, we examined transients identified by the *KleineWelle* algorithm in auxiliary data channels at the time of hardware injections. Through this study, we could recognize couplings between auxiliary channels and the gravitational wave channels and assess the safety of the use of auxiliary channels as vetoes for gravitation wave candidates.

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## 1. Introduction

The LIGO observatories are currently collecting the data for their first long observing run at design sensitivity; this run began in November of 2005, and is designated as “S5”. During this run, hardware injections with various waveforms have been carried out to monitor the response and performance of the detectors. Hardware injections provide the only direct test of the entire system.

In this article, we describe how hardware injections are performed, and the techniques used to analyze the injection data. The primary analysis tools are linear filters: whitening filters, and filters matched to the injected waveforms. These methods were applied to recover the strength and timing of each injection, and compare them with expectations. This study shows that we have a good quantitative understanding of the total system response.

In addition, we used the transient search technique, called the KleineWelle algorithm[1], to check the response of auxiliary channels to hardware injections, which shows how the coupling between those channels and strain sensing channels can be tested.

## 2. Hardware injection procedures

Burst-type hardware injections are performed with twenty distinct waveforms, as listed in Table 1. Usually a subset of these are used in a single injection period, and the magnitude and time offsets are varied in a systematic fashion. The same waveforms are injected into all three interferometers at the same time with small (a few ms) or no time shifts. These planned injection periods take place several times each day at irregular intervals.

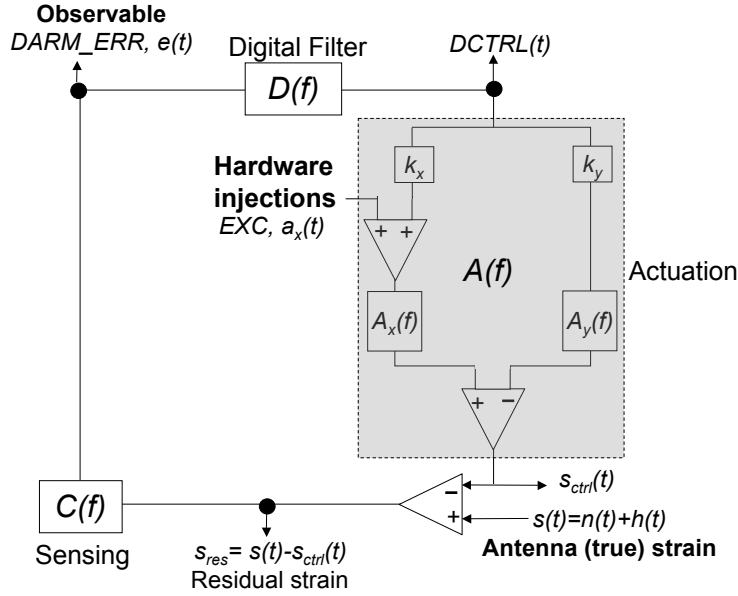
The crucial parts of the interferometer are shown in Fig. 1 as a highly simplified block diagram of the “differential-arm” servo system. The total strain measured by the antenna (noise plus gravitation) is shown as the quantity  $s(t) = n(t) + h(t)$ . The observable output of the system is the error signal  $e(t)$ , recorded from the channel called DARM\_ERR. The many components of the system can be condensed into three linear response functions, specified in the frequency domain: a “Sensing” function  $C(f)$ , a “Digital Filter” function  $D(f)$ , and an “Actuation” function  $A(f)$ . The actuation function is further divided into functions for each arm  $A_x(f)$  and  $A_y(f)$  and coupling coefficients  $k_x, k_y$ ,

$$A(f) = k_x A_x(f) - k_y A_y(f). \quad (1)$$

Then the servo system can be solved to find the response function of the detector  $R(f)$ , which converts the error signal  $e(f)$  into the strain signal  $s(f)$ ,

$$s(f) = \frac{1 + C(f)D(f)A(f)}{C(f)} e(f) \equiv R(f)e(f), \quad (2)$$

where  $e(f)$ ,  $s(f)$  are the Fourier transforms of  $e(t)$ ,  $s(t)$ .



**Figure 1.** A simplified block diagram of the differential arm servo system of the LIGO detector. The optics and analog electronics are represented in the Sensing block, the digital electronics in the Digital Filter block, and the mechanical components in the Actuation block. Their transfer functions are specified by frequency domain functions, such as  $C(f)$ .

Injections are done by applying prepared waveforms onto the excitation channel on the  $x$ -arm, ETMX\_EXC. Waveforms for injection,  $a_x(t)$ , are prepared by applying the actuation function,  $A_x(f)$ , in the frequency domain, onto waveforms generated as strain waveforms,  $h_{inj}(t)$ ,

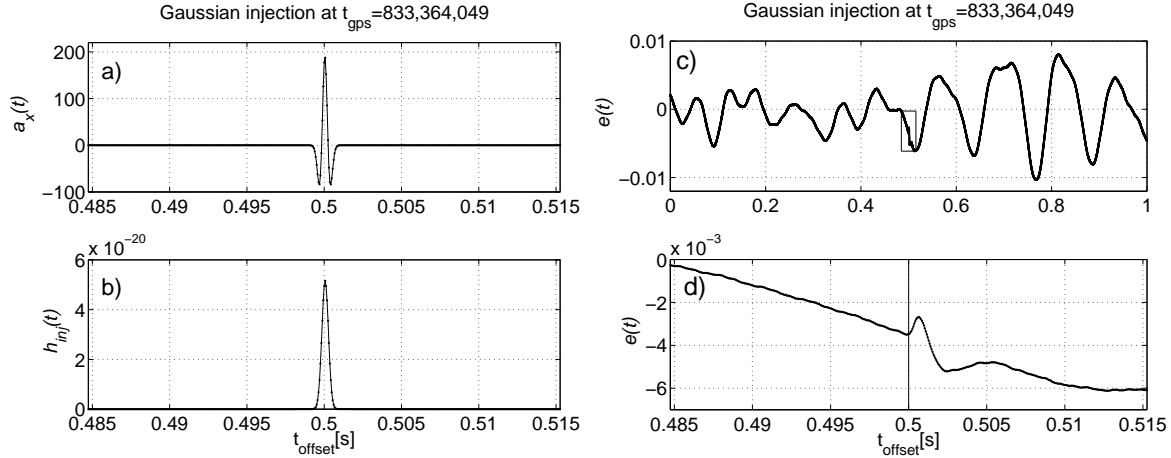
$$a_x(f) = -\frac{h_{inj}(f)}{A_x(f)}, \quad (3)$$

and then transforming back into the time domain. The time series of this waveform is then injected into the differential arm servo. An injection of a Gaussian with a short width of 0.3 ms, carried out at  $t_{gps} = 833,364,049$ , for example, is shown in Fig. 2. The waveform injected to the excitation channel is shown in Fig. 2 a) and the desired waveform in strain,  $h_{inj}(t)$ , is shown in Fig. 2 b). The designed time offset (0.5 s) from the injection time and magnitude ( $20 \times 10^{-21} \sqrt{s}$ ) scaling for this specific injection are applied. The detector response to this injection measured in the error signal channel DARM\_ERR,  $e(t)$ , is shown in Fig. 2 c) and d) with two different time scales.

### 3. Linear filters

Two different whitening filters are applied to the data to examine the error signal response  $e(t)$  to each injection with the noise reduced.

$$e_{sw}(t') = \int_{-\infty}^{\infty} df e^{-i2\pi ft'} \frac{1}{\sqrt{S_n(f)}} e(f), \quad (4)$$



**Figure 2.** Hardware injection with a Gaussian impulse with  $\tau = 0.3$  ms done at  $t_{\text{gps}} = 833,364,049$ : waveforms a) injected to ETMX\_EXC and b) desired in strain as  $h_{\text{inj}}(t)$ , and c) error signal data  $e(t)$  at the injection time and d) the same data with finer time scale.

for single whitening and

$$e_{\text{dw}}(t') = \int_{-\infty}^{\infty} df e^{-i2\pi ft'} \frac{1}{S_n(f)} e(f), \quad (5)$$

for double whitening, where  $S_n(f)$  is the power spectral density of noise spectrum, estimated from data.

The primary analysis is application of the the optimal linear filter [2], a standard method from the classical signal processing for known signal waveforms, was used. The optimal filter is the matched filter optimized with the double whitening filter:

$$\|h_\alpha(t')\| = N_\alpha \int_{-\infty}^{\infty} df e^{-2\pi i ft'} \tilde{h}_\alpha^*(f) \frac{1}{S_n(f)} s(f). \quad (6)$$

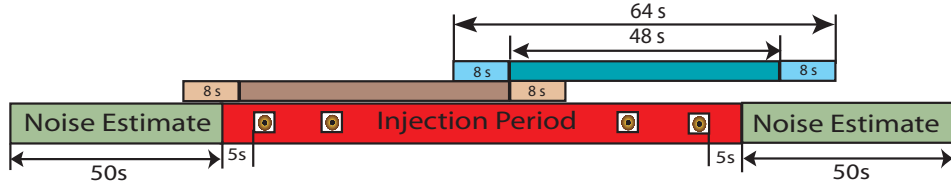
Here  $\|h_\alpha(t')\|$  is the output time series from the optimal filter with the template,  $h_\alpha(t)$ , and  $s(f)$  and  $\tilde{h}_\alpha(f)$  are the Fourier transforms of the strain data,  $s(t)$ , and  $h_\alpha(t)$ , respectively. The normalization factor,  $N_\alpha$ , in eq. (6), is derived to have the unbiased strength measurement of the reconstructed signal waveform as the filtered output, calculated in the unit of the norm of waveform,  $\|h_\alpha\| \equiv \sqrt{\int h_\alpha^*(t) h_\alpha(t) dt}$ . The injected waveform,  $h_{\text{inj}}(t)$  in Eq. (3) is used as template waveform  $h_\alpha(t)$ .

By using relations (2) to convert the template waveform,  $h_\alpha$ , and the noise spectrum,  $S_n$  in strain into functions of the error signal,  $e(t)$  and  $S_m$ , it can be seen that the equivalent formula for the optimal filter can be written for the error signal data, after the effect of the response function are cancelled out:

$$\|h_\alpha(t')\| = N_\alpha \int_{-\infty}^{\infty} df e^{-2\pi i ft'} \tilde{k}_\alpha^*(f) \frac{1}{S_m(f)} e(f), \quad (7)$$

where  $k_\alpha$  and  $S_m$  are the template waveform and the noise spectrum in terms of the error signal. This implies the optimal filter can be applied to either the strain data,  $h(t)$ , or the error signal data,  $e(t)$ , to get the same filtered output,  $\|h_\alpha(t')\|$ .

To use the discrete fourier transform, the data were segmented as shown in Fig. 3. An injection period starts 5 s before the first injection and ends 5 s (or more)



**Figure 3.** Time segmentation of the analysis. The injection period with injections is divided into 64 s segments with 16 s overlapping with the next segment. Noise spectrum is obtained from data of 50 s before and after the injection period.

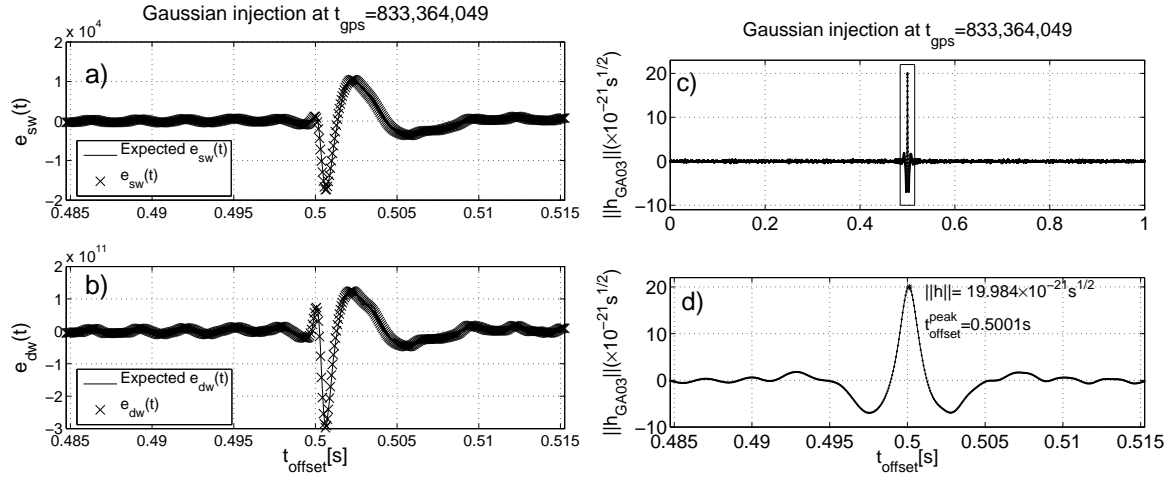
after the last injection. The injection period is divided into 64 s segments with 16 s overlapping with the next segment. The raw data from each analysis segment of 64 s is multiplied by a Tukey window [3] (flat over the middle 62 s), then Fourier transformed, then filtered, finally transformed back to the time-domain. The first segment starts 10 s before the first injection. After testing with various waveforms and different setups, to avoid discontinuity at the boundary of each segment, the middle 48 s of each time segment is kept, and the 8 s at each end are thrown away. Power spectral density of the noise spectrum for optimization with both the whitening and optimal filters was calculated from two 50 s long data before and after the injection period. Template waveforms,  $h_\alpha(t)$ , are obtained by reading the text files of strain waveforms injected, and elongated to 64 s long by padding zeros to fit with 64 s data segments.

#### 4. Results

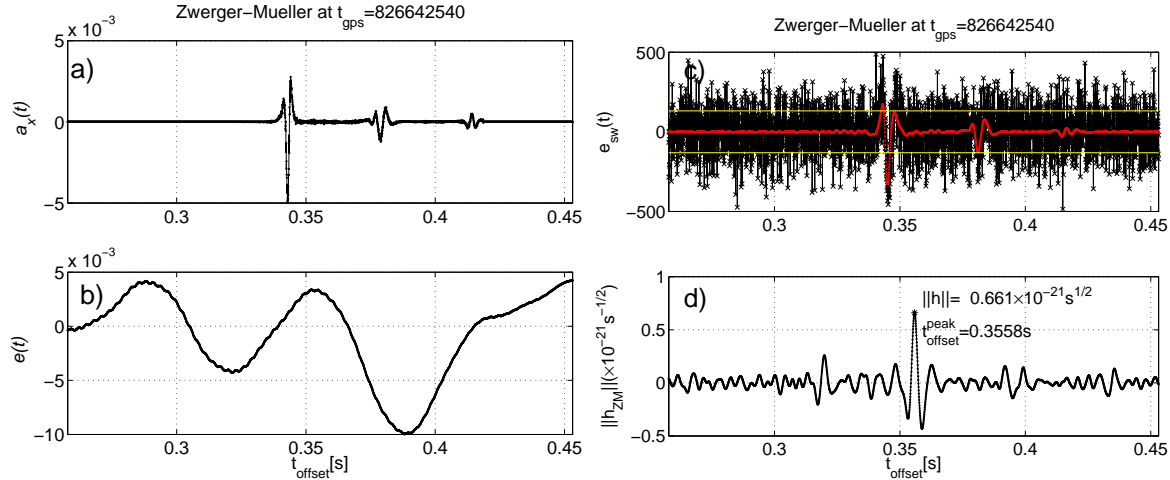
Figure 4 shows the single (a) and double (b) whitened error signal data with an injection of the Gaussian impulse shown in Fig. 2, as well as the expected curve for the injected Gaussian waveform with the same whitening filter and with the proper scaling and offsetting in time. Both whitened spectra agree well with the expected curves.

Filtered output of this same injection obtained from the optimal filter with the template of the injected Gaussian waveform is shown in Fig. 4 c) and d) in two different time scales. Figure 4 d) demonstrates how the strength and timing of injection are measured. Measured strength ( $\|h_{GA03}\| = 19.984 \times 10^{-21} \sqrt{s}$ ) and timing ( $t_{\text{offset}} = 0.5001$  s) of this injection agree with the injected values within a few percents. The root-mean-squared (RMS) of the noise level after filtering, around this injection period, is measured  $\sigma_{\text{noise}} = 0.0357 \times 10^{-21} \sqrt{s}$ , which is larger than the difference in the strength measurement.

More realistic example from an injection of a supernova waveform, Zwerger-Müller (A3B3G1) [4], is shown in Fig. 5. The injection was done with  $\|h_{ZM}\| = 0.6 \times 10^{-21} \sqrt{s}$  and  $t_{\text{offset}}^{\text{injected}} = 0.3555$  s, which is recovered with  $\|h_{ZM}\| = 0.6661 \times 10^{-21} \sqrt{s}$  ( $\sigma_{\text{noise}} =$



**Figure 4.** Output time series for an injection of the Gaussian pulse of Fig. 2 from a) single and b) double whitening filters and the optimal linear filter with two different time scales in c) and d). Measurement of strength and offset time are demonstrated in d).



**Figure 5.** Injection of Zwerger-Müller ( $A3B3G1$ ) waveforms: a) waveform injected to ETMX\_EXC, b) error signal data recorded at the channel DARM\_ERR, filtered outputs from c) single whitening filter (with the expected signal waveform from the injection) and d) the optimal filter. Measurement of strength and time offset is shown in d).

$0.0417 \times 10^{-21} \sqrt{\text{s}}$ ) and  $t_{\text{offset}}^{\text{measured}} = 0.3558$  s. It is noticeable in this example that the time measurement is the offset time, rather than the peak time of the waveform. This is the result expected from using the matched filter.

## 5. Statistical analysis

This report used hardware injections of about 8 months from January 20, 2006 to August 28, 2006, from all three interferometers in LIGO - 4 km detector (L1) at the Livingston observatory and 4 km (H1) and 2 km (H2) detectors at the Hanford observatory. During

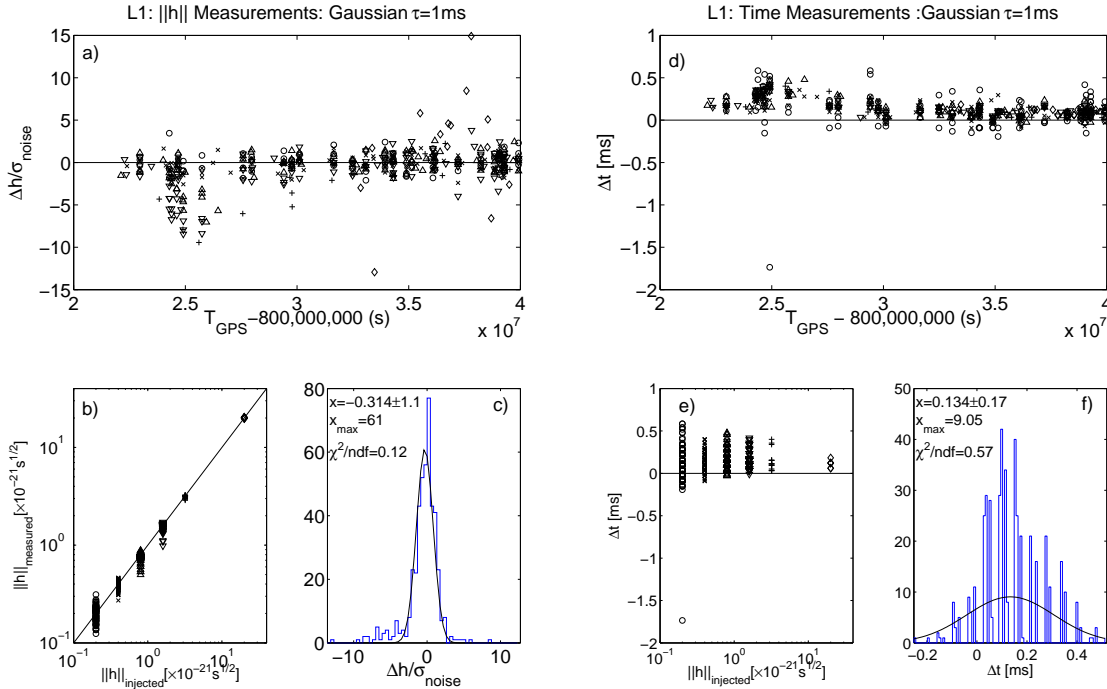
this period, total 4098 burst injections are carried out in L1 and 5018 and 5958 injections are done in H1 and H2 respectively. Table 1 shows how many injections were made for all 20 burst waveforms at each detector. Eight waveforms including a Gaussian with

**Table 1.** Numbers of hardware injections on each detector.

Injected waveform	L1	H1	H1
Gaussian $\tau = 0.3$ ms	40	48	52
Gaussian $\tau = 1$ ms	478	581	677
Gaussian $\tau = 3$ ms	40	48	52
Gaussian $\tau = 10$ ms	40	48	52
sine-Gaussian 50 Hz, $Q = 9$	34	46	58
sine-Gaussian 70 Hz, $Q = 9$	474	578	692
sine-Gaussian 100 Hz, $Q = 9$	34	46	58
sine-Gaussian 153 Hz, $Q = 9$	34	46	58
sine-Gaussian 235 Hz, $Q = 9$	472	579	683
sine-Gaussian 393 Hz, $Q = 9$	34	46	58
sine-Gaussian 554 Hz, $Q = 9$	34	46	58
sine-Gaussian 850 Hz, $Q = 9$	34	46	58
sine-Gaussian 914 Hz, $Q = 9$	440	524	634
sine-Gaussian 1304 Hz, $Q = 9$	34	46	58
sine-Gaussian 2000 Hz, $Q = 9$	472	579	683
sine-Gaussian 3068 Hz, $Q = 9$	34	46	58
Zwinger-Müller (A3B3G1)	430	527	617
Cosmic string cusp $f_{\text{cutoff}} = 220\text{Hz}$	430	527	617
Band-limit white noise, 250 Hz, $\delta f = 100$ Hz, $\sigma = 30\text{ms}$	440	524	634
Ringdown 2600 Hz, $\delta t = 30$ ms	70	95	101
Total	4098	5018	5958

$\tau = 1$  ms or sine-Gaussian with 70 Hz ( $Q = 9$ ), were injected more often and with more variety of strengths than others.

Each waveform was analyzed in terms of measurement of strength and time offset and an example of a Gaussian with the width of  $\tau = 1$  ms is shown in Fig. 6. The gps time dependence of measurements in Fig. 6 a) and d) shows that the performance of the detector can be monitored by recovering signals from hardware injections. Measurement of strengths is compared with the injected strengths in Fig. 6 b). The difference between injected and measured time offsets of injections from the injections is shown as a function of the injected strengths in Fig. 6 e). Uncertainty in strength and time measurements with this waveform can be estimated with a Gaussian fit as shown in in Fig. 6 c) and f). It is noticeable that injections with lower strengths have more fluctuations in measurements in both strengths and timings. The discreteness of the time measurement histogram in Fig. 6 is caused by a discrete estimate of arrival time.



**Figure 6.** Measurement of strengths and time of injections with a Gaussian with the width of  $\tau = 1$  ms at L1: a) gps time dependence of differences in the strength measurements ( $\Delta h \equiv ||h||_{\text{measured}} - ||h||_{\text{injected}}$ ) in term of noise level ( $\sigma_{\text{noise}}$ ), b) injected strengths vs. measured strengths of injections, c) distribution of differences of  $\Delta h/\sigma_{\text{noise}}$ , d) gps time dependence of differences of time measurements ( $\Delta t \equiv t_{\text{offset}}^{\text{measured}} - t_{\text{offset}}^{\text{injected}}$ ), e)  $\Delta t$  vs.  $||h||_{\text{injected}}$ , and f)  $\Delta t$  distribution.  $\Delta h$  is averaged  $(0.31 \pm 1.1)\sigma_{\text{noise}}$  and  $\Delta t$  is  $0.13 \pm 0.17$  ms. The same symbol assignment is used in a), b), d) and e), to show different injected strengths.

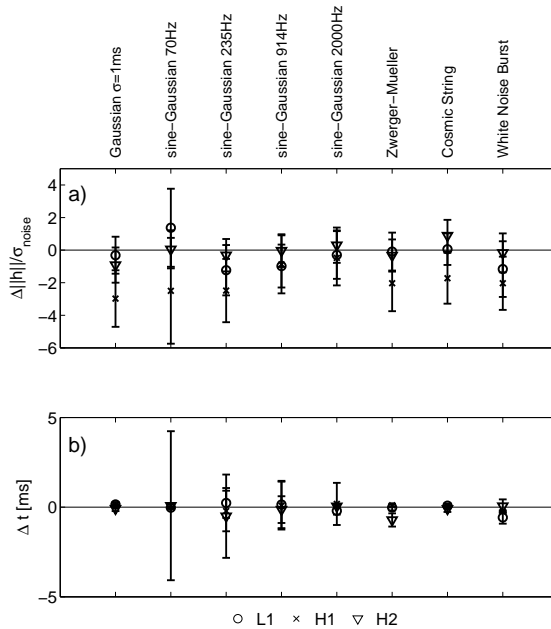
Figure 7 shows how eight injected waveform with better statistics from Table 1 is measured by all three detectors. Fluctuation in strength measurement is comparable with the noise level around injections and time measurement is in agreement within a few ms with injection time for all three detectors.

## 6. Coupling between auxiliary channels and gravitational wave channels

In the LIGO experiment many auxiliary channels are recorded as data to monitor the performance of detector and environmental changes during the experiment. These channels are not designed to detect any real signal from gravitational wave sources, so any signal candidates with excess strength in these channels can not be good candidates for gravitational wave. In other words, these auxiliary channels can be very useful to veto some events as gravitational wave candidates. However, for various reasons, it is possible that some of these channels are influenced by the signal from real gravitational wave sources if there is a coupling with the gravitational wave channel.

Hardware injection, which simulates realistic signal events into the detector,



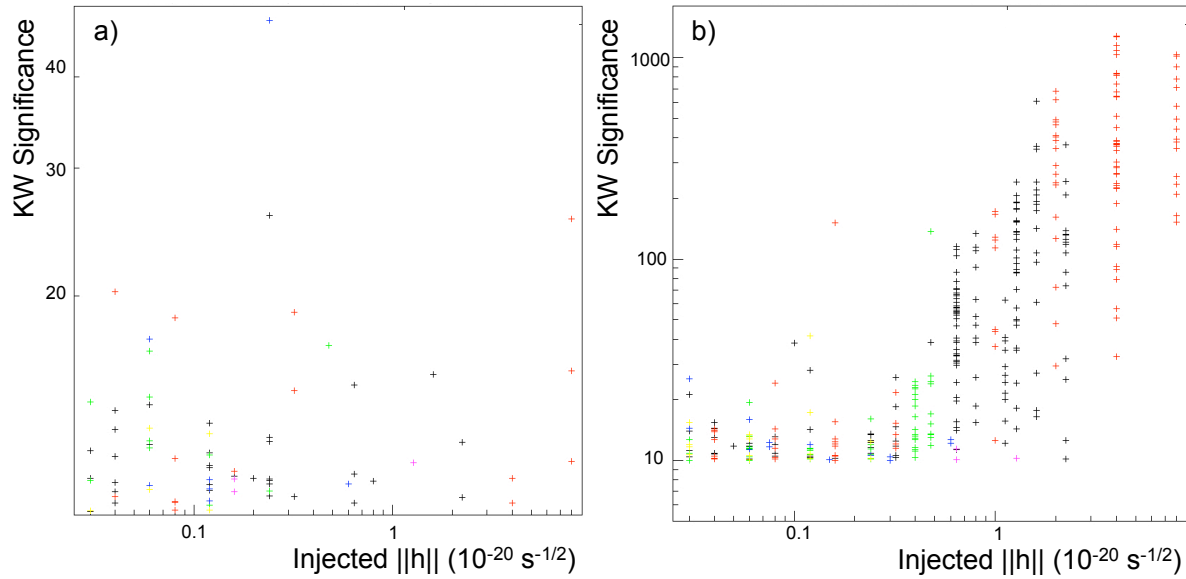


**Figure 7.** Measurement of a) strength and b) time of hardware injections for burst waveforms from three LIGO interferometers.

provides a useful tool to test whether an auxiliary channel has any coupling to the gravitational wave channel. The KleineWelle algorithm, which is developed to search for transients, was applied to many auxiliary channels at the time of injections. For this study, injections of 272 days from the S5 run were used. Some of these channels are found not suitable to be used for vetoing environmental events. Figure 8 shows significances of transient events around injection times, detected by the KleineWelle technique from two auxiliary channels, RMP and ASI, compared to injected strengths. While the events from RMP do not show noticeable dependence on injections, those from ASI have strong dependence to the injection, which indicates some coupling to gravitational channel above a certain intensity ( $\sim 2 \times 10^{-21} \sqrt{s}$ ). Timing distribution of these events also shows similar result and proves that the ASI channel has some coupling to gravitational wave channel. More detailed report on results from this study was presented in a separate talk in this conference by Erik Katsavounidis.

## 7. Summary

With this report, we demonstrate how hardware injections are useful to understand the performance of interferometers by measuring strengths of injections and time responses of detectors. Strengths and timings of the injections are measured by using filtered outputs from the optimal linear filter and compared to injected values. Hardware injections are reconstructed successfully, showing that the detector's performance is well understood. It is also shown that hardware injection is also useful to examine coupling of auxiliary channels to the gravitational wave channel.



**Figure 8.** Examples of coupling test done with auxiliary channels, a) RMP (Recycling Mirror Pitch) and b) ASI (AntiSymmetric port In Phase).

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